



Statische berekening

Projekt: ***Nieuwbouw trappenhuis aan de Manganstraat 9 te Nederweert***

Projectnummer: P21-087

Onderdeel: Hoofdberekening – t.b.v. bouwaanvraag

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| | | | | | |
|----------------|--------------|---------------|---------------------|-------------|---------------|
| | | | | | |
| 0 | 23-11-2021 | Definitief | t.b.v. bouwaanvraag | M.V. | M.V. |
| Revisie | Datum | Status | Omschrijving | Door | Gezien |

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1 Algemene gegevens

Beton: Betonkwaliteit: C20/25
Milieuklasse XC2
Consistentiegebied C3
Wapening: FeB 500 HWL voor staven en netten
Deze basisgegevens zijn van toepassing, tenzij anders aangegeven.

Staal: Staalsoort: S235JR
Elektrisch te lassen volgens nadere detailberekeningen
Boutkwaliteit: 8.8
Ankerkwaliteit : 4.6
Deze basisgegevens zijn van toepassing, tenzij anders aangegeven.

Normen: Eurocode 0 - Grondslagen van het constructief ontwerp
Eurocode 1 - Belastingen op constructies
Eurocode 2 - Ontwerp en berekening van betonconstructies
Eurocode 3 - Ontwerp en berekening van staalconstructies
Eurocode 4 - Ontwerp en berekening van staal-betonconstructies
Eurocode 5 - Ontwerp en berekening van houtconstructies
Eurocode 6 - Ontwerp en berekening van constructies van metselwerk
Eurocode 7 - Geotechnisch ontwerp

Software: Word - Tekstverwerking
Excel - Spreadsheetprogramma
Buildsoft: - Diamonds 2018
Technosoft: - Raamwerken V6
- Construct V6
AutoCAD LT2019 - Tekeningen

2 Ontwerpparameters

| Ontwerplevensduur (NEN-EN1990, bijlage A1.1, tabel 2.1) | | |
|---|---------------------------|--|
| Ontwerplevensduurklasse | Ontwerplevensduur [jaren] | Toepassing |
| 3 | 50 | Gebouwen en andere gewone constructies |

| Definitie van gevolklassen (NEN-EN1990, bijlage B3.1, tabel B1) | | |
|---|--|-------------|
| Gevolklasse | Omschrijving | Toepassing |
| CC2 | Middelmatige gevolgen t.a.v. het verlies van mensenlevens, en/of aanzienlijke economische of sociale gevolgen voor de omgeving | Trappenhuis |

| K _{FI} faktor voor belastingen (NEN-EN 1990, bijlage B3.3, tabel B3) | | |
|---|------------------------|-----------------|
| Gevolklasse | Betrouwbaarheidsklasse | K _{FI} |
| CC2 | RC2 | 1,0 |

Fundamentele combinaties (NEN-EN 1990, art. 6.4.3.2):

Formule 6.10a: $\Sigma(\gamma_{G,j} * G_{k,j}) + \gamma_p * P + \gamma_{Q,1} * \psi_{0,1} * Q_{k,1} + \Sigma(\gamma_{Q,i} * \psi_{0,i} * Q_{k,i})$

Formule 6.10b: $\Sigma(\xi * \gamma_{G,j} * G_{k,j}) + \gamma_p * P + \gamma_{Q,1} * Q_{k,1} + \Sigma(\gamma_{Q,i} * \psi_{0,i} * Q_{k,i})$

Belastingfactoren:

| | | | | |
|------------------------------------|------------|---|------------|--------------|
| Permanente belastingen | γ_G | = | 1,35 / 0.9 | |
| Reductiefactor blijvende belasting | ξ | = | 0.89 | (volgens NB) |
| Veranderlijke belastingen | γ_Q | = | 1,5 | |

| Rekenwaarden van belastingen (STR/GEO) (Groep B) (NEN-EN1990, bijlage A1.3.1, tabel A1.2(B)) | | | |
|---|--------------|-------------|--------------|
| | permanent | | Veranderlijk |
| | ongunstig | gunstig | |
| Formule 6.10a | $1,35 * G_k$ | $0,9 * G_k$ | $1,50 * Q_k$ |
| Formule 6.10b | $1,20 * G_k$ | $0,9 * G_k$ | $1,50 * Q_k$ |

3 Belastingen

| Plat dak hoog: | | | | | |
|--------------------|------------------------|--|---|--------------------|----------------------------|
| | Type | | : | Stalen dakplaat | |
| | Helling | | : | 1,0 ° | |
| g _k : | Eigen gewicht | | : | 0,10 /cos 1,0 | = 0,10 kN/m ² |
| | Afwerklaag | <input checked="" type="checkbox"/> | : | 0,20 /cos 1,0 | = 0,20 kN/m ² |
| | PIR isolatie 160 mm | <input checked="" type="checkbox"/> | : | 0,05 /cos 1,0 | = 0,05 kN/m ² |
| | Zonnepanelen + ballast | <input checked="" type="checkbox"/> | : | 0,20 /cos 1,0 | = 0,20 kN/m ² |
| | | | | g _{k,tot} | = 0,55 kN/m ² + |
| q _{k,s} : | | s _k *μ ₁ *C _e *C _t | : | 0,7*0,8*1*1 | = 0,56 kN/m ² |
| | | α ≤ 30° μ ₁ | : | 0,8 | |

Trap / Bordes: type: Prefab balkonplaat-vlgs fabrikant/leverancier

| | | | | |
|--------------------|--|------|-------------------|--|
| G _{rep} : | eigengewicht: | 5.00 | kN/m ² | |
| | plafond: | 0.00 | kN/m ² | |
| | afwerklaag: | 0.00 | kN/m ² | = 5.00 kN/m ² |
| q _k : | NEN-EN 1991-1-1, NB.1-6.2-gebruiksklasse A | = | 2.50 | kN/m ² (ψ ₀ =0.40) |

| Plat dak laag: | | | | | |
|------------------|---|--|---|--------------------|--|
| | Type | | : | Balklaag | |
| g _k : | Eigen gewicht | | : | = 0,35 | kN/m ² |
| | Geen zonnepanelen!! | | : | = 0,00 | kN/m ² |
| | Afwerklaag + isolatie | | : | = 0,20 | kN/m ² |
| | Plafond 0,10 kN/m ² | | : | = 0,10 | kN/m ² |
| | | | | g _{k,tot} | = 0,65 kN/m ² + |
| q _k : | NEN-EN 1991-1-1, NB.1 - 6.10 - gebruiksklasse H | | | = | 1,00 kN/m ² Ψ ₀ = 0,00 |

| Windlasten gevels: | | | | | |
|--------------------|---|-----|---|------------------|------------------------|
| Windgebied | : | III | | Onbebouwd | |
| Hoogte | : | 7 | m | q _p = | 0,62 kN/m ² |
| h/d ≤ | : | 1 | C _{pe} : druk = 0,8; zuiging = 0,5 | | |

| | | | |
|---|---|------|-------------------|
| Beton: gewapend/ongewapend | = | 24.0 | kN/m ³ |
| Prefab beton gewapend | = | 25.0 | kN/m ³ |
| Metselwerk: steens/spouw | = | 4.0 | kN/m ² |
| halfsteens | = | 2.0 | kN/m ² |
| kalkzandsteen d = 100 mm | = | 2.0 | kN/m ² |
| kalkzandsteen d = 150 mm | = | 3.0 | kN/m ² |
| kalkzandsteen d = 214 mm | = | 4.0 | kN/m ² |
| gasbeton | = | 8.0 | kN/m ³ |
| Kozijnen (incl beglazing/deuren) | = | 0.8 | kN/m ² |
| Stalen damwand gevelbeplating + binnendozen | = | 0.30 | kN/m ² |
| <i>indien belasting gunstig werkt:</i> | = | 0.15 | kN/m ² |
| Geïsoleerde prefab betonplint 200 mm dik | = | 4.00 | kN/m ² |

indien belasting gunstig werkt: = 3.50 kN/m²

4 Compartimentering

Er zijn op de bestektekening geen eisen aangegeven t.a.v. compartimentering.

Het gehele gebouw is gerekend als 1 compartiment.

5 Brandwerendheid

De eisen t.a.v. brandwerendheid dienen te worden aangegeven door de architect.

In dit geval zijn er geen eisen t.a.v. brandwerendheid aangegeven.

Er is bij de berekening van de hoofdconstructie-onderdelen geen rekening gehouden met brandwerendheidseisen. Om aan eventuele brandwerendheidseisen te voldoen dienen de nodige hoofdconstructieonderdelen brandwerend bekleed te worden of voorzien te worden van brandwerende conservering.

6 Houtprofielen

6.1 Balklaag plat dak laag

Geen grind gerekend !!
 Toepassen: B*H = 59x146mm – doorgaand C18 h.o.h. max 610 mm
 Balklaag vrankeren aan metselwerk d.m.v. balklaagankers (rondom)
 Stalen oplegschoenen volgens tekening en berekening fabrikant
 Volgplaten: Toepassen bij alle te bouten houtverbindingen
 - strip 30*2 lg 30 mm bij bouten M8 en M10
 - strip 40*3 lg 40 mm bij bouten M12, M16 en M20
 (tenzij anders aangegeven)
 Hout-op-hout-verbindingen uitvoeren d.m.v. stalen hoeken
 Alle houtverbindingen uitvoeren volgens Eurocode 5

Technosoft Construct release 6.70a

23 nov 2021

Eenheden : kN/m/rad

Toegepaste normen volgens Eurocode met Nederlandse NB

| | | | |
|-------------|----------------------|------------------|--------------|
| Belastingen | NEN-EN 1990:2002 | C2:2010 | NB:2011 (nl) |
| | NEN-EN 1991-1-1:2002 | C1:2009 | NB:2011 (nl) |
| | NEN-EN 1991-1-3:2003 | C1:2009 | NB:2011 (nl) |
| | NEN-EN 1991-1-4:2005 | C2:2011 | NB:2011 (nl) |
| Hout | NEN-EN 1995-1-1:2005 | A1:2011, C1:2006 | NB:2013 (nl) |
| | NEN-EN 14080:2013 | | |

Balklaag plat dak

platdak

Algemene gegevens

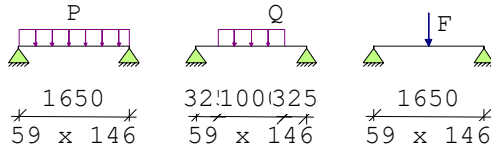
| | | | | | |
|-----------------------|------|------------------------|------------------------|----------------------|-----------|
| B x H | [mm] | : 59 x 146 | Sterkteklasse | : | C18 |
| Overspanning | [mm] | : 1650 | Klimaatklasse | : | I |
| Aantal zijdl. steunen | : | - | Referentie periode [j] | : | 50 |
| Opleglengte | [mm] | : 100 | | | |
| Hoh in het dakvlak | [mm] | : 610 | | | |
| Helling | : | : 0.00 | | | |
| Beschot sterkteklasse | : | : C18 | | | |
| Dikte beschot | [mm] | : 12 | $E_{0, mean} \times I$ | [Nm ² /m] | : 1296.0 |
| Windgebied | : | : 3 | Terrein | : | Onbebouwd |
| Gebouw L x B x H | [m] | : 10.00 x 10.00 x 3.20 | | | |

Permanente belastingen G_{rep}

| | | |
|-----------------------------|---|--------|
| EG balklaag | : | : 0.65 |
| Isolatie | : | : 0.00 |
| Extra gewicht | : | : 0.00 |
| Totaal [kN/m ²] | : | : 0.65 |

Veranderlijke belastingen

| | | | |
|---------------------------|----------------------|---|--|
| Q_k | [kN/m ²] | : | : 1.00 |
| Q_k | [kN/m] | : | : 2.00 |
| Q_k | [kN] | : | : 2.00 |
| Q_k oppervlak | [m ²] | : | : 0.05 x 0.05 |
| Reductiefactor | : | : | : 0.83 |
| Wind $Q_{p, prob}$ | [kN/m ²] | : | : 0.49 (= $C_{prob}^2 * Q_p = 1.00^2 * 0.49$) |
| Sneeuw vormfactor μ_1 | : | : | : 2.86 |



Belastingfactoren (NEN-EN 1990 - Bijlage A1.3)

Formule 6.10a: $\gamma_G : 1.35$ $\gamma_Q : 1.50$

Formule 6.10b: $\xi\gamma_G : 1.20$ $\gamma_Q : 1.50$

Perm.bel. gunstig : 0.90

Partiële factor (Tabel 2.3 NEN-EN 1995-1-1)

$\gamma_M [-]$: 1.30

Stabiliteit

1. Toetsing kipstabiliteit m.b.t. montagefase volgens par.6.3.3. is n.v.t.:
- u hebt het belastingsgeval 'Uitvoering' niet toegepast.

2. Factoren t.b.v. toetsing kipstabiliteit m.b.t. gebruiksfase volgens par.6.3.3:
Belastingcombinatie wind omhoog (opbuigend moment):

$\kappa_{crit,y} [-]$: 1.00 frm(6.34)

Resultaten (maatgevende combinaties)

| | | eis | u.c. |
|-------------------|------------------------|--------------------------------------|------|
| Geconc. belasting | frm(6.13) $\tau_{v,d}$ | $= 0.46 < 2.09$ [N/mm ²] | 0.22 |

| | | | |
|-------------------|---|--|--|
| Geconc. belasting | frm(6.3) $\sigma_{c,90,q,d} / (k_{c,90,q} * f_{c,90,d}) +$ $\sigma_{c,90,F,d} / (k_{c,90,F} * f_{c,90,d})$ | < 1.00 $= 0.07 / 1.35 + 0.51 / 2.03 = 0.30$ | |
|-------------------|---|--|--|

| | | | |
|-------------------|----------------------------|---------------------------------------|------|
| Geconc. belasting | frm(6.11) $\sigma_{m,y,d}$ | $= 5.69 < 11.14$ [N/mm ²] | 0.51 |
|-------------------|----------------------------|---------------------------------------|------|

Let op: bij 1 of meerdere belastingcombinaties wind treedt een opwaartse oplegreactie op. Houdt hiermee rekening in het ontwerp van de oplegverbinding.

| | | | |
|----------|---------------|----------------------|------|
| Lijnlast | u_{bij} | $= 1.31 < 6.60$ [mm] | 0.20 |
| Lijnlast | $u_{net,fin}$ | $= 1.59 < 6.60$ [mm] | 0.24 |

7 Stabiliteit

In 1 richting verkrijgt het gebouw stabiliteit uit ongeschoorde portalen. In de andere richting verkrijgt het gebouw stabiliteit uit het bestaande gebouw. De constructie wordt zowel op vloerniveau als op dakniveau aan de bestaande constructie gekoppeld

7.1 Wind loodrecht op as

Windgebied III, onbebouwd

$q_{p;wind}$

$$= 0.62 \text{ kN/m}^2$$

7.1.1 Windverband dakvlak

Gebouwbreedte: 3.35 m

Gebouwlengte: 5.25 m

Er is 1 windverbandvak. Uitgangspunt is dat het windverbandvak in staat is de gehele windbelasting op te nemen.

$$\begin{aligned}
 q_{k;wind}: \quad \text{winddruk:} & \quad (0.5 \cdot 3.3 + 0.5) \cdot 0.62 \cdot 0.8 & = & 1.07 \text{ kN/m} \\
 & \text{windzuiging:} & (0.5 \cdot 3.3 + 0.5) \cdot 0.62 \cdot 0.5 & = 0.67 \text{ kN/m} \\
 & \text{windwrijving:} & 5.25 \cdot 0.02 \cdot 0.62 & = 0.07 \text{ kN/m} + \\
 & & & \underline{=} 1.81 \text{ kN/m} \\
 q_{k;wind;totaal} & & & = 1.81 \text{ kN/m}
 \end{aligned}$$

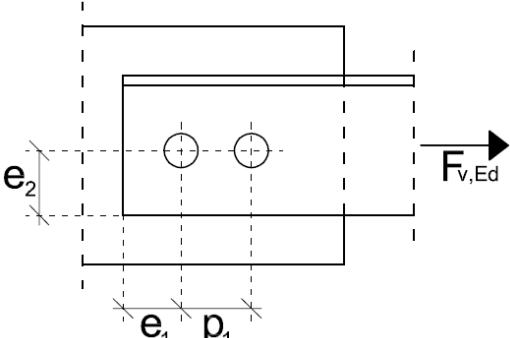
Dit geeft een reactiekracht t.p.v. as 1 & 2:

$$R_{k;1\&2} = 1.81 \cdot 0.5 \cdot 3.35 = 3.03 \text{ kN}$$

Maximale trek in windverband:

$$N_d = 1.81 \cdot 0.5 \cdot 3.35 \cdot 1.50 \cdot \sqrt{2} = 6.43 \text{ kN}$$

Berekening boutverbinding: bout-hoekprofiel (enkelsnedig)

| Gegevens | | | |
|---|--|-------------------------------------|---|
| Max. trekkracht, $F_{v,Ed}$ | = 6,43 | kN |  |
| Bout afmeting | = M12 | | |
| Aantal bouten, n | = 2 | | |
| Boutklasse | = 8.8 | | |
| Profielbenaming | = H50/50/5 | | |
| Staalsoort hoekprofiel | = S235 | | |
| e_1 | = 25 | mm (Voldoet) | |
| e_2 | = 25 | mm (Voldoet) | |
| p_1 | = 50 | mm (Voldoet) | |
| Type gat(en) | = Normaal gat | | |
| Toetsing afschuifweerstand bout(en) | | $F_{v,Ed} / F_{v,Rd} = 0,10$ | VOLDOET |
| Het afschuifvlak gaat door de draad van de bout | | | |
| $F_{v,Rd}$ ($f_{ub} \leq 800 \text{ N/mm}^2$) | = $0,6 \cdot f_{ub} \cdot A_s \cdot n / \gamma_{M2}$ | = 65 kN | |
| Toetsing stuikweerstand hoekprofiel | | $F_{v,Ed} / F_{b,Rd} \leq 1 = 0,12$ | VOLDOET |
| $F_{b,Rd}$ | = $k_1 \cdot \alpha_b \cdot f_u \cdot d \cdot t \cdot n / \gamma_{M2}$ | = 55 kN | |
| Toetsing trekweerstand hoekprofiel | | $F_{v,Ed} / N_{u,Rd} \leq 1 = 0,10$ | VOLDOET |
| $N_{u,Rd}$ | = $\beta_2 \cdot A_{netto} \cdot f_u / \gamma_{M2}$ | = 67 kN | |

Toepassen: H50/50/5 2 M12 - 8.8 aan iedere zijde

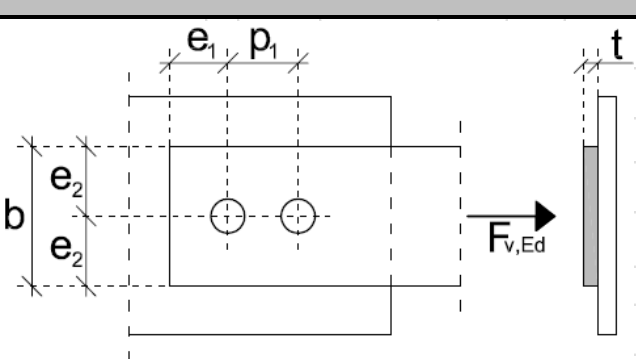
7.1.2 Verticaal verband as 1&2 – boven 1e VV

$$\begin{aligned}
 Q_{k;wind}: \quad & \text{dakvlak:} & & = & 3.03 \text{ kN} \\
 & \text{wrijving gevel:} & (0.5 \cdot 3.3 + 0.5) \cdot 5.25 \cdot 0.02 \cdot 0.62 & = & \underline{0.14 \text{ kN}} \\
 & & Q_{k;wind;totaal} & = & 3.17 \text{ kN}
 \end{aligned}$$

Hoogte windbok: 3.30 m
 Breedte windbok: 2.48 m
 Diagonaal: 4.13 m
 Aantal: 1 stuks

$$N_d = 3.17 / 1 \cdot 1.50 \cdot 4.13 / 2.48 = 7.92 \text{ kN}$$

Berekening boutverbinding: bout-strip (enkelsnedig)

| Gegevens | | | |
|--|--|---|----------------|
| Max. trekkracht, $F_{v,Ed}$ | = 7,92 kN |  | |
| Bout afmeting | = M12 | | |
| Aantal bouten, n | = 2 | | |
| Boutklasse | = 8.8 | | |
| Staalsoort strip | = S235 | | |
| b | = 50 mm | | |
| t | = 8 mm | | |
| e_1 | = 25 mm (Voldoet) | | |
| e_2 | = 25 mm (Voldoet) | | |
| p_1 | = 50 mm (Voldoet) | | |
| Type gat(en) | = Normaal gat | | |
| Toetsing afschuifweerstand bout(en) | | $F_{v,Ed} / F_{v,Rd} = 0,09$ | VOLDOET |
| Het afschuifvlak gaat door de | | schacht | van de bout |
| $F_{v,Rd}$ | $= 0,6 \cdot f_{ub} \cdot A_n / \gamma_{M2}$ | = 87 kN | |
| Toetsing stuikweerstand strip | | $F_{v,Ed} / F_{b,Rd} \leq 1 = 0,09$ | VOLDOET |
| $F_{b,Rd}$ | $= k_1 \cdot \alpha_b \cdot f_u \cdot d \cdot t \cdot n / \gamma_{M2}$ | = 89 kN | |
| Toetsing trekweerstand strip | | $F_{v,Ed} / N_{u,Rd} \leq 1 = 0,10$ | VOLDOET |
| De bout(en) hebben een | | normale zeskant kop | |
| $N_{u,Rd}$ | $= 0,9 \cdot A_{netto} \cdot f_u / \gamma_{M2}$ | = 77 kN | |

Toepassen: Er komt geen verticaal verband afsteunen tegen bestaande randligger HEA120 bestaand gebouw
 $Q_k = 3.17 \text{ kN}$

$$\text{Maximale trek/druk op 1}^e \text{ V.V.: } F_d = 3.17 / 1 \cdot 1.50 \cdot 3.3 / 2.48 \approx 6.33 \text{ kN}$$

7.1.3 Koppelkokers

Er moeten koppelkokers worden aangebracht op de overgang van kolom naar dakligger.

$$\begin{array}{rclcl} Q_{k;\text{wind}} & & = & 3.17 & \text{kN} \\ M_{k;t.g.v. \text{ excentriciteit}} & = & 0.04 * 3.17 & \approx & 0.13 \text{ kNm} \\ L & & = & 2.48 & \text{m} \end{array}$$

Toepassen: geen koppelkokers – deze belasting komt in de dakliggers op as 1&2

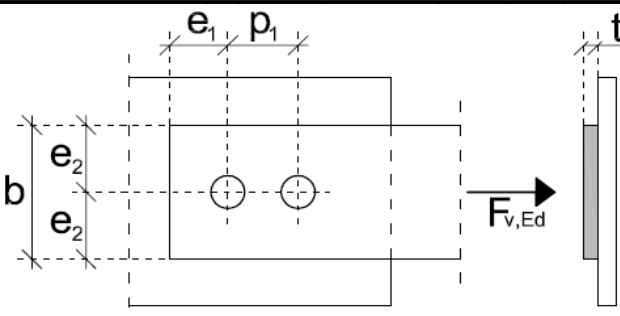
7.1.4 Verticaal verband as 1&2 – begane grond

Er wordt 3% van de veranderlijke belasting meegenomen als kracht in de verticale verbanden.

| | | | |
|----------------|----------------------|--|-----------|
| $Q_{k,wind}$: | dakvlak+wr.gevel: | = | 3.17 kN |
| | 1 ^e V.V.: | $0.5 \cdot 3.35 \cdot 3.3 \cdot 0.62 \cdot (0.8 + 0.5)$ | = 4.46 kN |
| | wr. gevel: | $3.30 \cdot 5.25 \cdot 0.02 \cdot 0.62$ | = 0.22 kN |
| | sch.st vl.: | $2.50 \cdot 0.5 \cdot (4.42 + 4.76 + 2 \cdot 2.79) \cdot 0.03$ | = 0.55 kN |
| | $Q_{k,wind;totaal}$ | = | 8.40 kN |

Hoogte windbok: 3.75 m
Breedte windbok: 2.48 m
Diagonaal: 4.50 m
Aantal: 1 stuks

$$N_d = 8.40 / 1 \cdot 1.50 \cdot 4.50 / 2.48 = 22.86 \text{ kN}$$

| Berekening boutverbinding: bout-strip (enkelsnedig) | | | |
|---|--|-------------|----------------|
| Gegevens | | | |
| Max. trekkracht, $F_{v,Ed}$ | = | 22,9 kN | |
| Bout afmeting | = | M12 | |
| Aantal bouten, n | = | 2 | |
| Boutklasse | = | 8.8 | |
| Staalsoort strip | = | S235 | |
| b | = | 50 mm | |
| t | = | 8 mm | |
| e_1 | = | 25 mm | (Voldoet) |
| e_2 | = | 25 mm | (Voldoet) |
| p_1 | = | 50 mm | (Voldoet) |
| Type gat(en) | = | Normaal gat | |
|  | | | |
| Toetsing afschuifweerstand bout(en) | $F_{v,Ed} / F_{v,Rd}$ | = 0,26 | VOLDOET |
| Het afschuifvlak gaat door de | schacht | van de bout | |
| $F_{v,Rd}$ | = $0,6 \cdot f_{ub} \cdot A^* \cdot n / \gamma_{M2}$ | = 87 kN | |
| Toetsing stuikweerstand strip | $F_{v,Ed} / F_{b,Rd} \leq 1$ | = 0,26 | VOLDOET |
| $F_{b,Rd}$ | = $k_1 \cdot \alpha_b \cdot f_u \cdot d^* \cdot t^* \cdot n / \gamma_{M2}$ | = 89 kN | |
| Toetsing trekweerstand strip | $F_{v,Ed} / N_{u,Rd} \leq 1$ | = 0,30 | VOLDOET |
| De bout(en) hebben een | normale zeskant kop | | |
| $N_{u,Rd}$ | = $0,9 \cdot A_{netto} \cdot f_u / \gamma_{M2}$ | = 77 kN | |

Toepassen: Er komt geen verticaal verband afsteunen tegen bestaande vloerligger HEA220 bestaand gebouw

$$Q_k = 8.4-3.17 \approx 5.23 \text{ kN}$$

Maximale trek/druk op fundering uit wind/scheefstand vloer:

$$F_d = 8.40/1*1.5*3.75/2.48 \approx 19.05 \text{ kN}$$

(zonder permanente belasting!!)

Ankers:

$$N_{v;s;d} = 12.60 \text{ kN}$$

$$N_{t;s;d} = 19.05 \text{ kN}$$

$$4 \text{ M16-4.6-gerolde draad: } F_{vb;Rd} = 4*18.50 \approx 74.0 \text{ kN} \rightarrow \text{akkoord}$$

$$N_{t;u;d} = 4*27.1 \approx 108.4 \text{ kN} \rightarrow \text{akkoord}$$

Gerekend is met het plaatsen van het verticaal verband centrisch t.o.v. centrum van de boutgroep. Indien dit anders is, ankers nog nader te bepalen/controleren !!

8 Ongeschoord portaal as A

8.1 Belasting t.g.v. permanente belasting

Belastinggeval 1 t.g.v permanente belastingen

$G_{k;dak}$: $0.55 \cdot 0.5 \cdot 2.47$ = 0.68 kN/m

$G_{k;tussenbordes}$: = 11.80 kN

Eigengewicht van de profielen wordt automatisch gegenereerd.

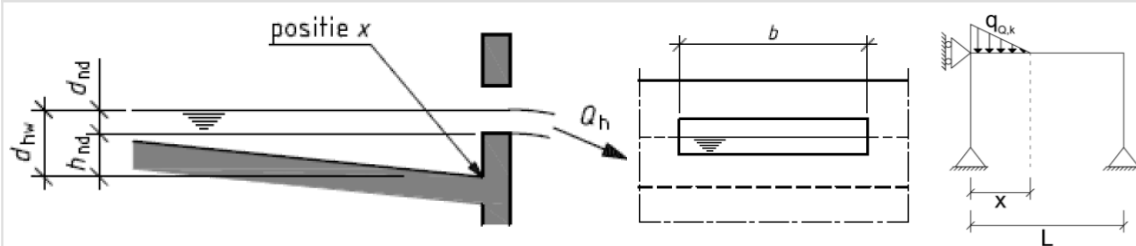
8.2 Belasting t.g.v. wateraccumulatie

Wateraccumulatie:

Min. afschot: 16 mm/m*3.15 \approx 55 mm

| Wateraccumulatie | | | |
|---|--|------------|---------------------------------|
| Referentieperiode | = | 50 | jaar |
| Neerslagintensiteit | $i_r =$ | 0,05 | $\cdot 10^{-3}$ m/s |
| Breedte dakvlak | $B =$ | 3,15 | m |
| Lengte dakvlak | $L =$ | 5,25 | m |
| Afschotzijden | = | 1 | |
| Aantal noodafvoeren per zijde | = | 1 | st. |
| Oppervlakte per noodafvoer | $A =$ | 16,6 | m^2 |
| Gekozen breedte noodafvoer | $b =$ | 0,30 | m |
| Maximaal toegestane waterhoogte t.p.v. het laagste punt | = | 0,08 | m (0,08 m is een veilige keuze) |
| Gekozen hoogte van de noodafvoer boven de dakrand of het dakvlak | $h_{nd} =$ | 0,03 | m (normaal 0,03 m) |
| Overspanning dakplaten | $L_t =$ | 2,47 | m |
| Afschot | = | 16,0 | mm/m |
| Volumieke gewicht van water | $\gamma_w =$ | 10,0 | kN/m^3 |
| Factor t.g.v. meervelds dakplaten | $\psi_0 =$ | 1,25 | |
| Q_h | = $A \cdot i_r$ | = 0,0009 | m^3/s |
| d_{nd} | = $0,70 \cdot (Q_h/b)^{2/3}$ | = 14,6 | mm |
| d_{nd} is de maximale waterhoogte boven de onderzijde van de noodafvoer | | | |
| d_{hw} | = $d_{nd} + h_{nd}$ | = 44,6 | mm |
| d_{hw} is de maximale waterhoogte ter plaatse van de dakrand | | | |
| d_n | = $0,004 \cdot L_t$ | = 9,9 | mm |
| d_n is de extra waterhoogte door de doorbuiging van het dakvlak | | | |
| $q_{Q,k}$ | = $(d_{hw} + d_n) \cdot \gamma_w \cdot L_t \cdot \psi_0$ | = 1,69 | kN/m |
| x | = $(d_{hw} + d_n) / (\text{afschot} \cdot L) / L$ | = 3,41 | m |
| Minimale afmetingen noodafvoer: | | | |
| $h \times b$ | = $(d_{nd} + 50 \text{ mm}) \times b$ | = 65 x 300 | mm x mm |

Er is rekening gehouden met 50 mm vrije hoogte boven de bepaalde waterhoogte i.v.m. verstopping



Aandachtspunt:

Noodafvoeren mogen niet op een gesloten (riool-)afvoersysteem worden aangesloten.

NA: HxB = 100x300 mm

8.3 Belasting t.g.v. sneeuw

Belastinggeval 3 t.g.v. sneeuw

Belastingbreedte voor sneeuw: = 1.24 m

8.4 Belasting t.g.v. veranderlijke vloerbelasting

Belastinggeval 3 t.g.v. veranderlijke vloerbelasting

$Q_{k;tussenbordes}$: = 5.78 kN

8.5 Uitvoer as A

| | |
|-----------------------|------------------------|
| Toepassen: Dakligger: | HEA140 |
| | afschot 1-zijdig 55 mm |
| Vloerligger: | HEA140 |
| Kolommen: | HEA160 |

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Dimensies....: kN;m;rad (tenzij anders aangegeven)

Belastingbreedte.: 1.240

Rekenmodel.....: 1e-orde-elastisch.

Theorie voor de bepaling van de krachtsverdeling:

Geometrisch lineair.

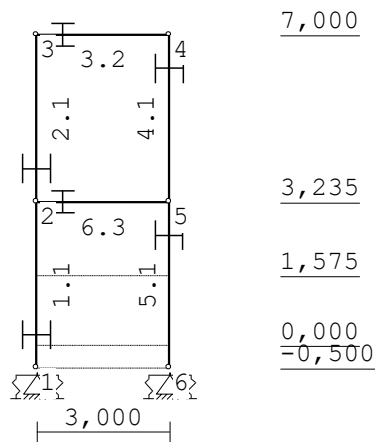
Fysisch lineair.

Gunstige werking van de permanente belasting wordt automatisch verwerkt.

Toegepaste normen volgens Eurocode met Nederlandse NB

| | | | |
|-------------|--------------------------|-----------------|-------------|
| Belastingen | NEN-EN 1990:2002 | C2:2010,A1:2019 | NB:2019(nl) |
| | NEN-EN 1991-1-1:2002 | C1/C11:2019 | NB:2019(nl) |
| | NEN-EN 1991-1-3:2003 | C1:2009 | NB:2011(nl) |
| | NEN-EN 1991-1-4:2005 | C2:2011 | NB:2011(nl) |
| Beton | NEN-EN 1992-1-1:2011(nl) | C2/A1:2015(nl) | NB:2016(nl) |
| Staal | NEN-EN 1993-1-1:2006 | C2:2011,A1:2016 | NB:2016(nl) |
| | NEN-EN 1993-1-8:2006 | C2:2009 | NB:2011(nl) |

GEOMETRIE



STRAMIENLIJNEN

| Nr. | Naam | X | Z-min | Z-max |
|-----|------|-------|--------|-------|
| 1 | | 0.000 | -0.500 | 7.000 |
| 2 | | 3.000 | -0.500 | 7.000 |

NIVEAUS

| Nr. | Z | X-min | X-max |
|-----|--------|-------|-------|
| 1 | -0.500 | 0.000 | 3.000 |
| 2 | 0.000 | 0.000 | 3.000 |
| 3 | 1.575 | 0.000 | 3.000 |
| 4 | 3.235 | 0.000 | 3.000 |
| 5 | 7.000 | 0.000 | 3.000 |

MATERIALEN

| Mt | Kwaliteit | E-modulus [N/mm ²] | S.G. | Pois. | Uitz. coëff |
|----|-----------|--------------------------------|------|-------|-------------|
| 1 | S235 | 210000 | 78.5 | 0.30 | 1.2000e-05 |

PROFIELEN [mm]

| Prof. | Omschrijving | Materiaal | Oppervlak | Traagheid | Vormf. |
|-------|--------------|-----------|------------|------------|--------|
| 1 | HEA160 | 1:S235 | 3.8800e+03 | 1.6730e+07 | 0.00 |
| 2 | HEA140 | 1:S235 | 3.1420e+03 | 1.0330e+07 | 0.00 |
| 3 | HEA140 | 1:S235 | 3.1420e+03 | 1.0330e+07 | 0.00 |

PROFIELEN vervolg [mm]

| Prof. | Staaftype | Breedte | Hoogte | e | Type | b1 | h1 | b2 | h2 |
|-------|-----------|---------|--------|------|------|----|----|----|----|
| 1 | 0:Normaal | 160 | 152 | 76.0 | | | | | |
| 2 | 0:Normaal | 140 | 133 | 66.5 | | | | | |
| 3 | 0:Normaal | 140 | 133 | 66.5 | | | | | |

PROFIELVORMEN [mm]

1 HEA160



2 HEA140



3 HEA140



KNOPEN

| Knoop | X | Z | Knoop | X | Z |
|-------|-------|--------|-------|-------|--------|
| 1 | 0.000 | -0.500 | 6 | 3.000 | -0.500 |
| 2 | 0.000 | 3.235 | | | |
| 3 | 0.000 | 7.000 | | | |
| 4 | 3.000 | 7.000 | | | |
| 5 | 3.000 | 3.235 | | | |

STAVEN

| St. | ki | kj | Profiel | Aansl.i | Aansl.j | Lengte |
|-----|----|----|----------|---------|-----------|---------|
| 1 | 1 | 2 | 1:HEA160 | NDV | NDM | 3.735 2 |
| 2 | 2 | 3 | 1:HEA160 | NDM | NDM | 3.765 |
| 3 | 3 | 4 | 2:HEA140 | NDV | NDV | 3.000 2 |
| 4 | 4 | 5 | 1:HEA160 | NDM | NDM | 3.765 |
| 5 | 5 | 6 | 1:HEA160 | NDM | NDV | 3.735 2 |
| 6 | 2 | 5 | 3:HEA140 | NDV | NDV | 3.000 2 |

Opmerkingen

[2] De momentveerwaarde is vastgelegd met een tri-lineair moment-veerstijfheidsdiagram volgens onderstaande tabel

STAVEN (vervolg - tri-lineair moment-veerstijfheidsdiagram)

| St. | Kn. | Mvud | Cvud | Cvsd (Mvud/1.2) | Cvsd (Mvud/1.5) |
|-----|-----|-------|------|-----------------|-----------------|
| 1 | 1 | 11.11 | 555 | 907 | 1658 |
| 3 | 3 | 12.46 | 869 | 1421 | 2596 |

| | | | | | |
|---|---|-------|-----|------|------|
| | 4 | 12.46 | 869 | 1421 | 2596 |
| 5 | 6 | 11.11 | 555 | 907 | 1658 |
| 6 | 2 | 13.10 | 869 | 1421 | 2596 |
| | 5 | 13.10 | 869 | 1421 | 2596 |

VASTE STEUNPUNTEN

| Nr. knoop | Kode | XZR 1=vast 0=vrij | Hoek |
|-----------|-------|-------------------|------|
| 1 | 1 110 | | 0.00 |
| 2 | 6 110 | | 0.00 |

VEREN

| Veer | Knoop | Richting | Hoek | Veerwaarde | Type | Ondergrens | Bovengrens |
|------|-------|-----------|------|------------|---------|------------|------------|
| 1 | 1 | 3:Rotatie | 0.00 | 5.000e+02 | Normaal | -1.000e+10 | 1.000e+10 |
| 2 | 6 | 3:Rotatie | 0.00 | 5.000e+02 | Normaal | -1.000e+10 | 1.000e+10 |

BELASTINGENERATIE ALGEMEEN.

| | | | |
|------------------------------|------|-------------------------|------|
| Betrouwbaarheidsklasse.....: | 2 | Referentieperiode.....: | 50 |
| Gebouwdiepte.....: | 4.94 | Gebouwhoogte.....: | 7.00 |
| Niveau aansl.terrein.....: | 0.00 | E.g. scheid.w. [kN/m2]: | 1.20 |

WIND

| | |
|-----------------------------------|----------------------------------|
| Terrein categorie ...[4.3.2]....: | Onbebouwd |
| Windgebied | 3 Vb,0 ..[4.2].....: 24.500 |
| Positie spant in het gebouw....: | 2.470 Kr[4.3.2].....: 0.209 |
| z0 | 0.200 Zmin ..[4.3.2].....: 4.000 |

WIND

| | | | |
|-----------------------------------|-------|--------------------------|-------|
| Co wind van links ..[4.3.3]....: | 1.000 | Co wind van rechts.....: | 1.000 |
| Co wind loodrecht ..[4.3.3]....: | 1.000 | | |
| Cpi wind van links ..[7.2.9]....: | 0.200 | -0.300 | |
| Cpi windloodrecht ...[7.2.9]....: | 0.200 | -0.300 | |
| Cpi wind van rechts .[7.2.9]....: | 0.200 | -0.300 | |
| Cfr windwrijving[7.5].....: | 0.040 | | |

SNEEUW

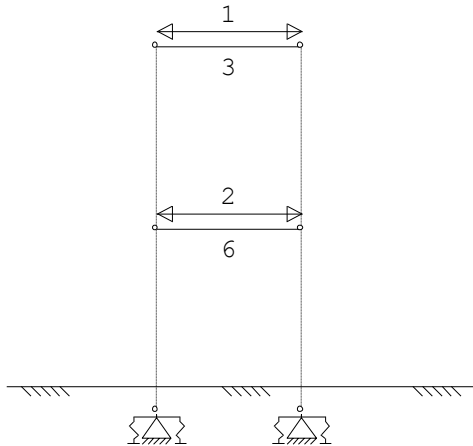
| | |
|--------------------------------|------|
| Sneeuwbelasting (sk) 50 jaar : | 0.70 |
| Sneeuwbelasting (sn) n jaar : | 0.70 |

STAAFTYPEN

| Type | staven |
|------------------|--------|
| 1:Vloer. | : 6 |
| 5:Linker gevel. | : 1,2 |
| 6:Rechter gevel. | : 4,5 |
| 7:Dak. | : 3 |

LASTVELDEN

Veranderlijke belastingen door personen

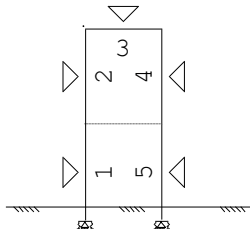


LASTVELDEN

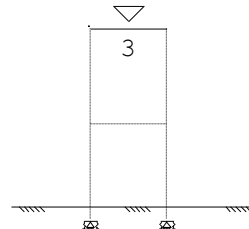
| Nr | StAAF | Tabel | Klasse-Gebruiksfunctie | Verd. | q_k | Q_k |
|------|-------|-------|--------------------------|-------|-------|-------|
| 1 | 3-3 | 6.10 | H-Dak (onder dakbeschot) | 2 | -1.00 | -2.00 |
| 1.00 | | | | | | |
| 2 | 6-6 | 6.2 | C-Vluchtroutes, trappen | 1 | -5.00 | -7.00 |
| 1.00 | | | | | | |

LASTVELDEN

Wind staven



Sneeuw staven

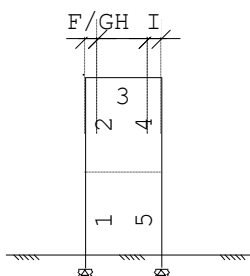


WIND DAKTYPES

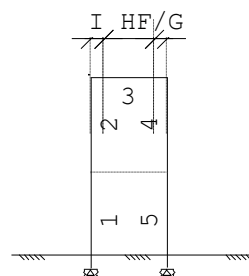
| Nr. | StAAF | Type | reductie bij wind van links | reductie bij wind van rechts | Cpe volgens art: |
|-----|-------|----------|--------------------------------|---------------------------------|------------------|
| 1 | 1-2 | Gevel | 1.000 | 1.000 | 7.2.2 |
| 2 | 3 | Plat dak | 1.000 | 1.000 | 7.2.3 |
| 3 | 4-5 | Gevel | 1.000 | 1.000 | 7.2.2 |

WIND ZONES

Wind van links



Wind van rechts



WIND VAN LINKS ZONES

| Nr. | Staafl | Positie | Lengte | Zone |
|-----|--------|---------|--------|------|
| 1 | 1-2 | 0.000 | 7.500 | D |
| 2 | 3 | 0.000 | 0.494 | F/G |
| 3 | 3 | 0.494 | 1.976 | H |
| 4 | 3 | 2.470 | 0.530 | I |
| 5 | 4-5 | 0.000 | 7.500 | E |

WIND VAN RECHTS ZONES

| Nr. | Staafl | Positie | Lengte | Zone |
|-----|--------|---------|--------|------|
| 1 | 4-5 | 0.000 | 7.500 | D |
| 2 | 3 | 0.000 | 0.494 | F/G |
| 3 | 3 | 0.494 | 1.976 | H |
| 4 | 3 | 2.470 | 0.530 | I |
| 5 | 1-2 | 0.000 | 7.500 | E |

Wind indexen

| Index | CsCd | Cpe/Cpi | qp | breedte | reductie | Qw | Zone | Hoek(en) |
|-------|------|---------|-------|---------|----------|--------|------|----------|
| Qw1 | | 0.300 | 0.615 | 1.240 | | -0.229 | -i | |
| Qw2 | 1.00 | 0.800 | 0.536 | 1.240 | | -0.532 | D | |
| Qw3 | 1.00 | 0.800 | 0.615 | 1.240 | | -0.610 | D | |
| Qw4 | 1.00 | -1.200 | 0.615 | 1.240 | | 0.915 | G | 0.0 |
| Qw5 | 1.00 | -0.700 | 0.615 | 1.240 | | 0.534 | H | 0.0 |
| Qw6 | 1.00 | -0.200 | 0.615 | 1.240 | | 0.153 | I | 0.0 |
| Qw7 | 1.00 | -0.567 | 0.536 | 1.240 | | 0.377 | E | |
| Qw8 | 1.00 | -0.567 | 0.615 | 1.240 | | 0.432 | E | |
| Qw9 | | -0.200 | 0.615 | 1.240 | | 0.153 | +i | |
| Qw10 | 1.00 | 0.200 | 0.615 | 1.240 | | -0.153 | I | 0.0 |
| Qw11 | 1.00 | -0.800 | 0.491 | 1.150 | | 0.451 | B | |
| Qw12 | 1.00 | -0.500 | 0.491 | 0.090 | | 0.022 | C | |
| Qw13 | 1.00 | -0.800 | 0.615 | 1.150 | | 0.566 | B | |
| Qw14 | 1.00 | -0.500 | 0.615 | 0.090 | | 0.028 | C | |

SNEEUW DAKTYPEN

| Staafl | artikel |
|--------|---------------------|
| 3-3 | 5.3.2 Lessenaarsdak |

Sneeuw indexen

| Index | art | μ | s_k | red. | posfac | breedte | Q_s | hoek |
|-------|-------|-------|-------|------|--------|---------|-------|------|
| Qs1 | 5.3.2 | 0.800 | 0.70 | 1.00 | | 1.240 | 0.694 | 0.0 |

BELASTINGGEVALLEN

| B.G. | Omschrijving | Type |
|------|----------------------------------|------------|
| | 1 Permanente belasting EGZ=-1.00 | 1 |
| | 2 Ver. bel. pers. ed. (q_k) | 2 |
| g | 3 Ver. bel. pers. ed. (q_k) | 2 |
| g | 4 Ver. bel. pers. ed. (Q_k) | 3 |
| g | 5 Wind van links onderdruk A | 7 |
| g | 6 Wind van links overdruk A | 8 |
| g | 7 Wind van links onderdruk B | 9 |
| g | 8 Wind van links overdruk B | 10 |
| g | 9 Wind van rechts onderdruk A | 11 |
| g | 10 Wind van rechts overdruk A | 12 |
| g | 11 Wind van rechts onderdruk B | 13 |
| g | 12 Wind van rechts overdruk B | 14 |
| g | 13 Wind loodrecht onderdruk A | 15 |
| g | 14 Wind loodrecht overdruk A | 16 |
| g* | 15 Sneeuw A | 22 |
| | 16 Knik | 0 Onbekend |

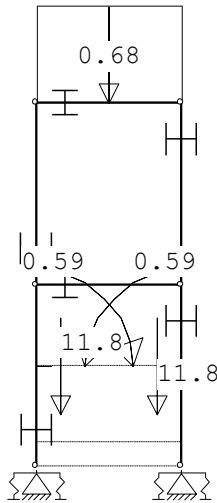
g = gegeneerd belastinggeval

* = belastinggeval bevat 1 of meer handmatig toegevoegde en/of gewijzigde lasten

BELASTINGEN

B.G:1 Permanente belasting

Eigen gewicht van alle staven is meegenomen in berekening. Richting:↓



STAAFBELASTINGEN

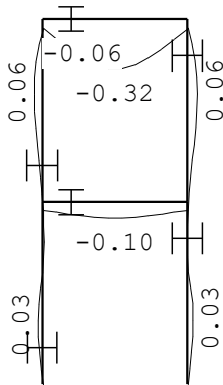
B.G:1 Permanente belasting

| StAAF | Type | q1/p/m | q2 | A | B | ψ_0 | ψ_1 | ψ_2 |
|-------|--------------|--------|-------|-------|-------|----------|----------|----------|
| 3 | 3:QZgeProj. | -0.68 | -0.68 | 0.000 | 0.000 | | | |
| 1 | 10:PZGeproj. | -11.80 | | 2.075 | | | | |
| 5 | 10:PZGeproj. | -11.80 | | 1.660 | | | | |
| 1 | 12:MYLokaal | 0.59 | | 2.075 | | | | |
| 5 | 12:MYLokaal | -0.59 | | 1.660 | | | | |

VERPLAATSINGEN

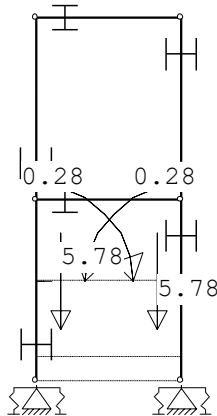
[mm]

B.G:1 Permanente belasting



BELASTINGEN

B.G:2 Ver. bel. pers. ed. (q_k)



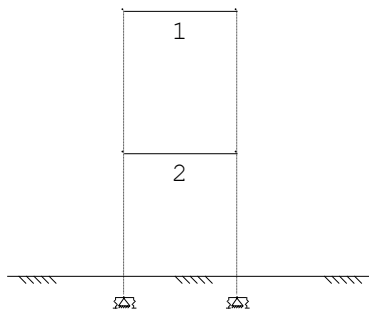
STAAFBELASTINGEN

B.G:2 Ver. bel. pers. ed. (q_k)

| Staaftype | Type | q1/p/m | q2 | A | B | Ψ ₀ | Ψ ₁ | Ψ ₂ |
|-----------|--------------|--------|----|-------|---|----------------|----------------|----------------|
| 1 | 10:PZGeproj. | -5.78 | | 2.075 | | 0.00 | 0.00 | 0.00 |
| 5 | 10:PZGeproj. | -5.78 | | 1.660 | | 0.00 | 0.00 | 0.00 |
| 1 | 12:MYLokaal | 0.28 | | 2.075 | | 0.00 | 0.00 | 0.00 |
| 5 | 12:MYLokaal | -0.28 | | 1.660 | | 0.00 | 0.00 | 0.00 |

SITUATIES BELAST/ONBELAST

B.G:2 Ver. bel. pers. ed. (q_k)



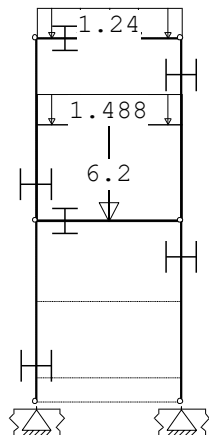
SITUATIES BELAST/ONBELAST

Belastingtype: q_k

| Nr Lastvelden belast | Lastvelden onbelast |
|----------------------|---------------------|
| 1 1,2 | |

BELASTINGEN

B.G:3 Ver. bel. pers. ed. (q_k)



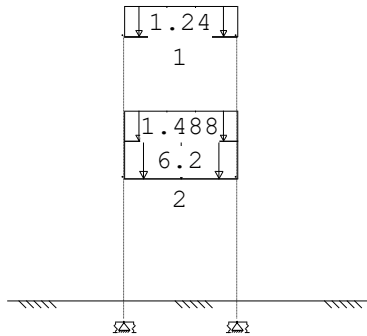
STAAFBELASTINGEN

B.G:3 Ver. bel. pers. ed. (q_k)

| StAAF Type | $q1/p/m$ | $q2$ | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|---------------|----------|-------|-------|-------|----------|----------|----------|
| 3 3:QZgeProj. | -1.24 | -1.24 | 0.000 | 0.000 | 0.00 | 0.00 | 0.00 |
| 6 3:QZgeProj. | -6.20 | -6.20 | 0.000 | 0.000 | 0.60 | 0.70 | 0.60 |
| 6 3:QZgeProj. | -1.49 | -1.49 | 0.000 | 0.000 | 0.60 | 0.70 | 0.60 |

SITUATIES BELAST/ONBELAST

B.G:3 Ver. bel. pers. ed. (q_k)



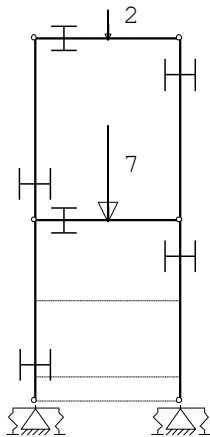
SITUATIES BELAST/ONBELAST

Belastingtype: q_k

| Nr Lastvelden belast | Lastvelden onbelast |
|----------------------|---------------------|
| 1 1,2 | |

BELASTINGEN

B.G:4 Ver. bel. pers. ed. (Q_k)



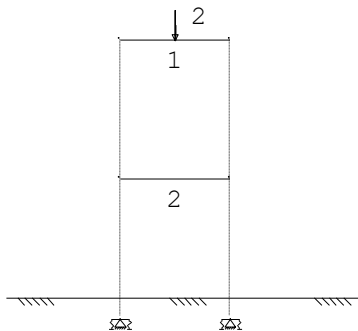
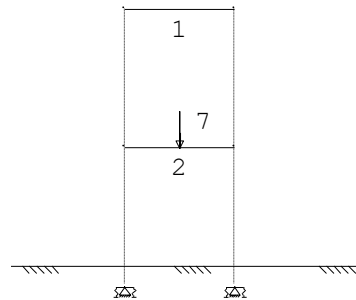
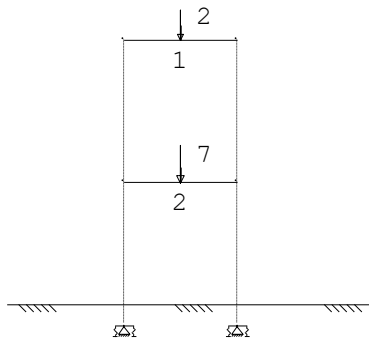
STAAFBELASTINGEN

B.G:4 Ver. bel. pers. ed. (Q_k)

| StAAF Type | $q1/p/m$ | $q2$ | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-----------------|----------|------|-------|---|----------|----------|----------|
| 3 10:PZGeproij. | -2.00 | | 1.500 | | 0.00 | 0.00 | 0.00 |
| 6 10:PZGeproij. | -7.00 | | 1.500 | | 0.60 | 0.70 | 0.60 |

SITUATIES BELAST/ONBELAST

B.G:4 Ver. bel. pers. ed. (Q_k)



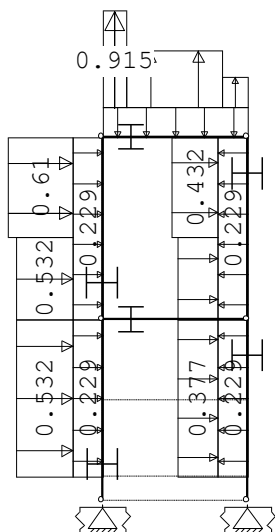
SITUATIES BELAST/ONBELAST

Belastingtype: Q_k

| Nr Lastvelden belast | Lastvelden onbelast |
|----------------------|---------------------|
| 1 1,2 | |
| 2 2 | 1 |
| 3 1 | 2 |

BELASTINGEN

B.G:5 Wind van links onderdruk A



STAAFBELASTINGEN

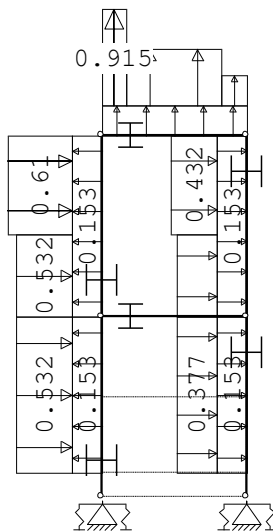
B.G:5 Wind van links onderdruk A

| Staat | Type | Index | $q_1/p/m$ | q_2 | A | B | ψ_0 | ψ_1 | ψ_2 |
|-------|------------|-------|-----------|-------|-------|-------|----------|----------|----------|
| 1 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |

| | | | | | | | | | |
|---|------------|-----|-------|-------|-------|-------|------|------|------|
| 4 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw2 | -0.53 | -0.53 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw2 | -0.53 | -0.53 | 0.000 | 2.060 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw3 | -0.61 | -0.61 | 1.705 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | | 0.00 | 0.00 | 0.000 | 2.506 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw4 | 0.92 | 0.92 | 0.000 | 2.506 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw5 | 0.53 | 0.53 | 0.494 | 0.530 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw6 | 0.15 | 0.15 | 2.470 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw7 | 0.38 | 0.38 | 2.060 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw8 | 0.43 | 0.43 | 0.000 | 1.705 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw7 | 0.38 | 0.38 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |

BELASTINGEN

B.G:6 Wind van links overdruk A



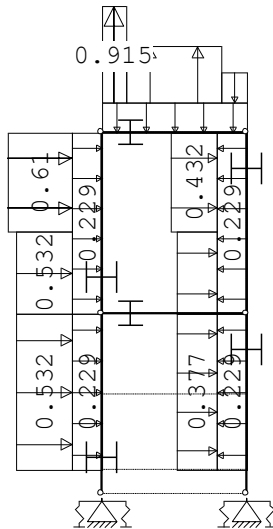
STAAFBELASTINGEN

B.G:6 Wind van links overdruk A

| StAAF | Type | Index | q1/p/m | q2 | A | B | ψ_0 | ψ_1 | ψ_2 |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 1 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw2 | -0.53 | -0.53 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw2 | -0.53 | -0.53 | 0.000 | 2.060 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw3 | -0.61 | -0.61 | 1.705 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | | 0.00 | 0.00 | 0.000 | 2.506 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw4 | 0.92 | 0.92 | 0.000 | 2.506 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw5 | 0.53 | 0.53 | 0.494 | 0.530 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw6 | 0.15 | 0.15 | 2.470 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw7 | 0.38 | 0.38 | 2.060 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw8 | 0.43 | 0.43 | 0.000 | 1.705 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw7 | 0.38 | 0.38 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |

BELASTINGEN

B.G:7 Wind van links onderdruk B



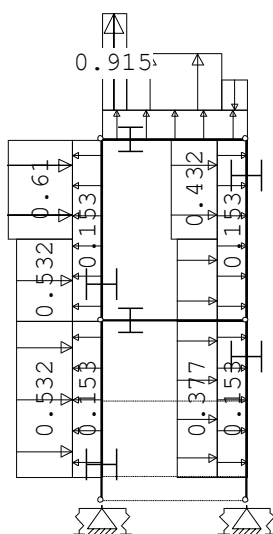
STAAFBELASTINGEN

B.G:7 Wind van links onderdruk B

| StAAF | Type | Index | q1/p/m | q2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 1 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw2 | -0.53 | -0.53 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw2 | -0.53 | -0.53 | 0.000 | 2.060 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw3 | -0.61 | -0.61 | 1.705 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | | 0.00 | 0.00 | 0.000 | 2.506 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw4 | 0.92 | 0.92 | 0.000 | 2.506 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw5 | 0.53 | 0.53 | 0.494 | 0.530 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw10 | -0.15 | -0.15 | 2.470 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw7 | 0.38 | 0.38 | 2.060 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw8 | 0.43 | 0.43 | 0.000 | 1.705 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw7 | 0.38 | 0.38 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |

BELASTINGEN

B.G:8 Wind van links overdruk B



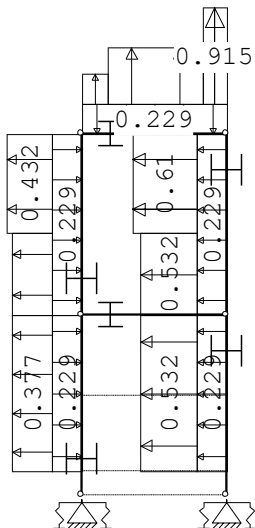
STAAFBELASTINGEN

B.G:8 Wind van links overdruk B

| Staaftype | Type | Index | q1/p/m | q2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-----------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 1 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw2 | -0.53 | -0.53 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw2 | -0.53 | -0.53 | 0.000 | 2.060 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw3 | -0.61 | -0.61 | 1.705 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | | 0.00 | 0.00 | 0.000 | 2.506 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw4 | 0.92 | 0.92 | 0.000 | 2.506 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw5 | 0.53 | 0.53 | 0.494 | 0.530 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw10 | -0.15 | -0.15 | 2.470 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw7 | 0.38 | 0.38 | 2.060 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw8 | 0.43 | 0.43 | 0.000 | 1.705 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw7 | 0.38 | 0.38 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |

BELASTINGEN

B.G:9 Wind van rechts onderdruk A



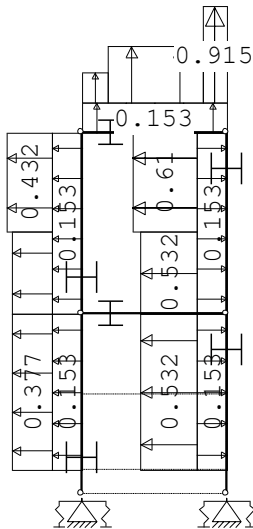
STAAFBELASTINGEN

B.G:9 Wind van rechts onderdruk A

| Staaftype | Type | Index | q1/p/m | q2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-----------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 1 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw2 | -0.53 | -0.53 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw2 | -0.53 | -0.53 | 2.060 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw3 | -0.61 | -0.61 | 0.000 | 1.705 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | | 0.00 | 0.00 | 2.506 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw4 | 0.92 | 0.92 | 2.506 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw5 | 0.53 | 0.53 | 0.530 | 0.494 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw6 | 0.15 | 0.15 | 0.000 | 2.470 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw7 | 0.38 | 0.38 | 0.000 | 2.060 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw8 | 0.43 | 0.43 | 1.705 | 0.000 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw7 | 0.38 | 0.38 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |

BELASTINGEN

B.G:10 Wind van rechts overdruk A



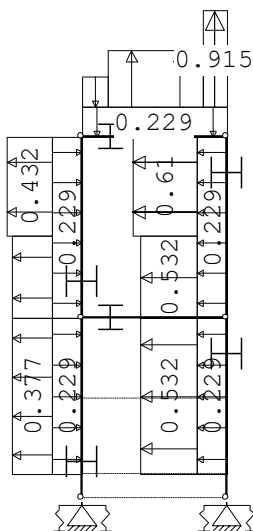
STAAFBELASTINGEN

B.G:10 Wind van rechts overdruk A

| StAAF | Type | Index | q1/p/m | q2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 1 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw2 | -0.53 | -0.53 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw2 | -0.53 | -0.53 | 2.060 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw3 | -0.61 | -0.61 | 0.000 | 1.705 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | | 0.00 | 0.00 | 2.506 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw4 | 0.92 | 0.92 | 2.506 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw5 | 0.53 | 0.53 | 0.530 | 0.494 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw6 | 0.15 | 0.15 | 0.000 | 2.470 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw7 | 0.38 | 0.38 | 0.000 | 2.060 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw8 | 0.43 | 0.43 | 1.705 | 0.000 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw7 | 0.38 | 0.38 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |

BELASTINGEN

B.G:11 Wind van rechts onderdruk B



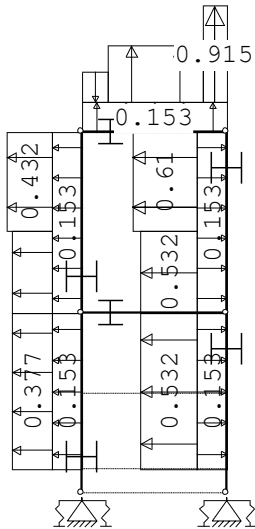
STAAFBELASTINGEN

B.G:11 Wind van rechts onderdruk B

| StAAF | Type | Index | q1/p/m | q2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 1 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw2 | -0.53 | -0.53 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw2 | -0.53 | -0.53 | 2.060 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw3 | -0.61 | -0.61 | 0.000 | 1.705 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | | 0.00 | 0.00 | 2.506 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw4 | 0.92 | 0.92 | 2.506 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw5 | 0.53 | 0.53 | 0.530 | 0.494 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw10 | -0.15 | -0.15 | 0.000 | 2.470 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw7 | 0.38 | 0.38 | 0.000 | 2.060 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw8 | 0.43 | 0.43 | 1.705 | 0.000 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw7 | 0.38 | 0.38 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |

BELASTINGEN

B.G:12 Wind van rechts overdruk B



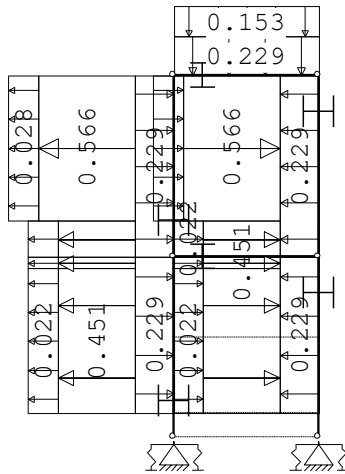
STAAFBELASTINGEN

B.G:12 Wind van rechts overdruk B

| StAAF | Type | Index | q1/p/m | q2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 1 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw2 | -0.53 | -0.53 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw2 | -0.53 | -0.53 | 2.060 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw3 | -0.61 | -0.61 | 0.000 | 1.705 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | | 0.00 | 0.00 | 2.506 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw4 | 0.92 | 0.92 | 2.506 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw5 | 0.53 | 0.53 | 0.530 | 0.494 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw10 | -0.15 | -0.15 | 0.000 | 2.470 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw7 | 0.38 | 0.38 | 0.000 | 2.060 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw8 | 0.43 | 0.43 | 1.705 | 0.000 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw7 | 0.38 | 0.38 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |

BELASTINGEN

B.G:13 Wind loodrecht onderdruk A



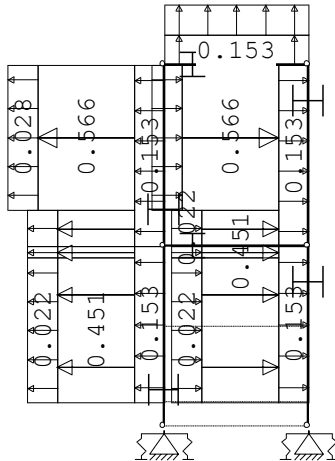
STAAFBELASTINGEN

B.G:13 Wind loodrecht onderdruk A

| Staaftype | Type | Index | q1/p/m | q2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-----------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 1 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw1 | -0.23 | -0.23 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.500 | 0.235 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw12 | 0.02 | 0.02 | 0.500 | 0.235 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 3.501 | 0.000 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw12 | 0.02 | 0.02 | 3.501 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.000 | 3.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw12 | 0.02 | 0.02 | 0.000 | 3.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw13 | 0.57 | 0.57 | 0.765 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw14 | 0.03 | 0.03 | 0.765 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 3.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw12 | 0.02 | 0.02 | 3.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw13 | 0.57 | 0.57 | 0.000 | 0.765 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw14 | 0.03 | 0.03 | 0.000 | 0.765 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.235 | 0.500 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw12 | 0.02 | 0.02 | 0.235 | 0.500 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.000 | 3.501 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw12 | 0.02 | 0.02 | 0.000 | 3.501 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw10 | -0.15 | -0.15 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |

BELASTINGEN

B.G:14 Wind loodrecht overdruk A



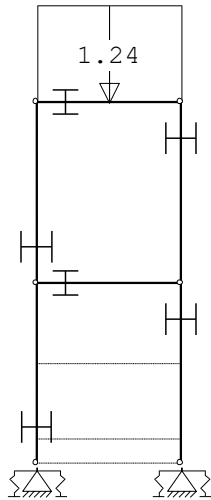
STAAFBELASTINGEN

B.G:14 Wind loodrecht overdruk A

| Staaftype | Type | Index | q1/p/m | q2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-----------|------------|-------|--------|------|-------|-------|----------|----------|----------|
| 1 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw9 | 0.15 | 0.15 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.500 | 0.235 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw12 | 0.02 | 0.02 | 0.500 | 0.235 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 3.501 | 0.000 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw12 | 0.02 | 0.02 | 3.501 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.000 | 3.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw12 | 0.02 | 0.02 | 0.000 | 3.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw13 | 0.57 | 0.57 | 0.765 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw14 | 0.03 | 0.03 | 0.765 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 3.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw12 | 0.02 | 0.02 | 3.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw13 | 0.57 | 0.57 | 0.000 | 0.765 | 0.00 | 0.20 | 0.00 |
| 4 | 1:QZLokaal | Qw14 | 0.03 | 0.03 | 0.000 | 0.765 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.235 | 0.500 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw12 | 0.02 | 0.02 | 0.235 | 0.500 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.000 | 3.501 | 0.00 | 0.20 | 0.00 |
| 5 | 1:QZLokaal | Qw12 | 0.02 | 0.02 | 0.000 | 3.501 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw6 | 0.15 | 0.15 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |

BELASTINGEN

B.G:15 Sneeuw A



STAAFBELASTINGEN

B.G:15 Sneeuw A

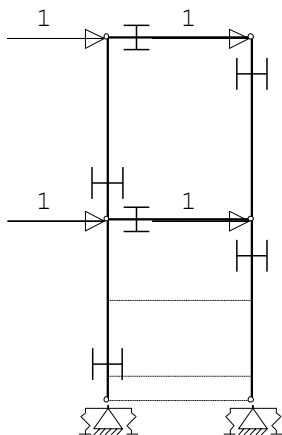
| StAAF Type | Index | q1/p/m | q2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|---------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 3 3:QZgeProj. | * | -1.24 | -1.24 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |

Opmerkingen

[*] Deze belasting is handmatig toegevoegd of gewijzigd.

BELASTINGEN

B.G:16 Knik



KNOOPBELASTINGEN

B.G:16 Knik

| Last | Knoop | Richting | waarde | Ψ_0 | Ψ_1 | Ψ_2 |
|------|-------|----------|--------|----------|----------|----------|
| 1 | 2 | X | 1.000 | | | |
| 2 | 3 | X | 1.000 | | | |
| 3 | 4 | X | 1.000 | | | |
| 4 | 5 | X | 1.000 | | | |

REACTIES

| Kn. | B.G. | X-min | X-max | Z-min | Z-max | M-min | M-max |
|-----|------|-------|-------|-------|-------|-------|-------|
| 1 | 1 | 0.16 | | 15.84 | | 0.01 | |
| 1 | 2 | 0.08 | | 5.78 | | 0.01 | |
| 1 | 3 | 0.42 | | 13.39 | | 0.09 | |
| 1 | 4 | -0.02 | 0.20 | 1.00 | 4.50 | -0.00 | 0.04 |
| 1 | 5 | -3.61 | | -7.80 | | -2.86 | |
| 1 | 6 | -3.23 | | -8.37 | | -2.82 | |
| 1 | 7 | -3.61 | | -7.78 | | -2.86 | |
| 1 | 8 | -3.23 | | -8.36 | | -2.82 | |
| 1 | 9 | 3.02 | | 6.90 | | 2.81 | |
| 1 | 10 | 3.41 | | 6.32 | | 2.85 | |
| 1 | 11 | 3.02 | | 7.04 | | 2.81 | |
| 1 | 12 | 3.41 | | 6.47 | | 2.85 | |
| 1 | 13 | 0.21 | | 0.57 | | 0.02 | |
| 1 | 14 | 0.61 | | -0.46 | | 0.06 | |
| 1 | 15 | -0.03 | | 1.86 | | -0.01 | |
| 1 | 16 | -2.00 | | -6.11 | | -2.07 | |
| 6 | 1 | -0.16 | | 15.84 | | -0.01 | |
| 6 | 2 | -0.08 | | 5.78 | | -0.01 | |
| 6 | 3 | -0.42 | | 13.39 | | -0.09 | |
| 6 | 4 | -0.20 | 0.02 | 1.00 | 4.50 | -0.04 | 0.00 |
| 6 | 5 | -3.02 | | 6.90 | | -2.81 | |
| 6 | 6 | -3.41 | | 6.32 | | -2.85 | |
| 6 | 7 | -3.02 | | 7.04 | | -2.81 | |
| 6 | 8 | -3.41 | | 6.47 | | -2.85 | |
| 6 | 9 | 3.61 | | -7.80 | | 2.86 | |
| 6 | 10 | 3.23 | | -8.37 | | 2.82 | |
| 6 | 11 | 3.61 | | -7.78 | | 2.86 | |
| 6 | 12 | 3.23 | | -8.36 | | 2.82 | |
| 6 | 13 | -0.21 | | 0.57 | | -0.02 | |
| 6 | 14 | -0.61 | | -0.46 | | -0.06 | |
| 6 | 15 | 0.03 | | 1.86 | | 0.01 | |
| 6 | 16 | -2.00 | | 6.11 | | -2.07 | |

BELASTINGCOMBINATIES

| BC Type | BG Gen. Factor | BG Gen. Factor | BG Gen. Factor | BG Gen. Factor |
|----------|----------------|----------------|----------------|----------------|
| 1 Fund. | 1 Perm | 1.35 | | |
| 2 Fund. | 1 Perm | 0.90 | | |
| 3 Fund. | 1 Perm | 1.35 | 4 psi0 | 1.50 |
| 4 Fund. | 1 Perm | 1.20 | 4 Extr | 1.50 |
| 5 Fund. | 1 Perm | 1.20 | 5 Extr | 1.50 |
| 6 Fund. | 1 Perm | 1.20 | 6 Extr | 1.50 |
| 7 Fund. | 1 Perm | 1.20 | 7 Extr | 1.50 |
| 8 Fund. | 1 Perm | 1.20 | 8 Extr | 1.50 |
| 9 Fund. | 1 Perm | 1.20 | 9 Extr | 1.50 |
| 10 Fund. | 1 Perm | 1.20 | 10 Extr | 1.50 |
| 11 Fund. | 1 Perm | 1.20 | 11 Extr | 1.50 |
| 12 Fund. | 1 Perm | 1.20 | 12 Extr | 1.50 |
| 13 Fund. | 1 Perm | 1.20 | 13 Extr | 1.50 |
| 14 Fund. | 1 Perm | 1.20 | 14 Extr | 1.50 |
| 15 Fund. | 1 Perm | 1.20 | 15 Extr | 1.50 |
| 16 Fund. | 1 Perm | 0.90 | 4 psi0 | 1.50 |
| 17 Fund. | 1 Perm | 0.90 | 4 Extr | 1.50 |
| 18 Fund. | 1 Perm | 0.90 | 5 Extr | 1.50 |
| 19 Fund. | 1 Perm | 0.90 | 6 Extr | 1.50 |
| 20 Fund. | 1 Perm | 0.90 | 7 Extr | 1.50 |
| 21 Fund. | 1 Perm | 0.90 | 8 Extr | 1.50 |

| | | | | | | | | | | | |
|----|-------|---|------|------|----|------|------|---|------|------|-------------|
| 22 | Fund. | 1 | Perm | 0.90 | 9 | Extr | 1.50 | | | | |
| 23 | Fund. | 1 | Perm | 0.90 | 10 | Extr | 1.50 | | | | |
| 24 | Fund. | 1 | Perm | 0.90 | 11 | Extr | 1.50 | | | | |
| 25 | Fund. | 1 | Perm | 0.90 | 12 | Extr | 1.50 | | | | |
| 26 | Fund. | 1 | Perm | 0.90 | 13 | Extr | 1.50 | | | | |
| 27 | Fund. | 1 | Perm | 0.90 | 14 | Extr | 1.50 | | | | |
| 28 | Fund. | 1 | Perm | 0.90 | 15 | Extr | 1.50 | | | | |
| 29 | Fund. | 1 | Perm | 1.35 | 2 | psi0 | 1.50 | 3 | psi0 | 1.50 | |
| 30 | Fund. | 1 | Perm | 1.20 | 2 | Extr | 1.50 | 3 | Extr | 1.50 | |
| 31 | Fund. | 1 | Perm | 1.20 | 5 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 32 | Fund. | 1 | Perm | 1.20 | 6 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 33 | Fund. | 1 | Perm | 1.20 | 7 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 34 | Fund. | 1 | Perm | 1.20 | 8 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 35 | Fund. | 1 | Perm | 1.20 | 9 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 36 | Fund. | 1 | Perm | 1.20 | 10 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 37 | Fund. | 1 | Perm | 1.20 | 11 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 38 | Fund. | 1 | Perm | 1.20 | 12 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 39 | Fund. | 1 | Perm | 1.20 | 13 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 40 | Fund. | 1 | Perm | 1.20 | 14 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 41 | Fund. | 1 | Perm | 1.20 | 15 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 42 | Fund. | 1 | Perm | 0.90 | 2 | Extr | 1.50 | 3 | Extr | 1.50 | |
| 43 | Fund. | 1 | Perm | 0.90 | 2 | psi0 | 1.50 | 3 | psi0 | 1.50 | |
| 44 | Fund. | 1 | Perm | 0.90 | 5 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 45 | Fund. | 1 | Perm | 0.90 | 6 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 46 | Fund. | 1 | Perm | 0.90 | 7 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 47 | Fund. | 1 | Perm | 0.90 | 8 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 48 | Fund. | 1 | Perm | 0.90 | 9 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 49 | Fund. | 1 | Perm | 0.90 | 10 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 50 | Fund. | 1 | Perm | 0.90 | 11 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 51 | Fund. | 1 | Perm | 0.90 | 12 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 52 | Fund. | 1 | Perm | 0.90 | 13 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 53 | Fund. | 1 | Perm | 0.90 | 14 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 54 | Fund. | 1 | Perm | 0.90 | 15 | Extr | 1.50 | 4 | psi0 | 1.50 | |
| 55 | Fund. | 1 | Perm | 1.20 | 5 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 56 | Fund. | 1 | Perm | 1.20 | 6 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 57 | Fund. | 1 | Perm | 1.20 | 7 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 58 | Fund. | 1 | Perm | 1.20 | 8 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 59 | Fund. | 1 | Perm | 1.20 | 9 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 60 | Fund. | 1 | Perm | 1.20 | 10 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 61 | Fund. | 1 | Perm | 1.20 | 11 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 62 | Fund. | 1 | Perm | 1.20 | 12 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 63 | Fund. | 1 | Perm | 1.20 | 13 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 64 | Fund. | 1 | Perm | 1.20 | 14 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 65 | Fund. | 1 | Perm | 1.20 | 15 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 66 | Fund. | 1 | Perm | 0.90 | 5 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 67 | Fund. | 1 | Perm | 0.90 | 6 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 68 | Fund. | 1 | Perm | 0.90 | 7 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 69 | Fund. | 1 | Perm | 0.90 | 8 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 70 | Fund. | 1 | Perm | 0.90 | 9 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 71 | Fund. | 1 | Perm | 0.90 | 10 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 72 | Fund. | 1 | Perm | 0.90 | 11 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 73 | Fund. | 1 | Perm | 0.90 | 12 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 74 | Fund. | 1 | Perm | 0.90 | 13 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 75 | Fund. | 1 | Perm | 0.90 | 14 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 76 | Fund. | 1 | Perm | 0.90 | 15 | Extr | 1.50 | 2 | psi0 | 1.50 | 3 psi0 1.50 |
| 77 | Kar. | 1 | Perm | 1.00 | 4 | Extr | 1.00 | | | | |
| 78 | Kar. | 1 | Perm | 1.00 | 5 | Extr | 1.00 | | | | |
| 79 | Kar. | 1 | Perm | 1.00 | 6 | Extr | 1.00 | | | | |
| 80 | Kar. | 1 | Perm | 1.00 | 7 | Extr | 1.00 | | | | |

| | | | | | | | | | | | | | | | | | | | |
|-----|-------|---|------|------|----|------|------|---|------|------|---|------|------|--|--|--|--|--|--|
| 81 | Kar. | 1 | Perm | 1.00 | 8 | Extr | 1.00 | | | | | | | | | | | | |
| 82 | Kar. | 1 | Perm | 1.00 | 9 | Extr | 1.00 | | | | | | | | | | | | |
| 83 | Kar. | 1 | Perm | 1.00 | 10 | Extr | 1.00 | | | | | | | | | | | | |
| 84 | Kar. | 1 | Perm | 1.00 | 11 | Extr | 1.00 | | | | | | | | | | | | |
| 85 | Kar. | 1 | Perm | 1.00 | 12 | Extr | 1.00 | | | | | | | | | | | | |
| 86 | Kar. | 1 | Perm | 1.00 | 13 | Extr | 1.00 | | | | | | | | | | | | |
| 87 | Kar. | 1 | Perm | 1.00 | 14 | Extr | 1.00 | | | | | | | | | | | | |
| 88 | Kar. | 1 | Perm | 1.00 | 15 | Extr | 1.00 | | | | | | | | | | | | |
| 89 | Kar. | 1 | Perm | 1.00 | 2 | Extr | 1.00 | 3 | Extr | 1.00 | | | | | | | | | |
| 90 | Kar. | 1 | Perm | 1.00 | 5 | Extr | 1.00 | 4 | psi0 | 1.00 | | | | | | | | | |
| 91 | Kar. | 1 | Perm | 1.00 | 6 | Extr | 1.00 | 4 | psi0 | 1.00 | | | | | | | | | |
| 92 | Kar. | 1 | Perm | 1.00 | 7 | Extr | 1.00 | 4 | psi0 | 1.00 | | | | | | | | | |
| 93 | Kar. | 1 | Perm | 1.00 | 8 | Extr | 1.00 | 4 | psi0 | 1.00 | | | | | | | | | |
| 94 | Kar. | 1 | Perm | 1.00 | 9 | Extr | 1.00 | 4 | psi0 | 1.00 | | | | | | | | | |
| 95 | Kar. | 1 | Perm | 1.00 | 10 | Extr | 1.00 | 4 | psi0 | 1.00 | | | | | | | | | |
| 96 | Kar. | 1 | Perm | 1.00 | 11 | Extr | 1.00 | 4 | psi0 | 1.00 | | | | | | | | | |
| 97 | Kar. | 1 | Perm | 1.00 | 12 | Extr | 1.00 | 4 | psi0 | 1.00 | | | | | | | | | |
| 98 | Kar. | 1 | Perm | 1.00 | 13 | Extr | 1.00 | 4 | psi0 | 1.00 | | | | | | | | | |
| 99 | Kar. | 1 | Perm | 1.00 | 14 | Extr | 1.00 | 4 | psi0 | 1.00 | | | | | | | | | |
| 100 | Kar. | 1 | Perm | 1.00 | 15 | Extr | 1.00 | 4 | psi0 | 1.00 | | | | | | | | | |
| 101 | Kar. | 1 | Perm | 1.00 | 5 | Extr | 1.00 | 2 | psi0 | 1.00 | 3 | psi0 | 1.00 | | | | | | |
| 102 | Kar. | 1 | Perm | 1.00 | 6 | Extr | 1.00 | 2 | psi0 | 1.00 | 3 | psi0 | 1.00 | | | | | | |
| 103 | Kar. | 1 | Perm | 1.00 | 7 | Extr | 1.00 | 2 | psi0 | 1.00 | 3 | psi0 | 1.00 | | | | | | |
| 104 | Kar. | 1 | Perm | 1.00 | 8 | Extr | 1.00 | 2 | psi0 | 1.00 | 3 | psi0 | 1.00 | | | | | | |
| 105 | Kar. | 1 | Perm | 1.00 | 9 | Extr | 1.00 | 2 | psi0 | 1.00 | 3 | psi0 | 1.00 | | | | | | |
| 106 | Kar. | 1 | Perm | 1.00 | 10 | Extr | 1.00 | 2 | psi0 | 1.00 | 3 | psi0 | 1.00 | | | | | | |
| 107 | Kar. | 1 | Perm | 1.00 | 11 | Extr | 1.00 | 2 | psi0 | 1.00 | 3 | psi0 | 1.00 | | | | | | |
| 108 | Kar. | 1 | Perm | 1.00 | 12 | Extr | 1.00 | 2 | psi0 | 1.00 | 3 | psi0 | 1.00 | | | | | | |
| 109 | Kar. | 1 | Perm | 1.00 | 13 | Extr | 1.00 | 2 | psi0 | 1.00 | 3 | psi0 | 1.00 | | | | | | |
| 110 | Kar. | 1 | Perm | 1.00 | 14 | Extr | 1.00 | 2 | psi0 | 1.00 | 3 | psi0 | 1.00 | | | | | | |
| 111 | Kar. | 1 | Perm | 1.00 | 15 | Extr | 1.00 | 2 | psi0 | 1.00 | 3 | psi0 | 1.00 | | | | | | |
| 112 | Quas. | 1 | Perm | 1.00 | | | | | | | | | | | | | | | |
| 113 | Quas. | 1 | Perm | 1.00 | 4 | psi2 | 1.00 | | | | | | | | | | | | |
| 114 | Quas. | 1 | Perm | 1.00 | 2 | psi2 | 1.00 | 3 | psi2 | 1.00 | | | | | | | | | |
| 115 | Freq. | 1 | Perm | 1.00 | | | | | | | | | | | | | | | |
| 116 | Freq. | 1 | Perm | 1.00 | 4 | psi1 | 1.00 | | | | | | | | | | | | |
| 117 | Freq. | 1 | Perm | 1.00 | 5 | psi1 | 1.00 | | | | | | | | | | | | |
| 118 | Freq. | 1 | Perm | 1.00 | 6 | psi1 | 1.00 | | | | | | | | | | | | |
| 119 | Freq. | 1 | Perm | 1.00 | 7 | psi1 | 1.00 | | | | | | | | | | | | |
| 120 | Freq. | 1 | Perm | 1.00 | 8 | psi1 | 1.00 | | | | | | | | | | | | |
| 121 | Freq. | 1 | Perm | 1.00 | 9 | psi1 | 1.00 | | | | | | | | | | | | |
| 122 | Freq. | 1 | Perm | 1.00 | 10 | psi1 | 1.00 | | | | | | | | | | | | |
| 123 | Freq. | 1 | Perm | 1.00 | 11 | psi1 | 1.00 | | | | | | | | | | | | |
| 124 | Freq. | 1 | Perm | 1.00 | 12 | psi1 | 1.00 | | | | | | | | | | | | |
| 125 | Freq. | 1 | Perm | 1.00 | 13 | psi1 | 1.00 | | | | | | | | | | | | |
| 126 | Freq. | 1 | Perm | 1.00 | 14 | psi1 | 1.00 | | | | | | | | | | | | |
| 127 | Freq. | 1 | Perm | 1.00 | 15 | psi1 | 1.00 | | | | | | | | | | | | |
| 128 | Freq. | 1 | Perm | 1.00 | 2 | psi1 | 1.00 | 3 | psi1 | 1.00 | | | | | | | | | |
| 129 | Freq. | 1 | Perm | 1.00 | 5 | psi1 | 1.00 | 4 | psi2 | 1.00 | | | | | | | | | |
| 130 | Freq. | 1 | Perm | 1.00 | 6 | psi1 | 1.00 | 4 | psi2 | 1.00 | | | | | | | | | |
| 131 | Freq. | 1 | Perm | 1.00 | 7 | psi1 | 1.00 | 4 | psi2 | 1.00 | | | | | | | | | |
| 132 | Freq. | 1 | Perm | 1.00 | 8 | psi1 | 1.00 | 4 | psi2 | 1.00 | | | | | | | | | |
| 133 | Freq. | 1 | Perm | 1.00 | 9 | psi1 | 1.00 | 4 | psi2 | 1.00 | | | | | | | | | |
| 134 | Freq. | 1 | Perm | 1.00 | 10 | psi1 | 1.00 | 4 | psi2 | 1.00 | | | | | | | | | |
| 135 | Freq. | 1 | Perm | 1.00 | 11 | psi1 | 1.00 | 4 | psi2 | 1.00 | | | | | | | | | |
| 136 | Freq. | 1 | Perm | 1.00 | 12 | psi1 | 1.00 | 4 | psi2 | 1.00 | | | | | | | | | |
| 137 | Freq. | 1 | Perm | 1.00 | 13 | psi1 | 1.00 | 4 | psi2 | 1.00 | | | | | | | | | |
| 138 | Freq. | 1 | Perm | 1.00 | 14 | psi1 | 1.00 | 4 | psi2 | 1.00 | | | | | | | | | |
| 139 | Freq. | 1 | Perm | 1.00 | 15 | psi1 | 1.00 | 4 | psi2 | 1.00 | | | | | | | | | |

| | | | | | | | | | |
|-----|-------|--------|------|---------|------|--------|------|--------|------|
| 140 | Freq. | 1 Perm | 1.00 | 5 psi1 | 1.00 | 2 psi2 | 1.00 | 3 psi2 | 1.00 |
| 141 | Freq. | 1 Perm | 1.00 | 6 psi1 | 1.00 | 2 psi2 | 1.00 | 3 psi2 | 1.00 |
| 142 | Freq. | 1 Perm | 1.00 | 7 psi1 | 1.00 | 2 psi2 | 1.00 | 3 psi2 | 1.00 |
| 143 | Freq. | 1 Perm | 1.00 | 8 psi1 | 1.00 | 2 psi2 | 1.00 | 3 psi2 | 1.00 |
| 144 | Freq. | 1 Perm | 1.00 | 9 psi1 | 1.00 | 2 psi2 | 1.00 | 3 psi2 | 1.00 |
| 145 | Freq. | 1 Perm | 1.00 | 10 psi1 | 1.00 | 2 psi2 | 1.00 | 3 psi2 | 1.00 |
| 146 | Freq. | 1 Perm | 1.00 | 11 psi1 | 1.00 | 2 psi2 | 1.00 | 3 psi2 | 1.00 |
| 147 | Freq. | 1 Perm | 1.00 | 12 psi1 | 1.00 | 2 psi2 | 1.00 | 3 psi2 | 1.00 |
| 148 | Freq. | 1 Perm | 1.00 | 13 psi1 | 1.00 | 2 psi2 | 1.00 | 3 psi2 | 1.00 |
| 149 | Freq. | 1 Perm | 1.00 | 14 psi1 | 1.00 | 2 psi2 | 1.00 | 3 psi2 | 1.00 |
| 150 | Freq. | 1 Perm | 1.00 | 15 psi1 | 1.00 | 2 psi2 | 1.00 | 3 psi2 | 1.00 |
| 151 | Blij. | 1 Perm | 1.00 | | | | | | |

GUNSTIGE WERKING PERMANENTE BELASTINGEN

BC Staven met gunstige werking

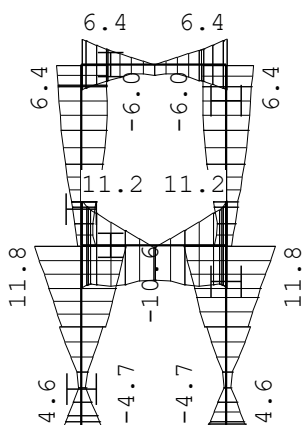
- 1 Geen
- 2 Alle staven de factor:0.90
- 3 Geen
- 4 Geen
- 5 Geen
- 6 Geen
- 7 Geen
- 8 Geen
- 9 Geen
- 10 Geen
- 11 Geen
- 12 Geen
- 13 Geen
- 14 Geen
- 15 Geen
- 16 Alle staven de factor:0.90
- 17 Alle staven de factor:0.90
- 18 Alle staven de factor:0.90
- 19 Alle staven de factor:0.90
- 20 Alle staven de factor:0.90
- 21 Alle staven de factor:0.90
- 22 Alle staven de factor:0.90
- 23 Alle staven de factor:0.90
- 24 Alle staven de factor:0.90
- 25 Alle staven de factor:0.90
- 26 Alle staven de factor:0.90
- 27 Alle staven de factor:0.90
- 28 Alle staven de factor:0.90
- 29 Geen
- 30 Geen
- 31 Geen
- 32 Geen
- 33 Geen
- 34 Geen
- 35 Geen
- 36 Geen
- 37 Geen
- 38 Geen
- 39 Geen
- 40 Geen
- 41 Geen
- 42 Alle staven de factor:0.90
- 43 Alle staven de factor:0.90

44 Alle staven de factor:0.90
45 Alle staven de factor:0.90
46 Alle staven de factor:0.90
47 Alle staven de factor:0.90
48 Alle staven de factor:0.90
49 Alle staven de factor:0.90
50 Alle staven de factor:0.90
51 Alle staven de factor:0.90
52 Alle staven de factor:0.90
53 Alle staven de factor:0.90
54 Alle staven de factor:0.90
55 Geen
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60 Geen
61 Geen
62 Geen
63 Geen
64 Geen
65 Geen
66 Alle staven de factor:0.90
67 Alle staven de factor:0.90
68 Alle staven de factor:0.90
69 Alle staven de factor:0.90
70 Alle staven de factor:0.90
71 Alle staven de factor:0.90
72 Alle staven de factor:0.90
73 Alle staven de factor:0.90
74 Alle staven de factor:0.90
75 Alle staven de factor:0.90
76 Alle staven de factor:0.90

OMHULLENDE VAN DE FUNDAMENTELE COMBINATIES

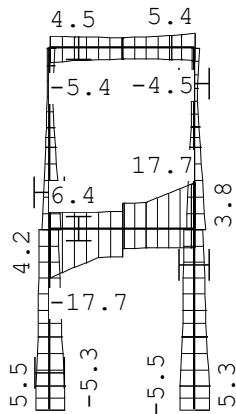
MOMENTEN

Fundamentele combinatie



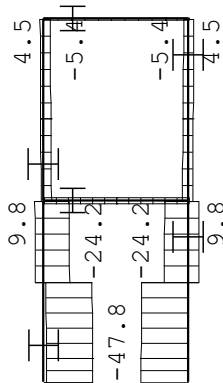
DWARSKRACHTEN

Fundamentele combinatie



NORMAALKRACHTEN

Fundamentele combinatie



STAAFKRACHTEN

Fundamentele combinatie

| St. | Kn. | Pos. | NXi/NXj | | DZi/DZj | | | | MYi/MYj | | | | | |
|-----|-----|-------|---------|----|---------|----|-------|----|---------|----|--------|----|-------|----|
| | | | Min | BC | Max | BC | Min | BC | Max | BC | Min | BC | Max | BC |
| 1 | 1 | | -47.77 | 30 | -1.89 | 19 | -5.29 | 20 | 5.48 | 60 | -4.68 | 60 | 4.61 | 66 |
| 1 | | 0.500 | -47.59 | 30 | -1.75 | 19 | -5.29 | 20 | 5.48 | 60 | -2.19 | 70 | 2.31 | 56 |
| 1 | | 0.804 | -47.48 | 30 | -1.67 | 19 | -4.94 | 20 | 5.24 | 60 | -0.75 | 24 | 0.97 | 56 |
| 1 | | 0.922 | -47.43 | 30 | -1.64 | 19 | -4.81 | 20 | 5.15 | 60 | -0.21 | 24 | 1.11 | 64 |
| 1 | | 2.075 | -47.01 | 30 | -1.32 | 19 | -3.81 | 21 | 4.55 | 59 | -5.00 | 20 | 5.70 | 60 |
| 1 | | 2.075 | -24.80 | 30 | 9.30 | 19 | -3.81 | 21 | 4.55 | 59 | -5.61 | 20 | 5.08 | 60 |
| 1 | 2 | | -24.19 | 61 | 9.75 | 19 | -2.86 | 21 | 4.18 | 59 | -10.65 | 8 | 11.82 | 70 |
| 2 | 2 | | -6.81 | 61 | 3.46 | 67 | -3.77 | 18 | 3.23 | 62 | -3.26 | 64 | 1.10 | 22 |
| 2 | | 0.409 | -6.66 | 61 | 3.57 | 67 | -3.30 | 18 | 2.91 | 62 | -2.33 | 30 | 1.80 | 22 |
| 2 | | 2.937 | -5.73 | 61 | 4.27 | 67 | -0.74 | 19 | 1.26 | 61 | -5.98 | 66 | 5.71 | 62 |
| 2 | | 2.995 | -5.71 | 61 | 4.28 | 67 | -0.80 | 27 | 1.24 | 61 | -5.99 | 66 | 5.75 | 62 |
| 2 | | 3.337 | -5.59 | 61 | 4.38 | 67 | -1.18 | 27 | 1.14 | 61 | -5.91 | 66 | 5.96 | 61 |
| 2 | | 3.410 | -5.56 | 61 | 4.40 | 67 | -1.26 | 27 | 1.12 | 61 | -5.93 | 67 | 6.04 | 61 |
| 2 | | 3.719 | -5.45 | 61 | 4.48 | 67 | -1.61 | 27 | 1.12 | 30 | -5.96 | 67 | 6.37 | 61 |
| 2 | 3 | | -5.43 | 61 | 4.49 | 67 | -1.66 | 27 | 1.12 | 30 | -5.96 | 67 | 6.42 | 61 |
| 3 | 3 | | -1.12 | 30 | 1.66 | 27 | -5.43 | 61 | 4.49 | 67 | -5.96 | 67 | 6.42 | 61 |
| 3 | | 1.073 | -1.12 | 30 | 1.66 | 27 | -4.20 | 59 | 4.00 | 67 | -1.95 | 7 | 1.86 | 71 |
| 3 | | 1.484 | -1.12 | 30 | 1.66 | 27 | -3.93 | 59 | 3.92 | 67 | -2.49 | 4 | 0.27 | 71 |
| 3 | | 1.500 | -1.12 | 30 | 1.66 | 27 | -3.92 | 59 | 3.92 | 55 | -2.52 | 4 | 0.20 | 71 |
| 3 | | 1.516 | -1.12 | 30 | 1.66 | 27 | -3.92 | 60 | 3.93 | 55 | -2.49 | 4 | 0.27 | 67 |
| 3 | | 1.927 | -1.12 | 30 | 1.66 | 27 | -4.00 | 71 | 4.20 | 55 | -1.95 | 41 | 1.86 | 67 |
| 3 | 4 | | -1.12 | 30 | 1.66 | 27 | -4.49 | 71 | 5.43 | 57 | -5.96 | 71 | 6.42 | 57 |

| | | | | | | | | | | | | | |
|---|-------|--------|----|-------|----|--------|----|-------|----|--------|----|-------|----|
| 4 | 4 | -5.43 | 57 | 4.49 | 71 | -1.12 | 30 | 1.66 | 27 | -5.96 | 71 | 6.42 | 57 |
| 4 | 0.046 | -5.45 | 57 | 4.48 | 71 | -1.12 | 30 | 1.61 | 27 | -5.96 | 71 | 6.38 | 57 |
| 4 | 0.354 | -5.56 | 57 | 4.40 | 71 | -1.12 | 30 | 1.26 | 27 | -5.93 | 71 | 6.04 | 57 |
| 4 | 0.428 | -5.59 | 57 | 4.38 | 71 | -1.14 | 57 | 1.18 | 27 | -5.91 | 71 | 5.96 | 57 |
| 4 | 0.769 | -5.71 | 57 | 4.28 | 71 | -1.24 | 57 | 0.80 | 27 | -5.99 | 70 | 5.75 | 58 |
| 4 | 0.828 | -5.73 | 57 | 4.27 | 71 | -1.26 | 57 | 0.74 | 27 | -5.98 | 70 | 5.71 | 58 |
| 4 | 3.356 | -6.66 | 57 | 3.57 | 71 | -2.91 | 58 | 3.30 | 22 | -2.33 | 62 | 1.80 | 18 |
| 4 | 5 | -6.81 | 57 | 3.46 | 71 | -3.23 | 58 | 3.77 | 22 | -3.26 | 64 | 1.10 | 18 |
| 5 | 5 | -24.19 | 57 | 9.75 | 23 | -4.18 | 55 | 2.86 | 25 | -10.65 | 12 | 11.82 | 66 |
| 5 | 1.660 | -24.80 | 57 | 9.30 | 23 | -4.55 | 55 | 3.81 | 25 | -5.61 | 11 | 5.08 | 67 |
| 5 | 1.660 | -47.01 | 57 | -1.32 | 23 | -4.55 | 55 | 3.81 | 25 | -5.00 | 11 | 5.70 | 67 |
| 5 | 2.813 | -47.43 | 30 | -1.64 | 23 | -5.15 | 56 | 4.81 | 24 | -0.21 | 24 | 1.11 | 64 |
| 5 | 2.931 | -47.48 | 30 | -1.67 | 23 | -5.24 | 56 | 4.94 | 24 | -0.75 | 20 | 0.97 | 64 |
| 5 | 3.235 | -47.59 | 30 | -1.75 | 23 | -5.48 | 56 | 5.29 | 24 | -2.19 | 66 | 2.31 | 60 |
| 5 | 6 | -47.77 | 30 | -1.89 | 23 | -5.48 | 56 | 5.29 | 24 | -4.68 | 56 | 4.61 | 70 |
| 6 | 2 | -2.18 | 9 | 4.43 | 75 | -17.74 | 30 | 6.41 | 18 | -10.09 | 18 | 11.23 | 59 |
| 6 | 0.077 | -2.18 | 9 | 4.43 | 75 | -16.83 | 30 | 6.43 | 18 | -9.59 | 18 | 9.90 | 59 |
| 6 | 0.159 | -2.18 | 9 | 4.43 | 75 | -16.24 | 60 | 6.45 | 18 | -9.07 | 6 | 9.04 | 48 |
| 6 | 0.590 | -2.18 | 9 | 4.43 | 75 | -13.13 | 60 | 6.54 | 18 | -9.73 | 56 | 6.01 | 23 |
| 6 | 1.280 | -2.18 | 9 | 4.43 | 75 | -9.92 | 36 | 6.70 | 18 | -8.01 | 56 | 1.28 | 25 |
| 6 | 1.468 | -2.18 | 9 | 4.43 | 75 | -9.86 | 36 | 6.74 | 18 | -8.29 | 30 | -0.00 | 25 |
| 6 | 1.481 | -2.18 | 9 | 4.43 | 75 | -9.86 | 49 | 6.74 | 18 | -8.30 | 30 | -0.09 | 25 |
| 6 | 1.500 | -2.18 | 9 | 4.43 | 75 | -9.85 | 49 | 6.75 | 18 | -8.30 | 30 | -0.08 | 26 |
| 6 | 1.500 | -2.18 | 9 | 4.43 | 75 | -6.75 | 49 | 9.85 | 18 | -8.30 | 30 | -0.08 | 26 |
| 6 | 1.519 | -2.18 | 9 | 4.43 | 75 | -6.74 | 22 | 9.86 | 45 | -8.30 | 30 | -0.08 | 26 |
| 6 | 1.532 | -2.18 | 9 | 4.43 | 75 | -6.74 | 22 | 9.86 | 32 | -8.29 | 30 | -0.00 | 21 |
| 6 | 1.720 | -2.18 | 9 | 4.43 | 75 | -6.70 | 22 | 9.92 | 32 | -8.01 | 30 | 1.28 | 21 |
| 6 | 2.410 | -2.18 | 9 | 4.43 | 75 | -6.54 | 22 | 13.13 | 56 | -9.73 | 60 | 6.01 | 19 |
| 6 | 2.841 | -2.18 | 9 | 4.43 | 75 | -6.45 | 22 | 16.24 | 56 | -9.07 | 71 | 9.04 | 44 |
| 6 | 2.923 | -2.18 | 9 | 4.43 | 75 | -6.43 | 22 | 16.83 | 56 | -9.59 | 22 | 9.90 | 55 |
| 6 | 5 | -2.18 | 9 | 4.43 | 75 | -6.41 | 22 | 17.74 | 30 | -10.09 | 22 | 11.23 | 55 |

REACTIES

Fundamentele combinatie

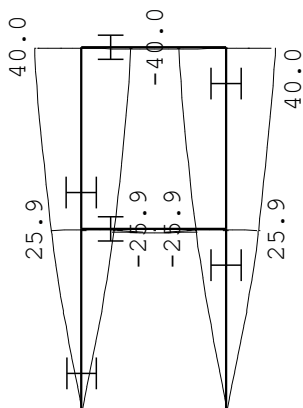
| Kn. | X-min | X-max | Z-min | Z-max | M-min | M-max |
|-----|-------|-------|-------|-------|-------|-------|
| 1 | -5.29 | 5.48 | 1.89 | 47.77 | -4.61 | 4.68 |
| 6 | -5.48 | 5.29 | 1.89 | 47.77 | -4.68 | 4.61 |

OMHULLENDE VAN DE KARAKTERISTIEKE COMBINATIES

VERPLAATSINGEN

[mm]

Karakteristieke combinatie



REACTIES

Karakteristieke combinatie

| Kn. | X-min | X-max | Z-min | Z-max | M-min | M-max |
|-----|-------|-------|-------|-------|-------|-------|
| 1 | -3.45 | 3.82 | 7.47 | 35.02 | -2.85 | 2.94 |
| 6 | -3.82 | 3.45 | 7.47 | 35.02 | -2.94 | 2.85 |

STAALPROFIELEN - ALGEMENE GEGEVENS

| | | |
|------------------------------|---|-------------|
| Stabiliteit: | Classificatie gehele constructie: | Ongeschoord |
| | Belastinggeval m.b.t. bepaling kniklengte: | 16=Knik |
| | Aanpassing inkl. parameter C : | Nee |
| Tweede-orde-effect: | | |
| | Aan te houden verhouding n/(n-1) voor steunmomenten en verplaatsingen: | 1.10 |
| Doorbuiging en verplaatsing: | | |
| | Aantal bouwlagen: | 1 |
| | Gebouwtype: | Industrieel |
| | Toel. horiz. verplaatsing gehele gebouw: | h/150 |
| | Kleinste gevelhoogte [m]: | 0.0 |

PROFIEL/MATERIAAL

| P/M nr. | Profielnaam | Vloeisp. [N/mm ²] | Productie methode | Min. drsn. klasse |
|---------|-------------|-------------------------------|-------------------|-------------------|
| 1 | HEA160 | 235 | Gewalst | 1 |
| 2 | HEA140 | 235 | Gewalst | 1 |
| 3 | HEA140 | 235 | Gewalst | 1 |

Partiële veiligheidsfactoren:

Gamma M;0 : 1.00 Gamma M;1 : 1.00

KNIKSTABILITEIT

| Staafl | l _{sys} [m] | Classif. y sterke as | l _{knik;y} [m] | Extra | | Extra | |
|--------|----------------------|----------------------|-------------------------|--------------|----------------------|-------------------------|--------------|
| | | | | aanp. y [kN] | Classif. z zwakke as | l _{knik;z} [m] | aanp. z [kN] |
| 1-2 | 7.500 | Ongeschoord | 14.681 | 0.0 | Geschoord | 7.500 | 0.0 |
| 3 | 3.000 | Ongeschoord | 3.981 | 0.0 | Geschoord | 3.000 | 0.0 |
| 4-5 | 7.500 | Ongeschoord | 14.681 | 0.0 | Geschoord | 7.500 | 0.0 |
| 6 | 3.000 | Ongeschoord | 3.964 | 0.0 | Geschoord | 3.000 | 0.0 |

KIPSTABILITEIT

| Staafl | Plts. aangr. | l gaffel [m] | Kipsteunafstanden [m] | |
|--------|--------------|--------------|-----------------------|-------------|
| 1-2 | 1.0*h | boven: | 7.50 | 7.500 |
| | | onder: | 7.50 | 7.500 |
| 3 | 1.0*h | boven: | 3.00 | 3.000 |
| | | onder: | 3.00 | 3.000 |
| 4-5 | 1.0*h | boven: | 7.50 | 3,765;3,735 |
| | | onder: | 7.50 | 3,765;3,735 |
| 6 | 1.0*h | boven: | 3.00 | 3.000 |
| | | onder: | 3.00 | 3.000 |

TOETSING SPANNINGEN

| Staafr. nr. | P/M | BC | Sit | Kl | Plaats | Norm | Artikel | Formule | Hoogste toetsing U.C. [N/mm ²] | Opm. |
|----------------|-----|----|-----|----|---------|---------|---------|---------|---|----------|
| 1-2 | 1 | 62 | 1 | 1 | Staafr. | EN3-1-1 | 6.3.3 | (6.61) | 0.558 131 | 42,46,47 |
| 3 | 2 | 61 | 1 | 1 | Begin | EN3-1-1 | 6.2.10 | (6.31) | 0.173 41 | 46 |
| 4-5 | 1 | 57 | 1 | 1 | Staafr. | EN3-1-1 | 6.3.3 | (6.61) | 0.511 120 | 42,46,47 |
| 6 | 3 | 59 | 1 | 1 | Begin | EN3-1-1 | 6.2.10 | (6.31) | 0.303 71 | |

Opmerkingen:

- [42] **Waarschuwing: Er sluiten tussentijds staven en/of opleggingen aan.**
- [46] T.b.v. kip is een equivalente Q-last berekend.
- [47] Bij verlopende normaalkracht wordt de grootste drukkracht genomen.

TOETSING DOORBUIGING

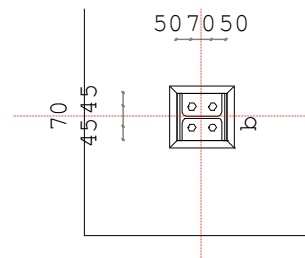
| Staafr. | Soort | Mtg | Lengte [m] | Overst I | Zeeg J | u _{t o t} [mm] | BC | Sit | u [mm] | Toelaatbaar [mm] | *1 |
|---------|-------|-----|---------------|-------------|-----------|----------------------------|----|-----------|-----------|---------------------|-------|
| 3 | Dak | db | 3.00 | N | N | 0.0 | 88 | 1 Eind | -0.7 | -12.0 | 0.004 |
| | | db | | | | | | 88 1 Bijk | -0.4 | -12.0 | 0.004 |
| 6 | Vloer | db | 3.00 | N | N | 0.0 | 89 | 1 Eind | -2.3 | ±12.0 | 0.004 |
| | | db | | | | | | 89 1 Bijk | -2.3 | ±9.0 | 0.003 |

8.5.1 Verbindingen

VERBINDINGEN - BASISGEGEVENS

Voetpl:1

| | |
|---|--------------------|
| Verbindingstype | Voetplaat |
| Knopen | 1,6 |
| Rekenwaarde vloeispanning $f_y; d$ platen | 235 |
| Hoek basis staaf AB t.o.v. globale as (linksom positief) | 0 |
| Classificatie constructie | Ongeschoord |
| Rekenmodel gebruikt bij de mechanicaresultaten | 1e orde elastisch |
| Statisch systeem | Statisch onbepaald |
| Verbinding t.p.v. plastisch scharnier | Nee |
| Alternatieve methode T-stuk volgens EN 1993-1-8 tabel 6.2 | Ja |
| Is poer gewapend? | Ja |



LEGENDA

| Onderdeel | Afmetingen | Aantal Lassen (d=dubb. hoeklas) |
|-------------|------------|---------------------------------|
| a Voetplaat | 160x170-15 | 1 $a_w=3d$ $a_f=5d$ |
| b Anker | M16 4.6 | 4 $L_{b1}=400$ $L_{b,tot}=53$ |

PROFIELEN

| Naam | Lengte | Prod.meth. | Exc | Hoek | f_y, d | |
|----------|--------|------------|---------|------|----------|-----|
| Staaft C | HEA160 | 3735 | Gewalst | 0 | 0 | 235 |

PROFIELGEGEVENS [mm]

| | | | Gewalst Klasse 1 HEA160 | | | |
|---------|-------|--------------|-------------------------|--------|---------------------|-------------------|
| h : | 152.0 | $i_y :$ 65.7 | A : | 3880.0 | $W_{e,y} :$ 220.1E3 | $I_y :$ 1673.0E4 |
| b : | 160.0 | $i_z :$ 39.8 | | | $W_{e,z} :$ 76.9E3 | $I_z :$ 616.0E4 |
| $t_w :$ | 6.0 | r : | 15.0 | | $W_{p,y} :$ 245.2E3 | $I_t :$ 12.1E4 |
| $t_f :$ | 9.0 | | | | $W_{p,z} :$ 117.6E3 | $I_w :$ 31409.7E6 |

PLATEN

| Plaats | h | b | t | Exc | a_w | a_f | a_e | Hoek | Las | f_y, d |
|-----------|----------|-----|-----|------|-------|------------------|------------------|------|-----|----------|
| Voetplaat | Staaft C | 170 | 160 | 15.0 | 0 | $\Delta\Delta 3$ | $\Delta\Delta 5$ | | | 235 |

Δ = Enkele stompe of hoeklas of dubbele hoeklas met slechts 1 las effectief

$\Delta\Delta$ = Dubbele hoeklas

ANKERS

| d | kw | hoh | milieu | lengte | v (vanaf zijde C) |
|----------|-----|-----|--------|------------|-------------------|
| Staaft C | M16 | 4.6 | 70 | Niet-corr. | 400 50;120 |

ANKERGEGEVENS

| d | d ₀ | d _m | d _{kop} | t _{kop} | d _{moer} | t _{moer} | A | A _s | γ _M | f _{ybd} | f _{tbd} | Draad |
|------|----------------|----------------|------------------|------------------|-------------------|-------------------|-------|----------------|----------------|------------------|------------------|--------|
| 16.0 | 20.0 | 33.3 | 24.0 | 10.0 | 24.0 | 13.0 | 201.1 | 156.7 | 1.25 | 240 | 400 | Gerold |

BETON EN VOEG

| | Lengte | Breedte | Dikte | Helling | Kwaliteit |
|------|--------|---------|-------|---------|-----------|
| Voeg | 170 | 160 | 25.0 | 45.0 | C20/25 |

KRACHTEN

Kn:6 BC:22 Sit:1

| | Normaalkr. | Dwarskr. | Moment | MSteun | DSteun |
|----------|------------|----------|--------|--------|--------|
| Staaft C | 2.75 | -5.29 | -4.56 | 0.46 | -0.53 |

RESULTATEN DRUKZONE

Kn:6 BC:22 Sit:1

| | | | | | |
|-------------------------------|--------------------|---|----------|-------------------------|-------|
| Vergrotingsfactor | k _c | : | 3.00 | | |
| Rekenwaarde druksterkte | f'_{c,Rd} | : | 13.33 | | |
| Rekenwaarde druksterkte | f_{jd} | : | 26.67 | | |
| Vorm van de indrukkingsprent | | : | I-vormig | 43 * | 160 |
| | | : | | 82 * | 0 |
| | | : | | 43 * | 160 |
| Max. drukoppervlakte | | : | | | 13995 |
| Spreidingsmaat // flenzen | l _s | : | 25.71 | | |
| Spreidingsmaat // lijf | l_{s lijf} | : | 25.71 | | |
| Rek meest gedrukte zijde | eps _c | : | 0.00051 | | |
| Spanning meest gedrukte zijde | sigma _c | : | 11.93 | | |
| Rek getrokken zijde | eps _t | : | -0.00071 | | |
| Momentcapaciteit | | : | 11.09 | | |
| Moment tbv. lassen | | : | 46.10 | gebaseerd op 0.8*MplRd | |
| Max. opneembare dwarskracht | | : | 74.36 | Crit.: Afsch.cap.ankers | |
| Trekcapaciteit ankerrij | | : | 90.26 | | |

RESULTATEN TREKZONE

Kn:6 BC:22 Sit:1

| Rij | F _{t,Rd} | Arm | Moment |
|-----|-------------------|-------|--------|
| 2 | 0.00 | 33.7 | 0.00 |
| 1 | 46.72 | 103.7 | 4.85 |

TUSSENRESULTATEN STIJFHEID

Kn:6 BC:22 Sit:1

| bij M _{v,Rd} voor boutrij binnen trekflens (h ₁) | | | | Staaft C |
|---|------------------------|----------------|-----------------|----------|
| i | Onderdeel | k _i | mu _i | Bijdrage |
| 13 | Drukzone beton | 1.845 | 2.988 | 44% |
| 15 | Buiging/trek voetplaat | 7.929 | 2.988 | 10% |
| 16 | Trekzone ankerbout | 1.796 | 2.988 | 45% |

STIJFHEID

Kn:6 BC:22 Sit:1

Maatgevend criterium: Trekzone ankerbout

Staaft C

| Verh. | M _{v,Rd} /Verh. | Arm | S _j | φ |
|-------|--------------------------|-----|----------------|---------|
| 1.0 | 11.09 | 98 | 553 | 0.02004 |
| 1.2 | 9.24 | 98 | 905 | 0.01021 |
| 1.5 | 7.39 | 98 | 1654 | 0.00447 |

Bij een moment M_{v,Ed}=5.02 geldt een stijfheid S_j=1654.
De in mechanica gebruikte stijfheid is S=1658 kNm/rad.

TOETSING VOETPLAAT-VERBINDING

Kn:6 BC:22 Sit:1

| Artikel | | | | Toetsing |
|---------|--------------------------------------|---|---------|--------------|
| 6.2.6.5 | m _{Ed} / m _{pl,Rd} | = | 9681 / | 13219 = 0.73 |
| 6.2.6.5 | σ _{Ed} / f _{jd} | = | 11.93 / | 26.67 = 0.45 |

TOETSING PROFIELEN EN AFSCHUIVING

Kn:6 BC:22 Sit:1

| Plaats | Profiel | Artikel | Formule | Toetsing |
|----------|---------|---------|-----------------|----------|
| Staaft C | HEA160 | EN3-1-1 | 6.2.10 (6.31) | 0.09 |
| | | EN3-1-1 | 6.2.8 (6.30) | 0.09 |
| | | EN3-1-1 | 6.2.5 (6.12y) | 0.09 |
| | | EN3-1-1 | 6.2.6 (6.17) | 0.03 |
| | | EN3-1-1 | 6.2.1 (6) N+D | 0.04 |
| | | EN3-1-8 | 6.2.2 (7) (6.2) | 0.08 |

MOMENTCLASSIFICATIE EN3-1-8 art.5.2.3

Kn:6 BC:22 Sit:1

| Plaats | $M_{v,Rd}$ | $M_{v,Rd,staaf}$ | Classificatie |
|----------|------------|------------------|---------------|
| Staaft C | 11.09 | 57.62 | Scharnierend |

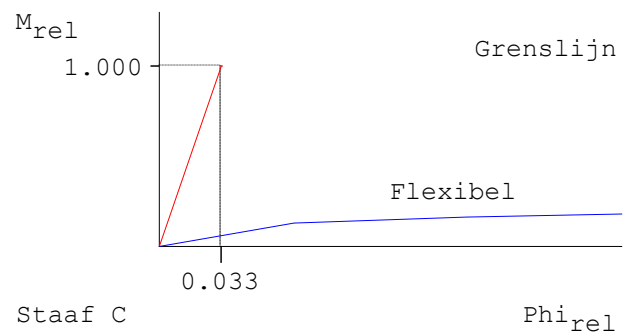
STIJFHEIDSClassificatie EN3-1-8 art.5.2.2

Kn:6 BC:22 Sit:1

| Plaats | Punt | Grenswaarden | | Actuele waarden | | Classificatie |
|----------|------|--------------|-----------|-----------------|-----------|---------------|
| | | Φ_{rel} | m_{rel} | Φ_{rel} | m_{rel} | |
| Staaft C | 1 | 0.000 | 0.000 | 0.000 | 0.000 | Flexibel |
| | 2 | 0.033 | 1.000 | 0.073 | 0.128 | |
| | 3 | 0.033 | 1.000 | 0.167 | 0.160 | |
| | 4 | 0.033 | 1.000 | 0.327 | 0.192 | |

M-PHI DIAGRAM EN3-1-8 fig. 5.4 Ongeschoord

Kn:6 BC:22 Sit:1



CONTROLES

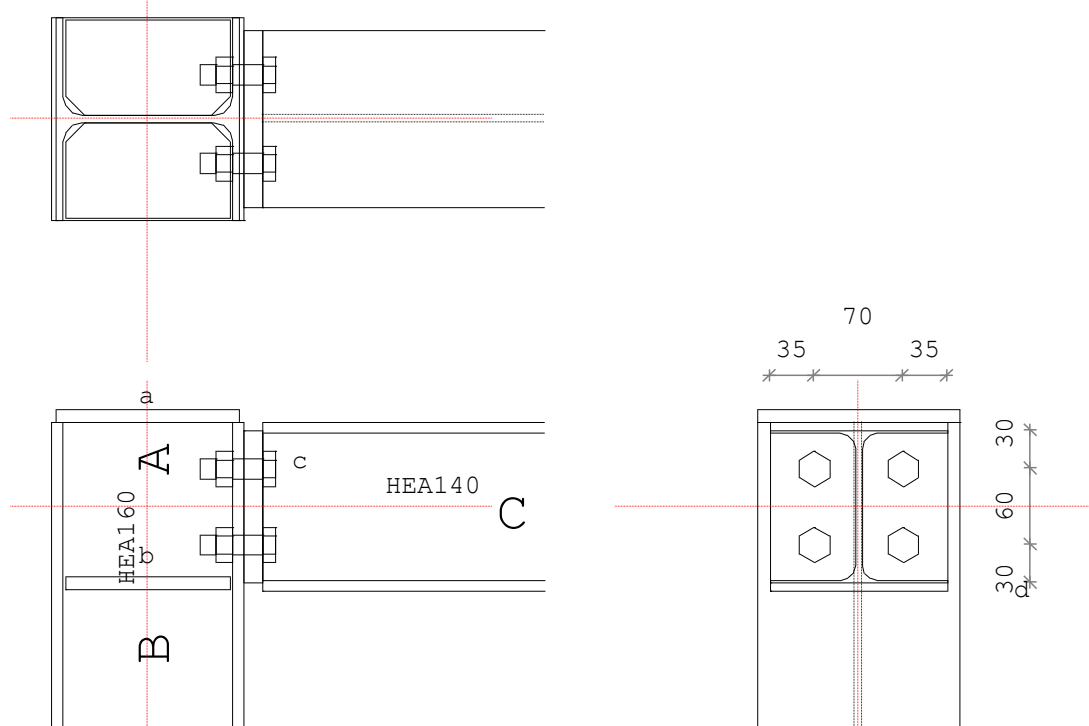
Kn:6 BC:22 Sit:1

| Onderdeel | Plaats | Rij | Item | Ernst | Art./ (Frm.) | Min. | Waarde | Max. |
|---------------|----------|-----|-------------------------|-----------|--------------|------|--------|-------|
| Anker | Staaft C | 1 | HOH-afstand p1 | 3.5 | (1) | 44.0 | 70.0 | |
| | | 1 | HOH-afstand p2 | 3.5 | (1) | 48.0 | 70.0 | 112.0 |
| | | 2 | HOH-afstand p2 | 3.5 | (1) | 48.0 | 70.0 | 112.0 |
| Anker (Plaat) | Staaft C | 1 | Eindafstand e1 | 3.5 | (1) | 24.0 | 50.0 | |
| | | 2 | Eindafstand e1 | 3.5 | (1) | 24.0 | 50.0 | |
| Voeg | Staaft C | | Betonsterkte | 6.2.5 | | 4.0 | 20.0 | |
| | | | Dikte | 6.2.5 | | 25.0 | 32.0 | |
| Voetplaat | Staaft C | | Dikte | 6.2.4 | | 12.8 | 15.0 | |
| | | | Flenslas $\Delta\Delta$ | 0.8*MplRd | | 3.32 | 5.00 | |
| | | | Lijflas $\Delta\Delta$ | 0.8*MplRd | | 3.00 | 3.00 | |
| | | | Positie boven | | | 83.1 | 85.0 | |
| | | | Positie onder | | | | -85.0 | -83.1 |

VERBINDINGEN - BASISGEGEVENS

Knie:1

| | |
|---|--------------------|
| Verbindingstype | Knie Gebout |
| Knopen | 3,4 |
| Rekenwaarde vloeispanning $f_y; d$ platen | 235 |
| Hoek basis staaf AB t.o.v. globale as (linksom positief) | 270 |
| Classificatie constructie | Ongeschoord |
| Classificatie lijf staaf AB | Geschoord |
| Afschuiving lijf staaf AB actief? | Ja |
| Rekenmodel gebruikt bij de mechanicaresultaten | 1e orde elastisch |
| Statisch systeem | Statisch onbepaald |
| Verbinding t.p.v. plastisch scharnier | Ja |
| Alternatieve methode T-stuk volgens EN 1993-1-8 tabel 6.2 | Ja |



LEGENDA

| Onderdeel | Afmetingen | Aantal | Lassen (d=dubb. hoeklas) |
|--------------|------------|--------|--------------------------|
| a Afdekplaat | 160x145-10 | 1 | aw=3d af=9 |
| b Schot AB | 75x130-10 | 1 | aw=5d af=5d |
| c Kopplaat | 140x120-15 | 1 | aw=3d af=4d |
| d Bout | M16 8.8 | 4 | |

PROFIELEN

| | Naam | Lengte | Prod.meth. | Exc | Hoek | $f_y; d$ |
|----------|--------|--------|------------|-----|------|----------|
| Staaft B | HEA160 | 3735 | Gewalst | 0 | 270 | 235 |
| Staaft C | HEA140 | 3000 | Gewalst | 0 | 0 | 235 |
| Staaft A | | 66 | | | | |

PROFIELGEGEVENS [mm]

| | | | | Gewalst Klasse 1 HEA160 | | | | | |
|---------|-------|---------|------|-------------------------|--------|-------------|---------|---------|-----------|
| h : | 152.0 | $i_y :$ | 65.7 | A : | 3880.0 | $W_{e_y} :$ | 220.1E3 | $I_y :$ | 1673.0E4 |
| b : | 160.0 | $i_z :$ | 39.8 | | | $W_{e_z} :$ | 76.9E3 | $I_z :$ | 616.0E4 |
| $t_w :$ | 6.0 | r : | 15.0 | | | $W_{p_y} :$ | 245.2E3 | $I_t :$ | 12.1E4 |
| $t_f :$ | 9.0 | | | | | $W_{p_z} :$ | 117.6E3 | $I_w :$ | 31409.7E6 |

PROFIELGEGEVENS [mm]

| PROFIELGEGEVENS [mm] | | | | Gewalst Klasse 1 HEA140 | | | | | |
|----------------------|-------|------------------|------|-------------------------|--------|--------------------|---------|------------------|-----------|
| h : | 133.0 | i _y : | 57.3 | A : | 3142.0 | W _{e y} : | 155.4E3 | I _y : | 1033.0E4 |
| b : | 140.0 | i _z : | 35.2 | | | W _{e z} : | 55.6E3 | I _z : | 389.0E4 |
| t _w : | 5.5 | r : | 12.0 | | | W _{p y} : | 173.4E3 | I _t : | 8.1E4 |
| t _f : | 8.5 | | | | | W _{p z} : | 84.8E3 | I _w : | 15063.7E6 |

PLATEN

| Plaats | h | b | t | Exc | a _w | a _f | a _e | Hoek | Las | f _{y, d} |
|------------|----------|-----|-----|------|----------------|----------------|----------------|------|-----|-------------------|
| Kopplaat | Staaft C | 120 | 140 | 15.0 | 0 | ΔΔ3 | ΔΔ4 | | | 235 |
| Schot | Staaft B | 130 | 75 | 10.0 | -60 | ΔΔ5 | ΔΔ5 | 0 | | 235 |
| Afdekplaat | | 145 | 160 | 10.0 | 0 | ΔΔ3 | Δ9 | 0 | | 235 |

Δ = Enkele stompe of hoeklas of dubbele hoeklas met slechts 1 las effectief
ΔΔ = Dubbele hoeklas

BOUTEN

| d | kw | hoh | milieu | lengte | v (vanaf zijde B) |
|----------|-----|-----|--------|------------|-------------------|
| Staaft C | M16 | 8.8 | 70 | Niet-corr. | 36 30;90 |

BOUTGEGEVENS

| d | d ₀ | d _m | d _{kop} | t _{kop} | d _{moer} | t _{moer} | A | A _s | γ _M | f _{ybd} | f _{tbd} | Draad |
|------|----------------|----------------|------------------|------------------|-------------------|-------------------|-------|----------------|----------------|------------------|------------------|--------|
| 16.0 | 18.0 | 33.3 | 24.0 | 10.0 | 24.0 | 13.0 | 201.1 | 156.7 | 1.25 | 640 | 800 | Gerold |

KRACHTEN

| | Normaalkr. | Dwarskr. | Moment | MSteun | DSteun |
|----------|------------|----------|--------|--------|--------|
| Staaft B | 24.19 | -4.18 | -11.80 | 1.18 | -0.42 |
| Staaft C | 1.01 | 5.43 | 6.42 | 0.64 | 0.54 |

Kn:3 BC:61 Sit:1

BEZWIJKKRACHTEN

| Onderdeel | F _{Rd} | Formule | b _{eff} | Staaft C |
|------------------------------|-----------------|---------|------------------|---------------------------------|
| Afsch. lijf staaft AB | 161.67 | (6.7) | Avc= 1324 | omega=0.80 beta=1.00 |
| Druk lijf staaft AB | 452.30 | (6.9) | 142.7 | Drukpunt 0.00 |
| Plooi lijf staaft AB | 452.30 | | 142.7 | kwc=1.00 l _{rel} =0.63 |
| Drukzone kopplaat staaft C/D | 326.29 | (6.21) | | |
| Trek bout | 90.26 | | | |
| Trek boutrij | 180.52 | | | |

Let op: De normaalkracht is verwerkt in bovengenoemde bezwijkkrachten.
Dwarskrachtcapaciteiten:
Stuik flens staaft AB 385.92 (6.7)
Stuik kopplaat 489.60 (6.7)
Afsch.cap. bouten na red. trek 163.70 (6.7)

TUSSENRESULTATEN KOLOMFLENS BUIGING

| Rij | p | m ₁ | e | n | m ₂ | alpha | l _{ef} | Formule | F _{t,fc,Rd} | Bezw.vorm |
|------|----|----------------|------|------|----------------|-------|-----------------|----------|----------------------|------------|
| 2 | 60 | 20.0 | 45.0 | 25.0 | 26.3 | 2*pi | 125.7 | T6.2v2 | 126.87 | 2=Plt+Bout |
| 1 | 60 | 20.0 | 45.0 | 25.0 | 19.3 | 2*pi | 125.7 | T6.2v2 | 126.87 | 2=Plt+Bout |
| 1- 2 | | | | | | | 175.1 | T6.2v1m2 | 225.34 | 1=Plt |

Kn:3 BC:61 Sit:1
Staaft C

TUSSENRESULTATEN KOPPLAAT BUIGING

| Rij | p | m ₁ | e | n | m ₂ | alpha | l _{ef} | Formule | F _{t,ep,Rd} | Bezw.vorm |
|------|----|----------------|------|------|----------------|-------|-----------------|---------|----------------------|------------|
| 2 | 60 | 28.9 | 35.0 | 35.0 | 23.5 | 2*pi | 181.3 | T6.2v2 | 174.01 | 2=Plt+Bout |
| 1 | 60 | 28.9 | 35.0 | 35.0 | 23.5 | 2*pi | 181.3 | T6.2v2 | 174.01 | 2=Plt+Bout |
| 1- 2 | | | | | | | 263.4 | T6.2v2 | 306.96 | 2=Plt+Bout |

Kn:3 BC:61 Sit:1
Staaft C

TUSSENRESULTATEN OVERIG

Kn:3 BC:61 Sit:1

| Rij | Trek lijf staaf AB 6.2.6.3 (6.15) | | Trek lijf staaf C/D 6.2.6.8 (6.22) | | Lassen Staaf C 4.5.3.2 (4.1) | |
|------|--------------------------------------|---------------|---------------------------------------|---------------|---------------------------------|------------|
| | b_{ef} | $F_{t,wc,Rd}$ | b_{ef} | $F_{t,wb,Rd}$ | b_{ef} | $F_{w,Rd}$ |
| 2 | 125.7 | 148.61 | 181.3 | 234.34 | 181.3 | 162.89 |
| 1 | 125.7 | 148.61 | 181.3 | 234.34 | 181.3 | 162.67 |
| 1- 2 | 175.1 | 183.07 | 263.4 | 340.49 | 263.4 | 236.68 |

BOU TRIJKRACHTEN

Herverdeling: Nee

Kn:3 BC:61 Sit:1

EN3-1-8 art. 6.2.7.2 Reductie : Ja Staaf C

| Rij | $F_{t,Rd,her}$ | $F_{t,Rd}$ | Arm | M | Criterium |
|----------------------|----------------|------------|--------------|---------------|--------------------------------|
| 2 | 126.87 | 126.87 | 90.0 | 11.42 | Flens staaf AB: Plaat+Bout |
| 1 | 56.20 | 34.81 | 30.0 | 1.04 | Trek lijf staaf AB |
| Som F= | | 161.67 | $M_{v,Rd} =$ | 12.46 | Afsch. lijf staaf AB |
| Moment tbv. lassen = | | | 40.75 | | gebaseerd op 1.0*MplRd |
| | | | $V_{v,Rd} =$ | 163.70 | Afsch.cap. bouten na red. trek |

TUSSENRESULTATEN STIJFHEID

Kn:3 BC:61 Sit:1

bij $M_{v,Rd}$ voor bou trij binnen trekflens (h_1)

Staaf C

| i | Onderdeel | k_i | μ_i | Bijdrage |
|----|----------------------------|--------|---------|----------|
| 1 | Afschuifzone lijf staaf AB | 6.835 | 2.988 | 33% |
| 2 | Drukzone lijf staaf AB | n.v.t. | | |
| 3 | Trekzone lijf staaf AB | 9.087 | 2.988 | 25% |
| 4 | Trekzone flens staaf AB | 17.611 | 2.988 | 13% |
| 5 | Trekzone kopplaat | 27.147 | 2.988 | 8% |
| 10 | Trekzone bouten | 11.514 | 2.988 | 20% |

STIJFHEID

Kn:3 BC:61 Sit:1

Maatgevend criterium: Afschuifzone lijf staaf AB

Staaf C

| Verh. | $M_{v,Rd}/Verh.$ | Arm | S_j | ϕ |
|-------|------------------|-----|------------|---------|
| 1.0 | 12.46 | 74 | 869 | 0.01435 |
| 1.2 | 10.39 | 74 | 1421 | 0.00731 |
| 1.5 | 8.31 | 74 | 2596 | 0.00320 |

Bij een moment $M_{v,Ed}=7.06$ geldt een stijfheid $S_j=2596$.

De in mechanica gebruikte stijfheid is $S=2596$ kNm/rad.

TOETSING VERBINDING

Kn:3 BC:61 Sit:1

| Artikel | $M_{v,Ed}$ | $M_{v,Rd}$ | Z | $V_{wp,Ed}$ | $V_{wp,Rd}$ | Toetsing |
|---------|------------|------------|----|-------------|-------------|----------|
| 6.2.7.1 | 7.06 | 12.46 | | | | 0.57 |
| 6.2.6.1 | | | 77 | -4.60 | 161.67 | 0.03 |

Let op: Normalkrachten in staven C & D zijn verwerkt in de bezwijk- en/of de bou trijkrachten. De conservatieve toetsingsformule van EN 1993-1-8 art. 6.2.7.1 (3) is niet gebruikt.

TOETSING PROFIELEN EN AFSCHUIVING

Kn:3 BC:61 Sit:1

| Plaats | Profiel | Artikel | Formule | Toetsing |
|---------|---------|---------|---------------|----------|
| Staaf B | HEA160 | EN3-1-1 | 6.2.10 (6.31) | 0.23 |
| | | EN3-1-1 | 6.2.8 (6.30) | 0.23 |
| | | EN3-1-1 | 6.2.5 (6.12y) | 0.23 |
| | | EN3-1-1 | 6.2.6 (6.17) | 0.03 |
| | | EN3-1-1 | 6.2.4 (6.9) | 0.03 |
| | | EN3-1-1 | 6.2.1(6) N+D | 0.05 |
| Staaf C | HEA140 | EN3-1-1 | 6.2.10 (6.31) | 0.17 |
| | | EN3-1-1 | 6.2.8 (6.30) | 0.17 |
| | | EN3-1-1 | 6.2.5 (6.12y) | 0.17 |

| | | | |
|---------|----------|--------|------|
| EN3-1-1 | 6.2.6 | (6.17) | 0.04 |
| EN3-1-1 | 6.2.1(6) | N+D | 0.04 |
| EN3-1-8 | T.3.4 | | 0.04 |

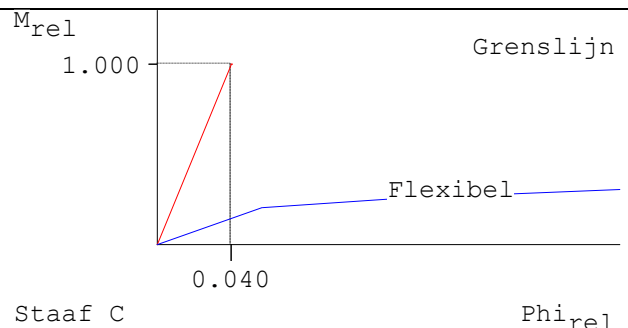
MOMENTCLASSIFICATIE EN3-1-8 art.5.2.3 Kn:3 BC:61 Sit:1

| Plaats | $M_{v,Rd}$ | $M_{v,Rd,staaf}$ | Classificatie |
|---------|------------|------------------|---------------------|
| Staaf C | 12.46 | 40.75 | Niet volledig sterk |

STIJFHEIDSClassificatie EN3-1-8 art.5.2.2 Kn:3 BC:61 Sit:1

| Plaats | Punt | Grenswaarden | | Actuele waarden | | Classificatie |
|---------|------|--------------|-----------|-----------------|-----------|---------------|
| | | Φ_{rel} | m_{rel} | Φ_{rel} | m_{rel} | |
| Staaf C | 1 | 0.000 | 0.000 | 0.000 | 0.000 | Flexibel |
| | 2 | 0.040 | 1.000 | 0.057 | 0.204 | |
| | 3 | 0.040 | 1.000 | 0.130 | 0.255 | |
| | 4 | 0.040 | 1.000 | 0.255 | 0.306 | |

M-PHI DIAGRAM EN3-1-8 fig. 5.4 Ongeschoord Kn:3 BC:61 Sit:1



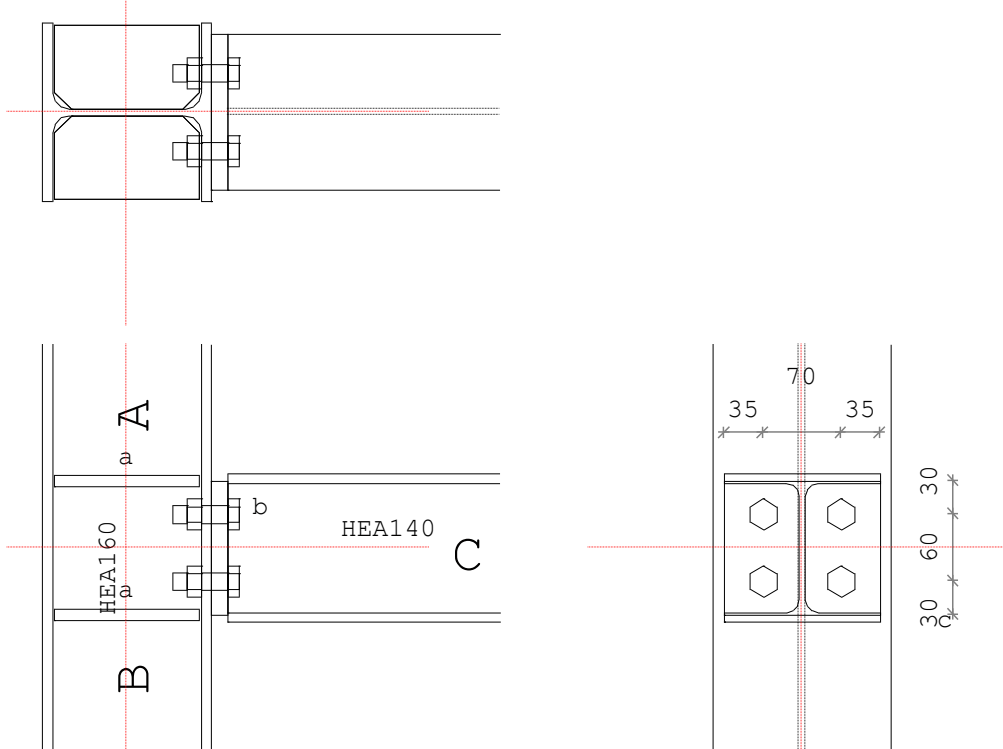
CONTROLES

| Onderdeel | Plaats | Rij Item | Ernst Art./ (Frm.) | Min. Waarde | Max. |
|--------------|---------|-------------------------|--------------------|-------------|-------------|
| Afdekplaat | Staaf C | Dikte | frmb 5.2.a | 2.8 | 10.0 |
| | Staaf C | Flenslas Δ | 1.0*MplRd | 8.31 | 9.00 |
| | Staaf C | Lengte | | 139.0 | 145.0 152.0 |
| Bout | Staaf C | Lijflas $\Delta\Delta$ | 1.0*MplRd | 3.00 | 3.00 |
| | Staaf C | 1 HOH-afstand p1 | 3.5(1) | 39.6 | 60.0 126.0 |
| | Staaf C | 1 HOH-afstand p2 | 3.5(1) | 69.3 | 70.0 96.8 |
| Bout (Flens) | Staaf C | 2 HOH-afstand p2 | 3.5(1) | 69.3 | 70.0 96.8 |
| | Staaf C | 2 Eindafstand e1 | 3.5(1) | 21.6 | 36.5 |
| Bout (Plaat) | Staaf C | 1 Eindafstand e1 | 3.5(1) | 21.6 | 30.0 |
| | Staaf C | 2 Eindafstand e1 | 3.5(1) | 21.6 | 30.0 |
| Kopplaat | Staaf C | Flenslas $\Delta\Delta$ | 1.0*MplRd | 3.92 | 4.00 |
| | Staaf C | Lijflas $\Delta\Delta$ | 1.0*MplRd | 3.00 | 3.00 |
| | Staaf C | Positie boven | | | 60.0 60.8 |
| | Staaf C | Positie onder | | -60.8 | -60.0 |
| Schot AB | Staaf B | Dikte | frmb 5.6.a | 4.3 | 10.0 |
| | Staaf B | Lengte | | 124.0 | 130.0 134.0 |
| | Staaf B | Lijflas $\Delta\Delta$ | 1.0*MplRd | 3.08 | 5.00 |

VERBINDINGEN - BASISGEGEVENS

T1:1

| | |
|---|--------------------|
| Verbindingstype | T-1 Gebout |
| Knopen | 2,5 |
| Rekenwaarde vloeispanning $f_y; d$ platen | 235 |
| Hoek basis staaf AB t.o.v. globale as (linksom positief) | 270 |
| Classificatie constructie | Ongeschoord |
| Classificatie lijf staaf AB | Geschoord |
| Afschuiving lijf staaf AB actief? | Ja |
| Rekenmodel gebruikt bij de mechanicaresultaten | 1e orde elastisch |
| Statisch systeem | Statisch onbepaald |
| Verbinding t.p.v. plastisch scharnier | Ja |
| Alternatieve methode T-stuk volgens EN 1993-1-8 tabel 6.2 | Ja |



LEGENDA

| Onderdeel | Afmetingen | Aantal | Lassen (d=dubb. hoeklas) |
|------------|------------|--------|--------------------------|
| a Schot AB | 75x130-10 | 2 | aw=5d af=5d |
| b Kopplaat | 140x120-15 | 1 | aw=3d af=4d |
| c Bout | M16 8.8 | 4 | |

PROFIELEN

| | Naam | Lengte | Prod.meth. | Exc | Hoek | $f_y; d$ |
|----------|--------|--------|------------|-----|------|----------|
| Staaft B | HEA160 | 3735 | Gewalst | 0 | 270 | 235 |
| Staaft C | HEA140 | 3000 | Gewalst | 0 | 0 | 235 |
| Staaft A | | 3765 | | | | |

PROFIELGEGEVENS [mm]

| | | | | Gewalst Klasse 1 HEA160 | | | | | |
|---------|-------|---------|------|-------------------------|--------|------------|---------|---------|-----------|
| h : | 152.0 | $i_y :$ | 65.7 | A : | 3880.0 | $W_{ey} :$ | 220.1E3 | $I_y :$ | 1673.0E4 |
| b : | 160.0 | $i_z :$ | 39.8 | | | $W_{ez} :$ | 76.9E3 | $I_z :$ | 616.0E4 |
| $t_w :$ | 6.0 | r : | 15.0 | | | $W_{py} :$ | 245.2E3 | $I_t :$ | 12.1E4 |
| $t_f :$ | 9.0 | | | | | $W_{pz} :$ | 117.6E3 | $I_w :$ | 31409.7E6 |

PROFIELGEGEVENS [mm]

| PROFIELGEGEVENS [mm] | | | | Gewalst Klasse 1 HEA140 | | | | | |
|----------------------|-------|------------------|------|-------------------------|--------|-------------------|---------|------------------|-----------|
| h : | 133.0 | i _y : | 57.3 | A : | 3142.0 | W _{ey} : | 155.4E3 | I _y : | 1033.0E4 |
| b : | 140.0 | i _z : | 35.2 | | | W _{ez} : | 55.6E3 | I _z : | 389.0E4 |
| t _w : | 5.5 | r : | 12.0 | | | W _{py} : | 173.4E3 | I _t : | 8.1E4 |
| t _f : | 8.5 | | | | | W _{pz} : | 84.8E3 | I _w : | 15063.7E6 |

PLATEN

| | Plaats | h | b | t | Exc | a _w | a _f | a _e | Hoek | Las | f _{y,d} |
|----------|---------|-----|-----|------|-----|----------------|----------------|----------------|------|-----|------------------|
| Kopplaat | Staaf C | 120 | 140 | 15.0 | 0 | ΔΔ3 | ΔΔ4 | | | | 235 |
| Schot | Staaf A | 130 | 75 | 10.0 | 60 | ΔΔ5 | ΔΔ5 | | 0 | | 235 |
| Schot | Staaf B | 130 | 75 | 10.0 | -60 | ΔΔ5 | ΔΔ5 | | 0 | | 235 |

Δ = Enkele stompe of hoeklas of dubbele hoeklas met slechts 1 las effectief
ΔΔ = Dubbele hoeklas

BOUTEN

| | d | kw | hoh | milieu | lengte | v (vanaf zijde B) |
|---------|-----|-----|-----|------------|--------|-------------------|
| Staaf C | M16 | 8.8 | 70 | Niet-corr. | 36 | 30;90 |

BOUTGEGEVENS

| d | d ₀ | d _m | d _{kop} | t _{kop} | d _{moer} | t _{moer} | A | A _s | γ _M | f _{ybd} | f _{tbd} | Draad |
|------|----------------|----------------|------------------|------------------|-------------------|-------------------|-------|----------------|----------------|------------------|------------------|--------|
| 16.0 | 18.0 | 33.3 | 24.0 | 10.0 | 24.0 | 13.0 | 201.1 | 156.7 | 1.25 | 640 | 800 | Gerold |

KRACHTEN

| | Normaalkr. | Dwarskr. | Moment | MSteun | DSteun | Kn:2 BC:60 Sit:1 |
|---------|------------|----------|--------|--------|--------|------------------|
| Staaf A | 5.72 | -3.23 | -0.30 | 0.03 | -0.32 | |
| Staaf B | 23.11 | -2.91 | -10.92 | 1.09 | -0.29 | |
| Staaf C | -0.32 | 17.39 | 11.22 | 1.12 | 1.74 | |

BEZWIJKKRACHTEN

| Onderdeel | F _{Rd} | Formule | b _{eff} | Staat C | Kn:2 BC:60 Sit:1 |
|-----------------------------|-----------------|---------|------------------|---------------------------------|----------------------|
| Afsch. lijf staaf AB | 187.05 | (6.7) | Avc= | 1324 | omega=0.80 beta=1.00 |
| Druk lijf staaf AB | 453.63 | (6.9) | 142.7 | Drukpunt | 0.00 |
| Plooi lijf staaf AB | 453.63 | | 142.7 | kwc=1.00 l _{rel} =0.63 | |
| Drukzone kopplaat staaf C/D | 327.62 | (6.21) | | | |
| Trek bout | 90.26 | | | | |
| Trek boutrij | 180.52 | | | | |

Let op: De normaalkracht is verwerkt in bovengenoemde bezwijkkrachten.
Dwarskrachtcapaciteiten:
Stuik flens staaf AB 385.92 (6.7)
Stuik kopplaat 489.60 (6.7)
Afsch.cap. bouten na red. trek 153.67 (6.7)

TUSSENRESULTATEN KOLOMFLENS BUIGING

| Rij | p | m ₁ | e | n | m ₂ | alpha | l _{ef} | Formule | F _{t;fc;Rd} | Bezw.vorm | Kn:2 BC:60 Sit:1 |
|------|----|----------------|------|------|----------------|-------|-----------------|----------|----------------------|------------|------------------|
| 2 | 60 | 20.0 | 45.0 | 25.0 | 19.3 | 2*pi | 125.7 | T6.2v2 | 126.87 | 2=Plt+Bout | Staat C |
| 1 | 60 | 20.0 | 45.0 | 25.0 | 19.3 | 2*pi | 125.7 | T6.2v2 | 126.87 | 2=Plt+Bout | |
| 1- 2 | | | | | | | 175.1 | T6.2vlm2 | 225.34 | 1=Plt | |

TUSSENRESULTATEN KOPPLAAT BUIGING

| Rij | p | m ₁ | e | n | m ₂ | alpha | l _{ef} | Formule | F _{t;ep;Rd} | Bezw.vorm | Kn:2 BC:60 Sit:1 |
|------|----|----------------|------|------|----------------|-------|-----------------|---------|----------------------|------------|------------------|
| 2 | 60 | 28.9 | 35.0 | 35.0 | 23.5 | 2*pi | 181.3 | T6.2v2 | 174.01 | 2=Plt+Bout | Staat C |
| 1 | 60 | 28.9 | 35.0 | 35.0 | 23.5 | 2*pi | 181.3 | T6.2v2 | 174.01 | 2=Plt+Bout | |
| 1- 2 | | | | | | | 263.4 | T6.2v2 | 306.96 | 2=Plt+Bout | |

TUSSENRESULTATEN OVERIG

Kn:2 BC:60 Sit:1

| Rij | Trek lijf staaf AB 6.2.6.3 (6.15) | | Trek lijf staaf C/D 6.2.6.8 (6.22) | | Lassen Staaf C 4.5.3.2 (4.1) | |
|------|--------------------------------------|---------------|---------------------------------------|---------------|---------------------------------|------------|
| | b_{ef} | $F_{t,wc,Rd}$ | b_{ef} | $F_{t,wb,Rd}$ | b_{ef} | $F_{w,Rd}$ |
| 2 | 125.7 | 148.61 | 181.3 | 234.34 | 181.3 | 162.89 |
| 1 | 125.7 | 148.61 | 181.3 | 234.34 | 181.3 | 160.55 |
| 1- 2 | 175.1 | 183.07 | 263.4 | 340.49 | 263.4 | 236.68 |

BOU TRIJKRACHTEN

Herverdeling: Nee

Kn:2 BC:60 Sit:1

EN3-1-8 art. 6.2.7.2 Reductie : Ja Staaf C

| Rij | $F_{t,Rd,her}$ | $F_{t,Rd}$ | Arm | M | Criterium |
|----------------------|----------------|------------|--------------|---------------|--------------------------------|
| 2 | 126.87 | 126.87 | 90.0 | 11.42 | Flens staaf AB: Plaat+Bout |
| 1 | 56.20 | 55.88 | 30.0 | 1.68 | Trek lijf staaf AB |
| Som F= | | 182.75 | $M_{v,Rd} =$ | 13.09 | Bout/Plaat-combinatie |
| Moment tbv. lassen = | | | 40.75 | | gebaseerd op 1.0*MplRd |
| | | | $V_{v,Rd} =$ | 153.67 | Afsch.cap. bouten na red. trek |

TUSSENRESULTATEN STIJFHEID

Kn:2 BC:60 Sit:1

bij $M_{v,Rd}$ voor boutrij binnen trekflens (h_1)

Staaf C

| i | Onderdeel | k_i | μ_i | Bijdrage |
|----|----------------------------|--------|---------|----------|
| 1 | Afschuifzone lijf staaf AB | 6.835 | 2.988 | 33% |
| 2 | Drukzone lijf staaf AB | n.v.t. | | |
| 3 | Trekzone lijf staaf AB | 9.087 | 2.988 | 25% |
| 4 | Trekzone flens staaf AB | 17.611 | 2.988 | 13% |
| 5 | Trekzone kopplaat | 27.147 | 2.988 | 8% |
| 10 | Trekzone bouten | 11.514 | 2.988 | 20% |

STIJFHEID

Kn:2 BC:60 Sit:1

Maatgevend criterium: Afschuifzone lijf staaf AB

Staaf C

| Verh. | $M_{v,Rd}/Verh.$ | Arm | S_j | ϕ |
|-------|------------------|-----|------------|---------|
| 1.0 | 13.09 | 74 | 869 | 0.01507 |
| 1.2 | 10.91 | 74 | 1421 | 0.00768 |
| 1.5 | 8.73 | 74 | 2596 | 0.00336 |

Bij een moment $M_{v,Ed}=12.34$ geldt een stijfheid $S_j=1059$.

De in mechanica gebruikte stijfheid is $S=1345$ kNm/rad.

TOETSING VERBINDING

Kn:2 BC:60 Sit:1

| Artikel | $M_{v,Ed}$ | $M_{v,Rd}$ | Z | $V_{wp,Ed}$ | $V_{wp,Rd}$ | Toetsing |
|---------|------------|------------|----|-------------|-------------|----------|
| 6.2.7.1 | 12.34 | 13.09 | | | | 0.94 |
| 6.2.6.1 | | | 72 | 3.55 | 187.05 | 0.02 |

Let op: Normalkrachten in staven C & D zijn verwerkt in de bezwijk- en/of de boutrijkkrachten. De conservatieve toetsingsformule van EN 1993-1-8 art. 6.2.7.1 (3) is niet gebruikt.

TOETSING PROFIELEN EN AFSCHUIVING

Kn:2 BC:60 Sit:1

| Plaats | Profiel | Artikel | Formule | Toetsing |
|---------|---------|---------|---------------|----------|
| Staaf B | HEA160 | EN3-1-1 | 6.2.10 (6.31) | 0.21 |
| | | EN3-1-1 | 6.2.8 (6.30) | 0.21 |
| | | EN3-1-1 | 6.2.5 (6.12y) | 0.21 |
| | | EN3-1-1 | 6.2.6 (6.17) | 0.02 |
| | | EN3-1-1 | 6.2.4 (6.9) | 0.03 |
| | | EN3-1-1 | 6.2.1(6) N+D | 0.04 |
| Staaf C | HEA140 | EN3-1-1 | 6.2.10 (6.31) | 0.30 |
| | | EN3-1-1 | 6.2.8 (6.30) | 0.30 |
| | | EN3-1-1 | 6.2.5 (6.12y) | 0.30 |

| | | | | | |
|----------|--------|---------|----------|--------|------|
| Staaft A | HEA160 | EN3-1-1 | 6.2.6 | (6.17) | 0.14 |
| | | EN3-1-1 | 6.2.1(6) | N+D | 0.14 |
| | | EN3-1-8 | T.3.4 | | 0.12 |
| | | EN3-1-1 | 6.2.6 | (6.17) | 0.02 |
| | | EN3-1-1 | 6.2.1(6) | N+D | 0.03 |

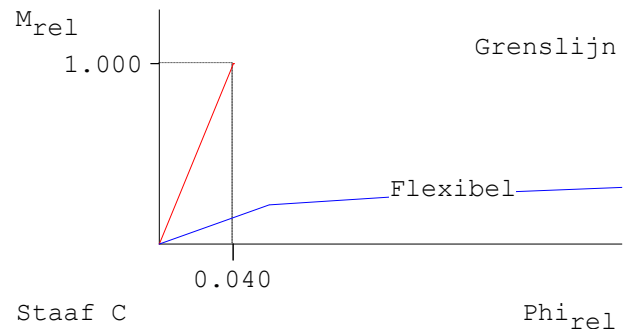
MOMENTCLASSIFICATIE EN3-1-8 art.5.2.3 Kn:2 BC:60 Sit:1

| Plaats | $M_{v,Rd}$ | $M_{v,Rd,staaf}$ | Classificatie |
|----------|------------|------------------|---------------------|
| Staaft C | 13.09 | 40.75 | Niet volledig sterk |

STIJFHEIDSCCLASSIFICATIE EN3-1-8 art.5.2.2 Kn:2 BC:60 Sit:1

| Plaats | Punt | Grenswaarden | | Actuele waarden | | Classificatie |
|----------|------|--------------|-----------|-----------------|-----------|---------------|
| | | Φ_{rel} | m_{rel} | Φ_{rel} | m_{rel} | |
| Staaft C | 1 | 0.000 | 0.000 | 0.000 | 0.000 | Flexibel |
| | 2 | 0.040 | 1.000 | 0.060 | 0.214 | |
| | 3 | 0.040 | 1.000 | 0.136 | 0.268 | |
| | 4 | 0.040 | 1.000 | 0.268 | 0.321 | |

M-PHI DIAGRAM EN3-1-8 fig. 5.4 Ongeschoord Kn:2 BC:60 Sit:1



CONTROLES

| Onderdeel | Plaats | Rij | Item | Ernst | Art./ (Frm.) | Min. Waarde | Max. |
|--------------|----------|-----|-------------------------|------------|--------------|-------------|-------|
| Bout | Staaft C | 1 | HOH-afstand p1 | 3.5(1) | | 39.6 | 126.0 |
| | Staaft C | 1 | HOH-afstand p2 | 3.5(1) | | 69.3 | 96.8 |
| | Staaft C | 2 | HOH-afstand p2 | 3.5(1) | | 69.3 | 96.8 |
| Bout (Plaat) | Staaft C | 1 | Eindafstand e1 | 3.5(1) | | 21.6 | 30.0 |
| | Staaft C | 2 | Eindafstand e1 | 3.5(1) | | 21.6 | 30.0 |
| Kopplaat | Staaft C | | Flenslas $\Delta\Delta$ | 1.0*MplRd | | 3.92 | 4.00 |
| | Staaft C | | Lijflas $\Delta\Delta$ | 1.0*MplRd | | 3.00 | 3.00 |
| | Staaft C | | Positie boven | | | 60.0 | 60.8 |
| | Staaft C | | Positie onder | | | -60.8 | -60.0 |
| Schot AB | Staaft A | | Dikte | frmb 5.5.b | | 3.5 | 10.0 |
| | Staaft A | | Flenslas $\Delta\Delta$ | 1.0*MplRd | | 4.26 | 5.00 |
| | Staaft A | | Lengte | | | 124.0 | 134.0 |
| | Staaft A | | Lengte | frmb 5.5.b | | 47.5 | 130.0 |
| | Staaft B | | Dikte | frmb 5.6.a | | 4.9 | 10.0 |
| | Staaft B | | Lengte | | | 124.0 | 134.0 |
| | Staaft B | | Lijflas $\Delta\Delta$ | 1.0*MplRd | | 3.08 | 5.00 |

9 Ongeschoord portaal as B

9.1 Belasting t.g.v. permanente belasting

Belastinggeval 1 t.g.v permanente belastingen

$G_{k;dak}$: $0.55 \cdot 2.47 \cdot 1.25$ = 1.70 kN/m

$G_{k;tussenbordes}$: = 7.56 kN

$G_{k;bovenbordes}$: = 8.38 kN

Eigengewicht van de profielen wordt automatisch gegenereerd.

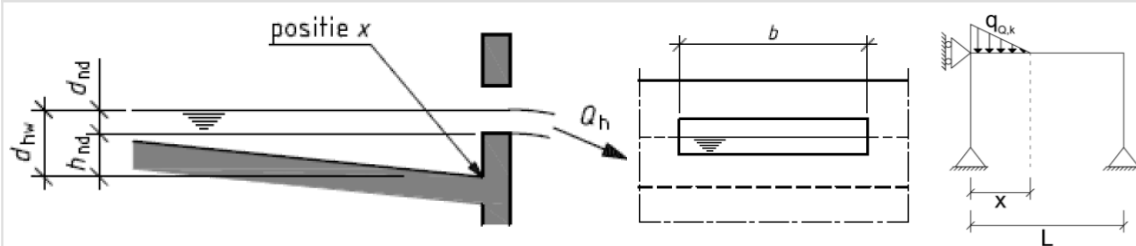
9.2 Belasting t.g.v. wateraccumulatie

Wateraccumulatie:

Min. afschot: 16 mm/m*3.15 \approx 55 mm

| Wateraccumulatie | | | |
|---|--|-------------------|---------------------------------|
| Referentieperiode | = | 50 | jaar |
| Neerslagintensiteit | $i_r =$ | 0,05 | $\cdot 10^{-3}$ m/s |
| Breedte dakvlak | $B =$ | 3,15 | m |
| Lengte dakvlak | $L =$ | 5,25 | m |
| Afschotzijden | = | 1 | |
| Aantal noodafvoeren per zijde | = | 1 | st. |
| Oppervlakte per noodafvoer | $A =$ | 16,6 | m^2 |
| Gekozen breedte noodafvoer | $b =$ | 0,30 | m |
| Maximaal toegestane waterhoogte t.p.v. het laagste punt | = | 0,08 | m (0,08 m is een veilige keuze) |
| Gekozen hoogte van de noodafvoer boven de dakrand of het dakvlak | $h_{nd} =$ | 0,03 | m (normaal 0,03 m) |
| Overspanning dakplaten | $L_t =$ | 2,47 | m |
| Afschot | = | 16,0 | mm/m |
| Volumieke gewicht van water | $\gamma_w =$ | 10,0 | kN/m^3 |
| Factor t.g.v. meervelds dakplaten | $\psi_0 =$ | 1,25 | |
| Q_h | $= A \cdot i_r$ | $= 0,0009$ | m^3/s |
| d_{nd} | $= 0,70 \cdot (Q_h/b)^{2/3}$ | $= 14,6$ | mm |
| d_{nd} is de maximale waterhoogte boven de onderzijde van de noodafvoer | | | |
| d_{hw} | $= d_{nd} + h_{nd}$ | $= 44,6$ | mm |
| d_{hw} is de maximale waterhoogte ter plaatse van de dakrand | | | |
| d_n | $= 0,004 \cdot L_t$ | $= 9,9$ | mm |
| d_n is de extra waterhoogte door de doorbuiging van het dakvlak | | | |
| $q_{Q,k}$ | $= (d_{hw} + d_n) \cdot \gamma_w \cdot L_t \cdot \psi_0$ | $= 1,69$ | kN/m |
| x | $= (d_{hw} + d_n) / (\text{afschot} \cdot L) / L$ | $= 3,41$ | m |
| Minimale afmetingen noodafvoer: | | | |
| $h \times b$ | $= (d_{nd} + 50 \text{ mm}) \times b$ | $= 65 \times 300$ | mm x mm |

Er is rekening gehouden met 50 mm vrije hoogte boven de bepaalde waterhoogte i.v.m. verstopping



Aandachtspunt:

Noodafvoeren mogen niet op een gesloten (riool-)afvoersysteem worden aangesloten.

NA: HxB = 100x300 mm

9.3 Belasting t.g.v. sneeuw

Belastinggeval 3 t.g.v. sneeuw

Belastingbreedte voor sneeuw: = 2.47 m

9.4 Belasting t.g.v. veranderlijke vloerbelasting

Belastinggeval 3 t.g.v. veranderlijke vloerbelasting

$Q_{k;tussenbordes}$: = 3.66 kN

$Q_{k;bovenbordes}$: = 4.07 kN

9.5 Uitvoer as B

| | |
|-----------------------|----------------------------------|
| Toepassen: Dakligger: | IPE200 afschot 1-zijdig 55 mm |
| Kolommen: | HEA200 |

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Dimensies....: kN;m;rad (tenzij anders aangegeven)

Belastingbreedte.: 2.470

Rekenmodel.....: 1e-orde-elastisch.

Theorie voor de bepaling van de krachtsverdeling:

Geometrisch lineair.

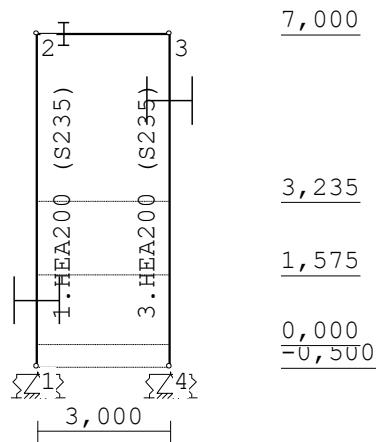
Fysisch lineair.

Gunstige werking van de permanente belasting wordt automatisch verwerkt.

Toegepaste normen volgens Eurocode met Nederlandse NB

| | | | |
|-------------|---------------------------|-----------------|--------------|
| Belastingen | NEN-EN 1990:2002 | C2:2010,A1:2019 | NB:2019 (nl) |
| | NEN-EN 1991-1-1:2002 | C1/C11:2019 | NB:2019 (nl) |
| | NEN-EN 1991-1-3:2003 | C1:2009 | NB:2011 (nl) |
| | NEN-EN 1991-1-4:2005 | C2:2011 | NB:2011 (nl) |
| Beton | NEN-EN 1992-1-1:2011 (nl) | C2/A1:2015 (nl) | NB:2016 (nl) |
| Staal | NEN-EN 1993-1-1:2006 | C2:2011,A1:2016 | NB:2016 (nl) |
| | NEN-EN 1993-1-8:2006 | C2:2009 | NB:2011 (nl) |

GEOMETRIE



STRAMIENLIJNEN

| Nr. | Naam | X | Z-min | Z-max |
|-----|------|-------|--------|-------|
| 1 | | 0.000 | -0.500 | 7.000 |
| 2 | | 3.000 | -0.500 | 7.000 |

NIVEAUS

| Nr. | Z | X-min | X-max |
|-----|--------|-------|-------|
| 1 | -0.500 | 0.000 | 3.000 |
| 2 | 0.000 | 0.000 | 3.000 |
| 3 | 1.575 | 0.000 | 3.000 |
| 4 | 3.235 | 0.000 | 3.000 |
| 5 | 7.000 | 0.000 | 3.000 |

MATERIALEN

| Mt | Kwaliteit | E-modulus [N/mm ²] | S.G. | Pois. | Uitz. coëff |
|----|-----------|--------------------------------|------|-------|-------------|
| 1 | S235 | 210000 | 78.5 | 0.30 | 1.2000e-05 |

PROFIELEN [mm]

| Prof. | Omschrijving | Materiaal | Oppervlak | Traagheid | Vormf. |
|-------|--------------|-----------|------------|------------|--------|
| 1 | HEA200 | 1:S235 | 5.3800e+03 | 3.6920e+07 | 0.00 |
| 2 | IPE200 | 1:S235 | 2.8480e+03 | 1.9430e+07 | 0.00 |

PROFIELEN vervolg [mm]

| Prof. | Staaftype | Breedte | Hoogte | e | Type | b1 | h1 | b2 | h2 |
|-------|-----------|---------|--------|-------|------|----|----|----|----|
| 1 | 0:Normaal | 200 | 190 | 95.0 | | | | | |
| 2 | 0:Normaal | 100 | 200 | 100.0 | | | | | |

PROFIELVORMEN [mm]

1 HEA200



2 IPE200



KNOPEN

| Knoop | X | Z |
|-------|-------|--------|
| 1 | 0.000 | -0.500 |
| 2 | 0.000 | 7.000 |
| 3 | 3.000 | 7.000 |
| 4 | 3.000 | -0.500 |

STAVEN

| St. | ki | kj | Profiel | Aansl.i | Aansl.j | Lengte |
|-----|----|----|----------|---------|-----------|---------------|
| 1 | 1 | 2 | 1:HEA200 | NDV | NDM | 7.500 2 |
| 2 | 2 | 3 | 2:IPE200 | NDV | NDV | 3.000 2 |
| 3 | 3 | 4 | 1:HEA200 | NDM | NDV | 7.500 2 |

Opmerkingen

[2] De momentveerwaarde is vastgelegd met een tri-lineair moment-veerstijfheidsdiagram volgens onderstaande tabel

STAVEN (vervolg - tri-lineair moment-veerstijfheidsdiagram)

| St. | Kn. | Mvud | Cvud | Cvud (Mvud/1.2) | Cvud (Mvud/1.5) |
|-----|-----|--------|------|-----------------|-----------------|
| 1 | 1 | 16.22 | 1124 | 1839 | 3359 |
| 2 | 2 | -44.86 | 5410 | 8851 | 16167 |
| | | 47.03 | 5605 | 9170 | 16751 |
| | 3 | -44.86 | 5410 | 8851 | 16167 |
| | | 47.03 | 5605 | 9170 | 16751 |
| 3 | 4 | 16.22 | 1124 | 1839 | 3359 |

VASTE STEUNPUNTEN

| Nr. | knoop | Kode | XZR | l=vast | 0=vrij | Hoek |
|-----|-------|------|-----|--------|--------|------|
| 1 | 1 | 110 | | | | 0.00 |
| 2 | 4 | 110 | | | | 0.00 |

VEREN

| Veer | Knoop | Richting | Hoek | Veerwaarde | Type | Ondergrens | Bovengrens |
|------|-------|-----------|------|------------|---------|------------|------------|
| 1 | 1 | 3:Rotatie | 0.00 | 5.000e+02 | Normaal | -1.000e+10 | 1.000e+10 |
| 2 | 4 | 3:Rotatie | 0.00 | 5.000e+02 | Normaal | -1.000e+10 | 1.000e+10 |

BELASTINGENERATIE ALGEMEEN.

| | | | |
|------------------------------|------|-------------------------|------|
| Betrouwbaarheidsklasse.....: | 2 | Referentieperiode.....: | 50 |
| Gebouwdiepte.....: | 4.94 | Gebouwhoogte.....: | 7.00 |
| Niveau aansl.terrein.....: | 0.00 | E.g. scheid.w. [kN/m2]: | 1.20 |

WIND

| | | | |
|-----------------------------------|-----------|--------------------------|--------|
| Terrein categorie ...[4.3.2]....: | Onbebouwd | | |
| Windgebied | 3 | Vb,0 ..[4.2].....: | 24.500 |
| Positie spant in het gebouw....: | 2.470 | Kr[4.3.2].....: | 0.209 |
| z0 | 0.200 | Zmin ..[4.3.2].....: | 4.000 |
| Co wind van links ..[4.3.3]....: | 1.000 | Co wind van rechts.....: | 1.000 |
| Co wind loodrecht ..[4.3.3]....: | 1.000 | | |
| Cpi wind van links ..[7.2.9]....: | 0.200 | -0.300 | |
| Cpi windloodrecht ...[7.2.9]....: | 0.200 | -0.300 | |
| Cpi wind van rechts .[7.2.9]....: | 0.200 | -0.300 | |
| Cfr windwrijving[7.5].....: | 0.040 | | |

SNEEUW

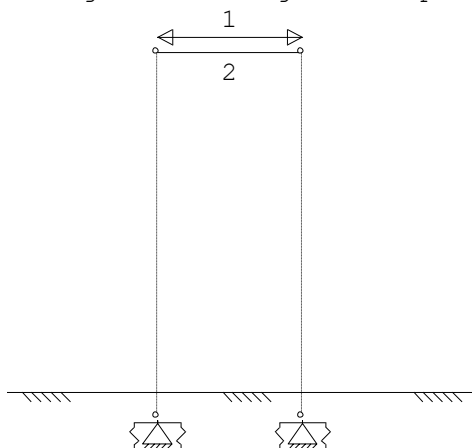
| | |
|--------------------------------|------|
| Sneeuwbelasting (sk) 50 jaar : | 0.70 |
| Sneeuwbelasting (sn) n jaar : | 0.70 |

STAAFTYPEN

| Type | staven |
|------------------|--------|
| 5:Linker gevel. | : 1 |
| 6:Rechter gevel. | : 3 |
| 7:Dak. | : 2 |

LASTVELDEN

Veranderlijke belastingen door personen

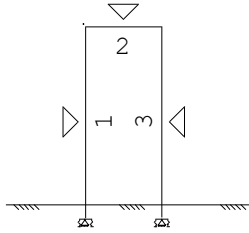


LASTVELDEN

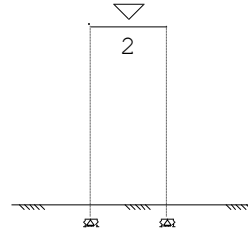
| Nr | StAAF | Tabel | Klasse-Gebruiksfunctie | Verd. | q _k | Q _k | F _t /F _{t,0} |
|----|-------|-------|--------------------------|-------|----------------|----------------|----------------------------------|
| 1 | 2-2 | 6.10 | H-Dak (onder dakbeschet) | 1 | -1.00 | -2.00 | 1.00 |

LASTVELDEN

Wind staven



Sneeuw staven

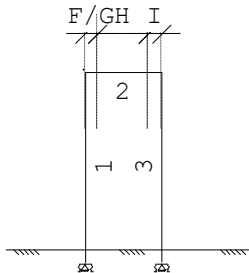


WIND DAKTYPES

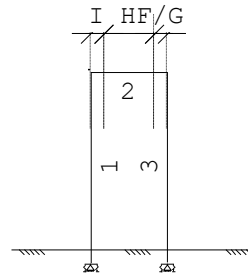
| Nr. | Staaftype | reductie bij wind van links | reductie bij wind van rechts | Cpe volgens art: |
|-----|------------|-----------------------------|------------------------------|------------------|
| 1 | 1 Gevel | 1.000 | 1.000 | 7.2.2 |
| 2 | 2 Plat dak | 1.000 | 1.000 | 7.2.3 |
| 3 | 3 Gevel | 1.000 | 1.000 | 7.2.2 |

WIND ZONES

Wind van links



Wind van rechts



WIND VAN LINKS ZONES

| Nr. | Staaftype | Positie | Lengte | Zone |
|-----|-----------|---------|--------|------|
| 1 | 1 | 0.000 | 7.500 | D |
| 2 | 2 | 0.000 | 0.494 | F/G |
| 3 | 2 | 0.494 | 1.976 | H |
| 4 | 2 | 2.470 | 0.530 | I |
| 5 | 3 | 0.000 | 7.500 | E |

WIND VAN RECHTS ZONES

| Nr. | Staaftype | Positie | Lengte | Zone |
|-----|-----------|---------|--------|------|
| 1 | 3 | 0.000 | 7.500 | D |
| 2 | 2 | 0.000 | 0.494 | F/G |
| 3 | 2 | 0.494 | 1.976 | H |
| 4 | 2 | 2.470 | 0.530 | I |
| 5 | 1 | 0.000 | 7.500 | E |

Wind indexen

| Index | CsCd | Cpe/Cpi | qp | breedte | reductie | Qw | Zone | Hoek(en) |
|-------|------|---------|-------|---------|----------|--------|------|----------|
| Qw1 | | 0.300 | 0.615 | 2.470 | | -0.456 | -i | |
| Qw2 | 1.00 | 0.800 | 0.536 | 2.470 | | -1.060 | D | |
| Qw3 | 1.00 | 0.800 | 0.615 | 2.470 | | -1.215 | D | |
| Qw4 | 1.00 | -1.200 | 0.615 | 2.470 | | 1.823 | G | 0.0 |
| Qw5 | 1.00 | -0.700 | 0.615 | 2.470 | | 1.063 | H | 0.0 |
| Qw6 | 1.00 | -0.200 | 0.615 | 2.470 | | 0.304 | I | 0.0 |
| Qw7 | 1.00 | -0.567 | 0.536 | 2.470 | | 0.751 | E | |
| Qw8 | 1.00 | -0.567 | 0.615 | 2.470 | | 0.861 | E | |
| Qw9 | | -0.200 | 0.615 | 2.470 | | 0.304 | +i | |
| Qw10 | 1.00 | 0.200 | 0.615 | 2.470 | | -0.304 | I | 0.0 |
| Qw11 | 1.00 | -0.800 | 0.491 | 1.765 | | 0.693 | B | |
| Qw12 | 1.00 | -0.500 | 0.491 | 0.705 | | 0.173 | C | |
| Qw13 | 1.00 | -0.800 | 0.615 | 1.765 | | 0.868 | B | |
| Qw14 | 1.00 | -0.500 | 0.615 | 0.705 | | 0.217 | C | |
| Qw15 | 1.00 | -0.700 | 0.615 | 0.265 | | 0.114 | H | 0.0 |
| Qw16 | 1.00 | 0.200 | 0.615 | 2.205 | | -0.271 | I | 0.0 |
| Qw17 | 1.00 | -0.200 | 0.615 | 2.205 | | 0.271 | I | 0.0 |

SNEEUW DAKTYPEN

| Staafl | artikel |
|--------|---------------------|
| 2-2 | 5.3.2 Lessenaarsdak |

Sneeuw indexen

| Index | art | μ | s_k | red. posfac | breedte | Q_s | hoek |
|-------|-------|-------|-------|-------------|---------|-------|------|
| Qs1 | 5.3.2 | 0.800 | 0.70 | 1.00 | 2.470 | 1.383 | 0.0 |

BELASTINGGEVALLEN

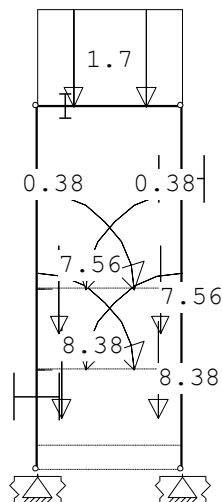
| B.G. | Omschrijving | Type |
|------|----------------------------------|------------|
| | 1 Permanente belasting EGZ=-1.00 | 1 |
| | 2 Ver. bel. pers. ed. (q_k) | 2 |
| g | 3 Ver. bel. pers. ed. (q_k) | 2 |
| g | 4 Ver. bel. pers. ed. (Q_k) | 3 |
| g | 5 Wind van links onderdruk A | 7 |
| g | 6 Wind van links overdruk A | 8 |
| g | 7 Wind van links onderdruk B | 9 |
| g | 8 Wind van links overdruk B | 10 |
| g | 9 Wind van rechts onderdruk A | 11 |
| g | 10 Wind van rechts overdruk A | 12 |
| g | 11 Wind van rechts onderdruk B | 13 |
| g | 12 Wind van rechts overdruk B | 14 |
| g | 13 Wind loodrecht onderdruk A | 15 |
| g | 14 Wind loodrecht overdruk A | 16 |
| g* | 15 Sneeuw A | 22 |
| | 16 Knik | 0 Onbekend |

g = gegeneerd belastinggeval
* = belastinggeval bevat 1 of meer handmatig toegevoegde en/of gewijzigde lasten

BELASTINGEN

B.G:1 Permanente belasting

Eigen gewicht van alle staven is meegenomen in berekening. Richting:↓



STAAFBELASTINGEN

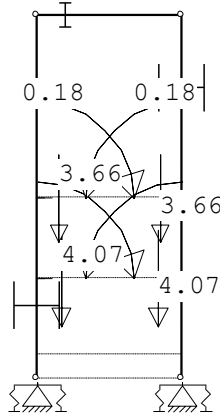
B.G:1 Permanente belasting

| Staafl | Type | $q_1/p/m$ | q_2 | A | B | ψ_0 | ψ_1 | ψ_2 |
|--------|---------------|-----------|-------|-------|-------|----------|----------|----------|
| 2 | 3:QZgeProj. | -1.70 | -1.70 | 0.000 | 0.000 | | | |
| 1 | 10:PZGeproij. | -8.38 | | 2.075 | | | | |
| 1 | 10:PZGeproij. | -7.56 | | 3.735 | | | | |
| 3 | 10:PZGeproij. | -7.56 | | 3.765 | | | | |

| | | | |
|---|---------------|-------|-------|
| 3 | 10:PZGepro.j. | -8.38 | 5.425 |
| 1 | 12:MYLokaal | 0.42 | 2.075 |
| 1 | 12:MYLokaal | 0.38 | 3.735 |
| 3 | 12:MYLokaal | -0.38 | 3.765 |
| 3 | 12:MYLokaal | -0.42 | 5.425 |

BELASTINGEN

B.G:2 Ver. bel. pers. ed. (q_k)



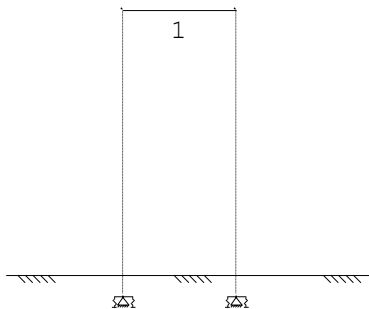
STAAFBELASTINGEN

B.G:2 Ver. bel. pers. ed. (q_k)

| StAAF Type | $q_1/p/m$ | q_2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-----------------|-----------|-------|-------|---|----------|----------|----------|
| 1 10:PZGepro.j. | -4.07 | | 2.075 | | 0.00 | 0.00 | 0.00 |
| 1 10:PZGepro.j. | -3.66 | | 3.735 | | 0.00 | 0.00 | 0.00 |
| 3 10:PZGepro.j. | -3.66 | | 3.765 | | 0.00 | 0.00 | 0.00 |
| 3 10:PZGepro.j. | -4.07 | | 5.425 | | 0.00 | 0.00 | 0.00 |
| 1 12:MYLokaal | 0.20 | | 2.075 | | 0.00 | 0.00 | 0.00 |
| 1 12:MYLokaal | 0.18 | | 3.735 | | 0.00 | 0.00 | 0.00 |
| 3 12:MYLokaal | -0.18 | | 3.765 | | 0.00 | 0.00 | 0.00 |
| 3 12:MYLokaal | -0.20 | | 5.425 | | 0.00 | 0.00 | 0.00 |

SITUATIES BELAST/ONBELAST

B.G:2 Ver. bel. pers. ed. (q_k)



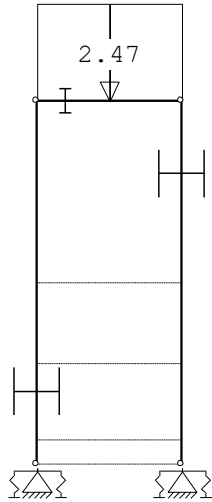
SITUATIES BELAST/ONBELAST

Belastingtype: q_k

| Nr Lastvelden belast | Lastvelden onbelast |
|----------------------|---------------------|
| 1 | 1 |

BELASTINGEN

B.G:3 Ver. bel. pers. ed. (q_k)



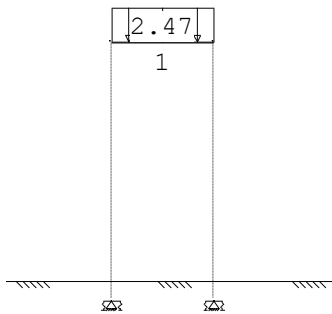
STAAFBELASTINGEN

B.G:3 Ver. bel. pers. ed. (q_k)

| StAAF Type | $q_1/p/m$ | q_2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|---------------|-----------|-------|-------|-------|----------|----------|----------|
| 2 3:QZgeProj. | -2.47 | -2.47 | 0.000 | 0.000 | 0.00 | 0.00 | 0.00 |

SITUATIES BELAST/ONBELAST

B.G:3 Ver. bel. pers. ed. (q_k)



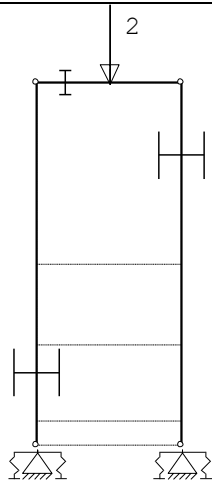
SITUATIES BELAST/ONBELAST

Belastingtype: q_k

| Nr Lastvelden belast | Lastvelden onbelast |
|----------------------|---------------------|
| 1 1 | |

BELASTINGEN

B.G:4 Ver. bel. pers. ed. (Q_k)



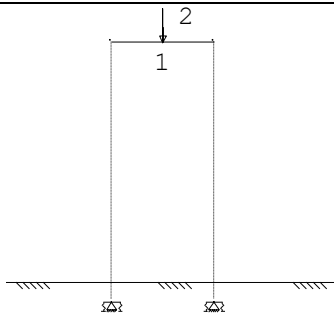
STAAFBELASTINGEN

B.G:4 Ver. bel. pers. ed. (Q_k)

| StAAF Type | q1/p/m | q2 | A | B | Ψ ₀ | Ψ ₁ | Ψ ₂ |
|-----------------|--------|----|-------|---|----------------|----------------|----------------|
| 2 10:PZGeproij. | -2.00 | | 1.500 | | 0.00 | 0.00 | 0.00 |

SITUATIES BELAST/ONBELAST

B.G:4 Ver. bel. pers. ed. (Q_k)



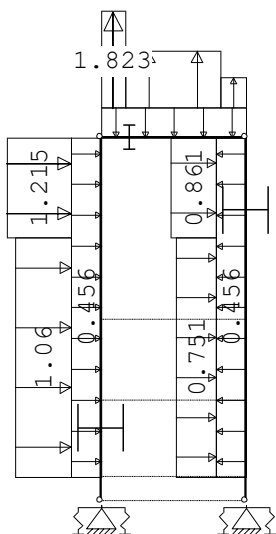
SITUATIES BELAST/ONBELAST

Belastingtype: Q_k

| Nr Lastvelden belast | Lastvelden onbelast |
|----------------------|---------------------|
| 1 | 1 |

BELASTINGEN

B.G:5 Wind van links onderdruk A



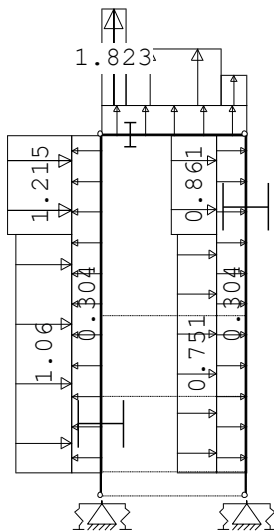
STAAFBELASTINGEN

B.G:5 Wind van links onderdruk A

| StAAF | Type | Index | q1/p/m | q2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 1 | 1:QZLokaal | Qw1 | -0.46 | -0.46 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw1 | -0.46 | -0.46 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw1 | -0.46 | -0.46 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw2 | -1.06 | -1.06 | 0.500 | 2.060 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw3 | -1.22 | -1.22 | 5.440 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | | 0.00 | 0.00 | 0.000 | 2.506 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw4 | 1.82 | 1.82 | 0.000 | 2.506 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw5 | 1.06 | 1.06 | 0.494 | 0.530 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw6 | 0.30 | 0.30 | 2.470 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw7 | 0.75 | 0.75 | 2.060 | 0.500 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw8 | 0.86 | 0.86 | 0.000 | 5.440 | 0.00 | 0.20 | 0.00 |

BELASTINGEN

B.G:6 Wind van links overdruk A



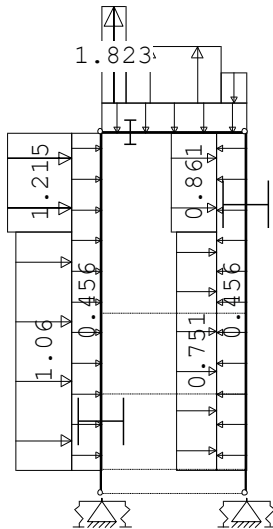
STAAFBELASTINGEN

B.G:6 Wind van links overdruk A

| StAAF | Type | Index | q1/p/m | q2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 1 | 1:QZLokaal | Qw9 | 0.30 | 0.30 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw9 | 0.30 | 0.30 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw9 | 0.30 | 0.30 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw2 | -1.06 | -1.06 | 0.500 | 2.060 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw3 | -1.22 | -1.22 | 5.440 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | | 0.00 | 0.00 | 0.000 | 2.506 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw4 | 1.82 | 1.82 | 0.000 | 2.506 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw5 | 1.06 | 1.06 | 0.494 | 0.530 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw6 | 0.30 | 0.30 | 2.470 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw7 | 0.75 | 0.75 | 2.060 | 0.500 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw8 | 0.86 | 0.86 | 0.000 | 5.440 | 0.00 | 0.20 | 0.00 |

BELASTINGEN

B.G:7 Wind van links onderdruk B



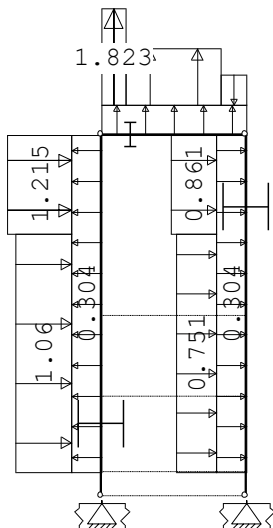
STAAFBELASTINGEN

B.G:7 Wind van links onderdruk B

| StAAF | Type | Index | q1/p/m | q2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 1 | 1:QZLokaal | Qw1 | -0.46 | -0.46 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw1 | -0.46 | -0.46 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw1 | -0.46 | -0.46 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw2 | -1.06 | -1.06 | 0.500 | 2.060 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw3 | -1.22 | -1.22 | 5.440 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | | 0.00 | 0.00 | 0.000 | 2.506 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw4 | 1.82 | 1.82 | 0.000 | 2.506 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw5 | 1.06 | 1.06 | 0.494 | 0.530 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw10 | -0.30 | -0.30 | 2.470 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw7 | 0.75 | 0.75 | 2.060 | 0.500 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw8 | 0.86 | 0.86 | 0.000 | 5.440 | 0.00 | 0.20 | 0.00 |

BELASTINGEN

B.G:8 Wind van links overdruk B



STAAFBELASTINGEN

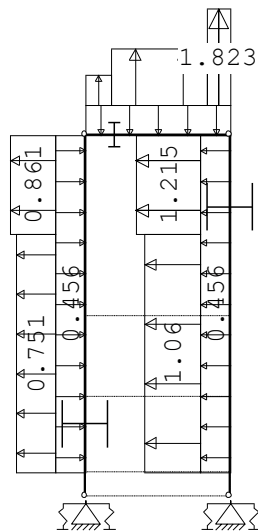
B.G:8 Wind van links overdruk B

| StAAF | Type | Index | q1/p/m | q2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-------|------------|-------|--------|------|-------|-------|----------|----------|----------|
| 1 | 1:QZLokaal | Qw9 | 0.30 | 0.30 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |

| | | | | | | | | | |
|---|------------|------|-------|-------|-------|-------|------|------|------|
| 2 | 1:QZLokaal | Qw9 | 0.30 | 0.30 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw9 | 0.30 | 0.30 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw2 | -1.06 | -1.06 | 0.500 | 2.060 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw3 | -1.22 | -1.22 | 5.440 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | | 0.00 | 0.00 | 0.000 | 2.506 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw4 | 1.82 | 1.82 | 0.000 | 2.506 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw5 | 1.06 | 1.06 | 0.494 | 0.530 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw10 | -0.30 | -0.30 | 2.470 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw7 | 0.75 | 0.75 | 2.060 | 0.500 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw8 | 0.86 | 0.86 | 0.000 | 5.440 | 0.00 | 0.20 | 0.00 |

BELASTINGEN

B.G:9 Wind van rechts onderdruk A



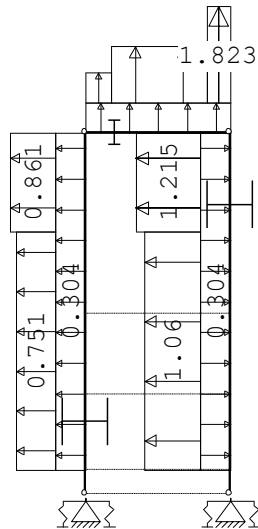
STAAFBELASTINGEN

B.G:9 Wind van rechts onderdruk A

| StAAF | Type | Index | q1/p/m | q2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 1 | 1:QZLokaal | Qw1 | -0.46 | -0.46 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw1 | -0.46 | -0.46 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw1 | -0.46 | -0.46 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw2 | -1.06 | -1.06 | 2.060 | 0.500 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw3 | -1.22 | -1.22 | 0.000 | 5.440 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | | 0.00 | 0.00 | 2.506 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw4 | 1.82 | 1.82 | 2.506 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw5 | 1.06 | 1.06 | 0.530 | 0.494 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw6 | 0.30 | 0.30 | 0.000 | 2.470 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw7 | 0.75 | 0.75 | 0.500 | 2.060 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw8 | 0.86 | 0.86 | 5.440 | 0.000 | 0.00 | 0.20 | 0.00 |

BELASTINGEN

B.G:10 Wind van rechts overdruk A



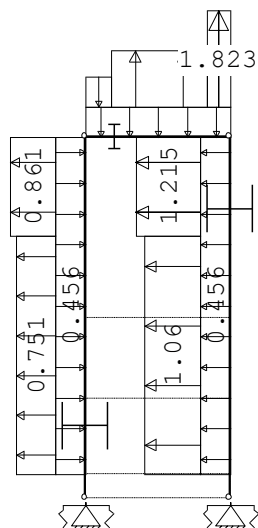
STAAFBELASTINGEN

B.G:10 Wind van rechts overdruk A

| StAAF | Type | Index | q1/p/m | q2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 1 | 1:QZLokaal | Qw9 | 0.30 | 0.30 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw9 | 0.30 | 0.30 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw9 | 0.30 | 0.30 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw2 | -1.06 | -1.06 | 2.060 | 0.500 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw3 | -1.22 | -1.22 | 0.000 | 5.440 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | | 0.00 | 0.00 | 2.506 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw4 | 1.82 | 1.82 | 2.506 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw5 | 1.06 | 1.06 | 0.530 | 0.494 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw6 | 0.30 | 0.30 | 0.000 | 2.470 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw7 | 0.75 | 0.75 | 0.500 | 2.060 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw8 | 0.86 | 0.86 | 5.440 | 0.000 | 0.00 | 0.20 | 0.00 |

BELASTINGEN

B.G:11 Wind van rechts onderdruk B



STAAFBELASTINGEN

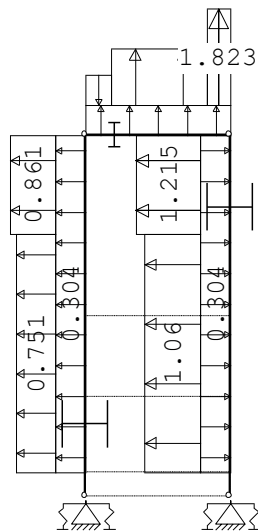
B.G:11 Wind van rechts onderdruk B

| StAAF | Type | Index | q1/p/m | q2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 1 | 1:QZLokaal | Qw1 | -0.46 | -0.46 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |

| | | | | | | | | | |
|---|------------|------|-------|-------|-------|-------|------|------|------|
| 2 | 1:QZLokaal | Qw1 | -0.46 | -0.46 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw1 | -0.46 | -0.46 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw2 | -1.06 | -1.06 | 2.060 | 0.500 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw3 | -1.22 | -1.22 | 0.000 | 5.440 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | | 0.00 | 0.00 | 2.506 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw4 | 1.82 | 1.82 | 2.506 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw5 | 1.06 | 1.06 | 0.530 | 0.494 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw10 | -0.30 | -0.30 | 0.000 | 2.470 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw7 | 0.75 | 0.75 | 0.500 | 2.060 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw8 | 0.86 | 0.86 | 5.440 | 0.000 | 0.00 | 0.20 | 0.00 |

BELASTINGEN

B.G:12 Wind van rechts overdruk B



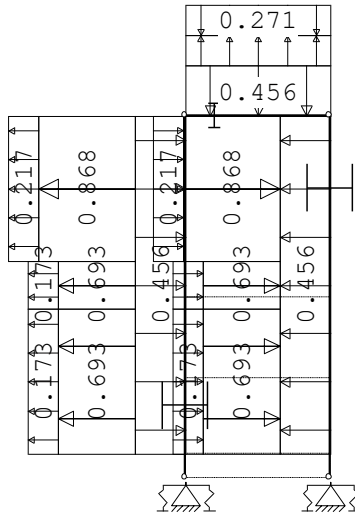
STAAFBELASTINGEN

B.G:12 Wind van rechts overdruk B

| StAAF | Type | Index | q1/p/m | q2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 1 | 1:QZLokaal | Qw9 | 0.30 | 0.30 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw9 | 0.30 | 0.30 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw9 | 0.30 | 0.30 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw2 | -1.06 | -1.06 | 2.060 | 0.500 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw3 | -1.22 | -1.22 | 0.000 | 5.440 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | | 0.00 | 0.00 | 2.506 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw4 | 1.82 | 1.82 | 2.506 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw5 | 1.06 | 1.06 | 0.530 | 0.494 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw10 | -0.30 | -0.30 | 0.000 | 2.470 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw7 | 0.75 | 0.75 | 0.500 | 2.060 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw8 | 0.86 | 0.86 | 5.440 | 0.000 | 0.00 | 0.20 | 0.00 |

BELASTINGEN

B.G:13 Wind loodrecht onderdruk A



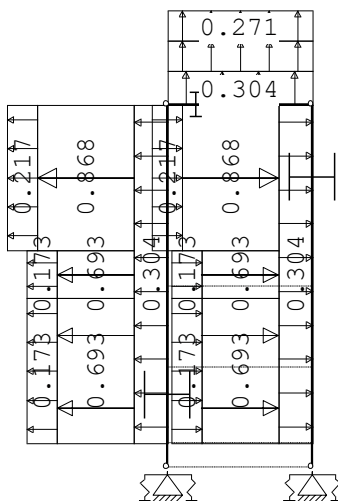
STAAFBELASTINGEN

B.G:13 Wind loodrecht onderdruk A

| StAAF | Type | Index | q1/p/m | q2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-------|------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 1 | 1:QZLokaal | Qw1 | -0.46 | -0.46 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw1 | -0.46 | -0.46 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw1 | -0.46 | -0.46 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw11 | 0.69 | 0.69 | 0.500 | 4.000 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw12 | 0.17 | 0.17 | 0.500 | 4.000 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw11 | 0.69 | 0.69 | 3.501 | 3.000 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw12 | 0.17 | 0.17 | 3.501 | 3.000 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw13 | 0.87 | 0.87 | 4.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw14 | 0.22 | 0.22 | 4.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw11 | 0.69 | 0.69 | 4.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw12 | 0.17 | 0.17 | 4.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw11 | 0.69 | 0.69 | 3.000 | 3.501 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw12 | 0.17 | 0.17 | 3.000 | 3.501 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw13 | 0.87 | 0.87 | 0.000 | 4.500 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw14 | 0.22 | 0.22 | 0.000 | 4.500 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw15 | 0.11 | 0.11 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw16 | -0.27 | -0.27 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |

BELASTINGEN

B.G:14 Wind loodrecht overdruk A



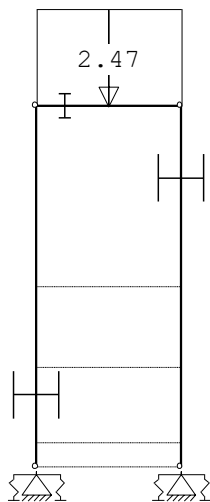
STAAFBELASTINGEN

B.G:14 Wind loodrecht overdruk A

| StAAF | Type | Index | q1/p/m | q2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-------|------------|-------|--------|------|-------|-------|----------|----------|----------|
| 1 | 1:QZLokaal | Qw9 | 0.30 | 0.30 | 0.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw9 | 0.30 | 0.30 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw9 | 0.30 | 0.30 | 0.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw11 | 0.69 | 0.69 | 0.500 | 4.000 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw12 | 0.17 | 0.17 | 0.500 | 4.000 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw11 | 0.69 | 0.69 | 3.501 | 3.000 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw12 | 0.17 | 0.17 | 3.501 | 3.000 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw13 | 0.87 | 0.87 | 4.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 1 | 1:QZLokaal | Qw14 | 0.22 | 0.22 | 4.500 | 0.000 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw11 | 0.69 | 0.69 | 4.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw12 | 0.17 | 0.17 | 4.000 | 0.500 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw11 | 0.69 | 0.69 | 3.000 | 3.501 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw12 | 0.17 | 0.17 | 3.000 | 3.501 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw13 | 0.87 | 0.87 | 0.000 | 4.500 | 0.00 | 0.20 | 0.00 |
| 3 | 1:QZLokaal | Qw14 | 0.22 | 0.22 | 0.000 | 4.500 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw15 | 0.11 | 0.11 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |
| 2 | 1:QZLokaal | Qw17 | 0.27 | 0.27 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |

BELASTINGEN

B.G:15 Sneeuw A



STAAFBELASTINGEN

B.G:15 Sneeuw A

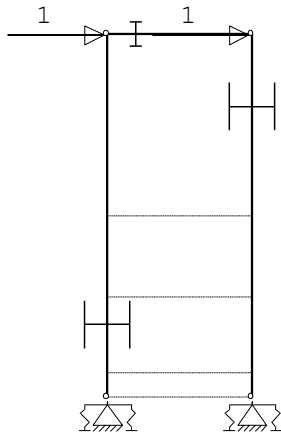
| StAAF | Type | Index | q1/p/m | q2 | A | B | Ψ_0 | Ψ_1 | Ψ_2 |
|-------|-------------|-------|--------|-------|-------|-------|----------|----------|----------|
| 2 | 3:QZgeProj. | * | -2.47 | -2.47 | 0.000 | 0.000 | 0.00 | 0.20 | 0.00 |

Opmerkingen

[*] Deze belasting is handmatig toegevoegd of gewijzigd.

BELASTINGEN

B.G:16 Knik



KNOOPBELASTINGEN

B.G:16 Knik

| Last | Knoop | Richting | waarde | Ψ_0 | Ψ_1 | Ψ_2 |
|------|-------|----------|--------|----------|----------|----------|
| 1 | 2 | X | 1.000 | | | |
| 2 | 3 | X | 1.000 | | | |

REACTIES

| Kn. | B.G. | X | Z | M |
|-----|------|-------|--------|-------|
| 1 | 1 | 0.22 | 21.99 | 0.04 |
| 1 | 2 | 0.06 | 7.73 | -0.00 |
| 1 | 3 | 0.13 | 3.71 | 0.06 |
| 1 | 4 | 0.05 | 1.00 | 0.02 |
| 1 | 5 | -8.46 | -14.99 | -6.89 |
| 1 | 6 | -6.24 | -16.12 | -6.40 |
| 1 | 7 | -8.46 | -14.96 | -6.89 |
| 1 | 8 | -6.24 | -16.10 | -6.40 |
| 1 | 9 | 4.76 | 13.19 | 6.04 |
| 1 | 10 | 6.98 | 12.05 | 6.54 |
| 1 | 11 | 4.76 | 13.48 | 6.04 |
| 1 | 12 | 6.99 | 12.34 | 6.54 |
| 1 | 13 | 1.36 | 0.92 | 0.33 |
| 1 | 14 | 3.55 | -1.03 | 0.82 |
| 1 | 15 | 0.13 | 3.71 | 0.06 |
| 1 | 16 | -1.00 | -4.03 | -1.46 |
| 4 | 1 | -0.22 | 21.99 | -0.04 |
| 4 | 2 | -0.06 | 7.73 | 0.00 |
| 4 | 3 | -0.13 | 3.71 | -0.06 |
| 4 | 4 | -0.05 | 1.00 | -0.02 |
| 4 | 5 | -4.76 | 13.19 | -6.04 |
| 4 | 6 | -6.98 | 12.05 | -6.54 |
| 4 | 7 | -4.76 | 13.48 | -6.04 |
| 4 | 8 | -6.99 | 12.34 | -6.54 |
| 4 | 9 | 8.46 | -14.99 | 6.89 |
| 4 | 10 | 6.24 | -16.12 | 6.40 |
| 4 | 11 | 8.46 | -14.96 | 6.89 |
| 4 | 12 | 6.24 | -16.10 | 6.40 |
| 4 | 13 | -1.36 | 0.92 | -0.33 |
| 4 | 14 | -3.55 | -1.03 | -0.82 |
| 4 | 15 | -0.13 | 3.71 | -0.06 |
| 4 | 16 | -1.00 | 4.03 | -1.46 |

BELASTINGCOMBINATIES

| BC | Type | BG | Gen. | Factor | BG | Gen. | Factor | BG | Gen. | Factor | BG | Gen. | Factor |
|----|-------|----|------|--------|----|------|--------|----|------|--------|----|------|--------|
| 1 | Fund. | 1 | Perm | 1.35 | | | | | | | | | |
| 2 | Fund. | 1 | Perm | 0.90 | | | | | | | | | |
| 3 | Fund. | 1 | Perm | 1.20 | 4 | Extr | 1.50 | | | | | | |
| 4 | Fund. | 1 | Perm | 1.20 | 5 | Extr | 1.50 | | | | | | |
| 5 | Fund. | 1 | Perm | 1.20 | 6 | Extr | 1.50 | | | | | | |
| 6 | Fund. | 1 | Perm | 1.20 | 7 | Extr | 1.50 | | | | | | |
| 7 | Fund. | 1 | Perm | 1.20 | 8 | Extr | 1.50 | | | | | | |
| 8 | Fund. | 1 | Perm | 1.20 | 9 | Extr | 1.50 | | | | | | |
| 9 | Fund. | 1 | Perm | 1.20 | 10 | Extr | 1.50 | | | | | | |
| 10 | Fund. | 1 | Perm | 1.20 | 11 | Extr | 1.50 | | | | | | |
| 11 | Fund. | 1 | Perm | 1.20 | 12 | Extr | 1.50 | | | | | | |
| 12 | Fund. | 1 | Perm | 1.20 | 13 | Extr | 1.50 | | | | | | |
| 13 | Fund. | 1 | Perm | 1.20 | 14 | Extr | 1.50 | | | | | | |
| 14 | Fund. | 1 | Perm | 1.20 | 15 | Extr | 1.50 | | | | | | |
| 15 | Fund. | 1 | Perm | 0.90 | 4 | Extr | 1.50 | | | | | | |
| 16 | Fund. | 1 | Perm | 0.90 | 5 | Extr | 1.50 | | | | | | |
| 17 | Fund. | 1 | Perm | 0.90 | 6 | Extr | 1.50 | | | | | | |
| 18 | Fund. | 1 | Perm | 0.90 | 7 | Extr | 1.50 | | | | | | |
| 19 | Fund. | 1 | Perm | 0.90 | 8 | Extr | 1.50 | | | | | | |
| 20 | Fund. | 1 | Perm | 0.90 | 9 | Extr | 1.50 | | | | | | |
| 21 | Fund. | 1 | Perm | 0.90 | 10 | Extr | 1.50 | | | | | | |
| 22 | Fund. | 1 | Perm | 0.90 | 11 | Extr | 1.50 | | | | | | |
| 23 | Fund. | 1 | Perm | 0.90 | 12 | Extr | 1.50 | | | | | | |
| 24 | Fund. | 1 | Perm | 0.90 | 13 | Extr | 1.50 | | | | | | |
| 25 | Fund. | 1 | Perm | 0.90 | 14 | Extr | 1.50 | | | | | | |
| 26 | Fund. | 1 | Perm | 0.90 | 15 | Extr | 1.50 | | | | | | |
| 27 | Fund. | 1 | Perm | 1.20 | 2 | Extr | 1.50 | 3 | Extr | 1.50 | | | |
| 28 | Fund. | 1 | Perm | 0.90 | 2 | Extr | 1.50 | 3 | Extr | 1.50 | | | |
| 29 | Kar. | 1 | Perm | 1.00 | 4 | Extr | 1.00 | | | | | | |
| 30 | Kar. | 1 | Perm | 1.00 | 5 | Extr | 1.00 | | | | | | |
| 31 | Kar. | 1 | Perm | 1.00 | 6 | Extr | 1.00 | | | | | | |
| 32 | Kar. | 1 | Perm | 1.00 | 7 | Extr | 1.00 | | | | | | |
| 33 | Kar. | 1 | Perm | 1.00 | 8 | Extr | 1.00 | | | | | | |
| 34 | Kar. | 1 | Perm | 1.00 | 9 | Extr | 1.00 | | | | | | |
| 35 | Kar. | 1 | Perm | 1.00 | 10 | Extr | 1.00 | | | | | | |
| 36 | Kar. | 1 | Perm | 1.00 | 11 | Extr | 1.00 | | | | | | |
| 37 | Kar. | 1 | Perm | 1.00 | 12 | Extr | 1.00 | | | | | | |
| 38 | Kar. | 1 | Perm | 1.00 | 13 | Extr | 1.00 | | | | | | |
| 39 | Kar. | 1 | Perm | 1.00 | 14 | Extr | 1.00 | | | | | | |
| 40 | Kar. | 1 | Perm | 1.00 | 15 | Extr | 1.00 | | | | | | |
| 41 | Kar. | 1 | Perm | 1.00 | 2 | Extr | 1.00 | 3 | Extr | 1.00 | | | |
| 42 | Quas. | 1 | Perm | 1.00 | | | | | | | | | |
| 43 | Freq. | 1 | Perm | 1.00 | | | | | | | | | |
| 44 | Freq. | 1 | Perm | 1.00 | 5 | psi1 | 1.00 | | | | | | |
| 45 | Freq. | 1 | Perm | 1.00 | 6 | psi1 | 1.00 | | | | | | |
| 46 | Freq. | 1 | Perm | 1.00 | 7 | psi1 | 1.00 | | | | | | |
| 47 | Freq. | 1 | Perm | 1.00 | 8 | psi1 | 1.00 | | | | | | |
| 48 | Freq. | 1 | Perm | 1.00 | 9 | psi1 | 1.00 | | | | | | |
| 49 | Freq. | 1 | Perm | 1.00 | 10 | psi1 | 1.00 | | | | | | |
| 50 | Freq. | 1 | Perm | 1.00 | 11 | psi1 | 1.00 | | | | | | |
| 51 | Freq. | 1 | Perm | 1.00 | 12 | psi1 | 1.00 | | | | | | |
| 52 | Freq. | 1 | Perm | 1.00 | 13 | psi1 | 1.00 | | | | | | |
| 53 | Freq. | 1 | Perm | 1.00 | 14 | psi1 | 1.00 | | | | | | |
| 54 | Freq. | 1 | Perm | 1.00 | 15 | psi1 | 1.00 | | | | | | |
| 55 | Blij. | 1 | Perm | 1.00 | | | | | | | | | |

GUNSTIGE WERKING PERMANENTE BELASTINGEN

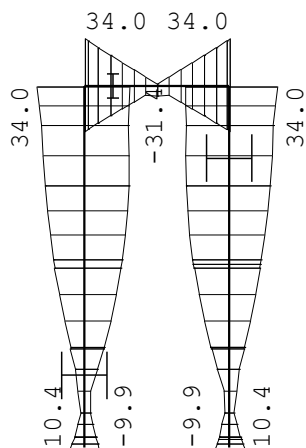
BC Staven met gunstige werking

- 1 Geen
- 2 Alle staven de factor:0.90
- 3 Geen
- 4 Geen
- 5 Geen
- 6 Geen
- 7 Geen
- 8 Geen
- 9 Geen
- 10 Geen
- 11 Geen
- 12 Geen
- 13 Geen
- 14 Geen
- 15 Alle staven de factor:0.90
- 16 Alle staven de factor:0.90
- 17 Alle staven de factor:0.90
- 18 Alle staven de factor:0.90
- 19 Alle staven de factor:0.90
- 20 Alle staven de factor:0.90
- 21 Alle staven de factor:0.90
- 22 Alle staven de factor:0.90
- 23 Alle staven de factor:0.90
- 24 Alle staven de factor:0.90
- 25 Alle staven de factor:0.90
- 26 Alle staven de factor:0.90
- 27 Geen
- 28 Alle staven de factor:0.90

OMHULLENDE VAN DE FUNDAMENTELE COMBINATIES

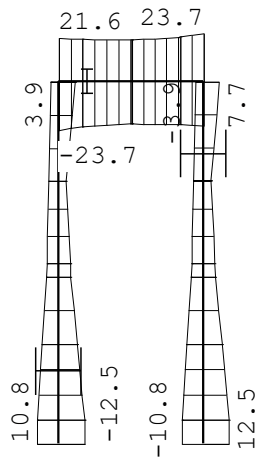
MOMENTEN

Fundamentele combinatie



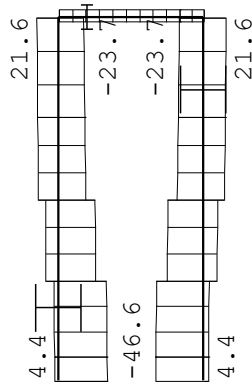
DWARSKRACHTEN

Fundamentele combinatie



NORMAALKRACHTEN

Fundamentele combinatie



STAAFKRACHTEN

Fundamentele combinatie

| St. | Kn. | Pos. | NXi/NXj | | DZi/DZj | | MYi/MYj | | | | | | | |
|-----|-----|-------|---------|--------|---------|--------|---------|--------|-------|----|--------|----|-------|----|
| | | | Min BC | Max BC | Min BC | Max BC | Min BC | Max BC | | | | | | |
| 1 | 1 | | -46.58 | 10 | 4.38 | 17 | -12.52 | 16 | 10.76 | 11 | -9.88 | 9 | 10.36 | 16 |
| 1 | | 0.500 | -46.33 | 10 | 4.57 | 17 | -12.52 | 16 | 10.76 | 11 | -5.48 | 20 | 5.03 | 5 |
| 1 | | 0.745 | -46.21 | 10 | 4.66 | 17 | -11.97 | 16 | 10.37 | 11 | -3.70 | 20 | 2.84 | 5 |
| 1 | | 1.001 | -46.08 | 10 | 4.76 | 17 | -11.38 | 16 | 9.96 | 11 | -1.87 | 20 | 4.10 | 13 |
| 1 | | 1.001 | -46.08 | 10 | 4.76 | 17 | -11.38 | 16 | 9.96 | 11 | -1.88 | 20 | 4.10 | 13 |
| 1 | | 2.075 | -45.53 | 10 | 5.16 | 17 | -8.94 | 16 | 8.26 | 11 | -12.80 | 16 | 10.47 | 11 |
| 1 | | 2.075 | -35.48 | 10 | 12.71 | 17 | -8.94 | 16 | 8.26 | 11 | -13.18 | 16 | 9.97 | 11 |
| 1 | | 3.735 | -34.63 | 10 | 13.34 | 17 | -5.47 | 17 | 5.94 | 10 | -24.89 | 16 | 21.51 | 11 |
| 1 | | 3.735 | -25.56 | 10 | 20.14 | 17 | -5.47 | 17 | 5.94 | 10 | -25.24 | 16 | 21.06 | 11 |
| 1 | | 5.464 | -24.69 | 10 | 20.80 | 17 | -3.51 | 17 | 5.17 | 10 | -30.77 | 16 | 28.44 | 11 |
| 1 | | 5.955 | -24.44 | 10 | 20.99 | 17 | -4.53 | 25 | 4.88 | 10 | -31.07 | 16 | 29.65 | 11 |
| 1 | | 6.691 | -24.06 | 10 | 21.26 | 17 | -6.06 | 25 | 4.43 | 10 | -30.39 | 16 | 30.68 | 11 |
| 1 | 2 | | -23.65 | 10 | 21.57 | 17 | -7.75 | 25 | 3.94 | 10 | -31.42 | 17 | 34.01 | 10 |
| 2 | 2 | | -3.94 | 6 | 7.75 | 25 | -23.65 | 10 | 21.57 | 17 | -31.42 | 17 | 34.01 | 10 |
| 2 | | 1.227 | -3.94 | 6 | 7.75 | 25 | -20.90 | 8 | 20.62 | 17 | -6.18 | 7 | 7.55 | 20 |
| 2 | | 1.495 | -3.94 | 6 | 7.75 | 25 | -20.53 | 9 | 20.53 | 17 | -6.23 | 13 | 2.02 | 20 |
| 2 | | 1.500 | -3.94 | 6 | 7.75 | 25 | -20.53 | 9 | 20.53 | 5 | -6.23 | 13 | 1.91 | 20 |
| 2 | | 1.505 | -3.94 | 6 | 7.75 | 25 | -20.53 | 9 | 20.53 | 5 | -6.23 | 13 | 2.02 | 16 |
| 2 | | 1.773 | -3.94 | 6 | 7.75 | 25 | -20.62 | 21 | 20.90 | 4 | -6.18 | 13 | 7.55 | 16 |
| 2 | 3 | | -3.94 | 6 | 7.75 | 25 | -21.57 | 21 | 23.65 | 6 | -31.42 | 21 | 34.01 | 6 |

STAAFKRACHTEN

Fundamentele combinatie

| St. | Kn. | Pos. | NXi/NXj | | DZi/DZj | | MYi/MYj | | | | | | | |
|-----|-----|-------|---------|--------|---------|--------|---------|--------|-------|----|--------|----|-------|----|
| | | | Min BC | Max BC | Min BC | Max BC | Min BC | Max BC | | | | | | |
| 3 | 3 | | -23.65 | 6 | 21.57 | 21 | -3.94 | 6 | 7.75 | 25 | -31.42 | 21 | 34.01 | 6 |
| 3 | | 0.809 | -24.06 | 6 | 21.26 | 21 | -4.43 | 6 | 6.06 | 25 | -30.39 | 21 | 30.68 | 7 |
| 3 | | 1.544 | -24.44 | 6 | 20.99 | 21 | -4.88 | 6 | 4.53 | 25 | -31.07 | 20 | 29.65 | 7 |
| 3 | | 2.035 | -24.69 | 6 | 20.80 | 21 | -5.17 | 6 | 3.51 | 25 | -30.77 | 20 | 28.44 | 7 |
| 3 | | 3.765 | -25.56 | 6 | 20.14 | 21 | -5.94 | 6 | 5.47 | 21 | -25.24 | 8 | 21.06 | 19 |
| 3 | | 3.765 | -34.63 | 6 | 13.34 | 21 | -5.94 | 6 | 5.47 | 21 | -24.89 | 8 | 21.51 | 19 |
| 3 | | 5.425 | -35.48 | 6 | 12.71 | 21 | -8.26 | 7 | 8.94 | 20 | -13.18 | 8 | 9.97 | 19 |
| 3 | | 5.425 | -45.53 | 6 | 5.16 | 21 | -8.26 | 7 | 8.94 | 20 | -12.80 | 8 | 10.47 | 19 |
| 3 | | 6.499 | -46.08 | 6 | 4.76 | 21 | -9.96 | 7 | 11.38 | 20 | -1.88 | 20 | 4.10 | 13 |
| 3 | | 6.499 | -46.08 | 6 | 4.76 | 21 | -9.96 | 7 | 11.38 | 20 | -1.87 | 20 | 4.10 | 13 |
| 3 | | 6.755 | -46.21 | 6 | 4.66 | 21 | -10.37 | 7 | 11.97 | 20 | -3.70 | 16 | 2.84 | 13 |
| 3 | | 7.000 | -46.33 | 6 | 4.57 | 21 | -10.76 | 7 | 12.52 | 20 | -5.48 | 16 | 5.03 | 9 |
| 3 | 4 | | -46.58 | 6 | 4.38 | 21 | -10.76 | 7 | 12.52 | 20 | -9.89 | 5 | 10.37 | 20 |

REACTIES

Fundamentele combinatie

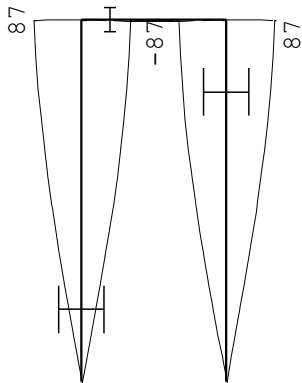
| Kn. | X-min | X-max | Z-min | Z-max | M-min | M-max |
|-----|--------|-------|-------|-------|--------|-------|
| 1 | -12.52 | 10.76 | -4.38 | 46.58 | -10.36 | 9.88 |
| 4 | -10.76 | 12.52 | -4.38 | 46.58 | -9.88 | 10.36 |

OMHULLENDE VAN DE KARAKTERISTIEKE COMBINATIES

VERPLAATSINGEN

[mm]

Karakteristieke combinatie



REACTIES

Karakteristieke combinatie

| Kn. | X-min | X-max | Z-min | Z-max | M-min | M-max |
|-----|-------|-------|-------|-------|-------|-------|
| 1 | -8.24 | 7.20 | 5.87 | 35.48 | -6.85 | 6.58 |
| 4 | -7.20 | 8.24 | 5.87 | 35.48 | -6.58 | 6.85 |

STAALPROFIELEN - ALGEMENE GEGEVENS

| | | |
|------------------------------|---|-------------|
| Stabiliteit: | Classificatie gehele constructie: | Ongeschoord |
| | Belastinggeval m.b.t. bepaling kniklengte: | 16=Knik |
| | Aanpassing inkl. parameter C : | Nee |
| Tweede-orde-effect: | | |
| | Aan te houden verhouding $n/(n-1)$ voor steunmomenten en verplaatsingen: | 1.10 |
| Doorbuiging en verplaatsing: | | |
| | Aantal bouwlagen: | 1 |
| | Gebouwtype: | Industrieel |
| | Toel. horiz. verplaatsing gehele gebouw: | h/150 |
| | Kleinste gevelhoogte [m]: | 0.0 |

PROFIEL/MATERIAAL

| P/M nr. | Profielnaam | Vloeisp. [N/mm ²] | Productie methode | Min. drsn. klasse |
|---------|-------------|-------------------------------|-------------------|-------------------|
| 1 | HEA200 | 235 | Gewalst | 1 |
| 2 | IPE200 | 235 | Gewalst | 1 |

Partiële veiligheidsfactoren:

| | | | | | |
|-----------|---|------|-----------|---|------|
| Gamma M;0 | : | 1.00 | Gamma M;1 | : | 1.00 |
|-----------|---|------|-----------|---|------|

KNIKSTABILITEIT

| Staafl | l_{sys} [m] | Classif. y sterke as | $l_{knik;y}$ [m] | Extra | | Extra | |
|--------|---------------|----------------------|------------------|--------------|----------------------|------------------|--------------|
| | | | | aanp. y [kN] | Classif. z zwakke as | $l_{knik;z}$ [m] | aanp. z [kN] |
| 1 | 7.500 | Ongeschoord | 15.239 | 0.0 | Geschoord | 7.500 | 0.0 |
| 2 | 3.000 | Ongeschoord | 3.973 | 0.0 | Geschoord | 3.000 | 0.0 |
| 3 | 7.500 | Ongeschoord | 15.223 | 0.0 | Geschoord | 7.500 | 0.0 |

KIPSTABILITEIT

| Staafl | Plts. aangr. | l gaffel [m] | Kipsteunafstanden [m] | |
|--------|--------------|--------------|-----------------------|-------|
| 1 | 1.0*h | boven: | 7.50 | 7.500 |
| | | | onder: | 7.50 |
| 2 | 1.0*h | boven: | 3.00 | 3.000 |
| | | | onder: | 3.00 |
| 3 | 1.0*h | boven: | 7.50 | 7.500 |
| | | | onder: | 7.50 |

TOETSING SPANNINGEN

| Staafl nr. | P/M | BC | Sit | Kl | Plaats | Norm | Artikel | Formule | Hoogste toetsing U.C. [N/mm ²] | | Opm. |
|------------|-----|----|-----|----|--------|---------|---------|---------|--|-----|-------|
| 1 | 1 | 10 | 1 | 1 | Staafl | EN3-1-1 | 6.3.3 | (6.61) | 0.568 | 134 | 46,47 |
| 2 | 2 | 6 | 1 | 1 | Einde | EN3-1-1 | 6.2.10 | (6.31) | 0.722 | 170 | 46 |
| 3 | 1 | 6 | 1 | 1 | Staafl | EN3-1-1 | 6.3.3 | (6.61) | 0.568 | 133 | 46,47 |

Opmerkingen:

[46] T.b.v. kip is een equivalente Q-last berekend.

[47] Bij verlopende normaalkracht wordt de grootste drukkracht genomen.

TOETSING DOORBUIGING

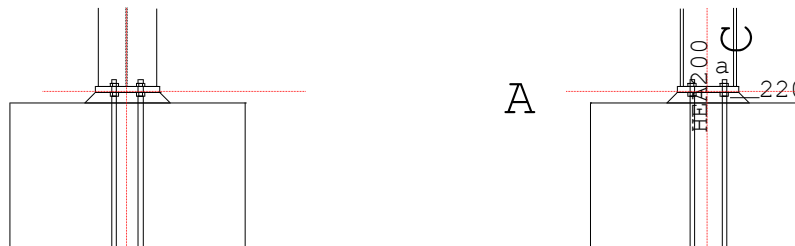
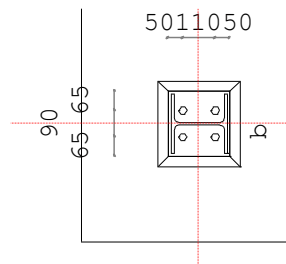
| Staafl | Soort | Mtg | Lengte [m] | Overst I | Zeeg J | Zeeg [mm] | u_{tot} [mm] | BC | Sit | u [mm] | Toelaatbaar [mm] | *1 |
|--------|-------|-----|------------|----------|--------|-----------|----------------|----|--------|--------|------------------|-------|
| 2 | Dak | db | 3.00 | N | N | 0.0 | -1.3 | 39 | 1 Eind | -1.3 | -12.0 | 0.004 |
| | | db | | | | | | | 39 | 1 Bijk | -1.0 | -12.0 |

9.5.1 Verbindingen

VERBINDINGEN - BASISGEGEVENS

Voetpl:1

| | |
|---|--------------------|
| Verbindingstype | Voetplaat |
| Knopen | 1,4 |
| Rekenwaarde vloeispanning $f_{y;d}$ platen | 235 |
| Hoek basis staaf AB t.o.v. globale as (linksom positief) | 0 |
| Classificatie constructie | Ongeschoord |
| Rekenmodel gebruikt bij de mechanicaresultaten | 1e orde elastisch |
| Statisch systeem | Statisch onbepaald |
| Verbinding t.p.v. plastisch scharnier | Nee |
| Alternatieve methode T-stuk volgens EN 1993-1-8 tabel 6.2 | Ja |
| Is poer gewapend? | Ja |



LEGENDA

| Onderdeel | Afmetingen | Aantal Lassen (d=dubb. hoeklas) |
|-------------|------------|---------------------------------|
| a Voetplaat | 220x210-20 | 1 $a_w=3d$ $a_f=5d$ |
| b Anker | M16 4.6 | 4 $L_{b1}=500$ $L_{b,tot}=68$ |

PROFIELEN

| Naam | Lengte | Prod.meth. | Exc | Hoek | $f_{y;d}$ | |
|----------|--------|------------|---------|------|-----------|-----|
| Staaft C | HEA200 | 7500 | Gewalst | 0 | 0 | 235 |

PROFIELGEGEVENS [mm]

| Gewalst Klasse 1 HEA200 | | | |
|-------------------------|-------|--------------|--------------------|
| h : | 190.0 | $i_y :$ 82.8 | A : 5380.0 |
| b : | 200.0 | $i_z :$ 49.8 | $W_{ey} :$ 389.0E3 |
| $t_w :$ | 6.5 | r : 18.0 | $I_y :$ 3692.0E4 |
| $t_f :$ | 10.0 | | $W_{ez} :$ 133.6E3 |
| | | | $I_z :$ 1336.0E4 |
| | | | $W_{py} :$ 429.4E3 |
| | | | $I_t :$ 21.1E4 |
| | | | $W_{pz} :$ 203.8E3 |
| | | | $I_w :$ 108000.0E6 |

PLATEN

| Plaats | h | b | t | Exc | a_w | a_f | a_e | Hoek | Las | $f_{y;d}$ |
|-----------|----------|-----|-----|------|-------|------------------|------------------|------|-----|-----------|
| Voetplaat | Staaft C | 210 | 220 | 20.0 | 0 | $\Delta\Delta 3$ | $\Delta\Delta 5$ | | | 235 |

Δ = Enkele stompe of hoeklas of dubbele hoeklas met slechts 1 las effectief

$\Delta\Delta$ = Dubbele hoeklas

ANKERS

| d | kw | hoh | milieu | lengte | v (vanaf zijde C) | |
|----------|-----|-----|--------|------------|-------------------|--------|
| Staaft C | M16 | 4.6 | 90 | Niet-corr. | 500 | 50;160 |

ANKERGEGEVENS

| d | d ₀ | d _m | d _{kop} | t _{kop} | d _{moer} | t _{moer} | A | A _s | γ _M | f _{ybd} | f _{tbd} | Draad |
|------|----------------|----------------|------------------|------------------|-------------------|-------------------|-------|----------------|----------------|------------------|------------------|--------|
| 16.0 | 20.0 | 33.3 | 24.0 | 10.0 | 24.0 | 13.0 | 201.1 | 156.7 | 1.25 | 240 | 400 | Gerold |

BETON EN VOEG

| | Lengte | Breedte | Dikte | Helling | Kwaliteit |
|------|--------|---------|-------|---------|-----------|
| Voeg | 210 | 220 | 35.0 | 45.0 | C20/25 |

KRACHTEN

Kn:4 BC:8 Sit:1

| | Normaalkr. | Dwarskr. | Moment | MSteun | DSteun |
|----------|------------|----------|--------|--------|--------|
| Staaft C | 3.95 | -12.46 | -10.36 | 1.04 | -1.25 |

RESULTATEN DRUKZONE

Kn:4 BC:8 Sit:1

| | | | | | |
|-------------------------------|--------------------|---|----------|-------------------------|--|
| Vergrotingsfactor | k _c | : | 3.00 | | |
| Rekenwaarde druksterkte | f'_{c,Rd} | : | 13.33 | | |
| Rekenwaarde druksterkte | f_{jd} | : | 26.67 | | |
| Vorm van de indrukingsprent | | : | I-vormig | 54 * 220 | |
| | | : | | 101 * 0 | |
| | | : | | 54 * 220 | |
| Max. drukoppervlakte | | : | | 23892 | |
| Spreidingsmaat // flenzen | l _s | : | 34.28 | | |
| Spreidingsmaat // lijf | l_{s lijf} | : | 34.28 | | |
| Rek meest gedrukte zijde | eps _c | : | 0.00058 | | |
| Spanning meest gedrukte zijde | sigma _c | : | 13.31 | | |
| Rek getrokken zijde | eps _t | : | -0.00118 | | |
| Momentcapaciteit | | : | 16.22 | | |
| Moment tbv. lassen | | : | 80.73 | gebaseerd op 0.8*MplRd | |
| Max. opneembare dwarskracht | | : | 74.60 | Crit.: Afsch.cap.ankers | |
| Trekcapaciteit ankerrij | | : | 90.26 | | |

RESULTATEN TREKZONE

Kn:4 BC:8 Sit:1

| Rij | F _{t,Rd} | Arm | Moment |
|-----|-------------------|-------|--------|
| 2 | 0.00 | 32.4 | 0.00 |
| 1 | 77.89 | 142.4 | 11.09 |

TUSSENRESULTATEN STIJFHEID

Kn:4 BC:8 Sit:1

| bij M _{v,Rd} voor boutrij binnen trekflens (h ₁) | | | | Staaft C |
|---|------------------------|----------------|-----------------|----------|
| i | Onderdeel | k _i | mu _i | Bijdrage |
| 13 | Drukzone beton | 2.142 | 2.988 | 40% |
| 15 | Buiging/trek voetplaat | 10.765 | 2.988 | 8% |
| 16 | Trekzone ankerbout | 1.654 | 2.988 | 52% |

STIJFHEID

Kn:4 BC:8 Sit:1

Maatgevend criterium: Trekzone ankerbout

Staaft C

| Verh. | M _{v,Rd} /Verh. | Arm | S _j | φ |
|-------|--------------------------|-----|----------------|---------|
| 1.0 | 16.22 | 136 | 1124 | 0.01443 |
| 1.2 | 13.52 | 136 | 1839 | 0.00735 |
| 1.5 | 10.82 | 136 | 3359 | 0.00322 |

Bij een moment M_{v,Ed}=11.39 geldt een stijfheid S_j=3033.
De in mechanica gebruikte stijfheid is S=3359 kNm/rad.

TOETSING VOETPLAAT-VERBINDING

Kn:4 BC:8 Sit:1

| Artikel | | | | Toetsing |
|---------|--------------------------------------|---|---------|--------------|
| 6.2.6.5 | m _{Ed} / m _{pl,Rd} | = | 7818 / | 23500 = 0.33 |
| 6.2.6.5 | σ _{Ed} / f _{jd} | = | 13.31 / | 26.67 = 0.50 |

TOETSING PROFIELEN EN AFSCHUIVING

Kn:4 BC:8 Sit:1

| Plaats | Profiel | Artikel | Formule | Toetsing |
|----------|---------|---------|-----------------|----------|
| Staaft C | HEA200 | EN3-1-1 | 6.2.10 (6.31) | 0.11 |
| | | EN3-1-1 | 6.2.8 (6.30) | 0.11 |
| | | EN3-1-1 | 6.2.5 (6.12y) | 0.11 |
| | | EN3-1-1 | 6.2.6 (6.17) | 0.06 |
| | | EN3-1-1 | 6.2.1 (6) N+D | 0.06 |
| | | EN3-1-8 | 6.2.2 (7) (6.2) | 0.18 |

MOMENTCLASSIFICATIE EN3-1-8 art.5.2.3

Kn:4 BC:8 Sit:1

| Plaats | $M_{v,Rd}$ | $M_{v,Rd,staaf}$ | Classificatie |
|----------|------------|------------------|---------------|
| Staaft C | 16.22 | 100.91 | Scharnierend |

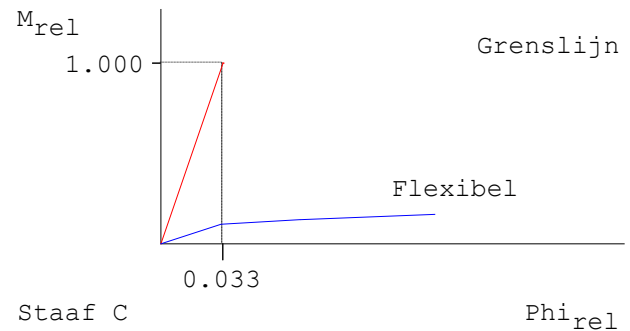
STIJFHEIDSClassificatie EN3-1-8 art.5.2.2

Kn:4 BC:8 Sit:1

| Plaats | Punt | Grenswaarden | | Actuele waarden | | Classificatie |
|----------|------|--------------|-----------|-----------------|-----------|---------------|
| | | Φ_{rel} | m_{rel} | Φ_{rel} | m_{rel} | |
| Staaft C | 1 | 0.000 | 0.000 | 0.000 | 0.000 | Flexibel |
| | 2 | 0.033 | 1.000 | 0.033 | 0.107 | |
| | 3 | 0.033 | 1.000 | 0.075 | 0.134 | |
| | 4 | 0.033 | 1.000 | 0.148 | 0.161 | |

M-PHI DIAGRAM EN3-1-8 fig. 5.4 Ongeschoord

Kn:4 BC:8 Sit:1



CONTROLES

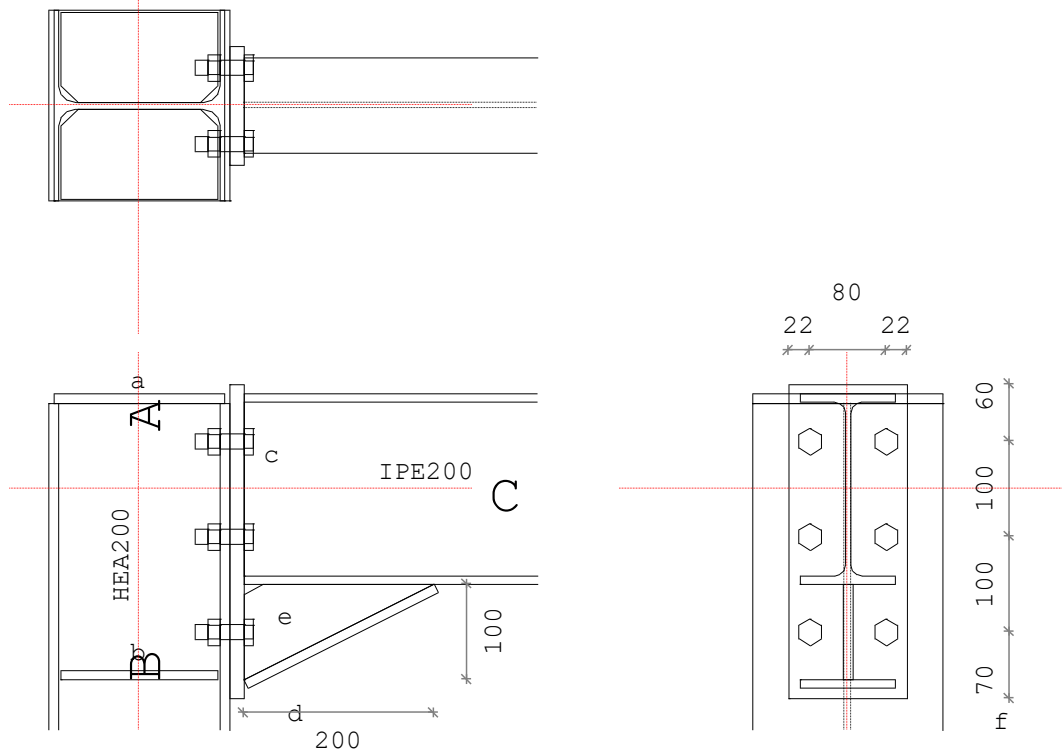
Kn:4 BC:8 Sit:1

| Onderdeel | Plaats | Rij | Item | Ernst | Art./ (Frm.) | Min. | Waarde | Max. |
|---------------|----------|-----|-------------------------|-------|--------------|-------|--------|--------------|
| Anker | Staaft C | 1 | HOH-afstand p1 | 3.5 | (1) | 44.0 | 110.0 | |
| | | 1 | HOH-afstand p2 | 3.5 | (1) | 48.2 | 90.0 | 172.0 |
| | | 2 | HOH-afstand p2 | 3.5 | (1) | 48.2 | 90.0 | 172.0 |
| Anker (Plaat) | Staaft C | 1 | Eindafstand e1 | 3.5 | (1) | 24.0 | 50.0 | |
| | | 2 | Eindafstand e1 | 3.5 | (1) | 24.0 | 50.0 | |
| Voeg | Staaft C | | Betonsterkte | 6.2.5 | | 4.0 | 20.0 | |
| | | | Dikte | 6.2.5 | | | 35.0 | 42.0 |
| Voetplaat | Staaft C | | Dikte | 6.2.5 | | 14.1 | 20.0 | |
| | | | Flenslas $\Delta\Delta$ | 0.8 | M_{plRd} | 3.69 | 5.00 | |
| | | | Lijflas $\Delta\Delta$ | 0.8 | M_{plRd} | 3.00 | 3.00 | |
| | | | Positie boven | | | 102.1 | 105.0 | |
| | | | Positie onder | | | | | -105.0-102.1 |

VERBINDINGEN - BASISGEGEVENS

Knie:1

| | |
|---|--------------------|
| Verbindingstype | Knie Gebout |
| Knopen | 2,3 |
| Rekenwaarde vloeispanning $f_y; d$ platen | 235 |
| Hoek basis staaf AB t.o.v. globale as (linksom positief) | 270 |
| Classificatie constructie | Ongeschoord |
| Classificatie lijf staaf AB | Geschoord |
| Afschuiving lijf staaf AB actief? | Ja |
| Rekenmodel gebruikt bij de mechanicaresultaten | 1e orde elastisch |
| Statisch systeem | Statisch onbepaald |
| Verbinding t.p.v. plastisch scharnier | Ja |
| Alternatieve methode T-stuk volgens EN 1993-1-8 tabel 6.2 | Ja |



LEGENDA

| Onderdeel | Afmetingen | Aantal Lassen (d=dubb. hoeklas) |
|----------------|------------|---------------------------------|
| a Afdekplaat | 200x180-10 | 1 $aw=3d$ $af=10$ |
| b Schot AB | 95x165-10 | 1 $aw=5d$ $af=5d$ |
| c Kopplaat | 125x330-15 | 1 $aw=3d$ $af=4d$ |
| d Consoleflens | 100x223-10 | 1 $afe=5d$ $aff=11$ $afw=5d$ |
| e Consolelijf | 100x200-10 | 1 $awe=5d$ $awf=5d$ |
| f Bout | M16 8.8 | 6 |

PROFIELEN

| Naam | Lengte | Prod.meth. | Exc | Hoek | $f_y; d$ |
|----------|--------|------------|-----|------|----------|
| Staaft B | 7500 | Gewalst | 0 | 270 | 235 |
| Staaft C | 3000 | Gewalst | 0 | 0 | 235 |
| Staaft A | 90 | | | | |

PROFIELGEGEVENS [mm]

| | | | | Gewalst Klasse 1 HEA200 | | | | | |
|---------|-------|---------|------|-------------------------|--------|------------|---------|---------|------------|
| h : | 190.0 | $i_y :$ | 82.8 | A : | 5380.0 | $W_{ey} :$ | 389.0E3 | $I_y :$ | 3692.0E4 |
| b : | 200.0 | $i_z :$ | 49.8 | | | $W_{ez} :$ | 133.6E3 | $I_z :$ | 1336.0E4 |
| $t_w :$ | 6.5 | r : | 18.0 | | | $W_{py} :$ | 429.4E3 | $I_t :$ | 21.1E4 |
| $t_f :$ | 10.0 | | | | | $W_{pz} :$ | 203.8E3 | $I_w :$ | 108000.0E6 |

PROFIELGEGEVENS [mm]

Gewalst Klasse 1 IPE200

| | | | | | | | | | |
|------------------|-------|------------------|------|-----|--------|--------------------|---------|------------------|-----------|
| h : | 200.0 | i _y : | 82.6 | A : | 2848.0 | W _{e y} : | 194.3E3 | I _y : | 1943.0E4 |
| b : | 100.0 | i _z : | 22.4 | | | W _{e z} : | 28.5E3 | I _z : | 142.4E4 |
| t _w : | 5.6 | r : | 12.0 | | | W _{p y} : | 220.6E3 | I _t : | 6.9E4 |
| t _f : | 8.5 | | | | | W _{p z} : | 44.6E3 | I _w : | 12988.1E6 |

PLATEN

| | Plaats | h | b | t | Exc | a _w | a _f | a _e | Hoek | Las | f _{y, d} |
|--------------|----------|-----|-----|------|------|----------------|----------------|----------------|------|-----|-------------------|
| Kopplaat | Staaft C | 330 | 125 | 15.0 | -55 | ΔΔ3 | ΔΔ4 | | | | 235 |
| Consolelijf | B-C | 100 | 200 | 10.0 | | | ΔΔ5 | ΔΔ5 | | | 235 |
| Consoleflens | B-C | | 100 | 10.0 | | | Δ11 | ΔΔ5 | | | 235 |
| Schot | Staaft B | 165 | 95 | 10.0 | -195 | ΔΔ5 | ΔΔ5 | | 0 | | 235 |
| Afdekplaat | | 180 | 200 | 10.0 | 0 | ΔΔ3 | Δ10 | | 0 | | 235 |

Δ = Enkele stompe of hoeklas of dubbele hoeklas met slechts 1 las effectief
ΔΔ = Dubbele hoeklas

BOUTEN

d kwal hoh milieu lengte v (vanaf zijde B)

| | | | | | | |
|----------|-----|-----|----|------------|----|------------|
| Staaft C | M16 | 8.8 | 80 | Niet-corr. | 37 | 70;170;270 |
|----------|-----|-----|----|------------|----|------------|

BOUTGEGEVENS

| d | d ₀ | d _m | d _{kop} | t _{kop} | d _{moer} | t _{moer} | A | A _s | γ _M | f _{ybd} | f _{tbd} | Draad |
|------|----------------|----------------|------------------|------------------|-------------------|-------------------|-------|----------------|----------------|------------------|------------------|--------|
| 16.0 | 18.0 | 33.3 | 24.0 | 10.0 | 24.0 | 13.0 | 201.1 | 156.7 | 1.25 | 640 | 800 | Gerold |

KRACHTEN

Kn:2 BC:20 Sit:1

| | Normaalkr. | Dwarskr. | Moment | MSteun | DSteun |
|----------|------------|----------|--------|--------|--------|
| Staaft B | 22.35 | -3.87 | -33.77 | 3.38 | -0.39 |
| Staaft C | 3.87 | 22.35 | 33.77 | 3.38 | 2.24 |

BEZWIJKKRACHTEN

Kn:2 BC:20 Sit:1

| Onderdeel | F _{Rd} | Formule | b _{eff} | Staaft C |
|------------------------------|-----------------|----------|------------------------|---------------------------------|
| Afsch. lijf staaft AB | 220.41 | (6.7) | Avc= 1805 | omega=0.81 beta=1.00 |
| Druk lijf staaft AB | 583.34 | (6.9) | 175.0 | Drukpunt 14.41 |
| Plooi lijf staaft AB | 583.34 | | 175.0 | kwc=1.00 l _{rel} =0.73 |
| Drukzone kopplaat staaft C/D | 266.84 | (6.21) | | |
| Grensmoment Mc console | | | | |
| Afsch. lijf staaft C/D (mtg) | 37.04 | frmb 3.2 | Fsd LR profiel | -79.3 |
| Plooi lijf staaft C/D | 48.59 | frmb 3.2 | 112.5 Fsd profielflens | -158.6 |
| Vloei lijf staaft C/D | 67.68 | frmb 3.2 | 112.5 Fsd console | 177.3 |
| Afsch. tgv. cons. | 37.98 | | | |
| Trek bout | 90.26 | | | |
| Trek boutrij | 180.52 | | | |

Let op: De normaalkracht is verwerkt in bovengenoemde bezwijkkrachten.

Dwarskrachtcapaciteiten:

| | | |
|--------------------------------|--------|-------|
| Stuik flens staaft AB | 691.20 | (6.7) |
| Stuik kopplaat | 746.50 | (6.7) |
| Afsch.cap. bouten na red. trek | 256.08 | (6.7) |

TUSSENRESULTATEN KOLOMFLENS BUIGING

Kn:2 BC:20 Sit:1

Staaf C

| Rij | p | m ₁ | e | n | m ₂ | alpha | l _{ef} | Formule | F _{t;fc;Rd} | Bezw.vorm |
|------|-----|----------------|------|------|----------------|-------|-----------------|---------|----------------------|------------|
| 3 | 100 | 22.3 | 60.0 | 22.5 | 28.7 | 2*pi | 140.4 | T6.2v2 | 127.35 | 2=Plt+Bout |
| 2 | 100 | 22.3 | 60.0 | 22.5 | | | 164.4 | T6.2v2 | 133.63 | 2=Plt+Bout |
| 1 | 100 | 22.3 | 60.0 | 22.5 | 34.3 | 2*pi | 140.4 | T6.2v2 | 127.35 | 2=Plt+Bout |
| 2- 3 | | | | | | | 240.4 | T6.2v2 | 244.11 | 2=Plt+Bout |
| 1- 3 | | | | | | | 316.5 | T6.2v2 | 354.59 | 2=Plt+Bout |
| 1- 2 | | | | | | | 240.4 | T6.2v2 | 244.11 | 2=Plt+Bout |

TUSSENRESULTATEN KOPPLAAT BUIGING

Kn:2 BC:20 Sit:1

Staaf C

| Rij | p | m ₁ | e | n | m ₂ | alpha | l _{ef} | Formule | F _{t;ep;Rd} | Bezw.vorm |
|------|-----|----------------|------|------|----------------|-------|-----------------|---------|----------------------|------------|
| 3 | 100 | 33.8 | 22.5 | 22.5 | 37.0 | 5.01 | 169.3 | T6.2v2 | 151.64 | 2=Plt+Bout |
| 2 | 100 | 33.8 | 22.5 | 22.5 | 37.0 | 5.01 | 169.3 | T6.2v2 | 151.64 | 2=Plt+Bout |
| 1 | 0 | 29.3 | 22.5 | 22.5 | 44.3 | 5.02 | 147.3 | T6.2v2 | 153.45 | 2=Plt+Bout |
| 2- 3 | | | | | | | 275.3 | T6.2v2 | 273.53 | 2=Plt+Bout |

TUSSENRESULTATEN OVERIG

Kn:2 BC:20 Sit:1

Trek lijf staaf AB Trek lijf staaf C/D

Lassen Staaf C

6.2.6.3 (6.15) 6.2.6.8 (6.22) 4.5.3.2 (4.1)

| Rij | b _{ef} | F _{t,wc,Rd} | b _{ef} | F _{t,wb,Rd} | b _{ef} | F _{w,Rd} |
|------|-----------------|----------------------|-----------------|----------------------|-----------------|-------------------|
| 3 | 140.4 | 185.83 | 169.3 | 222.83 | 169.3 | 152.13 |
| 2 | 164.4 | 208.14 | 169.3 | 222.83 | 169.3 | 152.13 |
| 1 | 140.4 | 185.83 | 147.3 | 346.11 | 147.3 | 217.68 |
| 2- 3 | 240.4 | 261.36 | 275.3 | 362.30 | 275.3 | 247.34 |
| 1- 3 | 316.5 | 294.82 | | | | |
| 1- 2 | 240.4 | 261.36 | | | | |

BOU TRIJKRACHTEN

Herverdeling: Nee

Kn:2 BC:20 Sit:1

EN3-1-8 art. 6.2.7.2

Reductie : Ja

Staaf C

| Rij | F _{t,Rd,her} | F _{t,Rd} | Arm | M | Criterium |
|----------------------|-----------------------|-------------------|---------------------|---------------|--------------------------------|
| 3 | 127.35 | 127.35 | 255.6 | 32.55 | Flens staaf AB: Plaat+Bout |
| 2 | 116.76 | 93.06 | 155.6 | 14.48 | Flens staaf AB: Plaat+Bout |
| 1 | 50.71 | 0.00 | 55.6 | 0.00 | Trek lijf staaf AB |
| Som F= | | 220.41 | M _{v,Rd} = | 47.03 | Afsch. lijf staaf AB |
| Moment tbv. lassen = | | | | 51.84 | gebaseerd op 1.0*MplRd |
| | | | V _{v,Rd} = | 256.08 | Afsch.cap. bouten na red. trek |

TUSSENRESULTATEN STIJFHEID

Kn:2 BC:20 Sit:1

bij M_{v,Rd} voor bou trij binnen trekflens (h₁)

Staaf C

| i | Onderdeel | k _i | mu _i | Bijdrage |
|----|----------------------------|----------------|-----------------|----------|
| 1 | Afschuifzone lijf staaf AB | 3.213 | 2.988 | 55% |
| 2 | Drukzone lijf staaf AB | n.v.t. | | |
| 3 | Trekzone lijf staaf AB | 11.657 | 2.988 | 15% |
| 4 | Trekzone flens staaf AB | 21.370 | 2.988 | 8% |
| 5 | Trekzone kopplaat | 20.842 | 2.988 | 8% |
| 10 | Trekzone bouten | 13.229 | 2.988 | 13% |

STIJFHEID

Kn:2 BC:20 Sit:1

Maatgevend criterium: Afschuifzone lijf staaf AB

Staaf C

| Verh. | $M_{v,Rd}/\text{Verh.}$ | Arm | S_j | ϕ |
|-------|-------------------------|-----|-------------|---------|
| 1.0 | 47.03 | 214 | 5605 | 0.00839 |
| 1.2 | 39.19 | 214 | 9170 | 0.00427 |
| 1.5 | 31.35 | 214 | 16751 | 0.00187 |

Bij een moment $M_{v,Ed}=37.15$ geldt een stijfheid $S_j=11145$.
De in mechanica gebruikte stijfheid is $S=14411$ kNm/rad.

TOETSING VERBINDING

Kn:2 BC:20 Sit:1

| Artikel | $M_{v,Ed}$ | $M_{v,Rd}$ | Z | $V_{wp,Ed}$ | $V_{wp,Rd}$ | Toetsing |
|---------|------------|------------|-----|-------------|-------------|----------|
| 6.2.7.1 | 37.15 | 47.03 | | | | 0.79 |
| 6.2.6.1 | | | 213 | -4.26 | 220.41 | 0.02 |

Let op: Normaalkrachten in staven C & D zijn verwerkt in de bezwijk-
en/of de boutrijkrachten. De conservatieve toetsingsformule van
EN 1993-1-8 art. 6.2.7.1 (3) is niet gebruikt.

Toetsing snede bij console-aanzet op momentcapaciteit M_c

Staaf C $M_c;s;d = 29.63$ $M_c = 37.04$ 6.2.7.1 u.c. = 0.80

TOETSING PROFIELEN EN AFSCHUIVING

Kn:2 BC:20 Sit:1

| Plaats | Profiel | Artikel | Formule | Toetsing |
|---------|---------|---------|---------------|----------|
| Staaf B | HEA200 | EN3-1-1 | 6.2.10 (6.31) | 0.37 |
| | | EN3-1-1 | 6.2.8 (6.30) | 0.37 |
| | | EN3-1-1 | 6.2.5 (6.12y) | 0.37 |
| | | EN3-1-1 | 6.2.6 (6.17) | 0.02 |
| | | EN3-1-1 | 6.2.4 (6.9) | 0.02 |
| | | EN3-1-1 | 6.2.1(6) N+D | 0.04 |
| Staaf C | IPE200 | EN3-1-1 | 6.2.10 (6.31) | 0.72 |
| | | EN3-1-1 | 6.2.8 (6.30) | 0.72 |
| | | EN3-1-1 | 6.2.5 (6.12y) | 0.72 |
| | | EN3-1-1 | 6.2.6 (6.17) | 0.13 |
| | | EN3-1-1 | 6.2.1(6) N+D | 0.14 |
| | | EN3-1-8 | T.3.4 | 0.10 |

MOMENTCLASSIFICATIE EN3-1-8 art.5.2.3

Kn:2 BC:20 Sit:1

| Plaats | $M_{v,Rd}$ | $M_{v,Rd,staaf}$ | Classificatie |
|---------|------------|------------------|---------------------|
| Staaf C | 47.03 | 51.84 | Niet volledig sterk |

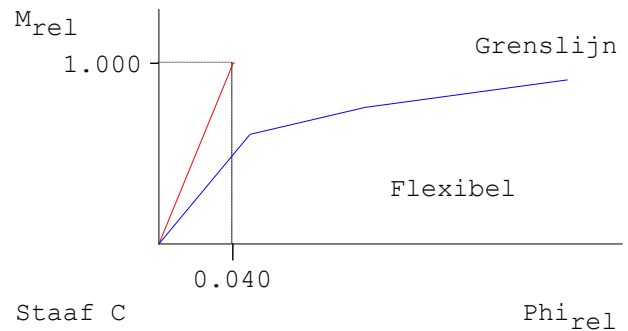
STIJFHEIDSCCLASSIFICATIE EN3-1-8 art.5.2.2

Kn:2 BC:20 Sit:1

| Plaats | Punt | Grenswaarden | | Actuele waarden | | Classificatie |
|---------|------|--------------|-----------|-----------------|-----------|---------------|
| | | Φ_{rel} | m_{rel} | Φ_{rel} | m_{rel} | |
| Staaf C | 1 | 0.000 | 0.000 | 0.000 | 0.000 | Flexibel |
| | 2 | 0.040 | 1.000 | 0.049 | 0.605 | |
| | 3 | 0.040 | 1.000 | 0.112 | 0.756 | |
| | 4 | 0.040 | 1.000 | 0.220 | 0.907 | |

M-PHI DIAGRAM EN3-1-8 fig. 5.4 Ongeschoord

Kn:2 BC:20 Sit:1



CONTROLES

Kn:2 BC:20 Sit:1

| Onderdeel | Plaats | Rij | Item | Ernst | Art./ (Frm.) | Min. | Waarde | Max. |
|--------------|----------|-----|-----------------------------|--------|--------------|-------|--------|-------|
| Afdekplaat | Staaaf C | | Dikte | | frmb 5.2.a | 4.7 | 10.0 | |
| | Staaaf C | | Flenslas Δ | | 1.0*MplRd | 9.2 | 10.0 | |
| | Staaaf C | | Lengte | | | 175.0 | 180.0 | 190.0 |
| | Staaaf C | | Lijflas $\Delta\Delta$ | | 1.0*MplRd | 3.00 | 3.00 | |
| Bout | Staaaf C | 1 | HOH-afstand p1 | 3.5(1) | | 39.6 | 100.0 | 140.0 |
| | Staaaf C | 1 | HOH-afstand p2 | 3.5(1) | | 75.8 | 80.0 | 81.8 |
| | Staaaf C | 2 | HOH-afstand p1 | 3.5(1) | | 39.6 | 100.0 | 140.0 |
| | Staaaf C | 2 | HOH-afstand p2 | 3.5(1) | | 75.8 | 80.0 | 81.8 |
| | Staaaf C | 3 | HOH-afstand p2 | 3.5(1) | | 75.8 | 80.0 | 81.8 |
| Bout (Flens) | Staaaf C | 3 | Eindafstand e1 | 3.5(1) | | 21.6 | 40.0 | |
| Bout (Plaat) | Staaaf C | 1 | Eindafstand e1 | 3.5(1) | | 21.6 | 70.0 | |
| | Staaaf C | 3 | Eindafstand e1 | 3.5(1) | | 21.6 | 60.0 | |
| Console | B-C | | Hoogte | | 6.2.6.7(2) | | 100.0 | 200.0 |
| Consoleflens | B-C | | Dikte | | frmb 5.3.a | 8.5 | 10.0 | |
| | B-C | | Las fl-fl Δ | | frmb 5.3.a | 10.3 | 11.0 | |
| | B-C | | Las fl-plt $\Delta\Delta$ | | 1.0*MplRd | 3.92 | 5.00 | |
| | B-C | | Las fl-plt $\Delta\Delta$ | | frmb 5.3.a | 2.58 | 5.00 | |
| Consolelijf | B-C | | Dikte | | frmb 5.3.a | 5.6 | 10.0 | |
| | B-C | | Las lijf-plt $\Delta\Delta$ | | 1.0*MplRd | 4.62 | 5.00 | |
| Kopplaat | Staaaf C | | Flenslas $\Delta\Delta$ | | 1.0*MplRd | 3.92 | 4.00 | |
| | Staaaf C | | Lijflas $\Delta\Delta$ | | 1.0*MplRd | 3.00 | 3.00 | |
| | Staaaf C | | Positie boven | | | 105.7 | 110.0 | |
| Schot AB | Staaaf B | | Dikte | | frmb 5.6.a | 4.7 | 10.0 | |
| | Staaaf B | | Lengte | | | 160.0 | 165.0 | 170.0 |
| | Staaaf B | | Lijflas $\Delta\Delta$ | | 1.0*MplRd | 3.05 | 5.00 | |

10 Liggers & kolommen

10.1 Dakliggers as 1&2

$L_{t;1} = 2.47$ m (dit is de systeemplengte, niet de daadwerkelijke lengte!!!)

Liggers tussen kolommen. Pui afsteunen tegen dakliggers.
→ hor. bel. op ligger

Belastinggeval 1 t.g.v. permanent
 $g_{k;dak}: 0.55 \cdot 1.0 = 0.55$ kN/m
Eigengewicht van de profielen wordt automatisch gegenereerd.

Belastinggeval 2 t.g.v. veranderlijk
 $Q_{k;water}: 1.0 \cdot 1.0 = 1.0$ kN/m

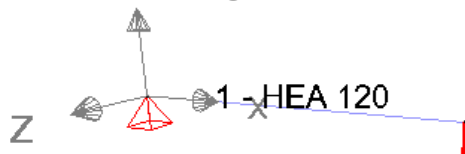
Belastinggeval 3 t.g.v. veranderlijk
 $Q_{k;wind}: = 3.17$ kN
(reactiekracht uit windverband, zie 7.1.2)

Belastinggeval 4 t.g.v. veranderlijk
 $Q_{wrep} = h \cdot p_w \cdot C_{dim} \cdot (C_{pe} + C_{pi}) = 1.36$ kN/m
 $(0.5 \cdot 3.3 + 0.5) \cdot 0.62 \cdot 0.93 \cdot 1.1$

| | |
|-----------------------|--------|
| Toepassen $L_{t;1}$: | HEA100 |
|-----------------------|--------|

10.1.1 Uitvoer

Geometrie voorstelling (mm)



Geometrie gegevens

Punten

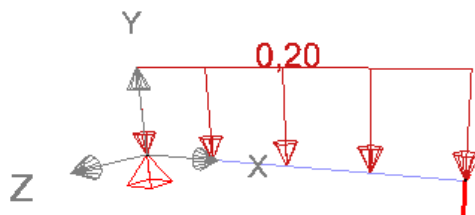
| punt | X (mm) | Y (mm) | Z (mm) | Ondersteuning (kN/m, kNm/Rad) | Naam van de verbinding |
|------|---------|--------|--------|-------------------------------|------------------------|
| 1 | 0,00 | 0,00 | 0,00 | kx;ky;kz | - |
| 2 | 2470,00 | 0,00 | 0,00 | ky;kz | - |

Staven

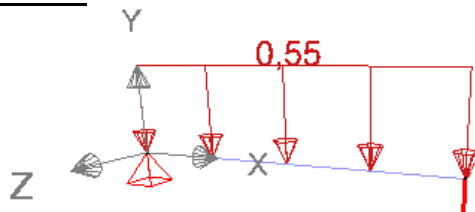
| s t a a f | b e i n d e k n o o p | d o r s n e d e | b e g i n d o r s n e d e k n o o p | e i n d o r s n e d e k n o o p | m a t e r i a l | l e n g t e (m m) | v o l u m e (m 3) | o r i e n t a t i e (°) | s t i j f h e i d b e g i n (k N / m , k N m / R a d) | s t i j f h e i d e i n d e (k N / m , k N m / R a d) | o n d e r t e u n i n g (k N / m , k N m / r a d / m) | K n i k l e n g t e o m y ' (u) (m m) | K n i k l e n g t e o m z ' (v) (m m) | K i p l e n g t e z > 0 (m m) | K i p l e n g t e z < 0 (m m) |
|-------------|-----------------------|-----------------|-------------------------------------|---------------------------------|-----------------|---------------------|---------------------|---------------------------|---|---|---|---|---|---------------------------------|---------------------------------|
| 1 | 1 | 2 | HEA 120 | 1 | 2 | Staal S235(1) | 24,70063 | 0,00 | stijf | stijf | - | 2470,28 | 2470,28 | [0,00mm - 2470,00mm] | [0,00mm - 2470,00mm] |
| t o t a a l | | | | | | 2470,00 | 0,0063 | | | | | | | | |

Voorstelling lasten (kN, kNm, mm, kN/m, kNm/m, kN/m²)

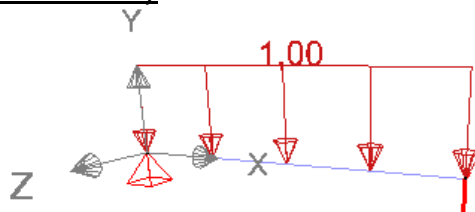
Eigengewicht



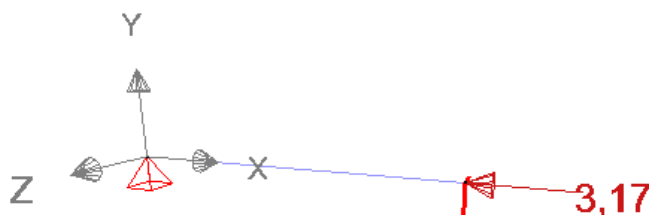
permanente lasten



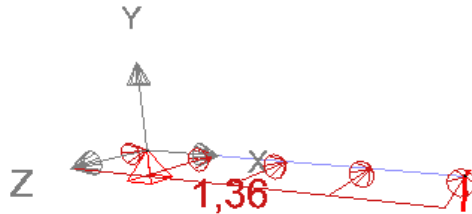
sneeuw (H <= 1000 m)



wind



wind



Gegevens lasten

Eigengewicht

Staven

| staaf | begin knoop last | einde knoop last | belastingstype | begin | einde | eenheid | afstand van het begin (mm) | afstand van het einde (mm) | orientatie |
|-------|------------------|------------------|----------------|-------|-------|---------|----------------------------|----------------------------|------------|
| 1 | 1 | 2 | Verdeelde last | 0,20 | 0,20 | kN/m | 0,00 | 0,00 | globaal Y |

permanente lasten

Staven

| staaf | begin knoop last | einde knoop last | belastingstype | begin | einde | eenheid | afstand van het begin (mm) | afstand van het einde (mm) | orientatie |
|-------|------------------|------------------|----------------|-------|-------|---------|----------------------------|----------------------------|------------|
| 1 | 1 | 2 | Verdeelde last | 0,55 | 0,55 | kN/m | 0,00 | 0,00 | globaal Y |

sneeuw (H <= 1000 m)

Staven

| staaf | begin knoop last | einde knoop last | belastingstype | begin | einde | eenheid | afstand van het begin (mm) | afstand van het einde (mm) | orientatie |
|-------|------------------|------------------|----------------|-------|-------|---------|----------------------------|----------------------------|------------|
| 1 | 1 | 2 | Verdeelde last | 1,00 | 1,00 | kN/m | 0,00 | 0,00 | globaal Y |

wind

Punten

| knoop | belastingstype | x waarde (mm,kN,kNm) | y waarde (mm,kN,kNm) | z waarde (mm,kN,kNm) |
|-------|----------------|----------------------|----------------------|----------------------|
| 2 | kracht | 3,17 | 0,00 | 0,00 |

wind

Staven

| staaf | begin knoop last | einde knoop last | belastingstype | begin | einde | eenheid | afstand van het begin (mm) | afstand van het einde (mm) | orientatie |
|-------|------------------|------------------|----------------|-------|-------|---------|----------------------------|----------------------------|------------|
| 1 | 1 | 2 | Verdeelde last | 1,36 | 1,36 | kN/m | 0,00 | 0,00 | globaal Z |

Lastengroepen

Belastingscoëfficiënten voor EN 1990(NL)

Klimaatklasse: 1

Gevolgklasse: 2

Ontwerplevensduur: 50 jaren

| Naam | yuls- | yuls+ | ysls- | ysls+ | ψ_0 | ψ_1 | ψ_2 | ξ | t 0 | kmod |
|----------------------|-------|-------|-------|-------|----------|----------|----------|-------|--------|---------------|
| Eigengewicht | 1,35 | 0,90 | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 | 0,89 | 0 | permanent |
| permanente lasten | 1,35 | 0,90 | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 | 0,89 | 0 | permanent |
| sneeuw (H <= 1000 m) | 1,50 | 0,00 | 1,00 | 0,00 | 0,00 | 0,20 | 0,00 | 1,00 | 0 | korte termijn |
| wind | 1,50 | 0,00 | 1,00 | 0,00 | 0,00 | 0,20 | 0,00 | 1,00 | 0 | korte termijn |
| wind | 1,50 | 0,00 | 1,00 | 0,00 | 0,00 | 0,20 | 0,00 | 1,00 | 0 | korte termijn |

Combinaties

uiterste grenstoestand - fundamentele combinatie

| | Naam | Eigengewicht | permanente lasten | sneeuw (H <= 1000 m) | wind | wind |
|---|-----------|--------------|-------------------|----------------------|-------------|-------------|
| 1 | UGT FC 1 | 1,00 x 1,20 | 1,00 x 1,20 | 1,00 x 1,50 | 0,00 | 0,00 |
| 2 | UGT FC 2 | 1,00 x 1,20 | 1,00 x 1,20 | 0,00 | 1,00 x 1,50 | 0,00 |
| 3 | UGT FC 3 | 1,00 x 1,20 | 1,00 x 1,20 | 0,00 | 0,00 | 1,00 x 1,50 |
| 4 | UGT FC 4 | 1,00 x 1,35 | 1,00 x 1,35 | 0,00 | 0,00 | 0,00 |
| 5 | UGT FC 13 | 1,00 x 0,90 | 1,00 x 0,90 | 1,00 x 1,50 | 0,00 | 0,00 |
| 6 | UGT FC 14 | 1,00 x 0,90 | 1,00 x 0,90 | 0,00 | 1,00 x 1,50 | 0,00 |
| 7 | UGT FC 15 | 1,00 x 0,90 | 1,00 x 0,90 | 0,00 | 0,00 | 1,00 x 1,50 |
| 8 | UGT FC 16 | 1,00 x 0,90 | 1,00 x 0,90 | 0,00 | 0,00 | 0,00 |

bruikbaarheidsgrenstoestand - zeldzame combinatie

| | Naam | Eigengewicht | permanente lasten | sneeuw (H <= 1000 m) | wind | wind |
|---|----------|--------------|-------------------|----------------------|-------------|-------------|
| 1 | BGT ZC 1 | 1,00 x 1,00 | 1,00 x 1,00 | 1,00 x 1,00 | 0,00 | 0,00 |
| 2 | BGT ZC 2 | 1,00 x 1,00 | 1,00 x 1,00 | 0,00 | 1,00 x 1,00 | 0,00 |
| 3 | BGT ZC 3 | 1,00 x 1,00 | 1,00 x 1,00 | 0,00 | 0,00 | 1,00 x 1,00 |
| 4 | BGT ZC 4 | 1,00 x 1,00 | 1,00 x 1,00 | 0,00 | 0,00 | 0,00 |

bruikbaarheidsgrenstoestand - frequente combinatie

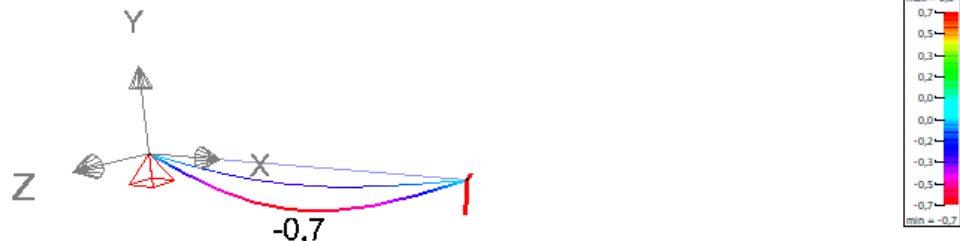
| | Naam | Eigengewicht | permanente lasten | sneeuw (H <= 1000 m) | wind | wind |
|---|----------|--------------|-------------------|----------------------|-------------|-------------|
| 1 | BGT FC 1 | 1,00 x 1,00 | 1,00 x 1,00 | 0,20 x 1,00 | 0,00 | 0,00 |
| 2 | BGT FC 2 | 1,00 x 1,00 | 1,00 x 1,00 | 0,00 | 0,20 x 1,00 | 0,00 |
| 3 | BGT FC 3 | 1,00 x 1,00 | 1,00 x 1,00 | 0,00 | 0,00 | 0,20 x 1,00 |
| 4 | BGT FC 4 | 1,00 x 1,00 | 1,00 x 1,00 | 0,00 | 0,00 | 0,00 |

bruikbaarheidsgrenstoestand - quasi-permanente combinatie

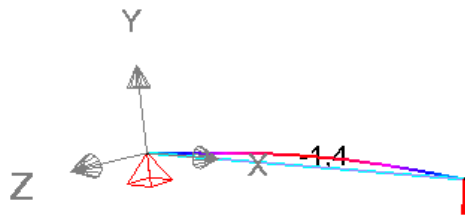
| | Naam | Eigengewicht | permanente lasten | sneeuw (H <= 1000 m) | wind | wind |
|---|----------|--------------|-------------------|----------------------|------|------|
| 1 | BGT QP 1 | 1,00 x 1,00 | 1,00 x 1,00 | 0,00 | 0,00 | 0,00 |

Voorstelling algemene resultaten

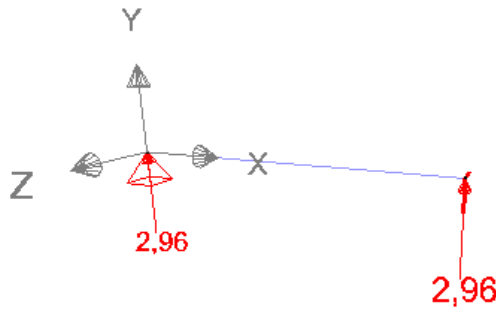
δ_y (mm) - BGT ZC Omhullende max



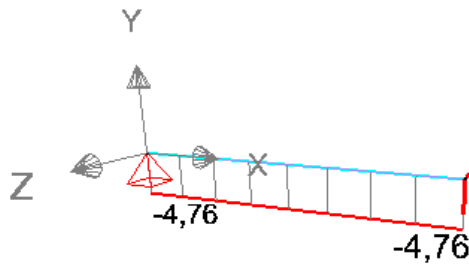
δ_z (mm) - BGT ZC Omhullende max



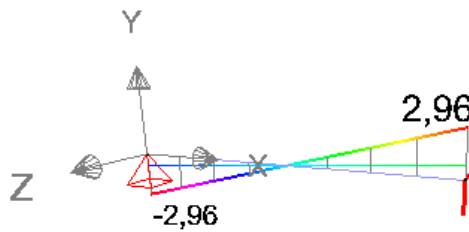
Reactie Ry op punt (kN) - UGT FC Omhullende



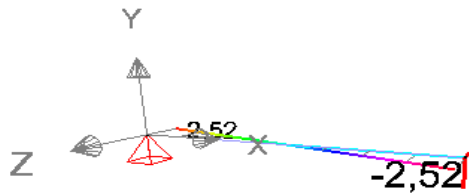
N in staaf (kN) - UGT FC Omhullende



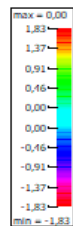
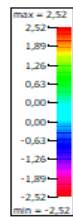
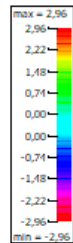
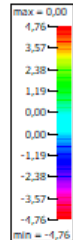
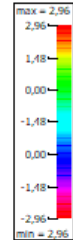
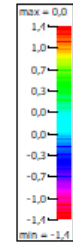
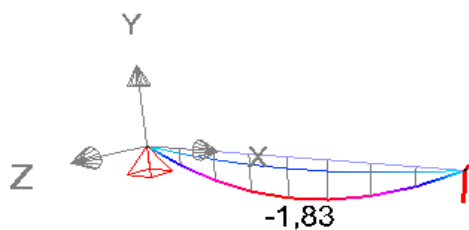
Vz in staaf (kN) - UGT FC Omhullende



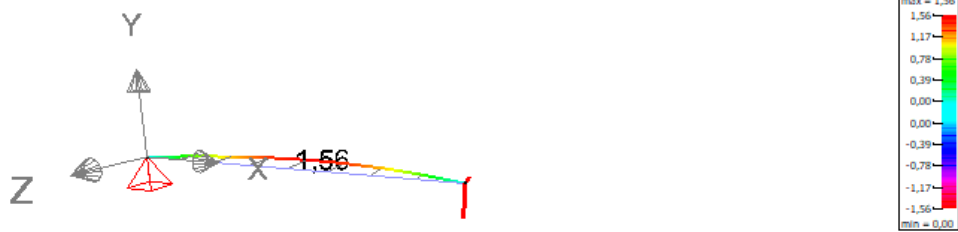
Vy in staaf (kN) - UGT FC Omhullende



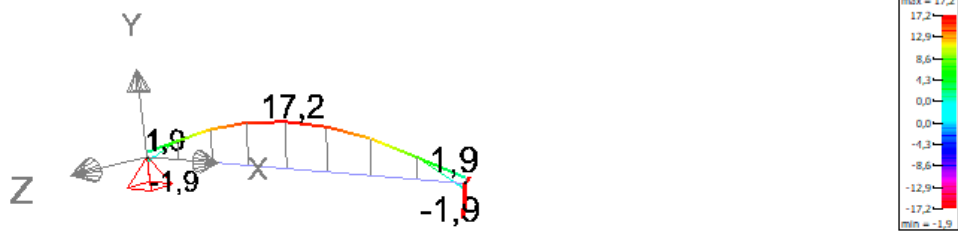
My in staaf (kNm) - UGT FC Omhullende



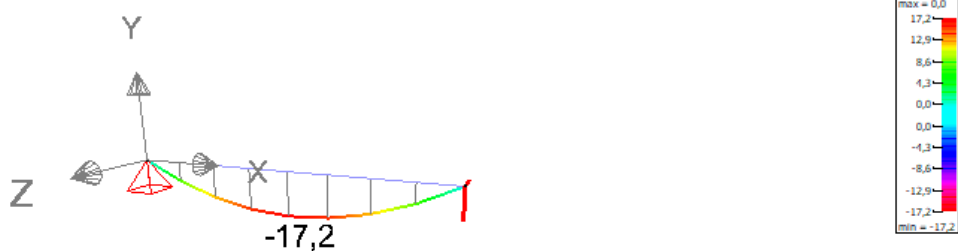
Mz in staaf (kNm) - UGT FC Omhullende



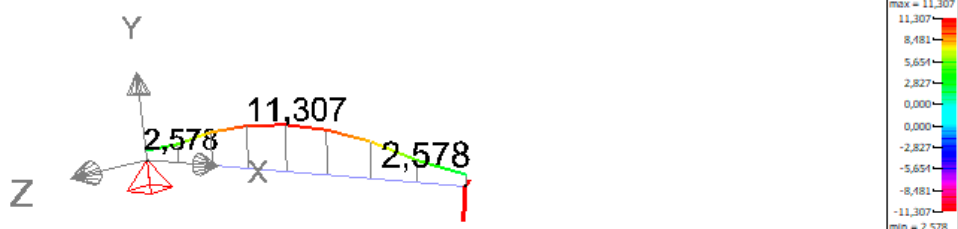
σ_c in staaf volgens sterke as (N/mm^2) - UGT FC Omhullende



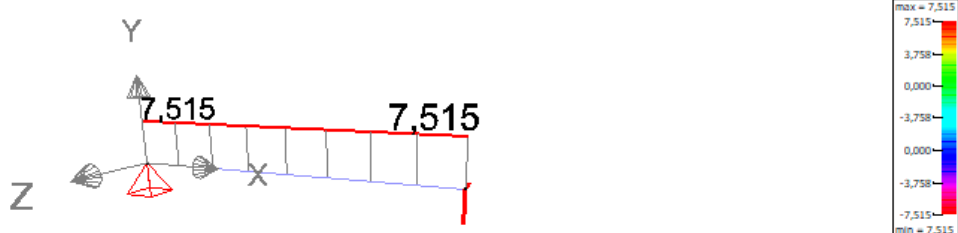
σ_t in staaf volgens sterke as (N/mm^2) - UGT FC Omhullende



Sterkte controle van staaf (%)



Stabiliteitscontrole van staaf (%)



Algemene resultaten

Doorbuiging staaf - BGT ZC Omhullende

| staaf nummer | Dx (mm) (min) | Dx (mm) (max) | Dy (mm) (min) | Dy (mm) (max) | Dz (mm) (min) | Dz (mm) (max) | φ_x (°) (min) | φ_x (°) (max) | φ_y (°) (min) | φ_y (°) (max) | φ_z (°) (min) | φ_z (°) (max) |
|--------------|---------------|---------------|---------------|---------------|---------------|---------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|
| 1 | 0,0 | 0,0 | -0,7 | 0,0 | -1,4 | 0,0 | 0,00 | 0,00 | -0,10 | 0,10 | -0,05 | 0,05 |

Reactie in punt - Eigengewicht

| punt nummer | reactie F_x (kN) | reactie F_y (kN) | reactie F_z (kN) | reactie M_x (kNm) | reactie M_y (kNm) | reactie M_z (kNm) |
|-------------|--------------------|--------------------|--------------------|---------------------|---------------------|---------------------|
| 1 | 0,00 | 0,24 | 0,00 | 0,00 | 0,00 | 0,00 |
| 2 | 0,00 | 0,24 | 0,00 | 0,00 | 0,00 | 0,00 |

Reactie in punt - permanente lasten

| punt nummer | reactie F_x (kN) | reactie F_y (kN) | reactie F_z (kN) | reactie M_x (kNm) | reactie M_y (kNm) | reactie M_z (kNm) |
|-------------|--------------------|--------------------|--------------------|---------------------|---------------------|---------------------|
| 1 | 0,00 | 0,68 | 0,00 | 0,00 | 0,00 | 0,00 |
| 2 | 0,00 | 0,68 | 0,00 | 0,00 | 0,00 | 0,00 |

Reactie in punt - sneeuw ($H \leq 1000$ m)

| punt nummer | reactie F_x (kN) | reactie F_y (kN) | reactie F_z (kN) | reactie M_x (kNm) | reactie M_y (kNm) | reactie M_z (kNm) |
|-------------|--------------------|--------------------|--------------------|---------------------|---------------------|---------------------|
| 1 | 0,00 | 1,24 | 0,00 | 0,00 | 0,00 | 0,00 |
| 2 | 0,00 | 1,24 | 0,00 | 0,00 | 0,00 | 0,00 |

Reactie in punt - wind

| punt nummer | reactie F_x (kN) | reactie F_y (kN) | reactie F_z (kN) | reactie M_x (kNm) | reactie M_y (kNm) | reactie M_z (kNm) |
|-------------|--------------------|--------------------|--------------------|---------------------|---------------------|---------------------|
| 1 | 3,17 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 |
| 2 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 |

Reactie in punt - wind (1)

| punt nummer | reactie F_x (kN) | reactie F_y (kN) | reactie F_z (kN) | reactie M_x (kNm) | reactie M_y (kNm) | reactie M_z (kNm) |
|-------------|--------------------|--------------------|--------------------|---------------------|---------------------|---------------------|
| 1 | 0,00 | 0,00 | 1,68 | 0,00 | 0,00 | 0,00 |
| 2 | 0,00 | 0,00 | 1,68 | 0,00 | 0,00 | 0,00 |

Reactie in punt - UGT FC Omhullende

| punt nummer (max) | reactie F_x (kN) (min) | reactie F_x (kN) (max) | reactie F_y (kN) (min) | reactie F_y (kN) (max) | reactie F_z (kN) (min) | reactie F_z (kN) (max) | reactie M_x (kNm) (min) | reactie M_x (kNm) (max) | reactie M_y (kNm) (min) | reactie M_y (kNm) (max) | reactie M_z (kNm) (min) | reactie M_z (kNm) (max) |
|-------------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 1 | 0,00 | 4,76 | 0,83 | 2,96 | 0,00 | 2,52 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 |
| 2 | 0,00 | 0,00 | 0,83 | 2,96 | 0,00 | 2,52 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 |

Controle van staven

| staaf nummer | Weerstand (%) | Stabiliteit (%) |
|--------------|----------------|-----------------|
| 1 | 2,578 ~ 11,307 | 7,515 |

Detail resultaten

Staal 1 - Weerstand- en knikcontroles

| positie | Weerstand (%) | Stabiliteit (%) |
|---------------------|----------------------|------------------------|
| 1 - 1 (0,00 mm) | 2,578 | 7,515 |
| 1 - 2 (308,75 mm) | 4,932 | 7,515 |
| 1 - 3 (308,75 mm) | 4,932 | 7,515 |
| 1 - 4 (617,50 mm) | 8,470 | 7,515 |
| 1 - 5 (617,50 mm) | 8,470 | 7,515 |
| 1 - 6 (926,25 mm) | 10,597 | 7,515 |
| 1 - 7 (926,25 mm) | 10,597 | 7,515 |
| 1 - 8 (1235,00 mm) | 11,307 | 7,515 |
| 1 - 9 (1235,00 mm) | 11,307 | 7,515 |
| 1 - 10 (1543,75 mm) | 10,597 | 7,515 |
| 1 - 11 (1543,75 mm) | 10,597 | 7,515 |
| 1 - 12 (1852,50 mm) | 8,470 | 7,515 |
| 1 - 13 (1852,50 mm) | 8,470 | 7,515 |
| 1 - 14 (2161,25 mm) | 4,932 | 7,515 |
| 1 - 15 (2161,25 mm) | 4,932 | 7,515 |
| 1 - 16 (2470,00 mm) | 2,578 | 7,515 |

10.2 Stalen vloerliggers as 1&2 tussenbordes

Toepassen: HEA140 praktisch (min HEA120)
prefab bordes verankeren/bevestigen op stalen liggers volgens fabrikant/leverancier

$L_t = 2.47$ m (dit is de systeemlengte, niet de daadwerkelijke lengte!!!)

Belastinggeval 1 t.g.v. permanente belasting

$g_{k;0-1430} = 5.0 \cdot 0.5 \cdot 3.15 = 7.88$ kN/m

$G_{k;1430} = 6.6 \cdot 0.5 \cdot 2.55 = 8.42$ kN

Belastinggeval 2 t.g.v. veranderlijke belasting

$q_{k;0-1430} = 2.5 \cdot 0.5 \cdot 3.15 = 3.94$ kN/m

$Q_{k;1430} = 3.3 \cdot 0.5 \cdot 2.55 = 4.21$ kN

10.2.1 Uitvoer

Technosoft Raamwerken release 6.73b

23 nov 2021

Dimensies....: kN;m;rad (tenzij anders aangegeven)

Belastingbreedte.: 1.000

Rekenmodel.....: 1e-orde-elastisch.

Theorie voor de bepaling van de krachtsverdeling:

Geometrisch lineair.

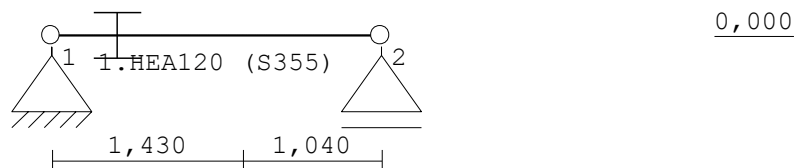
Fysisch lineair.

Gunstige werking van de permanente belasting wordt automatisch verwerkt.

Toegepaste normen volgens Eurocode met Nederlandse NB

| Belastingen | NEN-EN 1990:2002 | C2:2010,A1:2019 | NB:2019 (nl) |
|-------------|----------------------|-----------------|--------------|
| | NEN-EN 1991-1-1:2002 | C1/C11:2019 | NB:2019 (nl) |
| Staal | NEN-EN 1993-1-1:2006 | C2:2011,A1:2016 | NB:2016 (nl) |
| | NEN-EN 1993-1-8:2006 | C2:2009 | NB:2011 (nl) |

GEOMETRIE



STRAMIENLIJNEN

| Nr. | Naam | X | Z-min | Z-max |
|-----|------|-------|-------|-------|
| 1 | | 0.000 | 0.000 | 0.000 |
| 2 | | 1.430 | 0.000 | 0.000 |
| 3 | | 2.470 | 0.000 | 0.000 |

NIVEAUS

| Nr. | Z | X-min | X-max |
|-----|-------|-------|-------|
| 1 | 0.000 | 0.000 | 2.470 |

MATERIALEN

| Mt | Kwaliteit | E-modulus [N/mm ²] | S.G. | Pois. | Uitz. coëff |
|----|-----------|--------------------------------|------|-------|-------------|
| 1 | S355 | 210000 | 78.5 | 0.30 | 1.2000e-05 |

PROFIELEN [mm]

| Prof. | Omschrijving | Materiaal | Oppervlak | Traagheid | Vormf. |
|-------|--------------|-----------|------------|------------|--------|
| 1 | HEA120 | 1:S355 | 2.5340e+03 | 6.0600e+06 | 0.00 |

PROFIELEN vervolg [mm]

| Prof. | Staaftype | Breedte | Hoogte | e | Type | b1 | h1 | b2 | h2 |
|-------|-----------|---------|--------|------|------|----|----|----|----|
| 1 | 0:Normaal | 120 | 114 | 57.0 | | | | | |

PROFIELVORMEN [mm]

1 HEA120



KNOPEN

| Knoop | X | Z |
|-------|-------|-------|
| 1 | 0.000 | 0.000 |
| 2 | 2.470 | 0.000 |

STAVEN

| St. | ki | kj | Profiel | Aansl.i | Aansl.j | Lengte |
|------|----|----|----------|---------|---------|--------|
| Opm. | | | | | | |
| 1 | 1 | 2 | 1:HEA120 | NDM | NDM | 2.470 |

VASTE STEUNPUNTEN

| Nr. knoop | Kode | XZR 1=vast 0=vrij | Hoek |
|-----------|-------|-------------------|------|
| 1 | 1 110 | | 0.00 |
| 2 | 2 010 | | 0.00 |

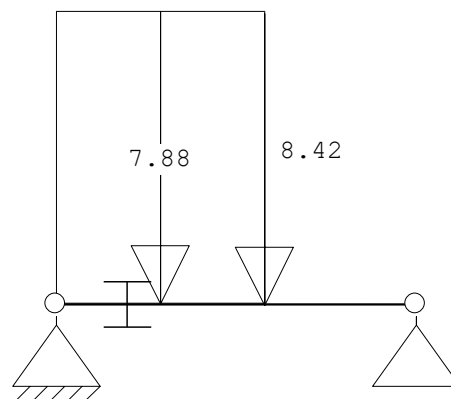
BELASTINGGEVALLEN

| B.G. | Omschrijving | Type |
|------|--------------------------------|-----------------------------|
| 1 | Permanente belasting EGZ=-1.00 | 1 |
| 2 | Veranderlijke belasting | 2 Ver. bel. pers. ed. (q_k) |

BELASTINGEN

B.G:1 Permanente belasting

Eigen gewicht van alle staven is meegenomen in berekening. Richting:↓

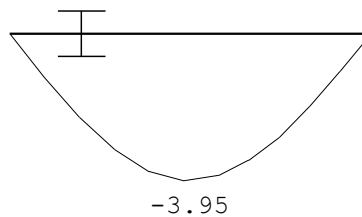


STAAFBELASTINGEN

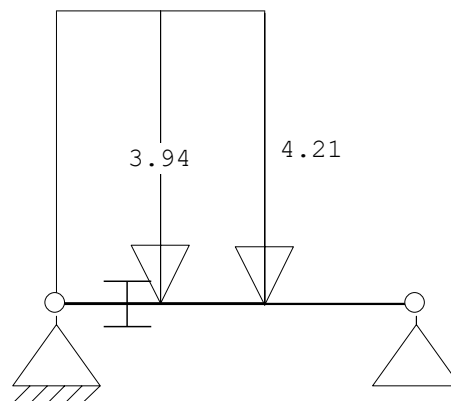
B.G:1 Permanente belasting

| StAAF | Type | q1/p/m | q2 | A | B | ψ_0 | ψ_1 | ψ_2 |
|-------|-------------|--------|-------|-------|-------|----------|----------|----------|
| 1 | 3:QZgeProj. | -7.88 | -7.88 | 0.000 | 1.040 | | | |
| 1 | 10:PZGproj. | -8.42 | | 1.430 | | | | |

VERPLAATSINGEN [mm] B.G:1 Permanente belasting



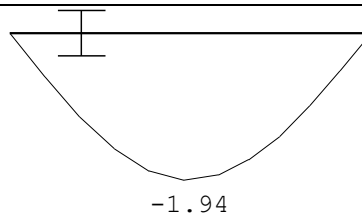
BELASTINGEN B.G:2 Veranderlijke belasting



STAAFBELASTINGEN B.G:2 Veranderlijke belasting

| Staf | Type | q1/p/m | q2 | A | B | ψ_0 | ψ_1 | ψ_2 |
|------|---------------|--------|-------|-------|-------|----------|----------|----------|
| 1 | 3:QZgeProj. | -3.94 | -3.94 | 0.000 | 1.040 | 0.40 | 0.70 | 0.60 |
| 1 | 10:PZGeproij. | -4.21 | | 1.430 | | 0.40 | 0.70 | 0.60 |

VERPLAATSINGEN [mm] B.G:2 Veranderlijke belasting



REACTIES

| Kn. | B.G. | X | Z | M |
|-----|------|------|-------|---|
| 1 | 1 | 0.00 | 11.80 | |
| 1 | 2 | 0.00 | 5.78 | |
| 2 | 1 | | 8.38 | |
| 2 | 2 | | 4.07 | |

BELASTINGCOMBINATIES

| BC | Type | BG | Gen. Factor | BG | Gen. Factor | BG | Gen. Factor | BG | Gen. Factor |
|----|-------|----|-------------|------|-------------|------|-------------|----|-------------|
| 1 | Fund. | 1 | Perm | 1.20 | 2 | Extr | 1.50 | | |
| 2 | Fund. | 1 | Perm | 1.35 | | | | | |
| 3 | Kar. | 1 | Perm | 1.00 | 2 | Extr | 1.00 | | |
| 4 | Kar. | 1 | Perm | 1.00 | | | | | |

GUNSTIGE WERKING PERMANENTE BELASTINGEN

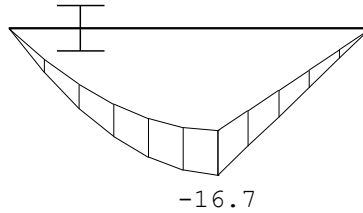
BC Staven met gunstige werking

- 1 Geen
2 Geen

OMHULLENDE VAN DE FUNDAMENTELE COMBINATIES

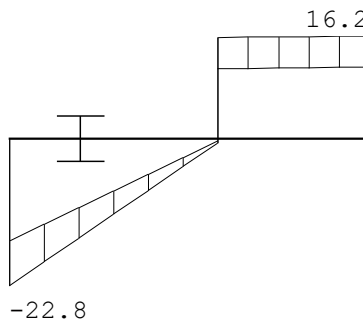
MOMENTEN

Fundamentele combinatie



DWARSKRACHTEN

Fundamentele combinatie



STAAFKRACHTEN

Fundamentele combinatie

| St. | Kn. | Pos. | NXi/NXj | | | DZi/DZj | | | MYi/MYj | | | | | |
|-----|-----|-------|---------|----|------|---------|--------|----|---------|----|--------|----|--------|----|
| | | | Min | BC | Max | BC | Min | BC | Max | BC | Min | BC | Max | BC |
| 1 | 1 | | 0.00 | 1 | 0.00 | 1 | -22.82 | 1 | -15.93 | 2 | 0.00 | 1 | 0.00 | 2 |
| 1 | | 1.430 | 0.00 | 1 | 0.00 | 1 | -0.51 | 1 | -0.33 | 2 | -16.68 | 1 | -11.62 | 2 |
| 1 | | 1.430 | 0.00 | 1 | 0.00 | 1 | 11.04 | 1 | 15.91 | 2 | -16.68 | 1 | -11.62 | 2 |
| 1 | 2 | | 0.00 | 1 | 0.00 | 1 | 11.32 | 2 | 16.16 | 1 | -0.00 | 1 | -0.00 | 2 |

REACTIES

Fundamentele combinatie

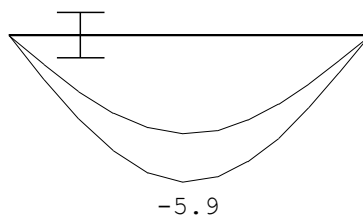
| Kn. | X-min | X-max | Z-min | Z-max | M-min | M-max |
|-----|-------|-------|-------|-------|-------|-------|
| 1 | 0.00 | 0.00 | 15.93 | 22.82 | | |
| 2 | | | 11.32 | 16.16 | | |

OMHULLENDE VAN DE KARAKTERISTIEKE COMBINATIES

VERPLAATSINGEN

[mm]

Karakteristieke combinatie



REACTIES

Karakteristieke combinatie

| Kn. | X-min | X-max | Z-min | Z-max | M-min | M-max |
|-----|-------|-------|-------|-------|-------|-------|
| 1 | 0.00 | 0.00 | 11.80 | 17.57 | | |
| 2 | | | 8.38 | 12.45 | | |

STAALPROFIELEN - ALGEMENE GEGEVENS

Stabiliteit: Classificatie gehele constructie: Geschoord

PROFIEL/MATERIAAL

| P/M nr. | Profielnaam | Vloeisp. [N/mm ²] | Productie methode | Min. drsn. klasse |
|---------|-------------|-------------------------------|-------------------|-------------------|
| 1 | HEA120 | 355 | Gewalst | 1 |

Partiële veiligheidsfactoren:

Gamma M;0 : 1.00 Gamma M;1 : 1.00

KNIKSTABILITEIT

| Staafl | l _{sys} [m] | Classif. y sterke as | l _{knik;y} [m] | Extra | | Extra | |
|--------|----------------------|----------------------|-------------------------|--------------|----------------------|-------------------------|--------------|
| | | | | aanp. y [kN] | Classif. z zwakke as | l _{knik;z} [m] | aanp. z [kN] |
| 1 | 2.470 | Geschoord | 2.470 | 0.0 | Geschoord | 2.470 | 0.0 |

KIPSTABILITEIT

| Staafl | Plts. aangr. | l gaffel | Kipsteunafstanden | |
|--------|--------------|----------|-------------------|------|
| | | | [m] | [m] |
| 1 | 1.0*h | boven: | 2.47 | 2,47 |
| | | | 2.47 | 2,47 |

TOETSING SPANNINGEN

| Staafl nr. | P/M | BC | Sit | Kl | Plaats | Norm | Artikel | Formule | Hoogste toetsing U.C. [N/mm ²] | Opmerkingen |
|------------|-----|----|-----|----|--------|---------|---------|---------|--|-------------|
| 1 | 1 | 1 | 1 | 1 | Staafl | EN3-1-1 | 6.3.2 | (6.54) | 0.469 167 | 46 |

Opmerkingen:

[46] T.b.v. kip is een equivalente Q-last berekend.

TOETSING DOORBUIGING

| Staafl | Soort | Mtg | Lengte [m] | Overst | | Zeeg [mm] | u _{tot} [mm] | BC | Sit | u [mm] | Toelaatbaar | |
|--------|-------|-----|------------|--------|---|-----------|-----------------------|----|--------|--------|-------------|-------|
| | | | | I | J | | | | | | [mm] | *1 |
| 1 | Vlr+w | db | 2.47 | N | N | 0.0 | -5.9 | 3 | 1 Eind | -5.9 | ±9.9 | 0.004 |

10.3 Stalen vloerliggers as 1&2 bovenbordes

Toepassen: HEA140 praktisch (min HEA120)
prefab bordes verankeren/bevestigen op stalen liggers volgens fabrikant/leverancier

$L_t = 2.47$ m (dit is de systeemlengte, niet de daadwerkelijke lengte!!!)

Belastinggeval 1 t.g.v. permanente belasting

$g_{k;1145-2470} = 5.0 \cdot 0.5 \cdot 3.15 = 7.88$ kN/m

$G_{k;1145} = 6.6 \cdot 0.5 \cdot 2.55 = 8.42$ kN

Belastinggeval 2 t.g.v. veranderlijke belasting

$q_{k;1145-2470} = 2.5 \cdot 0.5 \cdot 3.15 = 3.94$ kN/m

$Q_{k;1145} = 3.3 \cdot 0.5 \cdot 2.55 = 4.21$ kN

10.3.1 Uitvoer

Technosoft Raamwerken release 6.73b

23 nov 2021

Dimensies....: kN;m;rad (tenzij anders aangegeven)

Belastingbreedte.: 1.000

Rekenmodel.....: 1e-orde-elastisch.

Theorie voor de bepaling van de krachtsverdeling:

Geometrisch lineair.

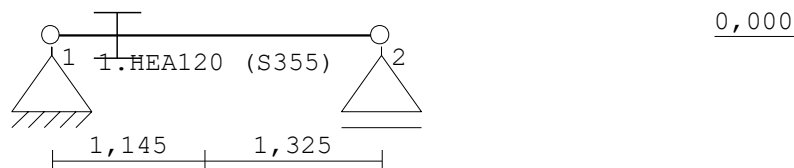
Fysisch lineair.

Gunstige werking van de permanente belasting wordt automatisch verwerkt.

Toegepaste normen volgens Eurocode met Nederlandse NB

| | | | |
|-------------|----------------------|-----------------|--------------|
| Belastingen | NEN-EN 1990:2002 | C2:2010,A1:2019 | NB:2019 (nl) |
| | NEN-EN 1991-1-1:2002 | C1/C11:2019 | NB:2019 (nl) |
| Staal | NEN-EN 1993-1-1:2006 | C2:2011,A1:2016 | NB:2016 (nl) |
| | NEN-EN 1993-1-8:2006 | C2:2009 | NB:2011 (nl) |

GEOMETRIE



STRAMIENLIJNEN

| Nr. | Naam | X | Z-min | Z-max |
|-----|------|-------|-------|-------|
| 1 | | 0.000 | 0.000 | 0.000 |
| 2 | | 1.145 | 0.000 | 0.000 |
| 3 | | 2.470 | 0.000 | 0.000 |

NIVEAUS

| Nr. | Z | X-min | X-max |
|-----|-------|-------|-------|
| 1 | 0.000 | 0.000 | 2.470 |

MATERIALEN

| Mt | Kwaliteit | E-modulus [N/mm ²] | S.G. | Pois. | Uitz. coëff |
|----|-----------|--------------------------------|------|-------|-------------|
| 1 | S355 | 210000 | 78.5 | 0.30 | 1.2000e-05 |

PROFIELEN [mm]

| Prof. | Omschrijving | Materiaal | Oppervlak | Traagheid | Vormf. |
|-------|--------------|-----------|------------|------------|--------|
| 1 | HEA120 | 1:S355 | 2.5340e+03 | 6.0600e+06 | 0.00 |

PROFIELEN vervolg [mm]

| Prof. | Staaftype | Breedte | Hoogte | e | Type | b1 | h1 | b2 | h2 |
|-------|-----------|---------|--------|------|------|----|----|----|----|
| 1 | 0:Normaal | 120 | 114 | 57.0 | | | | | |

PROFIELVORMEN [mm]

1 HEA120



KNOPEN

| Knoop | X | Z |
|-------|-------|-------|
| 1 | 0.000 | 0.000 |
| 2 | 2.470 | 0.000 |

STAVEN

| St. | ki | kj | Profiel | Aansl.i | Aansl.j | Lengte |
|------|----|----|----------|---------|---------|--------|
| Opm. | | | | | | |
| 1 | 1 | 2 | 1:HEA120 | NDM | NDM | 2.470 |

VASTE STEUNPUNTEN

| Nr. knoop | Kode | XZR 1=vast 0=vrij | Hoek |
|-----------|-------|-------------------|------|
| 1 | 1 110 | | 0.00 |
| 2 | 2 010 | | 0.00 |

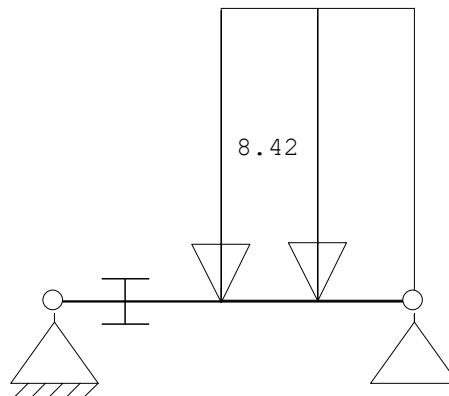
BELASTINGGEVALLEN

| B.G. | Omschrijving | Type |
|------|-------------------------|-----------------------------|
| 1 | Permanente belasting | EGZ=-1.00 1 |
| 2 | Veranderlijke belasting | 2 Ver. bel. pers. ed. (q_k) |

BELASTINGEN

B.G:1 Permanente belasting

Eigen gewicht van alle staven is meegenomen in berekening. Richting:↓

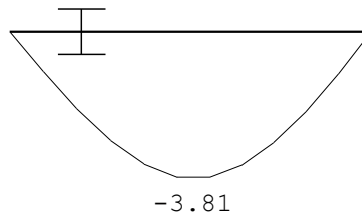


STAAFBELASTINGEN

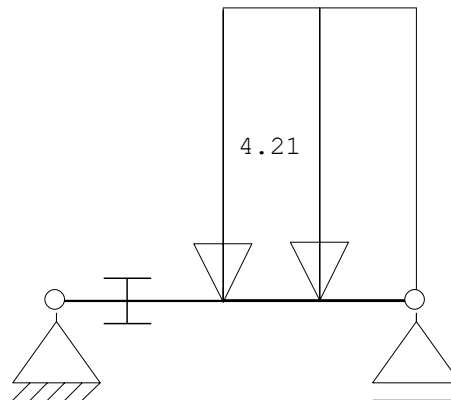
B.G:1 Permanente belasting

| Staat | Type | q1/p/m | q2 | A | B | ψ_0 | ψ_1 | ψ_2 |
|-------|-------------|--------|-------|-------|-------|----------|----------|----------|
| 1 | 3:QZgeProj. | -7.88 | -7.88 | 1.145 | 0.000 | | | |
| 1 | 10:PZGproj. | -8.42 | | 1.145 | | | | |

VERPLAATSINGEN [mm] B.G:1 Permanente belasting



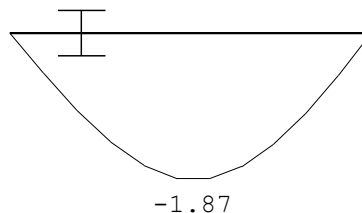
BELASTINGEN B.G:2 Veranderlijke belasting



STAAFBELASTINGEN B.G:2 Veranderlijke belasting

| Staaftype | Type | q1/p/m | q2 | A | B | ψ_0 | ψ_1 | ψ_2 |
|-----------|---------------|--------|-------|-------|-------|----------|----------|----------|
| 1 | 3:QZgeProj. | -3.94 | -3.94 | 1.145 | 0.000 | 0.40 | 0.70 | 0.60 |
| 1 | 10:PZGeproij. | -4.21 | | 1.145 | | 0.40 | 0.70 | 0.60 |

VERPLAATSINGEN [mm] B.G:2 Veranderlijke belasting



REACTIES

| Kn. | B.G. | X | Z | M |
|-----|------|------|-------|---|
| 1 | 1 | 0.00 | 7.56 | |
| 1 | 2 | 0.00 | 3.66 | |
| 2 | 1 | | 11.79 | |
| 2 | 2 | | 5.77 | |

BELASTINGCOMBINATIES

| BC | Type | BG | Gen. | Factor | BG | Gen. | Factor | BG | Gen. | Factor | BG | Gen. | Factor |
|----|-------|----|------|--------|----|------|--------|----|------|--------|----|------|--------|
| 1 | Fund. | 1 | Perm | 1.20 | 2 | Extr | 1.50 | | | | | | |
| 2 | Fund. | 1 | Perm | 1.35 | | | | | | | | | |
| 3 | Kar. | 1 | Perm | 1.00 | 2 | Extr | 1.00 | | | | | | |
| 4 | Kar. | 1 | Perm | 1.00 | | | | | | | | | |

GUNSTIGE WERKING PERMANENTE BELASTINGEN

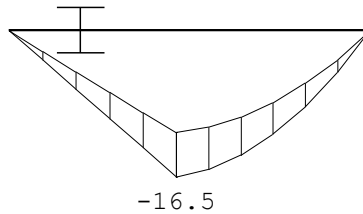
BC Staven met gunstige werking

- 1 Geen
- 2 Geen

OMHULLENDE VAN DE FUNDAMENTELE COMBINATIES

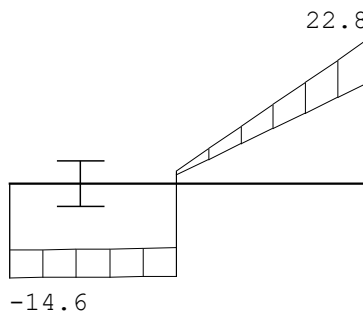
MOMENTEN

Fundamentele combinatie



DWARSKRACHTEN

Fundamentele combinatie



STAAFKRACHTEN

Fundamentele combinatie

| St. | Kn. | Pos. | NXi/NXj | | DZi/DZj | | | | MYi/MYj | | | | | |
|-----|-------|------|---------|--------|---------|--------|--------|--------|---------|--------|--------|---|--------|---|
| | | | Min BC | Max BC | Min BC | Max BC | Min BC | Max BC | Min BC | Max BC | | | | |
| 1 | 1 | | 0.00 | 1 | 0.00 | 1 | -14.56 | 1 | -10.21 | 2 | 0.00 | 1 | 0.00 | 2 |
| 1 | 1.145 | | 0.00 | 1 | 0.00 | 1 | -14.29 | 1 | -9.90 | 2 | -16.52 | 1 | -11.51 | 2 |
| 1 | 1.145 | | 0.00 | 1 | 0.00 | 1 | 1.46 | 1 | 2.13 | 2 | -16.52 | 1 | -11.51 | 2 |
| 1 | 2 | | 0.00 | 1 | 0.00 | 1 | 15.92 | 2 | 22.81 | 1 | -0.00 | 1 | -0.00 | 2 |

REACTIES

Fundamentele combinatie

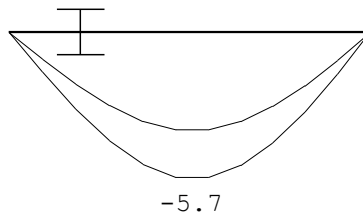
| Kn. | X-min | X-max | Z-min | Z-max | M-min | M-max |
|-----|-------|-------|-------|-------|-------|-------|
| 1 | 0.00 | 0.00 | 10.21 | 14.56 | | |
| 2 | | | 15.92 | 22.81 | | |

OMHULLENDE VAN DE KARAKTERISTIEKE COMBINATIES

VERPLAATSINGEN

[mm]

Karakteristieke combinatie



REACTIES

Karakteristieke combinatie

| Kn. | X-min | X-max | Z-min | Z-max | M-min | M-max |
|-----|-------|-------|-------|-------|-------|-------|
| 1 | 0.00 | 0.00 | 7.56 | 11.22 | | |
| 2 | | | 11.79 | 17.56 | | |

STAALPROFIELEN - ALGEMENE GEGEVENS

Stabiliteit: Classificatie gehele constructie: Geschoord

PROFIEL/MATERIAAL

| P/M nr. | Profielnaam | Vloeisp. [N/mm ²] | Productie methode | Min. drsn. klasse |
|---------|-------------|-------------------------------|-------------------|-------------------|
| 1 | HEA120 | 355 | Gewalst | 1 |

Partiële veiligheidsfactoren:
Gamma M;0 : 1.00 Gamma M;1 : 1.00

KNIKSTABILITEIT

| Staafl | l _{sys} [m] | Classif. y sterke as | l _{knik;y} [m] | Extra | | Extra | |
|--------|----------------------|----------------------|-------------------------|--------------|----------------------|-------------------------|--------------|
| | | | | aanp. y [kN] | Classif. z zwakke as | l _{knik;z} [m] | aanp. z [kN] |
| 1 | 2.470 | Geschoord | 2.470 | 0.0 | Geschoord | 2.470 | 0.0 |

KIPSTABILITEIT

| Staafl | Plts. aangr. | l gaffel | Kipsteunafstanden | |
|--------|--------------|----------|-------------------|------|
| | | | [m] | [m] |
| 1 | 1.0*h | boven: | 2.47 | 2,47 |
| | | onder: | 2.47 | 2,47 |

TOETSING SPANNINGEN

| Staafl nr. | P/M | BC | Sit | Kl | Plaats | Norm | Artikel | Formule | Hoogste toetsing U.C. [N/mm ²] | Opm. |
|------------|-----|----|-----|----|--------|---------|---------|---------|--|------|
| 1 | 1 | 1 | 1 | 1 | Staafl | EN3-1-1 | 6.3.2 | (6.54) | 0.465 165 | 46 |

Opmerkingen:
[46] T.b.v. kip is een equivalente Q-last berekend.

TOETSING DOORBUIGING

| Staafl | Soort | Mtg | Lengte [m] | Overst I | Zeeg J | u _{tot} [mm] | BC | Sit | u [mm] | Toelaatbaar [mm] | *1 |
|--------|-------|-----|------------|----------|--------|-----------------------|------|-----|--------|------------------|------------|
| 1 | Vlr+w | db | 2.47 | N | N | 0.0 | -5.7 | 3 | 1 Eind | -5.7 | ±9.9 0.004 |

11 Fundering

Poeren en stroken vorstvrij aanleggen op vaste grondslag c.q. grondverbetering met een minimale conuswaarde van 5 N/mm².

Onder gehele fundering bouwfolie aanbrengen

Funderingsstroken ongewapend uitvoeren, tenzij anders aangegeven

Aanlegdiepte fundering minimaal 800 mm –P (vorstvrij)

Funderingsstroken:

| | |
|--|--|
| Stroken t.p.v. gevelopeningen / verticale verbanden: | b=400mm onder+bovenwapening 3Ø12 |
| Overige situaties: | stroken d = 300 mm ongewapend uitvoeren |

Fundering volgens geotechnisch onderzoek en funderingsadvies van Geonius Geotechniek met documentnummer GA180122.R01.v1.0 en datum 14 september 2018.

11.1 Keuze funderingstype

Volgens het funderingsadvies is een fundering op staal mogelijk. Hierbij is grondverbetering noodzakelijk. Enige zettingen dienen geaccepteerd te worden.

11.2 Minimaal vereiste ontgravingsniveaus en bouwpeilhoogte

Tabel 5.1: te hanteren niveaus voor de fundering in fase A

| Sondering nr. | Maaiveldhoogte [m t.o.v. NAP] | Bouwpeilhoogte [m t.o.v. NAP] | Aanlegniveau [m t.o.v. NAP] | Minimaal ontgravingsniveau [m t.o.v. NAP] |
|---------------|-------------------------------|-------------------------------|-----------------------------|---|
| Kantoordeel | | | | |
| SW01 | 32,44 | 32,50 | 31,70 | 30,75 |
| SW02 | 32,62 | 32,50 | 31,70 | 31,20 |
| SW03 | 32,65 | 32,50 | 31,70 | 31,20 |
| SW04 | 32,59 | 32,50 | 31,70 | 31,20 |
| SW05 | 32,61 | 32,50 | 31,70 | 30,70 |
| SW06 | 32,51 | 32,50 | 31,70 | 30,70 |
| Hal | | | | |
| SW07 | 32,44 | 32,50 | 31,70 | 31,25 |
| SW08 | 32,41 | 32,50 | 31,70 | 31,00 |
| SW09 | 32,64 | 32,50 | 31,70 | 31,70 |
| SW10 | 32,68 | 32,50 | 31,70 | 31,70 |
| SW11 | 32,71 | 32,50 | 31,70 | 31,70 |
| SW12 | 32,78 | 32,50 | 31,70 | 31,70 |
| SW13 | 32,77 | 32,50 | 31,70 | 31,70 |
| SW14 | 32,71 | 32,50 | 31,70 | 30,00* |
| SW15 | 32,32 | 32,50 | 31,70 | 31,70 |

*zie 5.1 Algemeen

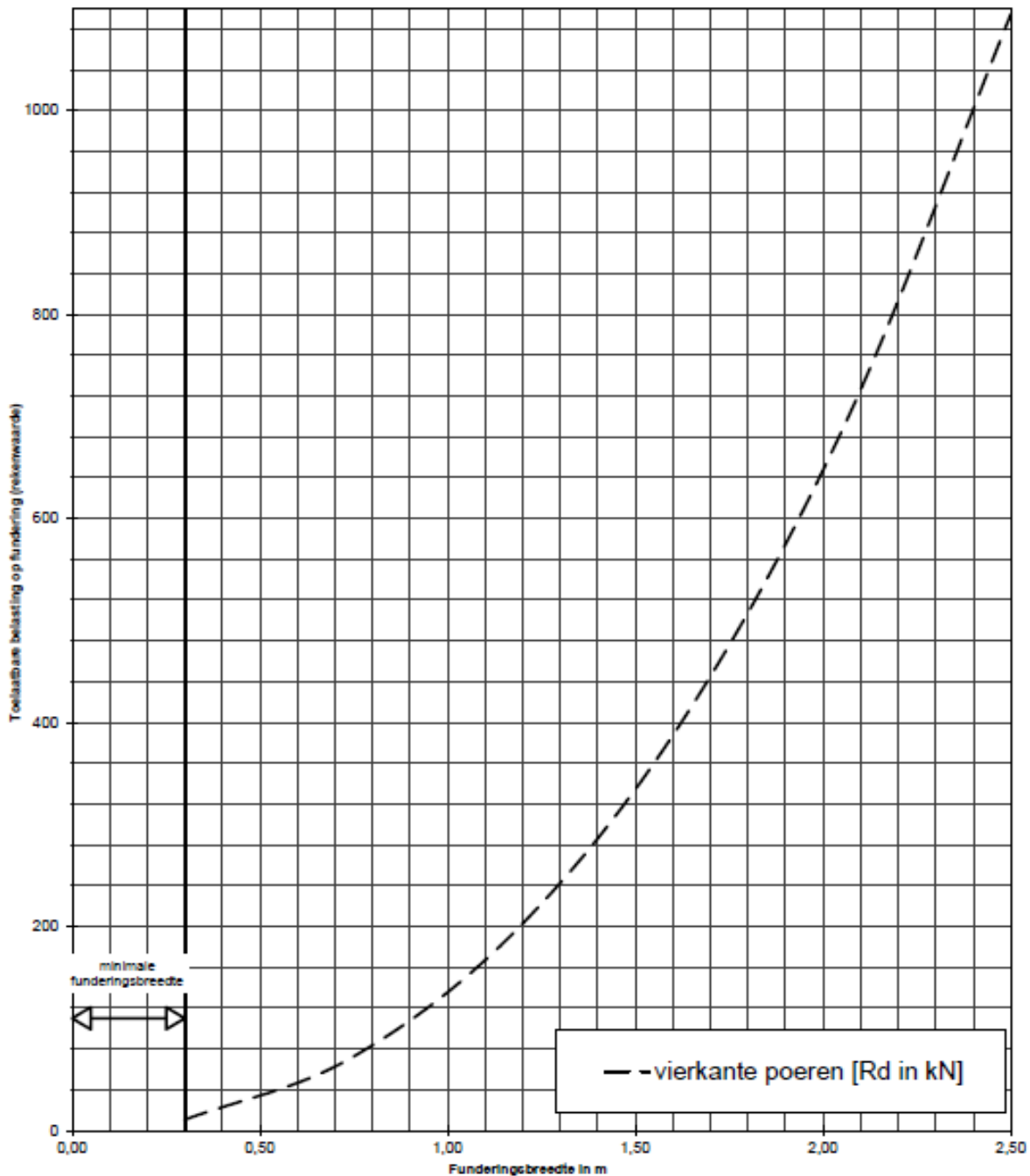
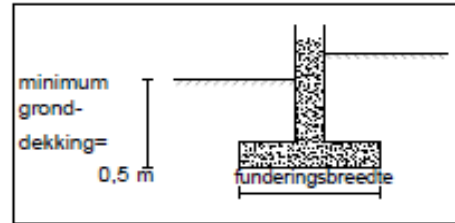
Tabel 5.2: te hanteren niveaus voor de fundering in fase C

| Sondering nr. | Maaiveldhoogte [m t.o.v. NAP] | Bouwpeilhoogte [m t.o.v. NAP] | Aanlegniveau [m t.o.v. NAP] | Minimaal ontgravingsniveau [m t.o.v. NAP] |
|---------------|-------------------------------|-------------------------------|-----------------------------|---|
| SW16 | 32,4 | 32,75 | 31,95 | 31,25 |
| SW17 | 32,4 | 32,75 | 31,95 | 31,60 |
| SW18 | 32,41 | 32,75 | 31,95 | 31,75 |
| SW19 | 32,48 | 32,75 | 31,95 | 31,45 |
| SW20 | 32,55 | 32,75 | 31,95 | 31,95 |
| SW21 | 32,44 | 32,75 | 31,95 | 31,60 |
| SW22 | 32,62 | 32,75 | 31,95 | 31,60 |
| SW23 | 32,55 | 32,75 | 31,95 | 31,95 |

11.3 Draagkracht

Rekenwaarde voor de maximaal toelaatbare belasting volgens NEN 9997-1:2016 bij verticaal centrisch belaste funderingen

Bijlagenr. : GA180122
Project : Nieuwbouw bedrijfspanden Comi Holding
Locatie : Manganstraat/Bronsstraat Weert
Grondsoort : Zand/klei
Volumiek gewicht : 11,0 kN/m³
Hoek inw. wrijving : 27,0 graden
Cohesie : 0,0 kN/m²



11.4 Zakkingen in de gebruikssituatie en beddingsconstante

Uitgaande van een zorgvuldig uitgevoerde grondverbetering, kunnen door zettingen van de onderliggende samendrukbare lagen, in de bruikbaarheidsgrenstoestand eindzakkingen van de funderingselementen optreden. De zettingsverschillen bedragen ca. 50%.

Tabel 5.4: Maximale geschatte verwachte zettingen ter plekke van de bouwblokken

| Bouwblok | Bouwpeilhoogte [m t.o.v. NAP] | Aanlegniveau [m t.o.v. NAP] | Zetting [mm] | Beddingsconstante (Poeren) [MN/m ³] |
|----------------|----------------------------------|--------------------------------|-----------------|---|
| Fase A kantoor | 32,50 | 31,70 | 30-35 | 3,0 |
| Fase A hallen | 32,50 | 31,70 | 10-15 | 6,0 |
| Fase B | 32,85 | 32,05 | 15-20 | 5,0 |
| Fase C | 32,75 | 31,95 | 25-30 | 3,0 |

11.5 Uitvoering

De ontgravingsniveaus dienen nauwgezet te worden geïnspecteerd op geroerde en/of verweekte zones. In geval van twijfel omtrent het aan te houden niveau kunt u contact opnemen met het geotechnisch adviesbureau.

Op het ontgravingsniveau voor de fundering kan siltig materiaal worden aangetroffen. Over het algemeen is dergelijk materiaal sterk gevoelig voor verweking. Een dergelijke verweking dient tijdens de uitvoering voorkomen te worden door het zo nodig afdekken van de ontgravingsniveaus en het zo spoedig mogelijk storten van werkvloeren en fundamenten.

Aanbevolen wordt om voor aanvang van het grondwerk de actuele grondwaterstand te controleren. Afhankelijk van de op dat moment heersende grondwaterstand kan tijdens de uitvoering een bemaling nodig zijn. Omtrent de inrichting van een eventuele bemaling kan het geotechnisch adviesbureau u desgewenst nader informeren.

Alle ontgravingsvlakken moeten, indien deze althans niet teveel leem en/of klei bevatten, zorgvuldig in droge toestand worden afgetrild. Zodoende worden ontgravingsverstoringen teniet gedaan en wordt een zo optimaal mogelijke funderingsgrondslag verkregen.

Voor algemene richtlijnen voor de uitvoering van ontgravingen en grondverbeteringen voor staalfunderingen wordt verwezen naar het funderingsadvies.

11.6 Grondwaterstand

11.6.1 Handboring bij grondonderzoek

Tijdens de uitvoering van het grondonderzoek is in de boor- en sondeergaten naar de actuele grondwaterstand gepeild. Deze werd niet aangetroffen tot een diepte van 1,6 tot 3,1 m- maaiveld. Deze opname is éénmalig en slechts bedoeld als een oriënterend gegeven.

11.7 Aanlegbreedte funderingsstroken

Funderingsstrook 1 (wand trap-tochtsluis)

| | | | | |
|---------------------------|---|---|---|-------------|
| Q _d ; plat dak | = | $0.5 \cdot 1.75 \cdot (0.65 \cdot 1.20 + 2.0 \cdot 1.50)$ | = | 3.31 kN/m |
| Q _d ; m.w. | = | $2.0 \cdot 3.30 \cdot 1.2$ | = | 7.92 kN/m + |
| Q _d ; totaal | = | | = | 11.23 kN/m |

B = 500 mm

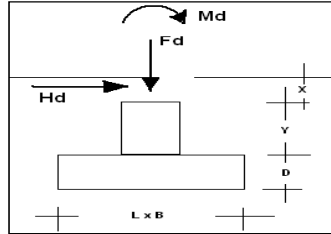
Ter plaatse van grote gevelopeningen #Ø8-150 onder + #Ø8-150 boven

11.8 Poeren as A

Toepassen: $L*B*D = 0.90*0.90*0.5$ m #Ø8-150 onder & boven

Poeren berekening

| Geometrie en belastingen | |
|--------------------------|----------|
| Fd = | 47,77 kN |
| Hd = | 5,48 kN |
| Md = | 4,68 kNm |
| x = | 0,50 m |
| y = | 0,00 m |
| L = | 0,90 m |
| B = | 0,90 m |
| D = | 0,50 m |



| Extra verticale belastingen $\gamma=1.0$ | | excentr. |
|--|---------|----------|
| F1 t.g.v. diverse | 0,00 kN | 0,00 m |
| F2 t.g.v. diverse | 0,00 kN | 0,00 m |
| F3 t.g.v. diverse | 0,00 kN | 0,00 m |
| F4 t.g.v. diverse | 0,00 kN | 0,00 m |
| F5 t.g.v. diverse | 0,00 kN | 0,00 m |

| Algemene gegevens | | | |
|-------------------|-------|-------------------------|--------------------------------|
| ρ | grond | 16,50 kN/m ³ | Betonkwaliteit: B 25 |
| ρ | beton | 24,00 kN/m ³ | Staalkwaliteit: FeB 500 |
| Dikte vloer: | | 0,12 m | Veiligheid tegen glijden: 1,3 |
| σ | grond | 150 kN/m ² | Beddingsconst.: 10000 |
| φ | grond | 33,00 ° | Factor passieve gronddruk: 1,0 |

Percentage oppervlak vloer t.o.v. oppervlak poer: 1,00

| Totale belastingen | | | | | |
|--------------------|--------|-------------|-----------------|-----------|-----------------|
| Fd | t.g.v. | kolom | 47,77 kN | Md | 7,42 kNm |
| | t.g.v. | poer | 11,66 kN | | |
| | t.g.v. | grond | 6,09 kN | | |
| | t.g.v. | bedrijfsvl. | 2,80 kN | | |
| | t.g.v. | F1 | 0,00 kN | 0,00 kNm | |
| | t.g.v. | F2 | 0,00 kN | 0,00 kNm | |
| | t.g.v. | F3 | 0,00 kN | 0,00 kNm | |
| | t.g.v. | F4 | 0,00 kN | 0,00 kNm | |
| | t.g.v. | F5 | 0,00 kN | 0,00 kNm | |
| | | Fd | 68,33 kN | Md | 7,42 kNm |

Optredende excentriciteit: Md/Fd

Excentriciteit kleiner als L : 3 0,300 m
Optredend excentriciteit: 0,109 m **voldoet** Geval 2

| Optredende grondspanning: | σ_1 (kN/m ²) | σ_2 (kN/m ²) | Toelaatbaar: |
|---------------------------|---|---------------------------------|-----------------------|
| | 23,29 | 145,43 | 150 kN/m ² |
| Unity check: | $\sigma_2 / 1.33 * \sigma_{\text{grond}} =$ | | 0,73 voldoet |

Meewerkende poerlengte: 0,90 m Veerconstante: 546,75 kNm/rad

Poeren berekening

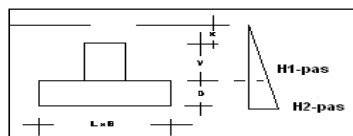
Maximaal opneembare horizontale belasting:

H1-passief: 8,25 kN/m'
H2-passief: 16,50 kN/m'

H t.g.v. wrijving: 22,78 kN
passief: 5,57 kN
H: 28,34 kN

Contra moment: 1,22 kNm

Unity check: Hd : H = 0,1933 **voldoet**



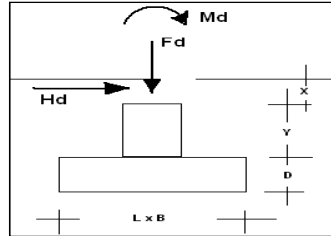
Let op: Hd dient kleiner te zijn dan passief

11.9 Poeren as B

Toepassen: $L*B*D = 1.10*1.10*0.5$ m #Ø8-150 onder & #Ø8-150 boven

Poeren berekening

| Geometrie en belastingen | |
|--------------------------|-----------|
| Fd = | 46,58 kN |
| Hd = | 12,52 kN |
| Md = | 10,36 kNm |
| x = | 0,50 m |
| y = | 0,00 m |
| L = | 1,10 m |
| B = | 1,10 m |
| D = | 0,50 m |



| Extra verticale belastingen $\gamma=1.0$ | | excentr. |
|--|---------|----------|
| F1 t.g.v. diverse | 0,00 kN | 0,00 m |
| F2 t.g.v. diverse | 0,00 kN | 0,00 m |
| F3 t.g.v. diverse | 0,00 kN | 0,00 m |
| F4 t.g.v. diverse | 0,00 kN | 0,00 m |
| F5 t.g.v. diverse | 0,00 kN | 0,00 m |

| Algemene gegevens | | | |
|-------------------|-------|-------------------------|-------------------------------|
| ρ | grond | 16,50 kN/m ³ | Betonkwaliteit: B 25 |
| ρ | beton | 24,00 kN/m ³ | Staalkwaliteit: FeB 500 |
| Dikte vloer: | | 0,12 m | Veiligheid tegen glijden 1,3 |
| σ | grond | 150 kN/m ² | Beddingsconst. 10000 |
| φ | grond | 33,00 ° | Factor passieve gronddruk 1,0 |

Percentage oppervlak vloer t.o.v. oppervlak poer: 1,00

| Totale belastingen | | | | | |
|--------------------|--------|-------------|-----------------|-----------|------------------|
| Fd | t.g.v. | kolom | 46,58 kN | Md | 16,62 kNm |
| | t.g.v. | poer | 17,42 kN | | |
| | t.g.v. | grond | 9,10 kN | | |
| | t.g.v. | bedrijfsvl. | 4,18 kN | | |
| | t.g.v. | F1 | 0,00 kN | 0,00 kNm | |
| | t.g.v. | F2 | 0,00 kN | 0,00 kNm | |
| | t.g.v. | F3 | 0,00 kN | 0,00 kNm | |
| | t.g.v. | F4 | 0,00 kN | 0,00 kNm | |
| | t.g.v. | F5 | 0,00 kN | 0,00 kNm | |
| | | Fd | 77,29 kN | Md | 16,62 kNm |

Optredende excentriciteit: Md/Fd

Excentriciteit kleiner als $L : 3$ 0,367 m

Optredend excentriciteit: 0,215 m **voldoet** Geval 3

| Optredende grondspanning: | σ_1 (kN/m ²) | σ_2 (kN/m ²) | Toelaatbaar: |
|---------------------------|--|---------------------------------|-----------------------|
| | 0 | 139,84 | 150 kN/m ² |
| Unity check: | $\sigma_2 / 1.33 * \sigma_{\text{grond}} = 0,70$ | | voldoet |

Meewerkende poerlengte: 1,00 m Veerconstante: 930,2 kNm/rad

Poeren berekening

Maximaal opneembare horizontale belasting:

H1-passief: 8,25 kN/m'

H2-passief: 16,50 kN/m'

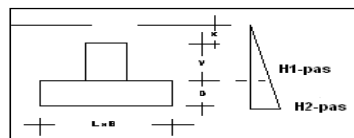
H t.g.v. wrijving: 25,76 kN

passief: 6,81 kN

H 32,57 kN

Contra moment: 2,45 kNm

Unity check: Hd : H = 0,3844 **voldoet**



Let op: Hd dient kleiner te zijn dan passief