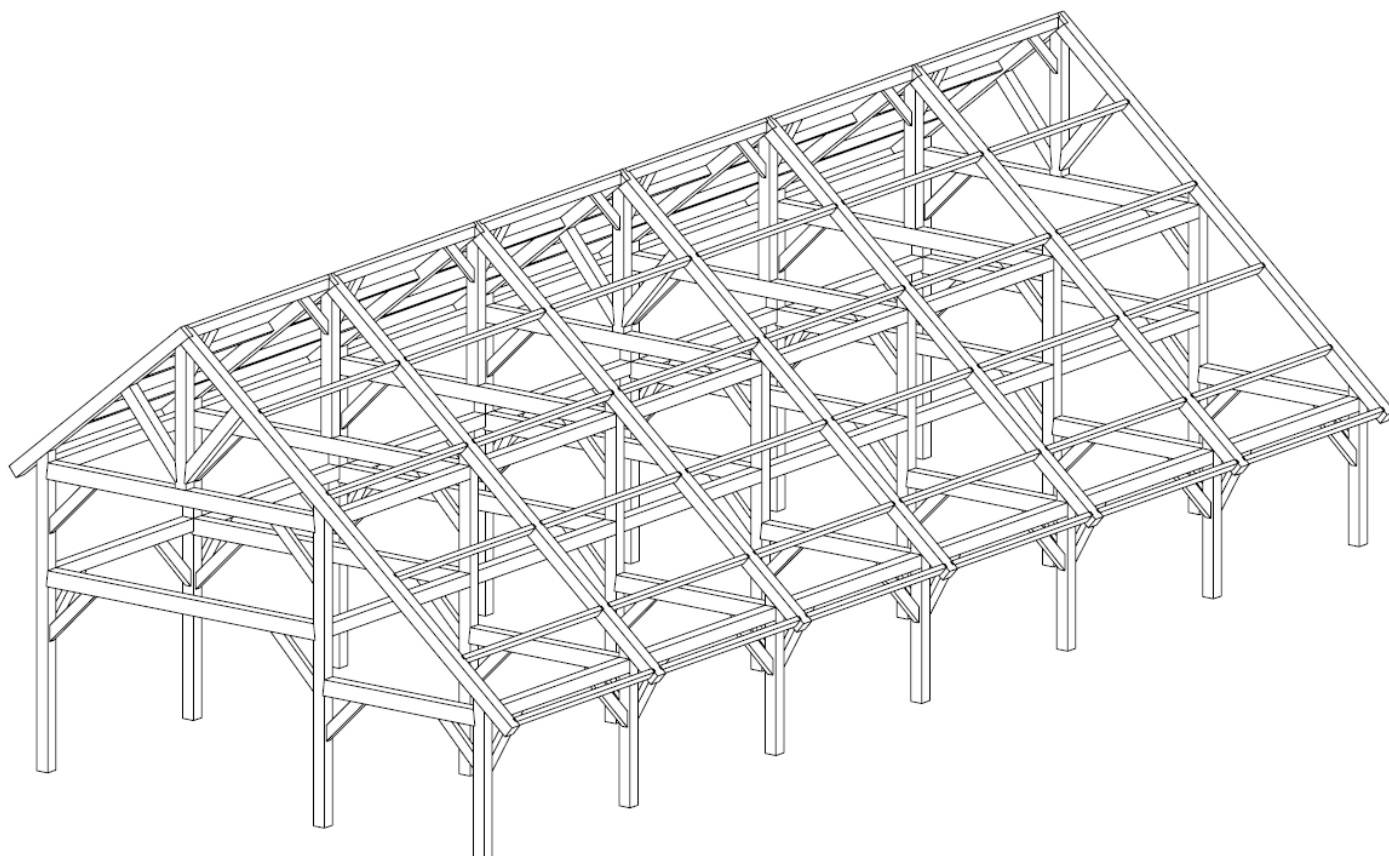


Statische Berekening

Overzicht constructie



Werk nr: **W023-18**
Datum: **05 oktober 2018**
Versie: **Schuur Meulenbrugge**

Betreft: **-Nieuwbouw schuur
-Landgoed Zelle
-Hengelo**

Opdrachtgever: **-Landgoed Zelle BV
-Ruurloseweg 92a**

Uitvoering bovenbouw: **-Houtbouw Neede
-Kisvelderweg 1
-7161 LC Neede
-0545 – 221 522**



liniekampen 32
7873 BT odoorn

E-mail: w.vanderhaar@ziggo.nl

telefoon:

bank: abn-amro
IBAN
BIC

kvk:

btw:

+31 (0) 654318997
40.03.08.924
NL52ABNA0400308924
ABNANL2A
56207484
NL852021100B01

Inhoudsopgave:

| | |
|--|-----------|
| INHOUDSOPGAVE: | 2 |
| UITGANGSPUNTEN: | 3 |
| 1.1 NORMEN: | 3 |
| Berekeningen worden uitgevoerd conform de Eurocode (NEN-EN + Nationale Bijlagen NL) voor gebouwen. | 3 |
| Toegepaste materialen:..... | 3 |
| Software:..... | 3 |
| Project uitgangspunten:..... | 4 |
| BELASTINGEN: | 4 |
| CONSTRUCTIE: | 4 |
| Plan van opzet | 4 |
| SPANT | 4 |
| Controle maatgevende onderdelen: | 23 |
| Kolom staaf 6 | 23 |
| Ligger staaf 30 | 24 |
| VERBINDINGEN: | 25 |
| Stiften ø22 | 25 |
| Knoop zijkolommen en vloerligger knoop 26 | 26 |
| Knoop Korbelen | 26 |
| GORDINGEN: | 26 |
| STABILITEIT LOODRECHT OP SPANT | 31 |

Uitgangspunten:

1.1 Normen:

Berekeningen worden uitgevoerd conform de Eurocode (NEN-EN + Nationale Bijlagen NL) voor gebouwen.

Eurocode 0:
NEN-EN 1990

Grondslagen.

Grondslagen voor het constructief ontwerp.

Eurocode 1:

NEN-EN 1991-1-1
NEN-EN 1991-1-2
NEN-EN 1991-1-3
NEN-EN 1991-1-4
NEN-EN 1991-1-5
NEN-EN 1991-1-6

Belastingen op constructies.

Dichtheden, eigen gewicht en opgelegde belastingen.
Belastingen bij brand.
Sneeuwbelastingen.
Windbelastingen.
Thermische belastingen.
Buitengewone belastingen (stootbelastingen, explosies).

Eurocode 2:

NEN-EN 1992-1-1
NEN-EN 1992-1-2

Ontwerp en berekening betonconstructies.

Algemene regels en regels voor gebouwen.
Ontwerp en berekening betonconstructies bij brand.

Eurocode 3:

NEN-EN 1993-1-1
NEN-EN 1993-1-2
NEN-EN 1993-1-3
NEN-EN 1993-1-8

Ontwerp en berekening staalconstructies.

Algemene regels en regels voor gebouwen.
Ontwerp en berekening staalconstructies bij brand.
Regels voor koudgevormde dunwandige profielen en platen.
Aanvullende regels voor verbindingen.

Eurocode 4:

NEN-EN 1994-1-1
NEN-EN 1994-1-2

Ontwerp en berekening staalbetonconstructies.

Algemene regels en regels voor gebouwen.
Ontwerp en berekening staalbetonconstructies bij brand.

Eurocode 5:

NEN-EN 1995-1-1
NEN-EN 1995-1-2

Ontwerp en berekening houtconstructies.

Algemene regels en regels voor gebouwen.
Ontwerp en berekening houtconstructies bij brand.

Eurocode 6:

NEN-EN 1996-1-1
NEN-EN 1996-1-2
NEN-EN 1996-2
NEN-EN 1996-3

Ontwerp en berekening metselwerk.

Algemene regels voor constructies van gewapend en ongewapend metselwerk.
Ontwerp en berekening metselwerkconstructies bij brand.
Ontwerp, materiaalkeuze en uitvoering constructies van metselwerk.
Vereenvoudigde rekenmethodes voor constructies van ongewapend metselwerk.

Toegepaste materialen:

Warmgewalst staal - S 235
Koudgewalst staal - S 275
Gezaagd hout - N.E. Vuren , C20
Gelamineerd hout - N.E. Vuren , GL24h
Eikenhout - C20
Azobe - D60

Software:

Technosoft
SCIA engineer
Excel 2010

Project uitgangspunten:

Het project betreft een schuur met een grote overkapte ruimte.
Het dak bestaat uit spanten hoh 3.60 m, met gordingen tussen de spanten.
De dakafwerking eternit golfplaten.
Er wordt in de gehele schuur geen zolder aangebracht.

Belastingen:

Dakbelasting:

Golfplaten: 0.20 kN/m²

Gordingen: 0.10 "

Extra: 0.10 "

Totaal -----
0.40 kN/m²

Sneeuwbelasting: zie berekening sporen

Constructie:

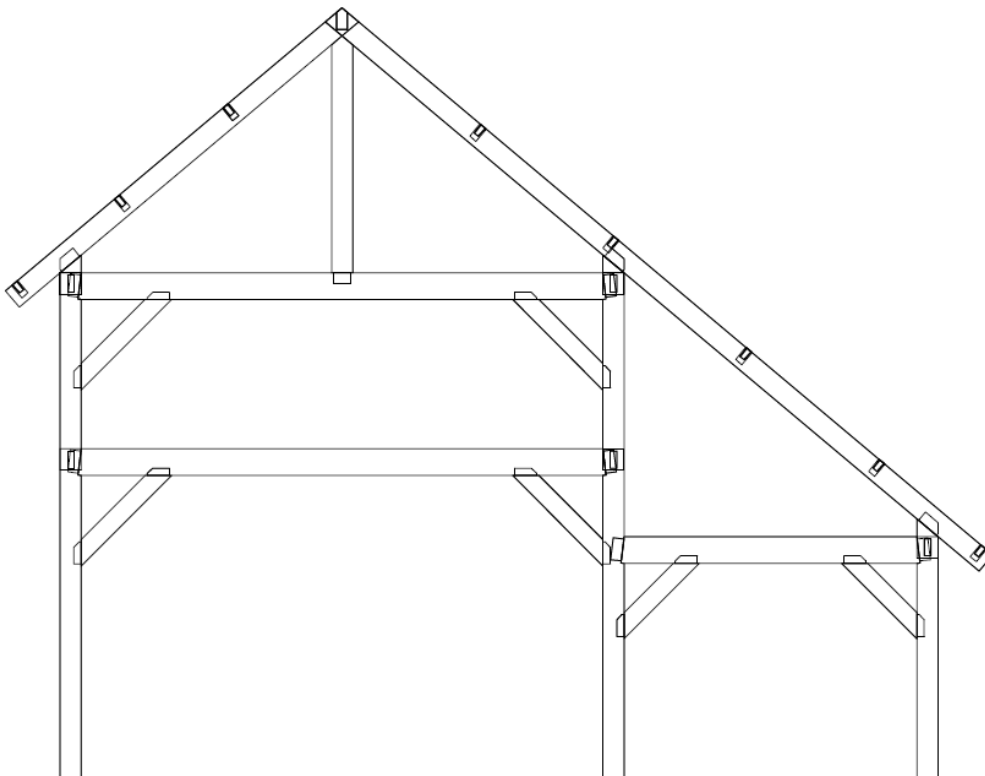
Plan van opzet

De spanten worden berekend. De stabiliteit wordt verzorgd door de schuine schoren in de spanten.

De gordingen worden berekend en ingekeept in de hoofdlijger.

De stabiliteit van het gebouw wordt door de schoren ter plaatse van de hoofdkolommen in de lengterichting verzorgd.

Spant.



Technosoft Raamwerken release 6.16

3 okt 2018

Project...: W023-18
Onderdeel: Meulenbrugge
Dimensies: kN;m;rad (tenzij anders aangegeven)
Datum....: 02/10/2018

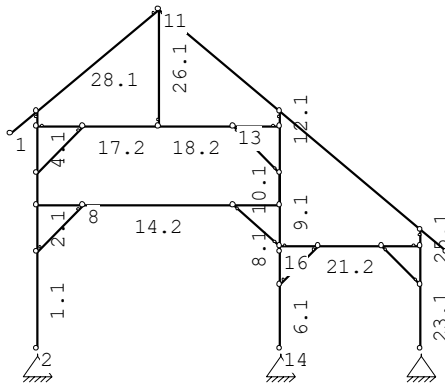
Belastingbreedte.: 3.600
Theorie voor de bepaling van de krachtsverdeling: Geometrisch lineair.

Gunstige werking van de permanente belasting wordt automatisch verwerkt.

Toegepaste normen volgens Eurocode met Nederlandse NB

| Belastingen | NEN-EN 1990:2002 | C2:2010 | NB:2011 (nl) |
|-------------|----------------------|---------|--------------|
| | NEN-EN 1991-1-1:2002 | C1:2009 | NB:2011 (nl) |
| | NEN-EN 1991-1-3:2003 | C1:2009 | NB:2011 (nl) |
| | NEN-EN 1991-1-4:2005 | C2:2011 | NB:2011 (nl) |

GEOMETRIE



MATERIALEN

| Mt | Omschrijving | E-modulus [N/mm ²] | S.M. | S.M.verhoogd | Pois. | Uitz. coëff |
|----|--------------|--------------------------------|------|--------------|-------|-------------|
| 1 | C20 | 9500 | 3.3 | 4.0 | 1.00 | 5.0000e-06 |

Bij de bepaling v.h. e.g. van houten staven is de S.M.verhoogd toegepast.

PROFIELEN [mm]

| Prof. | Omschrijving | Materiaal | Oppervlak | Traagheid | Vormf. |
|-------|--------------|-----------|------------|------------|--------|
| 1 | B*H 200*200 | 1:C20 | 4.0000e+04 | 1.3333e+08 | 0.00 |
| 2 | B*H 200*250 | 1:C20 | 5.0000e+04 | 2.6042e+08 | 0.00 |
| 3 | B*H 200*175 | 1:C20 | 3.5000e+04 | 8.9323e+07 | 0.00 |

PROFIELEN vervolg [mm]

| Prof. | Staaftype | Breedte | Hoogte | e | Type | b1 | h1 | b2 | h2 |
|-------|-----------|---------|--------|-------|------|----|----|----|----|
| 1 | 0:Normaal | 200 | 200 | 100.0 | 0:RH | | | | |
| 2 | 0:Normaal | 200 | 250 | 125.0 | 0:RH | | | | |
| 3 | 0:Normaal | 200 | 175 | 87.5 | 0:RH | | | | |

PROFIELVORMEN [mm]

1 B*H 200*200



2 B*H 200*250



3 B*H 200*175



KNOPEN

| Knoop | X | Z | Knoop | X | Z |
|-------|-------|-------|-------|-------|-------|
| 1 | 0.000 | 4.504 | 6 | 0.546 | 4.648 |
| 2 | 0.546 | 0.000 | 7 | 0.546 | 4.965 |
| 3 | 0.546 | 2.026 | 8 | 1.522 | 3.000 |
| 4 | 0.546 | 3.000 | 9 | 1.522 | 4.648 |
| 5 | 0.546 | 3.675 | 10 | 3.104 | 4.648 |
| 11 | 3.104 | 7.099 | 16 | 5.647 | 2.026 |

| | | | | | |
|----|-------|-------|----|-------|-------|
| 12 | 4.671 | 2.999 | 17 | 5.647 | 2.148 |
| 13 | 4.671 | 4.648 | 18 | 5.647 | 2.999 |
| 14 | 5.647 | 0.000 | 19 | 5.647 | 3.675 |
| 15 | 5.647 | 1.340 | 20 | 5.647 | 4.648 |
| 21 | 5.647 | 4.965 | 26 | 8.598 | 2.148 |
| 22 | 6.456 | 2.148 | 27 | 8.598 | 2.490 |
| 23 | 7.789 | 2.148 | 28 | 9.144 | 2.028 |
| 24 | 8.598 | 0.000 | | | |
| 25 | 8.598 | 1.340 | | | |

STAVEN

| St. | ki | kj | Profiel | Aansl.i | Aansl.j | Lengte | Opm. |
|-----|----|----|---------------|---------|---------|--------|------|
| 1 | 2 | 3 | 1:B*H 200*200 | NDM | NDM | 2.026 | |
| 2 | 3 | 4 | 1:B*H 200*200 | NDM | NDM | 0.974 | |
| 3 | 4 | 5 | 1:B*H 200*200 | NDM | NDM | 0.675 | |
| 4 | 5 | 6 | 1:B*H 200*200 | NDM | NDM | 0.973 | |
| 5 | 6 | 7 | 1:B*H 200*200 | NDM | ND- | 0.317 | |
| 6 | 14 | 15 | 1:B*H 200*200 | NDM | NDM | 1.340 | |
| 7 | 15 | 17 | 1:B*H 200*200 | NDM | NDM | 0.808 | |
| 8 | 17 | 16 | 1:B*H 200*200 | NDM | NDM | 0.122 | |
| 9 | 16 | 19 | 1:B*H 200*200 | NDM | NDM | 1.649 | |
| 10 | 19 | 18 | 1:B*H 200*200 | NDM | NDM | 0.676 | |
| 11 | 18 | 20 | 1:B*H 200*200 | NDM | NDM | 1.649 | |
| 12 | 20 | 21 | 1:B*H 200*200 | NDM | ND- | 0.317 | |
| 13 | 4 | 8 | 2:B*H 200*250 | NDM | NDM | 0.976 | |
| 14 | 8 | 12 | 2:B*H 200*250 | NDM | NDM | 3.149 | |
| 15 | 12 | 18 | 2:B*H 200*250 | NDM | NDM | 0.976 | |
| 16 | 6 | 9 | 2:B*H 200*250 | ND- | NDM | 0.976 | |
| 17 | 9 | 10 | 2:B*H 200*250 | NDM | NDM | 1.582 | |
| 18 | 10 | 13 | 2:B*H 200*250 | NDM | NDM | 1.567 | |
| 19 | 13 | 20 | 2:B*H 200*250 | NDM | ND- | 0.976 | |
| 20 | 17 | 22 | 2:B*H 200*250 | ND- | NDM | 0.809 | |
| 21 | 22 | 23 | 2:B*H 200*250 | NDM | NDM | 1.333 | |
| 22 | 23 | 26 | 2:B*H 200*250 | NDM | ND- | 0.809 | |
| 23 | 24 | 25 | 1:B*H 200*200 | NDM | NDM | 1.340 | |
| 24 | 25 | 26 | 1:B*H 200*200 | NDM | NDM | 0.808 | |
| 25 | 26 | 27 | 1:B*H 200*200 | NDM | ND- | 0.342 | |
| 26 | 10 | 11 | 1:B*H 200*200 | ND- | NDM | 2.451 | |
| 27 | 1 | 7 | 1:B*H 200*200 | NDM | NDM | 0.715 | |
| 28 | 7 | 11 | 1:B*H 200*200 | NDM | ND- | 3.331 | |
| 29 | 11 | 21 | 1:B*H 200*200 | ND- | NDM | 3.320 | |
| 30 | 21 | 27 | 1:B*H 200*200 | NDM | NDM | 3.851 | |
| 31 | 27 | 28 | 1:B*H 200*200 | NDM | NDM | 0.715 | |
| 32 | 3 | 8 | 3:B*H 200*175 | ND- | ND- | 1.379 | |
| 33 | 5 | 9 | 3:B*H 200*175 | NDM | ND- | 1.378 | |
| 34 | 17 | 12 | 3:B*H 200*175 | ND- | ND- | 1.295 | |
| 35 | 19 | 13 | 3:B*H 200*175 | ND- | ND- | 1.378 | |
| 36 | 15 | 22 | 3:B*H 200*175 | ND- | ND- | 1.143 | |
| 37 | 25 | 23 | 3:B*H 200*175 | ND- | ND- | 1.143 | |

VASTE STEUNPUNTEN

| Nr. knoop | Kode | XZR 1=vast 0=vrij | Hoek |
|-----------|------|-------------------|------|
| 1 | 2 | 110 | 0.00 |
| 2 | 14 | 110 | 0.00 |
| 3 | 24 | 110 | 0.00 |

BELASTINGGENERATIE ALGEMEEN.

| | | | |
|-----------------------------|-------|-------------------------|------|
| Betrouwbaarheidsklasse..... | 1 | Referentieperiode..... | 50 |
| Gebouwdiepte..... | 21.80 | Gebouwhoogte..... | 7.10 |
| Niveau aansl.terrein..... | 0.00 | E.g. scheid.w. [kN/m2]: | 1.20 |

WIND

| | |
|----------------------------------|---|
| Terrein categorie ...[4.3.2].... | Onbebouwd |
| Windgebied | 3 Vb,0 ..[4.2]..... 24.500 |
| Positie spant in het gebouw.... | 3.600 Kr[4.3.2]..... 0.209 |
| z0 | [4.3.2].... 0.200 Zmin ..[4.3.2]..... 4.000 |
| Co wind van links ..[4.3.3].... | 1.000 Co wind van rechts..... 1.000 |
| Co wind loodrecht ..[4.3.3].... | 1.000 |
| Cpi wind van links ..[7.2.9].... | 0.200 -0.300 |
| Cpi windloodrecht ...[7.2.9].... | 0.200 -0.300 |

Cpi wind van rechts .[7.2.9]...: 0.200 -0.300
 Cfr windwrijving[7.5].....: 0.040

SNEEUW

Sneeuwbelasting (sk) 50 jaar : 0.70
 Sneeuwbelasting (sn) n jaar : 0.70

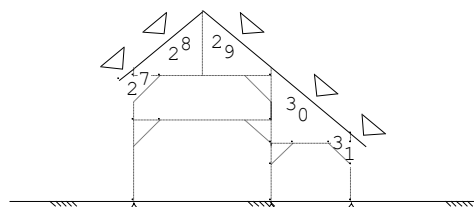
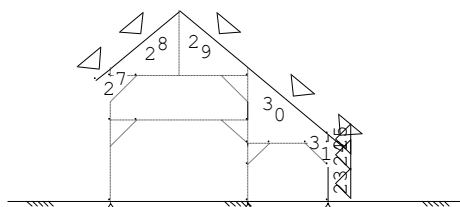
STAAPTYPEN

| Type | staven |
|------------------|-----------------|
| 6:Rechter gevel. | : 23-25 |
| 7:Dak. | : 27-31 |
| 9:Open. | : 1-22,26,32-37 |

LASTVELDEN

Wind staven

Sneeuw staven

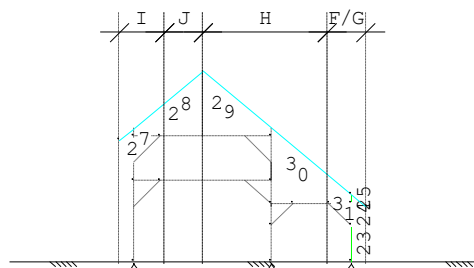
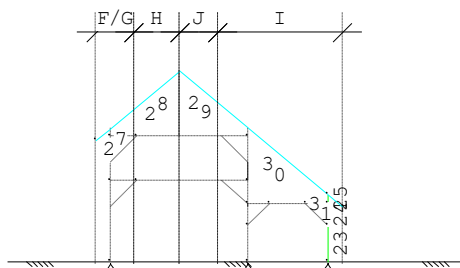
**WIND DAKTYPEN**

| Nr. | Staaft Type | reductie bij wind van links | reductie bij wind van Rechts | Cpe volgens art: |
|-----|----------------|--------------------------------|---------------------------------|------------------|
| 1 | 27-28 Zadeldak | 1.000 | 1.000 | 7.2.5 |
| 2 | 29-31 Zadeldak | 1.000 | 1.000 | 7.2.5 |
| 3 | 25-23 Gevel | 1.000 | 1.000 | 7.2.2 |

WIND ZONES

Wind van links

Wind van rechts

**WIND VAN LINKS ZONES****WIND VAN RECHTS ZONES**

| Nr. | Staaft | Positie | Lengte | Zone | Nr. | Staaft | Positie | Lengte | Zone |
|-----|--------|---------|--------|------|-----|--------|---------|--------|------|
| 1 | 27-28 | 0.000 | 1.420 | F/G | 1 | 25-23 | 0.000 | 2.490 | D |
| 2 | 27-28 | 1.420 | 1.684 | H | 2 | 29-31 | 0.000 | 1.420 | F/G |
| 3 | 29-31 | 0.000 | 1.420 | J | 3 | 29-31 | 1.420 | 4.620 | H |
| 4 | 29-31 | 1.420 | 4.620 | I | 4 | 27-28 | 0.000 | 1.420 | J |
| 5 | 25-23 | 0.000 | 2.490 | E | 5 | 27-28 | 1.420 | 1.684 | I |

Wind indexen

| Index | CsCd | Cpe/Cpi | qp | breedte | reductie | Qw | Zone | Hoek(en) |
|-------|------|---------|-------|---------|----------|--------|------|-----------|
| Qw1 | | 0.300 | 0.618 | 3.600 | | -0.668 | -i | |
| Qw2 | | -0.300 | 0.618 | 3.600 | | 0.668 | -i | |
| Qw3 | 1.00 | 0.700 | 0.618 | 1.750 | | -0.757 | F | 39.8 40.2 |
| Qw4 | 1.00 | 0.700 | 0.618 | 1.850 | | -0.801 | G | 39.8 40.2 |
| Qw5 | 1.00 | 0.531 | 0.618 | 3.600 | | -1.181 | H | 39.8 |
| Qw6 | 1.00 | -0.367 | 0.618 | 3.600 | | 0.816 | J | 40.0 |
| Qw7 | 1.00 | -0.267 | 0.618 | 3.600 | | 0.593 | I | 40.0 |
| Qw8 | 1.00 | 0.500 | 0.618 | 3.600 | | -1.113 | I | 40.2 |
| Qw9 | 1.00 | -0.264 | 0.618 | 3.600 | | 0.588 | I | 40.2 |
| Qw10 | 1.00 | 0.500 | 0.618 | 3.600 | | -1.113 | E | |
| Qw11 | | -0.200 | 0.618 | 3.600 | | 0.445 | +i | |
| Qw12 | | 0.200 | 0.618 | 3.600 | | -0.445 | +i | |
| Qw13 | 1.00 | -0.160 | 0.618 | 1.750 | | 0.173 | F | 40.2 |
| Qw14 | 1.00 | -0.160 | 0.618 | 1.850 | | 0.183 | G | 40.2 |
| Qw15 | 1.00 | -0.173 | 0.618 | 1.750 | | 0.187 | F | 39.8 |
| Qw16 | 1.00 | -0.173 | 0.618 | 1.850 | | 0.198 | G | 39.8 |
| Qw17 | 1.00 | -0.069 | 0.618 | 3.600 | | 0.154 | H | 39.8 |

| | | | | | | |
|------|------|--------|-------|-------|----------|------|
| Qw18 | 1.00 | -0.800 | 0.618 | 3.600 | 1.780 D | |
| Qw19 | 1.00 | -0.800 | 0.618 | 3.600 | 1.780 F | 40.2 |
| Qw20 | 1.00 | 0.533 | 0.618 | 3.600 | -1.187 H | 40.0 |
| Qw21 | 1.00 | -0.369 | 0.618 | 3.600 | 0.822 J | 39.8 |
| Qw22 | 1.00 | -0.269 | 0.618 | 3.600 | 0.599 I | 39.8 |
| Qw23 | 1.00 | -0.167 | 0.618 | 1.750 | 0.180 F | 40.0 |
| Qw24 | 1.00 | -0.167 | 0.618 | 1.850 | 0.191 G | 40.0 |
| Qw25 | 1.00 | -0.067 | 0.618 | 3.600 | 0.148 H | 40.0 |

SNEEUW DAKTYPEN

Staaft artikel

| | |
|-------|-----------------|
| 27-28 | 5.3.3 Zadel dak |
| 29-31 | 5.3.3 Zadel dak |

Sneeuw indexen

| Index | art | m | s _k | red. posfac | breedte | Q _s | hoek |
|-------|-------|-------|----------------|-------------|---------|----------------|------|
| Qs1 | 5.3.3 | 0.529 | 0.70 | 1.00 | 3.600 | 1.332 | 40.2 |
| Qs2 | 5.3.3 | 0.538 | 0.70 | 1.00 | 3.600 | 1.355 | 39.8 |
| Qs3 | 5.3.3 | 0.533 | 0.70 | 1.00 | 3.600 | 1.344 | 40.0 |
| Qs4 | 5.3.3 | 0.534 | 0.70 | 1.00 | 3.600 | 1.345 | 40.0 |
| Qs5 | 5.3.3 | 0.527 | 0.70 | 1.00 | 3.600 | 1.328 | 40.2 |
| Qs6 | 5.3.3 | 0.264 | 0.70 | 1.00 | 3.600 | 0.666 | 40.2 |
| Qs7 | 5.3.3 | 0.269 | 0.70 | 1.00 | 3.600 | 0.677 | 39.8 |
| Qs8 | 5.3.3 | 0.267 | 0.70 | 1.00 | 3.600 | 0.672 | 40.0 |
| Qs9 | 5.3.3 | 0.267 | 0.70 | 1.00 | 3.600 | 0.672 | 40.0 |
| Qs10 | 5.3.3 | 0.264 | 0.70 | 1.00 | 3.600 | 0.664 | 40.2 |

BELASTINGGEVALLEN

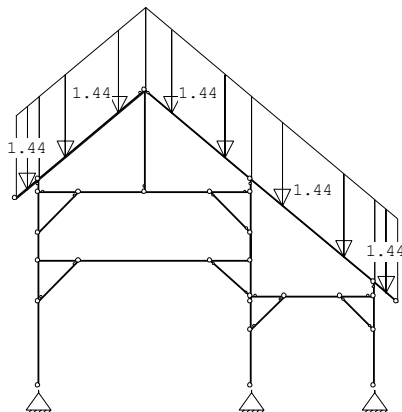
| B.G. | Omschrijving | Type |
|------|----------------------------------|------|
| | 1 Permanente belasting EGZ=-1.00 | 1 |
| g | 2 Wind van links onderdruk A | 7 |
| g | 3 Wind van links overdruk A | 8 |
| g | 4 Wind van links onderdruk B | 9 |
| g | 5 Wind van links overdruk B | 10 |
| g | 6 Wind van links onderdruk C | 37 |
| g | 7 Wind van links overdruk C | 38 |
| g | 8 Wind van links onderdruk D | 39 |
| g | 9 Wind van links overdruk D | 40 |
| g | 10 Wind van rechts onderdruk A | 11 |
| g | 11 Wind van rechts overdruk A | 12 |
| g | 12 Wind van rechts onderdruk B | 13 |
| g | 13 Wind van rechts overdruk B | 14 |
| g | 14 Wind van rechts onderdruk C | 41 |
| g | 15 Wind van rechts overdruk C | 42 |
| g | 16 Wind van rechts onderdruk D | 43 |
| g | 17 Wind van rechts overdruk D | 44 |
| g | 18 Sneeuw A | 22 |
| g | 19 Sneeuw B | 23 |
| g | 20 Sneeuw C | 33 |

g = gegeneerd belastinggeval

BELASTINGEN

B.G:1 Permanente belasting

Eigen gewicht van alle staven is meegenomen in berekening. Richting:—



STAAFBELASTINGEN

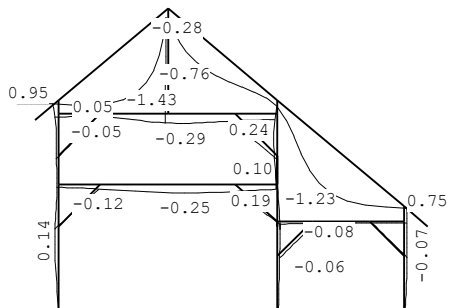
B.G:1 Permanente belasting

| Staaftype | Type | q1/p/m | q2 | A | B | y ₀ | y ₁ | y ₂ |
|-----------|-------------|--------|-------|-------|-------|----------------|----------------|----------------|
| 27 | 5:QZGlobaal | -1.44 | -1.44 | 0.000 | 0.000 | | | |
| 28 | 5:QZGlobaal | -1.44 | -1.44 | 0.000 | 0.000 | | | |
| 29 | 5:QZGlobaal | -1.44 | -1.44 | 0.000 | 0.000 | | | |
| 30 | 5:QZGlobaal | -1.44 | -1.44 | 0.000 | 0.000 | | | |
| 31 | 5:QZGlobaal | -1.44 | -1.44 | 0.000 | 0.000 | | | |

VERPLAATSINGEN

[mm]

B.G:1 Permanente belasting

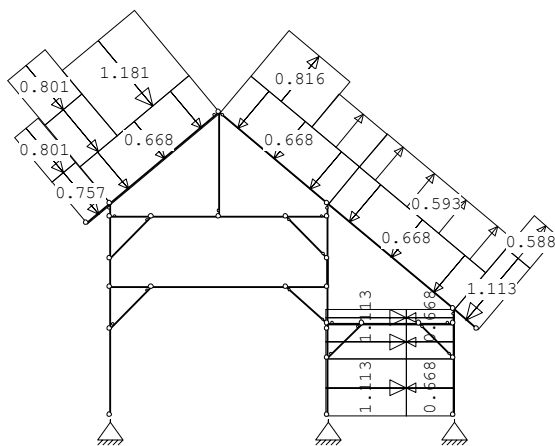
**REACTIES**

B.G:1 Permanente belasting

| Kn. | X | Z | M |
|-----|-------|--------|--------------------------|
| 2 | 0.10 | 8.76 | |
| 14 | 0.00 | 11.63 | |
| 24 | -0.10 | 4.96 | |
| | 0.00 | 25.35 | : Som van de reacties |
| | -0.00 | -25.35 | : Som van de belastingen |

BELASTINGEN

B.G:2 Wind van links onderdruk A

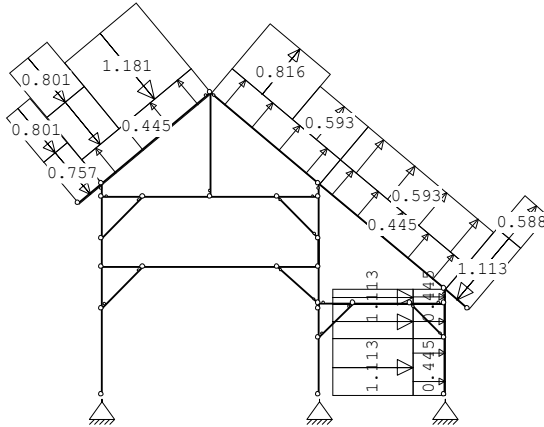
**STAAFBELASTINGEN**

B.G:2 Wind van links onderdruk A

| Staaftype | Type | Index | q1/p/m | q2 | A | B | y ₀ | y ₁ | y ₂ |
|-----------|------------|-------|--------|-------|-------|-------|----------------|----------------|----------------|
| 28 | 1:QZLokaal | Qw1 | -0.67 | -0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw1 | -0.67 | -0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw1 | -0.67 | -0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 25 | 1:QZLokaal | Qw2 | 0.67 | 0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 24 | 1:QZLokaal | Qw2 | 0.67 | 0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 23 | 1:QZLokaal | Qw2 | 0.67 | 0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 27 | 1:QZLokaal | Qw3 | -0.76 | -0.76 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 27 | 1:QZLokaal | Qw4 | -0.80 | -0.80 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw3 | -0.76 | -0.76 | 0.000 | 2.193 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw4 | -0.80 | -0.80 | 0.000 | 2.193 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw5 | -1.18 | -1.18 | 1.138 | 0.000 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw6 | 0.82 | 0.82 | 0.000 | 1.466 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw7 | 0.59 | 0.59 | 1.853 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw7 | 0.59 | 0.59 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 1:QZLokaal | Qw8 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 1:QZLokaal | Qw9 | 0.59 | 0.59 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 25 | 1:QZLokaal | Qw10 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 24 | 1:QZLokaal | Qw10 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 23 | 1:QZLokaal | Qw10 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |

BELASTINGEN

B.G:3 Wind van links overdruk A



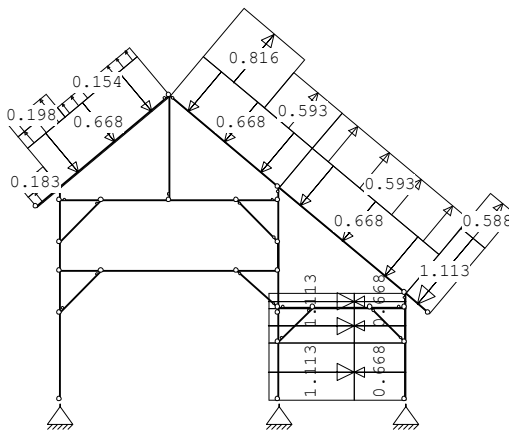
STAAFBELASTINGEN

B.G:3 Wind van links overdruk A

| Staaftype | Type | Index | q1/p/m | q2 | A | B | y ₀ | y ₁ | y ₂ |
|-----------|------------|-------|--------|-------|-------|-------|----------------|----------------|----------------|
| 28 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 25 | 1:QZLokaal | Qw12 | -0.45 | -0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 24 | 1:QZLokaal | Qw12 | -0.45 | -0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 23 | 1:QZLokaal | Qw12 | -0.45 | -0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 27 | 1:QZLokaal | Qw3 | -0.76 | -0.76 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 27 | 1:QZLokaal | Qw4 | -0.80 | -0.80 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw3 | -0.76 | -0.76 | 0.000 | 2.193 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw4 | -0.80 | -0.80 | 0.000 | 2.193 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw5 | -1.18 | -1.18 | 1.138 | 0.000 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw6 | 0.82 | 0.82 | 0.000 | 1.466 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw7 | 0.59 | 0.59 | 1.853 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw7 | 0.59 | 0.59 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 1:QZLokaal | Qw8 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 1:QZLokaal | Qw9 | 0.59 | 0.59 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 25 | 1:QZLokaal | Qw10 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 24 | 1:QZLokaal | Qw10 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 23 | 1:QZLokaal | Qw10 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |

BELASTINGEN

B.G:4 Wind van links onderdruk B



STAAFBELASTINGEN

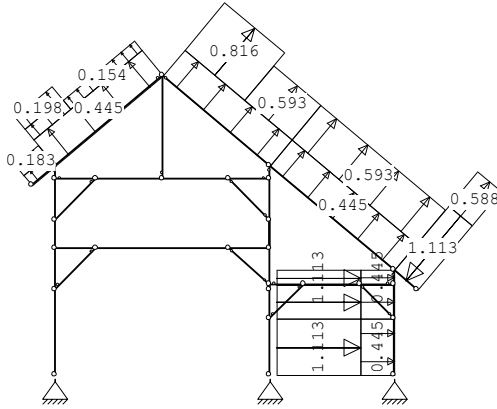
B.G:4 Wind van links onderdruk B

| Staaftype | Type | Index | q1/p/m | q2 | A | B | y ₀ | y ₁ | y ₂ |
|-----------|------------|-------|--------|-------|-------|-------|----------------|----------------|----------------|
| 28 | 1:QZLokaal | Qw1 | -0.67 | -0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw1 | -0.67 | -0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw1 | -0.67 | -0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 25 | 1:QZLokaal | Qw2 | 0.67 | 0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 24 | 1:QZLokaal | Qw2 | 0.67 | 0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 23 | 1:QZLokaal | Qw2 | 0.67 | 0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 27 | 1:QZLokaal | Qw13 | 0.17 | 0.17 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 27 | 1:QZLokaal | Qw14 | 0.18 | 0.18 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw15 | 0.19 | 0.19 | 0.000 | 2.193 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw16 | 0.20 | 0.20 | 0.000 | 2.193 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw17 | 0.15 | 0.15 | 1.138 | 0.000 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw6 | 0.82 | 0.82 | 0.000 | 1.466 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw7 | 0.59 | 0.59 | 1.853 | 0.000 | 0.0 | 0.2 | 0.0 |

| | | | | | | | | | |
|----|------------|------|-------|-------|-------|-------|-----|-----|-----|
| 30 | 1:QZLokaal | Qw7 | 0.59 | 0.59 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 1:QZLokaal | Qw8 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 1:QZLokaal | Qw9 | 0.59 | 0.59 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 25 | 1:QZLokaal | Qw10 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 24 | 1:QZLokaal | Qw10 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 23 | 1:QZLokaal | Qw10 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |

BELASTINGEN

B.G:5 Wind van links overdruk B

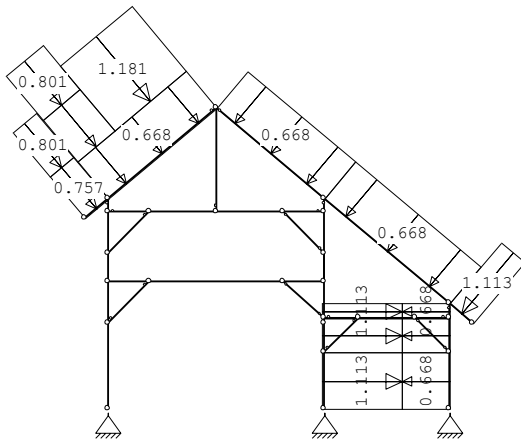
**STAAFBELASTINGEN**

B.G:5 Wind van links overdruk B

| Staat | Type | Index | q1/p/m | q2 | A | B | y ₀ | y ₁ | y ₂ |
|-------|------------|-------|--------|-------|-------|-------|----------------|----------------|----------------|
| 28 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 25 | 1:QZLokaal | Qw12 | -0.45 | -0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 24 | 1:QZLokaal | Qw12 | -0.45 | -0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 23 | 1:QZLokaal | Qw12 | -0.45 | -0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 27 | 1:QZLokaal | Qw13 | 0.17 | 0.17 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 27 | 1:QZLokaal | Qw14 | 0.18 | 0.18 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw15 | 0.19 | 0.19 | 0.000 | 2.193 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw16 | 0.20 | 0.20 | 0.000 | 2.193 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw17 | 0.15 | 0.15 | 1.138 | 0.000 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw6 | 0.82 | 0.82 | 0.000 | 1.466 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw7 | 0.59 | 0.59 | 1.853 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw7 | 0.59 | 0.59 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 1:QZLokaal | Qw8 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 1:QZLokaal | Qw9 | 0.59 | 0.59 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 25 | 1:QZLokaal | Qw10 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 24 | 1:QZLokaal | Qw10 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 23 | 1:QZLokaal | Qw10 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |

BELASTINGEN

B.G:6 Wind van links onderdruk C

**STAAFBELASTINGEN**

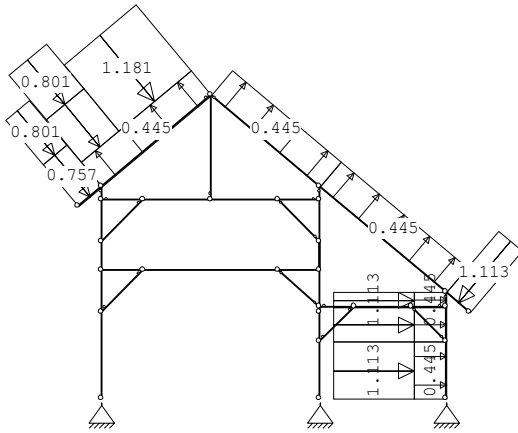
B.G:6 Wind van links onderdruk C

| Staat | Type | Index | q1/p/m | q2 | A | B | y ₀ | y ₁ | y ₂ |
|-------|------------|-------|--------|-------|-------|-------|----------------|----------------|----------------|
| 28 | 1:QZLokaal | Qw1 | -0.67 | -0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw1 | -0.67 | -0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw1 | -0.67 | -0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 25 | 1:QZLokaal | Qw2 | 0.67 | 0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 24 | 1:QZLokaal | Qw2 | 0.67 | 0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 23 | 1:QZLokaal | Qw2 | 0.67 | 0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |

| | | | | | | | | | |
|----|------------|------|-------|-------|-------|-------|-----|-----|-----|
| 27 | 1:QZLokaal | Qw3 | -0.76 | -0.76 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 27 | 1:QZLokaal | Qw4 | -0.80 | -0.80 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw3 | -0.76 | -0.76 | 0.000 | 2.193 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw4 | -0.80 | -0.80 | 0.000 | 2.193 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw5 | -1.18 | -1.18 | 1.138 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 1:QZLokaal | Qw8 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 25 | 1:QZLokaal | Qw10 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 24 | 1:QZLokaal | Qw10 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 23 | 1:QZLokaal | Qw10 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |

BELASTINGEN

B.G:7 Wind van links overdruk C

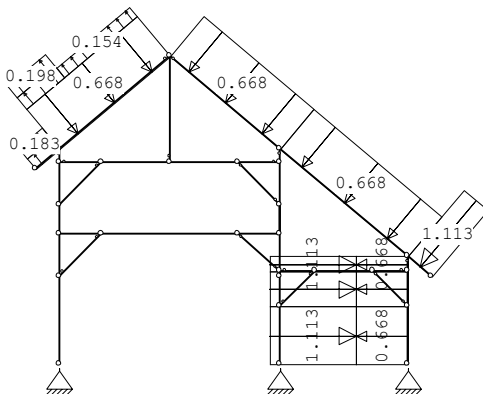
**STAAFBELASTINGEN**

B.G:7 Wind van links overdruk C

| Staaftype | Type | Index | q1/p/m | q2 | A | B | y ₀ | y ₁ | y ₂ |
|-----------|------------|-------|--------|-------|-------|-------|----------------|----------------|----------------|
| 28 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 25 | 1:QZLokaal | Qw12 | -0.45 | -0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 24 | 1:QZLokaal | Qw12 | -0.45 | -0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 23 | 1:QZLokaal | Qw12 | -0.45 | -0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 27 | 1:QZLokaal | Qw3 | -0.76 | -0.76 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 27 | 1:QZLokaal | Qw4 | -0.80 | -0.80 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw3 | -0.76 | -0.76 | 0.000 | 2.193 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw4 | -0.80 | -0.80 | 0.000 | 2.193 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw5 | -1.18 | -1.18 | 1.138 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 1:QZLokaal | Qw8 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 25 | 1:QZLokaal | Qw10 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 24 | 1:QZLokaal | Qw10 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 23 | 1:QZLokaal | Qw10 | -1.11 | -1.11 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |

BELASTINGEN

B.G:8 Wind van links onderdruk D

**STAAFBELASTINGEN**

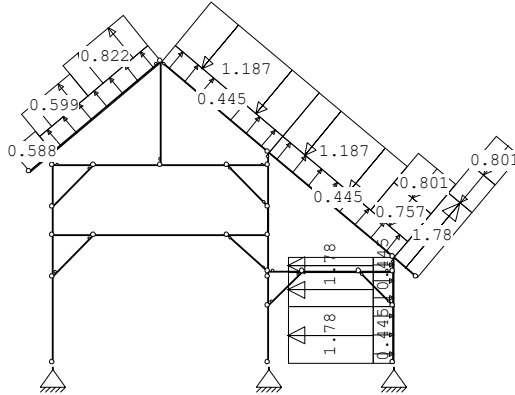
B.G:8 Wind van links onderdruk D

| Staaftype | Type | Index | q1/p/m | q2 | A | B | y ₀ | y ₁ | y ₂ |
|-----------|------------|-------|--------|-------|-------|-------|----------------|----------------|----------------|
| 28 | 1:QZLokaal | Qw1 | -0.67 | -0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw1 | -0.67 | -0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw1 | -0.67 | -0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 25 | 1:QZLokaal | Qw2 | 0.67 | 0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 24 | 1:QZLokaal | Qw2 | 0.67 | 0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 23 | 1:QZLokaal | Qw2 | 0.67 | 0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 27 | 1:QZLokaal | Qw13 | 0.17 | 0.17 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 27 | 1:QZLokaal | Qw14 | 0.18 | 0.18 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |

| | | | | | | | | | |
|----|------------|------|-------|-------|-------|-------|-----|-----|-----|
| 30 | 1:QZLokaal | Qw3 | -0.76 | -0.76 | 2.711 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw4 | -0.80 | -0.80 | 2.711 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw20 | -1.19 | -1.19 | 0.000 | 1.140 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw20 | -1.19 | -1.19 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw21 | 0.82 | 0.82 | 1.482 | 0.000 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw22 | 0.60 | 0.60 | 0.000 | 1.849 | 0.0 | 0.2 | 0.0 |
| 27 | 1:QZLokaal | Qw9 | 0.59 | 0.59 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |

BELASTINGEN

B.G:11 Wind van rechts overdruk A



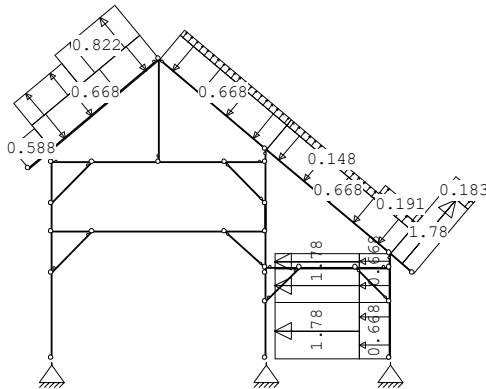
STAAFBELASTINGEN

B.G:11 Wind van rechts overdruk A

| Staaftype | Type | Index | q1/p/m | q2 | A | B | y ₀ | y ₁ | y ₂ |
|-----------|------------|-------|--------|-------|-------|-------|----------------|----------------|----------------|
| 28 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 25 | 1:QZLokaal | Qw12 | -0.45 | -0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 24 | 1:QZLokaal | Qw12 | -0.45 | -0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 23 | 1:QZLokaal | Qw12 | -0.45 | -0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 23 | 1:QZLokaal | Qw18 | 1.78 | 1.78 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 24 | 1:QZLokaal | Qw18 | 1.78 | 1.78 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 25 | 1:QZLokaal | Qw18 | 1.78 | 1.78 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 1:QZLokaal | Qw19 | 1.78 | 1.78 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 1:QZLokaal | Qw3 | -0.76 | -0.76 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 1:QZLokaal | Qw4 | -0.80 | -0.80 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw3 | -0.76 | -0.76 | 2.711 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw4 | -0.80 | -0.80 | 2.711 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw20 | -1.19 | -1.19 | 0.000 | 1.140 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw20 | -1.19 | -1.19 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw21 | 0.82 | 0.82 | 1.482 | 0.000 | 0.0 | 0.2 | 0.0 |
| 28 | 1:QZLokaal | Qw22 | 0.60 | 0.60 | 0.000 | 1.849 | 0.0 | 0.2 | 0.0 |
| 27 | 1:QZLokaal | Qw9 | 0.59 | 0.59 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |

BELASTINGEN

B.G:12 Wind van rechts onderdruk B



STAAFBELASTINGEN

B.G:12 Wind van rechts onderdruk B

| Staaftype | Type | Index | q1/p/m | q2 | A | B | y ₀ | y ₁ | y ₂ |
|-----------|------------|-------|--------|-------|-------|-------|----------------|----------------|----------------|
| 28 | 1:QZLokaal | Qw1 | -0.67 | -0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw1 | -0.67 | -0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw1 | -0.67 | -0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 25 | 1:QZLokaal | Qw2 | 0.67 | 0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 24 | 1:QZLokaal | Qw2 | 0.67 | 0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 23 | 1:QZLokaal | Qw2 | 0.67 | 0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 23 | 1:QZLokaal | Qw18 | 1.78 | 1.78 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 24 | 1:QZLokaal | Qw18 | 1.78 | 1.78 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |

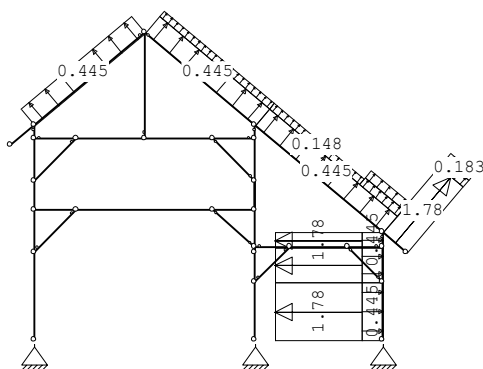
werk nr:
 betreft:

 W023-18
 Nieuwbouw schuur Zelle BV

| | | | | | | | | | |
|----|------------|------|------|------|-------|-------|-----|-----|-----|
| 24 | 1:QZLokaal | Qw18 | 1.78 | 1.78 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 25 | 1:QZLokaal | Qw18 | 1.78 | 1.78 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 1:QZLokaal | Qw19 | 1.78 | 1.78 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 1:QZLokaal | Qw13 | 0.17 | 0.17 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 1:QZLokaal | Qw14 | 0.18 | 0.18 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw23 | 0.18 | 0.18 | 2.711 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw24 | 0.19 | 0.19 | 2.711 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw25 | 0.15 | 0.15 | 0.000 | 1.140 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw25 | 0.15 | 0.15 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |

BELASTINGEN

B.G:17 Wind van rechts overdruk D

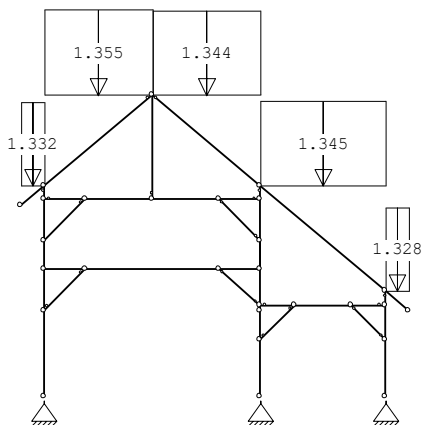
**STAAFBELASTINGEN**

B.G:17 Wind van rechts overdruk D

| Staat | Type | Index | q1/p/m | q2 | A | B | y ₀ | y ₁ | y ₂ |
|-------|------------|-------|--------|-------|-------|-------|----------------|----------------|----------------|
| 28 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw11 | 0.45 | 0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 25 | 1:QZLokaal | Qw12 | -0.45 | -0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 24 | 1:QZLokaal | Qw12 | -0.45 | -0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 23 | 1:QZLokaal | Qw12 | -0.45 | -0.45 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 23 | 1:QZLokaal | Qw18 | 1.78 | 1.78 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 24 | 1:QZLokaal | Qw18 | 1.78 | 1.78 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 25 | 1:QZLokaal | Qw18 | 1.78 | 1.78 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 1:QZLokaal | Qw19 | 1.78 | 1.78 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 1:QZLokaal | Qw13 | 0.17 | 0.17 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 1:QZLokaal | Qw14 | 0.18 | 0.18 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw23 | 0.18 | 0.18 | 2.711 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw24 | 0.19 | 0.19 | 2.711 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 1:QZLokaal | Qw25 | 0.15 | 0.15 | 0.000 | 1.140 | 0.0 | 0.2 | 0.0 |
| 29 | 1:QZLokaal | Qw25 | 0.15 | 0.15 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |

BELASTINGEN

B.G:18 Sneeuw A

**STAAFBELASTINGEN**

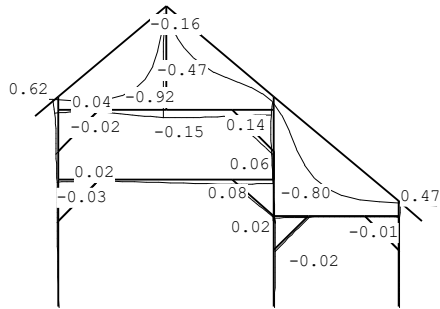
B.G:18 Sneeuw A

| Staat | Type | Index | q1/p/m | q2 | A | B | y ₀ | y ₁ | y ₂ |
|-------|-------------|-------|--------|-------|-------|-------|----------------|----------------|----------------|
| 27 | 3:QZgeProj. | Qs1 | -1.33 | -1.33 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 28 | 3:QZgeProj. | Qs2 | -1.35 | -1.35 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 29 | 3:QZgeProj. | Qs3 | -1.34 | -1.34 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 3:QZgeProj. | Qs4 | -1.34 | -1.34 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 3:QZgeProj. | Qs5 | -1.33 | -1.33 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |

VERPLAATSINGEN

[mm]

B.G:18 Sneeuw A



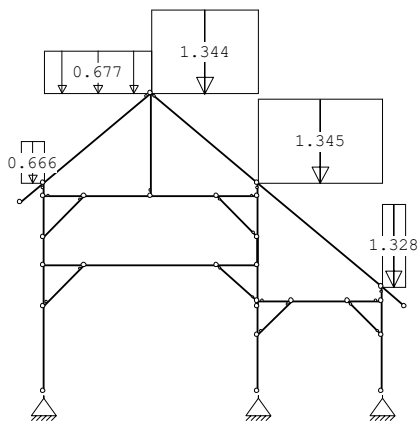
REACTIES

B.G:18 Sneeuw A

| Kn. | X | Z | M |
|-----|-------|--------|--------------------------|
| 2 | 0.01 | 4.13 | |
| 14 | -0.01 | 5.55 | |
| 24 | 0.00 | 2.63 | |
| | 0.00 | 12.30 | : Som van de reacties |
| | 0.00 | -12.30 | : Som van de belastingen |

BELASTINGEN

B.G:19 Sneeuw B



STAAFBELASTINGEN

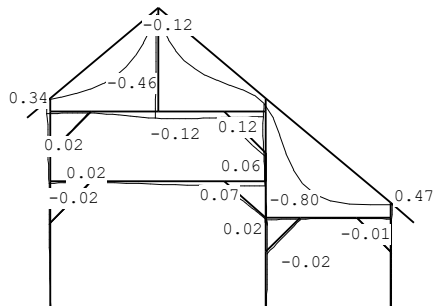
B.G:19 Sneeuw B

| Staf | Type | Index | q1/p/m | q2 | A | B | y ₀ | y ₁ | y _z |
|------|-------------|-------|--------|-------|-------|-------|----------------|----------------|----------------|
| 27 | 3:QZgeProj. | Qs6 | -0.67 | -0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 28 | 3:QZgeProj. | Qs7 | -0.68 | -0.68 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 29 | 3:QZgeProj. | Qs3 | -1.34 | -1.34 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 3:QZgeProj. | Qs4 | -1.34 | -1.34 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 3:QZgeProj. | Qs5 | -1.33 | -1.33 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |

VERPLAATSINGEN

[mm]

B.G:19 Sneeuw B



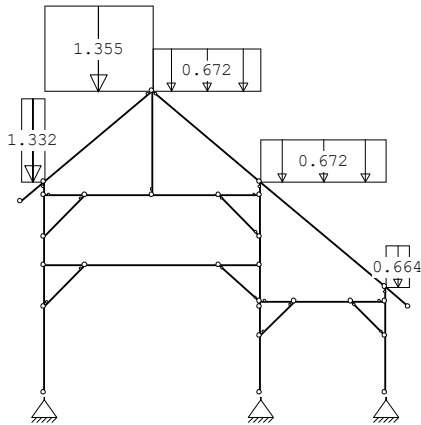
REACTIES

B.G:19 Sneeuw B

| Kn. | X | Z | M |
|-----|-------|--------|--------------------------|
| 2 | 0.01 | 2.42 | |
| 14 | -0.01 | 5.21 | |
| 24 | 0.00 | 2.58 | |
| | 0.00 | 10.21 | : Som van de reacties |
| | 0.00 | -10.21 | : Som van de belastingen |

BELASTINGEN

B.G:20 Sneeuw C



STAAFBELASTINGEN

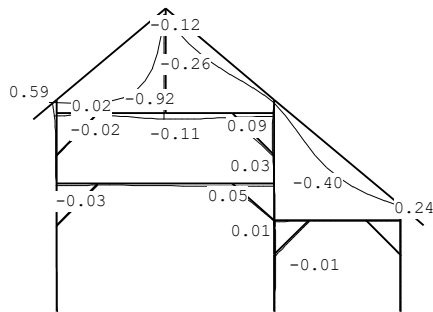
B.G:20 Sneeuw C

| Staaft | Type | Index | q1/p/m | q2 | A | B | y ₀ | y ₁ | y ₂ |
|--------|-------------|-------|--------|-------|-------|-------|----------------|----------------|----------------|
| 27 | 3:QZgeProj. | Qs1 | -1.33 | -1.33 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 28 | 3:QZgeProj. | Qs2 | -1.35 | -1.35 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 29 | 3:QZgeProj. | Qs8 | -0.67 | -0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 30 | 3:QZgeProj. | Qs9 | -0.67 | -0.67 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |
| 31 | 3:QZgeProj. | Qs10 | -0.66 | -0.66 | 0.000 | 0.000 | 0.0 | 0.2 | 0.0 |

VERPLAATSINGEN

[mm]

B.G:20 Sneeuw C



REACTIES

B.G:20 Sneeuw C

| Kn. | X | Z | M |
|-----|-------|-------|--------------------------|
| 2 | 0.01 | 3.77 | |
| 14 | -0.01 | 3.11 | |
| 24 | 0.00 | 1.36 | |
| | 0.00 | 8.25 | : Som van de reacties |
| | 0.00 | -8.25 | : Som van de belastingen |

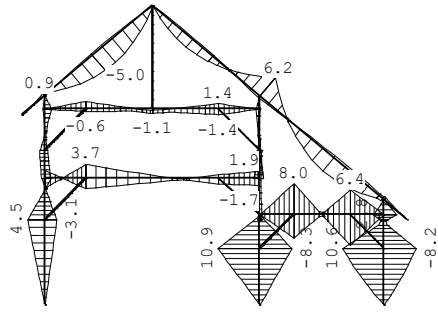
BELASTINGCOMBINATIES

| BC | Type |
|----|--|
| 1 | Fund. 1.22 G _{k,1} |
| 2 | Fund. 0.90 G _{k,1} |
| 3 | Fund. 1.08 G _{k,1} + 1.35 Q _{k,2} |
| 4 | Fund. 1.08 G _{k,1} + 1.35 Q _{k,3} |
| 5 | Fund. 1.08 G _{k,1} + 1.35 Q _{k,4} |
| 6 | Fund. 1.08 G _{k,1} + 1.35 Q _{k,5} |
| 7 | Fund. 1.08 G _{k,1} + 1.35 Q _{k,6} |
| 8 | Fund. 1.08 G _{k,1} + 1.35 Q _{k,7} |
| 9 | Fund. 1.08 G _{k,1} + 1.35 Q _{k,8} |
| 10 | Fund. 1.08 G _{k,1} + 1.35 Q _{k,9} |
| 11 | Fund. 1.08 G _{k,1} + 1.35 Q _{k,10} |
| 12 | Fund. 1.08 G _{k,1} + 1.35 Q _{k,11} |
| 13 | Fund. 1.08 G _{k,1} + 1.35 Q _{k,12} |
| 14 | Fund. 1.08 G _{k,1} + 1.35 Q _{k,13} |
| 15 | Fund. 1.08 G _{k,1} + 1.35 Q _{k,14} |
| 16 | Fund. 1.08 G _{k,1} + 1.35 Q _{k,15} |
| 17 | Fund. 1.08 G _{k,1} + 1.35 Q _{k,16} |
| 18 | Fund. 1.08 G _{k,1} + 1.35 Q _{k,17} |
| 19 | Fund. 1.08 G _{k,1} + 1.35 Q _{k,18} |
| 20 | Fund. 1.08 G _{k,1} + 1.35 Q _{k,19} |

| | | | | | | |
|----|-------|------|------------------|---|------|----------------------------------|
| 21 | Fund. | 1.08 | G _{k,1} | + | 1.35 | Q _{k,20} |
| 22 | Fund. | 0.90 | G _{k,1} | + | 1.35 | Q _{k,2} |
| 23 | Fund. | 0.90 | G _{k,1} | + | 1.35 | Q _{k,3} |
| 24 | Fund. | 0.90 | G _{k,1} | + | 1.35 | Q _{k,4} |
| 25 | Fund. | 0.90 | G _{k,1} | + | 1.35 | Q _{k,5} |
| 26 | Fund. | 0.90 | G _{k,1} | + | 1.35 | Q _{k,6} |
| 27 | Fund. | 0.90 | G _{k,1} | + | 1.35 | Q _{k,7} |
| 28 | Fund. | 0.90 | G _{k,1} | + | 1.35 | Q _{k,8} |
| 29 | Fund. | 0.90 | G _{k,1} | + | 1.35 | Q _{k,9} |
| 30 | Fund. | 0.90 | G _{k,1} | + | 1.35 | Q _{k,10} |
| 31 | Fund. | 0.90 | G _{k,1} | + | 1.35 | Q _{k,11} |
| 32 | Fund. | 0.90 | G _{k,1} | + | 1.35 | Q _{k,12} |
| 33 | Fund. | 0.90 | G _{k,1} | + | 1.35 | Q _{k,13} |
| 34 | Fund. | 0.90 | G _{k,1} | + | 1.35 | Q _{k,14} |
| 35 | Fund. | 0.90 | G _{k,1} | + | 1.35 | Q _{k,15} |
| 36 | Fund. | 0.90 | G _{k,1} | + | 1.35 | Q _{k,16} |
| 37 | Fund. | 0.90 | G _{k,1} | + | 1.35 | Q _{k,17} |
| 38 | Fund. | 0.90 | G _{k,1} | + | 1.35 | Q _{k,18} |
| 39 | Fund. | 0.90 | G _{k,1} | + | 1.35 | Q _{k,19} |
| 40 | Fund. | 0.90 | G _{k,1} | + | 1.35 | Q _{k,20} |
| 41 | Kar. | 1.00 | G _{k,1} | + | 1.00 | Q _{k,2} |
| 42 | Kar. | 1.00 | G _{k,1} | + | 1.00 | Q _{k,3} |
| 43 | Kar. | 1.00 | G _{k,1} | + | 1.00 | Q _{k,4} |
| 44 | Kar. | 1.00 | G _{k,1} | + | 1.00 | Q _{k,5} |
| 45 | Kar. | 1.00 | G _{k,1} | + | 1.00 | Q _{k,6} |
| 46 | Kar. | 1.00 | G _{k,1} | + | 1.00 | Q _{k,7} |
| 47 | Kar. | 1.00 | G _{k,1} | + | 1.00 | Q _{k,8} |
| 48 | Kar. | 1.00 | G _{k,1} | + | 1.00 | Q _{k,9} |
| 49 | Kar. | 1.00 | G _{k,1} | + | 1.00 | Q _{k,10} |
| 50 | Kar. | 1.00 | G _{k,1} | + | 1.00 | Q _{k,11} |
| 51 | Kar. | 1.00 | G _{k,1} | + | 1.00 | Q _{k,12} |
| 52 | Kar. | 1.00 | G _{k,1} | + | 1.00 | Q _{k,13} |
| 53 | Kar. | 1.00 | G _{k,1} | + | 1.00 | Q _{k,14} |
| 54 | Kar. | 1.00 | G _{k,1} | + | 1.00 | Q _{k,15} |
| 55 | Kar. | 1.00 | G _{k,1} | + | 1.00 | Q _{k,16} |
| 56 | Kar. | 1.00 | G _{k,1} | + | 1.00 | Q _{k,17} |
| 57 | Kar. | 1.00 | G _{k,1} | + | 1.00 | Q _{k,18} |
| 58 | Kar. | 1.00 | G _{k,1} | + | 1.00 | Q _{k,19} |
| 59 | Kar. | 1.00 | G _{k,1} | + | 1.00 | Q _{k,20} |
| 60 | Quas. | 1.00 | G _{k,1} | | | |
| 61 | Freq. | 1.00 | G _{k,1} | | | |
| 62 | Freq. | 1.00 | G _{k,1} | + | 1.00 | y ₁ Q _{k,2} |
| 63 | Freq. | 1.00 | G _{k,1} | + | 1.00 | y ₁ Q _{k,3} |
| 64 | Freq. | 1.00 | G _{k,1} | + | 1.00 | y ₁ Q _{k,4} |
| 65 | Freq. | 1.00 | G _{k,1} | + | 1.00 | y ₁ Q _{k,5} |
| 66 | Freq. | 1.00 | G _{k,1} | + | 1.00 | y ₁ Q _{k,6} |
| 67 | Freq. | 1.00 | G _{k,1} | + | 1.00 | y ₁ Q _{k,7} |
| 68 | Freq. | 1.00 | G _{k,1} | + | 1.00 | y ₁ Q _{k,8} |
| 69 | Freq. | 1.00 | G _{k,1} | + | 1.00 | y ₁ Q _{k,9} |
| 70 | Freq. | 1.00 | G _{k,1} | + | 1.00 | y ₁ Q _{k,10} |
| 71 | Freq. | 1.00 | G _{k,1} | + | 1.00 | y ₁ Q _{k,11} |
| 72 | Freq. | 1.00 | G _{k,1} | + | 1.00 | y ₁ Q _{k,12} |
| 73 | Freq. | 1.00 | G _{k,1} | + | 1.00 | y ₁ Q _{k,13} |
| 74 | Freq. | 1.00 | G _{k,1} | + | 1.00 | y ₁ Q _{k,14} |
| 75 | Freq. | 1.00 | G _{k,1} | + | 1.00 | y ₁ Q _{k,15} |
| 76 | Freq. | 1.00 | G _{k,1} | + | 1.00 | y ₁ Q _{k,16} |
| 77 | Freq. | 1.00 | G _{k,1} | + | 1.00 | y ₁ Q _{k,17} |
| 78 | Freq. | 1.00 | G _{k,1} | + | 1.00 | y ₁ Q _{k,18} |
| 79 | Freq. | 1.00 | G _{k,1} | + | 1.00 | y ₁ Q _{k,19} |
| 80 | Freq. | 1.00 | G _{k,1} | + | 1.00 | y ₁ Q _{k,20} |
| 81 | Blij. | 1.00 | G _{k,1} | | | |

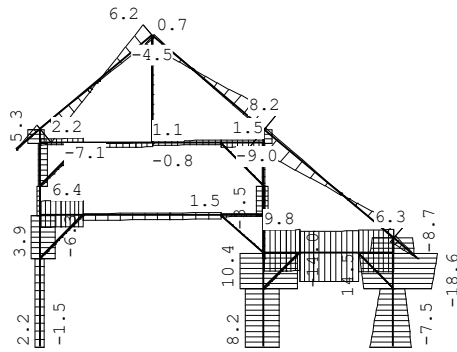
OMHULLENDE VAN DE FUNDAMENTELE COMBINATIES
MOMENTEN

Fundamentele combinatie



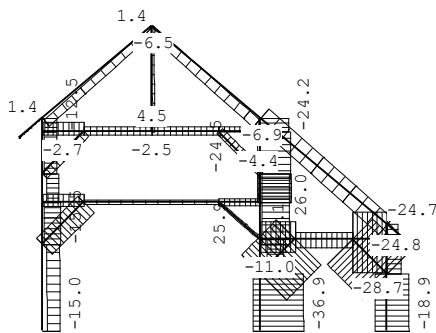
DWARSKRACHTEN

Fundamentele combinatie



NORMAALKRACHTEN

Fundamentele combinatie



STAAFKRACHTEN

Fundamentele combinatie

| St. | Kn. | Pos. | NXi/NXj | | Dzi/Dzj | | MYi/MYj | | | | | | | |
|-----|-------|------|---------|-----|---------|----|---------|-----|------|----|-------|----|-------|---------|
| | | | Min | Max | BC | BC | Min | Max | BC | | | | | |
| 1 | 2 | | -15.04 | 19 | -3.91 | 25 | -1.51 | 23 | 2.23 | 11 | 0.00 | 23 | 0.00 | 11 |
| 1 | 3 | | -14.69 | 19 | -3.62 | 25 | -1.51 | 23 | 2.23 | 11 | -3.06 | 23 | 4.51 | 11 |
| 2 | 3 | | -15.52 | 3 | -1.58 | 31 | -6.28 | 11 | 3.95 | 23 | -3.06 | 23 | 4.51 | 11 |
| 2 | 0.723 | | -15.40 | 3 | -1.47 | 31 | -6.28 | 11 | 3.95 | 23 | -0.24 | 8 | 0.00 | 32 |
| 2 | 0.728 | | -15.40 | 3 | -1.47 | 31 | -6.28 | 11 | 3.95 | 23 | -0.23 | 8 | -0.01 | 32 |
| 2 | 0.763 | | -15.39 | 3 | -1.47 | 31 | -6.28 | 11 | 3.95 | 23 | -0.28 | 11 | -0.05 | 3725.75 |
| 2 | 0.774 | | -15.39 | 3 | -1.47 | 31 | -6.28 | 11 | 3.95 | 23 | -0.35 | 11 | 0.00 | 23 |
| 2 | 4 | | -15.35 | 3 | -1.44 | 31 | -6.28 | 11 | 3.95 | 23 | -1.61 | 11 | 0.79 | 23 |
| 3 | 4 | | -13.92 | 7 | -3.38 | 33 | 0.28 | 36 | 1.54 | 19 | -1.37 | 4 | 0.96 | 30 |
| 3 | 5 | | -13.81 | 7 | -3.28 | 33 | 0.28 | 36 | 1.54 | 19 | -0.71 | 23 | 1.46 | 11 |
| 4 | 5 | | -12.42 | 7 | -1.57 | 33 | -2.97 | 11 | 1.12 | 23 | -0.57 | 23 | 1.20 | 11 |
| 4 | 0.291 | | -12.37 | 7 | -1.53 | 33 | -2.97 | 11 | 1.12 | 23 | -0.25 | 4 | 0.34 | 30 |
| 4 | 0.413 | | -12.35 | 7 | -1.51 | 33 | -2.97 | 11 | 1.12 | 23 | -0.31 | 6 | 0.06 | 34 |
| 4 | 6 | | -12.25 | 7 | -1.43 | 33 | -2.97 | 11 | 1.12 | 23 | -1.69 | 11 | 0.52 | 23 |
| 5 | 6 | | -12.53 | 7 | -1.95 | 33 | -1.63 | 23 | 5.33 | 11 | -1.69 | 11 | 0.52 | 23 |
| 5 | 7 | | -12.48 | 7 | -1.90 | 33 | -1.63 | 23 | 5.33 | 11 | 0.00 | 11 | 0.00 | 23 |
| 6 | 14 | | -36.86 | 11 | 6.44 | 23 | -6.17 | 23 | 8.15 | 11 | 0.00 | 23 | 0.00 | 11 |
| 6 | 15 | | -36.63 | 11 | 6.63 | 23 | -6.17 | 23 | 8.15 | 11 | -8.27 | 23 | 10.93 | 11 |

werk nr:
 betreft:

 W023-18
 Nieuwbouw schuur Zelle BV

| | | | | | | | | | | | | | |
|----|-------|--------|----|-------|----|--------|----|-------|----|-------|----|-------|----|
| 7 | 15 | -19.51 | 19 | -5.65 | 33 | -14.02 | 11 | 10.37 | 23 | -8.27 | 4 | 10.93 | 30 |
| 7 | 0.805 | -19.37 | 19 | -5.53 | 33 | -14.02 | 11 | 10.37 | 23 | -0.40 | 10 | 0.19 | 36 |
| 7 | 17 | -19.37 | 19 | -5.53 | 33 | -14.02 | 11 | 10.37 | 23 | -0.40 | 9 | 0.19 | 37 |
| 8 | 17 | 1.24 | 23 | 24.81 | 11 | -0.60 | 10 | 0.10 | 36 | -0.40 | 9 | 0.19 | 37 |
| 8 | 0.120 | 1.22 | 23 | 24.79 | 11 | -0.60 | 10 | 0.10 | 36 | -0.46 | 9 | 0.19 | 37 |
| 8 | 16 | 1.22 | 23 | 24.79 | 11 | -0.60 | 10 | 0.10 | 36 | -0.46 | 10 | 0.19 | 36 |
| 9 | 16 | -24.79 | 11 | -1.22 | 23 | -0.10 | 36 | 0.60 | 10 | -0.46 | 10 | 0.19 | 36 |
| 9 | 0.002 | -24.78 | 11 | -1.22 | 23 | -0.10 | 36 | 0.60 | 10 | -0.46 | 10 | 0.19 | 36 |
| 9 | 19 | -24.50 | 11 | -0.98 | 23 | -0.10 | 36 | 0.60 | 10 | -0.28 | 30 | 0.74 | 4 |
| 10 | 19 | -1.97 | 23 | 25.97 | 11 | -3.50 | 4 | 1.71 | 30 | -0.28 | 30 | 0.74 | 4 |
| 10 | 0.172 | -2.00 | 23 | 25.94 | 11 | -3.50 | 4 | 1.71 | 30 | -0.03 | 32 | 0.15 | 10 |
| 10 | 0.214 | -2.00 | 23 | 25.93 | 11 | -3.50 | 4 | 1.71 | 30 | -0.07 | 37 | 0.09 | 9 |
| 10 | 18 | -2.07 | 23 | 25.85 | 11 | -3.50 | 4 | 1.71 | 30 | -1.63 | 4 | 0.87 | 30 |
| 11 | 18 | -25.96 | 11 | 2.91 | 23 | -0.09 | 22 | 0.97 | 19 | -0.88 | 11 | 0.29 | 23 |
| 11 | 0.542 | -25.87 | 11 | 2.99 | 23 | -0.09 | 22 | 0.97 | 19 | -0.39 | 11 | 0.25 | 23 |
| 11 | 1.037 | -25.79 | 11 | 3.06 | 23 | -0.09 | 22 | 0.97 | 19 | -0.03 | 34 | 0.45 | 19 |
| 11 | 20 | -25.68 | 11 | 3.15 | 23 | -0.09 | 22 | 0.97 | 19 | -0.05 | 26 | 1.04 | 19 |
| 12 | 20 | -24.17 | 11 | 1.81 | 23 | -3.29 | 19 | 0.14 | 26 | -0.05 | 26 | 1.04 | 19 |
| 12 | 21 | -24.12 | 11 | 1.86 | 23 | -3.29 | 19 | 0.14 | 26 | 0.00 | 26 | 0.00 | 19 |
| 13 | 4 | -3.08 | 23 | 7.13 | 11 | -4.85 | 4 | 6.23 | 30 | -2.52 | 30 | 2.11 | 4 |
| 13 | 0.432 | -3.08 | 23 | 7.13 | 11 | -4.76 | 4 | 6.31 | 30 | -0.03 | 36 | 0.25 | 10 |
| 13 | 8 | -3.08 | 23 | 7.13 | 11 | -4.66 | 23 | 6.43 | 11 | -2.55 | 23 | 3.68 | 11 |
| 14 | 8 | -1.54 | 30 | 2.53 | 4 | -1.96 | 11 | 0.87 | 23 | -2.55 | 23 | 3.68 | 11 |
| 14 | 2.208 | -1.54 | 30 | 2.53 | 4 | -1.50 | 30 | 1.27 | 4 | -0.38 | 10 | -0.00 | 36 |
| 14 | 2.313 | -1.54 | 30 | 2.53 | 4 | -1.48 | 30 | 1.29 | 4 | -0.35 | 10 | -0.03 | 36 |
| 14 | 2.339 | -1.54 | 30 | 2.53 | 4 | -1.47 | 30 | 1.30 | 4 | -0.34 | 10 | -0.01 | 22 |
| 14 | 2.351 | -1.54 | 30 | 2.53 | 4 | -1.47 | 30 | 1.30 | 4 | -0.35 | 12 | -0.00 | 22 |
| 14 | 12 | -1.54 | 30 | 2.53 | 4 | -1.33 | 30 | 1.47 | 4 | -1.43 | 11 | 1.07 | 23 |
| 15 | 12 | -2.53 | 30 | 3.49 | 4 | -0.38 | 30 | 0.76 | 6 | -1.43 | 11 | 1.07 | 23 |
| 15 | 18 | -2.53 | 30 | 3.49 | 4 | -0.21 | 30 | 0.96 | 6 | -1.70 | 30 | 1.87 | 4 |
| 16 | 6 | -2.75 | 23 | 8.30 | 11 | -0.68 | 23 | 1.97 | 11 | 0.00 | 23 | 0.00 | 11 |
| 16 | 9 | -2.75 | 23 | 8.30 | 11 | -0.50 | 23 | 2.18 | 11 | -0.58 | 23 | 2.03 | 11 |
| 17 | 9 | -2.50 | 23 | 4.48 | 11 | -1.79 | 11 | -0.02 | 23 | -0.58 | 23 | 2.03 | 11 |
| 17 | 0.130 | -2.50 | 23 | 4.48 | 11 | -1.76 | 11 | 0.00 | 23 | -0.58 | 23 | 1.80 | 11 |
| 17 | 0.808 | -2.50 | 23 | 4.48 | 11 | -1.61 | 11 | 0.12 | 23 | -0.54 | 23 | 0.65 | 11 |
| 17 | 0.956 | -2.50 | 23 | 4.48 | 11 | -1.58 | 11 | 0.15 | 23 | -0.54 | 4 | 0.44 | 30 |
| 17 | 1.176 | -2.50 | 23 | 4.48 | 11 | -1.53 | 11 | 0.19 | 23 | -0.54 | 4 | 0.13 | 30 |
| 17 | 1.269 | -2.50 | 23 | 4.48 | 11 | -1.51 | 11 | 0.20 | 23 | -0.67 | 19 | -0.00 | 30 |
| 17 | 1.527 | -2.50 | 23 | 4.48 | 11 | -1.46 | 11 | 0.25 | 23 | -1.05 | 19 | -0.30 | 34 |
| 17 | 10 | -2.50 | 23 | 4.48 | 11 | -1.45 | 11 | 0.26 | 23 | -1.12 | 19 | -0.30 | 22 |
| 18 | 10 | -2.50 | 23 | 4.48 | 11 | -0.77 | 30 | 1.06 | 4 | -1.12 | 19 | -0.30 | 22 |
| 18 | 0.380 | -2.50 | 23 | 4.48 | 11 | -0.70 | 30 | 1.14 | 4 | -0.82 | 19 | -0.00 | 23 |
| 18 | 0.403 | -2.50 | 23 | 4.48 | 11 | -0.70 | 30 | 1.15 | 4 | -0.80 | 19 | 0.02 | 23 |
| 18 | 13 | -2.50 | 23 | 4.48 | 11 | -0.49 | 30 | 1.39 | 4 | -1.41 | 30 | 1.42 | 4 |
| 19 | 13 | -0.20 | 22 | 4.27 | 19 | -1.56 | 4 | 1.36 | 30 | -1.41 | 30 | 1.42 | 4 |
| 19 | 20 | -0.20 | 22 | 4.27 | 19 | -1.36 | 4 | 1.53 | 30 | 0.00 | 30 | 0.00 | 4 |
| 20 | 17 | -10.96 | 23 | 15.14 | 11 | -7.57 | 4 | 9.79 | 30 | 0.00 | 4 | 0.00 | 30 |
| 20 | 22 | -10.96 | 23 | 15.14 | 11 | -7.41 | 23 | 9.95 | 11 | -6.05 | 4 | 7.98 | 30 |
| 21 | 22 | -7.10 | 30 | 5.64 | 4 | -12.12 | 11 | 9.19 | 23 | -6.05 | 4 | 7.98 | 30 |
| 21 | 0.600 | -7.10 | 30 | 5.64 | 4 | -12.00 | 30 | 9.30 | 4 | -0.51 | 4 | 0.75 | 30 |
| 21 | 0.687 | -7.10 | 30 | 5.64 | 4 | -11.98 | 30 | 9.32 | 4 | -0.34 | 10 | 0.53 | 36 |
| 21 | 23 | -7.10 | 30 | 5.64 | 4 | -11.87 | 30 | 9.46 | 4 | -8.00 | 30 | 6.36 | 4 |
| 22 | 23 | -28.74 | 30 | 23.16 | 4 | -7.95 | 4 | 9.82 | 30 | -8.00 | 30 | 6.36 | 4 |
| 22 | 26 | -28.74 | 30 | 23.16 | 4 | -7.78 | 4 | 9.96 | 30 | 0.00 | 30 | 0.00 | 4 |
| 23 | 24 | -18.86 | 4 | 10.26 | 30 | -7.53 | 4 | 10.16 | 30 | 0.00 | 4 | 0.00 | 30 |
| 23 | 25 | -18.64 | 4 | 10.45 | 30 | -4.71 | 4 | 5.73 | 30 | -8.20 | 4 | 10.65 | 30 |
| 24 | 25 | -11.85 | 11 | 0.28 | 37 | -15.91 | 30 | 12.81 | 4 | -8.20 | 4 | 10.65 | 30 |
| 24 | 0.646 | -11.74 | 11 | 0.37 | 37 | -18.04 | 30 | 14.17 | 4 | -0.45 | 29 | 0.97 | 17 |
| 24 | 26 | -11.71 | 11 | 0.39 | 37 | -18.58 | 30 | 14.51 | 4 | -3.28 | 30 | 2.84 | 4 |
| 25 | 26 | -9.25 | 3 | 0.14 | 33 | -8.65 | 4 | 10.16 | 30 | -3.28 | 30 | 2.84 | 4 |
| 25 | 27 | -9.19 | 3 | 0.19 | 33 | -7.93 | 4 | 9.03 | 30 | 0.00 | 30 | 0.00 | 4 |

| | | | | | | | | | | | | | |
|----|-------|--------|----|-------|----|-------|----|-------|----|-------|----|-------|----|
| 26 | 10 | -2.17 | 19 | -0.43 | 34 | 0.00 | 11 | 0.00 | 23 | 0.00 | 11 | 0.00 | 23 |
| 26 | 11 | -1.75 | 19 | -0.08 | 34 | 0.00 | 11 | 0.00 | 23 | 0.00 | 11 | 0.00 | 23 |
| 27 | 1 | 0.00 | 23 | 0.00 | 19 | 0.00 | 33 | 0.00 | 7 | 0.00 | 33 | 0.00 | 7 |
| 27 | 7 | 0.66 | 23 | 1.43 | 19 | 0.22 | 33 | 2.45 | 7 | 0.08 | 33 | 0.87 | 7 |
| 28 | 7 | -8.89 | 19 | -1.72 | 25 | -7.11 | 7 | 0.64 | 33 | 0.08 | 32 | 0.87 | 8 |
| 28 | 0.043 | -8.81 | 19 | -1.68 | 25 | -6.92 | 7 | 0.63 | 33 | -0.00 | 32 | 0.68 | 8 |
| 28 | 0.160 | -8.57 | 19 | -1.57 | 25 | -6.42 | 7 | 0.59 | 33 | -0.26 | 5 | 0.18 | 27 |
| 28 | 1.666 | -6.89 | 15 | -0.18 | 25 | -0.18 | 19 | 0.08 | 33 | -5.03 | 3 | 0.71 | 31 |
| 28 | 1.708 | -6.85 | 15 | -0.14 | 25 | -0.10 | 10 | 0.11 | 32 | -5.03 | 3 | 0.72 | 31 |
| 28 | 1.790 | -6.75 | 15 | -0.07 | 25 | -0.07 | 29 | 0.31 | 3 | -5.02 | 3 | 0.72 | 31 |
| 28 | 1.869 | -6.67 | 15 | 0.00 | 25 | -0.05 | 29 | 0.62 | 3 | -4.98 | 3 | 0.72 | 31 |
| 28 | 11 | -5.05 | 15 | 1.35 | 25 | -0.93 | 31 | 6.20 | 3 | 0.00 | 3 | -0.00 | 31 |
| 29 | 11 | -6.52 | 7 | 1.32 | 33 | -4.49 | 11 | 0.70 | 23 | 0.00 | 11 | 0.00 | 23 |
| 29 | 1.135 | -7.78 | 7 | 0.27 | 33 | -0.15 | 11 | 0.02 | 23 | -2.63 | 11 | 0.41 | 23 |
| 29 | 1.162 | -7.81 | 7 | 0.24 | 33 | -0.08 | 9 | 0.02 | 37 | -2.64 | 11 | 0.41 | 23 |
| 29 | 1.174 | -7.82 | 7 | 0.23 | 33 | -0.05 | 9 | 0.03 | 37 | -2.64 | 11 | 0.41 | 23 |
| 29 | 1.208 | -7.86 | 7 | 0.20 | 33 | -0.03 | 29 | 0.13 | 15 | -2.64 | 11 | 0.40 | 23 |
| 29 | 2.300 | -9.07 | 7 | -0.81 | 33 | -0.55 | 25 | 4.31 | 15 | -0.25 | 9 | 0.05 | 23 |
| 29 | 2.456 | -9.25 | 7 | -0.95 | 33 | -0.60 | 25 | 4.91 | 15 | -0.05 | 29 | 0.51 | 15 |
| 29 | 21 | -10.20 | 7 | -1.75 | 33 | -0.86 | 25 | 8.21 | 15 | -0.68 | 25 | 6.17 | 15 |
| 30 | 21 | -6.88 | 23 | 10.84 | 11 | -8.99 | 15 | 0.87 | 25 | -0.68 | 25 | 6.17 | 15 |
| 30 | 0.833 | -7.65 | 23 | 9.91 | 11 | -5.80 | 15 | 0.62 | 25 | -0.05 | 25 | 0.05 | 19 |
| 30 | 0.890 | -7.70 | 23 | 9.85 | 11 | -5.58 | 15 | 0.61 | 25 | -0.31 | 11 | -0.00 | 27 |
| 30 | 0.902 | -7.71 | 23 | 9.84 | 11 | -5.54 | 15 | 0.60 | 25 | -0.38 | 11 | -0.01 | 27 |
| 30 | 0.912 | -7.72 | 23 | 9.83 | 11 | -5.50 | 15 | 0.60 | 25 | -0.44 | 11 | 0.00 | 23 |
| 30 | 2.291 | -9.10 | 4 | 8.40 | 30 | -0.23 | 34 | 0.19 | 6 | -4.38 | 11 | 0.54 | 23 |
| 30 | 2.349 | -9.17 | 4 | 8.35 | 30 | -0.09 | 37 | 0.24 | 9 | -4.39 | 11 | 0.55 | 23 |
| 30 | 2.843 | -9.72 | 4 | 7.89 | 30 | 0.02 | 37 | 1.96 | 11 | -3.91 | 11 | 0.60 | 23 |
| 30 | 2.906 | -9.79 | 4 | 7.84 | 30 | 0.00 | 23 | 2.23 | 11 | -3.78 | 11 | 0.60 | 23 |
| 30 | 3.680 | -10.64 | 4 | 7.12 | 30 | -0.23 | 23 | 5.58 | 11 | -0.83 | 13 | 0.51 | 23 |
| 30 | 27 | -10.83 | 4 | 6.96 | 30 | -0.28 | 23 | 6.32 | 11 | -0.46 | 32 | 0.72 | 8 |
| 31 | 27 | 0.66 | 31 | 1.43 | 19 | -2.02 | 8 | 1.28 | 32 | -0.46 | 32 | 0.72 | 8 |
| 31 | 28 | 0.00 | 31 | 0.00 | 19 | 0.00 | 8 | 0.00 | 32 | 0.00 | 32 | 0.00 | 8 |
| 32 | 3 | -12.09 | 11 | 7.65 | 23 | -0.08 | 1 | -0.06 | 2 | 0.00 | 1 | 0.00 | 2 |
| 32 | 0.689 | -12.02 | 11 | 7.71 | 23 | 0.00 | 1 | 0.00 | 2 | -0.03 | 1 | -0.02 | 2 |
| 32 | 8 | -11.95 | 11 | 7.77 | 23 | 0.06 | 2 | 0.08 | 1 | 0.00 | 1 | 0.00 | 2 |
| 33 | 5 | -5.65 | 11 | 0.40 | 23 | -0.26 | 11 | 0.04 | 25 | -0.14 | 6 | 0.26 | 30 |
| 33 | 9 | -5.50 | 11 | 0.52 | 23 | -0.13 | 30 | 0.18 | 6 | 0.00 | 6 | 0.00 | 30 |
| 34 | 17 | -1.34 | 4 | 1.27 | 30 | 0.06 | 2 | 0.08 | 1 | 0.00 | 2 | 0.00 | 1 |
| 34 | 0.647 | -1.28 | 23 | 1.32 | 11 | 0.00 | 2 | 0.00 | 1 | 0.02 | 2 | 0.03 | 1 |
| 34 | 12 | -1.22 | 23 | 1.39 | 11 | -0.08 | 1 | -0.06 | 2 | 0.00 | 2 | 0.00 | 1 |
| 35 | 19 | -4.41 | 4 | 2.43 | 30 | 0.06 | 2 | 0.08 | 1 | 0.00 | 2 | 0.00 | 1 |
| 35 | 0.689 | -4.34 | 4 | 2.49 | 30 | 0.00 | 2 | 0.00 | 1 | 0.02 | 2 | 0.03 | 1 |
| 35 | 13 | -4.26 | 4 | 2.55 | 30 | -0.08 | 1 | -0.06 | 2 | 0.00 | 2 | 0.00 | 1 |
| 36 | 15 | -31.40 | 11 | 23.33 | 23 | -0.07 | 1 | -0.05 | 2 | 0.00 | 1 | 0.00 | 2 |
| 36 | 0.572 | -31.34 | 11 | 23.38 | 23 | 0.00 | 1 | 0.00 | 2 | -0.02 | 1 | -0.01 | 2 |
| 36 | 22 | -31.28 | 11 | 23.43 | 23 | 0.05 | 2 | 0.07 | 1 | 0.00 | 1 | 0.00 | 2 |
| 37 | 25 | -24.82 | 4 | 30.53 | 30 | 0.05 | 2 | 0.07 | 1 | 0.00 | 2 | 0.00 | 1 |
| 37 | 0.572 | -24.76 | 4 | 30.59 | 30 | 0.00 | 2 | 0.00 | 1 | 0.01 | 2 | 0.02 | 1 |
| 37 | 23 | -24.70 | 4 | 30.64 | 30 | -0.07 | 1 | -0.05 | 2 | 0.00 | 2 | 0.00 | 1 |

REACTIES

| Kn. | X-min | X-max | Z-min | Z-max | M-min | M-max |
|-----|-------|-------|--------|-------|-------|-------|
| 2 | -1.51 | 2.23 | 3.91 | 15.04 | | |
| 14 | -6.17 | 8.15 | -6.44 | 36.86 | | |
| 24 | -7.53 | 10.16 | -10.26 | 18.86 | | |

Fundamentele combinatie

Controle maatgevende onderdelen:**Kolom staaf 6**

BEREKENING KOLOMMEN : Versie : 001
 staaf gesteund aan druk-zijde.

Basisgegevens:

Klimaatklasse = 2
 Belastingduurklasse = 3
 gamma_ugt = 1.20 , k_mod = 0.85

Gegevens hout:

Hoogte * Breedte = 200*200 mm²
 met $k_h = 1.00$ (alleen voor f_m)
 Sterkteklasse = C20
 $f_{ud} = k_h * k_{mod} * (f_{rep} / \gamma_m)$ N/mm²

| | | | f_{rep} | f_{ud} |
|---------------|------------|---|-----------|------------------------|
| Buigsterkte | f_{m0} | : | 20.0 | 14.2 N/mm ² |
| Druksterkte | f_{c0} | : | 19.0 | 13.5 |
| Druksterkte | f_{c90} | : | 2.3 | 1.6 |
| Schuifsterkte | f_{v0} | : | 2.2 | 1.6 |
| Elast.mod. | E_{0ser} | : | 9500 | 6729 |
| Elast.mod. | E_{0u} | : | 6400 | 4533 |
| Afschuifmod. | G_{ser} | : | 590 | 418 |

Statische gegevens hout

Doorsnede opp. : 40000 mm²
 Traagh.mom. I_y : 133333333 mm⁴
 Traagh.mom. I_z : 133333333 mm⁴
 Torsie.moment : 225066667 mm⁴
 Welvingsfactor : 400000000E3 (= Cw)

Geometrische gegevens + Belastingen

Kniklengte l_y : 2200 mm1
 Kniklengte l_z : 2200 mm1
 Normalkracht : 36.63 kN
 Moment links : 0.00 kNm
 Moment rechts : 0.00 kNm
 Belasting qd : 0.00 kN/m
 Puntlast F_d : 21.40 kN
 op afstand : 1400 mm1

Uitvoergegevens knikberekening

$k_{mom} = 1.00$, $k_{com} = 0.82$
 $uc_{Y;d} = 0.56$, $uc_{Z;d} = 0.49$

Uitvoergegevens spanningen

met $M_{midden} = 10.89$ kNm
 tgv. $M_{max} = 10.89$ kNm : $uc_S = 0.64$

Uitvoergegevens oplegging/dwarskracht

tgv. $D_{max} = 13.62$ kN : $uc_V = 0.33$
 min. opl.lengte : links = 24 mm , rechts = 42 mm

Ligger staaf 30

BEREKENING LIGGER : Versie : 001
 staaf gesteund aan druk-zijde.

Basisgegevens:

Klimaatklasse = 2
 Belastingduurklasse = 3
 $\gamma_{ugt} = 1.20$, $k_{mod} = 0.85$

Gegevens hout:

Hoogte * Breedte = 200*200 mm²
 met $k_h = 1.00$ (alleen voor f_m)
 Sterkteklasse = C20
 $f_{ud} = k_h * k_{mod} * (f_{rep} / \gamma_m)$ N/mm²

| | | | f_{rep} | f_{ud} |
|---------------|------------|---|-----------|------------------------|
| Buigsterkte | f_{m0} | : | 20.0 | 14.2 N/mm ² |
| Druksterkte | f_{c0} | : | 19.0 | 13.5 |
| Druksterkte | f_{c90} | : | 2.3 | 1.6 |
| Schuifsterkte | f_{v0} | : | 2.2 | 1.6 |
| Elast.mod. | E_{0ser} | : | 9500 | 6729 |
| Elast.mod. | E_{0u} | : | 6400 | 4533 |
| Afschuifmod. | G_{ser} | : | 590 | 418 |

Statische gegevens hout

Doorsnede opp. : 40000 mm²
 Traagh.mom. I_y : 133333333 mm⁴
 Traagh.mom. I_z : 133333333 mm⁴
 Torsie.moment : 225066667 mm⁴
 Welvingsfactor : 400000000E3 (= Cw)

Geometrische gegevens + Belastingen

Kniklengte l_y : 3850 mm1
 Kniklengte l_z : 1925 mm1
 Normalkracht : 8.99 kN

Moment links : -6.17 kNm
 Moment rechts : 0.00 kNm
 Belasting qd : 1.50 kN/m
 Puntlast Fd : 0.00 kN
 op afstand : 0 mm1

Uitvoergegevens knikberekening
 k_{mom} = 0.99 , k_{com} = 0.50
 uc_{Y;d} = 0.24 , uc_{Z;d} = 0.21

Uitvoergegevens spanningen
 met M_{midden} = 0.55 kNm
 tgv. M_{max} = 6.17 kNm : uc_S = 0.34

Uitvoergegevens oplegging/dwarskracht
 tgv. D_{max} = 4.49 kN : uc_V = 0.11
 min. opl.lengte : links = 16 mm , rechts = 4 mm

Verbindingen:

Voor C20 geldt: $f_{c;90;d} = 2 * 0.85 * 2.3 / 1.2 = 3.26 \text{ N/mm}^2$
 $f_{c;0;d} = 0.85 * 19.0 / 1.2 = 13.46 \text{ N/mm}^2$
 $f_{v;d} = 0.85 * 2.3 / 1.2 = 1.63 \text{ N/mm}^2$

Voor eikenhouten doken: $f_{v;d} = 0.85 * 2.5 / 1.2 = 1.77 \text{ N/mm}^2$

Doorsnede dook: $\frac{1}{4} * \pi * 22^2 = 380 \text{ mm}^2$

Afschuifvlak $2 * 380 = 760 \text{ mm}^2$

Op te nemen door eikenhouten dook: $760 * 1.77 = 1.35 \text{ kN}$

Door de taaiheid van de dook en de elasticiteit van het naastliggende hout zal er geen scherpe afschuiving plaats vinden.

Stiften ø22

VERBINDINGEN MET STALEN STIFTVORMIGE VERBINDINGSMIDDELEN
 Volgens : NEN-EN 1995-1-1, EC5 , Artikel.8
 Versie : VerbWinEC5 2013-02 , Rel.130701

UITVOER-GEDEEVENS van Stift:
 diameter = 22.0 mm¹
 lengte = 200.0 mm¹ , excl. afschuining
 f_{u;Rk} = 285 N/mm² , BlankAssenStaal
 M_{y;Rk} = 264.40 * 10³ Nmm = 0.3 * f_{u;Rk} * d^{2.6}

MODIFICATIE-FACTOREN:
 k_{mod} = 0.80 , gamma_M = 1.30
 Klimaatklasse 2 = Relatieve vochtigheid : >65% <80%
 Belastingsduur : Klasse III (kort)

BEREKENING SNEDEKRACHT:
 Dubbel-snedig. Opbouw = H.H.H
 Afmetingen : 70.0 + 60.0 + 70.0

| materiaal | rho _k [kg/m ³] | alfa [°] | f _{h;i;k} [N/mm ²] | t _i [mm ¹] |
|---|---------------------------------------|----------|---|-----------------------------------|
| 1 = C20 | 330 | 0.0 | 21.11 | 70.0 |
| 2 = C18 | 320 | 0.0 | 20.47 | 60.0 |
| 3 = C20 | 330 | 0.0 | 21.11 | 70.0 |
| beta = f _{emb;rep;2} / f _{emb;rep;1/3} = 0.97 | | | | |

SNEDEKRACHT , exclusief koordwerking (-K):
 F_{v;Rk} = volgens artikel 8.2.2
 F_{v;Rk} = 32504 N (8.7g) F_{v;Rk} = 14958 N (8.7h)
 = 13508 " (8.7i-K) = 17881 " (8.7k-K)

KOORDWERKING: Artikel 12.6.7
 F_{ax;Rk} = N.V.T.
 Geen koordwerking
 F_{ax;Rk} = 0 N , met 1/4 F_{ax;Rk} = 0 N

SNEDEKRACHT , inclusief koordwerking:
 Stift => Aandeel 1/4 F_{ax;Rk} max. 0% van F_{ax;Rk}(Form-K)

F_{v;Rk} = volgens artikel 8.2.2
 F_{v;Rk} = 32504 N (8.7g) F_{v;Rk} = 14958 N (8.7j+K)
 = 13508 " (8.7h) = 17881 " (8.7k+K)

REKENWAARDE SNEDEKRACHT , inclusief koordwerking:

$$\begin{aligned}
 F_{v;Rk} &= 13508 \text{ N} \\
 F_{v;Rd} &= n_{ef} * (k_{mod} * F_{v;Rk} / \gamma_M) \\
 &= n_{ef} * 1.00 * (0.80 * 13508 / 1.30) \\
 &= n_{ef} * 1.00 * 8313 \\
 &= n_{ef} * 8313 \text{ N per Snede}
 \end{aligned}$$

$$n_{ef} = (a_0/13d)^{1/4} * (n^{0.9}/n) \quad (8.5.1.1(4) , \text{Form.8.34})$$

EIND,RAND,TUSSEN-AFSTANDEN: Artikel 8.6 , Tabel 8.5

$$\begin{aligned}
 a_{3t} > 7 * d_{nom} &= 154 & a_{3c} > 3 * d_{nom} &= 66 \\
 a_{4t} > 4 * d_{nom} &= 88 & a_{4c} > 3 * d_{nom} &= 66 \\
 a_1 > 5 * d_{nom} &= 110 & a_2 > 3 * d_{nom} &= 66
 \end{aligned}$$

Voor rechthoekig patroon!

Knoop zijkolommen en vloerligger knoop 26

Max schuifkracht van ligger op kolom: 9.96 kN
 Maximale drukkracht ligger op kolom: 28.74 kN
 Maximale trekkracht ligger op kolom: 23.16 kN

Controle oppervlak: $28.74 * 10^3 / 200 * 200 = 0.72 < 3.26 \text{ N/mm}^2$
 Controle pen op afschuiving: $9.96 * 10^3 / 60 * 200 = 0.83 < 1.63 \text{ N/mm}^2$

Knoop Korbelen

Max drukkracht in korbeel : 24.70 kN
 Max trekkracht in korbeel : 30.60 kN

Maximale schuifkracht korbeel: $30.60 * \cos 45 = 21.63 \text{ kN}$

$$f_{v;45;d} = \sqrt{(1.63^2 + 3.26^2)} = 3.64 \text{ N/mm}^2$$

Controle pen op afschuiving: $21.63 * 10^3 / 60 * 200 = 1.80 < 3.64 \text{ N/mm}^2$

Controle pen op trek: 2 stiften $\varnothing 22$ Opneembaar // vezelrichting 8.3 kN per snede
 Opneembaar 45 vezelrichting 7.8 kN per snede

Opneembaar: // $2 * 2 * 8.3 = 33.2 \text{ kN}$
 Opneembaar: 45 graden $2 * 2 * 7.8 = 31.2 \text{ kN}$


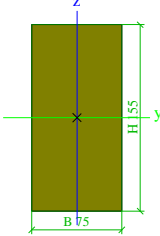
Gordingen:

Gordingen hoh 1.63 m Dakhelling 40 graden
 Strip over gordingen aanbrengen van nok tot laatse gording boven goot

1. Project


| | |
|---|---------------|
| Licentiernaam | Onbekend |
| Project | Meulenbrugge- |
| Onderdeel | Gording- |
| Omschrijving | - |
| Auteur | POD |
| Datum | 04. 10. 2018 |
| Constructie | Algemeen XYZ |
| Aantal knopen : | 2 |
| Aantal staven : | 1 |
| Aantal platen : | 0 |
| Aantal vaste lichamen : | 0 |
| Aantal gebruikte doorsneden : | 1 |
| Aantal belastingsgevallen : | 4 |
| Aantal gebruikte materialen : | 1 |
| Gravitatieversnelling [m/s ²] | 9,810 |
| Nationale norm | EC - EN |

2. Doorsneden

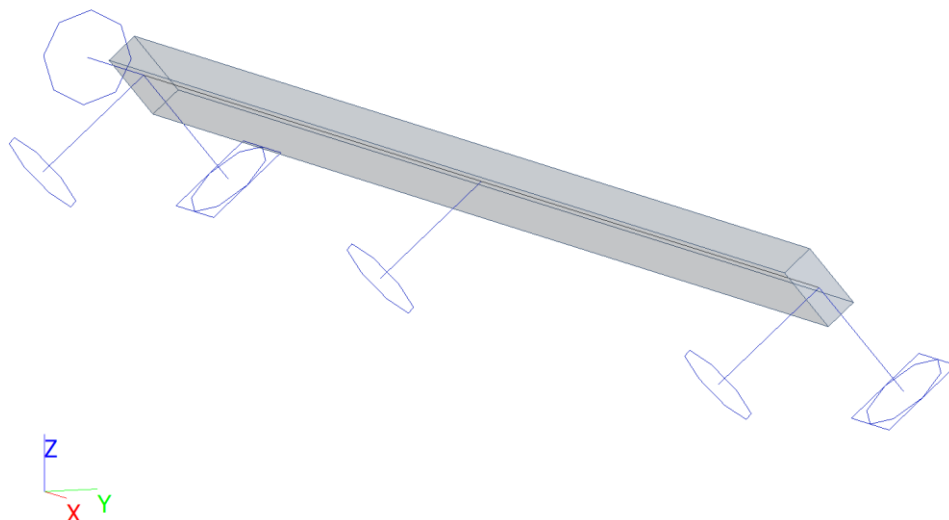
| CS2 | | |
|--|--|------------|
| Type | RECT | |
| Uitgebreid | 75; 155 | |
| Vorm type | Dikke wanden | |
| Onderdeelmateriaal | C20 (EN 338) | |
| Bouwwijze | hout | |
| Kleur |  | |
| A [m ²] | 1,1625e-02 | |
| A _y [m ²], A _z [m ²] | 9,7112e-03 | 9,6931e-03 |
| A _L [m ² /m], A _D [m ² /m] | 4,6000e-01 | 4,6000e-01 |
| C _{Y,UCS} [mm], C _{Z,UCS} [mm] | 38 | 78 |
| α [deg] | 0,00 | |
| I _y [m ⁴], I _z [m ⁴] | 2,3274e-05 | 5,4492e-06 |
| i _y [mm], i _z [mm] | 45 | 22 |
| W _{el,y} [m ³], W _{el,z} [m ³] | 3,0031e-04 | 1,4531e-04 |
| W _{pl,y} [m ³], W _{pl,z} [m ³] | 3,3970e-04 | 1,6437e-04 |
| M _{pl,y,+} [Nm], M _{pl,y,-} [Nm] | 6,45e+03 | 6,45e+03 |
| M _{pl,z,+} [Nm], M _{pl,z,-} [Nm] | 3,12e+03 | 3,12e+03 |
| d _y [mm], d _z [mm] | 0 | 0 |
| I _t [m ⁴], I _w [m ⁶] | 1,5142e-05 | 4,1998e-09 |
| β _y [mm], β _z [mm] | 0 | 0 |
| Afbeelding |  | |

3. Materialen

Hout EC5

| Naam | Houtsoort | μ | E _{mod} [MPa] | f _{m,k} [MPa] | f _{t,0,k} [MPa] | f _{t,90,k} [MPa] | f _{c,0,k} [MPa] | f _{c,90,k} [MPa] | f _{v,k} [MPa] | Kleur |
|--------------|------------------------|----------|------------------------|------------------------|--------------------------|---------------------------|--------------------------|---------------------------|------------------------|---|
| | ρ [kg/m ³] | α [m/mK] | G _{mod} [MPa] | | | | | | | |
| C20 (EN 338) | Vast | 0 | 9,5000e+03 | 20,0 | 11,5 | 0,4 | 19,0 | 2,3 | 3,6 |  |
| | 400,0 | 0,00 | 5,9000e+02 | | | | | | | |

4. Rekenmodel



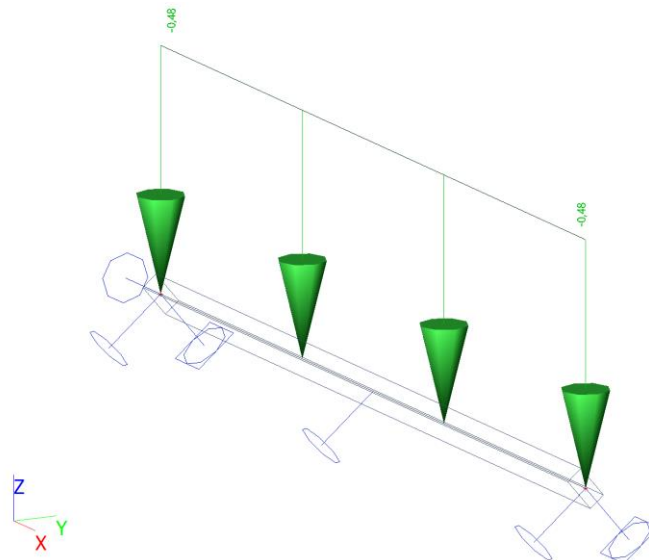
5. Belastingsgevallen

| Naam | Omschrijving | Actie type | Lastgroep | Richting | Duur | 'Master' belastingsgeval |
|------|--------------------------------------|----------------------------|-----------|----------|------|--------------------------|
| | Spec | Belastingtype | | | | |
| BG1 | Eigen gewicht | Permanent Eigen gewicht | LG1 | -Z | | |
| BG2 | Permanente belasting | Permanent Standaard | LG1 | | | |
| BG3 | Veranderlijke belasting Standaard | Variabel Statisch | LG2 | | Kort | Geen |
| BG4 | Wind Standaard | Variabel Statisch | LG3 | | Kort | Geen |

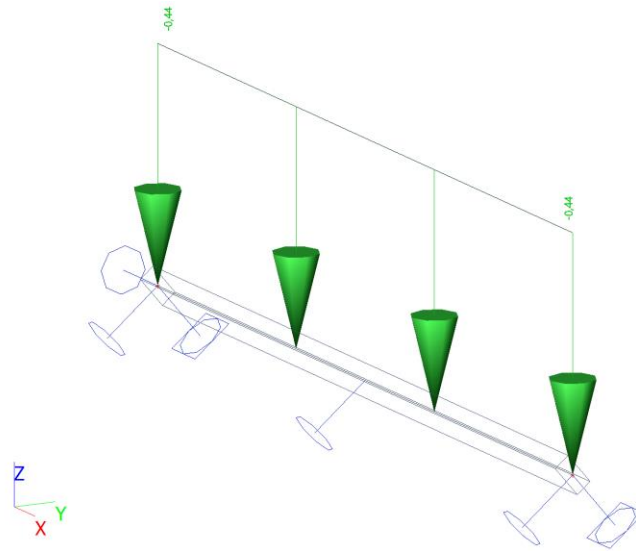
6. Lijnlast

| Naam | StAAF | Type | Rich | Waarde - P ₁ [kN/m] | Pos x ₁ | Coör | Oors | Exc ey [m] |
|-----------|-------------------------------------|---------------|------------------|-----------------------------------|--------------------|----------------|-------------|----------------|
| | Belastingsgeval | Systeem | Verdeling | Waarde - P ₂ [kN/m] | Pos x ₂ | Loc | | Exc ez [m] |
| Lijnlast1 | S1 BG2 - Permanente belasting | Kracht GCS | Z Gelijkmatig | -0,48 | 0.000 1.000 | Rela Lengte | Vanaf begin | 0,000 0,000 |
| Lijnlast2 | S1 BG3 - Veranderlijke belasting | Kracht GCS | Z Gelijkmatig | -0,44 | 0.000 1.000 | Rela Lengte | Vanaf begin | 0,000 0,000 |
| Lijnlast4 | S1 BG4 - Wind | Kracht LCS | Z Gelijkmatig | -0,95 | 0.000 1.000 | Rela Lengte | Vanaf begin | 0,000 0,000 |

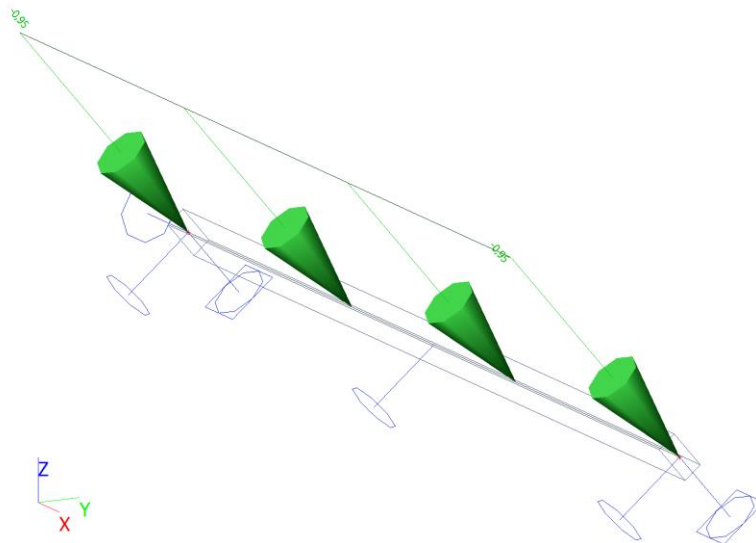
7. BG2 /Permanent



8. BG3 / Veranderlijk



9. BG4 / Wind



10. Belastinggroepen

| Naam | Last | Relatie | Type |
|------|-----------|-----------|---------------|
| LG1 | Permanent | | |
| LG2 | Variabel | Standaard | Cat A: Woning |
| LG3 | Variabel | Standaard | Cat A: Woning |

11. Combinaties

| Naam | Omschrijving | Type | Belastingsgevallen | Coëff. [-] |
|-------------------------|--------------|-------------------------|-------------------------------|------------|
| UGT-Set B (automatisch) | | EN-UGT (STR/GEO) Set B | BG1 - Eigen gewicht | 1,00 |
| | | | BG2 - Permanente belasting | 1,00 |
| | | | BG3 - Veranderlijke belasting | 1,00 |
| | | | BG4 - Wind | 1,00 |
| BGT-kar (automatisch) | | EN - BGT Karakteristiek | BG1 - Eigen gewicht | 1,00 |
| | | | BG2 - Permanente belasting | 1,00 |
| | | | BG3 - Veranderlijke belasting | 1,00 |
| | | | BG4 - Wind | 1,00 |

12. Resultaatklassen

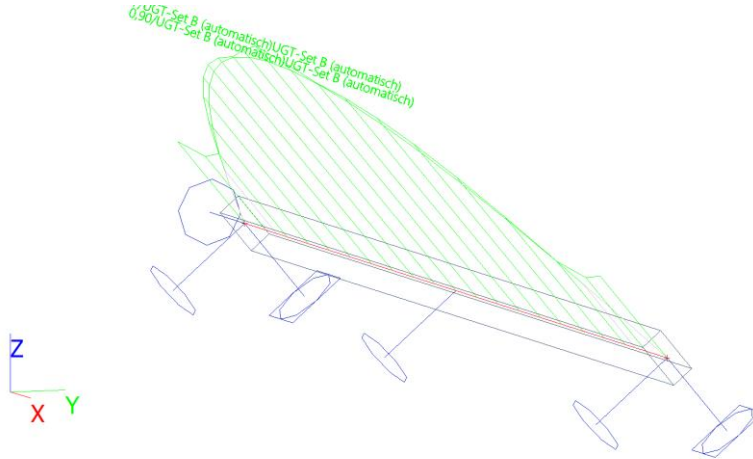
| Naam | Lijst |
|--------------|---|
| Alle UGT | UGT-Set B (automatisch) - EN-UGT (STR/GEO) Set B |
| Alle BGT | BGT-kar (automatisch) - EN - BGT Karakteristiek |
| Alle UGT+BGT | UGT-Set B (automatisch) - EN-UGT (STR/GEO) Set B BGT-kar (automatisch) - EN - BGT Karakteristiek |

| Naam | Lijst |
|------|--|
| GEO | UGT-Set B (automatisch) - EN-UGT (STR/GEO) Set B |

13. Staven

| Naam | Doorsnede | Materiaal | Lengte [m] | Beginknoop | Eindknoop | Type |
|------|----------------------|--------------|------------|------------|-----------|--------------|
| S1 | CS2 - RECT (75; 155) | C20 (EN 338) | 3,600 | K1 | K2 | Algemeen (0) |

14. Hout UGT controle; Eenheidscontrole, Doorsnedecontrole, Stabiliteitscontrole

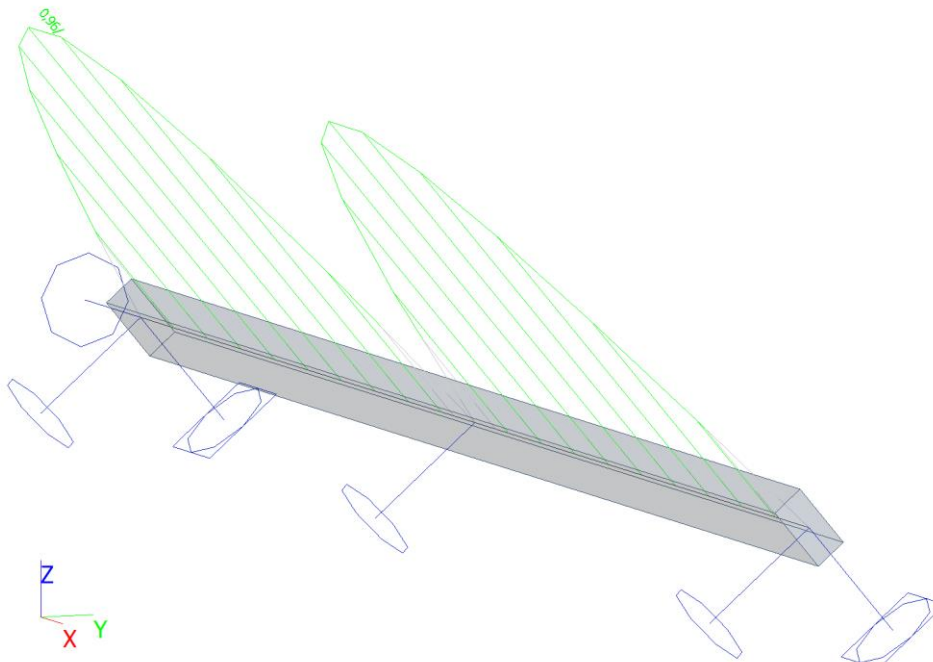


16. Hout BGT controle

Lineaire berekening, Extreem : Globaal
Selectie : Alle
Belastingsgevallen : BG1

| Staf | Doorsnede | dx [m] | Belastingsgeval | Eenheidscontrole [-] | uy inst [mm] | Rel uy inst [1/xx] | Controleer uy inst [-] | uy fin [mm] | Rel uy fin [1/xx] | Controleer uy fin [-] |
|------|--------------|--------|-----------------|----------------------|--------------|--------------------|------------------------|-------------|-------------------|-----------------------|
| | Materiaal | | k_{def} [-] | | uz inst [mm] | Rel uz inst [1/xx] | Controleer uz inst [-] | uz fin [mm] | Rel uz fin [1/xx] | Controleer uz fin [-] |
| S1 | CS2 - RECT | 1,080 | BG1 | 0,02 | 0,0 | 1/10000 | 0,00 | 0,0 | 1/10000 | 0,00 |
| | C20 (EN 338) | | 0,60 | | -0,1 | 1/10000 | 0,02 | -0,1 | 1/10000 | 0,02 |

17. Hout BGT controle; Eenheidscontrole



Stabiliteit loodrecht op spant

Het oppervlak van de kopgevel is : 43.6 m²

Totale winddruk op te nemen door wanden:

| | | |
|-----------------------|--|------------|
| Uit kopgevel voor: | $(0.8 + 0.4) * 0.62 * 43.6$ | = 32.43 kN |
| Uit kopgevel achterl | $(0.8 + 0.4) * 0.62 * 43.6$ | = 32.43 kN |
| Wrijving dak + wanden | $0.02 * (2.00 + 7.98 + 4.10) * 0.62 * 21.80$ | = 3.80 kN |

Hiervan gaat de helft van het onderste deel rechtstreeks naar de fundering.

Op te nemen door schoren: $(32.43 + 32.43 + 3.80) * 0.75 = 51.50$ kN

Op te nemen door 2 rijen schoren. Per rij = 25.75 kN

Technosoft Raamwerken release 6.16

5 okt 2018

Dimensies: kN;m;rad (tenzij anders aangegeven)

Datum....: 05/10/2018

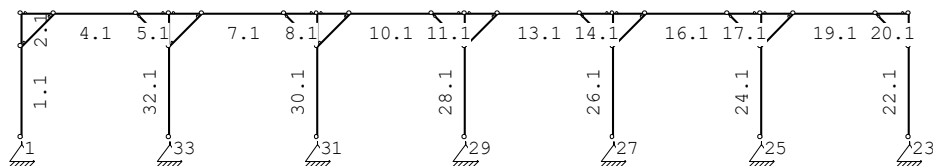
Theorie voor de bepaling van de krachtsverdeling: Geometrisch lineair.

Gunstige werking van de permanente belasting wordt automatisch verwerkt.

Toegepaste normen volgens Eurocode met Nederlandse NB

| | | | |
|-------------|----------------------|---------|--------------|
| Belastingen | NEN-EN 1990:2002 | C2:2010 | NB:2011 (nl) |
| | NEN-EN 1991-1-1:2002 | C1:2009 | NB:2011 (nl) |

GEOMETRIE



MATERIALEN

| Mt | Omschrijving | E-modulus [N/mm ²] | S.M. | S.M.verhoogd | Pois. | Uitz. coëff |
|----|--------------|--------------------------------|------|--------------|-------|-------------|
|----|--------------|--------------------------------|------|--------------|-------|-------------|

| | | | | | | |
|---|-----|------|-----|-----|------|------------|
| 1 | C18 | 9000 | 3.2 | 3.8 | 1.00 | 5.0000e-06 |
|---|-----|------|-----|-----|------|------------|

Bij de bepaling v.h. e.g. van houten staven is de S.M.verhoogd toegepast.

PROFIELEN [mm]

| Prof. | Omschrijving | Materiaal | Oppervlak | Traagheid | Vormf. |
|-------|--------------|-----------|------------|------------|--------|
| 1 | B*H 200*200 | 1:C18 | 4.0000e+04 | 1.3333e+08 | 0.00 |
| 2 | B*H 150*200 | 1:C18 | 3.0000e+04 | 1.0000e+08 | 0.00 |

PROFIELEN vervolg [mm]

| Prof. | Staaftype | Breedte | Hoogte | e | Type | b1 | h1 | b2 | h2 |
|-------|-----------|---------|--------|-------|------|----|----|----|----|
| 1 | 0:Normaal | 200 | 200 | 100.0 | 0:RH | | | | |
| 2 | 0:Normaal | 150 | 200 | 100.0 | 0:RH | | | | |

PROFIELVORMEN [mm]

1 B*H 200*200



2 B*H 150*200



KNOPEN

| Knoop | X | Z | Knoop | X | Z |
|-------|-------|-------|-------|-------|-------|
| 1 | 0.000 | 0.000 | 6 | 3.600 | 3.000 |
| 2 | 0.000 | 2.200 | 7 | 4.400 | 3.000 |
| 3 | 0.000 | 3.000 | 8 | 6.400 | 3.000 |
| 4 | 0.800 | 3.000 | 9 | 7.200 | 3.000 |
| 5 | 2.800 | 3.000 | 10 | 8.000 | 3.000 |

| | | | | | |
|----|--------|-------|----|--------|-------|
| 11 | 10.000 | 3.000 | 16 | 15.200 | 3.000 |
| 12 | 10.800 | 3.000 | 17 | 17.200 | 3.000 |
| 13 | 11.600 | 3.000 | 18 | 18.000 | 3.000 |
| 14 | 13.600 | 3.000 | 19 | 18.800 | 3.000 |
| 15 | 14.400 | 3.000 | 20 | 20.800 | 3.000 |
| 21 | 21.600 | 3.000 | 26 | 14.400 | 2.200 |
| 22 | 21.600 | 2.200 | 27 | 14.400 | 0.000 |
| 23 | 21.600 | 0.000 | 28 | 10.800 | 2.200 |
| 24 | 18.000 | 2.200 | 29 | 10.800 | 0.000 |
| 25 | 18.000 | 0.000 | 30 | 7.200 | 2.200 |
| 31 | 7.200 | 0.000 | | | |
| 32 | 3.600 | 2.200 | | | |
| 33 | 3.600 | 0.000 | | | |

STAVEN

| St. | ki | kj | Profiel | Aansl.i | Aansl.j | Lengte Opm. |
|-----|----|----|---------------|---------|---------|-------------|
| 1 | 1 | 2 | 1:B*H 200*200 | NDM | NDM | 2.200 |
| 2 | 2 | 3 | 1:B*H 200*200 | NDM | NDM | 0.800 |
| 3 | 3 | 4 | 1:B*H 200*200 | ND- | NDM | 0.800 |
| 4 | 4 | 5 | 1:B*H 200*200 | NDM | NDM | 2.000 |
| 5 | 5 | 6 | 1:B*H 200*200 | NDM | ND- | 0.800 |
| 6 | 6 | 7 | 1:B*H 200*200 | ND- | NDM | 0.800 |
| 7 | 7 | 8 | 1:B*H 200*200 | NDM | NDM | 2.000 |
| 8 | 8 | 9 | 1:B*H 200*200 | NDM | ND- | 0.800 |
| 9 | 9 | 10 | 1:B*H 200*200 | ND- | NDM | 0.800 |
| 10 | 10 | 11 | 1:B*H 200*200 | NDM | NDM | 2.000 |
| 11 | 11 | 12 | 1:B*H 200*200 | NDM | ND- | 0.800 |
| 12 | 12 | 13 | 1:B*H 200*200 | ND- | NDM | 0.800 |
| 13 | 13 | 14 | 1:B*H 200*200 | NDM | NDM | 2.000 |
| 14 | 14 | 15 | 1:B*H 200*200 | NDM | ND- | 0.800 |
| 15 | 15 | 16 | 1:B*H 200*200 | ND- | NDM | 0.800 |
| 16 | 16 | 17 | 1:B*H 200*200 | NDM | NDM | 2.000 |
| 17 | 17 | 18 | 1:B*H 200*200 | NDM | ND- | 0.800 |
| 18 | 18 | 19 | 1:B*H 200*200 | ND- | NDM | 0.800 |
| 19 | 19 | 20 | 1:B*H 200*200 | NDM | NDM | 2.000 |
| 20 | 20 | 21 | 1:B*H 200*200 | NDM | ND- | 0.800 |
| 21 | 21 | 22 | 1:B*H 200*200 | NDM | NDM | 0.800 |
| 22 | 22 | 23 | 1:B*H 200*200 | NDM | NDM | 2.200 |
| 23 | 18 | 24 | 1:B*H 200*200 | NDM | NDM | 0.800 |
| 24 | 24 | 25 | 1:B*H 200*200 | NDM | NDM | 2.200 |
| 25 | 15 | 26 | 1:B*H 200*200 | NDM | NDM | 0.800 |
| 26 | 26 | 27 | 1:B*H 200*200 | NDM | NDM | 2.200 |
| 27 | 12 | 28 | 1:B*H 200*200 | NDM | NDM | 0.800 |
| 28 | 28 | 29 | 1:B*H 200*200 | NDM | NDM | 2.200 |
| 29 | 9 | 30 | 1:B*H 200*200 | NDM | NDM | 0.800 |
| 30 | 30 | 31 | 1:B*H 200*200 | NDM | NDM | 2.200 |
| 31 | 6 | 32 | 1:B*H 200*200 | NDM | NDM | 0.800 |
| 32 | 32 | 33 | 1:B*H 200*200 | NDM | NDM | 2.200 |
| 33 | 2 | 4 | 2:B*H 150*200 | ND- | ND- | 1.131 |
| 34 | 5 | 32 | 2:B*H 150*200 | ND- | ND- | 1.131 |
| 35 | 32 | 7 | 2:B*H 150*200 | ND- | ND- | 1.131 |
| 36 | 8 | 30 | 2:B*H 150*200 | ND- | ND- | 1.131 |
| 37 | 30 | 10 | 2:B*H 150*200 | ND- | ND- | 1.131 |
| 38 | 11 | 28 | 2:B*H 150*200 | ND- | ND- | 1.131 |
| 39 | 28 | 13 | 2:B*H 150*200 | ND- | ND- | 1.131 |
| 40 | 14 | 26 | 2:B*H 150*200 | ND- | ND- | 1.131 |
| 41 | 26 | 16 | 2:B*H 150*200 | ND- | ND- | 1.131 |
| 42 | 17 | 24 | 2:B*H 150*200 | ND- | ND- | 1.131 |
| 43 | 24 | 19 | 2:B*H 150*200 | ND- | ND- | 1.131 |
| 44 | 20 | 22 | 2:B*H 150*200 | ND- | ND- | 1.131 |

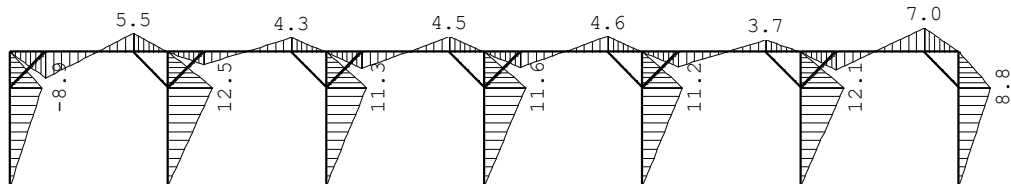
VASTE STEUNPUNTEN

| Nr. | knoop | Kode | XZR | l=vast | 0=vrij | Hoek |
|-----|-------|------|-----|--------|--------|------|
| 1 | 1 | 110 | | | | 0.00 |
| 2 | 23 | 110 | | | | 0.00 |
| 3 | 25 | 110 | | | | 0.00 |
| 4 | 27 | 110 | | | | 0.00 |
| 5 | 29 | 110 | | | | 0.00 |

| | | |
|--------|-------|----------------------------------|
| 29 | -3.91 | 16.82 |
| 31 | -3.81 | 16.30 |
| 33 | -4.22 | 18.67 |
| -25.75 | | 101.61 : Som van de reacties |
| 25.75 | | -101.61 : Som van de belastingen |

OMHULLENDE VAN DE FUNDAMENTELE COMBINATIES
MOMENTEN

Fundamentele combinatie


REACTIES

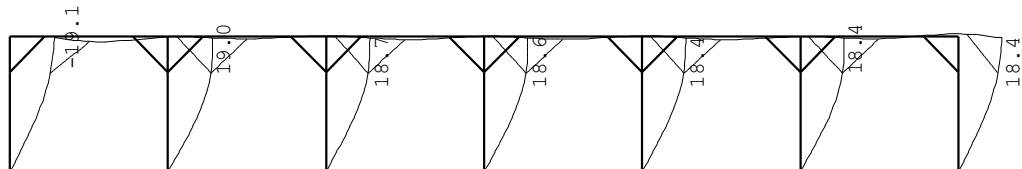
Fundamentele combinatie

| Kn. | X | Z | M |
|-----|-------|-------|---|
| 1 | -4.06 | 3.19 | |
| 23 | -4.02 | 15.58 | |
| 25 | -5.51 | 15.93 | |
| 27 | -5.08 | 18.72 | |
| 29 | -5.28 | 18.17 | |
| 31 | -5.14 | 17.49 | |
| 33 | -5.69 | 20.66 | |

OMHULLENDE VAN DE KARAKTERISTIEKE COMBINATIES
VERPLAATSINGEN

[mm]

Karakteristieke combinatie



Kolom en schoorberekening : zie berekening spant. De waarden komen vrijwel obvereen.

De vervorming zal im werkelijkheid lager zijn dan de berekende waarden, omdat er ook gevels aan het gebouw zijn aangebracht.

De vervorming is 18.4 mm . Dat is 1/164. Voor een schuur is 1/150 toegelaten.

Odoorn: 05 oktober 2018



Ing. W. v.d. Haar