

MEGATON

PREFAB SYSTEMS

member of the  **WILLY GROUP
NAESSENS**

Berekeningsnota

Kanaalplaten

DATUM: 29/09/2015

Projectnr.

MP 250589

Project

Plaats

Steenbergen

Onderdeel

Behoort bij beschikking

d.d. 17-12-2015

nr.(s) ZK15000992

Medewerker
Publiekszaken/vergunningen



Revisie:

Nr.	Naam	Datum	Omschrijving	Designed by	Checked by	Approved by
1		9/10/2015	index A			

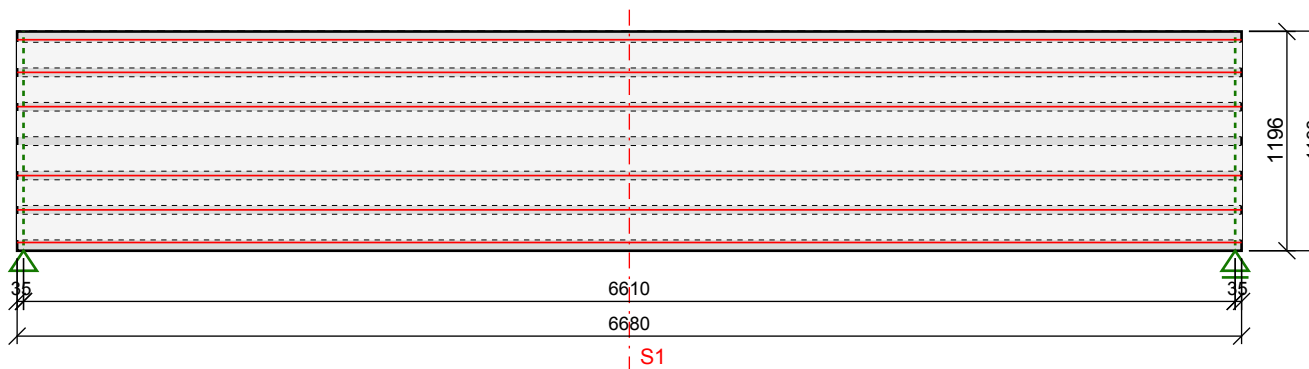
Megaton N.V.
Nederwijk-Oost 279
8792 Ninove

DEFINITIEF 09/10/15

T: 054 33 45 11
F: 054 32 60 47
M: info@megaton.be

PROJECT - OVERZICHT

ID	Nummer	Naam	Doorsnede	L (mm)	Wapening
1. Fase 1					
1.1	REK 1	WXT200+0	WXT200	6680	S200-N6
1.2	REK 2	WXT150+0	WXT150	6780	S150-N5



BELASTINGEN

[EN1991-1-1]

Verticaal

Nr.	N/A	Belastingsgeval	Type	Soort	t1	t2	Definitie
0	-	Voorspanning	-	permanent	1	8	-
1	-	prefabelement	SWP	eigengewicht	1	8	fac=1.00 sw=-2.86(kN/m2)
2	-	voegvulling	SWP	eigengewicht	3	8	fac=1.00 sw=-0.12(kN/m2)
3	-	Permanente last	PU	permanent	6	8	p=-1.40(kN/m2)
4	-	Variabele last	PU	CAT A	7	8	p=-3.70(kN/m2)
5	-	prefabelement_TR	BF	permanent	3	8	x=1.50(m)y=0.50(-) F=-1.29(kN) α=1.00
6	-	voegvulling_TR	BF	permanent	3	8	x=1.50(m)y=0.50(-) F=-0.06(kN) α=1.00
7	-	Permanente last_TR	BF	permanent	6	8	x=1.50(m)y=0.50(-) F=-0.45(kN) α=1.00
8	-	Variabele last_TR	BF	CAT A	7	8	x=1.50(m)y=0.50(-) F=-1.67(kN) α=1.00
9	-	prefabelement_TR	BF	permanent	3	8	x=5.40(m)y=0.50(-) F=-1.60(kN) α=1.00
10	-	voegvulling_TR	BF	permanent	3	8	x=5.40(m)y=0.50(-) F=-0.05(kN) α=1.00
11	-	Permanente last_TR	BF	permanent	6	8	x=5.40(m)y=0.50(-) F=-0.60(kN) α=1.00
12	-	Variabele last_TR	BF	CAT A	7	8	x=5.40(m)y=0.50(-) F=-1.44(kN) α=1.00

BELASTINGSCOMBINATIES

[EN1990: 6.4.3 + EN1990: ANNEX A1.2]

Partiële veiligheidsfactoren [EN 1990]

Blijvende belasting:	$\gamma_G = 1.20$
Veranderlijke belasting:	$\gamma_Q = 1.50$
Voorspanning:	$\gamma_P = 1.00$

Samenstelfactoren [EN 1991-1]

Combinatiewaarde:	$\psi_0 = 0.7$
Frequente waarde:	$\psi_1 = 0.5$
Quasi-permanente waarde:	$\psi_2 = 0.3$

Combinaties voor tijdstippen: {8}

I	Nr.	Belastingscombinatie	Type	t	Definitie
1	107	ULS_STR_t8	ULS_STR	8	$1.20*(1+2+3+5+6+7+9+10+11)+1.50*(4+8+12)$
2	200	ULS_FIRE_t8	ULS_FIRE	8	$1.00*(1+2+3+5+6+7+9+10+11)+1.00*0.30*(4+8+12)$
3	307	SLS_Char_t8	SLS_Char	8	$1.00*(1+2+3+5+6+7+9+10+11+4+8+12)$
4	407	SLS_Freq_t8	SLS_Freq	8	$1.00*(1+2+3+5+6+7+9+10+11)+1.00*0.50*(4+8+12)$
5	507	SLS_QP_t8	SLS_QP	8	$1.00*(1+2+3+5+6+7+9+10+11)+1.00*0.30*(4+8+12)$

RESULTATEN EINDIGE ELEMENTEN ANALYSE

OPLEGKRACHTEN

Combinaties voor tijdstippen: {8}

Tijdstip	Nr.	Naam	Type	SupNr.	x (mm)	rFX (kN)	rFZ (kN)	rMY (kNm)
8	107	ULS_STR_t8	ULS_STR	1	35	0.00	47.85	0.00
				2	6645	0.00	48.30	0.00
	200	ULS_FIRE_t8	ULS_FIRE	1	35	0.00	24.30	0.00
				2	6645	0.00	24.70	0.00
	307	SLS_Char_t8	SLS_Char	1	35	0.00	35.78	0.00
				2	6645	0.00	36.15	0.00

SNEDEKRACHTEN

Combinaties voor tijdstippen: {8}

Tijdstip	Nr.	Naam	Type	x (mm)	FX (kN)	FZ (kN)	MY (kNm)
8	107	ULS_STR_t8	ULS_STR	35	0.00	47.40	0.00
				3328	0.00	0.04	77.27
				6645	0.00	-47.84	0.00
	200	ULS_FIRE_t8	ULS_FIRE	35	0.00	24.07	0.00
				3328	0.00	0.08	39.34
				6645	0.00	-24.47	0.00

VOORSPANNING

VOORSPANVERLIEZEN

Samenvatting gemiddelde voorspanverliezen:

Tijdstip	$\Delta P/P$	$\Sigma(\Delta P)/P$	Pmt (kN)	Mpmt (kNm)
Voorspankracht: t0 (spanbank)				
0	0.00%	0.00%	406.22	-24.84
Onmiddellijke voorspanverliezen: t1				
1	2.94%	2.94%	394.27	-24.11
Tijdsafhankelijke voorspanverliezen: > t1				
8	7.54%	14.72%	346.42	-21.22

SAMENVATTING BEREKENINGSRISULTATEN

Legende

?	Eenheidscontrole	Controle
●	$0.00 \leq EC \leq 1.00$	Verification is satisfied
▲	$1.00 < EC \leq 1.03$	Warning: verification is barely satisfied
■	$1.03 < EC$	Verification is NOT satisfied
-	-	Results not available
×	-	Results not valid

CONTROLE VOORSPANNING

criterium	Tijdstip	Controle		eenheid	EC	?
Maximale aanvangskracht op spanbank σ_0						
	-	$\sigma_0=1302.00$	< $\sigma_{lim}=1488.00$	N/mm ²	87.5%	●
Voorspankracht na directe verliezen σ_1						
	1	$\sigma_1=1263.69$	< $\sigma_{lim}=1395.00$	N/mm ²	90.6%	●
		-> X = 0.0 mm				
Voorspanverliezen						
directe verliezen ΔP_{0_lim}						
	1	$\Delta P_0=2.9\%$	< $\Delta P_{0_lim}=8.0\%$	-	36.8%	●
		-> Weighted mean value				
totale verliezen ΔP_{t_lim}						
	8	$\Delta P_t=14.7\%$	< $\Delta P_{t_lim}=30.0\%$	-	49.1%	●
		-> Weighted mean value				

CONTROLE UITERSTE GRENSTOESTAND (UGT)

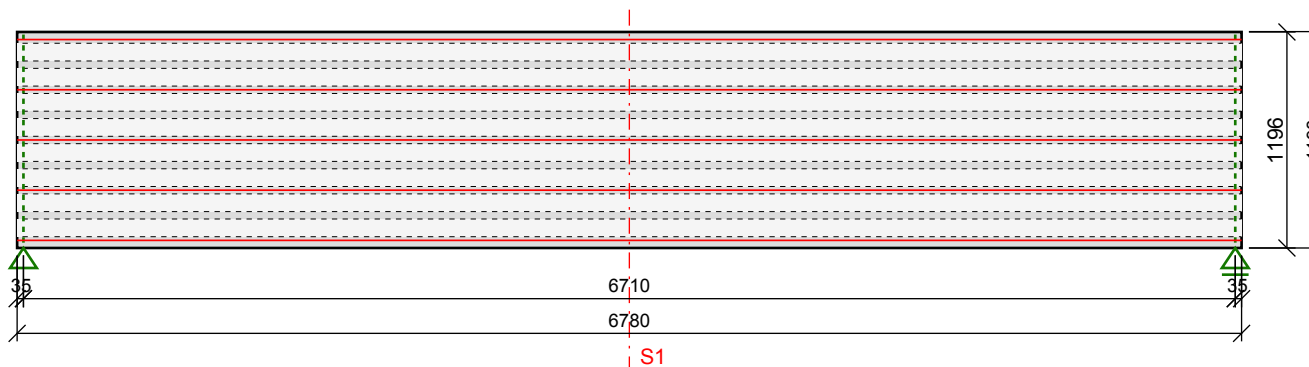
criterium	Tijdstip	Controle		eenheid	EC	?
Momentencapaciteit						
positief moment MRd+						
	3	MEd (+)=25.86	< MRd (+)=82.79	kNm	31.2%	●
		-> LC: 102 - ULS_STR_t3 -> X = 3328.1 mm				
	4	MEd (+)=25.86	< MRd (+)=83.62	kNm	30.9%	●
		-> LC: 103 - ULS_STR_t4 -> X = 3328.1 mm				
	6	MEd (+)=37.72	< MRd (+)=84.72	kNm	44.5%	●
		-> LC: 105 - ULS_STR_t6 -> X = 3328.1 mm				
	8	MEd (+)=77.27	< MRd (+)=84.81	kNm	91.1%	●
		-> LC: 107 - ULS_STR_t8 -> X = 3328.1 mm				
[Brand]	8	MEd (+)=39.34	< MRd (+)=60.73	kNm	64.8%	●
		-> LC: 200 - ULS_FIRE_t8 -> X = 3328.1 mm				
Dwarskrachtcapaciteit						
dwarskracht-druk VRd(+)						
	3	-	< VRd=61.03	kN	0.0%	●
		-> X = 3340.0 mm				
	4	-	< VRd=63.40	kN	0.0%	●
		-> X = 3340.0 mm				
	6	-	< VRd=67.64	kN	0.0%	●
		-> X = 3340.0 mm				
	7	VEd=23.10	< VRd=67.71	kN	34.1%	●
		-> LC: 106 - ULS_STR_t7 -> X = 5112.2 mm				
	8	VEd=29.25	< VRd=65.97	kN	44.3%	●
		-> LC: 107 - ULS_STR_t8 -> X = 1434.6 mm				
dwarskracht-trek VRd,t						
	3	VEd=15.58	< VRd=72.47	kN	21.5%	●
		-> LC: 102 - ULS_STR_t3 -> X = 6511.1 (-) mm				
	4	VEd=15.58	< VRd=72.92	kN	21.4%	●
		-> LC: 103 - ULS_STR_t4 -> X = 6511.1 (-) mm				

criterium	Tijdstip	Controle	eenheid	EC	?
	6	$VEd=22.68 < VRd=95.96$ -> LC: 105 - ULS_STR_t6 -> X = 6511.1 (-) mm	kN	23.6%	●
	7	$VEd=46.11 < VRd=97.34$ -> LC: 106 - ULS_STR_t7 -> X = 6511.1 (-) mm	kN	47.4%	●
	8	$VEd=46.11 < VRd=96.49$ -> LC: 107 - ULS_STR_t8 -> X = 6511.1 (-) mm	kN	47.8%	●
dwarskracht-druk VRd,fi(+)					
[Brand]	8	$VEd=23.58 < VRd,fi=70.26$ -> LC: 200 - ULS_FIRE_t8 -> X = 6511.1 (-) mm	kN	33.6%	●
Verankering voorspanwapening					
begin element fp_lim					
	8	$N/Cr < fp_lim=0.00$ -> no cracked sections	N/mm2	N/Cr	●
einde element fp_lim					
	8	$N/Cr < fp_lim=0.00$ -> no cracked sections	N/mm2	N/Cr	●

CONTROLE GEBRUIKSGRENSTOESTAND (GGT)

criterium	Tijdstip	Controle	eenheid	EC	?
Betonspanningen					
prefabelement fc_lim					
	3	$\sigma_c=5.06 < fc_lim=18.00$ -> LC: 302 - SLS_Char_t3 -> X = 671.1 (Y=10.0;Z=0.0) mm	N/mm2	28.1%	●
	4	$\sigma_c=5.14 < fc_lim=21.50$ -> LC: 303 - SLS_Char_t4 -> X = 671.1 (Y=10.0;Z=0.0) mm	N/mm2	23.9%	●
	5	$\sigma_c=5.03 < fc_lim=26.64$ -> LC: 304 - SLS_Char_t5 -> X = 671.1 (Y=10.0;Z=0.0) mm	N/mm2	18.9%	●
	6	$\sigma_c=4.46 < fc_lim=29.49$ -> LC: 305 - SLS_Char_t6 -> X = 671.1 (Y=10.0;Z=0.0) mm	N/mm2	15.1%	●
	7	$\sigma_c=7.82 < fc_lim=30.00$ -> LC: 306 - SLS_Char_t7 -> X = 3340.0 (Y=30.0;Z=200.0) mm	N/mm2	26.1%	●
	8	$\sigma_c=7.89 < fc_lim=30.00$ -> LC: 307 - SLS_Char_t8 -> X = 3340.0 (Y=30.0;Z=200.0) mm	N/mm2	26.3%	●
Spanningen in voorspanwapening					
	3	$\sigma_p=-1221.14 < fp_lim=-1395.00$ -> LC: 302 - SLS_Char_t3 -> X = 3340.0 mm	N/mm2	87.5%	●
	4	$\sigma_p=-1221.17 < fp_lim=-1395.00$ -> LC: 303 - SLS_Char_t4 -> X = 3340.0 mm	N/mm2	87.5%	●
	5	$\sigma_p=-1210.41 < fp_lim=-1395.00$ -> LC: 304 - SLS_Char_t5 -> X = 3340.0 mm	N/mm2	86.8%	●
	6	$\sigma_p=-1208.11 < fp_lim=-1395.00$ -> LC: 305 - SLS_Char_t6 -> X = 3340.0 mm	N/mm2	86.6%	●
	7	$\sigma_p=-1211.43 < fp_lim=-1395.00$ -> LC: 306 - SLS_Char_t7 -> X = 3340.0 mm	N/mm2	86.8%	●
	8	$\sigma_p=-1115.46 < fp_lim=-1395.00$ -> LC: 307 - SLS_Char_t8 -> X = 3340.0 mm	N/mm2	80.0%	●
Scheurwijdte					
	6	$N/Cr < wk_lim=0.20$ -> LC: 405 - SLS_Freq_t6 -> no cracked sections No cracking at any bottom fibre.	mm	N/Cr	●
	7	$N/Cr < wk_lim=0.20$ -> LC: 406 - SLS_Freq_t7 -> no cracked sections No cracking at any bottom fibre.	mm	N/Cr	●
	8	$N/Cr < wk_lim=0.20$ -> LC: 407 - SLS_Freq_t8 -> no cracked sections No cracking at any bottom fibre.	mm	N/Cr	●
Vervormingen					

Criterion	Tijdstip	Controle	eenheid	EC	?
zeeg QP , CAM (t)					
relatieve waarde	3	$UZ = 4.52 = L/1464 < UZ_lim = 26.44 = L/250$ -> LC: 502 - SLS_QP_t3 -> X = 3340.00 mm (Segment 1)	mm	17.1%	●
totale doorbuiging QP , APP (t)					
relatieve waarde	8	$UZ = -7.15 = L/924 < UZ_lim = 26.44 = L/250$ -> LC: 507 - SLS_QP_t8 -> X = 3340.00 mm (Segment 1)	mm	27.0%	●
bijkomende doorbuiging QP , DAM (Δt)					
relatieve waarde	5+>8	$\Delta UZ = -9.18 = L/720 < \Delta UZ_lim = 13.22 = L/500$ -> LC: 507 - SLS_QP_t8 -> X = 3340.00 mm (Segment 1)	mm	69.5%	●
relatieve waarde	6+>8	$\Delta UZ = -7.11 = L/930 < \Delta UZ_lim = 13.22 = L/500$ -> LC: 507 - SLS_QP_t8 -> X = 3340.00 mm (Segment 1)	mm	53.8%	●
bijkomende doorbuiging QP , UTIL (Δt)					
relatieve waarde	7->8	$\Delta UZ = -5.95 = L/1111 < \Delta UZ_lim = 26.44 = L/250$ -> LC: 507 - SLS_QP_t8 -> X = 3340.00 mm (Segment 1)	mm	22.5%	●
totale doorbuiging QP+(1- ψ 2)•Qk , APP (t)					
relatieve waarde	8	$UZ = -10.90 = L/606 < UZ_lim = 22.03 = L/300$ -> LC: 507 - SLS_QP_t8 -> X = 3340.00 mm (Segment 1)	mm	49.5%	●
bijkomende doorbuiging QP+(1- ψ 2)•Qk , DAM (Δt)					
relatieve waarde	5+>8	$\Delta UZ = -12.94 = L/511 < \Delta UZ_lim = 13.22 = L/500$ -> LC: 507 - SLS_QP_t8 -> X = 3340.00 mm (Segment 1)	mm	97.9%	●
relatieve waarde	6+>8	$\Delta UZ = -10.86 = L/609 < \Delta UZ_lim = 13.22 = L/500$ -> LC: 507 - SLS_QP_t8 -> X = 3340.00 mm (Segment 1)	mm	82.2%	●
bijkomende doorbuiging QP+(1- ψ 2)•Qk , UTIL (Δt)					
relatieve waarde	7->8	$\Delta UZ = -9.70 = L/681 < \Delta UZ_lim = 22.03 = L/300$ -> LC: 507 - SLS_QP_t8 -> X = 3340.00 mm (Segment 1)	mm	44.0%	●



BELASTINGEN

[EN1991-1-1]

Verticaal

Nr.	N/A	Belastingsgeval	Type	Soort	t1	t2	Definitie
0	-	Voorspanning	-	permanent	1	8	-
1	-	prefabelement	SWP	eigengewicht	1	8	fac=1.00 sw=-2.30(kN/m ²)
2	-	voegvulling	SWP	eigengewicht	3	8	fac=1.00 sw=-0.11(kN/m ²)
3	-	Permanente last	PU	permanent	6	8	p=-1.40(kN/m ²)
4	-	Variabele last	PU	CAT H	7	8	p=-1.00(kN/m ²)

BELASTINGSCOMBINATIES

[EN1990: 6.4.3 + EN1990: ANNEX A1.2]

Partiële veiligheidsfactoren [EN 1990]

Blijvende belasting:	$\gamma_G = 1.20$
Veranderlijke belasting:	$\gamma_Q = 1.50$
Voorspanning:	$\gamma_P = 1.00$

Samenstelfactoren [EN 1991-1]

Combinatiewaarde:	$\psi_0 = 0$
Frequente waarde:	$\psi_1 = 0$
Quasi-permanente waarde:	$\psi_2 = 0$

Combinaties voor tijdstippen: {8}

i	Nr.	Belastingscombinatie	Type	t	Definitie
1	107	ULS_STR_t8	ULS_STR	8	$1.20*(1+2+3)+1.50*(4)$
2	200	ULS_FIRE_t8	ULS_FIRE	8	$1.00*(1+2+3)+1.00*0.00*(4)$
3	307	SLS_Char_t8	SLS_Char	8	$1.00*(1+2+3+4)$
4	407	SLS_Freq_t8	SLS_Freq	8	$1.00*(1+2+3)+1.00*0.00*(4)$
5	507	SLS_QP_t8	SLS_QP	8	$1.00*(1+2+3)+1.00*0.00*(4)$

RESULTATEN EINDIGE ELEMENTEN ANALYSE

OPLEGKRACHTEN

Combinaties voor tijdstippen: {8}

Tijdstip	Nr.	Naam	Type	SupNr.	x (mm)	rFX (kN)	rFZ (kN)	rMY (kNm)
8	107	ULS_STR_t8	ULS_STR	1	35	0.00	24.71	0.00
				2	6745	0.00	24.71	0.00
	200	ULS_FIRE_t8	ULS_FIRE	1	35	0.00	15.51	0.00
				2	6745	0.00	15.51	0.00
	307	SLS_Char_t8	SLS_Char	1	35	0.00	19.58	0.00
				2	6745	0.00	19.58	0.00

SNEDEKRACHTEN

Combinaties voor tijdstippen: {8}

Tijdstip	Nr.	Naam	Type	x (mm)	FX (kN)	FZ (kN)	MY (kNm)
8	107	ULS_STR_t8	ULS_STR	35	0.00	24.46	0.00
				3390	0.00	0.00	41.03
				6745	0.00	-24.46	0.00
	200	ULS_FIRE_t8	ULS_FIRE	35	0.00	15.35	0.00

Tijdstip	Nr.	Naam	Type	x (mm)	FX (kN)	FZ (kN)	MY (kNm)
				3390	0.00	0.00	25.75
				6745	0.00	-15.35	0.00

VOORSPANNING

VOORSPANVERLIEZEN

Samenvatting gemiddelde voorspanverliezen:

Tijdstip	$\Delta P/P$	$\Sigma(\Delta P)/P$	Pmt (kN)	Mpmt (kNm)
Voorspankracht: t0 (spanbank)				
0	0.00%	0.00%	338.52	-12.48
Onmiddellijke voorspanverliezen: t1				
1	2.64%	2.64%	329.58	-12.15
Tijdsafhankelijke voorspanverliezen: > t1				
8	7.23%	14.56%	289.24	-10.68

SAMENVATTING BEREKENINGSRISULTATEN

Legende

?	Eenheidscontrole	Controle
●	$0.00 \leq EC \leq 1.00$	Verification is satisfied
▲	$1.00 < EC \leq 1.03$	Warning: verification is barely satisfied
■	$1.03 < EC$	Verification is NOT satisfied
-	-	Results not available
×	-	Results not valid

CONTROLE VOORSPANNING

criterium	Tijdstip	Controle		eenheid	EC	?
Maximale aanvangskracht op spanbank σ_0						
	-	$\sigma_0=1302.00$	< $\sigma_{lim}=1488.00$	N/mm ²	87.5%	●
Voorspankracht na directe verliezen σ_1						
	1	$\sigma_1=1267.61$	< $\sigma_{lim}=1395.00$	N/mm ²	90.9%	●
		-> X = 0.0 mm				
Voorspanverliezen						
directe verliezen ΔP_0_{lim}						
	1	$\Delta P_0=2.6\%$	< $\Delta P_0_{lim}=8.0\%$	-	33.0%	●
		-> Weighted mean value				
totale verliezen ΔP_t_{lim}						
	8	$\Delta P_t=14.6\%$	< $\Delta P_t_{lim}=30.0\%$	-	48.5%	●
		-> Weighted mean value				

CONTROLE UITERSTE GRENSTOESTAND (UGT)

criterium	Tijdstip	Controle		eenheid	EC	?
Momentencapaciteit						
positief moment MRd+						
	3	MEd (+)=19.55	< MRd (+)=47.19	kNm	41.4%	●
		-> LC: 102 - ULS_STR_t3 -> X = 3390.0 mm				
	4	MEd (+)=19.55	< MRd (+)=47.79	kNm	40.9%	●
		-> LC: 103 - ULS_STR_t4 -> X = 3390.0 mm				
	6	MEd (+)=30.90	< MRd (+)=48.59	kNm	63.6%	●
		-> LC: 105 - ULS_STR_t6 -> X = 3390.0 mm				
	8	MEd (+)=41.03	< MRd (+)=48.64	kNm	84.4%	●
		-> LC: 107 - ULS_STR_t8 -> X = 3390.0 mm				
[Brand]	8	MEd (+)=25.75	< MRd (+)=34.94	kNm	73.7%	●
		-> LC: 200 - ULS_FIRE_t8 -> X = 3390.0 mm				
Dwarskrachtcapaciteit						
dwarskracht-druk VRd(+)						
	3	-	< VRd=48.26	kN	0.0%	●
		-> X = 3390.0 mm				
	4	-	< VRd=50.14	kN	0.0%	●
		-> X = 3390.0 mm				
	6	-	< VRd=53.47	kN	0.0%	●
		-> X = 3390.0 mm				
	7	VEd=11.89	< VRd=53.44	kN	22.2%	●
		-> LC: 106 - ULS_STR_t7 -> X = 5020.6 mm				
	8	VEd=12.85	< VRd=52.12	kN	24.7%	●
		-> LC: 107 - ULS_STR_t8 -> X = 5153.0 mm				
dwarskracht-trek VRd,t						
	3	VEd=11.28	< VRd=58.22	kN	19.4%	●
		-> LC: 102 - ULS_STR_t3 -> X = 144.3 (+) mm				
	4	VEd=11.28	< VRd=58.59	kN	19.2%	●
		-> LC: 103 - ULS_STR_t4 -> X = 144.3 (+) mm				

Criterion	Tijdstip	Controle	eenheid	EC	?
	6	VEd=17.82 < VRd=77.39 -> LC: 105 - ULS_STR_t6 -> X = 144.3 (+) mm	kN	23.0%	●
	7	VEd=23.66 < VRd=78.49 -> LC: 106 - ULS_STR_t7 -> X = 144.3 (+) mm	kN	30.1%	●
	8	VEd=23.66 < VRd=77.89 -> LC: 107 - ULS_STR_t8 -> X = 144.3 (+) mm	kN	30.4%	●
dwarskracht-druk VRd,fi(+)					
[Brand]	8	VEd=14.85 < VRd,fi=51.68 -> LC: 200 - ULS_FIRE_t8 -> X = 144.3 (+) mm	kN	28.7%	●
Verankering voorspanwapening					
begin element fp_lim					
	8	N/Cr < fp_lim=0.00 -> no cracked sections	N/mm2	N/Cr	●
einde element fp_lim					
	8	N/Cr < fp_lim=0.00 -> no cracked sections	N/mm2	N/Cr	●

CONTROLE GEBRUIKSGRENSTOESTAND (GGT)

Criterion	Tijdstip	Controle	eenheid	EC	?
Betonspanningen					
prefabelement fc_lim					
	3	$\sigma_c=4.41$ < $f_{c_lim}=18.00$ -> LC: 302 - SLS_Char_t3 -> X = 6106.8 (Y=10.0;Z=0.0) mm	N/mm2	24.5%	●
	4	$\sigma_c=4.48$ < $f_{c_lim}=21.50$ -> LC: 303 - SLS_Char_t4 -> X = 6106.8 (Y=10.0;Z=0.0) mm	N/mm2	20.9%	●
	5	$\sigma_c=4.38$ < $f_{c_lim}=26.64$ -> LC: 304 - SLS_Char_t5 -> X = 6106.8 (Y=10.0;Z=0.0) mm	N/mm2	16.4%	●
	6	$\sigma_c=6.34$ < $f_{c_lim}=29.49$ -> LC: 305 - SLS_Char_t6 -> X = 3390.0 (Y=35.0;Z=150.0) mm	N/mm2	21.5%	●
	7	$\sigma_c=8.09$ < $f_{c_lim}=30.00$ -> LC: 306 - SLS_Char_t7 -> X = 3390.0 (Y=35.0;Z=150.0) mm	N/mm2	27.0%	●
	8	$\sigma_c=8.11$ < $f_{c_lim}=30.00$ -> LC: 307 - SLS_Char_t8 -> X = 3390.0 (Y=35.0;Z=150.0) mm	N/mm2	27.0%	●
Spanningen in voorspanwapening					
	3	$\sigma_p= -1229.32 $ < $f_{p_lim}= -1395.00 $ -> LC: 302 - SLS_Char_t3 -> X = 3390.0 mm	N/mm2	88.1%	●
	4	$\sigma_p= -1229.86 $ < $f_{p_lim}= -1395.00 $ -> LC: 303 - SLS_Char_t4 -> X = 3390.0 mm	N/mm2	88.2%	●
	5	$\sigma_p= -1217.60 $ < $f_{p_lim}= -1395.00 $ -> LC: 304 - SLS_Char_t5 -> X = 3390.0 mm	N/mm2	87.3%	●
	6	$\sigma_p= -1217.65 $ < $f_{p_lim}= -1395.00 $ -> LC: 305 - SLS_Char_t6 -> X = 3390.0 mm	N/mm2	87.3%	●
	7	$\sigma_p= -1205.98 $ < $f_{p_lim}= -1395.00 $ -> LC: 306 - SLS_Char_t7 -> X = 3390.0 mm	N/mm2	86.5%	●
	8	$\sigma_p= -1113.75 $ < $f_{p_lim}= -1395.00 $ -> LC: 307 - SLS_Char_t8 -> X = 3390.0 mm	N/mm2	79.8%	●
Scheurwijdte					
	6	N/Cr < wk_lim=0.20 -> LC: 405 - SLS_Freq_t6 -> no cracked sections No cracking at any bottom fibre.	mm	N/Cr	●
	7	N/Cr < wk_lim=0.20 -> LC: 406 - SLS_Freq_t7 -> no cracked sections No cracking at any bottom fibre.	mm	N/Cr	●
	8	N/Cr < wk_lim=0.20 -> LC: 407 - SLS_Freq_t8 -> no cracked sections No cracking at any bottom fibre.	mm	N/Cr	●
Vervormingen					

criterium	Tijdstip	Controle	eenheid	EC	?
zeeg QP , CAM (t)					
relatieve waarde	3	$UZ = 2.69 = L/2497 < UZ_lim = 26.84 = L/250$	mm	10.0%	●
-> LC: 502 - SLS_QP_t3 -> X = 3390.00 mm (Segment 1)					
totale doorbuiging QP , APP (t)					
relatieve waarde	8	$UZ = -17.89 = L/375 < UZ_lim = 26.84 = L/250$	mm	66.6%	●
-> LC: 507 - SLS_QP_t8 -> X = 3390.00 mm (Segment 1)					
bijkomende doorbuiging QP , DAM (Δt)					
relatieve waarde	6+->8	$\Delta UZ = -10.55 = L/636 < \Delta UZ_lim = 13.42 = L/500$	mm	78.6%	●
-> LC: 507 - SLS_QP_t8 -> X = 3390.00 mm (Segment 1)					
bijkomende doorbuiging QP , UTIL (Δt)					
relatieve waarde	7->8	$\Delta UZ = -7.13 = L/942 < \Delta UZ_lim = 26.84 = L/250$	mm	26.5%	●
-> LC: 507 - SLS_QP_t8 -> X = 3390.00 mm (Segment 1)					