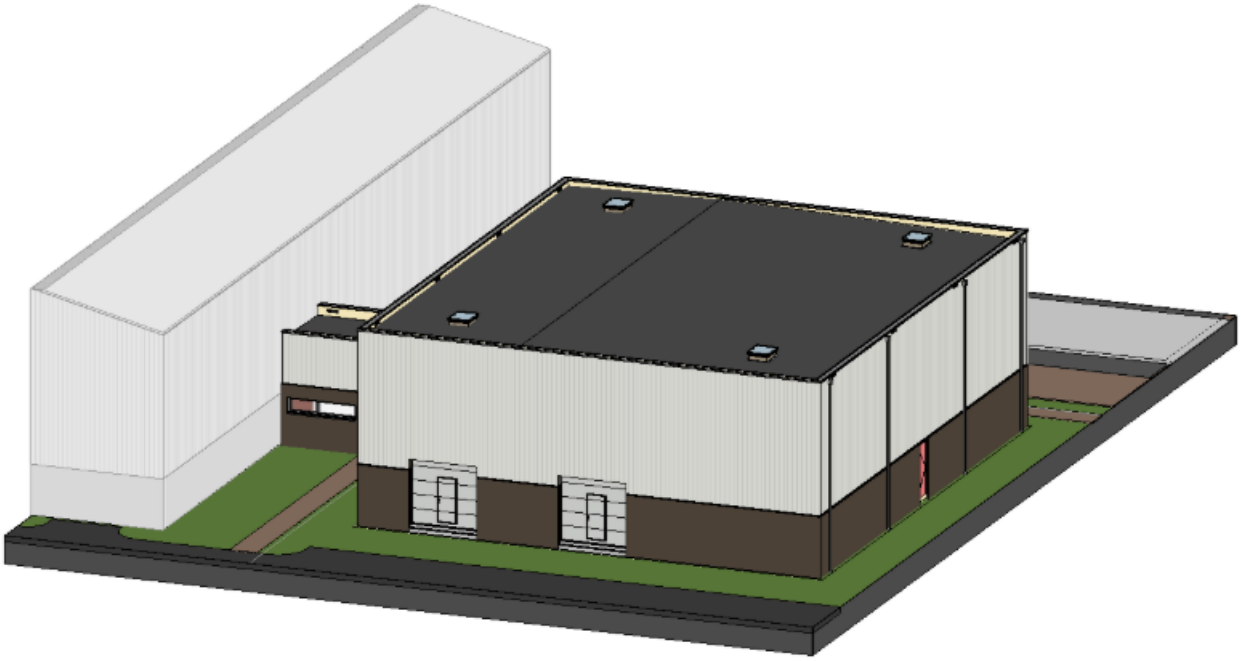
# Berekeningsrapport

## Celanese Production Netherlands B.V.

## PGS 15 opslag hal



| DOCUMENT AUTORISATIE & REVISIE OVERZICHT | | | |
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# INHOUDSOPGAVE

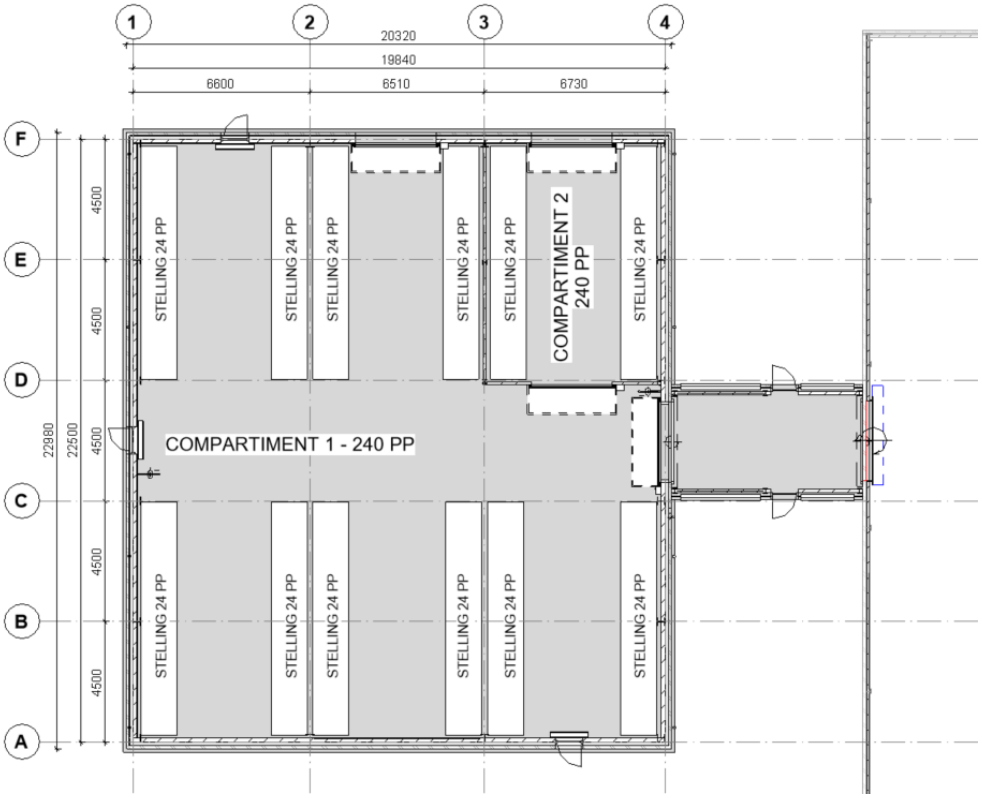
# 1 ALGEMEEN

## 1.1 Inleiding

Dit uitgangspuntendocument vormt de basis voor het ontwerp van de nieuwe hal ten behoeve van het opslaan van de gevaarlijke stoffen PGS 15.

## 1.2 Overzicht

De vloer van de nieuwe opslag hal dient vloeistofdicht uitgevoerd te worden en voorzien van vloeistofkerende wanden. De nieuwe opslagvoorziening zal geschikt zijn voor maximaal 288 palletplaatsen in daarvoor geschikte stellingen en vakindelingen. De stellingen worden maximaal 4 hoog uitgevoerd. De hal zal ongeveer 20,5 meter lang zijn, 23 meter breed en 8,5 meter hoog. Het zal een flexibele vakindeling krijgen met een aparte compartiment. De nieuwe opslag hal wordt middels een sluis verbonden aan de bestaande hal. In de toekomst komen er mogelijk zonnepanelen op het dak van de nieuwe opslag hal. De constructie moet zodanig worden ontworpen dat het ook voldoet met de additionele belasting vanuit de zonnepanelen.




**Figuur 1.1: Bovenaanzicht nieuwe opslag hal**

## 1.3 Uitgangspunten

In de berekening wordt uitgegaan van de volgende veronderstellingen.

*Algemeen*
De voor de berekening – in aanvulling op de geldende normen en voorschriften – noodzakelijke gegevens komen uit de door de opdrachtgever aangeleverde documenten en het door VIRO opgestelde uitgangspuntendocument. Deze zijn opgesomd in paragraaf 1.4, Overige uitgangspunten en aannames worden hieronder beschreven.

*Brandwerendheid*
Constructie dient minimaal te zijn voorzien van 60 minuten brandwerendheid, met uitzondering van de staalconstructie dat de twee compartimenten scheidt. Deze dient minimaal te zijn voorzien van 120 minuten brandwerendheid. Uitgangspunt is dat er met de standaardbrand-kromme wordt gerekend.

*Corrosie*
In de berekening wordt ervan uitgegaan dat eventuele vereisten met betrekking tot de beperking van corrosie door de opdrachtgever worden aangebracht.

*Fasering*
De analyse bevat alleen de blijvende eindsituatie

*Fundatie*
Fundering op staal op basis van ref.[3].
Beddingsconstante is 7000kN/m$^3$.

*Grondwater*
Er is uitgegaan dat het niveau van het grondwater heeft geen invloed op de berekening.

*Wateraccumulatie*
Het afschot van het dak is voldoende om wateraccumulatie te voorkomen.

**Dakoppervlak:**

| | | | |
|---|---|---|---|
| Breedte = | 13 | m | |
| Lengte = | 23 | m | x |
| Oppervlak = | 299 | m² | |

**Benodigde afvoercapaciteit:**

| | | |
|---|---|---|
| Referentieperiode = | 50 | jaar |
| Neerslagintensiteit $i_r$ = | 0,0500 | x $10^{-3}$ m/s |
| $Q_h$ = | 0,015 | $m^3/s$ |

**Hoogte noodafvoer boven het dakvlak :**

| | | | |
|---|---|---|---|
| $h_{nd}$ = | 0,11 | m | hoogte van de noodafvoer of dakrand boven het dak |

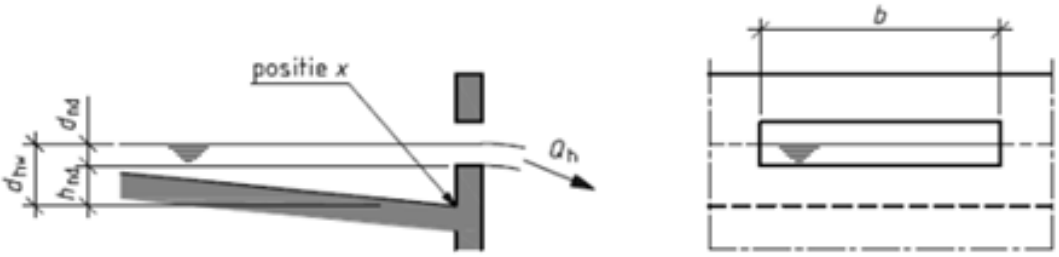
**Waterhoogte boven de noodafvoer :**

Type noodafvoer: Rechte vrije overlaat

| | | | | | |
|---|---|---|---|---|---|
| $b$ = | 2,000 | m | | | |
| $h$ = | 0,100 | m | ≥ | $h_{min}$ = | 0,057 |
| $d_{nd}(x)$ = | 0,027 | m | waterhoogte boven de noodafvoer | | |
| $d_{hw}(x)$ = | 0,137 | m | waterhoogte t.p.v. dakrand of noodafvoer | | |

**Belasting door regenwater op dakoppervlak**

| | | |
|---|---|---|
| $p_w(x)$ = | 1,3676 | kN/m² |




## 1.4 Referentie documenten

| Van | Document nr. | Rev. | Titel | Datum | Ref. |
|---|---|---|---|---|---|
| VIRO | 23920_0018 | 00 | Uitgangspunten document PGS 15 opslag | 28-04-2022 | [1] |
| Celanese | -- | -- | Layout voor WION Celanese PPG BV rev6 – optie 1 20220422.dwg | 11-07-2022 | [2] |
| Geonius | GC200516.R01 .V01 | -- | Ontwerpadvies fundering | 15-09-2022 | [3] |

## 1.5 Voorschriften

De normen die van toepassing zijn op de constructie en waarnaar in dit verslag verwezen wordt, staan in de onderstaande tabellen weergegeven. Hiervoor gelden in Nederland steeds de Eurocodes met de Nederlandse Nationale Bijlage.

| CODE | OMSCHRIJVING |
|---|---|
| **Eurocode 0** | **Grondslagen** |
| NEN-EN 1990 | Grondslagen van het constructief ontwerp |

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| **Eurocode 1** | **Belastingen op constructies** |
|---|---|
| NEN-EN 1991-1-1 | Deel 1-1: Algemene belastingen – Volumieke gewichten, eigengewicht en opgelegde belastingen voor gebouwen |
| NEN-EN 1991-1-2 | Deel 1-2: Algemene belastingen – Belastingen bij brand |
| NEN-EN 1991-1-3 | Deel 1-3: Algemene belastingen – Sneeuwbelasting |
| NEN-EN 1991-1-4 | Deel 1-4: Algemene belastingen – Windbelasting |

| **Eurocode 2** | **Ontwerp en berekening van betonconstructies** |
|---|---|
| NEN-EN 1992-1-1 | Deel 1-1: Algemene regels en regels voor gebouwen |
| NEN-EN 1992-1-2 | Deel 1-2: Ontwerp en berekening van betonconstructies bij brand |

| **Eurocode 3** | **Ontwerp en berekening van staalconstructies** |
|---|---|
| NEN-EN 1993-1-1 | Deel 1-1: Algemene regels en regels voor gebouwen |
| NEN-EN 1993-1-2 | Deel 1-2: Ontwerp en berekening van constructies bij brand |
| NEN-EN 1993-1-8 | Deel 1-8: Ontwerp en berekening van verbindingen |

| **Eurocode 7** | **Geotechnisch ontwerp** |
|---|---|
| NEN-EN 1997-1 | Deel 1: Algemene regels |
| NEN 9997 | Deel 1: Algemene regels (Aanvullende regels voor toepassing van NEN-EN 1997-1) |

| **Eurocode 8** | **Ontwerp en berekening van aardbevingsbestendige constructies** |
|---|---|
| NEN-EN 1998-1 | Deel 1: Algemene regels, aardbevingsacties en regels voor gebouwen |
| NPR 9998 | Grondslagen voor aardbevingsbelastingen: Geïnduceerde aardbevingen |

## 1.6 Materiaalgrootheden

Uitgangspunt in de berekening zijn de onderstaande materiaalgrootheden, tenzij anders is aangegeven.

**Lasbaar constructiestaal**

| Aanduiding | Eigenschap | Waarde | Eenheid | Eigenschap | Waarde | Eenheid |
|---|---|---|---|---|---|---|
| Staal S235 | E | 210000 | $N/mm^2$ | G | 81000 | $N/mm^2$ |
| t ≤ 40mm | $f_y$ | 235 | $N/mm^2$ | $f_u$ | 360 | $N/mm^2$ |
| 40mm < t ≤ 80mm | $f_y$ | 215 | $N/mm^2$ | $f_u$ | 360 | $N/mm^2$ |
| Staal S275 | E | 210000 | $N/mm^2$ | G | 81000 | $N/mm^2$ |
| t ≤ 40mm | $f_y$ | 275 | $N/mm^2$ | $f_u$ | 430 | $N/mm^2$ |
| 40mm < t ≤ 80mm | $f_y$ | 255 | $N/mm^2$ | $f_u$ | 410 | $N/mm^2$ |
| Staal S355 | E | 210000 | $N/mm^2$ | G | 81000 | $N/mm^2$ |
| t ≤ 40mm | $f_y$ | 355 | $N/mm^2$ | $f_u$ | 490 | $N/mm^2$ |
| 40mm < t ≤ 80mm | $f_y$ | 335 | $N/mm^2$ | $f_u$ | 470 | $N/mm^2$ |

**Bouten en ankers**

| Aanduiding | Eigenschap | Waarde | Eenheid | Eigenschap | Waarde | Eenheid |
|---|---|---|---|---|---|---|
| Bouten/ankers (4.6) | $f_{yb}$ | 240 | N/mm2 | $f_{ub}$ | 400 | N/mm2 |
| Bouten/ankers (8.8) | $f_{yb}$ | 640 | N/mm2 | $f_{ub}$ | 800 | N/mm2 |

**Beton**

| Aanduiding | Eigenschap | Waarde | Eenheid | Eigenschap | Waarde | Eenheid |
|---|---|---|---|---|---|---|
| Beton C12/15 | $f_{ck}$ | 12 | N/mm$^2$ | $f_{ctm}$ | 1,60 | N/mm$^2$ |
| | $f_{cd}$ | 8 | N/mm$^2$ | $f_{ctk;0,05}$ | 1,10 | N/mm$^2$ |
| | $E_{cm}$ | 27000 | N/mm$^2$ | $f_{ctd}$ | 0,73 | N/mm$^2$ |
| Beton C30/37 | $f_{ck}$ | 30 | N/mm$^2$ | $f_{ctm}$ | 2,90 | N/mm$^2$ |
| | $f_{cd}$ | 20 | N/mm$^2$ | $f_{ctk;0,05}$ | 2,03 | N/mm$^2$ |
| | $E_{cm}$ | 33000 | N/mm$^2$ | $f_{ctd}$ | 1,35 | N/mm$^2$ |

**Betonstaal lasbaar**

| Aanduiding | Eigenschap | Waarde | Eenheid | Eigenschap | Waarde | Eenheid |
|---|---|---|---|---|---|---|
| B500 B | $f_{yk}$ | 500 | N/mm$^2$ | $f_{yd}$ | 435 | N/mm$^2$ |
| (NEN-EN 10080) | $\varepsilon_{uk}$ | ≥ 5,0 | (%) | $(f_t/f_y)_k$ | ≥ 1,08 | (%) |

## 1.7 Duurzaamheid

Tenzij anders vermeld worden de volgende randvoorwaarden m.b.t. duurzaamheid toegepast:

Milieuklassen betonconstructies

- Funderingsbalken XC3
- Betonvloer hal: bovenkant XC4, XD3, XA3
- Betonvloer hal: onderkant XC3
- Wand XC4, XD3, XA3

Dekking vloer $c_{nom}$ = 35 + 5 = 40mm
Dekking balk $c_{nom}$ = 25 + 5 = 30mm

Conservering staalconstructies

- Buitenconstructies thermisch verzinkt
- Staal binnen poedercoating

## 1.8 Vervormingen

De vervorming van de constructie en onderdelen daarvan worden getoetst volgens NEN EN 1990 Bijlage A + NB art. A1.4.2 (2): de strengste criteria volgens A1.4.3 en A1.4.4, en EN-EN 1992 tot en met NEN-EN 1999 zijn gebruikt.

<u>Doorbuiging</u>

Maximale totale doorbuiging voor daken en vloeren: $^1/_{250} \cdot l_v$

Maximale bijkomende doorbuiging voor daken: $^1/_{250} \cdot l_v$

Maximale bijkomende doorbuiging voor vloeren: $^1/_{500} \cdot l_v$ (semi-rigide fundering voor stellingen)

Voor uitkragingen gelden twee keer de bovengenoemde waarden.

Horizontale verplaatsing

De horizontale verplaatsing van gebouwen met slechts één bouwlaag bij de karakteristieke belastingscombinatie mag niet groter zijn dan:

h/150 voor industriegebouwen;

waarin:
h is de kleinste gevelhoogte of de kleinste bouwlaaghoogte.

# 2 BELASTINGEN

## 2.1 Bouwwerkcategorie en veiligheid

| **Bouwwerkaanduiding** | **Ontwerplevensduurklasse** | **Ontwerplevensduur** |
|---|---|---|
| | NEN-EN 1990 art.2.3 / NB Bijlage A1 Tabel 2.1 | |
| Gebouwen en andere gewone constructies | 3 | 50 jaar |

| **Betrouwbaarheidsniveau** | **Gevolgklasse** | **Betrouwbaar-heidsindex $\beta$** | **Betrouwbaar-heidsklasse** | **$K_{FI}$-factor** |
|---|---|---|---|---|
| Art.2.2 / Bijlage B | Tabel B1 (NB) | Tabel B2 | Art.(2) B3.2 | Tabel B3 |
| Industriegebouw voor gevaarlijke stoffen en/of processen | CC3 | 4,3 | RC3 | 1,1 |

Tabel C.1 Keuze van uitvoeringsklasse (EXC)

| **Constructiedeel** | **Gevolgklasse** Tabel B1 (NB) | **Type belasting** | **Uitvoeringsklasse** Tabel B.3 |
|---|---|---|---|
| Gebouw | CC3 | Seismische DCL | **EXC3** |

| **Constructiedeel** | **Uitvoeringsklasse** Tabel B.3 |
|---|---|
| Beton (EN 13670) | **EXC3** |

## 2.2 BELASTINGSFACTOREN

### 2.2.1 Belastingsfactoren voor de uiterste grenstoestand

**Tabel NB.4 en tabel NB.5 – Rekenwaarden van belastingen (STR/GEO) (groep B)**

| **CC** | **Blijvende en tijdelijke ontwerp-situaties** | **Blijvende belastingen** | | **Overheersende veranderlijke belasting** | **Veranderlijke belasting gelijktijdig met de overheersende** | |
|---|---|---|---|---|---|---|
| | | Ongunstig | Gunstig | | Belangrijkste (indien aanwezig) | Andere |
| 3 | (vgl. 6.10a) | 1,5 $G_{k,j,sup}$ [a] | 0,9 $G_{k,j,inf}$ | | 1,65 $\psi_{0,1} \cdot Q_{k,1}$ | 1,65 $\psi_{0,i} \cdot Q_{k,i}$ (i>1) |
| | (vgl. 6.10b) | 1,3 $G_{k,j,sup}$ [b] | 0,9 $G_{k,j,inf}$ | 1,65 $Q_{k,1}$ | | 1,65 $\psi_{0,i} \cdot Q_{k,i}$ (i>1) |

**Tabel A1.3(A) – Rekenwaarden van belastingen voor het gebruik in buitengewone belastingscombinaties**

| **Ontwerpsituaties** | **Blijvende belastingen** | | **Overheersende buitengewone belasting** | **Veranderlijke belasting gelijktijdig met de overheersende** | |
|---|---|---|---|---|---|
| | Ongunstig | Gunstig | | Belangrijkste (indien aanwezig) | Andere |
| Buitengewoon (vgl. 6.11a/b) | 1,0 $G_{k,j,sup}$ | 1,0 $G_{k,j,inf}$ | 1,0 $A_d$ | 1,0 $\psi_{1,1} \cdot Q_{k,1}$ [a] | 1,0 $\psi_{2,i} \cdot Q_{k,i}$ (i>1) |
| Aardbeving (vgl. 6.12a/b) | 1,0 $G_{k,j,sup}$ | 1,0 $G_{k,j,inf}$ | 1,0 $A_{ek}$ of 1,0 $A_{Ed}$ | 1,0 $\psi_{2,1} \cdot Q_{k,1}$ | 1,0 $\psi_{2,i} \cdot Q_{k,i}$ (i>1) |

| |
|---|
| [a] Uitsluitend voor wind in combinatie met brand bij het beoordelen van de disproportionele schade volgens NEN-EN 1991-1-7; voor overige gevallen $\psi_{2,1}$ |

### 2.2.2 Belastingsfactoren voor de bruikbaarheidsgrenstoestand

**Tabel A1.4 – Rekenwaarden van belastingen voor het gebruik in bruikbaarheidsgrenstoestand**

| Combinatie | Blijvende belastingen | | Veranderlijke belasting | |
|---|---|---|---|---|
| | Ongunstig | Gunstig | Overheersende | Andere |
| Karakteristiek | $G_{k,j,sup}$ | $G_{k,j,inf}$ | $Q_{k,1}$ | $\psi_{0,i}\ Q_{k,i}$ (i>1) |
| Frequent | $G_{k,j,sup}$ | $G_{k,j,inf}$ | $\psi_{1,1}\ Q_{k,1}$ | $\psi_{2,i}\ Q_{k,i}$ (i>1) |
| Quasi-blijvend | $G_{k,j,sup}$ | $G_{k,j,inf}$ | $\psi_{2,1}\ Q_{k,1}$ | $\psi_{2,i}\ Q_{k,i}$ (i>1) |

## 2.3 Waarden van Ψ-factoren

Combinatiefactoren voor het combineren van gelijktijdig optreden de belastingen volgens NEN EN 1990 Bijlage A + NB art. A1.2.2.
Het gaat hier om een industriegebouw zodat de vloerbelasting valt in categorie E en het dak valt in categorie H niet toegankelijk. De bijbehorende waarden voor Ψ zijn:

| Ψ -factoren | Karakteristiek | Frequent | Quasi-statisch |
|---|---|---|---|
| **Belasting categorie** | **($\Psi_0$)** | **($\Psi_1$)** | **($\Psi_2$)** |
| Categorie E: opslagruimtes | 1,0 | 0,9 | 0,8 |
| Categorie H: daken (niet toegankelijk) | 0 | 0 | 0 |
| Windbelasting | 0 | 0,2 | 0 |
| Sneeuwbelasting | 0 | 0,2 | 0 |

## 2.4 Permanente belastingen

### 2.4.1 Eigengewicht vloer BG10

De betonvloer is 200mm dik, dus eigengewicht is 0,2m · 25kN/m³ = 5,0kN/m².

De vloer is voorzien van randbalken (incl. vloer), afmeting 800mm · 400mm (L x B).

### 2.4.2 Dakbedekking BG20

Voor het dak is een gelijkmatig verdeelde belasting aangehouden van 0,85 kN/m².
Dit is gebaseerd op de volgende opbouw van het dak-pakket:

| | | | |
|---|---|---|---|
| Dakbedekking 2-laags bitumen: | | 0,10 | kN/m² |
| Isolatie steenwol: | | 0,25 | kN/m² |
| Stalen dakplaat: | | 0,20 | kN/m² |
| Installatie onder dak, verlichting: | | 0,30 | kN/m² + |
| $q_{g,dak}$ | = | 0,85 | kN/m² |

### 2.4.3 Gevel kalkzandsteen/metselwerk BG30

Eigengewicht van kalkzandsteen/metselwerk aangenomen 18,0kN/m³

| | | |
|---|---|---|
| Kalkzandsteen | 0,15m · 2,5m · 18kN/m³ | = 6,75kN/m¹ |
| Metselwerk | 0,10m · 2,5m · 18kN/m³ | = 4,50kN/m¹ |
| Totaal | | = 11,25kN/m¹ |

### 2.4.4 Binnen-/buitendoos BG40

Eigengewicht van binnen-/buitendoos aangenomen 0,30kN/m²

## 2.5 Veranderlijke belastingen

### 2.5.1 Vloerbelasting BG100 en BG110

Vloerbelasting 3,0kN/m$^2$

### 2.5.2 Dakbelasting BG120

Dakbelasting onderhoud 1,0kN/m$^2$

### 2.5.3 Zonnepanelen BG130

Er wordt aangenomen dat de zonnepanelen (inclusief stellage en ballast) een gewicht hebben van 0,50kN/m$^2$.

| Soort zonnepaneel | Gewicht | Omvang |
|---|---|---|
| Plat dak inclusief stellage en ballast | 30 - 50 kilo per m$^2$ | 2,5 m$^2$ per paneel |
| Schuin dak inclusief stellage en ballast | 15 - 25 kilo per m$^2$ | 1,65 m$^2$ per paneel |

### 2.5.4 Stellingen en pallet BG140

Eigengewicht stellingen 2,5kN/m$^1$
Gewicht per pallet 10kN (L x B x H = 1,2m x 1,2m x 1,2m)

E.G. Stelling 2,5kN/m$^1$ / 1,35m = 1,85kN/m$^2$
Pallet 4 · 10kN / (1,2m · 1,2m) = 27,8kN/m$^2$
Totaal = 29,65kN/m$^2$ → 30kN/m$^2$

### 2.5.5 Heftruck BG150

Klasse vorkheftruck: FL2
Heftruck As-last: 40kN

$Q_{k,dyn}$ = 1,4 · 40kN/2 = 28kN
$F_h$ = 0,3 · 40kN/2 = 6kN

Tabel 6.5 - Afmetingen van vorkheftrucks volgens de FL-klassen

| Klasse vorkheftruck | Nettogewicht kN | Hijslast kN | Asbreedte a m | Totale breedte b m | Totale lengte l m |
|---|---|---|---|---|---|
| FL 1 | 21 | 10 | 0,85 | 1,00 | 2,60 |
| FL 2 | 31 | 15 | 0,95 | 1,10 | 3,00 |
| FL 3 | 44 | 25 | 1,00 | 1,20 | 3,30 |
| FL 4 | 60 | 40 | 1,20 | 1,40 | 4,00 |
| FL 5 | 90 | 60 | 1,50 | 1,90 | 4,60 |
| FL 6 | 110 | 80 | 1,80 | 2,30 | 5,10 |

Tabel 6.6 - Asbelastingen van vorkheftrucks

| Klasse vorkheftruck | Asbelasting $Q_k$ kN |
|---|---|
| FL 1 | 26 |
| FL 2 | 40 |
| FL 3 | 63 |
| FL 4 | 90 |
| FL 5 | 140 |
| FL 6 | 170 |

(7) Horizontale belastingen ten gevolge van versnelling of vertraging van vorkheftrucks mogen gelijk aan 30 % van de verticale asbelastingen $Q_k$ zijn aangenomen.

**OPMERKING**

Het is niet nodig om dynamische factoren toe te passen.

### 2.5.6 Sneeuwbelasting BG300

De sneeuwbelasting volgt uit NEN EN 1993-1-3.

De coëfficiënten $C_e$ en $C_t$ voor blootstelling en warmtedoorgang zijn in de NB vastgesteld op 1,0.

$s = \mu_i \cdot C_e \cdot C_t \cdot s_k$ [art.5.2 (3) a]

Sneeuwbelasting op de grond [art.4.1 + NB]
$s_k$ = 0,7 kN/m² $\Rightarrow$ $s = \mu_i \cdot 1 \cdot 1 \cdot 0{,}7 = \mu_i \cdot 0{,}7$ kN/m².

Dakhelling: $\alpha = 0° \Rightarrow \mu_1 = 0{,}8$
Sneeuwophoping door obstakels / hoogte verschil: $\mu_2 = 2{,}0$

$q_{k,sn,1} = 0{,}8 \cdot 0{,}7 = 0{,}56$ kN/m²

$q_{k,sn,2} = 2{,}0 \cdot 0{,}7 = 1{,}4$ kN/m² (maatgevend)

### 2.5.7 Windbelasting BG401 – BG404

Belasting volgens NEN 1991-1-4 + NB.

$q_{w,x} = \frac{F_{w,x}}{A_{ref}} = c_s c_d \cdot w_x$ en $w_x = q_p \cdot c_x$, zodat $q_{w,x} = c_s c_d \cdot q_p \cdot c_x$ [art.5.2 + 5.3] (de x staat voor f, e, i of fr).

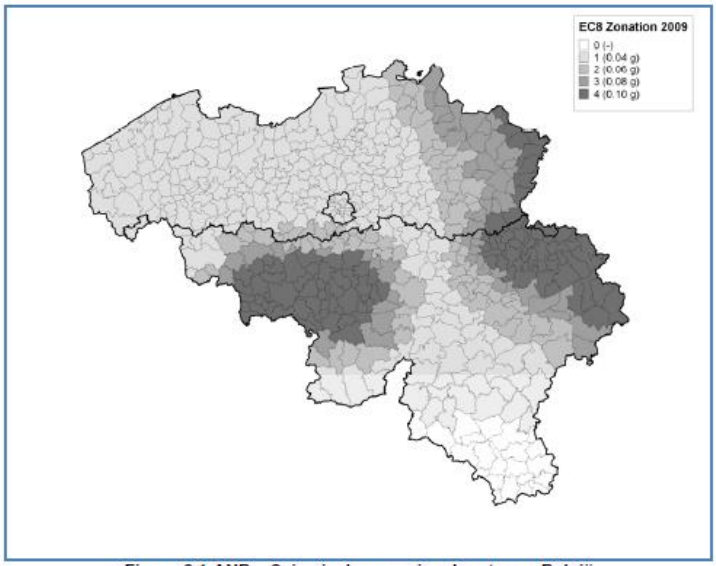
Voor de bouwwerkfactor $c_s c_d$ mag volgens art 6.2 (1) c. de waarde 1 worden aangehouden: hoogte van het gebouw is minder dan 4 keer de diepte.

*Extreme stuwdruk $q_p(z)$*

| | | | |
|---|---|---|---|
| Geleen | Windgebied III | $v_{b,0}$ = 24,5 m/s | Tabel NB.1 |
| Terreincategorie II | Onbebouwd | Industrieterrein | |
| | $z_o$ = 0,2 m; $z_{min}$ = 4 m | | NB Tabel 4.1 |
| Bouwwerkhoogte | $z$ = 8,5 m | | |
| Extreme stuwdruk | $q_p(z)$ = 0,67 kN/m² | | Tabel NB.5 |

### 2.5.8 Aardbeving BG800 – BG807

Volgens ref.[1] is er sprake van aardbeving, maar uit de NEN-EN 1998-1 zijn er geen regels voor het bepalen van aardbevingsbelastingen. Er wordt gekeken naar de buurlanden en uitgangspunt is dat de aardbevingsbelasting wordt bepaald aan de hand van NBN EN 1998-1 ANB (Belgische norm).




Figuur 3.1-ANB – Seismische zoneringskaart voor België

Er wordt gerekend met seismische zone 4, $a_{gR}$ = 0,98m/s$^2$

| | |
|---|---|
| Ground Type | D |
| Importance Class | III |
| Importance factor $\gamma_I$ = | 1,2 |

Earthquake Calculation according EN 1998-1

**General Input**

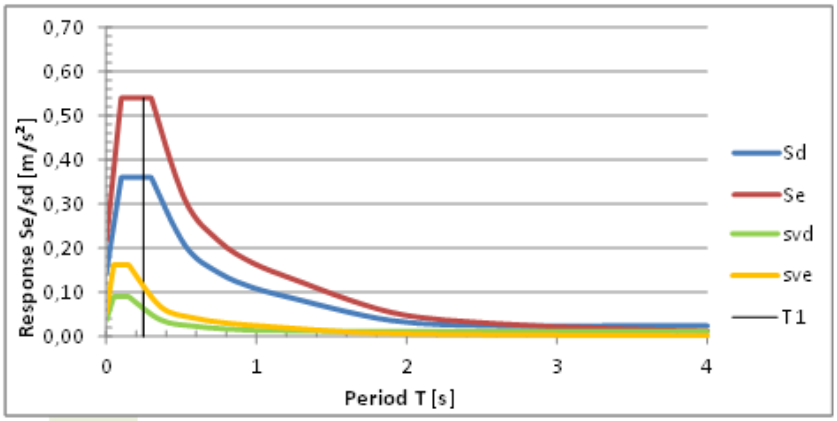
| | | | | | |
|---|---|---|---|---|---|
| National Annex: | | NBN | | Belgium NA | |
| Ground Type | | D | | | |
| Recommended elastic response spectra | | Type 2 | | Magnitude M < 5.5 | |
| Importance factor $\gamma_I$: | $\gamma_I$: | 1,2 | | Class: | III |
| Reference peak ground acceleration on type A ground: | $a_{gr}$: | 0,98 | $m/s^2$ | Zone: | 4 |
| Ground acceleration on type A ground $a_g$: | $a_g$: | 1,18 | $m/s^2$ | 0,12 | g |
| | $a_g \cdot S$: | 2,12 | $m/s^2$ | | |
| Gravitation: | g: | 9,81 | $m/s^2$ | | |
| Viscous damping ratio: | $\xi$: | 5,0 | % | EN 1998-1 chapt. 3.2.2.2 (1&4) | |
| Damping correction factor: | $\eta$: | 1,00 | | EN 1998-1 chapt. 3.2.2.2 (3) | |

Parameters Hor. elast resp. sp.

| | | | |
|---|---|---|---|
| Soil Factor: | S: | 1,80 | |
| Period $T_B$: | $T_B$: | 0,10 | s |
| Period $T_C$: | $T_C$: | 0,30 | s |
| Period $T_D$: | $T_D$: | 1,20 | s |

Parameters vert elast resp. sp.

| | | | |
|---|---|---|---|
| $A_{vg}/a_g$ | | 0,45 | |
| Period $T_B$: | $T_B$: | 0,05 | s |
| Period $T_C$: | $T_C$: | 0,15 | s |
| Period $T_D$: | $T_D$: | 1,00 | s |




Vertical ground ac $A_{vg}$: 0,53 $m/s^2$ 0,05 g

**Structural period**

| | | | | |
|---|---|---|---|---|
| Height of sturcture H: | | H: | 8,50 | m | |
| $C_T$ for: | Other structures | $C_T$: | 0,05 | | EN 1998-1 chapt. 4.3.3.2.2 (3) |
| Vibration period T: | | T: | 0,2489 | s | EN 1998-1 chapt. 4.3.3.2.2 (4.6) |

This calculation meets the requirements according to EN1998-1 chapter 4.3.3.2.1 (2) a)

**Calculation structural period**

| | | | |
|---|---|---|---|
| Number of storeys: | n: | 1 | |
| Correction factor: | $\lambda$: | 1,00 | |
| Behaviour factor q: | q: | 1,5 | EN 1998-1 chapt. 6.3.2 |
| Lower bound factor: | $\beta$: | 0,2 | EN 1998-1 chapt. 3.2.2.5(4) |

## 2.5.9 Brand

De constructie wordt getoetst aan de hand van de standaardbrand-kromme.

Voor het bepalen van de nodige dikte ($d_p$) zijn de materiaaleigenschappen van de veel gebruikte bekledingsmateriaal, profielvolgende bespuiting (mineraalvezels) gekozen als uitgangspunt.

Volumieke massa = 300 [kg/m³]
Thermische geleiding = 0,12 [W/m·K]
Specifieke hitte = 1200 [J/(kg·K)]

# 3 REKENMODEL

## 3.1 Constructieve overzicht

CUR-AANBEVELINGEN 065
Elastisch ondersteunde vloeren en verhardingen, in het werk gestort

| | | |
|---|---|---|
| Minimale dikte vloer | h = 160 mm | (4.4.2.1) |
| Minimale dikte verharding | h = 180 mm | (4.4.2.1) |
| Max. toelaatbare gem. scheurwijdte ter hoogte van de wapening | w ≤ 0,15 mm | (4.4.2.3) |
| Max. staafafstand | s = 100 mm | (4.4.2.3) |

Vrijdragende vloeren en in het werk gestorte wanden

| | | |
|---|---|---|
| Minimale dikte vloer | h = 160 mm | (4.4.3.1) |
| Minimale dikte wand | h = 200 mm | (4.4.3.1) |

De constructie bestaat uit een geschoord stalen frame. De vloer van de hal bestaat uit een monolitisch afgewerkte betonvloer. De fundatie bestaat uit een betonconstructie op staal gefundeerd.

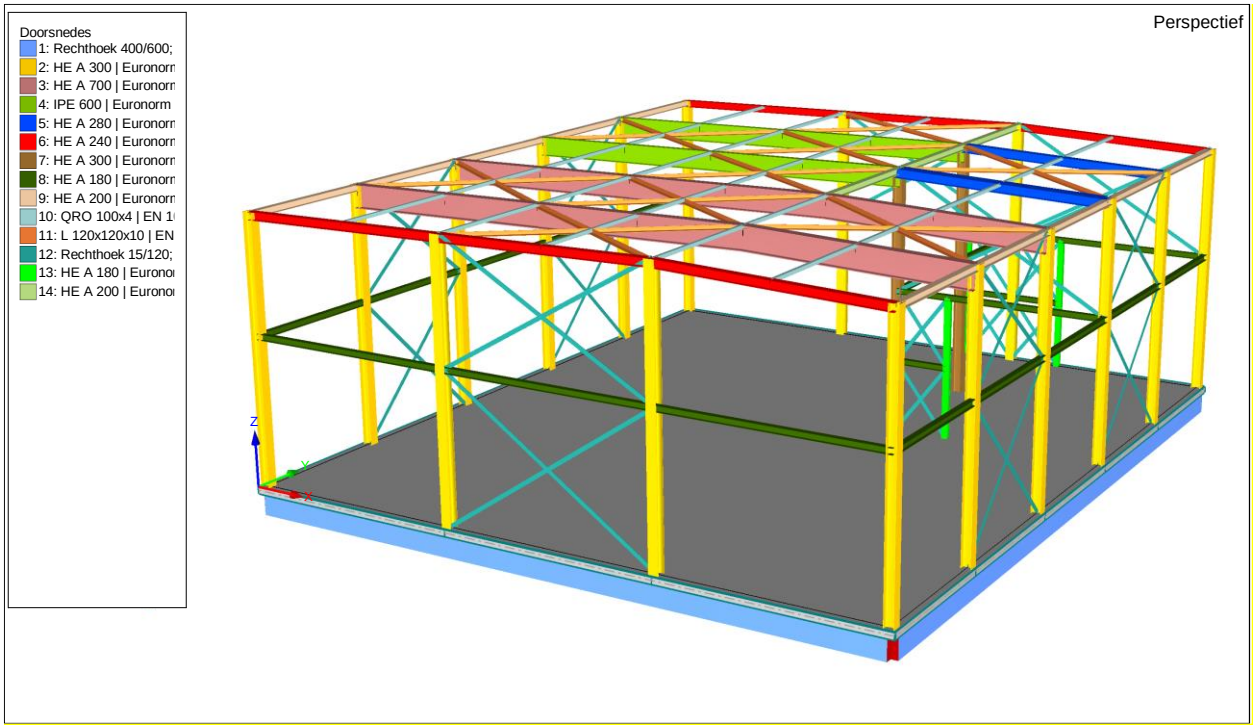
| | |
|---|---|
| Dakvloer | Stalen dakplaten |
| Begane grondvloer | In het werk gestort |
| Fundatie | Fundering op staal |
| Kolommen | Stalen kolommen |

De stabiliteit wordt verzorgd door stabiliteitskruizen in dak en gevels.

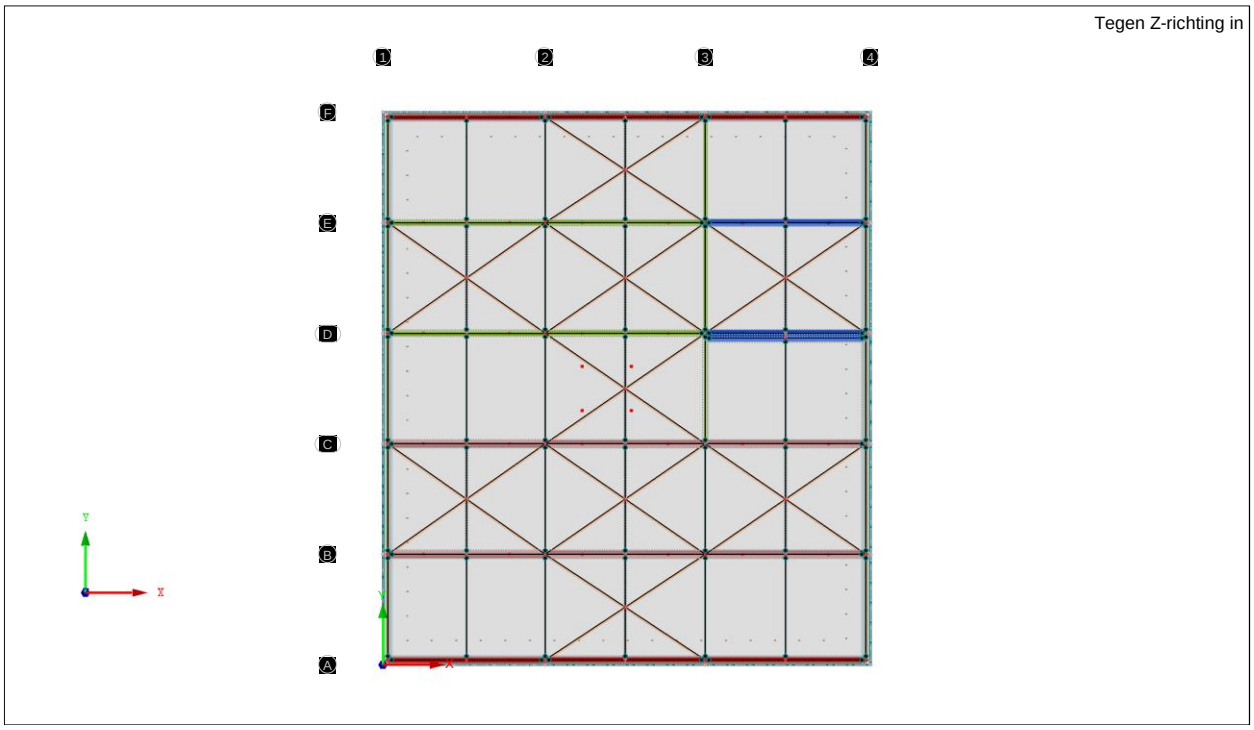
De belastingen die ontstaan ten gevolge van de uitvoering dienen door de aannemer tijdig te worden opgegeven en gecoordineerd met onder andere zijn leveranciers. Tenzij anders vermeld worden deze niet verwerkt in de berekening.

Tijdens de montagefase worden de verschillende constructie elementen geplaatst en gekoppeld. Elk element of samengesteld deel kan hierdoor tijdelijk een stabiliteitsvoorziening nodig hebben die in de eindfase niet noodzakelijk zal zijn.

Uitgangspunt is dat de verantwoordelijkheid voor de inzet van deze middelen tijdens de montage betreffende de standzekerheid van constructie elementen en samengestelde delen ligt bij de partij die deze montage verzorgt namen de hoofdaannemer. Zij (of de hoofdaannemer) zullen hierin het nodige advies dienen te verzorgen (montageplannen, werkplannen e.d.).




**Figuur 3.1: 3D overzicht rekenmodel**




**Figuur 3.2: Bovenaanzicht dakvlak**

De hal bestaat uit twee compartimenten, een grote en een kleine compartiment. Het kleine compartiment bevindt zich tussen As D tot en met As F en As 3 - As 4. De stalenconstructie van de hal is tot 60 minuten brandwerend. Aanvullend mag bij het bezwijken van de ene compartiment niet leiden tot het bezwijken van de ander compartiment. Om dit te realiseren zijn er op de knooppunten D3, E3 en F3 een kantelnok aanwezig. Bij hoge temperatuur kan de ligger vrij vervormen zonder de kolom mee te trekken.

# 4 RESULTATEN

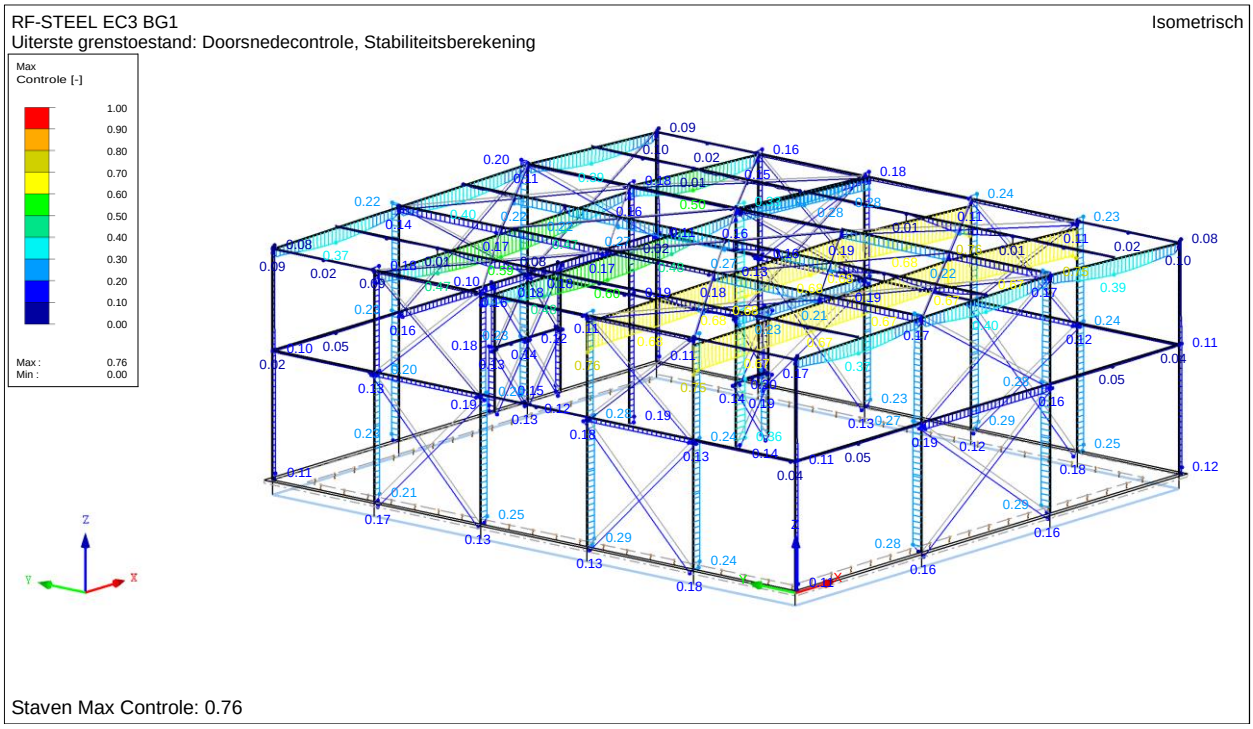
## 4.1 Opslaghal

In dit hoofdstuk worden de resultaten van het rekenmodel samengevat. Voor een gedetailleerde uiteenzetting van de resultaten, zie bijlage A, B en C. De plaatjes in dit rapport kunnen iets afwijken van de bijlage. De bijlage is in dat geval altijd leidend.

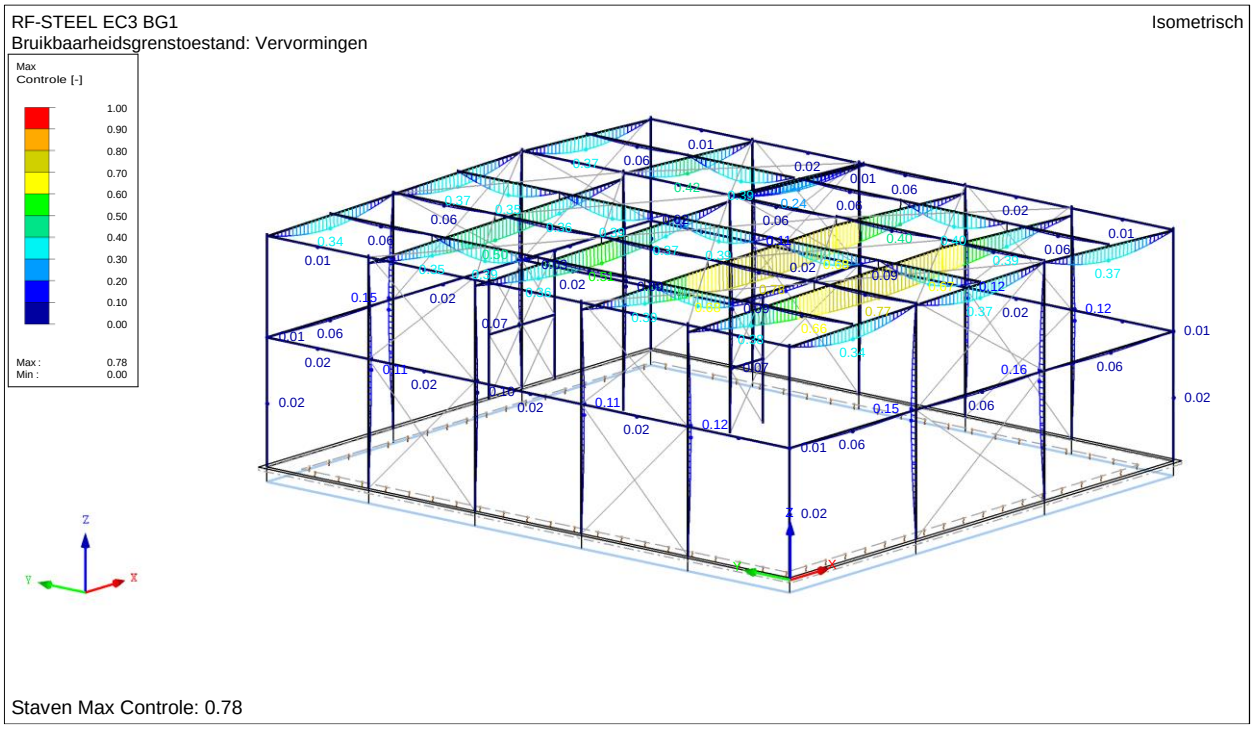
### 4.1.1 Staalcontrole

De staalconstructie is op elementniveau getoetst volgens de NEN-EN 1993-1-1, NEN-EN 1993-1-2 en NEN-EN 1998-1. Alle resulterende eenheidscontroles zijn kleiner dan of gelijk aan 1. Op elementniveau voldoet de staalconstructie dus aan de eisen voor wat betreft sterkte, stijfheid en stabiliteit.

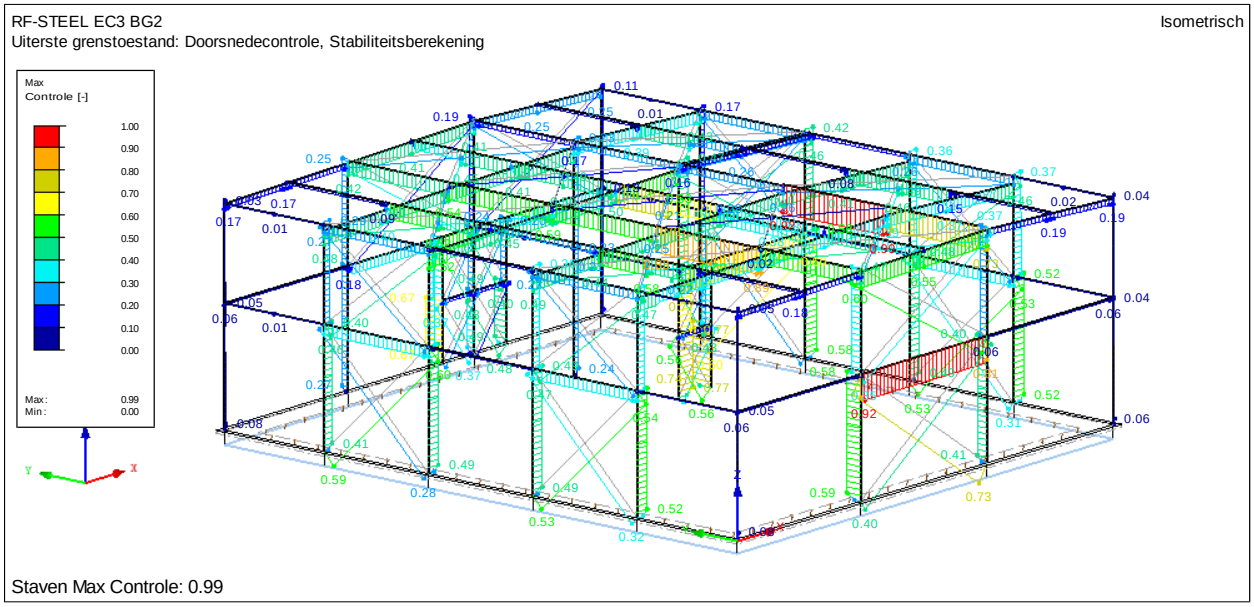
De maatgevende toetsing heeft een eenheidscontrole van 0,99 < 1. → **OK**



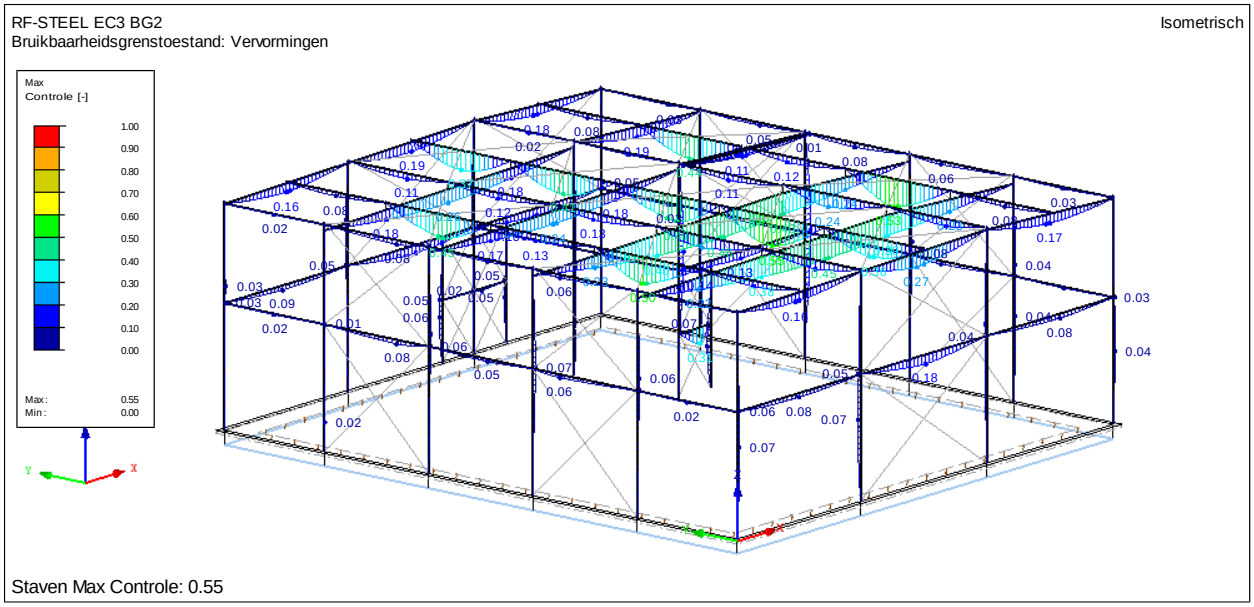

**Figuur 4.1: UGT eenheidscontrole**



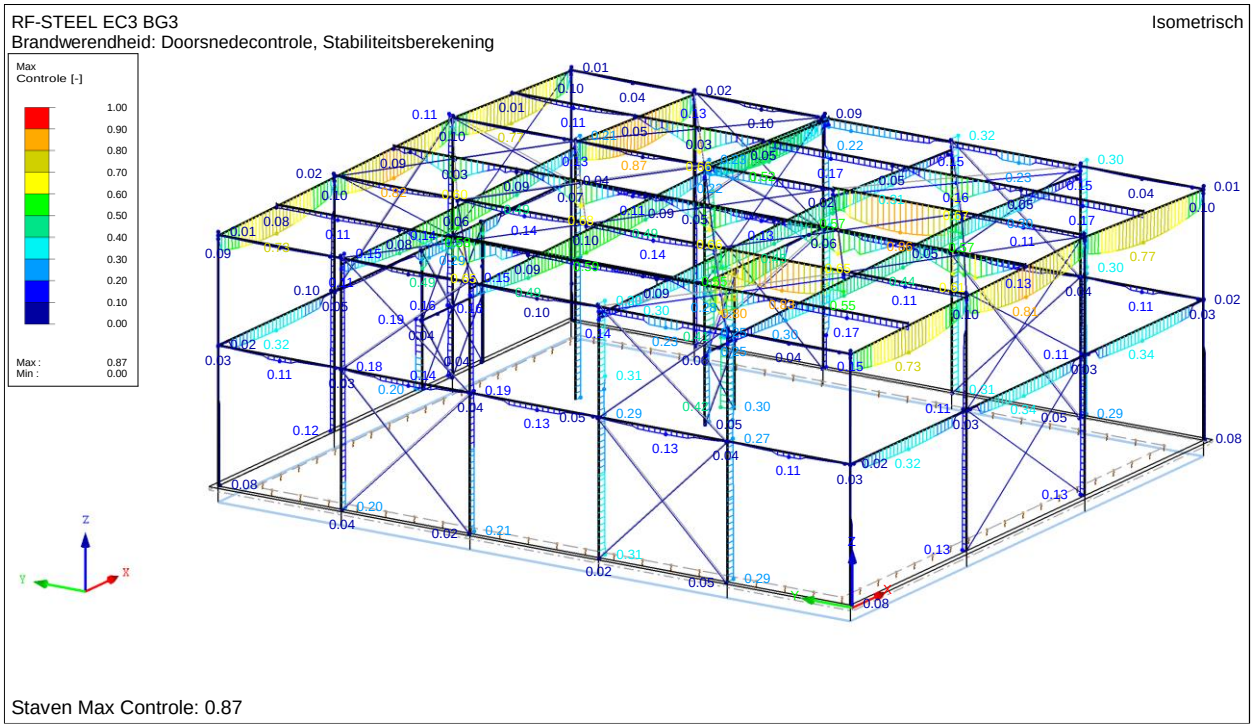

**Figuur 4.2: BGT eenheidscontrole**



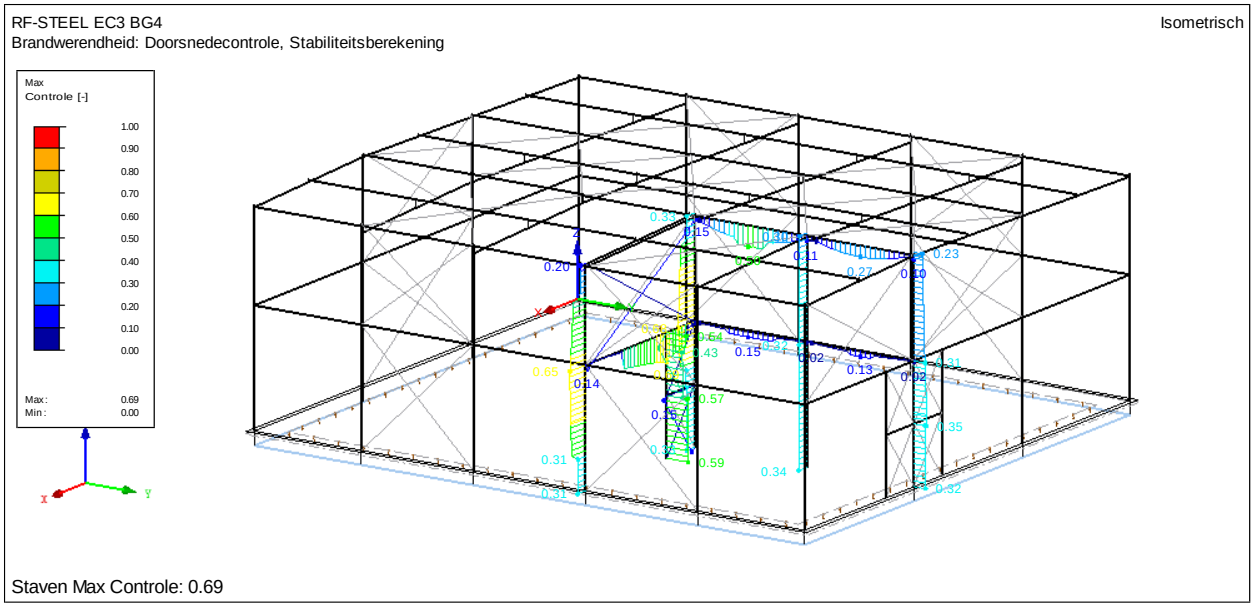

**Figuur 4.3: Aardbeving UGT eenheidscontrole**



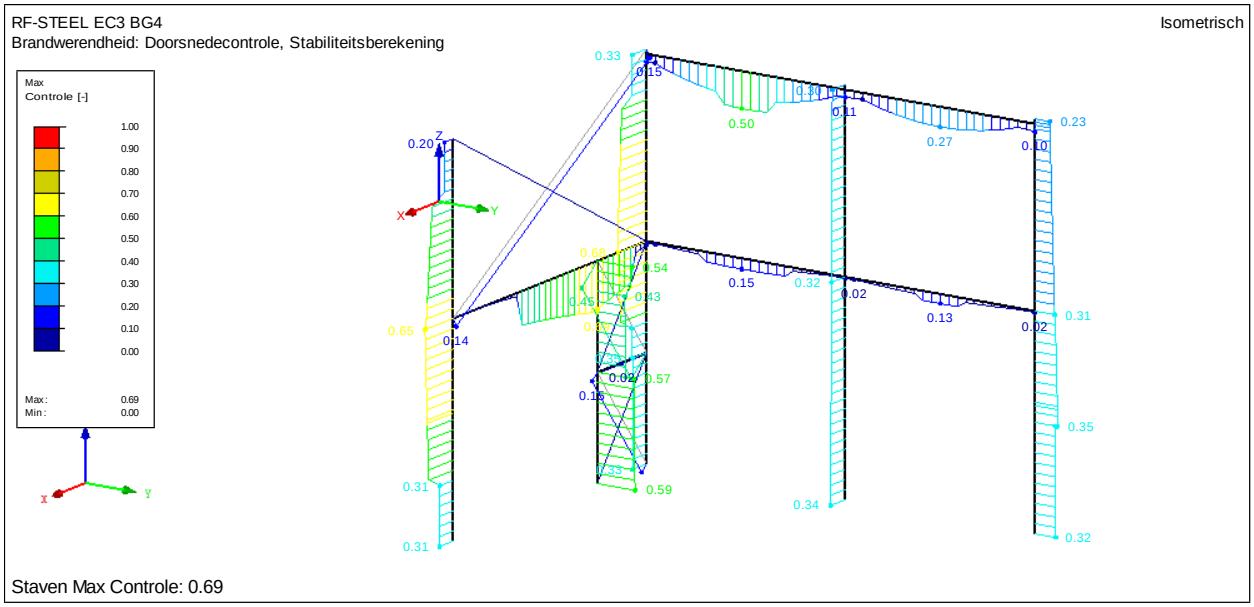

**Figuur 4.4: Aardbeving BGT eenheidscontrole**




**Figuur 4.5: 60min brandwerend eenheidscontrole**




**Figuur 4.6: 120min brandwerend eenheidscontrole**




**Figuur 4.7: 120min brandwerend eenheidscontrole**

Benodigde laagdikte voor de profielen op basis van de doorsnedenummering uit het rekenmodel:

| # | Doorsnede | Bij 60min brand toetsing $d_p$ [mm] | Bij 120min brand toetsing $d_p$ [mm] |
|---|---|---|---|
| 1 | Betonbalk | n.v.t. | n.v.t. |
| 2 | HEA300 | 5 | 15 |
| 3 | HEA700 | 10 | -- |
| 4 | IPE600 | 10 | -- |
| 5 | HEA280 | 10 | -- |
| 6 | HEA240 | 10 | -- |
| 7 | HEA300 | -- | 20 |
| 8 | HEA180 | 10 | 20 |
| 9 | HEA200 | 5 | -- |

| | | | |
|---|---|---|---|
| 10 | Koker 100x4 | 10 | -- |
| 11 | L120x120x10 | 5 | -- |
| 12 | Strip 15x120 | 5 | 10 |
| 13 | HEA180 | 5 | 15 |
| 14 | HEA200 | 5 | -- |

### 4.1.2 Vervorming

De horizontale verplaatsing mag niet groter zijn dan h/150 → 7850/150 = 52mm.
De maximale aanwezige horizontale verplaatsing is 6,6mm < 52mm → OK

Horizontale verplaatsing ten gevolge van aardbeving is 38,6mm.
NEN-EN 1998-1 (4.4.3.2): $d_r v \leq 0{,}0075h$ → $d_r \leq 0{,}0075 \cdot 7850mm / 0{,}4 = 147mm$
$d_r = q \cdot d_s = 1{,}5 \cdot 38{,}6mm = 57{,}9mm < 147mm$ → OK

### 4.1.3 Betoncontrole

De vloer en randbalken zijn getoetst volgens NEN-EN 1992-1-1, met de eisen uit CUR-065 voor wat betreft een vloeistofdichte vloer. Voor een gedetailleerde uiteenzetting van de resultaten, zie bijlage C.

Voor het bepalen van de wapening in de vloer is gebruik gemaakt van het rekenblad van CROW, scheurwijdte bij verhinderde vervorming.

Toegepaste wapening voor de vloer voor zowel boven als onder: # Ø12-75mm
Hiermee wordt aan de eis voldaan voor de scheurwijdte: $w_k = 0{,}12 < 0{,}15$

De optredende krachten in de randbalken zijn:
$M_{y,Ed}$ = 170kNm
$M_{z,Ed}$ = 29kNm
$V_{z,Ed}$ = 211kN
$V_{y,Ed}$ = 99kN
$M_{T,Ed}$ = 90kNm
$N_{,Ed}$ = -495kN/+263kN

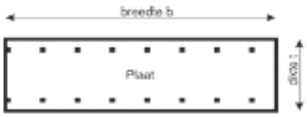
Toegepaste langswapening voor de randbalken voor zowel boven als onder: 4Ø16
Bijleggen staven Ø12, zie bijlage B en C voor hoeveelheid.
Zijwapening staven Ø12, zie bijlage B en C voor hoeveelheid.

Toegepaste beugels voor de randbalken:
Ø10 - 50-300mm, zie bijlage B en C voor hoeveelheid.

| | |
|---|---|
| project: 23920-21 | auteur: KCN |
| onderdeel: Vloer | datum: 21/09/2022 |
| omschrijving: | |

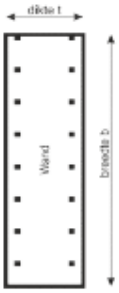
**Uitgangspunten**

| | | | | |
|---|---|---|---|---|
| betonkwaliteit | | C30/37 | | |
| karakteristieke cilinderdruksterkte | $f_{ck}$ = | 30 | MPa | |
| gemiddelde treksterkte | $f_{ctm}$ = | 2,9 | MPa | *(=0.3*fck^(2/3))* |
| secans-elasticiteitsmodulus | $E_{cm}$ = | 33 | GPa | *(= MROUND(22 * ((fck+8)/10)^0.3,1))* |
| wapening | | B500B | | |
| vloeisterkte | $f_{yk}$ = | 500 | MPa | |
| elasticiteitsmodulus | $E_s$ = | 200 | GPa | |




**Afmetingen**

| | | | | |
|---|---|---|---|---|
| totale breedte van de doorsnede | b = | 1000 | mm | |
| totale dikte van de doorsnede | t = | 200 | mm | |




**Wapening**

| | | | | |
|---|---|---|---|---|
| staafdiameter | $Ø_{km}$ = | 12 | mm | |
| staafafstand | $s_{wap}$ = | 75 | mm | |
| Uitgegaan wordt van symmetrische wapening in de doorsnede. | | | | |
| staaloppervlak in de totale doorsnede | $A_s$ = | 3.016 | mm² | *=2*PI()/4*Økm^2*b./swap* |
| dekking op berekende wapening | c = | 52 | mm | |

**Berekening scheurwijdte verhinderde vervorming**

| | | | | |
|---|---|---|---|---|
| oppervlakte beton in gehele doorsnede | $A_{ct}$ = | 0,200 | m² | *=b. * t. * 10^-6* |
| absolute wapeningspercentage | ρ = | 1,51% | | *=As / (Act*10^6)* |
| factor spreiding treksterkte | $\alpha_{ct}$ = | 0,70 | [-] | |
| treksterkte beton bij scheuren | $f_{ct.eff}$ = | 2,03 | MPa | *(=act * fctm)* |
| coëfficiënt eigenspanningen | k = | 1 | [-] | *=IF(t.<300,1, IF(t.>800,0.65, -7*10^-4*t.+1.21))* |
| zuivere trek | $k_c$ = | 1,00 | [-] | |
| scheurkracht betonnen doorsnede | $N_{cr}$ = | 443 | kN | *=Act*10^6 * fct.eff * (1 + αe*ρ) *k. *10^-3* |
| staalspanning na ontstaan scheur | $\sigma_s$ = | 147 | MPa | *=Ncr*10^3 / As* |

**CONTROLE** — **optredende staalspanning onder vloeispanning**

| | | | | |
|---|---|---|---|---|
| effectieve hoogte trekband | $h_{c.eff}$ = | 100 | mm | *=MIN(2.5*(c.+0.5*Økm), t./2)* |
| effectief oppervlak trekband | $A_{c.eff}$ = | 0,100 | m² | *=hc.eff * b. * 10^-6* |
| relatieve wapeningshoeveelheid | $\rho_{p.eff}$ = | 1,51% | | *=0.5*As / (Ac.eff*10^6)* |
| verhouding elasticiteitsmoduli | $\alpha_e$ = | 6,06 | [-] | *(=Es / Ecm)* |
| factor voor belastingduur | $k_t$ = | 0,40 | [-] | |
| gemiddelde rek | $\varepsilon_{sm}\_\varepsilon_{cm}$ = | 0,440 | [*10^-3] | *=MAX((σs-kt*fct.eff/ρp.eff*(1+αe*ρp.eff)), 0.6*σs) / Es* |
| coëfficiënt hechtende wapening | $k_1$ = | 0,80 | [-] | |
| coëfficiënt rekverdeling | $k_2$ = | 1,00 | [-] | |
| | $k_3$ = | 0,00 | [-] | |
| | $k_4$ = | 0,425 | [-] | |
| maximale scheurafstand | $s_{r.max}$ = | 271 | mm | *=k.3*c.+k.1*k.2*k.4*Økm/ρp.eff* |
| grenswaarde scheurafstand NB | $s_{r.NB}$ = | 312 | mm | *=MAX(50-0.8*fck, 15) * Økm* |
| berekende scheurwijdte | $w_k$ = | 0,12 | mm | *=MIN(sr.max,sr.NB) * (εsm_εcm*10^-3)* |

## 4.1.4 Ponscontrole

**Technosoft Construct release 6.71a 27 sep 2022**

Project : Opslaghal
Datum : 27/09/2022
Eenheden : kN/m/rad
Bestand : P:\ELMG_Celanese\23920-21 - PGS 15 Opslag - Basic Engineering\15_notities_intern\CB\Rekenmodellen\5000_00\Pons.cnw

### Toegepaste normen volgens Eurocode met Nederlandse NB

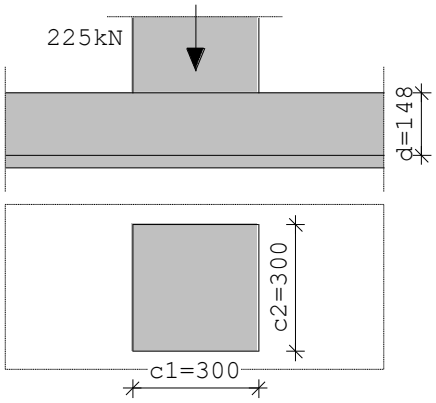
| | | | |
|---|---|---|---|
| Belastingen | NEN-EN 1990:2002 | C2:2010,A1:2019 | NB:2019(nl) |
| | NEN-EN 1991-1-1:2002 | C1/C11:2019 | NB:2019(nl) |
| Beton | NEN-EN 1992-1-1:2011(nl) | C2/A1:2015(nl) | NB:2016(nl) |

### Pons. (B)

**GEOMETRIE**

Kolomvorm : Rechthoekig
Vorm omtrek : Rechthoekig
Kolomsoort : Midden - op de vloer - art. 6.4.4 (2) (6.50)
Betonkwaliteit : C30/37
Nuttige hoogte d [mm]: 148

Kolom
Breedte lastvlak $c_1$ [mm]: 300 Lengte lastvlak $c_2$ [mm]: 300




**WAPENING**

Staalkwaliteit : B500A
Wapeningsratio $\rho_{l\,y}$ : 0.00700 Wapeningsratio $\rho_{l\,z}$ : 0.00700
Radiale afstand $s_r$ [mm]: 111 Tangentiële afstand $s_t$ [mm]: 222
Beugel diameter [mm]: 6 Hoek $\alpha$ : 90

**BELASTING**

Kracht $V_{E\,d}$ [kN]: 225.0

**RESULTATEN**

| Ponsomtrek | | $v_{Rd,c}$ | $v_{Rd,max}$ | $v_{Ed}$ | $v_{Rd,s}$ | $A_{sw}/s_r$ | $A_{sw}$ | code |
|---|---|---|---|---|---|---|---|---|
| | [mm] | [N/mm²] | [N/mm²] | [N/mm²] | [N/mm²] | [mm²/mm] | [mm²] | |
| $u_0$ | 1200 | n.v.t. | 4.22 | 1.46 | n.v.t. | n.v.t. | n.v.t. | |
| $u_1$ | 3060 | 0.66 | 4.22 | 0.57 | 0.00 | 0.00 | 0 | [42] |

**Opmerkingen**

[ 42] Er is geen ponswapening nodig (vEd < vRd,c).

**Controle-omtrek $u_0$ ( 1200 mm )**

Rekenwaarde schuifspanning volgens art. 6.4.5 (formule 6.53)
Nuttige plaatdikte d [mm]: 148 Omtrek $u_0$ [mm]: 1200
Factor β : 1.15
Schuifsp. $v_{Ed}$ [N/mm²]: 1.46 Schuifsp. $v_{Rd,max}$ [N/mm²]: 4.22

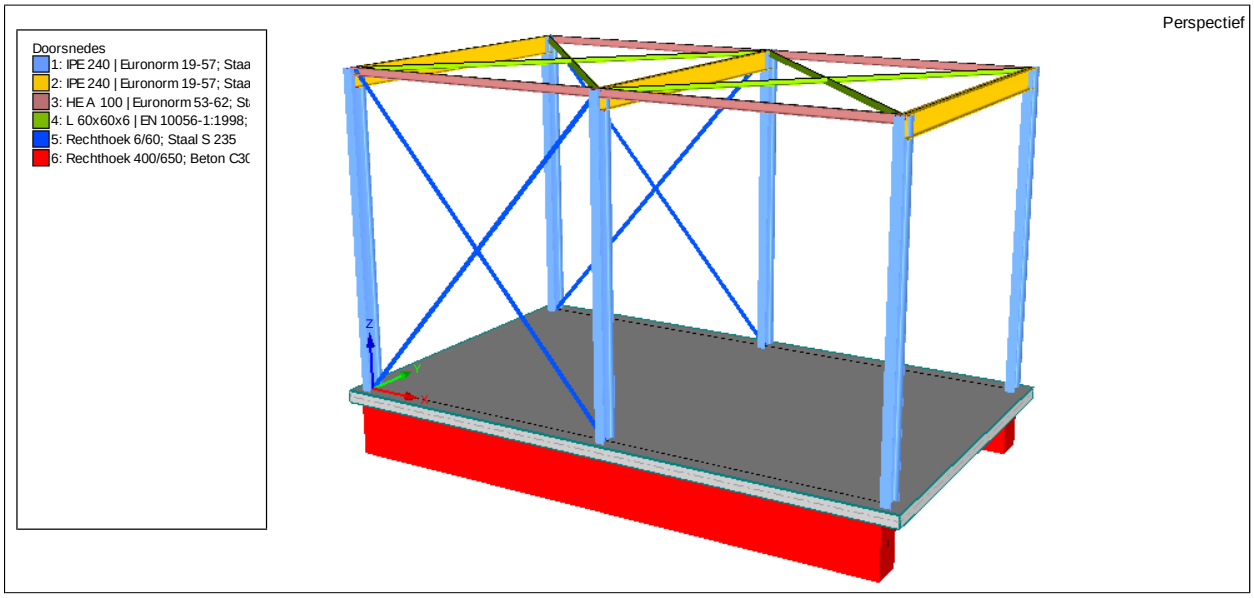
**Controle-omtrek $u_1$ ( 3060 mm )**

Vorm omtrek : Rechthoekig
Rekenwaarde schuifspanning volgens art. 6.4
Afstand tot aan kolom[mm]: 296
Nuttige plaatdikte d [mm]: 148 Omtrek $u_1$ [mm]: 3060
Factor β : 1.15
Schuifsp. $v_{Ed}$ [N/mm²]: 0.57
Schuifsp. $v_{Rd,c}$ [N/mm²]: 0.66

## 4.2 Sluis

In deze paragraaf worden de resultaten van het rekenmodel van de sluis samengevat. Voor een gedetailleerde uiteenzetting van de resultaten, zie bijlage D en E.

De sluis is onafhankelijk van de opslaghal en behoeft niet te worden getoetst op zowel brandbelasting als vloeistofdichtheid.

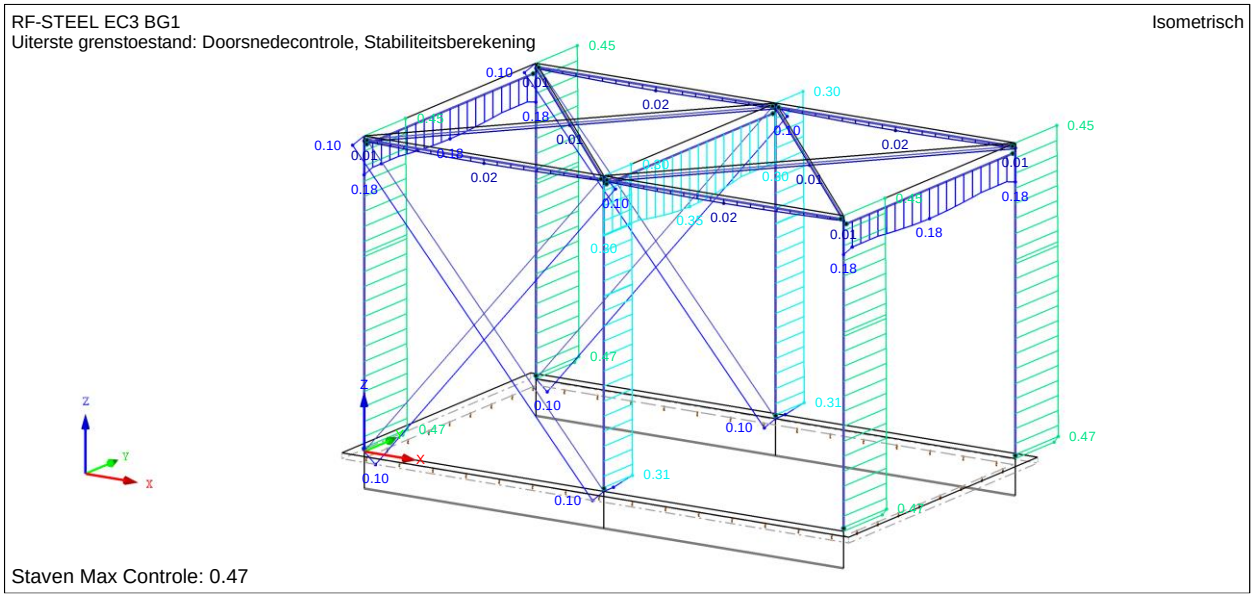



**Figuur 4.8: 3D overzicht rekenmodel sluis**

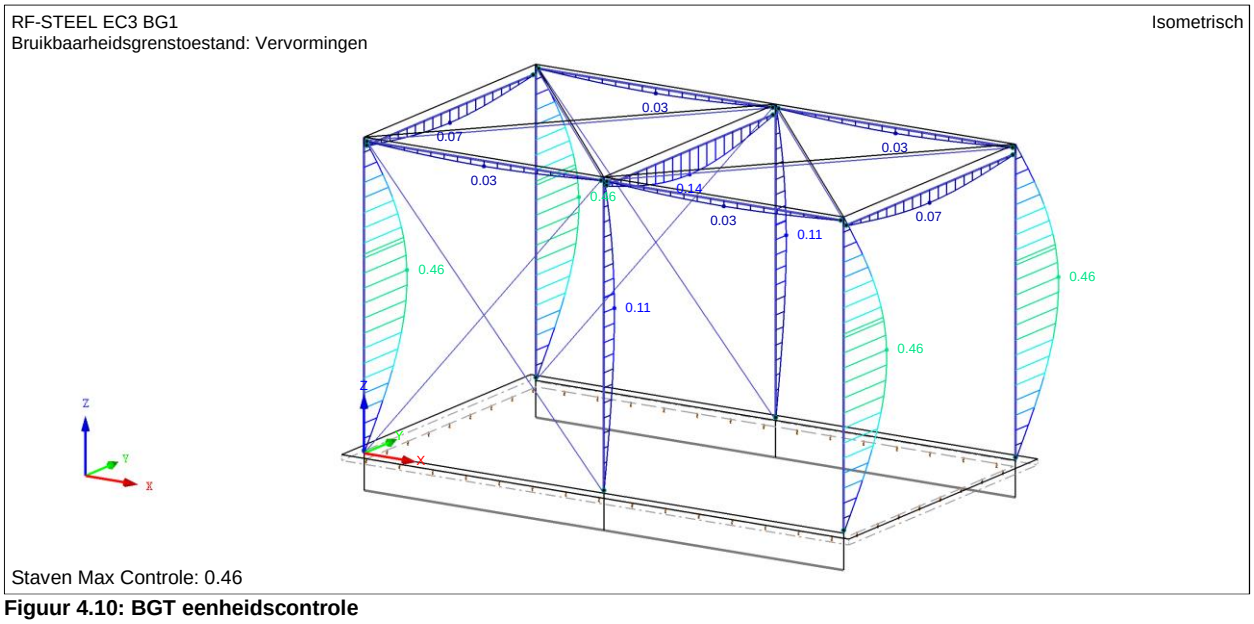
### 4.2.1 Staalcontrole

De staalconstructie is op elementniveau getoetst volgens de NEN-EN 1993-1-1 en NEN-EN 1998-1. Alle resulterende eenheidscontroles zijn kleiner dan of gelijk aan 1. Op elementniveau voldoet de staalconstructie dus aan de eisen voor wat betreft sterkte, stijfheid en stabiliteit.

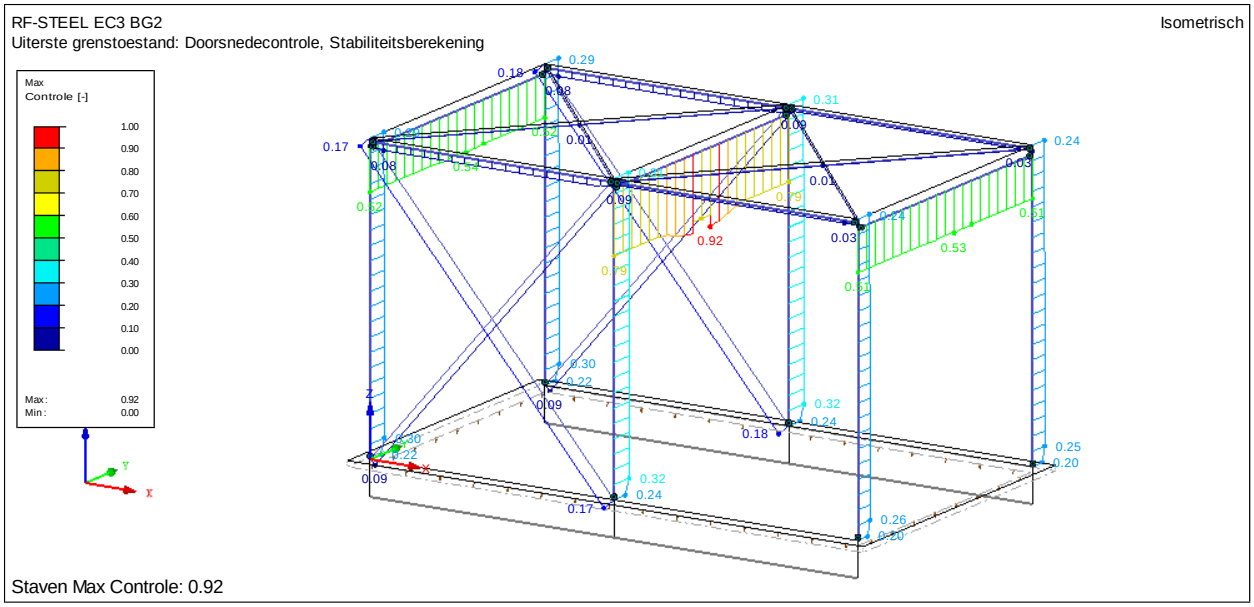
De maatgevende toetsing heeft een eenheidscontrole van 0,96 < 1. → **OK**



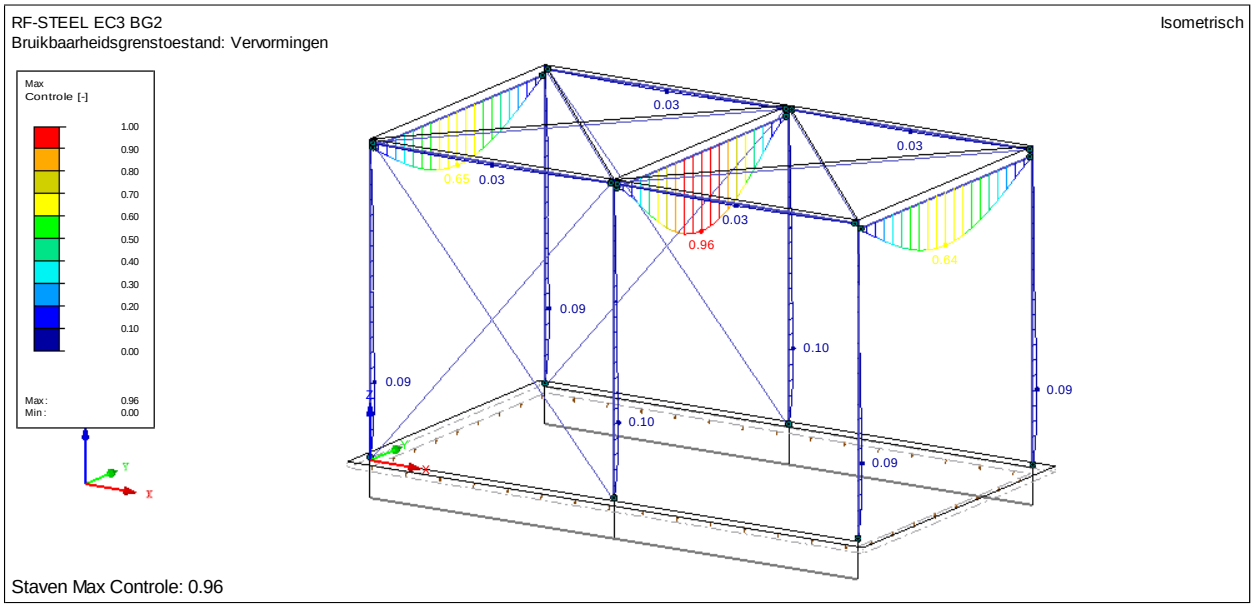

**Figuur 4.9: UGT eenheidscontrole**




**Figuur 4.10: BGT eenheidscontrole**




**Figuur 4.11: Aardbeving UGT eenheidscontrole**




**Figuur 4.12: Aardbeving BGT eenheidscontrole**

## 4.2.2 Vervorming

De horizontale verplaatsing mag niet groter zijn dan h/150 → 4050/150 = 27mm.
De maximale aanwezige horizontale verplaatsing is 17,6mm < 27mm → OK

Horizontale verplaatsing ten gevolge van aardbeving is 19,3mm.
NEN-EN 1998-1 (4.4.3.2): $d_rv \leq 0{,}0075h$ → $d_r \leq 0{,}0075 \cdot 4050mm / 0{,}4 = 76mm$
$d_r = q \cdot d_s = 1{,}5 \cdot 19{,}3mm = 29mm < 76mm$ → OK

### 4.2.3 Betoncontrole

Voor het bepalen van de wapening in de vloer is gebruik gemaakt van het rekenblad van CROW, scheurwijdte bij verhinderde vervorming.

Toegepaste wapening voor de vloer voor zowel boven als onder: # Ø12-150mm
Hiermee wordt aan de eis voldaan voor de scheurwijdte: $w_k = 0{,}26 < 0{,}30$

De optredende krachten in de randbalken zijn:

| | |
|---|---|
| $M_{y,Ed}$ | = 26kNm |
| $M_{z,Ed}$ | = 4kNm |
| $V_{z,Ed}$ | = 19kN |
| $V_{y,Ed}$ | = 7kN |
| $M_{T,Ed}$ | = 9kNm |
| $N_{,Ed}$ | = -10kN/+66kN |

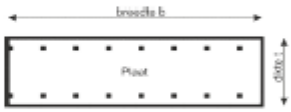
Toegepaste langswapening voor de randbalken voor zowel boven als onder: 3Ø16
Bijleggen staven Ø12, zie bijlage D en E voor hoeveelheid.
Zijwapening staven Ø12, zie bijlage D en E voor hoeveelheid.

Toegepaste beugels voor de randbalken:
Ø10 - 50-300mm, zie bijlage D en E voor hoeveelheid.

project: **23920-21** | auteur: **KCN**
onderdeel: **Sluis** | datum: **22/09/2022**
omschrijving:

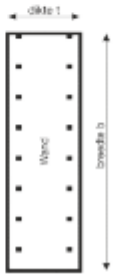
**Uitgangspunten**

| | | | | |
|---|---|---|---|---|
| betonkwaliteit | | C30/37 | | |
| karakteristieke cilinderdruksterkte | $f_{ck}$ = | 30 | MPa | |
| gemiddelde treksterkte | $f_{ctm}$ = | 2,9 | MPa | *(=0.3*fck^(2/3))* |
| secans-elasticiteitsmodulus | $E_{cm}$ = | 33 | GPa | *(= MROUND(22 * ((fck+8)/10)^0.3,1))* |
| wapening | | B500B | | |
| vloeisterkte | $f_{yk}$ = | 500 | MPa | |
| elasticiteitsmodulus | $E_s$ = | 200 | GPa | |




**Afmetingen**

| | | | |
|---|---|---|---|
| totale breedte van de doorsnede | b = | 1000 | mm |
| totale dikte van de doorsnede | t = | 200 | mm |




**Wapening**

| | | | | |
|---|---|---|---|---|
| staafdiameter | $Ø_{km}$ = | 12 | mm | |
| staafafstand | $s_{wap}$ = | 150 | mm | |
| Uitgegaan wordt van symmetrische wapening in de doorsnede. | | | | |
| staaloppervlak in de totale doorsnede | $A_s$ = | 1.508 | mm² | *=2*PI()/4*Økm^2*b./swap* |
| dekking op berekende wapening | c = | 42 | mm | |

**Berekening scheurwijdte verhinderde vervorming**

| | | | | |
|---|---|---|---|---|
| oppervlakte beton in gehele doorsnede | $A_{ct}$ = | 0,200 | m² | *=b. * t. * 10^-6* |
| absolute wapeningspercentage | ρ = | 0,75% | | *=As / (Act*10^6)* |
| factor spreiding treksterkte | $α_{ct}$ = | 0,70 | [-] | |
| treksterkte beton bij scheuren | $f_{ct.eff}$ = | 2,03 | MPa | *(=act * fctm)* |
| coëfficiënt eigenspanningen | k = | 1 | [-] | *=IF(t.<300,1, IF(t.>800,0.65, -7*10^-4*t.+1.21))* |
| zuivere trek | $k_c$ = | 1,00 | [-] | |
| scheurkracht betonnen doorsnede | $N_{cr}$ = | 424 | kN | *=Act*10^6 * fct.eff * (1 + αe*ρ) *k. *10^-3* |
| staalspanning na ontstaan scheur | $σ_s$ = | 281 | MPa | *=Ncr*10^3 / As* |

**CONTROLE** — **optredende staalspanning onder vloeispanning**

| | | | | |
|---|---|---|---|---|
| effectieve hoogte trekband | $h_{c.eff}$ = | 100 | mm | *=MIN(2.5*(c.+0.5*Økm), t./2)* |
| effectief oppervlak trekband | $A_{c.eff}$ = | 0,100 | m² | *=hc.eff * b. * 10^-6* |
| relatieve wapeningshoeveelheid | $ρ_{p.eff}$ = | 0,75% | | *=0.5*As / (Ac.eff*10^6)* |
| verhouding elasticiteitsmoduli | $α_e$ = | 6,06 | [-] | *(=Es / Ecm)* |
| factor voor belastingduur | $k_t$ = | 0,40 | [-] | |
| gemiddelde rek | $ε_{sm}-ε_{cm}$ = | 0,844 | [*10^-3] | *=MAX((σs-kt*fct.eff/ρp.eff*(1+αe*ρp.eff)), 0.6*σs) / Es* |
| coëfficiënt hechtende wapening | $k_1$ = | 0,80 | [-] | |
| coëfficiënt rekverdeling | $k_2$ = | 1,00 | [-] | |
| | $k_3$ = | 0,00 | [-] | |
| | $k_4$ = | 0,425 | [-] | |
| maximale scheurafstand | $s_{r.max}$ = | 541 | mm | *=k.3*c.+k.1*k.2*k.4*Økm/ρp.eff* |
| grenswaarde scheurafstand NB | $s_{r.NB}$ = | 312 | mm | *=MAX(50-0.8*fck, 15) * Økm* |
| berekende scheurwijdte | $w_k$ = | 0,26 | mm | *=MIN(sr.max,sr.NB) * (εsm_εcm*10^-3)* |

## 4.2.4 Ponscontrole

**Technosoft Construct release 6.71a** **28 sep 2022**

Project : Sluis
Datum : 28/09/2022
Eenheden : kN/m/rad
Bestand : P:\ELMG_Celanese\23920-21 - PGS 15 Opslag - Basic Engineering\15_notities_intern\CB\Rekenmodellen\5001_00\Pons_Sluis.cnw

### Toegepaste normen volgens Eurocode met Nederlandse NB

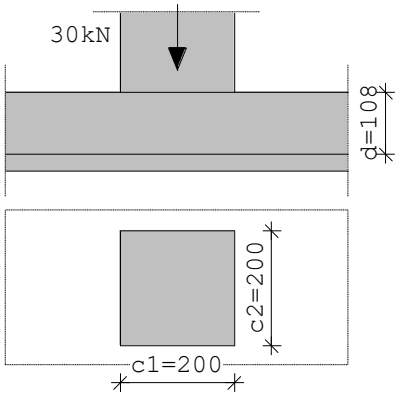
| | | | |
|---|---|---|---|
| Belastingen | NEN-EN 1990:2002 | C2:2010,A1:2019 | NB:2019(nl) |
| | NEN-EN 1991-1-1:2002 | C1/C11:2019 | NB:2019(nl) |
| Beton | NEN-EN 1992-1-1:2011(nl) | C2/A1:2015(nl) | NB:2016(nl) |

### Pons. (B)

**GEOMETRIE**

Kolomvorm : Rechthoekig
Vorm omtrek : Rechthoekig
Kolomsoort : Midden - op de vloer - art. 6.4.4 (2) (6.50)
Betonkwaliteit : C30/37
Nuttige hoogte d [mm]: 108

Kolom
Breedte lastvlak $c_1$ [mm]: 200 Lengte lastvlak $c_2$ [mm]: 200




**WAPENING**

Staalkwaliteit : B500A
Wapeningsratio $\rho_{1y}$ : 0.00500 Wapeningsratio $\rho_{1z}$ : 0.00500
Radiale afstand $s_r$ [mm]: 81 Tangentiële afstand $s_t$ [mm]: 162
Beugel diameter [mm]: 6 Hoek $\alpha$ : 90

**BELASTING**

Kracht $V_{Ed}$ [kN]: 30.0

**RESULTATEN**

| Ponsomtrek | | $v_{Rd,c}$ | $v_{Rd,max}$ | $v_{Ed}$ | $v_{Rd,s}$ | $A_{sw}/s_r$ | $A_{sw}$ | code |
|---|---|---|---|---|---|---|---|---|
| | [mm] | [N/mm²] | [N/mm²] | [N/mm²] | [N/mm²] | [mm²/mm] | [mm²] | |
| $u_0$ | 800 | n.v.t. | 4.22 | 0.40 | n.v.t. | n.v.t. | n.v.t. | |
| $u_1$ | 2157 | 0.59 | 4.22 | 0.15 | 0.00 | 0.00 | 0 | [42] |

## Opmerkingen

[ 42] Er is geen ponswapening nodig (vEd < vRd,c).

**Controle-omtrek $u_0$ ( 800 mm )**

Rekenwaarde schuifspanning volgens art. 6.4.5 (formule 6.53)
Nuttige plaatdikte d [mm]: 108 Omtrek $u_0$ [mm]: 800
Factor β : 1.15
Schuifsp. $v_{Ed}$ [N/mm²]: 0.40 Schuifsp. $v_{Rd,max}$ [N/mm²]: 4.22

**Controle-omtrek $u_1$ ( 2157 mm )**

Vorm omtrek : Rechthoekig
Rekenwaarde schuifspanning volgens art. 6.4
Afstand tot aan kolom[mm]: 216
Nuttige plaatdikte d [mm]: 108 Omtrek $u_1$ [mm]: 2157
Factor β : 1.15
Schuifsp. $v_{Ed}$ [N/mm²]: 0.15
Schuifsp. $v_{Rd,c}$ [N/mm²]: 0.59

# 5 CONCLUSIE

Alle berekende onderdelen voldoen aan de gestelde eisen wat betreft sterkte en vervorming bij toepassing van de in de berekening opgegeven afmetingen en materiaalkwaliteiten.

## INHOUD



## ALGEMENE GEGEVENS MODEL

| | | | |
|---|---|---|---|
| Algemeen | Modelnaam | : | 23920-21_5000_00_01_Opslaghal_050102022_1219 |
| | Modeltype | : | 3D |
| | Positieve richting van globale z-as | : | Naar Boven |
| | Classificatie van belastingsgevallen en combinaties | : | Volgens norm: EN 1990<br>Nationale Bijlage: NEN - Nederland |
| | ☒Combinaties automatisch aanmaken | : | ☒Belastingscombinaties |

| | | |
|---|---|---|
| Opties | ☐ | RF-FORM-FINDING - Vind aanvangsevenwichtsvormen van membranen en kabelconstructies |
| | ☐ | RF-CUTTING-PATTERN |
| | ☐ | Leidingwerk berekening |
| | ☐ | Gebruik CQC regel |
| | ☐ | CAD/BIM model mogelijk maken |

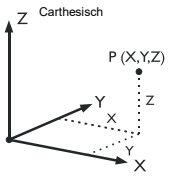
| | | |
|---|---|---|
| Standaard zwaartekracht | | |
| g | : | 10.00 m/s$^2$ |

## EE-NETINSTELLINGEN

| | | | | |
|---|---|---|---|---|
| Algemeen | Doellengte van eindige elementen | $l_{FE}$ | : | 500 mm |
| | Max. afstand tussen een knoop en een lijn om in de lijn te integreren | $\varepsilon$ | : | 1 mm |
| | Max. aantal netknopen (in duizenden) | | : | 500 |
| Staven | Aantal staafverdelingen van kabels, Elastische bedding, voutes of plastische karakteristiek | | : | 10 |
| | ☒ Stel staafverdelingen in voor grote vervorming of post-kritische berekening | | | |
| | ☒ Gebruik staafverdeling ook voor rechte staven, die niet zijn geï¿½ntegreerd in de vlakken, met | | : | Stel Lengte $l_{FE}$ in = 0 [mm] |
| | Min. aantal staafverdelingen | | : | 5 |
| | ☒ Gebruik staafverdeling door de knopen die op de staaf liggen | | | |
| Vlakken | Max. verh. van EE-rechthoekdiagonalen | $\Delta_D$ | : | 2 |
| | Max. uit-het-vlak hoek van twee EE | $\alpha$ | : | 0.50 ° |

## EE-NETINSTELLINGEN

uit het vlak
☒ Integreer ook ongebruikte objecten in de vlakken
Vorm van de eindige elementen : Driehoeken en schalen
☒Gelijke Vierhoeken genereren indien mogelijk




## 1.1 KNOPEN

| Knoop No. | Knooptype | Referentie knoop | Coï¿½rdinaten Syteem | Knoopcoï¿½rdinaten X [mm] | Y [mm] | Z [mm] | Opm. |
|---|---|---|---|---|---|---|---|
| 1 | Standaard | - | Carthesisch | 0 | 0 | 0 | |
| 2 | Standaard | - | Carthesisch | 19840 | 0 | 0 | |
| 3 | Standaard | - | Carthesisch | 19840 | 22500 | 0 | |
| 4 | Standaard | - | Carthesisch | 0 | 22500 | 0 | |
| 5 | Standaard | - | Carthesisch | 200 | 200 | 0 | |
| 6 | Standaard | - | Carthesisch | 19640 | 200 | 0 | |
| 7 | Standaard | - | Carthesisch | 19640 | 22300 | 0 | |
| 8 | Standaard | - | Carthesisch | 200 | 22300 | 0 | |
| 9 | Standaard | - | Carthesisch | 200 | 200 | 4345 | |
| 10 | Standaard | - | Carthesisch | 6600 | 0 | 0 | |
| 11 | Standaard | - | Carthesisch | 13110 | 0 | 0 | |
| 12 | Standaard | - | Carthesisch | 19640 | 200 | 4345 | |
| 13 | Standaard | - | Carthesisch | 200 | 200 | 2500 | |
| 14 | Standaard | - | Carthesisch | 0 | 4500 | 0 | |
| 15 | Standaard | - | Carthesisch | 19840 | 4500 | 0 | |
| 16 | Standaard | - | Carthesisch | 200 | 22300 | 4345 | |
| 17 | Standaard | - | Carthesisch | 19640 | 22300 | 4345 | |
| 18 | Standaard | - | Carthesisch | 19640 | 200 | 2500 | |
| 19 | Standaard | - | Carthesisch | 0 | 9000 | 0 | |
| 20 | Standaard | - | Carthesisch | 19840 | 9000 | 0 | |
| 21 | Standaard | - | Carthesisch | 19640 | 22300 | 2500 | |
| 22 | Standaard | - | Carthesisch | 200 | 22300 | 2500 | |
| 23 | Standaard | - | Carthesisch | 3400 | 6750 | 7910 | |
| 24 | Standaard | - | Carthesisch | 0 | 13500 | 0 | |
| 25 | Standaard | - | Carthesisch | 19840 | 13500 | 0 | |
| 26 | Standaard | - | Carthesisch | 3400 | 15750 | 7910 | |
| 27 | Standaard | - | Carthesisch | 9855 | 2350 | 8032 | |
| 28 | Standaard | - | Carthesisch | 9855 | 6750 | 8032 | |
| 29 | Standaard | - | Carthesisch | 0 | 18000 | 0 | |
| 30 | Standaard | - | Carthesisch | 19840 | 18000 | 0 | |
| 31 | Standaard | - | Carthesisch | 9855 | 11250 | 8032 | |
| 32 | Standaard | - | Carthesisch | 9855 | 15750 | 8032 | |
| 33 | Standaard | - | Carthesisch | 9855 | 20150 | 8032 | |
| 34 | Standaard | - | Carthesisch | 6600 | 22500 | 0 | |
| 35 | Standaard | - | Carthesisch | 6600 | 200 | 7970 | |
| 36 | Standaard | - | Carthesisch | 19640 | 4500 | 0 | |
| 37 | Standaard | - | Carthesisch | 19640 | 4500 | 7850 | |
| 38 | Standaard | - | Carthesisch | 16375 | 6750 | 7972 | |
| 39 | Standaard | - | Carthesisch | 13110 | 200 | 8093 | |
| 40 | Standaard | - | Carthesisch | 13110 | 22500 | 0 | |
| 41 | Standaard | - | Carthesisch | 6600 | 22300 | 7970 | |
| 42 | Standaard | - | Carthesisch | 13110 | 22300 | 8093 | |
| 43 | Standaard | - | Carthesisch | 13110 | 18000 | 0 | |
| 44 | Standaard | - | Carthesisch | 6600 | 200 | 0 | |
| 45 | Standaard | - | Carthesisch | 200 | 200 | 7850 | |
| 46 | Standaard | - | Carthesisch | 19640 | 200 | 7850 | |
| 47 | Standaard | - | Carthesisch | 13110 | 200 | 0 | |
| 48 | Standaard | - | Carthesisch | 200 | 4500 | 0 | |
| 49 | Standaard | - | Carthesisch | 200 | 4500 | 7850 | |
| 50 | Standaard | - | Carthesisch | 200 | 9000 | 0 | |
| 51 | Standaard | - | Carthesisch | 200 | 9000 | 7850 | |
| 52 | Standaard | - | Carthesisch | 200 | 13500 | 0 | |
| 53 | Standaard | - | Carthesisch | 200 | 13500 | 7850 | |
| 54 | Standaard | - | Carthesisch | 200 | 18000 | 0 | |
| 55 | Standaard | - | Carthesisch | 200 | 18000 | 7850 | |
| 56 | Standaard | - | Carthesisch | 200 | 22300 | 7850 | |
| 57 | Standaard | - | Carthesisch | 19640 | 22300 | 7850 | |
| 58 | Standaard | - | Carthesisch | 6600 | 22300 | 0 | |
| 59 | Standaard | - | Carthesisch | 13110 | 22300 | 0 | |
| 60 | Standaard | - | Carthesisch | 19640 | 9000 | 0 | |
| 61 | Standaard | - | Carthesisch | 19640 | 9000 | 7850 | |
| 62 | Standaard | - | Carthesisch | 19640 | 13500 | 0 | |
| 63 | Standaard | - | Carthesisch | 19640 | 13500 | 7850 | |
| 64 | Standaard | - | Carthesisch | 19640 | 18000 | 0 | |
| 65 | Standaard | - | Carthesisch | 19640 | 18000 | 7850 | |
| 66 | Standaard | - | Carthesisch | 13110 | 13500 | 0 | |
| 67 | Standaard | - | Carthesisch | 13110 | 18000 | 8093 | |
| 68 | Standaard | - | Carthesisch | 13110 | 13500 | 8093 | |
| 69 | Standaard | - | Carthesisch | 6600 | 200 | 4345 | |
| 70 | Standaard | - | Carthesisch | 13110 | 200 | 4345 | |
| 71 | Standaard | - | Carthesisch | 200 | 4500 | 4345 | |
| 72 | Standaard | - | Carthesisch | 200 | 9000 | 4345 | |
| 73 | Standaard | - | Carthesisch | 200 | 13500 | 4345 | |
| 74 | Standaard | - | Carthesisch | 200 | 18000 | 4345 | |
| 75 | Standaard | - | Carthesisch | 19640 | 4500 | 4345 | |
| 76 | Standaard | - | Carthesisch | 19640 | 9000 | 4345 | |
| 77 | Standaard | - | Carthesisch | 19640 | 13500 | 4345 | |
| 78 | Standaard | - | Carthesisch | 19640 | 18000 | 4345 | |
| 79 | Standaard | - | Carthesisch | 6600 | 22300 | 4345 | |
| 80 | Standaard | - | Carthesisch | 13110 | 22300 | 4345 | |
| 81 | Standaard | - | Carthesisch | 6600 | 4500 | 7970 | |
| 82 | Standaard | - | Carthesisch | 6600 | 9000 | 7970 | |
| 83 | Standaard | - | Carthesisch | 6600 | 13500 | 7970 | |
| 84 | Standaard | - | Carthesisch | 6600 | 18000 | 7970 | |
| 85 | Standaard | - | Carthesisch | 13110 | 4500 | 8093 | |

## 1.1 KNOPEN

| Knoop No. | Knooptype | Referentie knoop | Coï¿½rdinaten Syteem | Knoopcoï¿½rdinaten X [mm] | Y [mm] | Z [mm] | Opm. |
|---|---|---|---|---|---|---|---|
| 86 | Standaard | - | Carthesisch | 13110 | 9000 | 8093 | |
| 87 | Standaard | - | Carthesisch | 13110 | 18000 | 4345 | |
| 88 | Standaard | - | Carthesisch | 13110 | 13500 | 4345 | |
| 89 | Standaard | - | Carthesisch | 14775 | 22300 | 4345 | |
| 90 | Standaard | - | Carthesisch | 14775 | 22300 | 0 | |
| 91 | Standaard | - | Carthesisch | 14775 | 22300 | 2173 | |
| 92 | Standaard | - | Carthesisch | 13110 | 22300 | 2173 | |
| 93 | Standaard | - | Carthesisch | 11445 | 22300 | 4345 | |
| 94 | Standaard | - | Carthesisch | 11445 | 22300 | 0 | |
| 95 | Standaard | - | Carthesisch | 11445 | 22300 | 2173 | |
| 96 | Standaard | - | Carthesisch | 14775 | 13500 | 4345 | |
| 97 | Standaard | - | Carthesisch | 14775 | 13500 | 0 | |
| 98 | Standaard | - | Carthesisch | 14775 | 13500 | 2173 | |
| 99 | Standaard | - | Carthesisch | 13110 | 13500 | 2173 | |
| 100 | Standaard | - | Carthesisch | 5150 | 200 | 0 | |
| 101 | Standaard | - | Carthesisch | 19640 | 13300 | 7850 | |
| 102 | Standaard | - | Carthesisch | 13110 | 13300 | 8093 | |
| 103 | Standaard | - | Carthesisch | 1650 | 200 | 0 | |
| 104 | Standaard | - | Carthesisch | 8105 | 200 | 0 | |
| 105 | Standaard | - | Carthesisch | 11605 | 200 | 0 | |
| 106 | Standaard | - | Carthesisch | 14625 | 200 | 0 | |
| 107 | Standaard | - | Carthesisch | 18125 | 200 | 0 | |
| 108 | Standaard | - | Carthesisch | 6600 | 9000 | 0 | |
| 109 | Standaard | - | Carthesisch | 13110 | 9000 | 0 | |
| 110 | Standaard | - | Carthesisch | 5150 | 9000 | 0 | |
| 111 | Standaard | - | Carthesisch | 1650 | 9000 | 0 | |
| 112 | Standaard | - | Carthesisch | 8105 | 9000 | 0 | |
| 113 | Standaard | - | Carthesisch | 11605 | 9000 | 0 | |
| 114 | Standaard | - | Carthesisch | 14625 | 9000 | 0 | |
| 115 | Standaard | - | Carthesisch | 18125 | 9000 | 0 | |
| 116 | Standaard | - | Carthesisch | 6600 | 13500 | 0 | |
| 117 | Standaard | - | Carthesisch | 5150 | 13500 | 0 | |
| 118 | Standaard | - | Carthesisch | 1650 | 13500 | 0 | |
| 119 | Standaard | - | Carthesisch | 8105 | 13500 | 0 | |
| 120 | Standaard | - | Carthesisch | 11605 | 13500 | 0 | |
| 121 | Standaard | - | Carthesisch | 14625 | 13500 | 0 | |
| 122 | Standaard | - | Carthesisch | 18125 | 13500 | 0 | |
| 123 | Standaard | - | Carthesisch | 5150 | 22300 | 0 | |
| 124 | Standaard | - | Carthesisch | 1650 | 22300 | 0 | |
| 125 | Standaard | - | Carthesisch | 8105 | 22300 | 0 | |
| 126 | Standaard | - | Carthesisch | 11605 | 22300 | 0 | |
| 127 | Standaard | - | Carthesisch | 14625 | 22300 | 0 | |
| 128 | Standaard | - | Carthesisch | 18125 | 22300 | 0 | |
| 129 | Standaard | - | Carthesisch | 5150 | 4500 | 0 | |
| 130 | Standaard | - | Carthesisch | 1650 | 4500 | 0 | |
| 131 | Standaard | - | Carthesisch | 8105 | 4500 | 0 | |
| 132 | Standaard | - | Carthesisch | 11605 | 4500 | 0 | |
| 133 | Standaard | - | Carthesisch | 14625 | 4500 | 0 | |
| 134 | Standaard | - | Carthesisch | 18125 | 4500 | 0 | |
| 135 | Standaard | - | Carthesisch | 5150 | 18000 | 0 | |
| 136 | Standaard | - | Carthesisch | 1650 | 18000 | 0 | |
| 137 | Standaard | - | Carthesisch | 8105 | 18000 | 0 | |
| 138 | Standaard | - | Carthesisch | 11605 | 18000 | 0 | |
| 139 | Standaard | - | Carthesisch | 14625 | 18000 | 0 | |
| 140 | Standaard | - | Carthesisch | 18125 | 18000 | 0 | |
| 141 | Standaard | - | Carthesisch | 8105 | 12150 | 0 | |
| 142 | Standaard | - | Carthesisch | 8105 | 10350 | 0 | |
| 143 | Standaard | - | Carthesisch | 10105 | 12150 | 0 | |
| 144 | Standaard | - | Carthesisch | 10105 | 10350 | 0 | |
| 145 | Standaard | - | Carthesisch | 3400 | 22300 | 7910 | |
| 146 | Standaard | - | Carthesisch | 3400 | 18000 | 7910 | |
| 147 | Standaard | - | Carthesisch | 3400 | 13500 | 7910 | |
| 148 | Standaard | - | Carthesisch | 3400 | 9000 | 7910 | |
| 149 | Standaard | - | Carthesisch | 3400 | 4500 | 7910 | |
| 150 | Standaard | - | Carthesisch | 3400 | 200 | 7910 | |
| 151 | Standaard | - | Carthesisch | 9855 | 22300 | 8032 | |
| 152 | Standaard | - | Carthesisch | 9855 | 18000 | 8032 | |
| 153 | Standaard | - | Carthesisch | 9855 | 13500 | 8032 | |
| 154 | Standaard | - | Carthesisch | 9855 | 9000 | 8032 | |
| 155 | Standaard | - | Carthesisch | 9855 | 4500 | 8032 | |
| 156 | Standaard | - | Carthesisch | 9855 | 200 | 8032 | |
| 157 | Standaard | - | Carthesisch | 16375 | 22300 | 7972 | |
| 158 | Standaard | - | Carthesisch | 16375 | 18000 | 7972 | |
| 159 | Standaard | - | Carthesisch | 16375 | 13500 | 7972 | |
| 160 | Standaard | - | Carthesisch | 16375 | 13300 | 7972 | |
| 161 | Standaard | - | Carthesisch | 16375 | 9000 | 7972 | |
| 162 | Standaard | - | Carthesisch | 16375 | 4500 | 7972 | |
| 163 | Standaard | - | Carthesisch | 16375 | 200 | 7972 | |
| 164 | Standaard | - | Carthesisch | 16375 | 15750 | 7972 | |

## 1.2 LIJNEN

| Lijn No. | Lijntype | Knopen No. | Lijnlengte L [mm] | | Opm. |
|---|---|---|---|---|---|
| 1 | Polylijn | 1,10 | 6600 | X | |
| 2 | Polylijn | 2,15 | 4500 | Y | |
| 3 | Polylijn | 3,40 | 6730 | X | |
| 4 | Polylijn | 4,29 | 4500 | Y | |
| 5 | Polylijn | 5,44 | 6400 | X | |
| 6 | Polylijn | 6,36 | 4300 | Y | |
| 7 | Polylijn | 7,59 | 6530 | X | |
| 8 | Polylijn | 8,54 | 4300 | Y | |

## 1.2 LIJNEN

| Lijn No. | Lijntype | Knopen No. | Lijnlengte L [mm] | | Opm. |
|---|---|---|---|---|---|
| 9 | Polylijn | 5,9 | 4345 | Z | |
| 10 | Polylijn | 6,12 | 4345 | Z | |
| 11 | Polylijn | 45,150 | 3201 | XZ | |
| 12 | Polylijn | 46,163 | 3267 | XZ | |
| 13 | Polylijn | 48,71 | 4345 | Z | |
| 14 | Polylijn | 36,75 | 4345 | Z | |
| 15 | Polylijn | 49,149 | 3201 | XZ | |
| 16 | Polylijn | 37,162 | 3267 | XZ | |
| 17 | Polylijn | 15,20 | 4500 | Y | |
| 18 | Polylijn | 14,1 | 4500 | Y | |
| 19 | Polylijn | 50,72 | 4345 | Z | |
| 20 | Polylijn | 60,76 | 4345 | Z | |
| 21 | Polylijn | 51,148 | 3201 | XZ | |
| 22 | Polylijn | 61,161 | 3267 | XZ | |
| 23 | Polylijn | 19,14 | 4500 | Y | |
| 24 | Polylijn | 20,25 | 4500 | Y | |
| 25 | Polylijn | 52,73 | 4345 | Z | |
| 26 | Polylijn | 62,77 | 4345 | Z | |
| 27 | Polylijn | 53,147 | 3201 | XZ | |
| 28 | Polylijn | 63,159 | 3267 | XZ | |
| 29 | Polylijn | 24,19 | 4500 | Y | |
| 30 | Polylijn | 25,30 | 4500 | Y | |
| 31 | Polylijn | 54,74 | 4345 | Z | |
| 32 | Polylijn | 64,78 | 4345 | Z | |
| 33 | Polylijn | 55,146 | 3201 | XZ | |
| 34 | Polylijn | 65,158 | 3267 | XZ | |
| 35 | Polylijn | 29,24 | 4500 | Y | |
| 36 | Polylijn | 30,3 | 4500 | Y | |
| 37 | Polylijn | 8,16 | 4345 | Z | |
| 38 | Polylijn | 7,17 | 4345 | Z | |
| 39 | Polylijn | 56,145 | 3201 | XZ | |
| 40 | Polylijn | 57,157 | 3267 | XZ | |
| 41 | Polylijn | 44,69 | 4345 | Z | |
| 42 | Polylijn | 10,11 | 6510 | X | |
| 43 | Polylijn | 47,70 | 4345 | Z | |
| 44 | Polylijn | 11,2 | 6730 | X | |
| 45 | Polylijn | 58,79 | 4345 | Z | |
| 46 | Polylijn | 59,92 | 2173 | Z | |
| 47 | Polylijn | 40,34 | 6510 | X | |
| 48 | Polylijn | 34,4 | 6600 | X | |
| 49 | Polylijn | 90,91 | 2173 | Z | |
| 50 | Polylijn | 42,151 | 3256 | XZ | |
| 51 | Polylijn | 44,47 | 6510 | X | |
| 52 | Polylijn | 47,6 | 6530 | X | |
| 53 | Polylijn | 79,42 | 7512 | XZ | |
| 54 | Polylijn | 39,156 | 3256 | XZ | |
| 55 | Polylijn | 54,52 | 4500 | Y | |
| 56 | Polylijn | 52,50 | 4500 | Y | |
| 57 | Polylijn | 50,48 | 4500 | Y | |
| 58 | Polylijn | 48,5 | 4300 | Y | |
| 59 | Polylijn | 43,87 | 4345 | Z | |
| 60 | Polylijn | 66,99 | 2173 | Z | |
| 61 | Polylijn | 67,152 | 3256 | XZ | |
| 62 | Polylijn | 68,153 | 3256 | XZ | |
| 63 | Polylijn | 9,69 | 6400 | X | |
| 64 | Polylijn | 69,70 | 6510 | X | |
| 65 | Polylijn | 70,12 | 6530 | X | |
| 66 | Polylijn | 16,79 | 6400 | X | |
| 67 | Polylijn | 79,93 | 4845 | X | |
| 68 | Polylijn | 80,89 | 1665 | X | |
| 69 | Polylijn | 9,71 | 4300 | Y | |
| 70 | Polylijn | 71,72 | 4500 | Y | |
| 71 | Polylijn | 72,73 | 4500 | Y | |
| 72 | Polylijn | 73,74 | 4500 | Y | |
| 73 | Polylijn | 74,16 | 4300 | Y | |
| 74 | Polylijn | 12,75 | 4300 | Y | |
| 75 | Polylijn | 75,76 | 4500 | Y | |
| 76 | Polylijn | 76,77 | 4500 | Y | |
| 77 | Polylijn | 77,78 | 4500 | Y | |
| 78 | Polylijn | 78,17 | 4300 | Y | |
| 79 | Polylijn | 45,49 | 4300 | Y | |
| 80 | Polylijn | 49,51 | 4500 | Y | |
| 81 | Polylijn | 51,53 | 4500 | Y | |
| 82 | Polylijn | 53,55 | 4500 | Y | |
| 83 | Polylijn | 55,56 | 4300 | Y | |
| 84 | Polylijn | 46,37 | 4300 | Y | |
| 85 | Polylijn | 37,61 | 4500 | Y | |
| 86 | Polylijn | 61,101 | 4300 | Y | |
| 87 | Polylijn | 63,65 | 4500 | Y | |
| 88 | Polylijn | 65,57 | 4300 | Y | |
| 89 | Polylijn | 35,81 | 4300 | Y | |
| 90 | Polylijn | 80,57 | 7411 | XZ | |
| 91 | Polylijn | 81,82 | 4500 | Y | |
| 92 | Polylijn | 17,42 | 7529 | XZ | |
| 93 | Polylijn | 82,83 | 4500 | Y | |
| 94 | Polylijn | 92,91 | 1665 | X | |
| 95 | Polylijn | 83,84 | 4500 | Y | |
| 96 | Polylijn | 80,41 | 7451 | XZ | |
| 97 | Polylijn | 84,41 | 4300 | Y | |
| 98 | Polylijn | 39,85 | 4300 | Y | |
| 99 | Polylijn | 85,155 | 3256 | XZ | |
| 100 | Polylijn | 85,86 | 4500 | Y | |
| 101 | Polylijn | 86,154 | 3256 | XZ | |
| 102 | Polylijn | 86,102 | 4300 | Y | |

## 1.2 LIJNEN

| Lijn No. | Lijntype | Knopen No. | Lijnlengte L [mm] | | Opm. |
|---|---|---|---|---|---|
| 103 | Polylijn | 68,67 | 4500 | Y | |
| 104 | Polylijn | 67,42 | 4300 | Y | |
| 105 | Polylijn | 35,27 | 3901 | | |
| 106 | Polylijn | 81,27 | 3901 | | |
| 107 | Polylijn | 49,23 | 3912 | | |
| 108 | Polylijn | 51,23 | 3912 | | |
| 109 | Polylijn | 82,31 | 3957 | | |
| 110 | Polylijn | 83,31 | 3957 | | |
| 111 | Polylijn | 53,26 | 3912 | | |
| 112 | Polylijn | 55,26 | 3912 | | |
| 113 | Polylijn | 84,33 | 3901 | | |
| 114 | Polylijn | 41,33 | 3901 | | |
| 115 | Polylijn | 88,87 | 4500 | Y | |
| 116 | Polylijn | 87,67 | 3748 | Z | |
| 117 | Polylijn | 88,68 | 3748 | Z | |
| 118 | Polylijn | 87,80 | 4300 | Y | |
| 119 | Polylijn | 80,42 | 3748 | Z | |
| 120 | Polylijn | 59,58 | 6510 | X | |
| 121 | Polylijn | 58,8 | 6400 | X | |
| 122 | Polylijn | 88,96 | 1665 | X | |
| 123 | Polylijn | 77,63 | 3505 | Z | |
| 124 | Polylijn | 62,64 | 4500 | Y | |
| 125 | Polylijn | 36,60 | 4500 | Y | |
| 126 | Polylijn | 60,62 | 4500 | Y | |
| 127 | Polylijn | 64,7 | 4300 | Y | |
| 128 | Polylijn | 83,32 | 3957 | | |
| 129 | Polylijn | 84,32 | 3957 | | |
| 130 | Polylijn | 68,164 | 3967 | | |
| 131 | Polylijn | 67,164 | 3967 | | |
| 132 | Polylijn | 81,28 | 3957 | | |
| 133 | Polylijn | 82,28 | 3957 | | |
| 134 | Polylijn | 85,38 | 3967 | | |
| 135 | Polylijn | 86,38 | 3967 | | |
| 136 | Polylijn | 48,72 | 6255 | YZ | |
| 137 | Polylijn | 50,71 | 6255 | YZ | |
| 138 | Polylijn | 71,51 | 5704 | YZ | |
| 139 | Polylijn | 72,49 | 5704 | YZ | |
| 140 | Polylijn | 36,76 | 6255 | YZ | |
| 141 | Polylijn | 60,75 | 6255 | YZ | |
| 142 | Polylijn | 75,61 | 5704 | YZ | |
| 143 | Polylijn | 76,37 | 5704 | YZ | |
| 144 | Polylijn | 52,74 | 6255 | YZ | |
| 145 | Polylijn | 54,73 | 6255 | YZ | |
| 146 | Polylijn | 73,55 | 5704 | YZ | |
| 147 | Polylijn | 74,53 | 5704 | YZ | |
| 148 | Polylijn | 62,78 | 6255 | YZ | |
| 149 | Polylijn | 64,77 | 6255 | YZ | |
| 150 | Polylijn | 77,65 | 5704 | YZ | |
| 151 | Polylijn | 78,63 | 5704 | YZ | |
| 152 | Polylijn | 44,70 | 7827 | XZ | |
| 153 | Polylijn | 69,39 | 7512 | XZ | |
| 154 | Polylijn | 47,69 | 7827 | XZ | |
| 155 | Polylijn | 70,35 | 7451 | XZ | |
| 156 | Polylijn | 94,95 | 2173 | Z | |
| 157 | Polylijn | 97,98 | 2173 | Z | |
| 158 | Polylijn | 95,92 | 1665 | X | |
| 159 | Polylijn | 94,92 | 2737 | XZ | |
| 160 | Polylijn | 59,95 | 2737 | XZ | |
| 161 | Polylijn | 95,80 | 2737 | XZ | |
| 162 | Polylijn | 92,93 | 2737 | XZ | |
| 163 | Polylijn | 88,63 | 7411 | XZ | |
| 164 | Polylijn | 59,91 | 2737 | XZ | |
| 165 | Polylijn | 90,92 | 2737 | XZ | |
| 166 | Polylijn | 92,89 | 2737 | XZ | |
| 167 | Polylijn | 91,80 | 2737 | XZ | |
| 168 | Polylijn | 77,68 | 7529 | XZ | |
| 169 | Polylijn | 99,98 | 1665 | X | |
| 170 | Polylijn | 66,98 | 2737 | XZ | |
| 171 | Polylijn | 97,99 | 2737 | XZ | |
| 172 | Polylijn | 99,96 | 2737 | XZ | |
| 173 | Polylijn | 98,88 | 2737 | XZ | |
| 174 | Polylijn | 101,160 | 3267 | XZ | |
| 175 | Polylijn | 102,68 | 200 | Y | |
| 176 | Polylijn | 101,63 | 200 | Y | |
| 177 | Polylijn | 89,17 | 4865 | X | |
| 178 | Polylijn | 93,80 | 1665 | X | |
| 179 | Polylijn | 96,77 | 4865 | X | |
| 180 | Polylijn | 17,57 | 3505 | Z | |
| 181 | Polylijn | 79,41 | 3625 | Z | |
| 182 | Polylijn | 16,56 | 3505 | Z | |
| 183 | Polylijn | 74,55 | 3505 | Z | |
| 184 | Polylijn | 72,51 | 3505 | Z | |
| 185 | Polylijn | 73,53 | 3505 | Z | |
| 186 | Polylijn | 71,49 | 3505 | Z | |
| 187 | Polylijn | 9,45 | 3505 | Z | |
| 188 | Polylijn | 69,35 | 3625 | Z | |
| 189 | Polylijn | 70,39 | 3748 | Z | |
| 190 | Polylijn | 12,46 | 3505 | Z | |
| 191 | Polylijn | 75,37 | 3505 | Z | |
| 192 | Polylijn | 76,61 | 3505 | Z | |
| 193 | Polylijn | 78,65 | 3505 | Z | |
| 194 | Polylijn | 92,80 | 2173 | Z | |
| 195 | Polylijn | 95,93 | 2173 | Z | |
| 196 | Polylijn | 91,89 | 2173 | Z | |

## 1.2 LIJNEN

| Lijn No. | Lijntype | Knopen No. | Lijnlengte L [mm] | | Opm. |
|---|---|---|---|---|---|
| 197 | Polylijn | 99,88 | 2173 | Z | |
| 198 | Polylijn | 98,96 | 2173 | Z | |
| 199 | Polylijn | 145,41 | 3201 | XZ | |
| 200 | Polylijn | 146,84 | 3201 | XZ | |
| 201 | Polylijn | 147,83 | 3201 | XZ | |
| 202 | Polylijn | 148,82 | 3201 | XZ | |
| 203 | Polylijn | 149,81 | 3201 | XZ | |
| 204 | Polylijn | 150,35 | 3201 | XZ | |
| 205 | Polylijn | 151,41 | 3256 | XZ | |
| 206 | Polylijn | 152,84 | 3256 | XZ | |
| 207 | Polylijn | 153,83 | 3256 | XZ | |
| 208 | Polylijn | 154,82 | 3256 | XZ | |
| 209 | Polylijn | 155,81 | 3256 | XZ | |
| 210 | Polylijn | 156,35 | 3256 | XZ | |
| 211 | Polylijn | 157,42 | 3267 | XZ | |
| 212 | Polylijn | 158,67 | 3267 | XZ | |
| 213 | Polylijn | 159,68 | 3267 | XZ | |
| 214 | Polylijn | 160,102 | 3267 | XZ | |
| 215 | Polylijn | 161,86 | 3267 | XZ | |
| 216 | Polylijn | 162,85 | 3267 | XZ | |
| 217 | Polylijn | 163,39 | 3267 | XZ | |
| 218 | Polylijn | 150,149 | 4300 | Y | |
| 219 | Polylijn | 149,23 | 2250 | Y | |
| 220 | Polylijn | 148,147 | 4500 | Y | |
| 221 | Polylijn | 147,26 | 2250 | Y | |
| 222 | Polylijn | 146,145 | 4300 | Y | |
| 223 | Polylijn | 156,27 | 2150 | Y | |
| 224 | Polylijn | 155,28 | 2250 | Y | |
| 225 | Polylijn | 154,31 | 2250 | Y | |
| 226 | Polylijn | 153,32 | 2250 | Y | |
| 227 | Polylijn | 152,33 | 2150 | Y | |
| 228 | Polylijn | 163,162 | 4300 | Y | |
| 229 | Polylijn | 162,38 | 2250 | Y | |
| 230 | Polylijn | 161,160 | 4300 | Y | |
| 231 | Polylijn | 159,164 | 2250 | Y | |
| 232 | Polylijn | 158,157 | 4300 | Y | |
| 233 | Polylijn | 23,82 | 3912 | | |
| 234 | Polylijn | 23,81 | 3912 | | |
| 235 | Polylijn | 23,148 | 2250 | Y | |
| 236 | Polylijn | 26,84 | 3912 | | |
| 237 | Polylijn | 26,83 | 3912 | | |
| 238 | Polylijn | 26,146 | 2250 | Y | |
| 239 | Polylijn | 27,85 | 3901 | | |
| 240 | Polylijn | 27,39 | 3901 | | |
| 241 | Polylijn | 27,155 | 2150 | Y | |
| 242 | Polylijn | 28,85 | 3957 | | |
| 243 | Polylijn | 28,86 | 3957 | | |
| 244 | Polylijn | 28,154 | 2250 | Y | |
| 245 | Polylijn | 31,86 | 3957 | | |
| 246 | Polylijn | 31,68 | 3957 | | |
| 247 | Polylijn | 31,153 | 2250 | Y | |
| 248 | Polylijn | 32,68 | 3957 | | |
| 249 | Polylijn | 32,67 | 3957 | | |
| 250 | Polylijn | 32,152 | 2250 | Y | |
| 251 | Polylijn | 33,67 | 3901 | | |
| 252 | Polylijn | 33,42 | 3901 | | |
| 253 | Polylijn | 33,151 | 2150 | Y | |
| 254 | Polylijn | 38,61 | 3967 | | |
| 255 | Polylijn | 38,37 | 3967 | | |
| 256 | Polylijn | 38,161 | 2250 | Y | |
| 257 | Polylijn | 164,65 | 3967 | | |
| 258 | Polylijn | 164,63 | 3967 | | |
| 259 | Polylijn | 164,158 | 2250 | Y | |

## 1.3 MATERIALEN

| Matl. No. | Modulus E [N/mm²] | Modulus G [N/mm²] | Coï¿½ff. v. Pois ν [-] | Vol. gewicht γ [kN/m³] | Therm. uitz. α [1/K] | Materiaalfactor $\gamma_M$ [-] | Materiaal Model |
|---|---|---|---|---|---|---|---|
| 1 | Staal S 235 \| NEN EN 1993-1-1:2007-11 | | | | | | |
| | 210000.0 | 80769.2 | 0.300 | 78.50 | 1.20E-05 | 1.00 | Isotroop Lineair Elastisch |
| 2 | Beton C30/37 \| EN 1992-1-1:2004/A1:2014 | | | | | | |
| | 33000.0 | 13750.0 | 0.200 | 25.00 | 1.00E-05 | 1.00 | Isotroop Lineair Elastisch |

## 1.4 VLAKKEN

| Vlak No. | Vlaktype Geometrie | Vlaktype Stijfheid | Randen No. | Matl. No. | Dikte Type | Dikte [mm] | Vlak A [mm²] | Gewicht G [kg] |
|---|---|---|---|---|---|---|---|---|
| 1 | Vlak | Standaard | 1,42,44,2,17,24,30, 36,3,47,48,4,35,29, 23,18 | 2 | &Blijvend | 200.0 | 4.46400E+08 | 223200.00 |

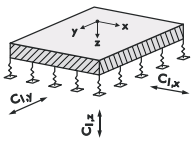
## 1.4.1 VLAKKEN - EXCENTRICITEITEN

| Vlak No. | Excentriciteit $e_z$ [mm] | Opm. |
|---|---|---|
| 1 | 100.0 | |

## 1.4.2 VLAKKEN - GEï¿½NTEGREERDE OBJECTEN

| Vlak No. | Geï¿½ntegreerde objecten No. | | | |
|---|---|---|---|---|
| | Knopen | Lijnen | Sparingen | Opm. |
| 1 | 43,66,90,94, 97,100,103-144 | 5-8,51,52,55-58,120,121,124-127 | | |

## 1.9 STEUNVLAKKEN

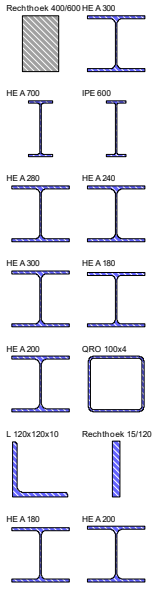



| Fund. No. | Op vlakken No. | Veerconstanten RF-SOILIN | Translationeel steunpunt of veer [kN/m³] | | | Dwarskrachtveer [kN/m] | |
|---|---|---|---|---|---|---|---|
| | | | $u_x$ | $u_y$ | $u_z$ | $v_{xz}$ | $v_{yz}$ |
| 1 | 1 | - | 1000.000 | 1000.000 | 7000.000 | ☐ | ☐ |

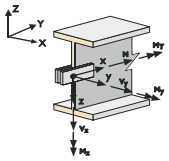
## 1.9.1 STEUNVLAKKEN - NIET-WERKZAAM

| Fund. No. | Op vlakken No. | Niet-werkzaam als contactspan. $\sigma_z$ | Vloeien vanaf contactspanning $\sigma_{z'}$ [kN/m²] | Wrijvingscoï¿½fficiï¿½nt $\mu_z$ [-] |
|---|---|---|---|---|
| 1 | 1 | Negatief | | |

## 1.13 DOORSNEDES

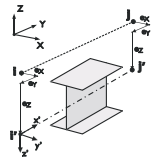



| Sneden No. | Matl. No. | J [mm⁴] / A [mm²] | $I_{y/u}$ [mm⁴] / $A_{y/u}$ [mm²] | $I_{z/v}$ [mm⁴] / $A_{z/v}$ [mm²] | Hoofdassen α [°] | Rotatie α' [°] | Globale maatvoering [mm] Breedte b | Hoogte h |
|---|---|---|---|---|---|---|---|---|
| 1 | Rechthoek 400/600 | | | | | | | |
| | 2 | 7511650816.0 | 7200000000.0 | 3200000000.0 | 0.00 | 0.00 | 400.0 | 600.0 |
| | | 240000.0 | 200000.0 | 200000.0 | | | | |
| | BetonRandbalk | | | | | | | |
| 2 | HE A 300 \| Euronorm 53-62 | | | | | | | |
| | 1 | 856000.0 | 182600000.0 | 63100000.0 | 0.00 | 0.00 | 300.0 | 290.0 |
| | | 11300.0 | 6988.5 | 2183.3 | | | | |
| | Hoofddraag kolom | | | | | | | |
| 3 | HE A 700 \| Euronorm 53-62 | | | | | | | |
| | 1 | 5150000.0 | 2152999936.0 | 121800000.0 | 0.00 | 0.00 | 300.0 | 690.0 |
| | | 26000.0 | 13538.1 | 9345.4 | | | | |
| | Hoofddraag ligger | | | | | | | |
| 4 | IPE 600 \| Euronorm 19-57 | | | | | | | |
| | 1 | 1660000.0 | 920800000.0 | 33900000.0 | 0.00 | 0.00 | 220.0 | 600.0 |
| | | 15600.0 | 7003.7 | 6799.2 | | | | |
| | Hoofddraag dakligger | | | | | | | |
| 5 | HE A 280 \| Euronorm 53-62 | | | | | | | |
| | 1 | 624000.0 | 136700000.0 | 47600000.0 | 0.00 | 0.00 | 280.0 | 270.0 |
| | | 9730.0 | 6059.9 | 1905.1 | | | | |
| | Hoofddraag dakligger | | | | | | | |
| 6 | HE A 240 \| Euronorm 53-62 | | | | | | | |
| | 1 | 417000.0 | 77600000.0 | 27700000.0 | 0.00 | 0.00 | 240.0 | 230.0 |
| | | 7680.0 | 4795.7 | 1509.8 | | | | |
| | Hoofddraag dakligger rand | | | | | | | |
| 7 | HE A 300 \| Euronorm 53-62 | | | | | | | |
| | 1 | 856000.0 | 182600000.0 | 63100000.0 | 0.00 | 0.00 | 300.0 | 290.0 |
| | | 11300.0 | 6988.5 | 2183.3 | | | | |
| | Tussenkolom | | | | | | | |
| 8 | HE A 180 \| Euronorm 53-62 | | | | | | | |
| | 1 | 149000.0 | 25100000.0 | 9250000.0 | 0.00 | 0.00 | 180.0 | 171.0 |
| | | 4530.0 | 2848.1 | 889.3 | | | | |
| | Tussenliggers | | | | | | | |
| 9 | HE A 200 \| Euronorm 53-62 | | | | | | | |
| | 1 | 211000.0 | 36900000.0 | 13400000.0 | 0.00 | 0.00 | 200.0 | 190.0 |
| | | 5380.0 | 3330.4 | 1076.8 | | | | |
| | Dakligger rand | | | | | | | |
| 10 | QRO 100x4 \| EN 10219-2:2006 | | | | | | | |
| | 1 | 3620000.0 | 2260000.0 | 2260000.0 | 0.00 | 0.00 | 100.0 | 100.0 |
| | | 1490.0 | 646.8 | 646.8 | | | | |
| | Dakligger midden | | | | | | | |
| 11 | L 120x120x10 \| EN 10056-1:1998 | | | | | | | |
| | 1 | 76700.0 | 4970000.0 | 1290000.0 | -45.00 | 0.00 | 120.0 | 120.0 |
| | | 2320.0 | 973.1 | 955.0 | | | | |
| | Horizontale verbanden | | | | | | | |
| 12 | Rechthoek 15/120 | | | | | | | |
| | 1 | 124369.0 | 2160000.0 | 33750.0 | 0.00 | 0.00 | 15.0 | 120.0 |
| | | 1800.0 | 1500.0 | 1500.0 | | | | |
| | Verticale verbanden | | | | | | | |
| 13 | HE A 180 \| Euronorm 53-62 | | | | | | | |
| | 1 | 149000.0 | 25100000.0 | 9250000.0 | 0.00 | 0.00 | 180.0 | 171.0 |
| | | 4530.0 | 2848.1 | 889.3 | | | | |
| | Kolom | | | | | | | |
| 14 | HE A 200 \| Euronorm 53-62 | | | | | | | |
| | 1 | 211000.0 | 36900000.0 | 13400000.0 | 0.00 | 0.00 | 200.0 | 190.0 |
| | | 5380.0 | 3330.4 | 1076.8 | | | | |
| | Dakligger | | | | | | | |



## 1.14 STAAFEINDSCHARNIEREN

| Vrijgave No. | Referentie Systeem | Normaal-/ Afschuifscharnier of Veer[k $u_x$ | $u_y$ | $u_z$ | Momentscharnier of veer[kNm/rad] $\varphi_x$ | $\varphi_y$ | $\varphi_z$ | Opm. |
|---|---|---|---|---|---|---|---|---|
| 1 | Lok. x,y,z | ☐ | ☐ | ☐ | ☐ | ☒ | ☒ | |
| 2 | Lok. x,y,z | ☐ | ☐ | ☐ | ☐ | ☒ | ☒ | |
| 3 | Lok. x,y,z | ☐ | ☐ | ☐ | ☐ | ☐ | ☒ | |

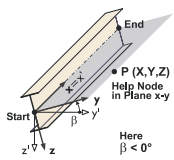


## 1.15/1 STAAFEXCENTRICITEITEN - ABSOLUUT

| Exc. No. | Referentie Systeem | Staafbegin - excentriciteit [mm] $e_{i,X}$ | $e_{i,Y}$ | $e_{i,Z}$ | Staafeind - Excentriciteit $e_{j,X}$ | $e_{j,Y}$ | $e_{j,Z}$ | Staafeindscharnier positie Staafbegin | Staafeinde |
|---|---|---|---|---|---|---|---|---|---|
| 1 | Globaal | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | op staaf | op staaf |

## 1.15/2 STAAFEXCENTRICITEITEN - RELATIEF

| Exc. No. | Doorsnede uitlijning y-as | z-as | Dwarsoffset van doorsnede tot ander object Object type | Object No. | y-as | z-as | Offset in langsrichting van aanlig Staafbegin | Staafeinde |
|---|---|---|---|---|---|---|---|---|
| 1 | Midden | Boven (-z) | Geen | 0 | Midden | Midden | ☐ | ☐ |




## 1.17 STAVEN

| Stf. No. | Lijn No. | Staaf | Rotatie Type | β[ï¿½] | Doorsnede Begin | Einde | Scharnier No. Begin | Einde | Exc. No. | Deel No. | Lengte L [mm] | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1 | 5 | Rib | Hoek | 0.00 | 1 | 1 | 3 | - | | - | 6400 | X |
| 2 | 6 | Rib | Hoek | 0.00 | 1 | 1 | 3 | - | | - | 4300 | Y |
| 3 | 7 | Rib | Hoek | 0.00 | 1 | 1 | 3 | - | | - | 6530 | X |
| 4 | 8 | Rib | Hoek | 0.00 | 1 | 1 | 3 | - | | - | 4300 | Y |
| 5 | 9 | Ligger | Hoek | 0.00 | 2 | 2 | 1 | - | - | - | 4345 | Z |
| 6 | 10 | Ligger | Hoek | 0.00 | 2 | 2 | 1 | - | - | - | 4345 | Z |
| 7 | 11 | Ligger | Hoek | 0.00 | 6 | 6 | 2 | - | 1 | - | 3201 | XZ |
| 8 | 12 | Ligger | Hoek | 0.00 | 6 | 6 | 2 | - | 1 | - | 3267 | XZ |
| 9 | 13 | Ligger | Hoek | 0.00 | 2 | 2 | 1 | - | - | - | 4345 | Z |
| 10 | 14 | Ligger | Hoek | 0.00 | 2 | 2 | 1 | - | - | - | 4345 | Z |
| 11 | 15 | Ligger | Hoek | 0.00 | 3 | 3 | 2 | - | 1 | - | 3201 | XZ |
| 12 | 16 | Ligger | Hoek | 0.00 | 3 | 3 | 2 | - | 1 | - | 3267 | XZ |
| 13 | 19 | Ligger | Hoek | 0.00 | 2 | 2 | 1 | - | - | - | 4345 | Z |
| 14 | 20 | Ligger | Hoek | 0.00 | 2 | 2 | 1 | - | - | - | 4345 | Z |
| 15 | 21 | Ligger | Hoek | 0.00 | 3 | 3 | 2 | - | 1 | - | 3201 | XZ |
| 16 | 22 | Ligger | Hoek | 0.00 | 3 | 3 | 2 | - | 1 | - | 3267 | XZ |
| 17 | 25 | Ligger | Hoek | 0.00 | 2 | 2 | 1 | - | - | - | 4345 | Z |
| 18 | 26 | Ligger | Hoek | 0.00 | 2 | 2 | 1 | - | - | - | 4345 | Z |
| 19 | 27 | Ligger | Hoek | 0.00 | 4 | 4 | 2 | - | 1 | - | 3201 | XZ |
| 20 | 28 | Ligger | Hoek | 0.00 | 5 | 5 | 2 | - | 1 | - | 3267 | XZ |
| 21 | 31 | Ligger | Hoek | 0.00 | 2 | 2 | 1 | - | - | - | 4345 | Z |
| 22 | 32 | Ligger | Hoek | 0.00 | 2 | 2 | 1 | - | - | - | 4345 | Z |
| 23 | 33 | Ligger | Hoek | 0.00 | 4 | 4 | 2 | - | 1 | - | 3201 | XZ |
| 24 | 34 | Ligger | Hoek | 0.00 | 5 | 5 | 2 | - | 1 | - | 3267 | XZ |
| 25 | 37 | Ligger | Hoek | 0.00 | 2 | 2 | 1 | - | - | - | 4345 | Z |
| 26 | 38 | Ligger | Hoek | 0.00 | 2 | 2 | 1 | - | - | - | 4345 | Z |
| 27 | 39 | Ligger | Hoek | 0.00 | 6 | 6 | 2 | - | 1 | - | 3201 | XZ |
| 28 | 40 | Ligger | Hoek | 0.00 | 6 | 6 | 2 | - | 1 | - | 3267 | XZ |
| 29 | 41 | Ligger | Hoek | 90.00 | 2 | 2 | 1 | - | - | - | 4345 | Z |
| 30 | 43 | Ligger | Hoek | 90.00 | 2 | 2 | 1 | - | - | - | 4345 | Z |
| 31 | 45 | Ligger | Hoek | 90.00 | 2 | 2 | 1 | - | - | - | 4345 | Z |
| 32 | 46 | Ligger | Hoek | 90.00 | 2 | 2 | 1 | - | - | - | 2173 | Z |
| 33 | 176 | Ligger | Hoek | 0.00 | 9 | 9 | - | 1 | 1 | - | 200 | Y |
| 34 | 50 | Ligger | Hoek | 0.00 | 6 | 6 | 2 | - | 1 | - | 3256 | XZ |
| 35 | 51 | Rib | Hoek | 0.00 | 1 | 1 | - | - | | - | 6510 | X |
| 36 | 52 | Rib | Hoek | 0.00 | 1 | 1 | - | 3 | | - | 6530 | X |
| 37 | 175 | Ligger | Hoek | 0.00 | 14 | 14 | - | 1 | 1 | - | 200 | Y |
| 38 | 54 | Ligger | Hoek | 0.00 | 6 | 6 | 2 | - | 1 | - | 3256 | XZ |
| 39 | 55 | Rib | Hoek | 0.00 | 1 | 1 | - | - | | - | 4500 | Y |
| 40 | 56 | Rib | Hoek | 0.00 | 1 | 1 | - | - | | - | 4500 | Y |
| 41 | 57 | Rib | Hoek | 0.00 | 1 | 1 | - | - | | - | 4500 | Y |
| 42 | 58 | Rib | Hoek | 0.00 | 1 | 1 | - | 3 | | - | 4300 | Y |
| 43 | 59 | Ligger | Hoek | 0.00 | 7 | 7 | 1 | - | - | - | 4345 | Z |
| 44 | 60 | Ligger | Hoek | 0.00 | 7 | 7 | 1 | - | - | - | 2173 | Z |
| 45 | 61 | Ligger | Hoek | 0.00 | 4 | 4 | 2 | - | 1 | - | 3256 | XZ |
| 46 | 62 | Ligger | Hoek | 0.00 | 4 | 4 | 2 | - | 1 | - | 3256 | XZ |
| 47 | 63 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | 1 | - | - | 6400 | X |
| 48 | 64 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | 1 | - | - | 6510 | X |
| 49 | 65 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | 1 | - | - | 6530 | X |
| 50 | 66 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | 1 | - | - | 6400 | X |
| 51 | 67 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | - | - | - | 4845 | X |
| 52 | 68 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | - | - | - | 1665 | X |
| 53 | 69 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | 1 | - | - | 4300 | Y |
| 54 | 70 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | 1 | - | - | 4500 | Y |
| 55 | 71 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | 1 | - | - | 4500 | Y |
| 56 | 72 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | 1 | - | - | 4500 | Y |
| 57 | 73 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | 1 | - | - | 4300 | Y |
| 58 | 74 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | 1 | - | - | 4300 | Y |
| 59 | 75 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | 1 | - | - | 4500 | Y |
| 60 | 76 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | 1 | - | - | 4500 | Y |
| 61 | 77 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | 1 | - | - | 4500 | Y |
| 62 | 78 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | 1 | - | - | 4300 | Y |
| 63 | 79 | Ligger | Hoek | 0.00 | 9 | 9 | 1 | 1 | 1 | - | 4300 | Y |

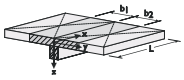
## 1.17 STAVEN

| Stf. No. | Lijn No. | Staaf | Rotatie Type | Rotatie β[ï¿½] | Doorsnede Begin | Doorsnede Einde | Scharnier No. Begin | Scharnier No. Einde | Exc. No. | Deel No. | Lengte L [mm] | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 64 | 80 | Ligger | Hoek | 0.00 | 9 | 9 | 1 | 1 | 1 | - | 4500 | Y |
| 65 | 81 | Ligger | Hoek | 0.00 | 9 | 9 | 1 | 1 | 1 | - | 4500 | Y |
| 66 | 82 | Ligger | Hoek | 0.00 | 9 | 9 | 1 | 1 | 1 | - | 4500 | Y |
| 67 | 83 | Ligger | Hoek | 0.00 | 9 | 9 | 1 | 1 | 1 | - | 4300 | Y |
| 68 | 84 | Ligger | Hoek | 0.00 | 9 | 9 | 1 | 1 | 1 | - | 4300 | Y |
| 69 | 85 | Ligger | Hoek | 0.00 | 9 | 9 | 1 | 1 | 1 | - | 4500 | Y |
| 70 | 86 | Ligger | Hoek | 0.00 | 9 | 9 | 1 | - | 1 | - | 4300 | Y |
| 71 | 87 | Ligger | Hoek | 0.00 | 9 | 9 | 1 | 1 | 1 | - | 4500 | Y |
| 72 | 88 | Ligger | Hoek | 0.00 | 9 | 9 | 1 | 1 | 1 | - | 4300 | Y |
| 73 | 89 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | 1 | 1 | - | 4300 | Y |
| 74 | 177 | Ligger | Hoek | 0.00 | 8 | 8 | - | 1 | - | - | 4865 | X |
| 75 | 91 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | 1 | 1 | - | 4500 | Y |
| 76 | 178 | Ligger | Hoek | 0.00 | 8 | 8 | - | 1 | - | - | 1665 | X |
| 77 | 93 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | 1 | 1 | - | 4500 | Y |
| 78 | 179 | Ligger | Hoek | 0.00 | 8 | 8 | - | 1 | - | - | 4865 | X |
| 79 | 95 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | 1 | 1 | - | 4500 | Y |
| 80 | 180 | Ligger | Hoek | 0.00 | 2 | 2 | - | - | - | - | 3505 | Z |
| 81 | 97 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | 1 | 1 | - | 4300 | Y |
| 82 | 98 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | 1 | 1 | - | 4300 | Y |
| 83 | 99 | Ligger | Hoek | 0.00 | 3 | 3 | - | - | 1 | - | 3256 | XZ |
| 84 | 100 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | 1 | 1 | - | 4500 | Y |
| 85 | 101 | Ligger | Hoek | 0.00 | 3 | 3 | - | - | 1 | - | 3256 | XZ |
| 86 | 102 | Ligger | Hoek | 0.00 | 14 | 14 | 1 | - | 1 | - | 4300 | Y |
| 87 | 103 | Ligger | Hoek | 0.00 | 14 | 14 | 1 | 1 | 1 | - | 4500 | Y |
| 88 | 104 | Ligger | Hoek | 0.00 | 14 | 14 | 1 | 1 | 1 | - | 4300 | Y |
| 89 | 105 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3901 | |
| 90 | 106 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3901 | |
| 91 | 107 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3912 | |
| 92 | 108 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3912 | |
| 93 | 109 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3957 | |
| 94 | 110 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3957 | |
| 95 | 111 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3912 | |
| 96 | 112 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3912 | |
| 97 | 113 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3901 | |
| 98 | 114 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3901 | |
| 99 | 115 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | 1 | - | - | 4500 | Y |
| 100 | 116 | Ligger | Hoek | 0.00 | 7 | 7 | - | - | - | - | 3748 | Z |
| 101 | 117 | Ligger | Hoek | 0.00 | 7 | 7 | - | - | - | - | 3748 | Z |
| 102 | 118 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | 1 | - | - | 4300 | Y |
| 103 | 119 | Ligger | Hoek | 90.00 | 2 | 2 | - | - | - | - | 3748 | Z |
| 104 | 120 | Rib | Hoek | 0.00 | 1 | 1 | - | - | | - | 6510 | X |
| 105 | 121 | Rib | Hoek | 0.00 | 1 | 1 | - | 3 | | - | 6400 | X |
| 106 | 122 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | - | - | - | 1665 | X |
| 107 | 123 | Ligger | Hoek | 0.00 | 2 | 2 | - | - | - | - | 3505 | Z |
| 108 | 124 | Rib | Hoek | 0.00 | 1 | 1 | - | - | | - | 4500 | Y |
| 109 | 125 | Rib | Hoek | 0.00 | 1 | 1 | - | - | | - | 4500 | Y |
| 110 | 126 | Rib | Hoek | 0.00 | 1 | 1 | - | - | | - | 4500 | Y |
| 111 | 127 | Rib | Hoek | 0.00 | 1 | 1 | - | 3 | | - | 4300 | Y |
| 112 | 128 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3957 | |
| 113 | 129 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3957 | |
| 114 | 130 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3967 | |
| 115 | 131 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3967 | |
| 116 | 132 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3957 | |
| 117 | 133 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3957 | |
| 118 | 134 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3967 | |
| 119 | 135 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3967 | |
| 120 | 136 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 6255 | YZ |
| 121 | 137 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 6255 | YZ |
| 122 | 138 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 5704 | YZ |
| 123 | 139 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 5704 | YZ |
| 124 | 140 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 6255 | YZ |
| 125 | 141 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 6255 | YZ |
| 126 | 142 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 5704 | YZ |
| 127 | 143 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 5704 | YZ |
| 128 | 144 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 6255 | YZ |
| 129 | 145 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 6255 | YZ |
| 130 | 146 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 5704 | YZ |
| 131 | 147 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 5704 | YZ |
| 132 | 148 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 6255 | YZ |
| 133 | 149 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 6255 | YZ |
| 134 | 150 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 5704 | YZ |
| 135 | 151 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 5704 | YZ |
| 136 | 152 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 7827 | XZ |
| 137 | 153 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 7512 | XZ |
| 138 | 154 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 7827 | XZ |
| 139 | 155 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 7451 | XZ |
| 140 | 182 | Ligger | Hoek | 0.00 | 2 | 2 | - | - | - | - | 3505 | Z |
| 141 | 181 | Ligger | Hoek | 90.00 | 2 | 2 | - | - | - | - | 3625 | Z |
| 142 | 183 | Ligger | Hoek | 0.00 | 2 | 2 | - | - | - | - | 3505 | Z |
| 143 | 184 | Ligger | Hoek | 0.00 | 2 | 2 | - | - | - | - | 3505 | Z |
| 144 | 49 | Ligger | Hoek | 90.00 | 13 | 13 | 1 | - | - | - | 2173 | Z |
| 145 | 185 | Ligger | Hoek | 0.00 | 2 | 2 | - | - | - | - | 3505 | Z |
| 146 | 90 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 7411 | XZ |
| 147 | 92 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 7529 | XZ |
| 148 | 94 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | 1 | - | - | 1665 | X |
| 149 | 186 | Ligger | Hoek | 0.00 | 2 | 2 | - | - | - | - | 3505 | Z |
| 150 | 187 | Ligger | Hoek | 0.00 | 2 | 2 | - | - | - | - | 3505 | Z |
| 151 | 188 | Ligger | Hoek | 90.00 | 2 | 2 | - | - | - | - | 3625 | Z |
| 152 | 189 | Ligger | Hoek | 90.00 | 2 | 2 | - | - | - | - | 3748 | Z |
| 153 | 190 | Ligger | Hoek | 0.00 | 2 | 2 | - | - | - | - | 3505 | Z |
| 154 | 164 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 2737 | XZ |
| 155 | 165 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 2737 | XZ |
| 156 | 166 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 2737 | XZ |
| 157 | 167 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 2737 | XZ |

## 1.17 STAVEN

| Stf. No. | Lijn No. | Staaf | Rotatie Type | Rotatie β[ï¿½] | Doorsnede Begin | Doorsnede Einde | Scharnier No. Begin | Scharnier No. Einde | Exc. No. | Deel No. | Lengte L [mm] | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 158 | 53 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 7512 | XZ |
| 159 | 96 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 7451 | XZ |
| 160 | 156 | Ligger | Hoek | 90.00 | 13 | 13 | 1 | - | - | - | 2173 | Z |
| 161 | 157 | Ligger | Hoek | 90.00 | 13 | 13 | 1 | - | - | - | 2173 | Z |
| 162 | 158 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | 1 | - | - | 1665 | X |
| 163 | 159 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 2737 | XZ |
| 164 | 160 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 2737 | XZ |
| 165 | 161 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 2737 | XZ |
| 166 | 162 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 2737 | XZ |
| 167 | 163 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 7411 | XZ |
| 168 | 168 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 7529 | XZ |
| 169 | 169 | Ligger | Hoek | 0.00 | 8 | 8 | 1 | 1 | - | - | 1665 | X |
| 170 | 170 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 2737 | XZ |
| 171 | 171 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 2737 | XZ |
| 172 | 172 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 2737 | XZ |
| 173 | 173 | Trek | Hoek | 0.00 | 12 | 12 | - | - | - | - | 2737 | XZ |
| 174 | 174 | Ligger | Hoek | 0.00 | 5 | 5 | 2 | - | 1 | - | 3267 | XZ |
| 175 | 191 | Ligger | Hoek | 0.00 | 2 | 2 | - | - | - | - | 3505 | Z |
| 176 | 192 | Ligger | Hoek | 0.00 | 2 | 2 | - | - | - | - | 3505 | Z |
| 177 | 193 | Ligger | Hoek | 0.00 | 2 | 2 | - | - | - | - | 3505 | Z |
| 178 | 194 | Ligger | Hoek | 90.00 | 2 | 2 | - | - | - | - | 2173 | Z |
| 179 | 195 | Ligger | Hoek | 90.00 | 13 | 13 | - | - | - | - | 2173 | Z |
| 180 | 196 | Ligger | Hoek | 90.00 | 13 | 13 | - | - | - | - | 2173 | Z |
| 181 | 197 | Ligger | Hoek | 0.00 | 7 | 7 | - | - | - | - | 2173 | Z |
| 182 | 198 | Ligger | Hoek | 90.00 | 13 | 13 | - | - | - | - | 2173 | Z |
| 183 | 199 | Ligger | Hoek | 0.00 | 6 | 6 | - | 2 | 1 | - | 3201 | XZ |
| 184 | 200 | Ligger | Hoek | 0.00 | 4 | 4 | - | - | 1 | - | 3201 | XZ |
| 185 | 201 | Ligger | Hoek | 0.00 | 4 | 4 | - | - | 1 | - | 3201 | XZ |
| 186 | 202 | Ligger | Hoek | 0.00 | 3 | 3 | - | - | 1 | - | 3201 | XZ |
| 187 | 203 | Ligger | Hoek | 0.00 | 3 | 3 | - | - | 1 | - | 3201 | XZ |
| 188 | 204 | Ligger | Hoek | 0.00 | 6 | 6 | - | 2 | 1 | - | 3201 | XZ |
| 189 | 205 | Ligger | Hoek | 0.00 | 6 | 6 | - | 2 | 1 | - | 3256 | XZ |
| 190 | 206 | Ligger | Hoek | 0.00 | 4 | 4 | - | - | 1 | - | 3256 | XZ |
| 191 | 207 | Ligger | Hoek | 0.00 | 4 | 4 | - | - | 1 | - | 3256 | XZ |
| 192 | 208 | Ligger | Hoek | 0.00 | 3 | 3 | - | - | 1 | - | 3256 | XZ |
| 193 | 209 | Ligger | Hoek | 0.00 | 3 | 3 | - | - | 1 | - | 3256 | XZ |
| 194 | 210 | Ligger | Hoek | 0.00 | 6 | 6 | - | 2 | 1 | - | 3256 | XZ |
| 195 | 211 | Ligger | Hoek | 0.00 | 6 | 6 | - | 2 | 1 | - | 3267 | XZ |
| 196 | 212 | Ligger | Hoek | 0.00 | 5 | 5 | - | 2 | 1 | - | 3267 | XZ |
| 197 | 213 | Ligger | Hoek | 0.00 | 5 | 5 | - | 2 | 1 | - | 3267 | XZ |
| 198 | 214 | Ligger | Hoek | 0.00 | 5 | 5 | - | 2 | 1 | - | 3267 | XZ |
| 199 | 215 | Ligger | Hoek | 0.00 | 3 | 3 | - | - | 1 | - | 3267 | XZ |
| 200 | 216 | Ligger | Hoek | 0.00 | 3 | 3 | - | - | 1 | - | 3267 | XZ |
| 201 | 217 | Ligger | Hoek | 0.00 | 6 | 6 | - | 2 | 1 | - | 3267 | XZ |
| 202 | 218 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | 1 | 1 | - | 4300 | Y |
| 203 | 219 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | - | 1 | - | 2250 | Y |
| 204 | 220 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | 1 | 1 | - | 4500 | Y |
| 205 | 221 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | - | 1 | - | 2250 | Y |
| 206 | 222 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | 1 | 1 | - | 4300 | Y |
| 207 | 223 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | - | 1 | - | 2150 | Y |
| 208 | 224 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | - | 1 | - | 2250 | Y |
| 209 | 225 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | - | 1 | - | 2250 | Y |
| 210 | 226 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | - | 1 | - | 2250 | Y |
| 211 | 227 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | - | 1 | - | 2150 | Y |
| 212 | 228 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | 1 | 1 | - | 4300 | Y |
| 213 | 229 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | - | 1 | - | 2250 | Y |
| 214 | 230 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | 1 | 1 | - | 4300 | Y |
| 215 | 231 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | - | 1 | - | 2250 | Y |
| 216 | 232 | Ligger | Hoek | 0.00 | 10 | 10 | 1 | 1 | 1 | - | 4300 | Y |
| 217 | 233 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3912 | |
| 218 | 234 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3912 | |
| 219 | 235 | Ligger | Hoek | 0.00 | 10 | 10 | - | 1 | 1 | - | 2250 | Y |
| 220 | 236 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3912 | |
| 221 | 237 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3912 | |
| 222 | 238 | Ligger | Hoek | 0.00 | 10 | 10 | - | 1 | 1 | - | 2250 | Y |
| 223 | 239 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3901 | |
| 224 | 240 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3901 | |
| 225 | 241 | Ligger | Hoek | 0.00 | 10 | 10 | - | 1 | 1 | - | 2150 | Y |
| 226 | 243 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3957 | |
| 227 | 242 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3957 | |
| 228 | 244 | Ligger | Hoek | 0.00 | 10 | 10 | - | 1 | 1 | - | 2250 | Y |
| 229 | 246 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3957 | |
| 230 | 245 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3957 | |
| 231 | 247 | Ligger | Hoek | 0.00 | 10 | 10 | - | 1 | 1 | - | 2250 | Y |
| 232 | 249 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3957 | |
| 233 | 248 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3957 | |
| 234 | 250 | Ligger | Hoek | 0.00 | 10 | 10 | - | 1 | 1 | - | 2250 | Y |
| 235 | 252 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3901 | |
| 236 | 251 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3901 | |
| 237 | 253 | Ligger | Hoek | 0.00 | 10 | 10 | - | 1 | 1 | - | 2150 | Y |
| 238 | 254 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3967 | |
| 239 | 255 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3967 | |
| 240 | 256 | Ligger | Hoek | 0.00 | 10 | 10 | - | 1 | 1 | - | 2250 | Y |
| 241 | 257 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3967 | |
| 242 | 258 | Trek | Hoek | 0.00 | 11 | 11 | - | - | 1 | - | 3967 | |
| 243 | 259 | Ligger | Hoek | 0.00 | 10 | 10 | - | 1 | 1 | - | 2250 | Y |

## 1.18 RIBBEN




| Stf. No. | Rib Positie | Meewerkende breedte - Zijde Vlak No. | $b_1$ [mm] | Meewerkende breedte - Zijde Vlak No. | $b_2$ [mm] | Opm. |
|---|---|---|---|---|---|---|
| 1 | Op +z-rand | 1 | 200 | | 0 | |
| 2 | Op +z-rand | 1 | 200 | | 0 | |
| 3 | Op +z-rand | 1 | 200 | | 0 | |
| 4 | Op +z-rand | 1 | 200 | | 0 | |
| 35 | Op +z-rand | 1 | 200 | | 0 | |
| 36 | Op +z-rand | 1 | 200 | | 0 | |
| 39 | Op +z-rand | 1 | 200 | | 0 | |
| 40 | Op +z-rand | 1 | 200 | | 0 | |
| 41 | Op +z-rand | 1 | 200 | | 0 | |
| 42 | Op +z-rand | 1 | 200 | | 0 | |
| 104 | Op +z-rand | 1 | 200 | | 0 | |
| 105 | Op +z-rand | 1 | 200 | | 0 | |
| 108 | Op +z-rand | 1 | 200 | | 0 | |
| 109 | Op +z-rand | 1 | 200 | | 0 | |
| 110 | Op +z-rand | 1 | 200 | | 0 | |
| 111 | Op +z-rand | 1 | 200 | | 0 | |

## 1.21 STAAFVERZAMELINGEN

| Staafver No. | Staafverzameling Omschrijving | Type | Staaf No. | Lengte [mm] | Opm. |
|---|---|---|---|---|---|
| 1 | Doorgaande staven 1 | Doorg. staaf | 5,150 | 7850 | Kolom |
| 2 | Doorgaande staven 2 | Doorg. staaf | 6,153 | 7850 | Kolom |
| 3 | Doorgaande staven 3 | Doorg. staaf | 9,149 | 7850 | Kolom |
| 4 | Doorgaande staven 4 | Doorg. staaf | 10,175 | 7850 | Kolom |
| 5 | Doorgaande staven 5 | Doorg. staaf | 13,143 | 7850 | Kolom |
| 6 | Doorgaande staven 6 | Doorg. staaf | 14,176 | 7850 | Kolom |
| 7 | Doorgaande staven 7 | Doorg. staaf | 17,145 | 7850 | Kolom |
| 8 | Doorgaande staven 8 | Doorg. staaf | 18,107 | 7850 | Kolom |
| 9 | Doorgaande staven 9 | Doorg. staaf | 21,142 | 7850 | Kolom |
| 10 | Doorgaande staven 10 | Doorg. staaf | 22,177 | 7850 | Kolom |
| 11 | Doorgaande staven 11 | Doorg. staaf | 25,140 | 7850 | Kolom |
| 12 | Doorgaande staven 12 | Doorg. staaf | 26,80 | 7850 | Kolom |
| 13 | Doorgaande staven 15 | Doorg. staaf | 15,186,192,85,199,16 | 19447 | Hoofddraagdakligger |
| 14 | Doorgaande staven 16 | Doorg. staaf | 19,185,191,46 | 12912 | Hoofddraagdakligger |
| 15 | Doorgaande staven 17 | Doorg. staaf | 23,184,190,45 | 12912 | Hoofddraagdakligger |
| 16 | Doorgaande staven 19 | Doorg. staaf | 29,151 | 7970 | Tussenkolom |
| 17 | Doorgaande staven 20 | Doorg. staaf | 30,152 | 8093 | Tussenkolom |
| 18 | Doorgaande staven 21 | Doorg. staaf | 31,141 | 7970 | Tussenkolom |
| 19 | Doorgaande staven 22 | Doorg. staaf | 32,178,103 | 8093 | Tussenkolom |
| 20 | Doorgaande staven 23 | Doorg. staaf | 43,100 | 8093 | CompartimentKolom |
| 21 | Doorgaande staven 24 | Doorg. staaf | 44,181,101 | 8093 | CompartimentKolom |
| 24 | Doorgaande staven 27 | Doorg. staaf | 11,187,193,83,200,12 | 19447 | Hoofddraag ligger |
| 25 | Doorgaande staven 25 | Doorg. staaf | 52,74 | 6530 | Doorgaande ligger |
| 28 | Doorgaande staven 28 | Doorg. staaf | 144,180 | 4345 | Kolom |
| 29 | Doorgaande staven 29 | Doorg. staaf | 160,179 | 4345 | Kolom |
| 30 | Doorgaande staven 30 | Doorg. staaf | 51,76 | 6510 | Doorgaande ligger |
| 31 | Doorgaande staven 31 | Doorg. staaf | 106,78 | 6530 | Doorgaande ligger |
| 32 | Doorgaande staven 32 | Doorg. staaf | 161,182 | 4345 | Kolom |
| 33 | Doorgaande staven 33 | Doorg. staaf | 70,33 | 4500 | |
| 34 | Doorgaande staven 34 | Doorg. staaf | 86,37 | 4500 | |
| 35 | Doorgaande staven 35 | Doorg. staaf | 28,195 | 6535 | Dakligger |
| 36 | Doorgaande staven 36 | Doorg. staaf | 34,189 | 6511 | Dakligger |
| 37 | Doorgaande staven 37 | Doorg. staaf | 27,183 | 6401 | Dakligger |
| 38 | Doorgaande staven 38 | Doorg. staaf | 8,201 | 6535 | Dakligger |
| 39 | Doorgaande staven 39 | Doorg. staaf | 38,194 | 6511 | Dakligger |
| 40 | Doorgaande staven 40 | Doorg. staaf | 7,188 | 6401 | Dakligger |
| 41 | Doorgaande staven 41 | Doorg. staaf | 24,196 | 6535 | Dakligger |
| 42 | Doorgaande staven 42 | Doorg. staaf | 20,197 | 6535 | Dakligger |
| 43 | Doorgaande staven 43 | Doorg. staaf | 174,198 | 6535 | Dakligger |
| 44 | Doorgaande staven 44 | Doorg. staaf | 203,219 | 4500 | Dakligger koker |
| 45 | Doorgaande staven 45 | Doorg. staaf | 205,222 | 4500 | Dakligger koker |
| 46 | Doorgaande staven 46 | Doorg. staaf | 207,225 | 4300 | Dakligger koker |
| 47 | Doorgaande staven 47 | Doorg. staaf | 208,228 | 4500 | Dakligger koker |
| 48 | Doorgaande staven 48 | Doorg. staaf | 209,231 | 4500 | Dakligger koker |
| 49 | Doorgaande staven 49 | Doorg. staaf | 210,234 | 4500 | Dakligger koker |
| 50 | Doorgaande staven 50 | Doorg. staaf | 211,237 | 4300 | Dakligger koker |
| 51 | Doorgaande staven 51 | Doorg. staaf | 213,240 | 4500 | Dakligger koker |
| 52 | Doorgaande staven 52 | Doorg. staaf | 215,243 | 4500 | Dakligger koker |

## 2.1 BELASTINGSGEVALLEN

| Bel. Geval | BG omschrijving | EN 1990 \| NEN Actiecategorie | Eigen gewicht - Factor in richting Actief | X | Y | Z |
|---|---|---|---|---|---|---|
| BG10 | PB: Eigen Gewicht | Blijvend | ☒ | 0.000 | 0.000 | -1.000 |
| BG20 | PB: Dakbedekking | Blijvend | ☐ | | | |
| BG30 | PB: KSZ - Metselwerk | Blijvend | ☐ | | | |
| BG40 | PB: Sandwichpaneel | Blijvend | ☐ | | | |
| BG100 | VB: Opgelegde belasting op vloeren 1 | Opgelegd - Categorie E: Industriefunctie en kantoorfunctie | ☐ | | | |
| BG110 | VB: Opgelegde belasting op vloeren 2 | Opgelegd - Categorie E: Industriefunctie en kantoorfunctie | ☐ | | | |
| BG120 | VB: Dakbelasting | Opgelegd - Categorie H: Daken | ☐ | | | |
| BG130 | VB: Zonnepanelen | Opgelegd - Categorie E: Industriefunctie en kantoorfunctie | ☐ | | | |
| BG140 | VB: Stellingen - Pallet | Opgelegd - Categorie E: Industriefunctie en kantoorfunctie | ☐ | | | |
| BG150 | VB: Heftruck | Opgelegd - Categorie E: Industriefunctie en kantoorfunctie | ☐ | | | |
| BG300 | VB: Sneeuw | Sneeuw (H ≤ 1000 m a.s.l.) | ☐ | | | |

## 2.1 BELASTINGSGEVALLEN

| Bel. Geval | BG omschrijving | EN 1990 \| NEN Actiecategorie | Eigen gewicht - Factor in richting | | | |
|---|---|---|---|---|---|---|
| | | | Actief | X | Y | Z |
| BG401 | VB: Wind (+X richting) | Wind | ☐ | | | |
| BG402 | VB: Wind (-X richting) | Wind | ☐ | | | |
| BG403 | VB: Wind (+Y richting) | Wind | ☐ | | | |
| BG404 | VB: Wind (-Y richting) | Wind | ☐ | | | |
| BG800 | DBG1 - Eigenvorm 1, richting - X | Aardbeving | ☐ | | | |
| BG801 | DBG1 - Eigenvorm 1, richting - Y | Aardbeving | ☐ | | | |
| BG802 | DBG1 - Eigenvorm 2, richting - X | Aardbeving | ☐ | | | |
| BG803 | DBG1 - Eigenvorm 2, richting - Y | Aardbeving | ☐ | | | |
| BG804 | DBG1 - Eigenvorm 4, richting - X | Aardbeving | ☐ | | | |
| BG805 | DBG1 - Eigenvorm 4, richting - Y | Aardbeving | ☐ | | | |
| BG806 | DBG1 - Eigenvorm 5, richting - X | Aardbeving | ☐ | | | |
| BG807 | DBG1 - Eigenvorm 5, richting - Y | Aardbeving | ☐ | | | |

## 2.1.1 BELASTINGSGEVALLEN - BEREKENINGSPARAMETERS

| Bel. Geval | BG omschrijving | Berekeningsparameters | | |
|---|---|---|---|---|
| BG10 | PB: Eigen Gewicht | Berekeningsmethode | : | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : | Newton-Raphson |
| | | Opties | : ☒ | Belasting met factor vermenigvuldigen: 1.000 |
| BG20 | PB: Dakbedekking | Berekeningsmethode | : | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : | Newton-Raphson |
| | | Opties | : ☒ | Belasting met factor vermenigvuldigen: 1.000 |
| BG30 | PB: KSZ - Metselwerk | Berekeningsmethode | : | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : | Newton-Raphson |
| | | Opties | : ☒ | Belasting met factor vermenigvuldigen: 1.000 |
| BG40 | PB: Sandwichpaneel | Berekeningsmethode | : | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : | Newton-Raphson |
| | | Opties | : ☒ | Belasting met factor vermenigvuldigen: 1.000 |
| BG100 | VB: Opgelegde belasting op vloeren 1 | Berekeningsmethode | : | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : | Newton-Raphson |
| | | Opties | : ☒ | Belasting met factor vermenigvuldigen: 1.000 |
| BG110 | VB: Opgelegde belasting op vloeren 2 | Berekeningsmethode | : | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : | Newton-Raphson |
| | | Opties | : ☒ | Belasting met factor vermenigvuldigen: 1.000 |
| BG120 | VB: Dakbelasting | Berekeningsmethode | : | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : | Newton-Raphson |
| | | Opties | : ☒ | Belasting met factor vermenigvuldigen: 1.000 |
| BG130 | VB: Zonnepanelen | Berekeningsmethode | : | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : | Newton-Raphson |
| | | Opties | : ☒ | Belasting met factor vermenigvuldigen: 1.000 |
| BG140 | VB: Stellingen - Pallet | Berekeningsmethode | : | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : | Newton-Raphson |
| | | Opties | : ☒ | Belasting met factor vermenigvuldigen: 1.000 |
| BG150 | VB: Heftruck | Berekeningsmethode | : | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : | Newton-Raphson |
| | | Opties | : ☒ | Belasting met factor vermenigvuldigen: 1.000 |
| BG300 | VB: Sneeuw | Berekeningsmethode | : | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : | Newton-Raphson |
| | | Opties | : ☒ | Belasting met factor vermenigvuldigen: 1.000 |
| BG401 | VB: Wind (+X richting) | Berekeningsmethode | : | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : | Newton-Raphson |
| | | Opties | : ☒ | Belasting met factor vermenigvuldigen: 1.000 |
| BG402 | VB: Wind (-X richting) | Berekeningsmethode | : | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : | Newton-Raphson |
| | | Opties | : ☒ | Belasting met factor vermenigvuldigen: 1.000 |
| BG403 | VB: Wind (+Y richting) | Berekeningsmethode | : | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : | Newton-Raphson |
| | | Opties | : ☒ | Belasting met factor vermenigvuldigen: 1.000 |
| BG404 | VB: Wind (-Y richting) | Berekeningsmethode | : | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire a | : | Newton-Raphson |

## 2.1.1 BELASTINGSGEVALLEN - BEREKENINGSPARAMETERS

| Bel. Geval | BG omschrijving | Berekeningsparameters | | |
|---|---|---|---|---|
| | | algebraïsche vergelijkingen<br>Opties | : ☒ | Belasting met factor vermenigvuldigen: 1.000 |
| BG800 | DBG1 - Eigenvorm 1, richting - X | Berekeningsmethode | : ⊙ | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : ⊙ | Newton-Raphson |
| BG801 | DBG1 - Eigenvorm 1, richting - Y | Berekeningsmethode | : ⊙ | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : ⊙ | Newton-Raphson |
| BG802 | DBG1 - Eigenvorm 2, richting - X | Berekeningsmethode | : ⊙ | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : ⊙ | Newton-Raphson |
| BG803 | DBG1 - Eigenvorm 2, richting - Y | Berekeningsmethode | : ⊙ | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : ⊙ | Newton-Raphson |
| BG804 | DBG1 - Eigenvorm 4, richting - X | Berekeningsmethode | : ⊙ | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : ⊙ | Newton-Raphson |
| BG805 | DBG1 - Eigenvorm 4, richting - Y | Berekeningsmethode | : ⊙ | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : ⊙ | Newton-Raphson |
| BG806 | DBG1 - Eigenvorm 5, richting - X | Berekeningsmethode | : ⊙ | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : ⊙ | Newton-Raphson |
| BG807 | DBG1 - Eigenvorm 5, richting - Y | Berekeningsmethode | : ⊙ | Geometrisch lineaire berekening |
| | | Methode voor het oplossen van een systeem met niet-lineaire algebraïsche vergelijkingen | : ⊙ | Newton-Raphson |

## 2.1.5 BELASTINGSGEVALLEN - PARAMETERS VOOR CQC-REGEL

| Bel. Geval | BG omschrijving | Hoekfrequentie [rad/s] | Demping [-] |
|---|---|---|---|
| BG800 | DBG1 - Eigenvorm 1, richting - X | 18.63 | 0.000 |
| BG801 | DBG1 - Eigenvorm 1, richting - Y | 18.63 | 0.000 |
| BG802 | DBG1 - Eigenvorm 2, richting - X | 19.36 | 0.000 |
| BG803 | DBG1 - Eigenvorm 2, richting - Y | 19.36 | 0.000 |
| BG804 | DBG1 - Eigenvorm 4, richting - X | 26.87 | 0.000 |
| BG805 | DBG1 - Eigenvorm 4, richting - Y | 26.87 | 0.000 |
| BG806 | DBG1 - Eigenvorm 5, richting - X | 27.30 | 0.000 |
| BG807 | DBG1 - Eigenvorm 5, richting - Y | 27.30 | 0.000 |

## 2.2 ACTIES

| Actie | Actie Omschrijving | EN 1990 \| NEN Actiecategorie | Inwerkend | Belastingsgevallen in actie | |
|---|---|---|---|---|---|
| A1 | Blijvend | Blijvend | Gelijktijdig | BG10<br>BG20<br>BG30<br>BG40 | PB: Eigen Gewicht<br>PB: Dakbedekking<br>PB: KSZ - Metselwerk<br>PB: Sandwichpaneel |
| A2 | Opgelegd | Opgelegd - Categorie E: Industriefunctie en kantoorfunctie | Gelijktijdig | BG100<br>BG110<br>BG130<br>BG140<br>BG150 | VB: Opgelegde belasting op vloeren 1<br>VB: Opgelegde belasting op vloeren 2<br>VB: Zonnepanelen<br>VB: Stellingen - Pallet<br>VB: Heftruck |
| A3 | Opgelegd | Opgelegd - Categorie H: Daken | | BG120 | VB: Dakbelasting |
| A4 | Sneeuw | Sneeuw (H ≤ 1000 m a.s.l.) | | BG300 | VB: Sneeuw |
| A5 | Wind | Wind | Alternatief | BG401<br>BG402<br>BG403<br>BG404 | VB: Wind (+X richting)<br>VB: Wind (-X richting)<br>VB: Wind (+Y richting)<br>VB: Wind (-Y richting) |

## 2.3 COMBINATIEREGELS

| CE. No. | Omschrijving | EN 1990 \| NEN Ontwerpsituatie | Instellingen | | |
|---|---|---|---|---|---|
| CE1 | UGT | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | Beschouw | : ☒ | Gunstige blijvende acties |
| | | | Nummeren van gegenereerde combinaties | | 1e Nummer van gegenereerde: |

## 2.3 COMBINATIEREGELS

| CE. No. | Omschrijving | EN 1990 \| NEN Ontwerpsituatie | Instellingen | |
|---|---|---|---|---|
| | | | Opties | 1 - Belastingscombinaties<br>1 - Resultaatcombinaties<br>☒Veranderlijke- en verkeersbelastingen worden samengevoegd als ï¿½ï¿½n onafhankelijke actie |
| | | | Resultaatcombinaties | ☒Genereer aanvullende of/of resultaatcombinatie (omhullende)<br>☒Genereer aanvullend een verschillende of/of resultaatcombinatie voor elke combinatieregel |
| | | | Gegenereerde belastingscombinaties | |
| | | | Berekeningsmethode : | Geometrisch lineair |
| CE2 | BGT | BGT - Karakteristiek | Beschouw : | ☐Gunstige blijvende acties |
| | | | Nummeren van gegenereerde combinaties | 1e Nummer van gegenereerde: |
| | | | Opties | 1 - Belastingscombinaties<br>1 - Resultaatcombinaties<br>☒Veranderlijke- en verkeersbelastingen worden samengevoegd als ï¿½ï¿½n onafhankelijke actie |
| | | | Resultaatcombinaties | ☒Genereer aanvullende of/of resultaatcombinatie (omhullende)<br>☒Genereer aanvullend een verschillende of/of resultaatcombinatie voor elke combinatieregel |
| | | | Gegenereerde belastingscombinaties | |
| | | | Berekeningsmethode : | Geometrisch lineair |
| CE3 | BGT | BGT - Frequent | Beschouw : | ☐Gunstige blijvende acties |
| | | | Nummeren van gegenereerde combinaties | 1e Nummer van gegenereerde: |
| | | | Opties | 1 - Belastingscombinaties<br>1 - Resultaatcombinaties<br>☒Veranderlijke- en verkeersbelastingen worden samengevoegd als ï¿½ï¿½n onafhankelijke actie |
| | | | Resultaatcombinaties | ☒Genereer aanvullende of/of resultaatcombinatie (omhullende)<br>☒Genereer aanvullend een verschillende of/of resultaatcombinatie voor elke combinatieregel |
| | | | Gegenereerde belastingscombinaties | |
| | | | Berekeningsmethode : | Geometrisch lineair |
| CE4 | BGT | BGT - Quasi-blijvend | Beschouw : | ☐Gunstige blijvende acties |
| | | | Nummeren van gegenereerde combinaties | 1e Nummer van gegenereerde: |
| | | | Opties | 1 - Belastingscombinaties<br>1 - Resultaatcombinaties<br>☒Veranderlijke- en verkeersbelastingen worden samengevoegd als ï¿½ï¿½n onafhankelijke actie |
| | | | Resultaatcombinaties | ☒Genereer aanvullende of/of resultaatcombinatie (omhullende)<br>☒Genereer aanvullend een verschillende of/of resultaatcombinatie voor elke combinatieregel |
| | | | Gegenereerde belastingscombinaties | |
| | | | Berekeningsmethode : | Geometrisch lineair |
| | | | Nummeren van gegenereerde combinaties | 1e Nummer van gegenereerde: |
| | | | Resultaatcombinaties | 1 - Belastingscombinaties<br>1 - Resultaatcombinaties<br>☒Genereer aanvullende of/of resultaatcombinatie (omhullende)<br>☒Genereer aanvullend een verschillende of/of resultaatcombinatie voor elke combinatieregel |
| | | | Gegenereerde belastingscombinaties | |
| | | | Berekeningsmethode : | Geometrisch lineair |
| CE5 | Brand | UGT (STR/GEO) - Buitengewoon - psi-2,1 | Berekeningsmethode | Geometrisch lineair |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| BC1 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| BC2 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| BC3 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| BC4 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| BC5 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC6 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| BC7 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC8 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC9 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC10 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC11 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG130 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| BC12 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG130 + 1 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | 1.65*BG140 | | | | |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC13 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC14 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC15 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG140 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC16 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC17 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG150 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| BC18 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| BC19 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG130 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| BC20 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC21 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC22 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC23 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG140 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC24 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC25 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG150 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| BC26 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG130 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| BC27 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG130 + 1.65*BG140 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC28 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC29 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG130 + 1.65*BG150 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| BC30 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG140 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC31 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG140 + 1.65*BG150 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| BC32 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG150 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| BC33 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| BC34 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| BC35 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| BC36 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| BC37 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | 1.65*BG140 | | | | |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC38 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| BC39 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC40 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC41 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC42 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC43 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| BC44 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC45 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC46 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC47 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC48 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC49 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| BC50 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| BC51 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| BC52 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC53 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC54 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC55 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC56 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC57 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| BC58 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| BC59 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC60 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC61 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| BC62 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC63 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| BC64 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| BC65 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| BC66 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| BC67 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| BC68 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC69 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| BC70 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC71 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC72 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | 1.65*BG140 + 1.65*BG150 | | | | |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC73 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC74 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| BC75 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC76 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC77 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC78 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC79 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC80 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| BC81 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| BC82 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| BC83 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC84 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC85 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC86 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC87 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC88 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| BC89 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| BC90 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC91 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC92 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| BC93 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC94 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| BC95 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| BC96 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | 1.32*BG40 + 1.65*BG120 | | | | |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG120 | VB: Dakbelasting |
| BC97 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| BC98 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG120 | VB: Dakbelasting |
| BC99 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.65 | BG130 | VB: Zonnepanelen |
| BC100 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 9 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC101 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 9 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 10 | 1.65 | BG150 | VB: Heftruck |
| BC102 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| BC103 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC104 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| BC105 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC106 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| BC107 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC108 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| BC109 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC110 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG140 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC111 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC112 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC113 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| BC114 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| BC115 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC116 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| BC117 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC118 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC119 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC120 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC121 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG130 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| BC122 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC123 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC124 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC125 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG140 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| BC126 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC127 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| BC128 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG300 | VB: Sneeuw |
| BC129 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG300 | VB: Sneeuw |
| BC130 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG300 | VB: Sneeuw |
| BC131 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG300 | VB: Sneeuw |
| BC132 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG300 | VB: Sneeuw |
| BC133 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| | | | 10 | 1.65 | BG300 | VB: Sneeuw |
| BC134 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG300 | VB: Sneeuw |
| BC135 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG300 | VB: Sneeuw |
| BC136 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 | | | | |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG300 | VB: Sneeuw |
| BC137 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG300 | VB: Sneeuw |
| BC138 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG300 | VB: Sneeuw |
| BC139 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG300 | VB: Sneeuw |
| BC140 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG300 | VB: Sneeuw |
| BC141 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG300 | VB: Sneeuw |
| BC142 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG300 | VB: Sneeuw |
| BC143 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG300 | VB: Sneeuw |
| BC144 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG300 | VB: Sneeuw |
| BC145 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 6 | 1.65 | BG300 | VB: Sneeuw |
| BC146 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG300 | VB: Sneeuw |
| BC147 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG300 | VB: Sneeuw |
| BC148 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG300 | VB: Sneeuw |
| BC149 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG300 | VB: Sneeuw |
| BC150 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG300 | VB: Sneeuw |
| BC151 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG300 | VB: Sneeuw |
| BC152 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG300 | VB: Sneeuw |
| BC153 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG300 | VB: Sneeuw |
| BC154 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG300 | VB: Sneeuw |
| BC155 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 8 | 1.65 | BG300 | VB: Sneeuw |
| BC156 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG300 | VB: Sneeuw |
| BC157 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG300 | VB: Sneeuw |
| BC158 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG300 | VB: Sneeuw |
| BC159 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| | | | 6 | 1.65 | BG300 | VB: Sneeuw |
| BC160 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC161 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC162 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC163 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC164 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC165 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC166 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC167 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC168 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG401 | VB: Wind (+X richting) |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| BC169 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC170 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC171 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC172 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC173 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC174 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC175 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC176 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC177 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC178 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC179 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC180 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| | | | 10 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC181 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| | | | 10 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC182 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| | | | 10 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC183 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| | | | 10 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC184 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC185 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC186 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC187 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC188 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC189 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC190 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC191 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC192 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC193 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC194 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC195 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | 1.65*BG140 + 1.65*BG150 + 1.65*BG404 | | | | |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC196 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC197 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC198 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC199 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC200 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC201 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC202 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC203 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC204 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 8 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC205 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC206 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC207 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC208 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC209 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC210 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC211 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC212 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC213 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 8 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC214 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC215 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC216 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC217 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC218 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC219 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC220 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC221 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC222 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC223 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC224 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC225 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC226 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC227 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC228 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC229 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC230 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC231 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC232 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC233 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC234 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG403 | VB: Wind (+Y richting) |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| BC235 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC236 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC237 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC238 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC239 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC240 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC241 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC242 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC243 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC244 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 | | | | |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC245 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC246 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC247 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC248 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC249 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC250 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC251 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC252 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC253 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 8 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC254 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC255 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC256 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC257 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC258 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC259 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC260 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC261 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC262 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC263 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC264 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG401 | VB: Wind (+X richting) |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| BC265 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC266 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC267 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC268 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC269 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC270 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC271 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC272 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC273 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC274 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG403 | VB: Wind (+Y richting) |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| BC275 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC276 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC277 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC278 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC279 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC280 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC281 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC282 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC283 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC284 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| | | | 6 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC285 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| | | | 6 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC286 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| | | | 6 | 1.65 | BG403 | VB: Wind (+Y richting) |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| BC287 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| | | | 6 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC288 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG120 | VB: Dakbelasting |
| BC289 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| BC290 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG120 | VB: Dakbelasting |
| BC291 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.65 | BG130 | VB: Zonnepanelen |
| BC292 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 9 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC293 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 9 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 10 | 1.65 | BG150 | VB: Heftruck |
| BC294 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| BC295 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC296 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| BC297 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG150 | | | | |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC298 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| BC299 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC300 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| BC301 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC302 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG140 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC303 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC304 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC305 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| BC306 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| BC307 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC308 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| BC309 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC310 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC311 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC312 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC313 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG130 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| BC314 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC315 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| BC316 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC317 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG140 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| BC318 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| BC319 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| BC320 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG300 | VB: Sneeuw |
| BC321 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG300 | VB: Sneeuw |
| BC322 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG300 | VB: Sneeuw |
| BC323 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG300 | VB: Sneeuw |
| BC324 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG300 | VB: Sneeuw |
| BC325 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| | | | 10 | 1.65 | BG300 | VB: Sneeuw |
| BC326 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG300 | VB: Sneeuw |
| BC327 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG300 | VB: Sneeuw |
| BC328 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG300 | VB: Sneeuw |
| BC329 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG300 | VB: Sneeuw |
| BC330 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG300 | VB: Sneeuw |
| BC331 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG300 | VB: Sneeuw |
| BC332 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG300 | VB: Sneeuw |
| BC333 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG300 | VB: Sneeuw |
| BC334 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG300 | VB: Sneeuw |
| BC335 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG300 | VB: Sneeuw |
| BC336 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG300 | VB: Sneeuw |
| BC337 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG300 | VB: Sneeuw |
| BC338 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 7 | 1.65 | BG300 | VB: Sneeuw |
| BC339 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG300 | VB: Sneeuw |
| BC340 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG300 | VB: Sneeuw |
| BC341 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG300 | VB: Sneeuw |
| BC342 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG300 | VB: Sneeuw |
| BC343 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG300 | VB: Sneeuw |
| BC344 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG300 | VB: Sneeuw |
| BC345 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG300 | VB: Sneeuw |
| BC346 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG300 | VB: Sneeuw |
| BC347 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG300 | VB: Sneeuw |
| BC348 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG300 | VB: Sneeuw |
| BC349 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG300 | VB: Sneeuw |
| BC350 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG300 | VB: Sneeuw |
| BC351 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| | | | 6 | 1.65 | BG300 | VB: Sneeuw |
| BC352 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC353 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC354 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC355 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC356 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC357 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC358 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC359 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC360 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC361 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC362 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 7 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC363 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC364 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC365 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC366 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC367 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC368 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC369 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC370 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC371 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC372 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 | | | | |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| | | | 10 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC373 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| | | | 10 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC374 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| | | | 10 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC375 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.65 | BG150 | VB: Heftruck |
| | | | 10 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC376 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC377 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC378 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC379 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC380 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC381 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC382 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC383 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC384 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC385 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC386 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC387 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC388 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC389 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC390 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC391 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC392 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC393 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC394 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC395 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC396 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC397 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC398 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC399 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC400 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC401 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC402 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC403 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC404 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC405 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC406 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC407 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC408 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC409 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC410 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC411 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC412 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC413 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC414 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC415 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC416 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC417 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC418 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC419 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC420 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC421 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC422 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC423 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC424 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC425 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC426 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC427 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC428 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC429 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC430 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 8 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC431 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC432 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC433 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC434 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC435 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.65 | BG150 | VB: Heftruck |
| | | | 9 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC436 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC437 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC438 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC439 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 8 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC440 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC441 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC442 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC443 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC444 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC445 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC446 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC447 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC448 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC449 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC450 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC451 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC452 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC453 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC454 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC455 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC456 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC457 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC458 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC459 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC460 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC461 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC462 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC463 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.65 | BG150 | VB: Heftruck |
| | | | 8 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC464 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC465 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC466 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC467 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC468 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC469 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC470 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC471 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC472 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC473 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC474 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | 1.65*BG140 + 1.65*BG150 + 1.65*BG403 | | | | |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC475 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| | | | 7 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC476 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| | | | 6 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC477 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| | | | 6 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC478 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| | | | 6 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC479 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| | | | 6 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC480 | S Ch | BG10 + BG20 + BG30 + BG40 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| BC481 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| BC482 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| BC483 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| BC484 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG140 | VB: Stellingen - Pallet |
| BC485 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.00 | BG150 | VB: Heftruck |
| BC486 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| BC487 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| BC488 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| BC489 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| BC490 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| BC491 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| BC492 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| BC493 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| BC494 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| BC495 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| BC496 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| BC497 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| BC498 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| BC499 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| BC500 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| BC501 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| BC502 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| BC503 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| BC504 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| BC505 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| BC506 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| BC507 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| BC508 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| BC509 | S Ch | BG10 + BG20 + BG30 + BG40 + BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG140 | VB: Stellingen - Pallet |
| BC510 | S Ch | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| BC511 | S Ch | BG10 + BG20 + BG30 + BG40 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG150 | VB: Heftruck |
| BC512 | S Ch | BG10 + BG20 + BG30 + BG40 + BG120 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG120 | VB: Dakbelasting |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| BC513 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG120 | VB: Dakbelasting |
| BC514 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG120 | VB: Dakbelasting |
| BC515 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.00 | BG130 | VB: Zonnepanelen |
| BC516 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG130 + BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 9 | 1.00 | BG140 | VB: Stellingen - Pallet |
| BC517 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG130 + BG140 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 9 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 10 | 1.00 | BG150 | VB: Heftruck |
| BC518 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG130 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 9 | 1.00 | BG150 | VB: Heftruck |
| BC519 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.00 | BG140 | VB: Stellingen - Pallet |
| BC520 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG140 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.00 | BG150 | VB: Heftruck |
| BC521 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| BC522 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| BC523 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG130 + BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG140 | VB: Stellingen - Pallet |
| BC524 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG130 + BG140 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.00 | BG150 | VB: Heftruck |
| BC525 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG130 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| BC526 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| BC527 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG140 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| BC528 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| BC529 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG120 | VB: Dakbelasting |
| BC530 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| BC531 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG130 + BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG140 | VB: Stellingen - Pallet |
| BC532 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG130 + BG140 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.00 | BG150 | VB: Heftruck |
| BC533 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG130 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| BC534 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + B | 1 | 1.00 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | BG120 + BG140 | | | | |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| BC535 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG140 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| BC536 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| BC537 | S Ch | BG10 + BG20 + BG30 + BG40 + BG120 + BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| BC538 | S Ch | BG10 + BG20 + BG30 + BG40 + BG120 + BG130 + BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| BC539 | S Ch | BG10 + BG20 + BG30 + BG40 + BG120 + BG130 + BG140 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| BC540 | S Ch | BG10 + BG20 + BG30 + BG40 + BG120 + BG130 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| BC541 | S Ch | BG10 + BG20 + BG30 + BG40 + BG120 + BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| BC542 | S Ch | BG10 + BG20 + BG30 + BG40 + BG120 + BG140 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| BC543 | S Ch | BG10 + BG20 + BG30 + BG40 + BG120 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| BC544 | S Ch | BG10 + BG20 + BG30 + BG40 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG300 | VB: Sneeuw |
| BC545 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG300 | VB: Sneeuw |
| BC546 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG300 | VB: Sneeuw |
| BC547 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG300 | VB: Sneeuw |
| BC548 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.00 | BG300 | VB: Sneeuw |
| BC549 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.00 | BG150 | VB: Heftruck |
| | | | 10 | 1.00 | BG300 | VB: Sneeuw |
| BC550 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| | | | 9 | 1.00 | BG300 | VB: Sneeuw |
| BC551 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG300 | VB: Sneeuw |
| BC552 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| | | | 9 | 1.00 | BG300 | VB: Sneeuw |
| BC553 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG300 | VB: Sneeuw |
| BC554 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG300 | VB: Sneeuw |
| BC555 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG300 | VB: Sneeuw |
| BC556 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| | | | 9 | 1.00 | BG300 | VB: Sneeuw |
| BC557 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG300 | VB: Sneeuw |
| BC558 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG300 | VB: Sneeuw |
| BC559 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG300 | VB: Sneeuw |
| BC560 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| | | | 7 | 1.00 | BG300 | VB: Sneeuw |
| BC561 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG300 | VB: Sneeuw |
| BC562 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG300 | VB: Sneeuw |
| BC563 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG300 | VB: Sneeuw |
| BC564 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| | | | 9 | 1.00 | BG300 | VB: Sneeuw |
| BC565 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG300 | VB: Sneeuw |
| BC566 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG300 | VB: Sneeuw |
| BC567 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG300 | VB: Sneeuw |
| BC568 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| | | | 7 | 1.00 | BG300 | VB: Sneeuw |
| BC569 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG300 | VB: Sneeuw |
| BC570 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG300 | VB: Sneeuw |
| BC571 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG300 | VB: Sneeuw |
| BC572 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| | | | 7 | 1.00 | BG300 | VB: Sneeuw |
| BC573 | S Ch | BG10 + BG20 + BG30 + BG40 + BG140 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.00 | BG300 | VB: Sneeuw |
| BC574 | S Ch | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| | | | 7 | 1.00 | BG300 | VB: Sneeuw |
| BC575 | S Ch | BG10 + BG20 + BG30 + BG40 + BG150 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG150 | VB: Heftruck |
| | | | 6 | 1.00 | BG300 | VB: Sneeuw |
| BC576 | S Ch | BG10 + BG20 + BG30 + BG40 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC577 | S Ch | BG10 + BG20 + BG30 + BG40 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC578 | S Ch | BG10 + BG20 + BG30 + BG40 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC579 | S Ch | BG10 + BG20 + BG30 + BG40 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC580 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG401 | VB: Wind (+X richting) |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| BC581 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC582 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC583 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC584 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC585 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC586 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC587 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC588 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC589 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC590 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC591 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC592 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC593 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC594 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC595 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC596 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.00 | BG150 | VB: Heftruck |
| | | | 10 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC597 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.00 | BG150 | VB: Heftruck |
| | | | 10 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC598 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.00 | BG150 | VB: Heftruck |
| | | | 10 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC599 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 1.00 | BG150 | VB: Heftruck |
| | | | 10 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC600 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| | | | 9 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC601 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| | | | 9 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC602 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| | | | 9 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC603 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| | | | 9 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC604 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC605 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC606 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC607 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC608 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| | | | 9 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC609 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| | | | 9 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC610 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| | | | 9 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC611 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| | | | 9 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC612 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC613 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC614 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC615 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC616 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC617 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC618 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC619 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC620 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC621 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC622 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + B | 1 | 1.00 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | BG130 + BG140 + BG403 | | | | |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC623 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC624 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| | | | 9 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC625 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| | | | 9 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC626 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| | | | 9 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC627 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| | | | 9 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC628 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC629 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC630 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC631 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC632 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + B | 1 | 1.00 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | BG140 + BG401 | | | | |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC633 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC634 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC635 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC636 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC637 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC638 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC639 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC640 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| | | | 7 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC641 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| | | | 7 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC642 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| | | | 7 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC643 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| | | | 7 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC644 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC645 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC646 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC647 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC648 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC649 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC650 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC651 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC652 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC653 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC654 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC655 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC656 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| | | | 9 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC657 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| | | | 9 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC658 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| | | | 9 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC659 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 1.00 | BG150 | VB: Heftruck |
| | | | 9 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC660 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC661 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC662 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC663 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC664 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC665 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC666 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC667 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC668 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC669 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC670 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC671 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC672 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| | | | 7 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC673 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| | | | 7 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC674 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| | | | 7 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC675 | S Ch | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| | | | 7 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC676 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC677 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC678 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC679 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC680 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC681 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC682 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC683 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC684 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC685 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC686 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC687 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 1.00 | BG150 | VB: Heftruck |
| | | | 8 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC688 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| | | | 7 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC689 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| | | | 7 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC690 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| | | | 7 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC691 | S Ch | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG130 | VB: Zonnepanelen |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| | | | 7 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC692 | S Ch | BG10 + BG20 + BG30 + BG40 + BG140 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC693 | S Ch | BG10 + BG20 + BG30 + BG40 + BG140 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC694 | S Ch | BG10 + BG20 + BG30 + BG40 + BG140 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC695 | S Ch | BG10 + BG20 + BG30 + BG40 + BG140 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC696 | S Ch | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| | | | 7 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC697 | S Ch | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| | | | 7 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC698 | S Ch | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| | | | 7 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC699 | S Ch | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| | | | 7 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC700 | S Ch | BG10 + BG20 + BG30 + BG40 + BG150 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 5 | 1.00 | BG150 | VB: Heftruck |
| | | | 6 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC701 | S Ch | BG10 + BG20 + BG30 + BG40 + BG150 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG150 | VB: Heftruck |
| | | | 6 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC702 | S Ch | BG10 + BG20 + BG30 + BG40 + BG150 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG150 | VB: Heftruck |
| | | | 6 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC703 | S Ch | BG10 + BG20 + BG30 + BG40 + BG150 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG150 | VB: Heftruck |
| | | | 6 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC704 | S Fr | BG10 + BG20 + BG30 + BG40 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| BC705 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| BC706 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.90 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| BC707 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 + 0.9*BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.90 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.90 | BG130 | VB: Zonnepanelen |
| BC708 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 + 0.9*BG130 + 0.9*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.90 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.90 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.90 | BG140 | VB: Stellingen - Pallet |
| BC709 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 + 0.9*BG130 + 0.9*BG140 + 0.9*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.90 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.90 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.90 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 0.90 | BG150 | VB: Heftruck |
| BC710 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 + 0.9*BG130 + 0.9*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.90 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.90 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.90 | BG150 | VB: Heftruck |
| BC711 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 + 0.9*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.90 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.90 | BG140 | VB: Stellingen - Pallet |
| BC712 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 + 0.9*BG140 + 0.9*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.90 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.90 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.90 | BG150 | VB: Heftruck |
| BC713 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | 0.9*BG110 + 0.9*BG150 | | | | |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.90 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.90 | BG150 | VB: Heftruck |
| BC714 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.90 | BG130 | VB: Zonnepanelen |
| BC715 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG130 + 0.9*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.90 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.90 | BG140 | VB: Stellingen - Pallet |
| BC716 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG130 + 0.9*BG140 + 0.9*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.90 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.90 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.90 | BG150 | VB: Heftruck |
| BC717 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG130 + 0.9*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.90 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.90 | BG150 | VB: Heftruck |
| BC718 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.90 | BG140 | VB: Stellingen - Pallet |
| BC719 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG140 + 0.9*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.90 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.90 | BG150 | VB: Heftruck |
| BC720 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.90 | BG150 | VB: Heftruck |
| BC721 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| BC722 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.90 | BG130 | VB: Zonnepanelen |
| BC723 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG130 + 0.9*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.90 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.90 | BG140 | VB: Stellingen - Pallet |
| BC724 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG130 + 0.9*BG140 + 0.9*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.90 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.90 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.90 | BG150 | VB: Heftruck |
| BC725 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG130 + 0.9*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.90 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.90 | BG150 | VB: Heftruck |
| BC726 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.90 | BG140 | VB: Stellingen - Pallet |
| BC727 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG140 + 0.9*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.90 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.90 | BG150 | VB: Heftruck |
| BC728 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.90 | BG150 | VB: Heftruck |
| BC729 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG130 | VB: Zonnepanelen |
| BC730 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG130 + 0.9*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.90 | BG140 | VB: Stellingen - Pallet |
| BC731 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG130 + 0.9*BG140 + 0.9*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.90 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.90 | BG150 | VB: Heftruck |
| BC732 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG130 + 0.9*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.90 | BG150 | VB: Heftruck |
| BC733 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG140 | VB: Stellingen - Pallet |
| BC734 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG140 + 0.9*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 0.90 | BG150 | VB: Heftruck |
| BC735 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG150 | VB: Heftruck |
| BC736 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.00 | BG120 | VB: Dakbelasting |
| BC737 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.00 | BG120 | VB: Dakbelasting |
| BC738 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 8 | 0.80 | BG130 | VB: Zonnepanelen |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| BC739 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG130 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 8 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 9 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC740 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 8 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 9 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 10 | 0.80 | BG150 | VB: Heftruck |
| BC741 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG130 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 8 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 9 | 0.80 | BG150 | VB: Heftruck |
| BC742 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 8 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC743 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 8 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 0.80 | BG150 | VB: Heftruck |
| BC744 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| BC745 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| BC746 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG130 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC747 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 0.80 | BG150 | VB: Heftruck |
| BC748 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG130 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.00 | BG120 | VB: Dakbelasting |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| BC749 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC750 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| BC751 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| BC752 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.00 | BG120 | VB: Dakbelasting |
| BC753 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0.8*BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| BC754 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0.8*BG130 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC755 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 0.80 | BG150 | VB: Heftruck |
| BC756 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0.8*BG130 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| BC757 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC758 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| BC759 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.00 | BG120 | VB: Dakbelasting |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| BC760 | S Fr | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| BC761 | S Fr | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG130 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC762 | S Fr | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| BC763 | S Fr | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG130 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| BC764 | S Fr | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC765 | S Fr | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| BC766 | S Fr | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| BC767 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.20 | BG300 | VB: Sneeuw |
| BC768 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.20 | BG300 | VB: Sneeuw |
| BC769 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.20 | BG300 | VB: Sneeuw |
| BC770 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.20 | BG300 | VB: Sneeuw |
| BC771 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG140 | VB: Stellingen - Pallet |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 9 | 0.20 | BG300 | VB: Sneeuw |
| BC772 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 0.80 | BG150 | VB: Heftruck |
| | | | 10 | 0.20 | BG300 | VB: Sneeuw |
| BC773 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| | | | 9 | 0.20 | BG300 | VB: Sneeuw |
| BC774 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.20 | BG300 | VB: Sneeuw |
| BC775 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| | | | 9 | 0.20 | BG300 | VB: Sneeuw |
| BC776 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG150 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG300 | VB: Sneeuw |
| BC777 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.20 | BG300 | VB: Sneeuw |
| BC778 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.20 | BG300 | VB: Sneeuw |
| BC779 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| | | | 9 | 0.20 | BG300 | VB: Sneeuw |
| BC780 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG300 | VB: Sneeuw |
| BC781 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.20 | BG300 | VB: Sneeuw |
| BC782 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG300 | VB: Sneeuw |
| BC783 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| | | | 7 | 0.20 | BG300 | VB: Sneeuw |
| BC784 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.20 | BG300 | VB: Sneeuw |
| BC785 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.20 | BG300 | VB: Sneeuw |
| BC786 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.20 | BG300 | VB: Sneeuw |
| BC787 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| | | | 9 | 0.20 | BG300 | VB: Sneeuw |
| BC788 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG300 | VB: Sneeuw |
| BC789 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.20 | BG300 | VB: Sneeuw |
| BC790 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG300 | VB: Sneeuw |
| BC791 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| | | | 7 | 0.20 | BG300 | VB: Sneeuw |
| BC792 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.20 | BG300 | VB: Sneeuw |
| BC793 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.20 | BG300 | VB: Sneeuw |
| BC794 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG300 | VB: Sneeuw |
| BC795 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| | | | 7 | 0.20 | BG300 | VB: Sneeuw |
| BC796 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 0.20 | BG300 | VB: Sneeuw |
| BC797 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| | | | 7 | 0.20 | BG300 | VB: Sneeuw |
| BC798 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG150 | VB: Heftruck |
| | | | 6 | 0.20 | BG300 | VB: Sneeuw |
| BC799 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC800 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC801 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC802 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC803 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC804 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC805 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC806 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC807 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC808 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC809 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC810 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC811 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC812 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC813 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC814 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC815 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC816 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 0.20 | BG402 | VB: Wind (-X richting) |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| BC817 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC818 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC819 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 0.80 | BG150 | VB: Heftruck |
| | | | 10 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC820 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 0.80 | BG150 | VB: Heftruck |
| | | | 10 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC821 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 0.80 | BG150 | VB: Heftruck |
| | | | 10 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC822 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 0.80 | BG150 | VB: Heftruck |
| | | | 10 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC823 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| | | | 9 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC824 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| | | | 9 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC825 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | 0.2*BG403 | | | | |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| | | | 9 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC826 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| | | | 9 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC827 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC828 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC829 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC830 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC831 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| | | | 9 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC832 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| | | | 9 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC833 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| | | | 9 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC834 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| | | | 9 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC835 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG150 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC836 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG150 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC837 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG150 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC838 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG150 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC839 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC840 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC841 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC842 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC843 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC844 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC845 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC846 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC847 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| | | | 9 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC848 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| | | | 9 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC849 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| | | | 9 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC850 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| | | | 9 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC851 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC852 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC853 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC854 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC855 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC856 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC857 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC858 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC859 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC860 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC861 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC862 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC863 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| | | | 7 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC864 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| | | | 7 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC865 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| | | | 7 | 0.20 | BG403 | VB: Wind (+Y richting) |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| BC866 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| | | | 7 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC867 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC868 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC869 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC870 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC871 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC872 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC873 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC874 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC875 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC876 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC877 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 8 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC878 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC879 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| | | | 9 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC880 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| | | | 9 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC881 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| | | | 9 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC882 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| | | | 9 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC883 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC884 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC885 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC886 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC887 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC888 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC889 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC890 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC891 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC892 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC893 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC894 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC895 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| | | | 7 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC896 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| | | | 7 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC897 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| | | | 7 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC898 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| | | | 7 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC899 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC900 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC901 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC902 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC903 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC904 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC905 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC906 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC907 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC908 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC909 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC910 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| | | | 8 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC911 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| | | | 7 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC912 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| | | | 7 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC913 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| | | | 7 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC914 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| | | | 7 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC915 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC916 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC917 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC918 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC919 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| | | | 7 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC920 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| | | | 7 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC921 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| | | | 7 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC922 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG140 | VB: Stellingen - Pallet |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| | | | 7 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC923 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG150 | VB: Heftruck |
| | | | 6 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC924 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG150 | VB: Heftruck |
| | | | 6 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC925 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG150 | VB: Heftruck |
| | | | 6 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC926 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG150 | VB: Heftruck |
| | | | 6 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC927 | S Qp | BG10 + BG20 + BG30 + BG40 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| BC928 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| BC929 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| BC930 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| BC931 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC932 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 0.80 | BG150 | VB: Heftruck |
| BC933 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| BC934 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC935 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| BC936 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| BC937 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| BC938 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC939 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| BC940 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| BC941 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC942 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| BC943 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| BC944 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| BC945 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| BC946 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC947 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| BC948 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| BC949 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC950 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| BC951 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| BC952 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| BC953 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC954 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| BC955 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| BC956 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC957 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| BC958 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG150 | VB: Heftruck |
| BC959 | ACC' | BG10 + BG20 + BG30 + BG40 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| BC960 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| BC961 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| BC962 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | 0.8*BG110 + 0.8*BG130 | | | | |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| BC963 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC964 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 9 | 0.80 | BG150 | VB: Heftruck |
| BC965 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| BC966 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC967 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| BC968 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| BC969 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| BC970 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC971 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| BC972 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| BC973 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | 0.8*BG140 | | | | |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC974 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| BC975 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| BC976 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| BC977 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| BC978 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC979 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 8 | 0.80 | BG150 | VB: Heftruck |
| BC980 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| BC981 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC982 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| BC983 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG110 | VB: Opgelegde belasting op vloeren 2 |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| BC984 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| BC985 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC986 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | Belastingscombinatie OS | Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 7 | 0.80 | BG150 | VB: Heftruck |
| BC987 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG130 | VB: Zonnepanelen |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| BC988 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG140 | VB: Stellingen - Pallet |
| BC989 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG140 | VB: Stellingen - Pallet |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| BC990 | ACC' | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG150 | VB: Heftruck |

## 2.7 RESULTAATCOMBINATIES

| Resulta Combin. | Omschrijving | Belasting |
|---|---|---|
| RC1 | UGT (STR/GEO) - Blijvend / tijdelijk - verg. 6.10a en 6.10b | BC1/b of tot BC479 |
| RC2 | BGT - Karakteristiek | BC480/b of tot BC703 |
| RC3 | BGT - Frequent | BC704/b of tot BC926 |
| RC4 | BGT - Quasi-blijvend | BC927/b of tot BC958 |
| RC5 | UGT (STR/GEO) - Buitengewoon - psi-2,1 | BC959/b of tot BC990 |
| RC10 | DBG1 - Resultaatomhullende - X | BG800/b + BG802/b + BG804/b + BG806/b |
| RC11 | DBG1 - Resultaatomhullende - Y | BG801/b + BG803/b + BG805/b + BG807/b |
| RC12 | DBG1 - Resultaatomhullende - 100% X/ 30% Y | RC10/b + 0.3*RC11/b |
| RC13 | DBG1 - Resultaatomhullende - 30% X/ 100% Y | 0.3*RC10/b + RC11/b |
| RC20 | Tabel NB.7 A1.3 | BG10/b + BG20/b + BG30/b + BG40/b + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + RC12 of RC13 |

**BG20**
PB: Dakbedekking

## 3.15 GEGENEREERDE LASTEN

BG20: PB: Dakbedekking

| No. | Belastingomschrijving | | | | | |
|---|---|---|---|---|---|---|
| 1 | **Van Vlaklasten via vlak** | | | | | |
| | Vlaklastrichting | Globaal gerelateerd aan geprojecteerde vlak: | | : | ☒ZP | |
| | Lasttoewijzingsbereik | ☒Volledig gesloten vlak | | | | |
| | Lastverdelingstype: | ☒Gecombineerd | | | | |
| | Vlaklast grootte | ☒Constant | | : | -0.850 | kN/m² |
| | Grens van vlaklast vlak | Hoekknopen | | : | 56,42,39,45; 42,57,46,39 | |
| | | Aanwijzing | | : | Elke rij in de lijst geeft een vlak weer | |
| | Verwijder invloed van | Staven parallel aan Staaf | | : | 67 | |
| | Gegenereerde totale belastingen in richting | $\Sigma P_{Vlakken}$ | X | : | 0.00 | kN |
| | | | Y | : | 0.00 | kN |
| | | | Z | : | -365.18 | kN |
| | | $\Sigma P_{Staven}$ | X | : | 0.00 | kN |
| | | | Y | : | 0.00 | kN |
| | | | Z | : | -365.18 | kN |
| | Totale moment bij de oorsprong | $\Sigma M_{Vlakken}$ | X | : | -4108.28 | kNm |
| | | | Y | : | 3622.59 | kNm |
| | | | Z | : | 0.00 | kNm |
| | | $\Sigma M_{Staven}$ | X | : | -4108.28 | kNm |
| | | | Y | : | 3622.90 | kNm |
| | | | Z | : | 0.00 | kNm |
| | Cellen geselecteerd voor genereren | Σ aantal cellen | | : | 11 | |
| | | Σ cel vlak | | : | 429624002 | mm² |
| | Converteren van Vlaklasten naar Staaf No. | | | : | 7,8,11,12,15,16,19,20, 23,24,27,28,34,38,45,4 | |

## 3.15 GEGENEREERDE LASTEN — BG20: PB: Dakbedekking

| No. | Belastingomschrijving |
|---|---|
| | 46,83,85,174,183-201 |

**BG30**
PB: KSZ - Metselwerk

## 3.2 STAAFBELASTINGEN — BG30: PB: KSZ - Metselwerk

| No. | Referentie tot | Op Staven No. | Belasting Type | Belasting Verdeling | Belasting Richting | Referentie Lengte | Lastparameters Symbool | Waarde | Eenheid |
|---|---|---|---|---|---|---|---|---|---|
| 1 | Staven | 1-4,35,36, 39-42,104, 105,108-111 | Kracht | Gelijkmatig | ZL | Ware Lengte | p | -11.25 | kN/m |

## 3.2/1 STAAFBELASTINGEN - EXCENTRICITEIT VAN DE KRACHT — BG30: PB: KSZ - Metselwerk

| No. | Referenti tot | Op Staven No. | Absolute Offset Staafbegin | Absolute Offset Staafeinde | Relatieve Offset Staafbegin | Relatieve Offset Staafeinde |
|---|---|---|---|---|---|---|
| | | | $e_Y$ [mm] / $e_Z$ [mm] | $e_Y$ [mm] / $e_Z$ [mm] | y-as / z-as | y-as / z-as |
| 1 | Staven | 1-4,35,36, 39-42,104, 105, 108-111 | 0.0 / 0.0 | 0.0 / 0.0 | Midden / Midden | Midden / Midden |

**BG40**
PB: Sandwichpaneel

## 3.15 GEGENEREERDE LASTEN — BG40: PB: Sandwichpaneel

| No. | Belastingomschrijving | | | |
|---|---|---|---|---|
| 1 | **Van Vlaklasten via vlak** | | | |
| | Vlaklastrichting | Globaal t.o.v. echt vlak: | : | ☒ZL |
| | Lasttoewijzingsbereik | ☒Volledig gesloten vlak | | |
| | Lastverdelingstype: | ☒Gecombineerd | | |
| | Vlaklast grootte | ☒Constant | : | -0.300 kN/m² |
| | Grens van vlaklast vlak | Hoekknopen | : | 13,22,56,45; 13,18,46,39,45; 18,21,57,46; 21,22,56,42,57 |
| | | Aanwijzing | : | Elke rij in de lijst geeft een vlak weer |
| | Verwijder invloed van | Enkele Liggers | : | 120,121,122,123,124, 125,126,127,128,129, 130,131,132,133,134, 135,136,137,138,139, 146,147,156,157,158, 159,165,166,179,180 |
| | | Staven parallel aan Staaf | : | 188,7,201,8,194,38,47, 53 |
| | Gegenereerde totale belastingen in richting | $\Sigma P_{Vlakken}$ X | : | 0.00 kN |
| | | Y | : | 0.00 kN |
| | | Z | : | -134.76 kN |
| | | $\Sigma P_{Staven}$ X | : | 0.00 kN |
| | | Y | : | 0.00 kN |
| | | Z | : | -134.76 kN |
| | Totale moment bij de oorsprong | $\Sigma M_{Vlakken}$ X | : | -1516.04 kNm |
| | | Y | : | 1338.32 kNm |
| | | Z | : | 0.00 kNm |
| | | $\Sigma M_{Staven}$ X | : | -1516.04 kNm |
| | | Y | : | 1338.32 kNm |
| | | Z | : | 0.00 kNm |
| | Cellen geselecteerd voor genereren | Σ aantal cellen | : | 16 |
| | | Σ cel vlak | : | 449195904 mm² |
| | Converteren van Vlaklasten naar Staaf No. | | : | 5,6,9,10,13,14,17,18, 21,22,25,26,29-31,80, 103,107,140-143,145, 149-153,175-178 |

**BG100**
VB: Opgelegde belasting op vloeren 1

## 3.8 VRIJE BLOKLASTEN — BG100: VB: Opgelegde belasting op vloeren 1

| No. | Op vlakken No. | Project. | Belasting Verdeling | Belasting Richting | Grootte Symbool | Waarde | Eenheid | Positie belasting X [mm] | Y [mm] | Z [mm] |
|---|---|---|---|---|---|---|---|---|---|---|
| 1 | 1 | XY | Gelijkmatig | ZL | p | -3.000 | kN/m² | 1650 | 200 | |
| | | | | | | | | 5150 | 4500 | |
| 2 | 1 | XY | Gelijkmatig | ZL | p | -3.000 | kN/m² | 8105 | 200 | |
| | | | | | | | | 11605 | 4500 | |
| 3 | 1 | XY | Gelijkmatig | ZL | p | -3.000 | kN/m² | 14625 | 200 | |
| | | | | | | | | 18125 | 4500 | |
| 4 | 1 | XY | Gelijkmatig | ZL | p | -3.000 | kN/m² | 1650 | 9000 | |
| | | | | | | | | 5150 | 13500 | |
| 5 | 1 | XY | Gelijkmatig | ZL | p | -3.000 | kN/m² | 8105 | 9000 | |
| | | | | | | | | 11605 | 13500 | |
| 6 | 1 | XY | Gelijkmatig | ZL | p | -3.000 | kN/m² | 14625 | 9000 | |
| | | | | | | | | 18125 | 13500 | |
| 7 | 1 | XY | Gelijkmatig | ZL | p | -3.000 | kN/m² | 1650 | 18000 | |

## 3.8 VRIJE BLOKLASTEN — BG100: VB: Opgelegde belasting op vloeren 1

| No. | Op vlakken No. | Project. | Belasting Verdeling | Belasting Richting | Grootte Symbool | Grootte Waarde | Grootte Eenheid | Positie belasting X [mm] | Positie belasting Y [mm] | Positie belasting Z [mm] |
|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | | | | 5150 | 22300 | |
| 8 | 1 | XY | Gelijkmatig | ZL | p | -3.000 | kN/m² | 8105 | 18000 | |
| | | | | | | | | 11605 | 22300 | |
| 9 | 1 | XY | Gelijkmatig | ZL | p | -3.000 | kN/m² | 14625 | 18000 | |
| | | | | | | | | 18125 | 22300 | |

**BG110**
VB: Opgelegde belasting op vloeren 2

## 3.8 VRIJE BLOKLASTEN — BG110: VB: Opgelegde belasting op vloeren 2

| No. | Op vlakken No. | Project. | Belasting Verdeling | Belasting Richting | Grootte Symbool | Grootte Waarde | Grootte Eenheid | Positie belasting X [mm] | Positie belasting Y [mm] | Positie belasting Z [mm] |
|---|---|---|---|---|---|---|---|---|---|---|
| 1 | 1 | XY | Gelijkmatig | ZL | p | -3.000 | kN/m² | 1650 | 4500 | |
| | | | | | | | | 5150 | 9000 | |
| 2 | 1 | XY | Gelijkmatig | ZL | p | -3.000 | kN/m² | 8105 | 4500 | |
| | | | | | | | | 11605 | 9000 | |
| 3 | 1 | XY | Gelijkmatig | ZL | p | -3.000 | kN/m² | 14625 | 4500 | |
| | | | | | | | | 18125 | 9000 | |
| 4 | 1 | XY | Gelijkmatig | ZL | p | -3.000 | kN/m² | 5150 | 9000 | |
| | | | | | | | | 8105 | 13500 | |
| 5 | 1 | XY | Gelijkmatig | ZL | p | -3.000 | kN/m² | 11605 | 9000 | |
| | | | | | | | | 14625 | 13500 | |
| 6 | 1 | XY | Gelijkmatig | ZL | p | -3.000 | kN/m² | 1650 | 13500 | |
| | | | | | | | | 5150 | 18000 | |
| 7 | 1 | XY | Gelijkmatig | ZL | p | -3.000 | kN/m² | 8105 | 13500 | |
| | | | | | | | | 11605 | 18000 | |
| 8 | 1 | XY | Gelijkmatig | ZL | p | -3.000 | kN/m² | 14625 | 13500 | |
| | | | | | | | | 18125 | 18000 | |
| 9 | 1 | XY | Gelijkmatig | ZL | p | -3.000 | kN/m² | 200 | 9000 | |
| | | | | | | | | 1650 | 13500 | |
| 10 | 1 | XY | Gelijkmatig | ZL | p | -3.000 | kN/m² | 18125 | 9000 | |
| | | | | | | | | 19640 | 13500 | |

**BG120**
VB: Dakbelasting

## 3.15 GEGENEREERDE LASTEN — BG120: VB: Dakbelasting

| No. | Belastingomschrijving | | | | |
|---|---|---|---|---|---|
| 1 | **Van Vlaklasten via vlak** | | | | |
| | Vlaklastrichting | Globaal gerelateerd aan geprojecteerde vlak: | | : | ☒ZP |
| | Lasttoewijzingsbereik | ☒Volledig gesloten vlak | | | |
| | Lastverdelingstype: | ☒Gecombineerd | | | |
| | Vlaklast grootte | ☒Constant | | : | -1.000 kN/m² |
| | Grens van vlaklast vlak | Hoekknopen | | : | 56,42,39,45; 42,57,46,39 |
| | | Aanwijzing | | : | Elke rij in de lijst geeft een vlak weer |
| | Verwijder invloed van | Staven parallel aan Staaf | | : | 67 |
| | Gegenereerde totale belastingen in richting | $\Sigma P_{Vlakken}$ | X | : | 0.00 kN |
| | | | Y | : | 0.00 kN |
| | | | Z | : | -429.62 kN |
| | | $\Sigma P_{Staven}$ | X | : | 0.00 kN |
| | | | Y | : | 0.00 kN |
| | | | Z | : | -429.62 kN |
| | Totale moment bij de oorsprong | $\Sigma M_{Vlakken}$ | X | : | -4833.27 kNm |
| | | | Y | : | 4261.87 kNm |
| | | | Z | : | 0.00 kNm |
| | | $\Sigma M_{Staven}$ | X | : | -4833.27 kNm |
| | | | Y | : | 4262.23 kNm |
| | | | Z | : | 0.00 kNm |
| | Cellen geselecteerd voor genereren | Σ aantal cellen | | : | 11 |
| | | Σ cel vlak | | : | 429624002 mm² |
| | Converteren van Vlaklasten naar Staaf No. | | | : | 7,8,11,12,15,16,19,20, 23,24,27,28,34,38,45, 46,83,85,174,183-201 |

**BG130**
VB: Zonnepanelen

## 3.15 GEGENEREERDE LASTEN — BG130: VB: Zonnepanelen

| No. | Belastingomschrijving | | | |
|---|---|---|---|---|
| 1 | **Van Vlaklasten via vlak** | | | |
| | Vlaklastrichting | Globaal gerelateerd aan geprojecteerde vlak: | : | ☒ZP |
| | Lasttoewijzingsbereik | ☒Volledig gesloten vlak | | |
| | Lastverdelingstype: | ☒Gecombineerd | | |
| | Vlaklast grootte | ☒Constant | : | -0.500 kN/m² |
| | Grens van vlaklast vlak | Hoekknopen | : | 56,42,39,45; 42,57,46,39 |
| | | Aanwijzing | : | Elke rij in de lijst geeft een vlak weer |

## 3.15 GEGENEREERDE LASTEN — BG130: VB: Zonnepanelen

| No. | Belastingomschrijving | | | | | |
|---|---|---|---|---|---|---|
| | Verwijder invloed van | Staven parallel aan Staaf | | : | 67 | |
| | Gegenereerde totale belastingen in richting | $\Sigma P_{Vlakken}$ | X | : | 0.00 | kN |
| | | | Y | : | 0.00 | kN |
| | | | Z | : | -214.81 | kN |
| | | $\Sigma P_{Staven}$ | X | : | 0.00 | kN |
| | | | Y | : | 0.00 | kN |
| | | | Z | : | -214.81 | kN |
| | Totale moment bij de oorsprong | $\Sigma M_{Vlakken}$ | X | : | -2416.63 | kNm |
| | | | Y | : | 2130.93 | kNm |
| | | | Z | : | 0.00 | kNm |
| | | $\Sigma M_{Staven}$ | X | : | -2416.63 | kNm |
| | | | Y | : | 2131.12 | kNm |
| | | | Z | : | 0.00 | kNm |
| | Cellen geselecteerd voor genereren | Σ aantal cellen | | : | 11 | |
| | | Σ cel vlak | | : | 429624002 | $mm^2$ |
| | Converteren van Vlaklasten naar Staaf No. | | | : | 7,8,11,12,15,16,19,20, 23,24,27,28,34,38,45, 46,83,85,174,183-201 | |

**BG140**
VB: Stellingen - Pallet

## 3.8 VRIJE BLOKLASTEN — BG140: VB: Stellingen - Pallet

| No. | Op vlakken No. | Project. | Belasting Verdeling | Belasting Richting | Grootte Symbool | Grootte Waarde | Grootte Eenheid | Positie belasting X [mm] | Positie belasting Y [mm] | Positie belasting Z [mm] |
|---|---|---|---|---|---|---|---|---|---|---|
| 1 | 1 | XY | Gelijkmatig | ZL | p | -30.000 | $kN/m^2$ | 200 | 200 | |
| | | | | | | | | 1650 | 9000 | |
| 2 | 1 | XY | Gelijkmatig | ZL | p | -30.000 | $kN/m^2$ | 5150 | 200 | |
| | | | | | | | | 6600 | 9000 | |
| 3 | 1 | XY | Gelijkmatig | ZL | p | -30.000 | $kN/m^2$ | 6600 | 0 | |
| | | | | | | | | 8105 | 9000 | |
| 4 | 1 | XY | Gelijkmatig | ZL | p | -30.000 | $kN/m^2$ | 11605 | 200 | |
| | | | | | | | | 13110 | 9000 | |
| 5 | 1 | XY | Gelijkmatig | ZL | p | -30.000 | $kN/m^2$ | 18125 | 200 | |
| | | | | | | | | 19640 | 9000 | |
| 6 | 1 | XY | Gelijkmatig | ZL | p | -30.000 | $kN/m^2$ | 200 | 13500 | |
| | | | | | | | | 1650 | 22300 | |
| 7 | 1 | XY | Gelijkmatig | ZL | p | -30.000 | $kN/m^2$ | 5150 | 13500 | |
| | | | | | | | | 6600 | 22300 | |
| 8 | 1 | XY | Gelijkmatig | ZL | p | -30.000 | $kN/m^2$ | 6600 | 13500 | |
| | | | | | | | | 8105 | 22300 | |
| 9 | 1 | XY | Gelijkmatig | ZL | p | -30.000 | $kN/m^2$ | 11605 | 13500 | |
| | | | | | | | | 13110 | 22300 | |
| 10 | 1 | XY | Gelijkmatig | ZL | p | -30.000 | $kN/m^2$ | 13110 | 13500 | |
| | | | | | | | | 14625 | 22300 | |
| 11 | 1 | XY | Gelijkmatig | ZL | p | -30.000 | $kN/m^2$ | 18125 | 13500 | |
| | | | | | | | | 19640 | 22300 | |
| 12 | 1 | XY | Gelijkmatig | ZL | p | -30.000 | $kN/m^2$ | 13110 | 200 | |
| | | | | | | | | 14625 | 9000 | |

**BG150**
VB: Heftruck

## 3.1 KNOOPBELASTINGEN - PER COMPONENT - COï¿½RDINATENSYSTEEM — BG150: VB: Heftruck

| No. | Op Knoop No. | Coï¿½rdinaten Syteem | Kracht [kN] $P_X$ / $P_U$ | $P_Y$ / $P_V$ | $P_Z$ / $P_W$ | Moment [kNm] $M_X$ / $M_U$ | $M_Y$ / $M_V$ | $M_Z$ / $M_W$ |
|---|---|---|---|---|---|---|---|---|
| 2 | 141-144 | 0 \| Globaal XYZ | 6.00 | 0.00 | -28.00 | 0.00 | 0.00 | 0.00 |

**BG300**
VB: Sneeuw

## 3.15 GEGENEREERDE LASTEN — BG300: VB: Sneeuw

| No. | Belastingomschrijving | | | | | |
|---|---|---|---|---|---|---|
| 1 | **Van Vlaklasten via vlak** | | | | | |
| | Vlaklastrichting | Globaal gerelateerd aan geprojecteerde vlak: | | : | ☒ZP | |
| | Lasttoewijzingsbereik | ☒Volledig gesloten vlak | | | | |
| | Lastverdelingstype: | ☒Gecombineerd | | | | |
| | Vlaklast grootte | ☒Constant | | : | -1.400 | $kN/m^2$ |
| | Grens van vlaklast vlak | Hoekknopen | | : | 56,42,39,45; 42,57,46,39 | |
| | | Aanwijzing | | : | Elke rij in de lijst geeft een vlak weer | |
| | Verwijder invloed van | Staven parallel aan Staaf | | : | 67 | |
| | Gegenereerde totale belastingen in richting | $\Sigma P_{Vlakken}$ | X | : | 0.00 | kN |
| | | | Y | : | 0.00 | kN |
| | | | Z | : | -601.47 | kN |
| | | $\Sigma P_{Staven}$ | X | : | 0.00 | kN |
| | | | Y | : | 0.00 | kN |
| | | | Z | : | -601.47 | kN |
| | Totale moment bij de oorsprong | $\Sigma M_{Vlakken}$ | X | : | -6766.58 | kNm |

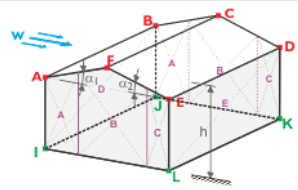
## 3.15 GEGENEREERDE LASTEN — BG300: VB: Sneeuw

| No. | Belastingomschrijving | | | | | |
|---|---|---|---|---|---|---|
| | | | Y | : | 5966.62 | kNm |
| | | | Z | : | 0.00 | kNm |
| | | $\Sigma M_{Staven}$ | X | : | -6766.58 | kNm |
| | | | Y | : | 5967.13 | kNm |
| | | | Z | : | 0.00 | kNm |
| | Cellen geselecteerd voor genereren | Σ aantal cellen | | : | 11 | |
| | | Σ cel vlak | | : | 429624002 | $mm^2$ |
| | Converteren van Vlaklasten naar Staaf No. | | | : | 7,8,11,12,15,16,19,20, 23,24,27,28,34,38,45, 46,83,85,174,183-201 | |

**BG401**
VB: Wind (+X richting)

## 3.15 GEGENEREERDE LASTEN — BG401: VB: Wind (+X richting)

| No. | Belastingomschrijving | | | | | |
|---|---|---|---|---|---|---|
| 2 | **Van Windbelastingen (Verticale Wanden)** | | | | | |




| | | | | | | |
|---|---|---|---|---|---|---|
| Snelheidsdruk | Volgens de norm | | : | EN 1991-1-4 | |
| | Nationale Bijlage | | : | Nederland | |
| | Windgebied | | : | III | |
| | Terrein categorie | | : | Categorie II | |
| | Constructie hoogte | h | : | 8500 | mm |
| | Fundamentele windsnelheid | $v_{b,0}$ | : | 24.5 | m/s |
| Basisgeometrie | Knoop | I | : | 5 | |
| | | J | : | 8 | |
| | | K | : | 7 | |
| | | L | : | 6 | |
| Daktype en geometrie | Type | | : | ⦿ Zadeldak | |
| | Knoop | A | : | 45 | |
| | | B | : | 56 | |
| | | C | : | 42 | |
| | | D | : | 57 | |
| | | E | : | 46 | |
| | | F | : | 39 | |
| BG genereren | ☒BG w | | : | BG401 | |
| Stel wind in op een zijde | ⦿ A - B | | | | |
| Maak Last Type | ⦿ Staafbelastingen | | | | |
| Lastverdelingstype | ⦿ Constant | | | | |
| Verwijder invloed van | Enkele Liggers | | : | 1,2,3,4,188,7,201,8, 183,27,195,28,189,34, 35,36,194,38,39,40,41, 42,47,48,49,50,51,52, 53,54,55,56,57,58,59, 60,61,62,63,64,65,66, 67,68,69,70,71,72,74, 76,104,105,108,109, 110,111,120,121,122, 123,124,125,126,127, 128,129,130,131,132, 133,134,135,136,137, 138,139,144,146,147, 148,154,155,156,157, 158,159,160,162,163, 164,165,166,179,180 | |
| Windbelasting wordt gegenereerd op staaf No. | | | : | 5,6,9,10,13,14,17,18, 21,22,25,26,29-33,80, 103,107,140-143,145, 149-153,175-178 | |
| Wandafmetingen | h | | : | 8500 | mm |
| | b | | : | 22100 | mm |
| | d | | : | 19440 | mm |
| | e | | : | 17000 | mm |
| | A | | : | 656901877 | $mm^2$ |
| | $d_A$ | | : | 3400 | mm |
| | $d_B$ | | : | 13600 | mm |
| | $d_C$ | | : | 2440 | mm |

| Gebied | Externe drukcoï¿½fficiï¿½nt $c_{pe,10}$ | Externe Druk $w_e$ [kN/m²] |
|---|---|---|
| A | -1.200 | -0.795 |
| B | -0.800 | -0.530 |
| C | -0.500 | -0.331 |

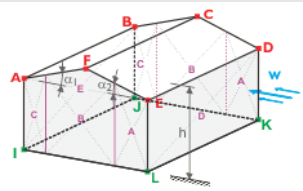
## 3.15 GEGENEREERDE LASTEN — BG401: VB: Wind (+X richting)

| No. | Belastingomschrijving | | | | |
|---|---|---|---|---|---|
| | D | 0.800 | 0.530 | | |
| | E | -0.500 | -0.331 | | |
| | Gegenereerde totaalbelastingen | $\Sigma P_{Vlakken}$ | : | 149.48 | kN |
| | | $\Sigma P$ | : | 149.48 | kN |
| | Totale moment bij de oorsprong | $\Sigma M_{Vlakken}$ | : | 1781.03 | kNm |
| | | $\Sigma M$ | : | 1781.02 | kNm |
| | Cellen geselecteerd voor genereren | $\Sigma$ aantal cellen | : | 28 | |
| | | $\Sigma$ cel vlak | : | 1276747749 | $mm^2$ |

**BG402**
VB: Wind (-X richting)

## 3.15 GEGENEREERDE LASTEN — BG402: VB: Wind (-X richting)

| No. | Belastingomschrijving | | | | |
|---|---|---|---|---|---|
| 2 | **Van Windbelastingen (Verticale Wanden)** | | | | |




| | | | | | |
|---|---|---|---|---|---|
| Snelheidsdruk | Volgens de norm | | : | EN 1991-1-4 | |
| | Nationale Bijlage | | : | Nederland | |
| | Windgebied | | : | III | |
| | Terrein categorie | | : | Categorie II | |
| | Constructie hoogte | h | : | 8500 | mm |
| | Fundamentele windsnelheid | $v_{b,0}$ | : | 24.5 | m/s |
| Basisgeometrie | Knoop | I | : | 5 | |
| | | J | : | 8 | |
| | | K | : | 7 | |
| | | L | : | 6 | |
| Daktype en geometrie | Type | | : | ⦿ Zadeldak | |
| | Knoop | A | : | 45 | |
| | | B | : | 56 | |
| | | C | : | 42 | |
| | | D | : | 57 | |
| | | E | : | 46 | |
| | | F | : | 39 | |
| BG genereren | ☒BG w | | : | BG402 | |
| Stel wind in op een zijde | ⦿ D - E | | | | |
| Maak Last Type | ⦿ Staafbelastingen | | | | |
| Lastverdelingstype | ⦿ Constant | | | | |
| Verwijder invloed van | Enkele Liggers | | : | 1,2,3,4,188,7,201,8, 183,27,195,28,189,34, 35,36,194,38,39,40,41, 42,47,48,49,50,51,52, 53,54,55,56,57,58,59, 60,61,62,63,64,65,66, 67,68,69,70,71,72,74, 76,104,105,108,109, 110,111,120,121,122, 123,124,125,126,127, 128,129,130,131,132, 133,134,135,136,137, 138,139,144,146,147, 148,154,155,156,157, 158,159,160,162,163, 164,165,166,179,180 | |
| Windbelasting wordt gegenereerd op staaf No. | | | : | 5,6,9,10,13,14,17,18, 21,22,25,26,29-33,80, 103,107,140-143,145, 149-153,175-178 | |
| Wandafmetingen | h | | : | 8500 | mm |
| | b | | : | 22100 | mm |
| | d | | : | 19440 | mm |
| | e | | : | 17000 | mm |
| | A | | : | 656901877 | $mm^2$ |
| | $d_A$ | | : | 3400 | mm |
| | $d_B$ | | : | 13600 | mm |
| | $d_C$ | | : | 2440 | mm |

| Gebied | Externe drukcoï¿½fficiï¿½nt $c_{pe,10}$ | Externe Druk $w_e$ [kN/m²] |
|---|---|---|
| A | -1.200 | -0.795 |
| B | -0.800 | -0.530 |
| C | -0.500 | -0.331 |
| D | 0.800 | 0.530 |

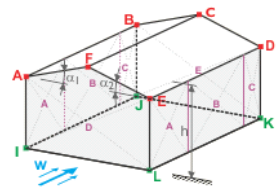
## 3.15 GEGENEREERDE LASTEN — BG402: VB: Wind (-X richting)

| No. | Belastingomschrijving | | | | |
|---|---|---|---|---|---|
| | E | -0.500 | | -0.331 | |
| | Gegenereerde totaalbelastingen | $\Sigma P_{Vlakken}$ | : | 149.48 | kN |
| | | $\Sigma P$ | : | 149.48 | kN |
| | Totale moment bij de oorsprong | $\Sigma M_{Vlakken}$ | : | 1781.03 | kNm |
| | | $\Sigma M$ | : | 1781.02 | kNm |
| | Cellen geselecteerd voor genereren | $\Sigma$ aantal cellen | : | 28 | |
| | | $\Sigma$ cel vlak | : | 1276747749 | $mm^2$ |

**BG403**
VB: Wind (+Y richting)

## 3.15 GEGENEREERDE LASTEN — BG403: VB: Wind (+Y richting)

| No. | Belastingomschrijving | | | | |
|---|---|---|---|---|---|
| 2 | **Van Windbelastingen (Verticale Wanden)** | | | | |




| | | | | | |
|---|---|---|---|---|---|
| Snelheidsdruk | Volgens de norm | | : | EN 1991-1-4 | |
| | Nationale Bijlage | | : | Nederland | |
| | Windgebied | | : | III | |
| | Terrein categorie | | : | Categorie II | |
| | Constructie hoogte | h | : | 8500 | mm |
| | Fundamentele windsnelheid | $v_{b,0}$ | : | 24.5 | m/s |
| Basisgeometrie | Knoop | I | : | 5 | |
| | | J | : | 8 | |
| | | K | : | 7 | |
| | | L | : | 6 | |
| Daktype en geometrie | Type | | : | ⦿ Zadeldak | |
| | Knoop | A | : | 45 | |
| | | B | : | 56 | |
| | | C | : | 42 | |
| | | D | : | 57 | |
| | | E | : | 46 | |
| | | F | : | 39 | |
| BG genereren | ☒BG w | | : | BG403 | |
| Stel wind in op een zijde | ⦿ E - F - A | | | | |
| Maak Last Type | ⦿ Staafbelastingen | | | | |
| Lastverdelingstype | ⦿ Constant | | | | |
| Verwijder invloed van | Enkele Liggers | | : | 1,2,3,4,188,7,201,8, 183,27,195,28,189,34, 35,36,194,38,39,40,41, 42,47,48,49,50,51,52, 53,54,55,56,57,58,59, 60,61,62,63,64,65,66, 67,68,69,70,71,72,74, 76,104,105,108,109, 110,111,120,121,122, 123,124,125,126,127, 128,129,130,131,132, 133,134,135,136,137, 138,139,144,146,147, 148,154,155,156,157, 158,159,160,162,163, 164,165,166,179,180 | |
| Windbelasting wordt gegenereerd op staaf No. | | | : | 5,6,9,10,13,14,17,18, 21,22,25,26,29-33,80, 103,107,140-143,145, 149-153,175-178 | |
| Wandafmetingen | h | | : | 8500 | mm |
| | b | | : | 19440 | mm |
| | d | | : | 22100 | mm |
| | e | | : | 17000 | mm |
| | A | | : | 656901877 | $mm^2$ |
| | $d_A$ | | : | 3400 | mm |
| | $d_B$ | | : | 13600 | mm |
| | $d_C$ | | : | 5100 | mm |

| Gebied | Externe drukcoï¿½fficiï¿½nt $c_{pe,10}$ | Externe Druk $w_e$ [kN/m²] |
|---|---|---|
| A | -1.200 | -0.795 |
| B | -0.800 | -0.530 |
| C | -0.500 | -0.331 |
| D | 0.800 | 0.530 |
| E | -0.500 | -0.331 |

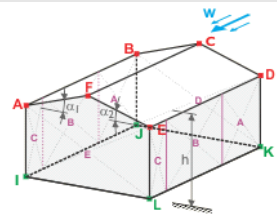
## 3.15 GEGENEREERDE LASTEN — BG403: VB: Wind (+Y richting)

| No. | Belastingomschrijving | | | | |
|---|---|---|---|---|---|
| | Gegenereerde totaalbelastingen | $\Sigma P_{Vlakken}$ | : | 133.52 | kN |
| | | $\Sigma P$ | : | 133.52 | kN |
| | Totale moment bij de oorsprong | $\Sigma M_{Vlakken}$ | : | 1429.44 | kNm |
| | | $\Sigma M$ | : | 1439.36 | kNm |
| | Cellen geselecteerd voor genereren | $\Sigma$ aantal cellen | : | 34 | |
| | | $\Sigma$ cel vlak | : | 1270765923 | $mm^2$ |

**BG404**
VB: Wind (-Y richting)

## 3.15 GEGENEREERDE LASTEN — BG404: VB: Wind (-Y richting)

| No. | Belastingomschrijving | | | | |
|---|---|---|---|---|---|
| 2 | **Van Windbelastingen (Verticale Wanden)** | | | | |




| | | | | | |
|---|---|---|---|---|---|
| Snelheidsdruk | Volgens de norm | | : | EN 1991-1-4 | |
| | Nationale Bijlage | | : | Nederland | |
| | Windgebied | | : | III | |
| | Terrein categorie | | : | Categorie II | |
| | Constructie hoogte | h | : | 8500 | mm |
| | Fundamentele windsnelheid | $v_{b,0}$ | : | 24.5 | m/s |
| Basisgeometrie | Knoop | I | : | 5 | |
| | | J | : | 8 | |
| | | K | : | 7 | |
| | | L | : | 6 | |
| Daktype en geometrie | Type | | : | ⦿ Zadeldak | |
| | Knoop | A | : | 45 | |
| | | B | : | 56 | |
| | | C | : | 42 | |
| | | D | : | 57 | |
| | | E | : | 46 | |
| | | F | : | 39 | |
| BG genereren | ☒BG w | | : | BG404 | |
| Stel wind in op een zijde | ⦿ B - C - D | | | | |
| Maak Last Type | ⦿ Staafbelastingen | | | | |
| Lastverdelingstype | ⦿ Constant | | | | |
| Verwijder invloed van | Enkele Liggers | | : | 1,2,3,4,188,7,201,8, 183,27,195,28,189,34, 35,36,194,38,39,40,41, 42,47,48,49,50,51,52, 53,54,55,56,57,58,59, 60,61,62,63,64,65,66, 67,68,69,70,71,72,74, 76,104,105,108,109, 110,111,120,121,122, 123,124,125,126,127, 128,129,130,131,132, 133,134,135,136,137, 138,139,144,146,147, 148,154,155,156,157, 158,159,160,162,163, 164,165,166,179,180 | |
| Windbelasting wordt gegenereerd op staaf No. | | | : | 5,6,9,10,13,14,17,18, 21,22,25,26,29-33,80, 103,107,140-143,145, 149-153,175-178 | |
| Wandafmetingen | h | | : | 8500 | mm |
| | b | | : | 19440 | mm |
| | d | | : | 22100 | mm |
| | e | | : | 17000 | mm |
| | A | | : | 656901877 | $mm^2$ |
| | $d_A$ | | : | 3400 | mm |
| | $d_B$ | | : | 13600 | mm |
| | $d_C$ | | : | 5100 | mm |

| Gebied | Externe drukcoï¿½fficiï¿½nt $c_{pe,10}$ | Externe Druk $w_e$ [kN/m²] |
|---|---|---|
| A | -1.200 | -0.795 |
| B | -0.800 | -0.530 |
| C | -0.500 | -0.331 |
| D | 0.800 | 0.530 |

## 3.15 GEGENEREERDE LASTEN

BG404: VB: Wind (-Y richting)

| No. | Belastingomschrijving | | | | |
|---|---|---|---|---|---|
| | E | -0.500 | -0.331 | | |
| | Gegenereerde totaalbelastingen | $\Sigma P_{Vlakken}$ | : | 133.52 | kN |
| | | $\Sigma P$ | : | 133.52 | kN |
| | Totale moment bij de oorsprong | $\Sigma M_{Vlakken}$ | : | 1429.44 | kNm |
| | | $\Sigma M$ | : | 1439.36 | kNm |
| | Cellen geselecteerd voor genereren | $\Sigma$ aantal cellen | : | 34 | |
| | | $\Sigma$ cel vlak | : | 1270765907 | $mm^2$ |

## 4.0 RESULTATEN - OPSOMMING

| | Omschrijving | Waarde | Eenh | Opm. |
|---|---|---|---|---|
| Belastingsgeval BG10 - PB: Eigen Gewicht | | | | |
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | -3137.99 | kN | |
| | Som van de steunpuntreacties in Z | -3137.99 | kN | Afwijking 0.00% |
| | Resultante van reacties om x-as | -0.01 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 0.7 | mm | EE-Knoop nr. 2266 (X: 1894, Y: 9000, Z: 7882 mm) |
| | Max. verplaatsing in y-as | -0.6 | mm | Staaf No. 192, x: 1085 mm |
| | Max. verplaatsing in z-as | -19.7 | mm | Staaf No. 116, x: 3957 mm |
| | Max. verplaatsing (vector) | 19.7 | mm | Staaf No. 116, x: 3957 mm |
| | Max. rotatie om x-as | 6.81 | mrad | EE-Knoop nr. 321 (X: 9855, Y: 13500, Z: 8032 mm) |
| | Max. rotatie om y-as | -1.74 | mrad | EE-Knoop nr. 176 (X: 19640, Y: 9000, Z: 7850 mm) |
| | Max. rotatie om z-as | 0.43 | mrad | EE-Knoop nr. 61 (X: 19640, Y: 9000, Z: 7850 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 5 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 2.001E+2596 17 | | |
| | Oneindige Norm | 2.262E+15 | | |
| Belastingsgeval BG20 - PB: Dakbedekking | | | | |
| | Berekening Status : De som van de belastingen en de som van de reactiekrachten in richting X zijn niet in evenwicht (afwijking -66.67%). | | | |
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | -365.18 | kN | |
| | Som van de steunpuntreacties in Z | -365.18 | kN | Afwijking 0.00% |
| | Resultante van reacties om x-as | 4.89 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | -16.11 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | -0.8 | mm | EE-Knoop nr. 199 (X: 13110, Y: 13500, Z: 8093 mm) |
| | Max. verplaatsing in y-as | -0.9 | mm | Staaf No. 192, x: 1085 mm |
| | Max. verplaatsing in z-as | -16.5 | mm | Staaf No. 85, x: 3256 mm |
| | Max. verplaatsing (vector) | 16.5 | mm | Staaf No. 85, x: 3256 mm |
| | Max. rotatie om x-as | 3.34 | mrad | EE-Knoop nr. 282 (X: 13110, Y: 13500, Z: 8093 mm) |
| | Max. rotatie om y-as | -2.57 | mrad | EE-Knoop nr. 176 (X: 19640, Y: 9000, Z: 7850 mm) |
| | Max. rotatie om z-as | 0.64 | mrad | EE-Knoop nr. 61 (X: 19640, Y: 9000, Z: 7850 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 4 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 4.032E+2596 16 | | |
| | Oneindige Norm | 2.262E+15 | | |
| Belastingsgeval BG30 - PB: KSZ - Metselwerk | | | | |
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | -934.65 | kN | |
| | Som van de steunpuntreacties in Z | -934.65 | kN | Afwijking 0.00% |
| | Resultante van reacties om x-as | 12.53 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | -42.01 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 0.3 | mm | EE-Knoop nr. 68 (X: 13110, Y: 13500, Z: 8093 mm) |
| | Max. verplaatsing in y-as | -0.2 | mm | Staaf No. 104, x: 1665 mm |
| | Max. verplaatsing in z-as | -1.7 | mm | EE-Knoop nr. 2 (X: 19840, Y: 0, Z: 0 mm) |
| | Max. verplaatsing (vector) | 1.7 | mm | EE-Knoop nr. 2 (X: 19840, Y: 0, Z: 0 mm) |
| | Max. rotatie om x-as | -0.61 | mrad | EE-Knoop nr. 94 (X: 11445, Y: 22300, Z: 0 mm) |
| | Max. rotatie om y-as | -0.63 | mrad | EE-Knoop nr. 4856 (X: 200, Y: 11000, Z: 0 mm) |
| | Max. rotatie om z-as | 0.10 | mrad | EE-Knoop nr. 224 (X: 19640, Y: 9000, Z: 4345 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 4 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 1.303E+2596 19 | | |
| | Oneindige Norm | 2.262E+15 | | |
| Belastingsgeval BG40 - PB: Sandwichpaneel | | | | |
| | Som van belastingen in X | 0.00 | kN | |

## 4.0 RESULTATEN - OPSOMMING

| | Omschrijving | Waarde | Eenh | Opm. |
|---|---|---|---|---|
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | -134.76 | kN | |
| | Som van de steunpuntreacties in Z | -134.76 | kN | Afwijking 0.00% |
| | Resultante van reacties om x-as | 1.81 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | -4.54 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 0.1 | mm | EE-Knoop nr. 55 (X: 200, Y: 18000, Z: 7850 mm) |
| | Max. verplaatsing in y-as | -0.0 | mm | Staaf No. 104, x: 502 mm |
| | Max. verplaatsing in z-as | -0.3 | mm | EE-Knoop nr. 168 (X: 19640, Y: 200, Z: 7850 mm) |
| | Max. verplaatsing (vector) | 0.3 | mm | EE-Knoop nr. 168 (X: 19640, Y: 200, Z: 7850 mm) |
| | Max. rotatie om x-as | -0.09 | mrad | EE-Knoop nr. 2040 (X: 13294, Y: 21962, Z: 0 mm) |
| | Max. rotatie om y-as | -0.09 | mrad | EE-Knoop nr. 52 (X: 200, Y: 13500, Z: 0 mm) |
| | Max. rotatie om z-as | 0.01 | mrad | EE-Knoop nr. 224 (X: 19640, Y: 9000, Z: 4345 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 6 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 1.454E+2596 19 | | |
| | Oneindige Norm | 2.262E+15 | | |

| Belastingsgeval BG100 - VB: Opgelegde belasting op vloeren 1 | | | | |
|---|---|---|---|---|
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | -412.65 | kN | |
| | Som van de steunpuntreacties in Z | -412.65 | kN | Afwijking 0.00% |
| | Resultante van reacties om x-as | 5.53 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | -36.43 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 0.0 | mm | EE-Knoop nr. 88 (X: 13110, Y: 13500, Z: 4345 mm) |
| | Max. verplaatsing in y-as | 0.0 | mm | Staaf No. 191, x: 2873 mm |
| | Max. verplaatsing in z-as | -0.3 | mm | EE-Knoop nr. 468 (X: 10050, Y: 1524, Z: 0 mm) |
| | Max. verplaatsing (vector) | 0.3 | mm | EE-Knoop nr. 468 (X: 10050, Y: 1524, Z: 0 mm) |
| | Max. rotatie om x-as | 0.09 | mrad | EE-Knoop nr. 83 (X: 6600, Y: 13500, Z: 7970 mm) |
| | Max. rotatie om y-as | 0.09 | mrad | EE-Knoop nr. 1175 (X: 1011, Y: 11000, Z: 0 mm) |
| | Max. rotatie om z-as | 0.01 | mrad | EE-Knoop nr. 226 (X: 19640, Y: 13500, Z: 4345 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 3 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 3.706E+2596 19 | | |
| | Oneindige Norm | 2.262E+15 | | |

| Belastingsgeval BG110 - VB: Opgelegde belasting op vloeren 2 | | | | |
|---|---|---|---|---|
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | -404.19 | kN | |
| | Som van de steunpuntreacties in Z | -404.19 | kN | Afwijking 0.00% |
| | Resultante van reacties om x-as | 5.42 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | -24.31 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 0.0 | mm | EE-Knoop nr. 88 (X: 13110, Y: 13500, Z: 4345 mm) |
| | Max. verplaatsing in y-as | -0.0 | mm | EE-Knoop nr. 247 (X: 19640, Y: 18000, Z: 7850 mm) |
| | Max. verplaatsing in z-as | -0.3 | mm | EE-Knoop nr. 1546 (X: 16368, Y: 15500, Z: 0 mm) |
| | Max. verplaatsing (vector) | 0.3 | mm | EE-Knoop nr. 1546 (X: 16368, Y: 15500, Z: 0 mm) |
| | Max. rotatie om x-as | -0.08 | mrad | EE-Knoop nr. 699 (X: 10039, Y: 4501, Z: 0 mm) |
| | Max. rotatie om y-as | 0.07 | mrad | EE-Knoop nr. 835 (X: 1523, Y: 6499, Z: 0 mm) |
| | Max. rotatie om z-as | 0.01 | mrad | EE-Knoop nr. 61 (X: 19640, Y: 9000, Z: 7850 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 5 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 2.723E+2596 22 | | |
| | Oneindige Norm | 2.262E+15 | | |

| Belastingsgeval BG120 - VB: Dakbelasting | | | | |
|---|---|---|---|---|
| | Berekening Status : | | | |
| | De som van de belastingen en de som van de reactiekrachten in richting X zijn niet in evenwicht (afwijking 4.76%). | | | |
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | 0.00 | kN | |

## 4.0 RESULTATEN - OPSOMMING

| | Omschrijving | Waarde | Eenh | Opm. |
|---|---|---|---|---|
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | -429.62 | kN | |
| | Som van de steunpuntreacties in Z | -429.62 | kN | Afwijking 0.00% |
| | Resultante van reacties om x-as | 5.76 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | -18.95 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | -0.9 | mm | EE-Knoop nr. 199 (X: 13110, Y: 13500, Z: 8093 mm) |
| | Max. verplaatsing in y-as | -1.0 | mm | Staaf No. 192, x: 1085 mm |
| | Max. verplaatsing in z-as | -19.4 | mm | Staaf No. 85, x: 3256 mm |
| | Max. verplaatsing (vector) | 19.4 | mm | Staaf No. 85, x: 3256 mm |
| | Max. rotatie om x-as | 3.93 | mrad | EE-Knoop nr. 282 (X: 13110, Y: 13500, Z: 8093 mm) |
| | Max. rotatie om y-as | -3.03 | mrad | EE-Knoop nr. 176 (X: 19640, Y: 9000, Z: 7850 mm) |
| | Max. rotatie om z-as | 0.76 | mrad | EE-Knoop nr. 61 (X: 19640, Y: 9000, Z: 7850 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 4 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 4.032E+259616 | | |
| | Oneindige Norm | 2.262E+15 | | |

| Belastingsgeval BG130 - VB: Zonnepanelen | | | | |
|---|---|---|---|---|
| | Berekening Status :<br>De som van de belastingen en de som van de reactiekrachten in richting X zijn niet in evenwicht (afwijking -30.77%). | | | |
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | -214.81 | kN | |
| | Som van de steunpuntreacties in Z | -214.81 | kN | Afwijking 0.00% |
| | Resultante van reacties om x-as | 2.88 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | -9.47 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | -0.5 | mm | EE-Knoop nr. 199 (X: 13110, Y: 13500, Z: 8093 mm) |
| | Max. verplaatsing in y-as | -0.5 | mm | Staaf No. 192, x: 1085 mm |
| | Max. verplaatsing in z-as | -9.7 | mm | Staaf No. 85, x: 3256 mm |
| | Max. verplaatsing (vector) | 9.7 | mm | Staaf No. 85, x: 3256 mm |
| | Max. rotatie om x-as | 1.96 | mrad | EE-Knoop nr. 282 (X: 13110, Y: 13500, Z: 8093 mm) |
| | Max. rotatie om y-as | -1.51 | mrad | EE-Knoop nr. 176 (X: 19640, Y: 9000, Z: 7850 mm) |
| | Max. rotatie om z-as | 0.38 | mrad | EE-Knoop nr. 61 (X: 19640, Y: 9000, Z: 7850 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 4 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 4.032E+259616 | | |
| | Oneindige Norm | 2.262E+15 | | |

| Belastingsgeval BG140 - VB: Stellingen - Pallet | | | | |
|---|---|---|---|---|
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | -4729.35 | kN | |
| | Som van de steunpuntreacties in Z | -4729.35 | kN | Afwijking 0.00% |
| | Resultante van reacties om x-as | 164.07 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | 4.48 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | -0.5 | mm | EE-Knoop nr. 96 (X: 14775, Y: 13500, Z: 4345 mm) |
| | Max. verplaatsing in y-as | 0.1 | mm | Staaf No. 3, x: 6530 mm |
| | Max. verplaatsing in z-as | -2.7 | mm | EE-Knoop nr. 43 (X: 13110, Y: 18000, Z: 0 mm) |
| | Max. verplaatsing (vector) | 2.7 | mm | EE-Knoop nr. 3677 (X: 13110, Y: 18000, Z: 4740 mm) |
| | Max. rotatie om x-as | 0.71 | mrad | EE-Knoop nr. 109 (X: 13110, Y: 9000, Z: 0 mm) |
| | Max. rotatie om y-as | 0.78 | mrad | EE-Knoop nr. 1212 (X: 19368, Y: 11000, Z: 0 mm) |
| | Max. rotatie om z-as | -0.12 | mrad | EE-Knoop nr. 270 (X: 13110, Y: 13500, Z: 4345 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 4 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 1.308E+259624 | | |
| | Oneindige Norm | 2.262E+15 | | |

| Belastingsgeval BG150 - VB: Heftruck | | | | |
|---|---|---|---|---|
| | Som van belastingen in X | 24.00 | kN | |
| | Som van de steunpuntreacties in X | 24.00 | kN | Afwijking 0.00% |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | -112.00 | kN | |

## 4.0 RESULTATEN - OPSOMMING

| | Omschrijving | Waarde | Eenh | Opm. |
|---|---|---|---|---|
| | Som van de steunpuntreacties in Z | -112.00 | kN | Afwijking 0.00% |
| | Resultante van reacties om x-as | 1.50 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | -108.82 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.32 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 0.1 | mm | EE-Knoop nr. 1187 (X: 7092, Y: 10972, Z: 0 mm) |
| | Max. verplaatsing in y-as | -0.0 | mm | EE-Knoop nr. 1345 (X: 9091, Y: 13082, Z: 0 mm) |
| | Max. verplaatsing in z-as | -0.7 | mm | EE-Knoop nr. 1191 (X: 9108, Y: 10946, Z: 0 mm) |
| | Max. verplaatsing (vector) | 0.7 | mm | EE-Knoop nr. 1191 (X: 9108, Y: 10946, Z: 0 mm) |
| | Max. rotatie om x-as | 0.23 | mrad | EE-Knoop nr. 1345 (X: 9091, Y: 13082, Z: 0 mm) |
| | Max. rotatie om y-as | -0.23 | mrad | EE-Knoop nr. 1234 (X: 11090, Y: 11528, Z: 0 mm) |
| | Max. rotatie om z-as | 0.02 | mrad | EE-Knoop nr. 61 (X: 19640, Y: 9000, Z: 7850 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 3 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 4.096E+2596 18 | | |
| | Oneindige Norm | 2.262E+15 | | |

Belastingsgeval BG300 - VB: Sneeuw

Berekening Status :
De som van de belastingen en de som van de reactiekrachten in richting X zijn niet in evenwicht (afwijking 100.00%).

| | Omschrijving | Waarde | Eenh | Opm. |
|---|---|---|---|---|
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | -601.47 | kN | |
| | Som van de steunpuntreacties in Z | -601.47 | kN | Afwijking 0.00% |
| | Resultante van reacties om x-as | 8.06 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | -26.53 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | -1.3 | mm | EE-Knoop nr. 199 (X: 13110, Y: 13500, Z: 8093 mm) |
| | Max. verplaatsing in y-as | -1.4 | mm | Staaf No. 192, x: 1085 mm |
| | Max. verplaatsing in z-as | -27.1 | mm | Staaf No. 85, x: 3256 mm |
| | Max. verplaatsing (vector) | 27.2 | mm | Staaf No. 85, x: 3256 mm |
| | Max. rotatie om x-as | 5.50 | mrad | EE-Knoop nr. 282 (X: 13110, Y: 13500, Z: 8093 mm) |
| | Max. rotatie om y-as | -4.24 | mrad | EE-Knoop nr. 176 (X: 19640, Y: 9000, Z: 7850 mm) |
| | Max. rotatie om z-as | 1.06 | mrad | EE-Knoop nr. 61 (X: 19640, Y: 9000, Z: 7850 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 4 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 4.032E+2596 16 | | |
| | Oneindige Norm | 2.262E+15 | | |

Belastingsgeval BG401 - VB: Wind (+X richting)

Berekening Status :
De som van de belastingen en de som van de reactiekrachten in richting Z zijn niet in evenwicht (afwijking 146.15%).

| | Omschrijving | Waarde | Eenh | Opm. |
|---|---|---|---|---|
| | Som van belastingen in X | 149.48 | kN | |
| | Som van de steunpuntreacties in X | 149.48 | kN | Afwijking 0.00% |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | 0.00 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | 508.79 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 2.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 4.8 | mm | EE-Knoop nr. 3834 (X: 200, Y: 9000, Z: 4929 mm) |
| | Max. verplaatsing in y-as | -4.9 | mm | EE-Knoop nr. 2575 (X: 13110, Y: 200, Z: 4148 mm) |
| | Max. verplaatsing in z-as | -0.6 | mm | EE-Knoop nr. 3427 (X: 16526, Y: 13500, Z: 4345 mm) |
| | Max. verplaatsing (vector) | 5.3 | mm | EE-Knoop nr. 70 (X: 13110, Y: 200, Z: 4345 mm) |
| | Max. rotatie om x-as | 3.71 | mrad | EE-Knoop nr. 86 (X: 13110, Y: 9000, Z: 8093 mm) |
| | Max. rotatie om y-as | 1.52 | mrad | EE-Knoop nr. 173 (X: 200, Y: 9000, Z: 0 mm) |
| | Max. rotatie om z-as | -1.73 | mrad | EE-Knoop nr. 61 (X: 19640, Y: 9000, Z: 7850 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 5 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 2.221E+2596 27 | | |
| | Oneindige Norm | 2.262E+15 | | |

Belastingsgeval BG402 - VB: Wind (-X richting)

Berekening Status :
De som van de belastingen en de som van de reactiekrachten in richting Z zijn niet in evenwicht (afwijking 966.67%).

| | Omschrijving | Waarde | Eenh | Opm. |
|---|---|---|---|---|
| | Som van belastingen in X | -149.48 | kN | |
| | Som van de steunpuntreacties in X | -149.48 | kN | Afwijking 0.00% |
| | Som van belastingen in Y | 0.00 | kN | |

## 4.0 RESULTATEN - OPSOMMING

| | Omschrijving | Waarde | Eenh | Opm. |
|---|---|---|---|---|
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | 0.00 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | -508.78 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | -2.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | -4.9 | mm | EE-Knoop nr. 4062 (X: 19640, Y: 18000, Z: 4734 mm) |
| | Max. verplaatsing in y-as | -5.2 | mm | EE-Knoop nr. 2574 (X: 13110, Y: 200, Z: 3950 mm) |
| | Max. verplaatsing in z-as | 0.5 | mm | EE-Knoop nr. 3427 (X: 16526, Y: 13500, Z: 4345 mm) |
| | Max. verplaatsing (vector) | 5.6 | mm | Staaf No. 30, x: 4148 mm |
| | Max. rotatie om x-as | -2.26 | mrad | EE-Knoop nr. 156 (X: 9855, Y: 200, Z: 8032 mm) |
| | Max. rotatie om y-as | -1.56 | mrad | EE-Knoop nr. 182 (X: 19640, Y: 18000, Z: 0 mm) |
| | Max. rotatie om z-as | 0.76 | mrad | Staaf No. 49, x: 3265 mm |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 5 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 5.799E+2596 26 | | |
| | Oneindige Norm | 2.262E+15 | | |
| Belastingsgeval BG403 - VB: Wind (+Y richting) | | | | |
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | 133.52 | kN | |
| | Som van de steunpuntreacties in Y | 133.52 | kN | Afwijking 0.00% |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | -462.62 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | -0.02 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 6.86 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 3.2 | mm | EE-Knoop nr. 2173 (X: 19640, Y: 4500, Z: 3753 mm) |
| | Max. verplaatsing in y-as | 6.9 | mm | EE-Knoop nr. 3937 (X: 13110, Y: 200, Z: 4542 mm) |
| | Max. verplaatsing in z-as | -0.3 | mm | Staaf No. 119, x: 0 mm |
| | Max. verplaatsing (vector) | 6.9 | mm | EE-Knoop nr. 3937 (X: 13110, Y: 200, Z: 4542 mm) |
| | Max. rotatie om x-as | -5.53 | mrad | EE-Knoop nr. 84 (X: 6600, Y: 18000, Z: 7970 mm) |
| | Max. rotatie om y-as | 1.48 | mrad | EE-Knoop nr. 49 (X: 200, Y: 4500, Z: 7850 mm) |
| | Max. rotatie om z-as | 1.43 | mrad | EE-Knoop nr. 61 (X: 19640, Y: 9000, Z: 7850 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 4 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 4.918E+2596 18 | | |
| | Oneindige Norm | 2.262E+15 | | |
| Belastingsgeval BG404 - VB: Wind (-Y richting) | | | | |
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | -133.52 | kN | |
| | Som van de steunpuntreacties in Y | -133.52 | kN | Afwijking 0.00% |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | 462.62 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | -0.02 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | -6.86 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 3.3 | mm | EE-Knoop nr. 2414 (X: 19640, Y: 18000, Z: 3950 mm) |
| | Max. verplaatsing in y-as | -6.6 | mm | EE-Knoop nr. 3797 (X: 6600, Y: 22300, Z: 4536 mm) |
| | Max. verplaatsing in z-as | -0.5 | mm | EE-Knoop nr. 3533 (X: 11770, Y: 4500, Z: 8068 mm) |
| | Max. verplaatsing (vector) | 6.6 | mm | EE-Knoop nr. 3797 (X: 6600, Y: 22300, Z: 4536 mm) |
| | Max. rotatie om x-as | 6.34 | mrad | EE-Knoop nr. 83 (X: 6600, Y: 13500, Z: 7970 mm) |
| | Max. rotatie om y-as | 1.52 | mrad | EE-Knoop nr. 55 (X: 200, Y: 18000, Z: 7850 mm) |
| | Max. rotatie om z-as | -0.85 | mrad | EE-Knoop nr. 37 (X: 19640, Y: 4500, Z: 7850 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 6 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 8.484E+2596 21 | | |
| | Oneindige Norm | 2.262E+15 | | |
| Belastingsgeval BG800 - DBG1 - Eigenvorm 1, richting - X | | | | |
| | Som van belastingen in X | -1534.94 | kN | |
| | Som van de steunpuntreacties in X | -1534.94 | kN | Afwijking 0.00% |
| | Som van belastingen in Y | -123.10 | kN | |
| | Som van de steunpuntreacties in Y | -123.10 | kN | Afwijking 0.00% |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | 307.55 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |

## 4.0 RESULTATEN - OPSOMMING

| | Omschrijving | Waarde | Eenh | Opm. |
|---|---|---|---|---|
| | Resultante van reacties om y-as | -3833.78 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | -2853.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | -33.7 | mm | EE-Knoop nr. 3238 (X: 19640, Y: 6065, Z: 7850 mm) |
| | Max. verplaatsing in y-as | -9.0 | mm | Staaf No. 199, x: 2178 mm |
| | Max. verplaatsing in z-as | 3.4 | mm | EE-Knoop nr. 3357 (X: 18278, Y: 22300, Z: 4345 mm) |
| | Max. verplaatsing (vector) | 33.9 | mm | EE-Knoop nr. 3238 (X: 19640, Y: 6065, Z: 7850 mm) |
| | Max. rotatie om x-as | -16.87 | mrad | EE-Knoop nr. 86 (X: 13110, Y: 9000, Z: 8093 mm) |
| | Max. rotatie om y-as | -7.79 | mrad | EE-Knoop nr. 3241 (X: 19640, Y: 6652, Z: 7850 mm) |
| | Max. rotatie om z-as | 8.00 | mrad | EE-Knoop nr. 61 (X: 19640, Y: 9000, Z: 7850 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 4 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 6.208E+2596 23 | | |
| | Oneindige Norm | 2.262E+15 | | |

| Belastingsgeval BG801 - DBG1 - Eigenvorm 1, richting - Y | | | | |
|---|---|---|---|---|
| | Som van belastingen in X | -123.10 | kN | |
| | Som van de steunpuntreacties in X | -123.10 | kN | Afwijking 0.00% |
| | Som van belastingen in Y | -9.87 | kN | |
| | Som van de steunpuntreacties in Y | -9.87 | kN | Afwijking 0.00% |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | 24.69 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | -307.45 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | -228.80 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | -2.7 | mm | EE-Knoop nr. 3238 (X: 19640, Y: 6065, Z: 7850 mm) |
| | Max. verplaatsing in y-as | -0.7 | mm | Staaf No. 199, x: 2178 mm |
| | Max. verplaatsing in z-as | 0.3 | mm | EE-Knoop nr. 3357 (X: 18278, Y: 22300, Z: 4345 mm) |
| | Max. verplaatsing (vector) | 2.7 | mm | EE-Knoop nr. 3238 (X: 19640, Y: 6065, Z: 7850 mm) |
| | Max. rotatie om x-as | -1.35 | mrad | EE-Knoop nr. 86 (X: 13110, Y: 9000, Z: 8093 mm) |
| | Max. rotatie om y-as | -0.62 | mrad | EE-Knoop nr. 3241 (X: 19640, Y: 6652, Z: 7850 mm) |
| | Max. rotatie om z-as | 0.64 | mrad | EE-Knoop nr. 61 (X: 19640, Y: 9000, Z: 7850 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 4 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 6.208E+2596 23 | | |
| | Oneindige Norm | 2.262E+15 | | |

| Belastingsgeval BG802 - DBG1 - Eigenvorm 2, richting - X | | | | |
|---|---|---|---|---|
| | Som van belastingen in X | -7.93 | kN | |
| | Som van de steunpuntreacties in X | -7.93 | kN | Afwijking 0.00% |
| | Som van belastingen in Y | 120.80 | kN | |
| | Som van de steunpuntreacties in Y | 120.80 | kN | Afwijking 0.00% |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | -262.93 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | -17.00 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | -122.18 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | -0.4 | mm | EE-Knoop nr. 3886 (X: 200, Y: 4500, Z: 4734 mm) |
| | Max. verplaatsing in y-as | 2.4 | mm | EE-Knoop nr. 4153 (X: 5282, Y: 18000, Z: 7945 mm) |
| | Max. verplaatsing in z-as | 0.3 | mm | EE-Knoop nr. 3539 (X: 10621, Y: 4500, Z: 8046 mm) |
| | Max. verplaatsing (vector) | 2.4 | mm | EE-Knoop nr. 4153 (X: 5282, Y: 18000, Z: 7945 mm) |
| | Max. rotatie om x-as | -5.35 | mrad | EE-Knoop nr. 4154 (X: 5471, Y: 18000, Z: 7949 mm) |
| | Max. rotatie om y-as | -0.25 | mrad | EE-Knoop nr. 37 (X: 19640, Y: 4500, Z: 7850 mm) |
| | Max. rotatie om z-as | 1.23 | mrad | EE-Knoop nr. 61 (X: 19640, Y: 9000, Z: 7850 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 5 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 3.193E+2596 23 | | |
| | Oneindige Norm | 2.262E+15 | | |

| Belastingsgeval BG803 - DBG1 - Eigenvorm 2, richting - Y | | | | |
|---|---|---|---|---|
| | Som van belastingen in X | 120.80 | kN | |
| | Som van de steunpuntreacties in X | 120.80 | kN | Afwijking 0.00% |
| | Som van belastingen in Y | -1838.98 | kN | |
| | Som van de steunpuntreacties in Y | -1838.98 | kN | Afwijking 0.00% |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | 4002.67 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | 259.04 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 1860.04 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 6.1 | mm | EE-Knoop nr. 4044 (X: 19640, Y: 9000, Z: 4540 mm) |
| | Max. verplaatsing in y-as | -36.7 | mm | EE-Knoop nr. 4265 (X: 7940, Y: 13500, Z: 7995 mm) |

## ■ 4.0 RESULTATEN - OPSOMMING

| | Omschrijving | Waarde | Eenh | Opm. |
|---|---|---|---|---|
| | Max. verplaatsing in z-as | -4.1 | mm | Staaf No. 118, x: 0 mm |
| | Max. verplaatsing (vector) | 36.8 | mm | EE-Knoop nr. 4265 (X: 7940, Y: 13500, Z: 7995 mm) |
| | Max. rotatie om x-as | 84.47 | mrad | EE-Knoop nr. 4170 (X: 5471, Y: 13500, Z: 7949 mm) |
| | Max. rotatie om y-as | 3.77 | mrad | EE-Knoop nr. 51 (X: 200, Y: 9000, Z: 7850 mm) |
| | Max. rotatie om z-as | -15.59 | mrad | EE-Knoop nr. 37 (X: 19640, Y: 4500, Z: 7850 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 7 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 4.431E+2596 21 | | |
| | Oneindige Norm | 2.262E+15 | | |
| Belastingsgeval BG804 - DBG1 - Eigenvorm 4, richting - X | | | | |
| | Som van belastingen in X | -1459.27 | kN | |
| | Som van de steunpuntreacties in X | -1459.27 | kN | Afwijking 0.00% |
| | Som van belastingen in Y | -98.77 | kN | |
| | Som van de steunpuntreacties in Y | -98.77 | kN | Afwijking 0.00% |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | -226.87 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | 3272.79 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | -832.63 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 14.1 | mm | EE-Knoop nr. 3133 (X: 200, Y: 6652, Z: 7850 mm) |
| | Max. verplaatsing in y-as | 3.5 | mm | Staaf No. 85, x: 958 mm |
| | Max. verplaatsing in z-as | -2.3 | mm | EE-Knoop nr. 3427 (X: 16526, Y: 13500, Z: 4345 mm) |
| | Max. verplaatsing (vector) | 14.1 | mm | EE-Knoop nr. 3133 (X: 200, Y: 6652, Z: 7850 mm) |
| | Max. rotatie om x-as | -8.57 | mrad | EE-Knoop nr. 4294 (X: 8515, Y: 4500, Z: 8006 mm) |
| | Max. rotatie om y-as | 5.12 | mrad | EE-Knoop nr. 3133 (X: 200, Y: 6652, Z: 7850 mm) |
| | Max. rotatie om z-as | 3.40 | mrad | EE-Knoop nr. 37 (X: 19640, Y: 4500, Z: 7850 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 5 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 1.847E+2596 23 | | |
| | Oneindige Norm | 2.262E+15 | | |
| Belastingsgeval BG805 - DBG1 - Eigenvorm 4, richting - Y | | | | |
| | Som van belastingen in X | -98.77 | kN | |
| | Som van de steunpuntreacties in X | -98.77 | kN | Afwijking 0.00% |
| | Som van belastingen in Y | -6.68 | kN | |
| | Som van de steunpuntreacties in Y | -6.68 | kN | Afwijking 0.00% |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | -15.36 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | 221.51 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | -56.35 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 1.0 | mm | EE-Knoop nr. 3133 (X: 200, Y: 6652, Z: 7850 mm) |
| | Max. verplaatsing in y-as | 0.2 | mm | Staaf No. 85, x: 958 mm |
| | Max. verplaatsing in z-as | -0.2 | mm | EE-Knoop nr. 3427 (X: 16526, Y: 13500, Z: 4345 mm) |
| | Max. verplaatsing (vector) | 1.0 | mm | EE-Knoop nr. 3133 (X: 200, Y: 6652, Z: 7850 mm) |
| | Max. rotatie om x-as | -0.58 | mrad | EE-Knoop nr. 4294 (X: 8515, Y: 4500, Z: 8006 mm) |
| | Max. rotatie om y-as | 0.35 | mrad | EE-Knoop nr. 3133 (X: 200, Y: 6652, Z: 7850 mm) |
| | Max. rotatie om z-as | 0.23 | mrad | EE-Knoop nr. 37 (X: 19640, Y: 4500, Z: 7850 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 4 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 1.847E+2596 23 | | |
| | Oneindige Norm | 2.262E+15 | | |
| Belastingsgeval BG806 - DBG1 - Eigenvorm 5, richting - X | | | | |
| | Som van belastingen in X | -4.71 | kN | |
| | Som van de steunpuntreacties in X | -4.71 | kN | Afwijking 0.00% |
| | Som van belastingen in Y | 76.15 | kN | |
| | Som van de steunpuntreacties in Y | 76.15 | kN | Afwijking -0.00% |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | 198.00 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | 11.92 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | -29.52 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 0.2 | mm | EE-Knoop nr. 4044 (X: 19640, Y: 9000, Z: 4540 mm) |
| | Max. verplaatsing in y-as | -1.0 | mm | EE-Knoop nr. 4264 (X: 8132, Y: 13500, Z: 7999 mm) |
| | Max. verplaatsing in z-as | -0.1 | mm | Staaf No. 118, x: 0 mm |
| | Max. verplaatsing (vector) | 1.0 | mm | EE-Knoop nr. 4264 (X: 8132, Y: 13500, Z: 7999 mm) |
| | Max. rotatie om x-as | 3.39 | mrad | EE-Knoop nr. 4266 (X: 7749, Y: 13500, Z: 7992 mm) |
| | Max. rotatie om y-as | 0.14 | mrad | EE-Knoop nr. 51 (X: 200, Y: 9000, Z: 7850 mm) |

## 4.0 RESULTATEN - OPSOMMING

| | Omschrijving | Waarde | Eenh | Opm. |
|---|---|---|---|---|
| | Max. rotatie om z-as | -0.56 | mrad | EE-Knoop nr. 37 (X: 19640, Y: 4500, Z: 7850 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 6 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 1.678E+2596 24 | | |
| | Oneindige Norm | 2.262E+15 | | |
| Belastingsgeval BG807 - DBG1 - Eigenvorm 5, richting - Y | | | | |
| | Som van belastingen in X | 76.15 | kN | |
| | Som van de steunpuntreacties in X | 76.15 | kN | Afwijking 0.00% |
| | Som van belastingen in Y | -1231.80 | kN | |
| | Som van de steunpuntreacties in Y | -1231.80 | kN | Afwijking 0.00% |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | -3202.98 | kNm | Bij zwaartepunt van de Constructie (X:9964.95, Y:11263.40, Z:621.12 mm) |
| | Resultante van reacties om y-as | -192.85 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 477.47 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | -3.0 | mm | EE-Knoop nr. 3886 (X: 200, Y: 4500, Z: 4734 mm) |
| | Max. verplaatsing in y-as | 16.1 | mm | EE-Knoop nr. 4249 (X: 7940, Y: 18000, Z: 7995 mm) |
| | Max. verplaatsing in z-as | 2.8 | mm | EE-Knoop nr. 3539 (X: 10621, Y: 4500, Z: 8046 mm) |
| | Max. verplaatsing (vector) | 16.2 | mm | EE-Knoop nr. 4249 (X: 7940, Y: 18000, Z: 7995 mm) |
| | Max. rotatie om x-as | -53.15 | mrad | EE-Knoop nr. 4250 (X: 7749, Y: 18000, Z: 7992 mm) |
| | Max. rotatie om y-as | -2.22 | mrad | EE-Knoop nr. 37 (X: 19640, Y: 4500, Z: 7850 mm) |
| | Max. rotatie om z-as | 11.07 | mrad | EE-Knoop nr. 61 (X: 19640, Y: 9000, Z: 7850 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 5 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 9.769E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 1.203E+05 | | |
| | Stijfheidsmatrix determinant | 4.104E+2596 25 | | |
| | Oneindige Norm | 2.262E+15 | | |
| Samenvatting | | | | |
| | Berekening Status: Probleem In BG20, BG120, BG130, BG300, BG401, BG402 | | | |
| | Max. verplaatsing in x-as | -33.7 | mm | BG800, EE-Knoop nr. 3238 (X: 19640, Y: 6065, Z: 7850 mm) |
| | Max. verplaatsing in y-as | -36.7 | mm | BG803, EE-Knoop nr. 4265 (X: 7940, Y: 13500, Z: 7995 mm) |
| | Max. verplaatsing in z-as | -27.1 | mm | BG300, Staaf No. 85, x: 3256 mm |
| | Max. verplaatsing (vector) | 36.8 | mm | BG803, EE-Knoop nr. 4265 (X: 7940, Y: 13500, Z: 7995 mm) |
| | Max. rotatie om x-as | 84.47 | mrad | BG803, EE-Knoop nr. 4170 (X: 5471, Y: 13500, Z: 7949 mm) |
| | Max. rotatie om y-as | -7.79 | mrad | BG800, EE-Knoop nr. 3241 (X: 19640, Y: 6652, Z: 7850 mm) |
| | Max. rotatie om z-as | -15.59 | mrad | BG803, EE-Knoop nr. 37 (X: 19640, Y: 4500, Z: 7850 mm) |
| | Andere instellingen: | | | |
| | Aantal 1D Eindige Elementen | 3176 | | |
| | Aantal 2D Eindige Elementen | 1993 | | |
| | Aantal 3D Eindige Elementen | 0 | | |
| | Aantal EE-netknopen | 4913 | | |
| | Aantal vergelijkingen | 29478 | | |
| | Max. aantal iteraties | 100 | | |
| | Aantal doorsnedes voor staafresultaten | 10 | | |
| | Verdeling van kabels/fundatie/verlopende staven | 10 | | |
| | Aantal staafverdelingen voor het zoeken naar max. waardes | 10 | | |
| | Onderverdelingen van EE-net voor grafische weergave resultaten | 0 | | |
| | Percentage van iteraties volgens de Picard-methode in combinatie met de Newton-Raphson methode | 5 | % | |
| | Zet Bezweken Staven AAN | ☒ | | |
| | Opties: | | | |
| | Afschuifstijfheid activeren voor Staven (Ay, Az) | ☐ | | |
| | Activeren van staafverdelingen voor grote vervorming of post-kritische berekening | ☒ | | |
| | Activeer ingevoerde stijfheidsmodificaties | ☒ | | |
| | Negeer rotatievrijheidsgraden | ☐ | | |
| | Controle van de kritische staafkrachten | ☐ | | |
| | Niet-symmetrische direct Solver als geï¿½ist door niet-lineair model | ☒ | | |
| | Oplossingsmethode voor de vergelijkingen | Direct | | |
| | Plaat-buigtheorie | Mindlin | | |
| | Solverversie | 64-bit | | |
| | Precisie en Tolerantie: | | | |
| | Wijzig standaardinstelling | ☐ | | |
| | Niet-lineaire effecten - Activeren: | | | |
| | Bezwijkende staven t.g.v. staaftype | ☒ | | |
| | Re-activeren van bezwijkende staven: | | | |
| | Controleer vervorming van bezwijkende staven en re-activeer indien van toepassing. | ☒ | | |

## 4.0 RESULTATEN - OPSOMMING

| | | | |
|---|---|---|---|
| | Max. aantal van re-activeringen | 5 | |
| | Aanvullende instellingen:<br>Bezwijkende staven weer gebruiken met gereduceerde stijfheid | | |
| | Reductiefactor voor Stijfheid | 100 | |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf | | Knoop | Snede | | Krachten [kN] | | | Momenten [kNm] | | | Bijbehorend |
|---|---|---|---|---|---|---|---|---|---|---|---|
| No. | RC | No. | x [mm] | | N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Belastingsgevallen |
| 1 | RC1 | 5 | 0 | Max N | -27.68 | -17.14 | -16.67 | 26.49 | -25.00 | 2.49 | BC 362 |
| | | | | Min N | -81.23 | -35.91 | -91.18 | 72.46 | -64.51 | 6.54 | BC 155 |
| | | | | Max $V_y$ | -37.43 | -16.04 | -50.55 | 33.46 | -28.23 | 2.85 | BC 380 |
| | | | | Min $V_y$ | -74.95 | -37.10 | -65.43 | 63.38 | -58.53 | 5.99 | BC 156 |
| | | | | Max $V_z$ | -27.70 | -17.16 | -16.63 | 26.51 | -25.03 | 2.49 | BC 390 |
| | | | | Min $V_z$ | -81.21 | -35.89 | -91.22 | 72.43 | -64.48 | 6.53 | BC 154 |
| | | | | Max $M_T$ | -81.23 | -35.91 | -91.18 | 72.46 | -64.51 | 6.54 | BC 155 |
| | | | | Min $M_T$ | -31.30 | -17.02 | -25.88 | 24.56 | -22.31 | 2.31 | BC 360 |
| | | | | Max $M_y$ | -31.30 | -17.02 | -25.88 | 24.56 | -22.31 | 2.31 | BC 360 |
| | | | | Min $M_y$ | -81.23 | -35.91 | -91.18 | 72.46 | -64.51 | 6.54 | BC 155 |
| | | | | Max $M_z$ | -81.23 | -35.91 | -91.18 | 72.46 | -64.51 | 6.54 | BC 155 |
| | | | | Min $M_z$ | -31.30 | -17.02 | -25.88 | 24.56 | -22.31 | 2.31 | BC 360 |
| | | | 1450 | Max N | -89.47 | -5.24 | -8.07 | 24.20 | -26.17 | 4.88 | BC 390 |
| | | | | Min N | -331.58 | -31.49 | -76.48 | 62.81 | -115.33 | 16.04 | BC 154 |
| | | | | Max $V_y$ | -98.85 | -4.50 | -6.84 | 30.15 | -29.87 | 5.53 | BC 389 |
| | | | | Min $V_y$ | -331.58 | -31.49 | -76.48 | 62.81 | -115.33 | 16.04 | BC 154 |
| | | | | Max $V_z$ | -100.30 | -4.66 | -6.75 | 30.05 | -30.30 | 5.59 | BC 417 |
| | | | | Min $V_z$ | -330.15 | -31.32 | -76.55 | 62.93 | -114.90 | 15.98 | BC 147 |
| | | | | Max $M_T$ | -330.16 | -31.32 | -76.54 | 62.97 | -114.93 | 15.98 | BC 148 |
| | | | | Min $M_T$ | -109.76 | -7.89 | -16.81 | 20.92 | -31.56 | 5.22 | BC 356 |
| | | | | Max $M_y$ | -89.47 | -5.24 | -8.07 | 24.20 | -26.17 | 4.88 | BC 390 |
| | | | | Min $M_y$ | -331.58 | -31.49 | -76.48 | 62.81 | -115.33 | 16.04 | BC 154 |
| | | | | Max $M_z$ | -331.58 | -31.49 | -76.48 | 62.81 | -115.33 | 16.04 | BC 154 |
| | | | | Min $M_z$ | -89.47 | -5.24 | -8.07 | 24.20 | -26.17 | 4.88 | BC 390 |
| | | | 1450 | Max N | -89.47 | -5.24 | -8.07 | 24.20 | -26.17 | 4.88 | BC 390 |
| | | | | Min N | -331.58 | -31.49 | -76.48 | 62.81 | -115.33 | 16.04 | BC 154 |
| | | | | Max $V_y$ | -98.85 | -4.50 | -6.84 | 30.15 | -29.87 | 5.53 | BC 389 |
| | | | | Min $V_y$ | -331.58 | -31.49 | -76.48 | 62.81 | -115.33 | 16.04 | BC 154 |
| | | | | Max $V_z$ | -100.30 | -4.66 | -6.75 | 30.05 | -30.30 | 5.59 | BC 417 |
| | | | | Min $V_z$ | -330.15 | -31.32 | -76.55 | 62.93 | -114.90 | 15.98 | BC 147 |
| | | | | Max $M_T$ | -330.16 | -31.32 | -76.54 | 62.97 | -114.93 | 15.98 | BC 148 |
| | | | | Min $M_T$ | -109.76 | -7.89 | -16.81 | 20.92 | -31.56 | 5.22 | BC 356 |
| | | | | Max $M_y$ | -89.47 | -5.24 | -8.07 | 24.20 | -26.17 | 4.88 | BC 390 |
| | | | | Min $M_y$ | -331.58 | -31.49 | -76.48 | 62.81 | -115.33 | 16.04 | BC 154 |
| | | | | Max $M_z$ | -331.58 | -31.49 | -76.48 | 62.81 | -115.33 | 16.04 | BC 154 |
| | | | | Min $M_z$ | -89.47 | -5.24 | -8.07 | 24.20 | -26.17 | 4.88 | BC 390 |
| | | | 4950 | Max N | -10.60 | 8.63 | 35.32 | 11.72 | -0.95 | 2.23 | BC 389 |
| | | | | Min N | -244.02 | 23.46 | 76.66 | -5.39 | -59.14 | 6.17 | BC 264 |
| | | | | Max $V_y$ | -104.19 | 31.77 | 115.97 | -1.70 | -21.56 | 3.84 | BC 269 |
| | | | | Min $V_y$ | -150.56 | 0.31 | -4.07 | 8.08 | -38.72 | 4.57 | BC 360 |
| | | | | Max $V_z$ | -104.19 | 31.77 | 115.97 | -1.70 | -21.56 | 3.84 | BC 269 |
| | | | | Min $V_z$ | -151.61 | 0.32 | -4.11 | 7.91 | -38.52 | 4.53 | BC 356 |
| | | | | Max $M_T$ | -167.47 | 12.36 | 49.05 | 17.44 | -43.05 | 7.05 | BC 134 |
| | | | | Min $M_T$ | -188.32 | 19.28 | 60.27 | -10.11 | -45.35 | 3.97 | BC 468 |
| | | | | Max $M_y$ | -11.75 | 8.67 | 35.47 | 11.55 | -0.79 | 2.20 | BC 417 |
| | | | | Min $M_y$ | -243.31 | 23.42 | 76.54 | -5.23 | -59.36 | 6.21 | BC 236 |
| | | | | Max $M_z$ | -174.74 | 14.10 | 54.85 | 16.03 | -44.77 | 7.18 | BC 146 |
| | | | | Min $M_z$ | -41.65 | 25.82 | 93.64 | -5.09 | -6.17 | 1.51 | BC 413 |
| | | | 4950 | Max N | -10.60 | 8.63 | 35.32 | 11.72 | -0.95 | 2.23 | BC 389 |
| | | | | Min N | -244.02 | 23.46 | 76.66 | -5.39 | -59.14 | 6.17 | BC 264 |
| | | | | Max $V_y$ | -104.19 | 31.77 | 115.97 | -1.70 | -21.56 | 3.84 | BC 269 |
| | | | | Min $V_y$ | -150.56 | 0.31 | -4.07 | 8.08 | -38.72 | 4.57 | BC 360 |
| | | | | Max $V_z$ | -104.19 | 31.77 | 115.97 | -1.70 | -21.56 | 3.84 | BC 269 |
| | | | | Min $V_z$ | -151.61 | 0.32 | -4.11 | 7.91 | -38.52 | 4.53 | BC 356 |
| | | | | Max $M_T$ | -167.47 | 12.36 | 49.05 | 17.44 | -43.05 | 7.05 | BC 134 |
| | | | | Min $M_T$ | -188.32 | 19.28 | 60.27 | -10.11 | -45.35 | 3.97 | BC 468 |
| | | | | Max $M_y$ | -11.75 | 8.67 | 35.47 | 11.55 | -0.79 | 2.20 | BC 417 |
| | | | | Min $M_y$ | -243.31 | 23.42 | 76.54 | -5.23 | -59.36 | 6.21 | BC 236 |
| | | | | Max $M_z$ | -174.74 | 14.10 | 54.85 | 16.03 | -44.77 | 7.18 | BC 146 |
| | | | | Min $M_z$ | -41.65 | 25.82 | 93.64 | -5.09 | -6.17 | 1.51 | BC 413 |
| | | 44 | 6400 | Max N | 131.61 | 8.23 | 76.18 | 0.28 | 65.18 | -9.10 | BC 433 |
| | | | | Min N | -162.50 | 16.73 | 9.32 | 13.08 | -45.82 | 3.99 | BC 164 |
| | | | | Max $V_y$ | -107.13 | 19.83 | 31.82 | 10.74 | -15.49 | -4.61 | BC 264 |
| | | | | Min $V_y$ | -20.59 | 1.37 | 25.54 | 2.17 | 2.44 | 1.77 | BC 418 |
| | | | | Max $V_z$ | 114.08 | 10.05 | 89.07 | 1.79 | 65.11 | -8.55 | BC 241 |
| | | | | Min $V_z$ | -145.10 | 14.84 | -3.44 | 11.53 | -45.66 | 3.44 | BC 356 |
| | | | | Max $M_T$ | -158.91 | 17.29 | 17.97 | 13.45 | -43.57 | 4.10 | BC 172 |
| | | | | Min $M_T$ | 35.34 | 3.96 | 39.07 | -0.40 | 30.58 | -6.94 | BC 470 |
| | | | | Max $M_y$ | 131.13 | 8.22 | 76.05 | 0.26 | 65.39 | -9.16 | BC 461 |
| | | | | Min $M_y$ | -162.50 | 16.73 | 9.32 | 13.08 | -45.82 | 3.99 | BC 164 |
| | | | | Max $M_z$ | -158.91 | 17.29 | 17.97 | 13.45 | -43.57 | 4.10 | BC 172 |
| | | | | Min $M_z$ | 130.54 | 7.48 | 67.66 | -0.13 | 63.45 | -9.24 | BC 473 |
| 2 | RC1 | 6 | 0 | Max N | -25.35 | -18.93 | -9.73 | 27.64 | -21.32 | 2.20 | BC 357 |
| | | | | Min N | -76.60 | -53.41 | 11.02 | 72.35 | -55.89 | 5.82 | BC 155 |
| | | | | Max $V_y$ | -32.64 | -18.68 | -19.55 | 27.32 | -19.20 | 2.07 | BC 362 |
| | | | | Min $V_y$ | -76.60 | -53.41 | 11.02 | 72.35 | -55.89 | 5.82 | BC 155 |
| | | | | Max $V_z$ | -38.57 | -31.65 | 21.02 | 38.96 | -33.54 | 3.37 | BC 461 |
| | | | | Min $V_z$ | -48.78 | -28.68 | -25.17 | 42.14 | -30.37 | 3.24 | BC 170 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 2 | RC1 | | | Max $M_T$ | -76.60 | -53.41 | 11.02 | 72.35 | -55.89 | 5.82 | BC 155 |
| | | | | Min $M_T$ | -25.37 | -18.87 | -9.94 | 27.09 | -21.24 | 2.19 | BC 361 |
| | | | | Max $M_y$ | -32.64 | -18.68 | -19.55 | 27.32 | -19.20 | 2.07 | BC 362 |
| | | | | Min $M_y$ | -76.60 | -53.41 | 11.02 | 72.35 | -55.89 | 5.82 | BC 155 |
| | | | | Max $M_z$ | -76.60 | -53.41 | 11.02 | 72.35 | -55.89 | 5.82 | BC 155 |
| | | | | Min $M_z$ | -32.64 | -18.68 | -19.55 | 27.32 | -19.20 | 2.07 | BC 362 |
| | | 36 | 4300 | Max N | 229.26 | 10.82 | 120.17 | 32.40 | 96.65 | -1.96 | BC 340 |
| | | | | Min N | -65.04 | 11.05 | 22.64 | 19.13 | -18.06 | 3.03 | BC 358 |
| | | | | Max $V_y$ | 49.15 | 18.84 | 62.31 | 33.76 | 27.07 | 1.38 | BC 238 |
| | | | | Min $V_y$ | 10.64 | 2.08 | 44.66 | 12.51 | 17.62 | 1.79 | BC 357 |
| | | | | Max $V_z$ | 164.86 | 11.38 | 146.75 | 32.96 | 80.73 | 0.71 | BC 149 |
| | | | | Min $V_z$ | -14.55 | 14.91 | 13.03 | 26.82 | -2.84 | 1.50 | BC 410 |
| | | | | Max $M_T$ | 216.70 | 10.85 | 137.16 | 40.96 | 99.52 | -0.65 | BC 140 |
| | | | | Min $M_T$ | 29.09 | 4.10 | 50.90 | 10.01 | 23.39 | 1.30 | BC 421 |
| | | | | Max $M_y$ | 228.23 | 12.94 | 141.41 | 38.88 | 102.50 | -1.00 | BC 148 |
| | | | | Min $M_y$ | -65.04 | 11.05 | 22.64 | 19.13 | -18.06 | 3.03 | BC 358 |
| | | | | Max $M_z$ | -63.79 | 12.94 | 44.61 | 25.37 | -11.14 | 3.95 | BC 166 |
| | | | | Min $M_z$ | 229.26 | 10.82 | 120.17 | 32.40 | 96.65 | -1.96 | BC 340 |
| 3 | RC1 | 7 | 0 | Max N | -24.62 | -16.58 | -9.68 | 22.05 | -19.77 | 2.03 | BC 363 |
| | | | | Min N | -65.65 | -30.92 | -66.74 | 54.81 | -45.25 | 4.73 | BC 155 |
| | | | | Max $V_y$ | -34.05 | -12.58 | -39.08 | 30.31 | -22.54 | 2.35 | BC 385 |
| | | | | Min $V_y$ | -59.85 | -33.39 | -43.26 | 46.37 | -40.40 | 4.28 | BC 153 |
| | | | | Max $V_z$ | -24.62 | -16.58 | -9.68 | 22.05 | -19.77 | 2.03 | BC 363 |
| | | | | Min $V_z$ | -65.64 | -30.95 | -66.80 | 54.79 | -45.24 | 4.73 | BC 154 |
| | | | | Max $M_T$ | -65.65 | -30.92 | -66.74 | 54.81 | -45.25 | 4.73 | BC 155 |
| | | | | Min $M_T$ | -24.62 | -16.58 | -9.68 | 22.05 | -19.77 | 2.03 | BC 363 |
| | | | | Max $M_y$ | -28.51 | -14.81 | -16.96 | 22.18 | -17.81 | 1.92 | BC 361 |
| | | | | Min $M_y$ | -65.65 | -30.92 | -66.74 | 54.81 | -45.25 | 4.73 | BC 155 |
| | | | | Max $M_z$ | -65.65 | -30.92 | -66.74 | 54.81 | -45.25 | 4.73 | BC 155 |
| | | | | Min $M_z$ | -28.51 | -14.81 | -16.96 | 22.18 | -17.81 | 1.92 | BC 361 |
| | | | 1515 | Max N | -71.46 | -3.09 | -2.85 | 20.91 | -17.01 | 3.96 | BC 363 |
| | | | | Min N | -273.25 | -26.58 | -62.44 | 48.49 | -85.53 | 12.84 | BC 155 |
| | | | | Max $V_y$ | -87.60 | -2.41 | -0.54 | 24.23 | -22.44 | 5.30 | BC 360 |
| | | | | Min $V_y$ | -273.25 | -26.58 | -62.44 | 48.49 | -85.53 | 12.84 | BC 155 |
| | | | | Max $V_z$ | -89.08 | -2.57 | -0.48 | 24.12 | -22.86 | 5.36 | BC 356 |
| | | | | Min $V_z$ | -240.72 | -26.00 | -64.79 | 42.12 | -74.48 | 10.48 | BC 241 |
| | | | | Max $M_T$ | -255.15 | -25.22 | -59.34 | 48.65 | -79.02 | 12.07 | BC 21 |
| | | | | Min $M_T$ | -93.18 | -6.42 | -14.33 | 20.22 | -23.85 | 3.96 | BC 357 |
| | | | | Max $M_y$ | -71.46 | -3.09 | -2.85 | 20.91 | -17.01 | 3.96 | BC 363 |
| | | | | Min $M_y$ | -273.21 | -26.57 | -62.38 | 48.47 | -85.55 | 12.85 | BC 154 |
| | | | | Max $M_z$ | -273.21 | -26.57 | -62.38 | 48.47 | -85.55 | 12.85 | BC 154 |
| | | | | Min $M_z$ | -92.11 | -6.33 | -14.63 | 20.38 | -23.65 | 3.90 | BC 389 |
| | | | 1515 | Max N | -71.46 | -3.09 | -2.85 | 20.91 | -17.01 | 3.96 | BC 363 |
| | | | | Min N | -273.25 | -26.58 | -62.44 | 48.49 | -85.53 | 12.84 | BC 155 |
| | | | | Max $V_y$ | -87.60 | -2.41 | -0.54 | 24.23 | -22.44 | 5.30 | BC 360 |
| | | | | Min $V_y$ | -273.25 | -26.58 | -62.44 | 48.49 | -85.53 | 12.84 | BC 155 |
| | | | | Max $V_z$ | -89.08 | -2.57 | -0.48 | 24.12 | -22.86 | 5.36 | BC 356 |
| | | | | Min $V_z$ | -240.72 | -26.00 | -64.79 | 42.12 | -74.48 | 10.48 | BC 241 |
| | | | | Max $M_T$ | -255.15 | -25.22 | -59.34 | 48.65 | -79.02 | 12.07 | BC 21 |
| | | | | Min $M_T$ | -93.18 | -6.42 | -14.33 | 20.22 | -23.85 | 3.96 | BC 357 |
| | | | | Max $M_y$ | -71.46 | -3.09 | -2.85 | 20.91 | -17.01 | 3.96 | BC 363 |
| | | | | Min $M_y$ | -273.21 | -26.57 | -62.38 | 48.47 | -85.55 | 12.85 | BC 154 |
| | | | | Max $M_z$ | -273.21 | -26.57 | -62.38 | 48.47 | -85.55 | 12.85 | BC 154 |
| | | | | Min $M_z$ | -92.11 | -6.33 | -14.63 | 20.38 | -23.65 | 3.90 | BC 389 |
| | | | 4865 | Max N | 8.50 | 1.94 | 43.01 | 2.48 | 25.15 | 0.41 | BC 360 |
| | | | | Min N | -210.56 | 36.69 | 72.95 | -0.09 | -66.76 | 6.85 | BC 269 |
| | | | | Max $V_y$ | -210.56 | 36.69 | 72.95 | -0.09 | -66.76 | 6.85 | BC 269 |
| | | | | Min $V_y$ | 8.50 | 1.94 | 43.01 | 2.48 | 25.15 | 0.41 | BC 360 |
| | | | | Max $V_z$ | -80.48 | 27.40 | 127.41 | -15.16 | 8.37 | 2.92 | BC 264 |
| | | | | Min $V_z$ | -120.30 | 11.42 | -11.02 | 17.54 | -49.69 | 4.33 | BC 389 |
| | | | | Max $M_T$ | -154.10 | 15.34 | 4.53 | 21.24 | -55.24 | 5.56 | BC 185 |
| | | | | Min $M_T$ | -44.81 | 23.44 | 111.85 | -18.90 | 14.35 | 1.65 | BC 468 |
| | | | | Max $M_y$ | 7.22 | 1.98 | 43.16 | 2.28 | 25.26 | 0.39 | BC 356 |
| | | | | Min $M_y$ | -209.91 | 36.68 | 72.84 | 0.12 | -67.04 | 6.88 | BC 241 |
| | | | | Max $M_z$ | -209.91 | 36.68 | 72.84 | 0.12 | -67.04 | 6.88 | BC 241 |
| | | | | Min $M_z$ | 7.22 | 1.98 | 43.16 | 2.28 | 25.26 | 0.39 | BC 356 |
| | | | 4865 | Max N | 10.43 | 1.87 | -28.14 | 1.99 | 24.36 | 1.04 | BC 360 |
| | | | | Min N | -233.51 | 37.68 | 139.48 | 2.02 | -56.96 | 6.93 | BC 269 |
| | | | | Max $V_y$ | -233.51 | 37.68 | 139.48 | 2.02 | -56.96 | 6.93 | BC 269 |
| | | | | Min $V_y$ | 10.43 | 1.87 | -28.14 | 1.99 | 24.36 | 1.04 | BC 360 |
| | | | | Max $V_z$ | -233.51 | 37.68 | 139.48 | 2.02 | -56.96 | 6.93 | BC 269 |
| | | | | Min $V_z$ | 10.43 | 1.87 | -28.14 | 1.99 | 24.36 | 1.04 | BC 360 |
| | | | | Max $M_T$ | -172.44 | 14.54 | 65.98 | 22.29 | -46.54 | 6.13 | BC 185 |
| | | | | Min $M_T$ | -47.85 | 25.12 | 44.13 | -18.37 | 14.95 | 1.80 | BC 468 |
| | | | | Max $M_y$ | 9.14 | 1.91 | -28.01 | 1.79 | 24.48 | 1.01 | BC 356 |
| | | | | Min $M_y$ | -232.89 | 37.66 | 139.47 | 2.22 | -57.23 | 6.97 | BC 241 |
| | | | | Max $M_z$ | -232.89 | 37.66 | 139.47 | 2.22 | -57.23 | 6.97 | BC 241 |
| | | | | Min $M_z$ | 9.14 | 1.91 | -28.01 | 1.79 | 24.48 | 1.01 | BC 356 |
| | | | 5015 | Max N | 2.87 | -0.50 | -22.62 | -0.04 | 22.92 | 0.79 | BC 360 |
| | | | | Min N | -173.89 | 36.09 | 132.77 | 3.00 | -56.62 | 4.43 | BC 269 |
| | | | | Max $V_y$ | -173.89 | 36.09 | 132.77 | 3.00 | -56.62 | 4.43 | BC 269 |
| | | | | Min $V_y$ | 2.87 | -0.50 | -22.62 | -0.04 | 22.92 | 0.79 | BC 360 |
| | | | | Max $V_z$ | -173.26 | 36.08 | 132.80 | 3.18 | -56.89 | 4.47 | BC 241 |
| | | | | Min $V_z$ | 2.87 | -0.50 | -22.62 | -0.04 | 22.92 | 0.79 | BC 360 |
| | | | | Max $M_T$ | -144.41 | 15.40 | 70.10 | 22.03 | -45.37 | 4.62 | BC 185 |
| | | | | Min $M_T$ | -24.81 | 20.14 | 38.87 | -19.09 | 12.91 | 0.53 | BC 468 |
| | | | | Max $M_y$ | 1.61 | -0.47 | -22.54 | -0.22 | 23.04 | 0.77 | BC 356 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 3 | RC1 | | | Min $M_y$ | -173.26 | 36.08 | 132.80 | 3.18 | -56.89 | 4.47 | BC 241 |
| | | | | Max $M_z$ | -148.86 | 17.44 | 76.38 | 20.78 | -47.12 | 4.75 | BC 245 |
| | | | | Min $M_z$ | -20.22 | 18.11 | 32.67 | -17.84 | 14.62 | 0.40 | BC 408 |
| | | | 5015 | Max N | 2.87 | -0.50 | -22.62 | -0.04 | 22.92 | 0.79 | BC 360 |
| | | | | Min N | -173.89 | 36.09 | 132.77 | 3.00 | -56.62 | 4.43 | BC 269 |
| | | | | Max $V_y$ | -173.89 | 36.09 | 132.77 | 3.00 | -56.62 | 4.43 | BC 269 |
| | | | | Min $V_y$ | 2.87 | -0.50 | -22.62 | -0.04 | 22.92 | 0.79 | BC 360 |
| | | | | Max $V_z$ | -173.26 | 36.08 | 132.80 | 3.18 | -56.89 | 4.47 | BC 241 |
| | | | | Min $V_z$ | 2.87 | -0.50 | -22.62 | -0.04 | 22.92 | 0.79 | BC 360 |
| | | | | Max $M_T$ | -144.41 | 15.40 | 70.10 | 22.03 | -45.37 | 4.62 | BC 185 |
| | | | | Min $M_T$ | -24.81 | 20.14 | 38.87 | -19.09 | 12.91 | 0.53 | BC 468 |
| | | | | Max $M_y$ | 1.61 | -0.47 | -22.54 | -0.22 | 23.04 | 0.77 | BC 356 |
| | | | | Min $M_y$ | -173.26 | 36.08 | 132.80 | 3.18 | -56.89 | 4.47 | BC 241 |
| | | | | Max $M_z$ | -148.86 | 17.44 | 76.38 | 20.78 | -47.12 | 4.75 | BC 245 |
| | | | | Min $M_z$ | -20.22 | 18.11 | 32.67 | -17.84 | 14.62 | 0.40 | BC 408 |
| | | 59 | 6530 | Max N | 64.10 | 3.32 | 32.05 | 0.25 | 34.26 | -8.04 | BC 435 |
| | | | | Min N | -34.09 | -7.36 | 2.73 | -7.11 | 12.70 | 0.98 | BC 164 |
| | | | | Max $V_y$ | 58.04 | 20.33 | 83.24 | 17.15 | 34.90 | -8.45 | BC 241 |
| | | | | Min $V_y$ | -29.44 | -8.40 | -8.00 | -8.45 | 9.33 | 0.85 | BC 356 |
| | | | | Max $V_z$ | 58.04 | 20.33 | 83.24 | 17.15 | 34.90 | -8.45 | BC 241 |
| | | | | Min $V_z$ | -29.44 | -8.40 | -8.00 | -8.45 | 9.33 | 0.85 | BC 356 |
| | | | | Max $M_T$ | 7.97 | 17.51 | 78.78 | 19.68 | 13.39 | 0.21 | BC 185 |
| | | | | Min $M_T$ | 21.11 | -6.76 | -4.59 | -11.55 | 31.12 | -7.75 | BC 468 |
| | | | | Max $M_y$ | 55.14 | 7.61 | 63.59 | 4.35 | 43.70 | -8.64 | BC 154 |
| | | | | Min $M_y$ | -20.93 | 2.49 | 23.49 | 2.73 | 4.42 | 1.05 | BC 362 |
| | | | | Max $M_z$ | -25.41 | 3.50 | 34.87 | 4.02 | 8.10 | 1.17 | BC 170 |
| | | | | Min $M_z$ | 59.33 | 6.85 | 52.50 | 3.36 | 39.63 | -8.75 | BC 347 |
| 4 | RC1 | 8 | 0 | Max N | -23.71 | -16.48 | -15.66 | 26.05 | -20.52 | 2.17 | BC 356 |
| | | | | Min N | -68.55 | -47.58 | 1.76 | 64.44 | -51.63 | 5.47 | BC 148 |
| | | | | Max $V_y$ | -23.73 | -16.42 | -15.89 | 25.47 | -20.43 | 2.15 | BC 360 |
| | | | | Min $V_y$ | -68.54 | -47.67 | 2.11 | 65.03 | -51.73 | 5.49 | BC 155 |
| | | | | Max $V_z$ | -37.30 | -29.19 | 18.59 | 36.00 | -31.67 | 3.26 | BC 470 |
| | | | | Min $V_z$ | -49.31 | -29.19 | -29.93 | 43.35 | -31.81 | 3.48 | BC 187 |
| | | | | Max $M_T$ | -68.54 | -47.67 | 2.11 | 65.03 | -51.73 | 5.49 | BC 155 |
| | | | | Min $M_T$ | -30.16 | -17.01 | -21.73 | 25.15 | -18.17 | 2.00 | BC 363 |
| | | | | Max $M_y$ | -30.16 | -17.01 | -21.73 | 25.15 | -18.17 | 2.00 | BC 363 |
| | | | | Min $M_y$ | -68.54 | -47.67 | 2.11 | 65.03 | -51.73 | 5.49 | BC 155 |
| | | | | Max $M_z$ | -68.54 | -47.67 | 2.11 | 65.03 | -51.73 | 5.49 | BC 155 |
| | | | | Min $M_z$ | -30.16 | -17.01 | -21.73 | 25.15 | -18.17 | 2.00 | BC 363 |
| | | 54 | 4300 | Max N | 92.93 | 5.64 | 59.00 | 20.75 | 52.31 | -0.63 | BC 430 |
| | | | | Min N | -130.18 | 10.47 | 24.16 | 24.84 | -30.60 | 4.84 | BC 227 |
| | | | | Max $V_y$ | -63.04 | 15.95 | 20.94 | 29.66 | -10.18 | 2.95 | BC 251 |
| | | | | Min $V_y$ | -56.94 | 0.28 | 27.36 | 12.38 | -3.15 | 2.92 | BC 416 |
| | | | | Max $V_z$ | 4.79 | 6.38 | 97.90 | 31.31 | 32.48 | 2.92 | BC 146 |
| | | | | Min $V_z$ | -61.80 | 13.03 | -0.82 | 26.55 | -16.60 | 2.22 | BC 415 |
| | | | | Max $M_T$ | 49.98 | 5.62 | 87.04 | 39.73 | 49.04 | 1.74 | BC 140 |
| | | | | Min $M_T$ | -37.90 | 2.45 | 33.74 | 9.71 | 2.58 | 2.42 | BC 420 |
| | | | | Max $M_y$ | 88.78 | 6.32 | 78.18 | 31.10 | 54.45 | 0.03 | BC 340 |
| | | | | Min $M_y$ | -109.54 | 9.20 | 9.06 | 18.82 | -30.81 | 3.63 | BC 419 |
| | | | | Max $M_z$ | -129.66 | 10.51 | 24.27 | 24.74 | -30.56 | 4.85 | BC 167 |
| | | | | Min $M_z$ | 92.70 | 5.58 | 59.00 | 20.85 | 52.39 | -0.64 | BC 434 |
| 5 | RC1 | 5 | 0 | Max N | -23.57 | -5.01 | -4.95 | 0.00 | 0.00 | 0.00 | BC 422 |
| | | | Links | Min N | -56.15 | 0.05 | 0.20 | -0.00 | 0.00 | 0.00 | BC 133 |
| | | | | Max $V_y$ | -40.37 | 6.88 | 3.81 | -0.00 | 0.00 | 0.00 | BC 236 |
| | | | | Min $V_y$ | -23.57 | -5.03 | -4.90 | 0.00 | 0.00 | 0.00 | BC 414 |
| | | | | Max $V_z$ | -40.37 | 6.88 | 3.81 | -0.00 | 0.00 | 0.00 | BC 240 |
| | | | | Min $V_z$ | -23.57 | -5.01 | -4.96 | 0.00 | 0.00 | 0.00 | BC 390 |
| | | | | Max $M_T$ | -23.57 | -5.03 | -4.89 | 0.00 | 0.00 | 0.00 | BC 474 |
| | | | | Min $M_T$ | -40.37 | 6.85 | 3.73 | -0.00 | 0.00 | 0.00 | BC 200 |
| | | | | Max $M_y$ | -29.22 | -5.02 | -4.89 | 0.00 | 0.00 | 0.00 | BC 374 |
| | | | | Min $M_y$ | -34.64 | 3.09 | -2.00 | -0.00 | -0.00 | 0.00 | BC 163 |
| | | | | Max $M_z$ | -40.32 | 0.01 | 0.15 | -0.00 | 0.00 | 0.00 | BC 91 |
| | | | | Min $M_z$ | -29.34 | 6.86 | 3.77 | -0.00 | 0.00 | -0.00 | BC 428 |
| | | | 0 | Max N | -23.57 | -5.01 | -4.95 | 0.00 | -0.00 | 0.00 | BC 422 |
| | | | Rechts | Min N | -56.15 | 0.05 | 0.20 | -0.00 | 0.00 | -0.00 | BC 133 |
| | | | | Max $V_y$ | -40.37 | 6.88 | 3.81 | -0.00 | 0.00 | -0.00 | BC 236 |
| | | | | Min $V_y$ | -23.57 | -5.03 | -4.90 | 0.00 | -0.00 | 0.00 | BC 414 |
| | | | | Max $V_z$ | -40.37 | 6.88 | 3.81 | -0.00 | 0.00 | -0.00 | BC 240 |
| | | | | Min $V_z$ | -23.57 | -5.01 | -4.96 | 0.00 | -0.00 | 0.00 | BC 390 |
| | | | | Max $M_T$ | -23.57 | -5.03 | -4.89 | 0.00 | -0.00 | 0.00 | BC 474 |
| | | | | Min $M_T$ | -40.37 | 6.85 | 3.73 | -0.00 | 0.00 | -0.00 | BC 200 |
| | | | | Max $M_y$ | -40.37 | 6.88 | 3.81 | -0.00 | 0.00 | -0.00 | BC 240 |
| | | | | Min $M_y$ | -23.57 | -5.01 | -4.96 | 0.00 | -0.00 | 0.00 | BC 390 |
| | | | | Max $M_z$ | -34.60 | -5.03 | -4.86 | 0.00 | -0.00 | 0.00 | BC 218 |
| | | | | Min $M_z$ | -40.37 | 6.88 | 3.81 | -0.00 | 0.00 | -0.00 | BC 236 |
| | | | 2500 | Max N | -21.57 | 2.03 | 2.00 | 0.00 | -3.68 | 3.72 | BC 422 |
| | | | Links | Min N | -53.23 | 0.05 | 0.20 | -0.00 | 0.50 | -0.12 | BC 133 |
| | | | | Max $V_y$ | -37.33 | 2.04 | 2.04 | 0.00 | -3.58 | 3.69 | BC 234 |
| | | | | Min $V_y$ | -21.69 | -2.94 | -0.96 | -0.00 | 3.49 | -4.87 | BC 412 |
| | | | | Max $V_z$ | -31.67 | 2.00 | 2.10 | 0.00 | -3.43 | 3.78 | BC 278 |
| | | | | Min $V_z$ | -21.69 | -2.93 | -1.02 | -0.00 | 3.33 | -4.89 | BC 356 |
| | | | | Max $M_T$ | -21.57 | 2.00 | 2.06 | 0.00 | -3.53 | 3.79 | BC 474 |
| | | | | Min $M_T$ | -37.45 | -2.93 | -0.97 | -0.00 | 3.45 | -4.90 | BC 200 |
| | | | | Max $M_y$ | -37.45 | -2.90 | -0.90 | -0.00 | 3.64 | -4.98 | BC 240 |
| | | | | Min $M_y$ | -21.57 | 2.03 | 1.99 | 0.00 | -3.71 | 3.73 | BC 390 |
| | | | | Max $M_z$ | -21.57 | 2.00 | 2.06 | 0.00 | -3.55 | 3.79 | BC 414 |
| | | | | Min $M_z$ | -37.45 | -2.90 | -0.90 | -0.00 | 3.64 | -4.98 | BC 236 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 5 | RC1 | | 2500 | Max N | -21.57 | 2.03 | 2.00 | 0.00 | -3.68 | 3.72 | BC 422 |
| | | | Rechts | Min N | -53.23 | 0.05 | 0.20 | -0.00 | 0.50 | -0.12 | BC 133 |
| | | | | Max $V_y$ | -37.33 | 2.04 | 2.05 | 0.00 | -3.58 | 3.69 | BC 234 |
| | | | | Min $V_y$ | -21.69 | -2.94 | -0.96 | -0.00 | 3.49 | -4.87 | BC 412 |
| | | | | Max $V_z$ | -31.67 | 2.00 | 2.10 | 0.00 | -3.43 | 3.78 | BC 278 |
| | | | | Min $V_z$ | -21.69 | -2.93 | -1.02 | -0.00 | 3.33 | -4.89 | BC 356 |
| | | | | Max $M_T$ | -21.57 | 2.00 | 2.06 | 0.00 | -3.53 | 3.79 | BC 474 |
| | | | | Min $M_T$ | -37.45 | -2.93 | -0.97 | -0.00 | 3.45 | -4.90 | BC 200 |
| | | | | Max $M_y$ | -37.45 | -2.90 | -0.90 | -0.00 | 3.64 | -4.98 | BC 240 |
| | | | | Min $M_y$ | -21.57 | 2.03 | 1.99 | 0.00 | -3.71 | 3.73 | BC 390 |
| | | | | Max $M_z$ | -21.57 | 2.00 | 2.06 | 0.00 | -3.55 | 3.79 | BC 414 |
| | | | | Min $M_z$ | -37.45 | -2.90 | -0.90 | -0.00 | 3.64 | -4.98 | BC 236 |
| | | | 4345 | Max N | -17.43 | 7.22 | 7.13 | 0.00 | 4.74 | -4.81 | BC 422 |
| | | | Links | Min N | -47.15 | 0.05 | 0.20 | -0.00 | 0.87 | -0.20 | BC 133 |
| | | | | Max $V_y$ | -31.25 | 7.23 | 7.17 | 0.00 | 4.93 | -4.86 | BC 234 |
| | | | | Min $V_y$ | -17.55 | -10.16 | -4.43 | -0.00 | -1.48 | 7.22 | BC 412 |
| | | | | Max $V_z$ | -25.60 | 7.20 | 7.23 | 0.00 | 5.18 | -4.70 | BC 278 |
| | | | | Min $V_z$ | -17.55 | -10.15 | -4.49 | -0.00 | -1.76 | 7.18 | BC 356 |
| | | | | Max $M_T$ | -17.43 | 7.19 | 7.19 | 0.00 | 5.01 | -4.70 | BC 474 |
| | | | | Min $M_T$ | -31.37 | -10.14 | -4.44 | -0.00 | -1.54 | 7.15 | BC 200 |
| | | | | Max $M_y$ | -25.60 | 7.20 | 7.23 | 0.00 | 5.18 | -4.70 | BC 278 |
| | | | | Min $M_y$ | -17.55 | -10.15 | -4.49 | -0.00 | -1.76 | 7.18 | BC 356 |
| | | | | Max $M_z$ | -17.55 | -10.16 | -4.43 | -0.00 | -1.48 | 7.22 | BC 412 |
| | | | | Min $M_z$ | -31.25 | 7.23 | 7.17 | 0.00 | 4.93 | -4.86 | BC 234 |
| | | 9 | 4345 | Max N | -17.43 | 7.22 | 7.13 | 0.00 | 4.74 | -4.81 | BC 422 |
| | | | Rechts | Min N | -47.15 | 0.05 | 0.20 | -0.00 | 0.87 | -0.20 | BC 133 |
| | | | | Max $V_y$ | -31.25 | 7.23 | 7.17 | 0.00 | 4.93 | -4.86 | BC 234 |
| | | | | Min $V_y$ | -17.55 | -10.16 | -4.43 | -0.00 | -1.48 | 7.22 | BC 412 |
| | | | | Max $V_z$ | -25.60 | 7.20 | 7.23 | 0.00 | 5.18 | -4.70 | BC 278 |
| | | | | Min $V_z$ | -17.55 | -10.15 | -4.49 | -0.00 | -1.76 | 7.18 | BC 356 |
| | | | | Max $M_T$ | -17.43 | 7.19 | 7.19 | 0.00 | 5.01 | -4.70 | BC 474 |
| | | | | Min $M_T$ | -31.37 | -10.14 | -4.44 | -0.00 | -1.54 | 7.15 | BC 200 |
| | | | | Max $M_y$ | -25.60 | 7.20 | 7.23 | 0.00 | 5.18 | -4.70 | BC 278 |
| | | | | Min $M_y$ | -17.55 | -10.15 | -4.49 | -0.00 | -1.76 | 7.18 | BC 356 |
| | | | | Max $M_z$ | -17.55 | -10.16 | -4.43 | -0.00 | -1.48 | 7.22 | BC 412 |
| | | | | Min $M_z$ | -31.25 | 7.23 | 7.17 | 0.00 | 4.93 | -4.86 | BC 234 |
| 6 | RC1 | 6 | 0 | Max N | -23.80 | -5.15 | 4.97 | -0.00 | 0.00 | 0.00 | BC 358 |
| | | | | Min N | -57.03 | 0.09 | -0.18 | 0.00 | -0.00 | 0.00 | BC 155 |
| | | | | Max $V_y$ | -40.98 | 7.01 | -3.76 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min $V_y$ | -34.97 | -5.16 | 4.92 | -0.00 | 0.00 | 0.00 | BC 218 |
| | | | | Max $V_z$ | -23.80 | -5.15 | 4.97 | -0.00 | 0.00 | 0.00 | BC 358 |
| | | | | Min $V_z$ | -40.98 | 7.00 | -3.76 | 0.00 | 0.00 | 0.00 | BC 265 |
| | | | | Max $M_T$ | -40.98 | 7.01 | -3.71 | 0.00 | 0.00 | 0.00 | BC 245 |
| | | | | Min $M_T$ | -23.80 | -5.14 | 4.97 | -0.00 | 0.00 | 0.00 | BC 362 |
| | | | | Max $M_y$ | -29.57 | -5.14 | 4.90 | -0.00 | 0.00 | 0.00 | BC 374 |
| | | | | Min $M_y$ | -35.04 | 3.17 | 2.06 | 0.00 | -0.00 | 0.00 | BC 163 |
| | | | | Max $M_z$ | -40.82 | 3.90 | 1.84 | 0.00 | -0.00 | 0.00 | BC 268 |
| | | | | Min $M_z$ | -24.04 | 7.00 | -3.67 | 0.00 | 0.00 | -0.00 | BC 353 |
| | | | 2500 | Max N | -21.80 | 2.07 | -1.98 | -0.00 | 3.74 | 3.85 | BC 358 |
| | | | Links | Min N | -54.10 | 0.09 | -0.18 | 0.00 | -0.46 | -0.22 | BC 155 |
| | | | | Max $V_y$ | -27.57 | 2.09 | -2.01 | -0.00 | 3.67 | 3.79 | BC 438 |
| | | | | Min $V_y$ | -22.04 | -3.01 | 0.99 | 0.00 | -3.41 | -4.96 | BC 413 |
| | | | | Max $V_z$ | -22.04 | -2.99 | 1.04 | 0.00 | -3.29 | -5.01 | BC 417 |
| | | | | Min $V_z$ | -37.81 | 2.07 | -2.08 | -0.00 | 3.48 | 3.83 | BC 242 |
| | | | | Max $M_T$ | -38.05 | -2.98 | 0.99 | 0.00 | -3.40 | -5.04 | BC 245 |
| | | | | Min $M_T$ | -21.80 | 2.07 | -1.98 | -0.00 | 3.74 | 3.84 | BC 362 |
| | | | | Max $M_y$ | -21.80 | 2.07 | -1.98 | -0.00 | 3.74 | 3.85 | BC 358 |
| | | | | Min $M_y$ | -38.05 | -2.98 | 0.94 | 0.00 | -3.52 | -5.02 | BC 265 |
| | | | | Max $M_z$ | -32.04 | 2.05 | -2.03 | -0.00 | 3.61 | 3.89 | BC 218 |
| | | | | Min $M_z$ | -38.05 | -2.97 | 0.94 | 0.00 | -3.52 | -5.06 | BC 241 |
| | | | 2500 | Max N | -21.80 | 2.07 | -1.98 | -0.00 | 3.74 | 3.85 | BC 358 |
| | | | Rechts | Min N | -54.10 | 0.09 | -0.18 | 0.00 | -0.46 | -0.22 | BC 155 |
| | | | | Max $V_y$ | -27.57 | 2.09 | -2.01 | -0.00 | 3.67 | 3.79 | BC 438 |
| | | | | Min $V_y$ | -22.04 | -3.01 | 0.99 | 0.00 | -3.41 | -4.96 | BC 413 |
| | | | | Max $V_z$ | -22.04 | -2.99 | 1.04 | 0.00 | -3.29 | -5.01 | BC 417 |
| | | | | Min $V_z$ | -37.81 | 2.07 | -2.08 | -0.00 | 3.48 | 3.83 | BC 242 |
| | | | | Max $M_T$ | -38.05 | -2.98 | 0.99 | 0.00 | -3.40 | -5.04 | BC 245 |
| | | | | Min $M_T$ | -21.80 | 2.07 | -1.98 | -0.00 | 3.74 | 3.84 | BC 362 |
| | | | | Max $M_y$ | -21.80 | 2.07 | -1.98 | -0.00 | 3.74 | 3.85 | BC 358 |
| | | | | Min $M_y$ | -38.05 | -2.98 | 0.94 | 0.00 | -3.52 | -5.02 | BC 265 |
| | | | | Max $M_z$ | -32.04 | 2.05 | -2.03 | -0.00 | 3.61 | 3.89 | BC 218 |
| | | | | Min $M_z$ | -38.05 | -2.97 | 0.94 | 0.00 | -3.52 | -5.06 | BC 241 |
| | | | 4345 | Max N | -17.62 | 7.39 | -7.11 | -0.00 | -4.64 | -4.88 | BC 358 |
| | | | Links | Min N | -47.98 | 0.09 | -0.18 | 0.00 | -0.79 | -0.38 | BC 154 |
| | | | | Max $V_y$ | -23.39 | 7.41 | -7.14 | -0.00 | -4.77 | -4.97 | BC 438 |
| | | | | Min $V_y$ | -17.87 | -10.38 | 4.46 | 0.00 | 1.61 | 7.39 | BC 413 |
| | | | | Max $V_z$ | -17.86 | -10.36 | 4.51 | 0.00 | 1.82 | 7.30 | BC 417 |
| | | | | Min $V_z$ | -31.68 | 7.40 | -7.21 | -0.00 | -5.10 | -4.91 | BC 242 |
| | | | | Max $M_T$ | -31.92 | -10.34 | 4.46 | 0.00 | 1.63 | 7.25 | BC 245 |
| | | | | Min $M_T$ | -17.62 | 7.40 | -7.11 | -0.00 | -4.65 | -4.90 | BC 362 |
| | | | | Max $M_y$ | -17.86 | -10.36 | 4.51 | 0.00 | 1.82 | 7.30 | BC 417 |
| | | | | Min $M_y$ | -31.68 | 7.40 | -7.21 | -0.00 | -5.10 | -4.91 | BC 242 |
| | | | | Max $M_z$ | -17.87 | -10.38 | 4.46 | 0.00 | 1.61 | 7.39 | BC 413 |
| | | | | Min $M_z$ | -23.39 | 7.41 | -7.14 | -0.00 | -4.77 | -4.97 | BC 438 |
| | | 12 | 4345 | Max N | -17.62 | 7.39 | -7.11 | -0.00 | -4.64 | -4.88 | BC 358 |
| | | | Rechts | Min N | -47.98 | 0.09 | -0.18 | 0.00 | -0.79 | -0.37 | BC 155 |
| | | | | Max $V_y$ | -23.39 | 7.41 | -7.14 | -0.00 | -4.77 | -4.97 | BC 438 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 6 | RC1 | | | Min $V_y$ | -17.87 | -10.38 | 4.46 | 0.00 | 1.61 | 7.39 | BC 413 |
| | | | | Max $V_z$ | -17.86 | -10.36 | 4.51 | 0.00 | 1.82 | 7.30 | BC 417 |
| | | | | Min $V_z$ | -31.68 | 7.40 | -7.21 | -0.00 | -5.10 | -4.91 | BC 242 |
| | | | | Max $M_T$ | -31.92 | -10.34 | 4.46 | 0.00 | 1.63 | 7.25 | BC 245 |
| | | | | Min $M_T$ | -17.62 | 7.40 | -7.11 | -0.00 | -4.65 | -4.90 | BC 362 |
| | | | | Max $M_y$ | -17.86 | -10.36 | 4.51 | 0.00 | 1.82 | 7.30 | BC 417 |
| | | | | Min $M_y$ | -31.68 | 7.40 | -7.21 | -0.00 | -5.10 | -4.91 | BC 242 |
| | | | | Max $M_z$ | -17.87 | -10.38 | 4.46 | 0.00 | 1.61 | 7.39 | BC 413 |
| | | | | Min $M_z$ | -23.39 | 7.41 | -7.14 | -0.00 | -4.77 | -4.97 | BC 438 |
| 7 | RC1 | 45 | 0 | Max N | 3.51 | 0.12 | 7.08 | 0.02 | 0.00 | 0.00 | BC 390 |
| | | | | Min N | -3.36 | 0.02 | 16.03 | -0.01 | 0.00 | 0.00 | BC 240 |
| | | | | Max $V_y$ | 3.27 | 0.13 | 16.03 | 0.02 | 0.00 | 0.00 | BC 234 |
| | | | | Min $V_y$ | 1.16 | -0.11 | 7.08 | -0.02 | 0.00 | 0.00 | BC 409 |
| | | | | Max $V_z$ | -0.79 | 0.05 | 31.86 | 0.00 | 0.00 | 0.00 | BC 138 |
| | | | | Min $V_z$ | -3.12 | 0.00 | 7.07 | -0.02 | 0.00 | 0.00 | BC 440 |
| | | | | Max $M_T$ | 3.27 | 0.13 | 16.03 | 0.02 | 0.00 | 0.00 | BC 234 |
| | | | | Min $M_T$ | 1.16 | -0.11 | 7.08 | -0.02 | 0.00 | 0.00 | BC 409 |
| | | | | Max $M_y$ | -0.46 | 0.03 | 18.38 | 0.00 | 0.00 | 0.00 | BC 304 |
| | | | | Min $M_y$ | -0.55 | 0.03 | 17.37 | 0.00 | -0.00 | 0.00 | BC 21 |
| | | | | Max $M_z$ | -0.37 | 0.02 | 11.71 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.37 | 0.02 | 11.71 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 150 | 3201 | Max N | 3.64 | 0.12 | 0.08 | 0.02 | 11.45 | -0.39 | BC 390 |
| | | | | Min N | -3.06 | 0.02 | 0.09 | -0.01 | 25.79 | -0.05 | BC 240 |
| | | | | Max $V_y$ | 3.57 | 0.13 | 0.09 | 0.02 | 25.80 | -0.42 | BC 234 |
| | | | | Min $V_y$ | 1.29 | -0.11 | 0.08 | -0.02 | 11.45 | 0.36 | BC 409 |
| | | | | Max $V_z$ | -0.13 | 0.02 | 0.13 | 0.00 | 18.95 | -0.06 | BC 17 |
| | | | | Min $V_z$ | -0.26 | 0.04 | -0.01 | 0.00 | 45.68 | -0.13 | BC 340 |
| | | | | Max $M_T$ | 3.57 | 0.13 | 0.09 | 0.02 | 25.80 | -0.42 | BC 234 |
| | | | | Min $M_T$ | 1.29 | -0.11 | 0.08 | -0.02 | 11.45 | 0.36 | BC 409 |
| | | | | Max $M_y$ | -0.19 | 0.05 | 0.03 | 0.00 | 51.03 | -0.15 | BC 138 |
| | | | | Min $M_y$ | -2.99 | 0.00 | 0.07 | -0.02 | 11.44 | -0.01 | BC 440 |
| | | | | Max $M_z$ | 1.29 | -0.11 | 0.08 | -0.02 | 11.45 | 0.36 | BC 409 |
| | | | | Min $M_z$ | 3.57 | 0.13 | 0.09 | 0.02 | 25.80 | -0.42 | BC 234 |
| 8 | RC1 | 46 | 0 | Max N | 3.39 | -0.13 | 7.22 | -0.02 | 0.00 | 0.00 | BC 358 |
| | | | | Min N | -3.62 | -0.03 | 16.35 | 0.01 | 0.00 | 0.00 | BC 265 |
| | | | | Max $V_y$ | 0.98 | 0.12 | 7.21 | 0.02 | 0.00 | 0.00 | BC 472 |
| | | | | Min $V_y$ | 2.90 | -0.15 | 16.35 | -0.02 | -0.00 | 0.00 | BC 242 |
| | | | | Max $V_z$ | -1.41 | -0.04 | 32.49 | -0.00 | 0.00 | 0.00 | BC 138 |
| | | | | Min $V_z$ | 1.18 | 0.02 | 7.21 | 0.01 | 0.00 | 0.00 | BC 443 |
| | | | | Max $M_T$ | 0.99 | 0.12 | 7.21 | 0.02 | 0.00 | 0.00 | BC 412 |
| | | | | Min $M_T$ | 2.90 | -0.15 | 16.35 | -0.02 | -0.00 | 0.00 | BC 242 |
| | | | | Max $M_y$ | 3.07 | -0.14 | 12.98 | -0.02 | 0.00 | 0.00 | BC 434 |
| | | | | Min $M_y$ | -0.82 | -0.02 | 18.75 | -0.00 | -0.00 | 0.00 | BC 304 |
| | | | | Max $M_z$ | -0.53 | -0.02 | 11.95 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.53 | -0.02 | 11.95 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | 163 | 3267 | Max N | 3.66 | -0.13 | 0.08 | -0.02 | 11.92 | 0.44 | BC 358 |
| | | | | Min N | -3.02 | -0.03 | 0.09 | 0.01 | 26.85 | 0.09 | BC 265 |
| | | | | Max $V_y$ | 1.24 | 0.12 | 0.08 | 0.02 | 11.91 | -0.39 | BC 472 |
| | | | | Min $V_y$ | 3.51 | -0.15 | 0.09 | -0.02 | 26.86 | 0.49 | BC 242 |
| | | | | Max $V_z$ | -0.09 | -0.02 | 0.13 | -0.00 | 19.73 | 0.06 | BC 17 |
| | | | | Min $V_z$ | -0.24 | -0.04 | -0.01 | -0.00 | 47.56 | 0.12 | BC 339 |
| | | | | Max $M_T$ | 1.25 | 0.12 | 0.08 | 0.02 | 11.91 | -0.39 | BC 412 |
| | | | | Min $M_T$ | 3.51 | -0.15 | 0.09 | -0.02 | 26.86 | 0.49 | BC 242 |
| | | | | Max $M_y$ | -0.21 | -0.04 | 0.03 | -0.00 | 53.13 | 0.13 | BC 138 |
| | | | | Min $M_y$ | 1.45 | 0.02 | 0.08 | 0.01 | 11.91 | -0.07 | BC 443 |
| | | | | Max $M_z$ | 3.51 | -0.15 | 0.09 | -0.02 | 26.86 | 0.49 | BC 242 |
| | | | | Min $M_z$ | 1.24 | 0.12 | 0.08 | 0.02 | 11.91 | -0.39 | BC 472 |
| 9 | RC1 | 48 | 0 | Max N | -46.00 | -0.16 | -17.65 | -0.00 | 0.00 | 0.00 | BC 414 |
| | | | | Min N | -253.15 | 0.05 | -1.74 | 0.02 | -0.00 | 0.00 | BC 146 |
| | | | | Max $V_y$ | -136.16 | 0.11 | 13.14 | 0.01 | 0.00 | 0.00 | BC 236 |
| | | | | Min $V_y$ | -46.00 | -0.16 | -17.65 | -0.00 | 0.00 | 0.00 | BC 414 |
| | | | | Max $V_z$ | -82.18 | 0.07 | 13.66 | 0.00 | 0.00 | 0.00 | BC 448 |
| | | | | Min $V_z$ | -116.73 | -0.15 | -17.93 | -0.00 | 0.00 | 0.00 | BC 206 |
| | | | | Max $M_T$ | -252.74 | 0.05 | -1.74 | 0.02 | -0.00 | 0.00 | BC 149 |
| | | | | Min $M_T$ | -58.01 | -0.12 | -17.60 | -0.00 | -0.00 | 0.00 | BC 390 |
| | | | | Max $M_y$ | -101.88 | 0.09 | 13.33 | 0.01 | 0.00 | -0.00 | BC 428 |
| | | | | Min $M_y$ | -77.12 | 0.08 | 13.64 | 0.00 | -0.00 | -0.00 | BC 356 |
| | | | | Max $M_z$ | -134.13 | 0.03 | -0.97 | 0.01 | 0.00 | 0.00 | BC 91 |
| | | | | Min $M_z$ | -101.82 | 0.09 | 13.33 | 0.01 | 0.00 | -0.00 | BC 432 |
| | | | 2500 | Max N | -44.01 | -0.16 | -6.55 | -0.00 | -30.25 | 0.41 | BC 414 |
| | | | Links | Min N | -250.22 | 0.05 | -1.74 | 0.02 | -4.34 | -0.12 | BC 146 |
| | | | | Max $V_y$ | -133.23 | 0.11 | 3.52 | 0.01 | 20.82 | -0.28 | BC 236 |
| | | | | Min $V_y$ | -44.01 | -0.16 | -6.55 | -0.00 | -30.25 | 0.41 | BC 414 |
| | | | | Max $V_z$ | -80.18 | 0.07 | 4.03 | 0.00 | 22.11 | -0.16 | BC 448 |
| | | | | Min $V_z$ | -113.80 | -0.15 | -6.84 | -0.00 | -30.96 | 0.38 | BC 206 |
| | | | | Max $M_T$ | -249.82 | 0.05 | -1.74 | 0.02 | -4.34 | -0.12 | BC 149 |
| | | | | Min $M_T$ | -56.02 | -0.12 | -6.50 | -0.00 | -30.13 | 0.31 | BC 390 |
| | | | | Max $M_y$ | -80.18 | 0.07 | 4.03 | 0.00 | 22.11 | -0.16 | BC 448 |
| | | | | Min $M_y$ | -113.80 | -0.15 | -6.84 | -0.00 | -30.96 | 0.38 | BC 206 |
| | | | | Max $M_z$ | -44.01 | -0.16 | -6.55 | -0.00 | -30.25 | 0.41 | BC 414 |
| | | | | Min $M_z$ | -133.23 | 0.11 | 3.52 | 0.01 | 20.82 | -0.28 | BC 236 |
| | | | 2500 | Max N | -44.01 | -0.16 | -6.55 | -0.00 | -30.25 | 0.41 | BC 414 |
| | | | Rechts | Min N | -250.22 | 0.05 | -1.74 | 0.02 | -4.34 | -0.12 | BC 146 |
| | | | | Max $V_y$ | -133.23 | 0.11 | 3.52 | 0.01 | 20.82 | -0.28 | BC 236 |
| | | | | Min $V_y$ | -44.01 | -0.16 | -6.55 | -0.00 | -30.25 | 0.41 | BC 414 |
| | | | | Max $V_z$ | -80.18 | 0.07 | 4.03 | 0.00 | 22.11 | -0.16 | BC 448 |
| | | | | Min $V_z$ | -113.80 | -0.15 | -6.84 | -0.00 | -30.96 | 0.38 | BC 206 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 9 | RC1 | | | Max $M_T$ | -249.82 | 0.05 | -1.74 | 0.02 | -4.34 | -0.12 | BC 149 |
| | | | | Min $M_T$ | -56.02 | -0.12 | -6.50 | -0.00 | -30.13 | 0.31 | BC 390 |
| | | | | Max $M_y$ | -80.18 | 0.07 | 4.03 | 0.00 | 22.11 | -0.16 | BC 448 |
| | | | | Min $M_y$ | -113.80 | -0.15 | -6.84 | -0.00 | -30.96 | 0.38 | BC 206 |
| | | | | Max $M_z$ | -44.01 | -0.16 | -6.55 | -0.00 | -30.25 | 0.41 | BC 414 |
| | | | | Min $M_z$ | -133.23 | 0.11 | 3.52 | 0.01 | 20.82 | -0.28 | BC 236 |
| | | | 4345 | Max N | -40.34 | -0.16 | 1.63 | -0.00 | -34.78 | 0.71 | BC 414 |
| | | | Links | Min N | -244.85 | 0.05 | -1.74 | 0.02 | -7.54 | -0.21 | BC 146 |
| | | | | Max $V_y$ | -127.86 | 0.11 | -3.58 | 0.01 | 20.76 | -0.49 | BC 236 |
| | | | | Min $V_y$ | -40.34 | -0.16 | 1.63 | -0.00 | -34.78 | 0.71 | BC 414 |
| | | | | Max $V_z$ | -120.39 | -0.04 | 1.71 | 0.01 | -19.97 | 0.19 | BC 451 |
| | | | | Min $V_z$ | -125.74 | 0.09 | -3.59 | 0.01 | 20.73 | -0.39 | BC 204 |
| | | | | Max $M_T$ | -244.44 | 0.05 | -1.74 | 0.02 | -7.55 | -0.22 | BC 149 |
| | | | | Min $M_T$ | -52.35 | -0.12 | 1.68 | -0.00 | -34.57 | 0.54 | BC 390 |
| | | | | Max $M_y$ | -76.52 | 0.07 | -3.07 | 0.00 | 23.00 | -0.28 | BC 448 |
| | | | | Min $M_y$ | -108.43 | -0.15 | 1.35 | -0.00 | -36.02 | 0.66 | BC 206 |
| | | | | Max $M_z$ | -40.34 | -0.16 | 1.63 | -0.00 | -34.78 | 0.71 | BC 414 |
| | | | | Min $M_z$ | -127.86 | 0.11 | -3.58 | 0.01 | 20.76 | -0.49 | BC 236 |
| | | 71 | 4345 | Max N | -40.34 | -0.16 | 1.64 | -0.00 | -34.78 | 0.71 | BC 414 |
| | | | Rechts | Min N | -244.85 | 0.05 | -1.74 | 0.02 | -7.55 | -0.21 | BC 146 |
| | | | | Max $V_y$ | -127.86 | 0.11 | -3.58 | 0.01 | 20.76 | -0.49 | BC 236 |
| | | | | Min $V_y$ | -40.34 | -0.16 | 1.64 | -0.00 | -34.78 | 0.71 | BC 414 |
| | | | | Max $V_z$ | -120.39 | -0.04 | 1.71 | 0.01 | -19.97 | 0.19 | BC 451 |
| | | | | Min $V_z$ | -125.74 | 0.09 | -3.59 | 0.01 | 20.73 | -0.39 | BC 204 |
| | | | | Max $M_T$ | -244.44 | 0.05 | -1.74 | 0.02 | -7.55 | -0.22 | BC 149 |
| | | | | Min $M_T$ | -52.35 | -0.12 | 1.68 | -0.00 | -34.57 | 0.54 | BC 390 |
| | | | | Max $M_y$ | -76.52 | 0.07 | -3.07 | 0.00 | 23.00 | -0.28 | BC 448 |
| | | | | Min $M_y$ | -108.43 | -0.15 | 1.35 | -0.00 | -36.02 | 0.66 | BC 206 |
| | | | | Max $M_z$ | -40.34 | -0.16 | 1.64 | -0.00 | -34.78 | 0.71 | BC 414 |
| | | | | Min $M_z$ | -127.86 | 0.11 | -3.58 | 0.01 | 20.76 | -0.49 | BC 236 |
| 10 | RC1 | 36 | 0 | Max N | -44.53 | -0.17 | 17.69 | 0.00 | 0.00 | 0.00 | BC 410 |
| | | | | Min N | -252.00 | 0.06 | 2.03 | -0.03 | 0.00 | -0.00 | BC 149 |
| | | | | Max $V_y$ | -238.20 | 0.11 | 2.07 | -0.03 | 0.00 | -0.00 | BC 147 |
| | | | | Min $V_y$ | -44.53 | -0.17 | 17.69 | 0.00 | 0.00 | 0.00 | BC 410 |
| | | | | Max $V_z$ | -114.84 | -0.16 | 18.02 | 0.00 | 0.00 | 0.00 | BC 206 |
| | | | | Min $V_z$ | -81.51 | 0.07 | -13.69 | -0.01 | -0.00 | 0.00 | BC 449 |
| | | | | Max $M_T$ | -44.53 | -0.17 | 17.69 | 0.00 | 0.00 | 0.00 | BC 410 |
| | | | | Min $M_T$ | -252.00 | 0.06 | 2.03 | -0.03 | 0.00 | -0.00 | BC 149 |
| | | | | Max $M_y$ | -70.19 | 0.04 | 9.66 | -0.00 | 0.00 | 0.00 | BC 356 |
| | | | | Min $M_y$ | -81.43 | 0.07 | -13.68 | -0.01 | -0.00 | 0.00 | BC 421 |
| | | | | Max $M_z$ | -131.91 | 0.04 | 10.29 | -0.01 | 0.00 | 0.00 | BC 268 |
| | | | | Min $M_z$ | -77.35 | 0.08 | -13.67 | -0.01 | 0.00 | -0.00 | BC 353 |
| | | | 2500 | Max N | -42.53 | -0.17 | 6.59 | 0.00 | 30.35 | 0.42 | BC 410 |
| | | | Links | Min N | -249.08 | 0.06 | 2.03 | -0.03 | 5.08 | -0.14 | BC 149 |
| | | | | Max $V_y$ | -235.28 | 0.11 | 2.07 | -0.03 | 5.17 | -0.27 | BC 147 |
| | | | | Min $V_y$ | -42.53 | -0.17 | 6.59 | 0.00 | 30.35 | 0.42 | BC 410 |
| | | | | Max $V_z$ | -111.91 | -0.16 | 6.93 | 0.00 | 31.19 | 0.39 | BC 206 |
| | | | | Min $V_z$ | -79.51 | 0.07 | -4.06 | -0.01 | -22.18 | -0.17 | BC 449 |
| | | | | Max $M_T$ | -42.53 | -0.17 | 6.59 | 0.00 | 30.35 | 0.42 | BC 410 |
| | | | | Min $M_T$ | -249.08 | 0.06 | 2.03 | -0.03 | 5.08 | -0.14 | BC 149 |
| | | | | Max $M_y$ | -111.91 | -0.16 | 6.93 | 0.00 | 31.19 | 0.39 | BC 206 |
| | | | | Min $M_y$ | -79.51 | 0.07 | -4.06 | -0.01 | -22.18 | -0.17 | BC 449 |
| | | | | Max $M_z$ | -42.53 | -0.17 | 6.59 | 0.00 | 30.35 | 0.42 | BC 410 |
| | | | | Min $M_z$ | -235.28 | 0.11 | 2.07 | -0.03 | 5.17 | -0.27 | BC 147 |
| | | | 2500 | Max N | -42.53 | -0.17 | 6.59 | 0.00 | 30.35 | 0.42 | BC 410 |
| | | | Rechts | Min N | -249.08 | 0.06 | 2.03 | -0.03 | 5.08 | -0.14 | BC 149 |
| | | | | Max $V_y$ | -235.28 | 0.11 | 2.07 | -0.03 | 5.17 | -0.27 | BC 147 |
| | | | | Min $V_y$ | -42.53 | -0.17 | 6.59 | 0.00 | 30.35 | 0.42 | BC 410 |
| | | | | Max $V_z$ | -111.91 | -0.16 | 6.93 | 0.00 | 31.19 | 0.39 | BC 206 |
| | | | | Min $V_z$ | -79.51 | 0.07 | -4.06 | -0.01 | -22.18 | -0.17 | BC 449 |
| | | | | Max $M_T$ | -42.53 | -0.17 | 6.59 | 0.00 | 30.35 | 0.42 | BC 410 |
| | | | | Min $M_T$ | -249.08 | 0.06 | 2.03 | -0.03 | 5.08 | -0.14 | BC 149 |
| | | | | Max $M_y$ | -111.91 | -0.16 | 6.93 | 0.00 | 31.19 | 0.39 | BC 206 |
| | | | | Min $M_y$ | -79.51 | 0.07 | -4.06 | -0.01 | -22.18 | -0.17 | BC 449 |
| | | | | Max $M_z$ | -42.53 | -0.17 | 6.59 | 0.00 | 30.35 | 0.42 | BC 410 |
| | | | | Min $M_z$ | -235.28 | 0.11 | 2.07 | -0.03 | 5.17 | -0.27 | BC 147 |
| | | | 4345 | Max N | -38.87 | -0.17 | -1.59 | 0.00 | 34.96 | 0.73 | BC 410 |
| | | | Links | Min N | -243.70 | 0.06 | 2.03 | -0.03 | 8.83 | -0.24 | BC 149 |
| | | | | Max $V_y$ | -229.90 | 0.11 | 2.07 | -0.03 | 8.98 | -0.47 | BC 147 |
| | | | | Min $V_y$ | -38.87 | -0.17 | -1.59 | 0.00 | 34.96 | 0.73 | BC 410 |
| | | | | Max $V_z$ | -125.23 | 0.08 | 3.64 | -0.02 | -20.51 | -0.34 | BC 205 |
| | | | | Min $V_z$ | -50.72 | -0.13 | -1.64 | 0.00 | 34.74 | 0.57 | BC 450 |
| | | | | Max $M_T$ | -38.87 | -0.17 | -1.59 | 0.00 | 34.96 | 0.73 | BC 410 |
| | | | | Min $M_T$ | -243.70 | 0.06 | 2.03 | -0.03 | 8.83 | -0.24 | BC 149 |
| | | | | Max $M_y$ | -106.54 | -0.16 | -1.26 | 0.00 | 36.43 | 0.68 | BC 206 |
| | | | | Min $M_y$ | -75.85 | 0.07 | 3.04 | -0.01 | -23.13 | -0.30 | BC 449 |
| | | | | Max $M_z$ | -38.87 | -0.17 | -1.59 | 0.00 | 34.96 | 0.73 | BC 410 |
| | | | | Min $M_z$ | -229.90 | 0.11 | 2.07 | -0.03 | 8.98 | -0.47 | BC 147 |
| | | 75 | 4345 | Max N | -38.87 | -0.17 | -1.59 | 0.00 | 34.96 | 0.73 | BC 410 |
| | | | Rechts | Min N | -243.70 | 0.06 | 2.03 | -0.03 | 8.83 | -0.24 | BC 149 |
| | | | | Max $V_y$ | -229.90 | 0.11 | 2.07 | -0.03 | 8.98 | -0.47 | BC 147 |
| | | | | Min $V_y$ | -38.87 | -0.17 | -1.59 | 0.00 | 34.96 | 0.73 | BC 410 |
| | | | | Max $V_z$ | -125.23 | 0.08 | 3.64 | -0.02 | -20.51 | -0.34 | BC 205 |
| | | | | Min $V_z$ | -50.72 | -0.13 | -1.64 | 0.00 | 34.74 | 0.57 | BC 450 |
| | | | | Max $M_T$ | -38.87 | -0.17 | -1.59 | 0.00 | 34.96 | 0.73 | BC 410 |
| | | | | Min $M_T$ | -243.70 | 0.06 | 2.03 | -0.03 | 8.83 | -0.24 | BC 149 |
| | | | | Max $M_y$ | -106.54 | -0.16 | -1.26 | 0.00 | 36.43 | 0.68 | BC 206 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 10 | RC1 | | | Min $M_y$ | -75.85 | 0.07 | 3.04 | -0.01 | -23.13 | -0.30 | BC 449 |
| | | | | Max $M_z$ | -38.87 | -0.17 | -1.59 | 0.00 | 34.96 | 0.73 | BC 410 |
| | | | | Min $M_z$ | -229.90 | 0.11 | 2.07 | -0.03 | 8.98 | -0.47 | BC 147 |
| 11 | RC1 | 49 | 0 | Max N | 11.37 | 0.02 | 54.72 | 0.68 | -0.00 | 0.00 | BC 451 |
| | | | | Min N | -53.56 | -0.16 | 115.11 | 0.48 | -0.00 | 0.00 | BC 204 |
| | | | | Max $V_y$ | -3.70 | 0.04 | 53.24 | -0.01 | 0.00 | 0.00 | BC 449 |
| | | | | Min $V_y$ | -52.26 | -0.20 | 213.05 | 0.94 | -0.00 | 0.00 | BC 148 |
| | | | | Max $V_z$ | -50.92 | -0.19 | 213.08 | 0.95 | -0.00 | 0.00 | BC 149 |
| | | | | Min $V_z$ | -5.09 | 0.03 | 53.21 | -0.02 | -0.00 | 0.00 | BC 413 |
| | | | | Max $M_T$ | -50.92 | -0.19 | 213.08 | 0.95 | -0.00 | 0.00 | BC 149 |
| | | | | Min $M_T$ | -12.41 | -0.03 | 53.76 | -0.06 | 0.00 | 0.00 | BC 474 |
| | | | | Max $M_y$ | -15.69 | 0.02 | 88.97 | -0.04 | 0.00 | 0.00 | BC 426 |
| | | | | Min $M_y$ | -52.43 | -0.20 | 213.04 | 0.94 | -0.00 | 0.00 | BC 140 |
| | | | | Max $M_z$ | -20.63 | -0.08 | 89.33 | 0.40 | -0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -45.46 | -0.17 | 184.85 | 0.81 | -0.00 | -0.00 | BC 115 |
| | | 149 | 3201 | Max N | 11.68 | 0.02 | 38.07 | 0.68 | 148.49 | -0.05 | BC 451 |
| | | | | Min N | -52.88 | -0.16 | 79.08 | 0.48 | 310.75 | 0.53 | BC 204 |
| | | | | Max $V_y$ | -3.39 | 0.04 | 36.59 | -0.01 | 143.76 | -0.12 | BC 449 |
| | | | | Min $V_y$ | -50.98 | -0.20 | 144.50 | 0.94 | 572.17 | 0.63 | BC 148 |
| | | | | Max $V_z$ | -49.63 | -0.19 | 144.53 | 0.95 | 572.26 | 0.62 | BC 149 |
| | | | | Min $V_z$ | -4.78 | 0.03 | 36.56 | -0.02 | 143.66 | -0.11 | BC 413 |
| | | | | Max $M_T$ | -49.63 | -0.19 | 144.53 | 0.95 | 572.26 | 0.62 | BC 149 |
| | | | | Min $M_T$ | -12.10 | -0.03 | 37.11 | -0.06 | 145.41 | 0.11 | BC 474 |
| | | | | Max $M_y$ | -49.63 | -0.19 | 144.53 | 0.95 | 572.26 | 0.62 | BC 149 |
| | | | | Min $M_y$ | -4.78 | 0.03 | 36.56 | -0.02 | 143.66 | -0.11 | BC 413 |
| | | | | Max $M_z$ | -50.98 | -0.20 | 144.50 | 0.94 | 572.17 | 0.63 | BC 148 |
| | | | | Min $M_z$ | -3.39 | 0.04 | 36.59 | -0.01 | 143.76 | -0.12 | BC 449 |
| 12 | RC1 | 37 | 0 | Max N | 8.09 | 0.14 | 55.51 | -0.57 | 0.00 | 0.00 | BC 451 |
| | | | | Min N | -59.73 | 0.32 | 213.01 | -0.77 | -0.00 | 0.00 | BC 139 |
| | | | | Max $V_y$ | -58.96 | 0.33 | 213.08 | -0.77 | -0.00 | 0.00 | BC 138 |
| | | | | Min $V_y$ | -22.56 | -0.11 | 113.72 | 0.03 | 0.00 | 0.00 | BC 242 |
| | | | | Max $V_z$ | -58.46 | 0.32 | 213.09 | -0.78 | -0.00 | 0.00 | BC 149 |
| | | | | Min $V_z$ | -13.34 | -0.07 | 53.51 | 0.05 | -0.00 | 0.00 | BC 410 |
| | | | | Max $M_T$ | -13.34 | -0.07 | 53.51 | 0.05 | -0.00 | 0.00 | BC 410 |
| | | | | Min $M_T$ | -58.46 | 0.32 | 213.09 | -0.78 | -0.00 | 0.00 | BC 149 |
| | | | | Max $M_y$ | -15.93 | -0.09 | 78.64 | 0.04 | 0.00 | 0.00 | BC 162 |
| | | | | Min $M_y$ | -59.44 | 0.33 | 213.02 | -0.77 | -0.00 | 0.00 | BC 133 |
| | | | | Max $M_z$ | -15.93 | -0.09 | 78.64 | 0.04 | 0.00 | 0.00 | BC 162 |
| | | | | Min $M_z$ | -37.93 | 0.09 | 53.76 | -0.15 | 0.00 | -0.00 | BC 381 |
| | | 162 | 3267 | Max N | 8.72 | 0.14 | 38.53 | -0.57 | 153.61 | -0.47 | BC 451 |
| | | | | Min N | -57.13 | 0.32 | 143.10 | -0.77 | 581.76 | -1.06 | BC 139 |
| | | | | Max $V_y$ | -56.36 | 0.33 | 143.17 | -0.77 | 581.96 | -1.07 | BC 138 |
| | | | | Min $V_y$ | -21.19 | -0.11 | 76.98 | 0.03 | 311.53 | 0.37 | BC 242 |
| | | | | Max $V_z$ | -55.86 | 0.32 | 143.18 | -0.78 | 582.02 | -1.05 | BC 149 |
| | | | | Min $V_z$ | -12.71 | -0.07 | 36.53 | 0.05 | 147.10 | 0.24 | BC 410 |
| | | | | Max $M_T$ | -12.71 | -0.07 | 36.53 | 0.05 | 147.10 | 0.24 | BC 410 |
| | | | | Min $M_T$ | -55.86 | 0.32 | 143.18 | -0.78 | 582.02 | -1.05 | BC 149 |
| | | | | Max $M_y$ | -55.86 | 0.32 | 143.18 | -0.78 | 582.02 | -1.05 | BC 149 |
| | | | | Min $M_y$ | -12.71 | -0.07 | 36.53 | 0.05 | 147.10 | 0.24 | BC 410 |
| | | | | Max $M_z$ | -21.19 | -0.11 | 76.98 | 0.03 | 311.53 | 0.37 | BC 242 |
| | | | | Min $M_z$ | -56.36 | 0.33 | 143.17 | -0.77 | 581.96 | -1.07 | BC 138 |
| 13 | RC1 | 50 | 0 | Max N | -50.85 | 0.09 | -15.67 | -0.00 | 0.00 | 0.00 | BC 451 |
| | | | | Min N | -247.28 | -0.08 | -1.71 | -0.02 | 0.00 | 0.00 | BC 140 |
| | | | | Max $V_y$ | -117.86 | 0.09 | -15.97 | -0.00 | -0.00 | 0.00 | BC 235 |
| | | | | Min $V_y$ | -245.67 | -0.09 | -1.71 | -0.02 | 0.00 | 0.00 | BC 154 |
| | | | | Max $V_z$ | -90.25 | 0.05 | 14.09 | -0.00 | 0.00 | 0.00 | BC 408 |
| | | | | Min $V_z$ | -118.01 | 0.09 | -15.97 | -0.00 | 0.00 | 0.00 | BC 247 |
| | | | | Max $M_T$ | -70.66 | 0.02 | 14.06 | -0.00 | -0.00 | 0.00 | BC 360 |
| | | | | Min $M_T$ | -247.28 | -0.08 | -1.71 | -0.02 | 0.00 | 0.00 | BC 140 |
| | | | | Max $M_y$ | -115.89 | 0.03 | 13.88 | -0.00 | 0.00 | 0.00 | BC 252 |
| | | | | Min $M_y$ | -70.66 | 0.02 | 14.06 | -0.00 | -0.00 | 0.00 | BC 360 |
| | | | | Max $M_z$ | -152.61 | -0.02 | -0.90 | -0.01 | -0.00 | 0.00 | BC 91 |
| | | | | Min $M_z$ | -115.84 | 0.02 | 13.80 | -0.00 | 0.00 | -0.00 | BC 432 |
| | | | 2500 | Max N | -48.85 | 0.09 | -5.89 | -0.00 | -26.95 | -0.21 | BC 451 |
| | | | Links | Min N | -244.35 | -0.08 | -1.71 | -0.02 | -4.28 | 0.20 | BC 140 |
| | | | | Max $V_y$ | -114.94 | 0.09 | -6.19 | -0.00 | -27.70 | -0.23 | BC 235 |
| | | | | Min $V_y$ | -242.75 | -0.09 | -1.71 | -0.02 | -4.27 | 0.21 | BC 154 |
| | | | | Max $V_z$ | -88.25 | 0.05 | 4.25 | -0.00 | 22.93 | -0.13 | BC 408 |
| | | | | Min $V_z$ | -115.09 | 0.09 | -6.19 | -0.00 | -27.70 | -0.23 | BC 247 |
| | | | | Max $M_T$ | -68.66 | 0.02 | 4.21 | -0.00 | 22.84 | -0.05 | BC 360 |
| | | | | Min $M_T$ | -244.35 | -0.08 | -1.71 | -0.02 | -4.28 | 0.20 | BC 140 |
| | | | | Max $M_y$ | -88.25 | 0.05 | 4.25 | -0.00 | 22.93 | -0.13 | BC 408 |
| | | | | Min $M_y$ | -115.09 | 0.09 | -6.19 | -0.00 | -27.70 | -0.23 | BC 247 |
| | | | | Max $M_z$ | -242.75 | -0.09 | -1.71 | -0.02 | -4.27 | 0.21 | BC 154 |
| | | | | Min $M_z$ | -114.94 | 0.09 | -6.19 | -0.00 | -27.70 | -0.23 | BC 235 |
| | | | 2500 | Max N | -48.85 | 0.09 | -5.89 | -0.00 | -26.95 | -0.21 | BC 451 |
| | | | Rechts | Min N | -244.35 | -0.08 | -1.71 | -0.02 | -4.28 | 0.20 | BC 140 |
| | | | | Max $V_y$ | -114.94 | 0.09 | -6.19 | -0.00 | -27.70 | -0.23 | BC 235 |
| | | | | Min $V_y$ | -242.75 | -0.09 | -1.71 | -0.02 | -4.27 | 0.21 | BC 154 |
| | | | | Max $V_z$ | -88.25 | 0.05 | 4.25 | -0.00 | 22.93 | -0.13 | BC 408 |
| | | | | Min $V_z$ | -115.09 | 0.09 | -6.19 | -0.00 | -27.70 | -0.23 | BC 247 |
| | | | | Max $M_T$ | -68.66 | 0.02 | 4.21 | -0.00 | 22.84 | -0.05 | BC 360 |
| | | | | Min $M_T$ | -244.35 | -0.08 | -1.71 | -0.02 | -4.28 | 0.20 | BC 140 |
| | | | | Max $M_y$ | -88.25 | 0.05 | 4.25 | -0.00 | 22.93 | -0.13 | BC 408 |
| | | | | Min $M_y$ | -115.09 | 0.09 | -6.19 | -0.00 | -27.70 | -0.23 | BC 247 |
| | | | | Max $M_z$ | -242.75 | -0.09 | -1.71 | -0.02 | -4.27 | 0.21 | BC 154 |
| | | | | Min $M_z$ | -114.94 | 0.09 | -6.19 | -0.00 | -27.70 | -0.23 | BC 235 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 13 | RC1 | | 4345 | Max N | -45.14 | 0.09 | 1.33 | -0.00 | -31.16 | -0.37 | BC 451 |
| | | | Links | Min N | -238.91 | -0.08 | -1.71 | -0.02 | -7.44 | 0.34 | BC 140 |
| | | | | Max $V_y$ | -109.49 | 0.09 | 1.03 | -0.00 | -32.46 | -0.40 | BC 235 |
| | | | | Min $V_y$ | -237.30 | -0.09 | -1.71 | -0.02 | -7.43 | 0.37 | BC 154 |
| | | | | Max $V_z$ | -134.83 | 0.02 | 2.33 | -0.01 | -27.02 | -0.09 | BC 410 |
| | | | | Min $V_z$ | -130.20 | 0.01 | -3.53 | -0.01 | 21.81 | -0.03 | BC 244 |
| | | | | Max $M_T$ | -64.95 | 0.02 | -3.05 | -0.00 | 23.91 | -0.08 | BC 360 |
| | | | | Min $M_T$ | -238.91 | -0.08 | -1.71 | -0.02 | -7.44 | 0.34 | BC 140 |
| | | | | Max $M_y$ | -84.54 | 0.05 | -3.01 | -0.00 | 24.07 | -0.23 | BC 408 |
| | | | | Min $M_y$ | -109.64 | 0.09 | 1.03 | -0.00 | -32.46 | -0.40 | BC 247 |
| | | | | Max $M_z$ | -237.30 | -0.09 | -1.71 | -0.02 | -7.43 | 0.37 | BC 154 |
| | | | | Min $M_z$ | -109.49 | 0.09 | 1.03 | -0.00 | -32.46 | -0.40 | BC 235 |
| | | 72 | 4345 | Max N | -45.14 | 0.09 | 1.33 | -0.00 | -31.16 | -0.37 | BC 451 |
| | | | Rechts | Min N | -238.91 | -0.08 | -1.71 | -0.02 | -7.44 | 0.34 | BC 140 |
| | | | | Max $V_y$ | -109.49 | 0.09 | 1.03 | -0.00 | -32.46 | -0.40 | BC 235 |
| | | | | Min $V_y$ | -237.30 | -0.09 | -1.71 | -0.02 | -7.43 | 0.37 | BC 154 |
| | | | | Max $V_z$ | -134.83 | 0.02 | 2.33 | -0.01 | -27.02 | -0.09 | BC 410 |
| | | | | Min $V_z$ | -130.20 | 0.01 | -3.53 | -0.01 | 21.81 | -0.03 | BC 244 |
| | | | | Max $M_T$ | -64.95 | 0.02 | -3.05 | -0.00 | 23.91 | -0.08 | BC 360 |
| | | | | Min $M_T$ | -238.91 | -0.08 | -1.71 | -0.02 | -7.44 | 0.34 | BC 140 |
| | | | | Max $M_y$ | -84.54 | 0.05 | -3.01 | -0.00 | 24.07 | -0.23 | BC 408 |
| | | | | Min $M_y$ | -109.64 | 0.09 | 1.03 | -0.00 | -32.46 | -0.40 | BC 247 |
| | | | | Max $M_z$ | -237.30 | -0.09 | -1.71 | -0.02 | -7.43 | 0.37 | BC 154 |
| | | | | Min $M_z$ | -109.49 | 0.09 | 1.03 | -0.00 | -32.46 | -0.40 | BC 235 |
| 14 | RC1 | 60 | 0 | Max N | -50.92 | 0.08 | 17.76 | 0.00 | -0.00 | 0.00 | BC 423 |
| | | | Links | Min N | -244.65 | -0.06 | 1.98 | 0.03 | 0.00 | 0.00 | BC 139 |
| | | | | Max $V_y$ | -84.22 | 0.08 | 17.91 | 0.01 | -0.00 | 0.00 | BC 231 |
| | | | | Min $V_y$ | -211.55 | -0.06 | 1.74 | 0.03 | 0.00 | 0.00 | BC 332 |
| | | | | Max $V_z$ | -119.01 | 0.08 | 18.10 | 0.01 | -0.00 | 0.00 | BC 235 |
| | | | | Min $V_z$ | -87.80 | 0.03 | -14.07 | 0.01 | -0.00 | 0.00 | BC 473 |
| | | | | Max $M_T$ | -238.56 | -0.04 | 2.01 | 0.03 | -0.00 | 0.00 | BC 134 |
| | | | | Min $M_T$ | -95.49 | 0.08 | 10.17 | -0.02 | -0.00 | 0.00 | BC 408 |
| | | | | Max $M_y$ | -156.81 | 0.04 | 10.76 | -0.01 | 0.00 | 0.00 | BC 264 |
| | | | | Min $M_y$ | -174.79 | 0.01 | 14.96 | 0.03 | -0.00 | 0.00 | BC 278 |
| | | | | Max $M_z$ | -156.77 | 0.04 | 10.75 | -0.01 | 0.00 | 0.00 | BC 268 |
| | | | | Min $M_z$ | -143.32 | -0.02 | 1.18 | 0.02 | -0.00 | -0.00 | BC 289 |
| | | | 0 | Max N | -50.92 | 0.08 | 17.76 | 0.00 | 0.00 | -0.00 | BC 423 |
| | | | Rechts | Min N | -244.65 | -0.06 | 1.98 | 0.03 | 0.00 | 0.00 | BC 139 |
| | | | | Max $V_y$ | -84.22 | 0.08 | 17.91 | 0.01 | 0.00 | -0.00 | BC 231 |
| | | | | Min $V_y$ | -211.55 | -0.06 | 1.74 | 0.03 | 0.00 | 0.00 | BC 332 |
| | | | | Max $V_z$ | -119.01 | 0.08 | 18.10 | 0.01 | 0.00 | -0.00 | BC 235 |
| | | | | Min $V_z$ | -87.80 | 0.03 | -14.07 | 0.01 | -0.00 | -0.00 | BC 473 |
| | | | | Max $M_T$ | -238.56 | -0.04 | 2.01 | 0.03 | 0.00 | 0.00 | BC 134 |
| | | | | Min $M_T$ | -95.49 | 0.08 | 10.17 | -0.02 | 0.00 | -0.00 | BC 408 |
| | | | | Max $M_y$ | -119.58 | 0.08 | 18.10 | 0.01 | 0.00 | -0.00 | BC 175 |
| | | | | Min $M_y$ | -72.30 | 0.01 | -14.04 | 0.01 | -0.00 | -0.00 | BC 353 |
| | | | | Max $M_z$ | -211.55 | -0.06 | 1.74 | 0.03 | 0.00 | 0.00 | BC 332 |
| | | | | Min $M_z$ | -84.22 | 0.08 | 17.91 | 0.01 | 0.00 | -0.00 | BC 231 |
| | | | 2500 | Max N | -48.92 | 0.08 | 6.61 | 0.00 | 30.44 | -0.20 | BC 423 |
| | | | Links | Min N | -241.72 | -0.06 | 1.98 | 0.03 | 4.96 | 0.14 | BC 139 |
| | | | | Max $V_y$ | -81.29 | 0.08 | 6.76 | 0.01 | 30.82 | -0.20 | BC 231 |
| | | | | Min $V_y$ | -209.55 | -0.06 | 1.74 | 0.03 | 4.35 | 0.16 | BC 332 |
| | | | | Max $V_z$ | -116.08 | 0.08 | 6.95 | 0.01 | 31.29 | -0.20 | BC 235 |
| | | | | Min $V_z$ | -85.80 | 0.03 | -4.11 | 0.01 | -22.71 | -0.07 | BC 473 |
| | | | | Max $M_T$ | -235.63 | -0.04 | 2.01 | 0.03 | 5.02 | 0.10 | BC 134 |
| | | | | Min $M_T$ | -93.50 | 0.08 | 3.94 | -0.02 | 17.63 | -0.19 | BC 408 |
| | | | | Max $M_y$ | -116.08 | 0.08 | 6.95 | 0.01 | 31.29 | -0.20 | BC 235 |
| | | | | Min $M_y$ | -85.80 | 0.03 | -4.11 | 0.01 | -22.71 | -0.07 | BC 473 |
| | | | | Max $M_z$ | -209.55 | -0.06 | 1.74 | 0.03 | 4.35 | 0.16 | BC 332 |
| | | | | Min $M_z$ | -81.29 | 0.08 | 6.76 | 0.01 | 30.82 | -0.20 | BC 231 |
| | | | 2500 | Max N | -48.92 | 0.08 | 6.61 | 0.00 | 30.44 | -0.20 | BC 423 |
| | | | Rechts | Min N | -241.72 | -0.06 | 1.98 | 0.03 | 4.96 | 0.14 | BC 139 |
| | | | | Max $V_y$ | -81.29 | 0.08 | 6.76 | 0.01 | 30.82 | -0.20 | BC 231 |
| | | | | Min $V_y$ | -209.55 | -0.06 | 1.74 | 0.03 | 4.35 | 0.16 | BC 332 |
| | | | | Max $V_z$ | -116.08 | 0.08 | 6.95 | 0.01 | 31.29 | -0.20 | BC 235 |
| | | | | Min $V_z$ | -85.80 | 0.03 | -4.11 | 0.01 | -22.71 | -0.07 | BC 473 |
| | | | | Max $M_T$ | -235.63 | -0.04 | 2.01 | 0.03 | 5.02 | 0.10 | BC 134 |
| | | | | Min $M_T$ | -93.50 | 0.08 | 3.94 | -0.02 | 17.63 | -0.19 | BC 408 |
| | | | | Max $M_y$ | -116.08 | 0.08 | 6.95 | 0.01 | 31.29 | -0.20 | BC 235 |
| | | | | Min $M_y$ | -85.80 | 0.03 | -4.11 | 0.01 | -22.71 | -0.07 | BC 473 |
| | | | | Max $M_z$ | -209.55 | -0.06 | 1.74 | 0.03 | 4.35 | 0.16 | BC 332 |
| | | | | Min $M_z$ | -81.29 | 0.08 | 6.76 | 0.01 | 30.82 | -0.20 | BC 231 |
| | | | 4345 | Max N | -45.21 | 0.08 | -1.54 | 0.00 | 35.11 | -0.35 | BC 423 |
| | | | Links | Min N | -236.28 | -0.06 | 1.98 | 0.03 | 8.62 | 0.25 | BC 139 |
| | | | | Max $V_y$ | -75.84 | 0.08 | -1.39 | 0.01 | 35.76 | -0.35 | BC 231 |
| | | | | Min $V_y$ | -205.84 | -0.06 | 1.74 | 0.03 | 7.57 | 0.28 | BC 332 |
| | | | | Max $V_z$ | -133.06 | -0.00 | 3.75 | 0.02 | -21.04 | 0.01 | BC 201 |
| | | | | Min $V_z$ | -138.18 | 0.03 | -2.32 | 0.03 | 27.23 | -0.12 | BC 414 |
| | | | | Max $M_T$ | -230.18 | -0.04 | 2.01 | 0.03 | 8.72 | 0.17 | BC 134 |
| | | | | Min $M_T$ | -89.78 | 0.08 | -0.60 | -0.02 | 20.70 | -0.33 | BC 408 |
| | | | | Max $M_y$ | -110.63 | 0.08 | -1.20 | 0.01 | 36.59 | -0.35 | BC 235 |
| | | | | Min $M_y$ | -82.09 | 0.03 | 3.16 | 0.01 | -23.58 | -0.13 | BC 473 |
| | | | | Max $M_z$ | -205.84 | -0.06 | 1.74 | 0.03 | 7.57 | 0.28 | BC 332 |
| | | | | Min $M_z$ | -75.84 | 0.08 | -1.39 | 0.01 | 35.76 | -0.35 | BC 231 |
| | | 76 | 4345 | Max N | -45.21 | 0.08 | -1.54 | 0.00 | 35.11 | -0.35 | BC 423 |
| | | | Rechts | Min N | -236.27 | -0.06 | 1.98 | 0.03 | 8.62 | 0.25 | BC 139 |
| | | | | Max $V_y$ | -75.84 | 0.08 | -1.39 | 0.01 | 35.76 | -0.35 | BC 231 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 14 | RC1 | | | Min $V_y$ | -205.84 | -0.06 | 1.74 | 0.03 | 7.57 | 0.28 | BC 332 |
| | | | | Max $V_z$ | -133.06 | -0.00 | 3.75 | 0.02 | -21.04 | 0.01 | BC 201 |
| | | | | Min $V_z$ | -138.18 | 0.03 | -2.32 | 0.03 | 27.23 | -0.12 | BC 414 |
| | | | | Max $M_T$ | -230.18 | -0.04 | 2.01 | 0.03 | 8.72 | 0.17 | BC 134 |
| | | | | Min $M_T$ | -89.78 | 0.08 | -0.60 | -0.02 | 20.70 | -0.33 | BC 408 |
| | | | | Max $M_y$ | -110.63 | 0.08 | -1.20 | 0.01 | 36.59 | -0.35 | BC 235 |
| | | | | Min $M_y$ | -82.09 | 0.03 | 3.16 | 0.01 | -23.58 | -0.13 | BC 473 |
| | | | | Max $M_z$ | -205.84 | -0.06 | 1.74 | 0.03 | 7.57 | 0.28 | BC 332 |
| | | | | Min $M_z$ | -75.84 | 0.08 | -1.39 | 0.01 | 35.76 | -0.35 | BC 231 |
| 15 | RC1 | 51 | 0 | Max N | 15.65 | 0.02 | 55.85 | -0.70 | 0.00 | 0.00 | BC 410 |
| | | | | Min N | -50.84 | 0.20 | 217.68 | -0.98 | 0.00 | 0.00 | BC 134 |
| | | | | Max $V_y$ | -50.18 | 0.21 | 217.72 | -0.98 | 0.00 | 0.00 | BC 132 |
| | | | | Min $V_y$ | -12.30 | 0.01 | 54.40 | -0.03 | 0.00 | 0.00 | BC 409 |
| | | | | Max $V_z$ | -50.13 | 0.21 | 217.72 | -0.99 | 0.00 | 0.00 | BC 140 |
| | | | | Min $V_z$ | -13.48 | 0.02 | 54.36 | -0.03 | -0.00 | 0.00 | BC 421 |
| | | | | Max $M_T$ | -13.64 | 0.12 | 54.74 | 0.02 | -0.00 | 0.00 | BC 359 |
| | | | | Min $M_T$ | -50.13 | 0.21 | 217.72 | -0.99 | 0.00 | 0.00 | BC 140 |
| | | | | Max $M_y$ | 14.66 | 0.08 | 91.96 | -0.72 | 0.00 | -0.00 | BC 406 |
| | | | | Min $M_y$ | -12.51 | 0.01 | 54.39 | -0.03 | -0.00 | 0.00 | BC 381 |
| | | | | Max $M_z$ | -21.05 | 0.08 | 91.00 | -0.40 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 14.65 | 0.08 | 91.96 | -0.72 | 0.00 | -0.00 | BC 378 |
| | | 148 | 3201 | Max N | 15.97 | 0.02 | 38.95 | -0.70 | 151.70 | -0.05 | BC 410 |
| | | | | Min N | -49.93 | 0.13 | 80.33 | -0.27 | 315.77 | -0.43 | BC 244 |
| | | | | Max $V_y$ | -48.87 | 0.21 | 147.81 | -0.98 | 584.94 | -0.68 | BC 132 |
| | | | | Min $V_y$ | -11.99 | 0.01 | 37.50 | -0.03 | 147.06 | -0.02 | BC 409 |
| | | | | Max $V_z$ | -48.82 | 0.21 | 147.81 | -0.99 | 584.95 | -0.68 | BC 140 |
| | | | | Min $V_z$ | -13.16 | 0.02 | 37.47 | -0.03 | 146.95 | -0.06 | BC 421 |
| | | | | Max $M_T$ | -13.32 | 0.12 | 37.85 | 0.02 | 148.18 | -0.39 | BC 359 |
| | | | | Min $M_T$ | -48.82 | 0.21 | 147.81 | -0.99 | 584.95 | -0.68 | BC 140 |
| | | | | Max $M_y$ | -48.82 | 0.21 | 147.81 | -0.99 | 584.95 | -0.68 | BC 140 |
| | | | | Min $M_y$ | -13.16 | 0.02 | 37.47 | -0.03 | 146.95 | -0.06 | BC 421 |
| | | | | Max $M_z$ | -11.99 | 0.01 | 37.50 | -0.03 | 147.06 | -0.02 | BC 409 |
| | | | | Min $M_z$ | -48.87 | 0.21 | 147.81 | -0.98 | 584.94 | -0.68 | BC 132 |
| 16 | RC1 | 61 | 0 | Max N | 14.35 | -0.18 | 56.63 | 0.61 | 0.00 | 0.00 | BC 414 |
| | | | | Min N | -57.70 | -0.21 | 216.63 | 0.83 | -0.00 | 0.00 | BC 146 |
| | | | | Max $V_y$ | -16.29 | 0.29 | 54.78 | -0.47 | -0.00 | 0.00 | BC 408 |
| | | | | Min $V_y$ | 11.50 | -0.22 | 118.30 | 0.63 | 0.00 | 0.00 | BC 242 |
| | | | | Max $V_z$ | -56.92 | -0.21 | 216.70 | 0.82 | 0.00 | 0.00 | BC 139 |
| | | | | Min $V_z$ | -15.81 | -0.10 | 54.46 | 0.06 | -0.00 | 0.00 | BC 423 |
| | | | | Max $M_T$ | -57.64 | -0.21 | 216.63 | 0.83 | -0.00 | 0.00 | BC 134 |
| | | | | Min $M_T$ | -17.59 | 0.29 | 54.71 | -0.47 | 0.00 | 0.00 | BC 356 |
| | | | | Max $M_y$ | 12.67 | -0.21 | 92.51 | 0.61 | 0.00 | 0.00 | BC 466 |
| | | | | Min $M_y$ | -38.41 | -0.07 | 54.66 | 0.19 | -0.00 | 0.00 | BC 381 |
| | | | | Max $M_z$ | 13.13 | -0.20 | 82.32 | 0.61 | 0.00 | 0.00 | BC 162 |
| | | | | Min $M_z$ | -25.44 | -0.09 | 90.96 | 0.35 | -0.00 | 0.00 | BC 1 |
| | | 161 | 3267 | Max N | 14.98 | -0.18 | 39.65 | 0.61 | 157.27 | 0.59 | BC 414 |
| | | | | Min N | -55.10 | -0.21 | 146.72 | 0.83 | 593.59 | 0.67 | BC 146 |
| | | | | Max $V_y$ | -15.66 | 0.29 | 37.80 | -0.47 | 151.25 | -0.95 | BC 408 |
| | | | | Min $V_y$ | 12.86 | -0.22 | 81.55 | 0.63 | 326.48 | 0.72 | BC 242 |
| | | | | Max $V_z$ | -54.32 | -0.21 | 146.79 | 0.82 | 593.82 | 0.68 | BC 139 |
| | | | | Min $V_z$ | -15.18 | -0.10 | 37.48 | 0.06 | 150.18 | 0.31 | BC 423 |
| | | | | Max $M_T$ | -55.04 | -0.21 | 146.72 | 0.83 | 593.59 | 0.68 | BC 134 |
| | | | | Min $M_T$ | -16.96 | 0.29 | 37.73 | -0.47 | 151.00 | -0.93 | BC 356 |
| | | | | Max $M_y$ | -54.32 | -0.21 | 146.79 | 0.82 | 593.82 | 0.68 | BC 139 |
| | | | | Min $M_y$ | -15.18 | -0.10 | 37.48 | 0.06 | 150.18 | 0.31 | BC 423 |
| | | | | Max $M_z$ | 12.86 | -0.22 | 81.55 | 0.63 | 326.48 | 0.72 | BC 242 |
| | | | | Min $M_z$ | -15.66 | 0.29 | 37.80 | -0.47 | 151.25 | -0.95 | BC 408 |
| 17 | RC1 | 52 | 0 | Max N | -27.41 | -0.09 | -15.42 | 0.00 | 0.00 | 0.00 | BC 450 |
| | | | | Min N | -161.78 | -0.02 | -0.15 | 0.00 | 0.00 | 0.00 | BC 139 |
| | | | | Max $V_y$ | -128.58 | 0.03 | -14.87 | 0.00 | 0.00 | 0.00 | BC 247 |
| | | | | Min $V_y$ | -71.38 | -0.10 | -15.29 | 0.00 | -0.00 | 0.00 | BC 234 |
| | | | | Max $V_z$ | -69.74 | -0.07 | 14.80 | 0.00 | -0.00 | 0.00 | BC 408 |
| | | | | Min $V_z$ | -36.42 | -0.07 | -15.45 | 0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Max $M_T$ | -93.06 | -0.00 | -14.84 | 0.00 | 0.00 | 0.00 | BC 419 |
| | | | | Min $M_T$ | -57.43 | -0.02 | -9.85 | 0.00 | -0.00 | 0.00 | BC 445 |
| | | | | Max $M_y$ | -105.68 | -0.05 | 14.76 | 0.00 | 0.00 | 0.00 | BC 268 |
| | | | | Min $M_y$ | -82.65 | -0.05 | 14.76 | 0.00 | -0.00 | -0.00 | BC 432 |
| | | | | Max $M_z$ | -101.39 | -0.01 | -0.09 | 0.00 | 0.00 | 0.00 | BC 91 |
| | | | | Min $M_z$ | -82.65 | -0.05 | 14.76 | 0.00 | -0.00 | -0.00 | BC 432 |
| | | | 2500 | Max N | -25.42 | -0.09 | -5.64 | 0.00 | -26.32 | 0.23 | BC 450 |
| | | | Links | Min N | -158.85 | -0.02 | -0.15 | 0.00 | -0.39 | 0.06 | BC 139 |
| | | | | Max $V_y$ | -125.66 | 0.03 | -5.03 | 0.00 | -24.88 | -0.08 | BC 247 |
| | | | | Min $V_y$ | -68.45 | -0.10 | -5.50 | 0.00 | -25.98 | 0.26 | BC 234 |
| | | | | Max $V_z$ | -67.74 | -0.07 | 4.96 | 0.00 | 24.70 | 0.18 | BC 408 |
| | | | | Min $V_z$ | -34.42 | -0.07 | -5.67 | 0.00 | -26.41 | 0.17 | BC 446 |
| | | | | Max $M_T$ | -91.06 | -0.00 | -5.00 | 0.00 | -24.80 | 0.01 | BC 419 |
| | | | | Min $M_T$ | -55.43 | -0.02 | -3.70 | 0.00 | -16.95 | 0.05 | BC 445 |
| | | | | Max $M_y$ | -67.74 | -0.07 | 4.96 | 0.00 | 24.70 | 0.18 | BC 408 |
| | | | | Min $M_y$ | -34.42 | -0.07 | -5.67 | 0.00 | -26.41 | 0.17 | BC 446 |
| | | | | Max $M_z$ | -68.45 | -0.10 | -5.50 | 0.00 | -25.98 | 0.26 | BC 234 |
| | | | | Min $M_z$ | -125.66 | 0.03 | -5.03 | 0.00 | -24.88 | -0.08 | BC 247 |
| | | | 2500 | Max N | -25.42 | -0.09 | -5.64 | 0.00 | -26.32 | 0.23 | BC 450 |
| | | | Rechts | Min N | -158.85 | -0.02 | -0.15 | 0.00 | -0.39 | 0.06 | BC 139 |
| | | | | Max $V_y$ | -125.66 | 0.03 | -5.03 | 0.00 | -24.88 | -0.08 | BC 247 |
| | | | | Min $V_y$ | -68.45 | -0.10 | -5.50 | 0.00 | -25.98 | 0.26 | BC 234 |
| | | | | Max $V_z$ | -67.74 | -0.07 | 4.96 | 0.00 | 24.70 | 0.18 | BC 408 |
| | | | | Min $V_z$ | -34.42 | -0.07 | -5.67 | 0.00 | -26.41 | 0.17 | BC 446 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 17 | RC1 | | | Max $M_T$ | -91.06 | -0.00 | -5.00 | 0.00 | -24.80 | 0.01 | BC 419 |
| | | | | Min $M_T$ | -55.43 | -0.02 | -3.70 | 0.00 | -16.95 | 0.05 | BC 445 |
| | | | | Max $M_y$ | -67.74 | -0.07 | 4.96 | 0.00 | 24.70 | 0.18 | BC 408 |
| | | | | Min $M_y$ | -34.42 | -0.07 | -5.67 | 0.00 | -26.41 | 0.17 | BC 446 |
| | | | | Max $M_z$ | -68.45 | -0.10 | -5.50 | 0.00 | -25.98 | 0.26 | BC 234 |
| | | | | Min $M_z$ | -125.66 | 0.03 | -5.03 | 0.00 | -24.88 | -0.08 | BC 247 |
| | | | 4345 | Max N | -21.70 | -0.09 | 1.58 | 0.00 | -30.06 | 0.39 | BC 450 |
| | | | Links | Min N | -153.40 | -0.02 | -0.15 | 0.00 | -0.67 | 0.11 | BC 139 |
| | | | | Max $V_y$ | -120.21 | 0.03 | 2.23 | 0.00 | -27.46 | -0.14 | BC 247 |
| | | | | Min $V_y$ | -63.01 | -0.10 | 1.72 | 0.00 | -29.47 | 0.45 | BC 234 |
| | | | | Max $V_z$ | -110.44 | -0.04 | 2.27 | 0.00 | -27.31 | 0.19 | BC 411 |
| | | | | Min $V_z$ | -85.42 | -0.03 | -2.36 | 0.00 | 26.90 | 0.14 | BC 244 |
| | | | | Max $M_T$ | -87.35 | -0.00 | 2.26 | 0.00 | -27.32 | 0.02 | BC 419 |
| | | | | Min $M_T$ | -51.72 | -0.02 | 0.84 | 0.00 | -19.59 | 0.08 | BC 445 |
| | | | | Max $M_y$ | -64.03 | -0.07 | -2.30 | 0.00 | 27.15 | 0.31 | BC 408 |
| | | | | Min $M_y$ | -30.71 | -0.07 | 1.55 | 0.00 | -30.21 | 0.30 | BC 446 |
| | | | | Max $M_z$ | -63.01 | -0.10 | 1.72 | 0.00 | -29.47 | 0.45 | BC 234 |
| | | | | Min $M_z$ | -120.21 | 0.03 | 2.23 | 0.00 | -27.46 | -0.14 | BC 247 |
| | | 73 | 4345 | Max N | -21.70 | -0.09 | 1.58 | 0.00 | -30.06 | 0.39 | BC 450 |
| | | | Rechts | Min N | -153.40 | -0.02 | -0.15 | 0.00 | -0.67 | 0.11 | BC 139 |
| | | | | Max $V_y$ | -120.21 | 0.03 | 2.23 | 0.00 | -27.46 | -0.14 | BC 247 |
| | | | | Min $V_y$ | -63.01 | -0.10 | 1.72 | 0.00 | -29.47 | 0.45 | BC 234 |
| | | | | Max $V_z$ | -110.44 | -0.04 | 2.27 | 0.00 | -27.31 | 0.19 | BC 411 |
| | | | | Min $V_z$ | -85.42 | -0.03 | -2.36 | 0.00 | 26.90 | 0.14 | BC 244 |
| | | | | Max $M_T$ | -87.35 | -0.00 | 2.26 | 0.00 | -27.32 | 0.02 | BC 419 |
| | | | | Min $M_T$ | -51.72 | -0.02 | 0.84 | 0.00 | -19.59 | 0.08 | BC 445 |
| | | | | Max $M_y$ | -64.03 | -0.07 | -2.30 | 0.00 | 27.15 | 0.31 | BC 408 |
| | | | | Min $M_y$ | -30.71 | -0.07 | 1.55 | 0.00 | -30.21 | 0.30 | BC 446 |
| | | | | Max $M_z$ | -63.01 | -0.10 | 1.72 | 0.00 | -29.47 | 0.45 | BC 234 |
| | | | | Min $M_z$ | -120.21 | 0.03 | 2.23 | 0.00 | -27.46 | -0.14 | BC 247 |
| 18 | RC1 | 62 | 0 | Max N | -4.02 | -0.09 | 7.02 | -0.00 | 0.00 | 0.00 | BC 422 |
| | | | Links | Min N | -125.42 | -0.06 | 3.49 | 0.00 | -0.00 | 0.00 | BC 211 |
| | | | | Max $V_y$ | -95.04 | 0.00 | 5.00 | 0.00 | 0.00 | 0.00 | BC 235 |
| | | | | Min $V_y$ | -30.26 | -0.10 | 5.95 | -0.00 | -0.00 | 0.00 | BC 246 |
| | | | | Max $V_z$ | -4.39 | -0.09 | 7.13 | -0.00 | 0.00 | 0.00 | BC 362 |
| | | | | Min $V_z$ | -64.94 | -0.08 | -13.31 | -0.00 | -0.00 | 0.00 | BC 269 |
| | | | | Max $M_T$ | -81.63 | -0.00 | 5.65 | 0.00 | -0.00 | 0.00 | BC 439 |
| | | | | Min $M_T$ | -86.38 | -0.05 | 2.24 | -0.00 | 0.00 | 0.00 | BC 204 |
| | | | | Max $M_y$ | -43.34 | -0.02 | 4.74 | -0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Min $M_y$ | -74.18 | -0.04 | -4.04 | -0.00 | -0.00 | 0.00 | BC 91 |
| | | | | Max $M_z$ | -85.60 | -0.05 | 2.06 | -0.00 | -0.00 | 0.00 | BC 268 |
| | | | | Min $M_z$ | -55.53 | -0.01 | -1.99 | -0.00 | 0.00 | -0.00 | BC 289 |
| | | | 0 | Max N | -4.02 | -0.09 | 7.02 | -0.00 | 0.00 | 0.00 | BC 422 |
| | | | Rechts | Min N | -125.42 | -0.06 | 3.49 | 0.00 | 0.00 | 0.00 | BC 211 |
| | | | | Max $V_y$ | -95.04 | 0.00 | 5.00 | 0.00 | 0.00 | -0.00 | BC 235 |
| | | | | Min $V_y$ | -30.26 | -0.10 | 5.95 | -0.00 | 0.00 | 0.00 | BC 246 |
| | | | | Max $V_z$ | -4.39 | -0.09 | 7.13 | -0.00 | 0.00 | 0.00 | BC 362 |
| | | | | Min $V_z$ | -64.94 | -0.08 | -13.31 | -0.00 | -0.00 | 0.00 | BC 269 |
| | | | | Max $M_T$ | -81.63 | -0.00 | 5.65 | 0.00 | 0.00 | 0.00 | BC 439 |
| | | | | Min $M_T$ | -86.38 | -0.05 | 2.24 | -0.00 | 0.00 | 0.00 | BC 204 |
| | | | | Max $M_y$ | -4.39 | -0.09 | 7.13 | -0.00 | 0.00 | 0.00 | BC 362 |
| | | | | Min $M_y$ | -64.94 | -0.08 | -13.31 | -0.00 | -0.00 | 0.00 | BC 269 |
| | | | | Max $M_z$ | -30.26 | -0.10 | 5.95 | -0.00 | 0.00 | 0.00 | BC 246 |
| | | | | Min $M_z$ | -95.04 | 0.00 | 5.00 | 0.00 | 0.00 | -0.00 | BC 235 |
| | | | 2500 | Max N | -2.02 | -0.09 | -4.02 | -0.00 | 3.72 | 0.22 | BC 422 |
| | | | Links | Min N | -122.50 | -0.06 | -6.36 | 0.00 | -3.62 | 0.16 | BC 211 |
| | | | | Max $V_y$ | -92.11 | 0.00 | -4.84 | 0.00 | 0.18 | -0.00 | BC 235 |
| | | | | Min $V_y$ | -27.34 | -0.10 | -5.08 | -0.00 | 1.06 | 0.26 | BC 246 |
| | | | | Max $V_z$ | -18.06 | -0.03 | -0.62 | -0.00 | -13.85 | 0.06 | BC 361 |
| | | | | Min $V_z$ | -38.86 | -0.08 | -6.61 | -0.00 | -2.76 | 0.20 | BC 270 |
| | | | | Max $M_T$ | -79.64 | -0.00 | -4.20 | 0.00 | 1.79 | 0.01 | BC 439 |
| | | | | Min $M_T$ | -83.45 | -0.05 | -3.92 | -0.00 | -2.11 | 0.13 | BC 204 |
| | | | | Max $M_y$ | -41.35 | -0.02 | -1.42 | -0.00 | 4.13 | 0.05 | BC 360 |
| | | | | Min $M_y$ | -62.01 | -0.08 | -3.46 | -0.00 | -20.94 | 0.21 | BC 269 |
| | | | | Max $M_z$ | -27.34 | -0.10 | -5.08 | -0.00 | 1.06 | 0.26 | BC 246 |
| | | | | Min $M_z$ | -92.11 | 0.00 | -4.84 | 0.00 | 0.18 | -0.00 | BC 235 |
| | | | 2500 | Max N | -2.02 | -0.09 | -4.02 | -0.00 | 3.72 | 0.22 | BC 422 |
| | | | Rechts | Min N | -122.50 | -0.06 | -6.36 | 0.00 | -3.62 | 0.16 | BC 211 |
| | | | | Max $V_y$ | -92.11 | 0.00 | -4.84 | 0.00 | 0.18 | -0.00 | BC 235 |
| | | | | Min $V_y$ | -27.34 | -0.10 | -5.08 | -0.00 | 1.06 | 0.26 | BC 246 |
| | | | | Max $V_z$ | -18.06 | -0.03 | -0.62 | -0.00 | -13.85 | 0.06 | BC 361 |
| | | | | Min $V_z$ | -38.86 | -0.08 | -6.61 | -0.00 | -2.76 | 0.20 | BC 270 |
| | | | | Max $M_T$ | -79.64 | -0.00 | -4.20 | 0.00 | 1.79 | 0.01 | BC 439 |
| | | | | Min $M_T$ | -83.45 | -0.05 | -3.92 | -0.00 | -2.11 | 0.13 | BC 204 |
| | | | | Max $M_y$ | -41.35 | -0.02 | -1.42 | -0.00 | 4.13 | 0.05 | BC 360 |
| | | | | Min $M_y$ | -62.01 | -0.08 | -3.46 | -0.00 | -20.94 | 0.21 | BC 269 |
| | | | | Max $M_z$ | -27.34 | -0.10 | -5.08 | -0.00 | 1.06 | 0.26 | BC 246 |
| | | | | Min $M_z$ | -92.11 | 0.00 | -4.84 | 0.00 | 0.18 | -0.00 | BC 235 |
| | | | 4345 | Max N | 1.69 | -0.09 | -12.09 | -0.00 | -11.15 | 0.39 | BC 422 |
| | | | Links | Min N | -117.05 | -0.06 | -13.56 | 0.00 | -22.00 | 0.27 | BC 211 |
| | | | | Max $V_y$ | -86.66 | 0.00 | -12.04 | 0.00 | -15.41 | -0.00 | BC 235 |
| | | | | Min $V_y$ | -21.89 | -0.10 | -13.16 | -0.00 | -15.78 | 0.45 | BC 246 |
| | | | | Max $V_z$ | -14.34 | -0.03 | 6.57 | -0.00 | -8.35 | 0.11 | BC 361 |
| | | | | Min $V_z$ | -33.41 | -0.08 | -14.68 | -0.00 | -22.41 | 0.34 | BC 270 |
| | | | | Max $M_T$ | -75.92 | -0.00 | -11.39 | 0.00 | -12.60 | 0.02 | BC 439 |
| | | | | Min $M_T$ | -78.00 | -0.05 | -8.41 | -0.00 | -13.50 | 0.22 | BC 204 |
| | | | | Max $M_y$ | -37.63 | -0.02 | -5.92 | -0.00 | -2.64 | 0.09 | BC 360 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 18 | RC1 | | | Min $M_y$ | -115.95 | -0.06 | -13.67 | 0.00 | -22.50 | 0.25 | BC 271 |
| | | | | Max $M_z$ | -21.89 | -0.10 | -13.16 | -0.00 | -15.78 | 0.45 | BC 246 |
| | | | | Min $M_z$ | -86.66 | 0.00 | -12.04 | 0.00 | -15.41 | -0.00 | BC 235 |
| | | 77 | 4345 | Max N | 1.69 | -0.09 | -12.09 | -0.00 | -11.16 | 0.39 | BC 422 |
| | | | Rechts | Min N | -117.05 | -0.06 | -13.56 | 0.00 | -22.00 | 0.27 | BC 211 |
| | | | | Max $V_y$ | -86.66 | 0.00 | -12.04 | 0.00 | -15.41 | -0.00 | BC 235 |
| | | | | Min $V_y$ | -21.89 | -0.10 | -13.16 | -0.00 | -15.78 | 0.45 | BC 246 |
| | | | | Max $V_z$ | -14.34 | -0.03 | 6.57 | -0.00 | -8.35 | 0.11 | BC 361 |
| | | | | Min $V_z$ | -33.41 | -0.08 | -14.68 | -0.00 | -22.41 | 0.34 | BC 270 |
| | | | | Max $M_T$ | -75.92 | -0.00 | -11.39 | 0.00 | -12.60 | 0.02 | BC 439 |
| | | | | Min $M_T$ | -78.00 | -0.05 | -8.41 | -0.00 | -13.50 | 0.22 | BC 204 |
| | | | | Max $M_y$ | -37.63 | -0.02 | -5.92 | -0.00 | -2.64 | 0.09 | BC 360 |
| | | | | Min $M_y$ | -115.95 | -0.06 | -13.67 | 0.00 | -22.50 | 0.25 | BC 271 |
| | | | | Max $M_z$ | -21.89 | -0.10 | -13.16 | -0.00 | -15.78 | 0.45 | BC 246 |
| | | | | Min $M_z$ | -86.66 | 0.00 | -12.04 | 0.00 | -15.41 | -0.00 | BC 235 |
| 19 | RC1 | 53 | 0 | Max N | 16.29 | -0.03 | 31.54 | 0.22 | 0.00 | 0.00 | BC 411 |
| | | | | Min N | -18.94 | -0.02 | 69.63 | 0.05 | 0.00 | 0.00 | BC 244 |
| | | | | Max $V_y$ | -10.54 | 0.04 | 31.34 | 0.03 | -0.00 | 0.00 | BC 473 |
| | | | | Min $V_y$ | 15.34 | -0.05 | 70.11 | 0.17 | -0.00 | 0.00 | BC 175 |
| | | | | Max $V_z$ | -4.36 | -0.04 | 136.86 | 0.04 | -0.00 | 0.00 | BC 131 |
| | | | | Min $V_z$ | -17.83 | -0.01 | 31.07 | 0.04 | 0.00 | 0.00 | BC 444 |
| | | | | Max $M_T$ | 16.29 | -0.03 | 31.54 | 0.22 | 0.00 | 0.00 | BC 411 |
| | | | | Min $M_T$ | -8.25 | -0.04 | 31.29 | 0.01 | 0.00 | 0.00 | BC 450 |
| | | | | Max $M_y$ | -5.29 | -0.04 | 136.83 | 0.04 | 0.00 | 0.00 | BC 133 |
| | | | | Min $M_y$ | -10.05 | 0.04 | 31.34 | 0.03 | -0.00 | 0.00 | BC 381 |
| | | | | Max $M_z$ | -5.32 | -0.04 | 55.23 | 0.02 | 0.00 | 0.00 | BC 406 |
| | | | | Min $M_z$ | -0.99 | -0.03 | 51.78 | 0.04 | 0.00 | 0.00 | BC 1 |
| | | 147 | 3201 | Max N | 16.56 | -0.03 | 16.99 | 0.22 | 77.66 | 0.11 | BC 411 |
| | | | | Min N | -18.31 | -0.02 | 36.43 | 0.05 | 169.72 | 0.08 | BC 244 |
| | | | | Max $V_y$ | -10.26 | 0.04 | 16.80 | 0.03 | 77.03 | -0.14 | BC 473 |
| | | | | Min $V_y$ | 15.96 | -0.05 | 36.90 | 0.17 | 171.25 | 0.16 | BC 175 |
| | | | | Max $V_z$ | -3.12 | -0.04 | 70.40 | 0.04 | 331.67 | 0.14 | BC 131 |
| | | | | Min $V_z$ | -17.56 | -0.01 | 16.53 | 0.04 | 76.18 | 0.04 | BC 444 |
| | | | | Max $M_T$ | 16.56 | -0.03 | 16.99 | 0.22 | 77.66 | 0.11 | BC 411 |
| | | | | Min $M_T$ | -7.97 | -0.04 | 16.75 | 0.01 | 76.88 | 0.14 | BC 450 |
| | | | | Max $M_y$ | -3.12 | -0.04 | 70.40 | 0.04 | 331.67 | 0.14 | BC 131 |
| | | | | Min $M_y$ | -17.56 | -0.01 | 16.53 | 0.04 | 76.18 | 0.04 | BC 444 |
| | | | | Max $M_z$ | 15.96 | -0.05 | 36.90 | 0.17 | 171.25 | 0.16 | BC 175 |
| | | | | Min $M_z$ | -10.26 | 0.04 | 16.80 | 0.03 | 77.03 | -0.14 | BC 473 |
| 20 | RC1 | 63 | 0 | Max N | 4.24 | -0.05 | 8.55 | 0.01 | -0.00 | 0.00 | BC 363 |
| | | | | Min N | -29.91 | 0.05 | 14.88 | -0.01 | 0.00 | 0.00 | BC 436 |
| | | | | Max $V_y$ | -25.20 | 0.06 | 18.87 | -0.01 | -0.00 | 0.00 | BC 204 |
| | | | | Min $V_y$ | 2.21 | -0.05 | 8.55 | 0.01 | 0.00 | 0.00 | BC 447 |
| | | | | Max $V_z$ | -5.82 | 0.00 | 36.58 | 0.00 | -0.00 | 0.00 | BC 134 |
| | | | | Min $V_z$ | 2.18 | -0.05 | 8.55 | 0.01 | 0.00 | 0.00 | BC 471 |
| | | | | Max $M_T$ | 2.22 | -0.04 | 18.87 | 0.01 | 0.00 | 0.00 | BC 235 |
| | | | | Min $M_T$ | -11.53 | 0.01 | 8.55 | -0.01 | 0.00 | 0.00 | BC 413 |
| | | | | Max $M_y$ | -3.64 | 0.00 | 21.20 | 0.00 | 0.00 | 0.00 | BC 304 |
| | | | | Min $M_y$ | -20.17 | 0.01 | 12.54 | -0.01 | -0.00 | 0.00 | BC 278 |
| | | | | Max $M_z$ | -4.30 | 0.01 | 14.16 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -4.30 | 0.01 | 14.16 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 159 | 3267 | Max N | 4.54 | -0.05 | 0.44 | 0.01 | 14.69 | 0.16 | BC 363 |
| | | | | Min N | -29.37 | 0.05 | 0.44 | -0.01 | 25.03 | -0.17 | BC 436 |
| | | | | Max $V_y$ | -24.52 | 0.06 | 0.65 | -0.01 | 31.88 | -0.20 | BC 204 |
| | | | | Min $V_y$ | 2.51 | -0.05 | 0.44 | 0.01 | 14.68 | 0.17 | BC 447 |
| | | | | Max $V_z$ | -3.29 | 0.01 | 0.73 | 0.00 | 24.33 | -0.03 | BC 10 |
| | | | | Min $V_z$ | 2.02 | -0.04 | 0.44 | 0.01 | 25.02 | 0.15 | BC 459 |
| | | | | Max $M_T$ | 2.90 | -0.04 | 0.65 | 0.01 | 31.89 | 0.14 | BC 235 |
| | | | | Min $M_T$ | -11.23 | 0.01 | 0.44 | -0.01 | 14.69 | -0.04 | BC 413 |
| | | | | Max $M_y$ | -4.48 | 0.00 | 0.65 | 0.00 | 60.82 | -0.02 | BC 134 |
| | | | | Min $M_y$ | 2.48 | -0.05 | 0.44 | 0.01 | 14.68 | 0.16 | BC 471 |
| | | | | Max $M_z$ | 2.51 | -0.05 | 0.44 | 0.01 | 14.68 | 0.17 | BC 447 |
| | | | | Min $M_z$ | -24.52 | 0.06 | 0.65 | -0.01 | 31.88 | -0.20 | BC 204 |
| 21 | RC1 | 54 | 0 | Max N | -23.54 | 0.17 | -17.38 | 0.00 | -0.00 | 0.00 | BC 415 |
| | | | | Min N | -177.50 | 0.03 | -0.09 | 0.00 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_y$ | -71.97 | 0.18 | -17.20 | 0.00 | 0.00 | 0.00 | BC 211 |
| | | | | Min $V_y$ | -97.47 | -0.09 | 14.23 | 0.00 | 0.00 | 0.00 | BC 212 |
| | | | | Max $V_z$ | -62.84 | -0.05 | 14.28 | -0.00 | 0.00 | 0.00 | BC 252 |
| | | | | Min $V_z$ | -33.03 | 0.14 | -17.39 | 0.00 | 0.00 | 0.00 | BC 419 |
| | | | | Max $M_T$ | -91.83 | -0.05 | -9.20 | 0.00 | -0.00 | 0.00 | BC 241 |
| | | | | Min $M_T$ | -80.60 | 0.00 | -10.95 | -0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Max $M_y$ | -51.39 | -0.07 | 14.25 | 0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Min $M_y$ | -53.29 | -0.00 | -9.16 | 0.00 | -0.00 | 0.00 | BC 357 |
| | | | | Max $M_z$ | -90.25 | 0.01 | -0.05 | -0.00 | 0.00 | 0.00 | BC 91 |
| | | | | Min $M_z$ | -94.17 | -0.02 | -0.06 | 0.00 | -0.00 | -0.00 | BC 310 |
| | | | 2500 | Max N | -21.54 | 0.17 | -6.28 | 0.00 | -29.58 | -0.43 | BC 415 |
| | | | Links | Min N | -174.58 | 0.03 | -0.09 | 0.00 | -0.24 | -0.08 | BC 149 |
| | | | | Max $V_y$ | -69.04 | 0.18 | -6.11 | 0.00 | -29.14 | -0.44 | BC 211 |
| | | | | Min $V_y$ | -94.54 | -0.09 | 4.61 | 0.00 | 23.55 | 0.21 | BC 212 |
| | | | | Max $V_z$ | -59.91 | -0.05 | 4.66 | -0.00 | 23.67 | 0.13 | BC 252 |
| | | | | Min $V_z$ | -31.04 | 0.14 | -6.30 | 0.00 | -29.60 | -0.34 | BC 419 |
| | | | | Max $M_T$ | -88.90 | -0.05 | -3.18 | 0.00 | -15.47 | 0.12 | BC 241 |
| | | | | Min $M_T$ | -78.61 | 0.00 | -3.69 | -0.00 | -18.30 | -0.01 | BC 446 |
| | | | | Max $M_y$ | -59.91 | -0.05 | 4.66 | -0.00 | 23.67 | 0.13 | BC 252 |
| | | | | Min $M_y$ | -31.04 | 0.14 | -6.30 | 0.00 | -29.60 | -0.34 | BC 419 |
| | | | | Max $M_z$ | -94.54 | -0.09 | 4.61 | 0.00 | 23.55 | 0.21 | BC 212 |
| | | | | Min $M_z$ | -69.04 | 0.18 | -6.11 | 0.00 | -29.14 | -0.44 | BC 211 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 21 | RC1 | | 2500 | Max N | -21.54 | 0.17 | -6.28 | 0.00 | -29.58 | -0.43 | BC 415 |
| | | | Rechts | Min N | -174.58 | 0.03 | -0.09 | 0.00 | -0.24 | -0.08 | BC 149 |
| | | | | Max $V_y$ | -69.04 | 0.18 | -6.11 | 0.00 | -29.14 | -0.44 | BC 211 |
| | | | | Min $V_y$ | -94.54 | -0.09 | 4.61 | 0.00 | 23.55 | 0.21 | BC 212 |
| | | | | Max $V_z$ | -59.91 | -0.05 | 4.66 | -0.00 | 23.67 | 0.13 | BC 252 |
| | | | | Min $V_z$ | -31.04 | 0.14 | -6.30 | 0.00 | -29.60 | -0.34 | BC 419 |
| | | | | Max $M_T$ | -88.90 | -0.05 | -3.18 | 0.00 | -15.47 | 0.12 | BC 241 |
| | | | | Min $M_T$ | -78.61 | 0.00 | -3.69 | -0.00 | -18.30 | -0.01 | BC 446 |
| | | | | Max $M_y$ | -59.91 | -0.05 | 4.66 | -0.00 | 23.67 | 0.13 | BC 252 |
| | | | | Min $M_y$ | -31.04 | 0.14 | -6.30 | 0.00 | -29.60 | -0.34 | BC 419 |
| | | | | Max $M_z$ | -94.54 | -0.09 | 4.61 | 0.00 | 23.55 | 0.21 | BC 212 |
| | | | | Min $M_z$ | -69.04 | 0.18 | -6.11 | 0.00 | -29.14 | -0.44 | BC 211 |
| | | | 4345 | Max N | -17.88 | 0.17 | 1.90 | 0.00 | -33.62 | -0.74 | BC 415 |
| | | | Links | Min N | -169.20 | 0.03 | -0.09 | 0.00 | -0.41 | -0.15 | BC 149 |
| | | | | Max $V_y$ | -63.67 | 0.18 | 2.08 | 0.00 | -32.86 | -0.76 | BC 211 |
| | | | | Min $V_y$ | -89.17 | -0.09 | -2.49 | 0.00 | 25.50 | 0.37 | BC 212 |
| | | | | Max $V_z$ | -65.88 | 0.17 | 2.10 | 0.00 | -32.78 | -0.73 | BC 243 |
| | | | | Min $V_z$ | -89.27 | -0.08 | -2.50 | 0.00 | 25.48 | 0.37 | BC 200 |
| | | | | Max $M_T$ | -83.53 | -0.05 | 1.26 | 0.00 | -17.25 | 0.21 | BC 241 |
| | | | | Min $M_T$ | -74.94 | 0.00 | 1.67 | -0.00 | -20.15 | -0.01 | BC 446 |
| | | | | Max $M_y$ | -54.53 | -0.05 | -2.45 | -0.00 | 25.71 | 0.22 | BC 252 |
| | | | | Min $M_y$ | -27.37 | 0.14 | 1.89 | 0.00 | -33.67 | -0.60 | BC 419 |
| | | | | Max $M_z$ | -89.17 | -0.09 | -2.49 | 0.00 | 25.50 | 0.37 | BC 212 |
| | | | | Min $M_z$ | -63.67 | 0.18 | 2.08 | 0.00 | -32.86 | -0.76 | BC 211 |
| | | 74 | 4345 | Max N | -17.88 | 0.17 | 1.90 | 0.00 | -33.62 | -0.74 | BC 415 |
| | | | Rechts | Min N | -169.20 | 0.03 | -0.09 | 0.00 | -0.41 | -0.15 | BC 149 |
| | | | | Max $V_y$ | -63.67 | 0.18 | 2.08 | 0.00 | -32.86 | -0.76 | BC 211 |
| | | | | Min $V_y$ | -89.17 | -0.09 | -2.49 | 0.00 | 25.50 | 0.37 | BC 212 |
| | | | | Max $V_z$ | -65.88 | 0.17 | 2.10 | 0.00 | -32.78 | -0.73 | BC 243 |
| | | | | Min $V_z$ | -89.27 | -0.08 | -2.50 | 0.00 | 25.48 | 0.37 | BC 200 |
| | | | | Max $M_T$ | -83.53 | -0.05 | 1.26 | 0.00 | -17.25 | 0.21 | BC 241 |
| | | | | Min $M_T$ | -74.94 | 0.00 | 1.67 | -0.00 | -20.15 | -0.01 | BC 446 |
| | | | | Max $M_y$ | -54.53 | -0.05 | -2.45 | -0.00 | 25.71 | 0.22 | BC 252 |
| | | | | Min $M_y$ | -27.37 | 0.14 | 1.89 | 0.00 | -33.67 | -0.60 | BC 419 |
| | | | | Max $M_z$ | -89.17 | -0.09 | -2.49 | 0.00 | 25.50 | 0.37 | BC 212 |
| | | | | Min $M_z$ | -63.67 | 0.18 | 2.08 | 0.00 | -32.86 | -0.76 | BC 211 |
| 22 | RC1 | 64 | 0 | Max N | -3.82 | 0.18 | 17.29 | 0.00 | -0.00 | 0.00 | BC 415 |
| | | | | Min N | -117.99 | 0.10 | 9.30 | -0.00 | 0.00 | 0.00 | BC 234 |
| | | | | Max $V_y$ | -31.67 | 0.18 | 17.26 | 0.00 | -0.00 | 0.00 | BC 207 |
| | | | | Min $V_y$ | -59.33 | -0.06 | -14.79 | -0.00 | -0.00 | 0.00 | BC 273 |
| | | | | Max $V_z$ | -5.86 | 0.17 | 17.29 | 0.00 | 0.00 | 0.00 | BC 447 |
| | | | | Min $V_z$ | -33.20 | -0.05 | -14.81 | -0.00 | 0.00 | 0.00 | BC 361 |
| | | | | Max $M_T$ | -30.82 | 0.14 | 17.25 | 0.00 | -0.00 | 0.00 | BC 171 |
| | | | | Min $M_T$ | -46.83 | -0.04 | -14.76 | -0.00 | -0.00 | 0.00 | BC 209 |
| | | | | Max $M_y$ | -37.77 | -0.01 | 9.29 | -0.00 | 0.00 | 0.00 | BC 388 |
| | | | | Min $M_y$ | -73.35 | 0.00 | 9.29 | -0.00 | -0.00 | 0.00 | BC 278 |
| | | | | Max $M_z$ | -50.48 | -0.02 | 9.30 | -0.00 | 0.00 | 0.00 | BC 268 |
| | | | | Min $M_z$ | -57.25 | 0.01 | 0.04 | -0.00 | 0.00 | -0.00 | BC 289 |
| | | | 2500 | Max N | -1.82 | 0.18 | 6.19 | 0.00 | 29.35 | -0.44 | BC 415 |
| | | | Links | Min N | -115.06 | 0.10 | 3.28 | -0.00 | 15.72 | -0.24 | BC 234 |
| | | | | Max $V_y$ | -28.74 | 0.18 | 6.17 | 0.00 | 29.28 | -0.46 | BC 207 |
| | | | | Min $V_y$ | -56.40 | -0.06 | -5.16 | -0.00 | -24.94 | 0.16 | BC 273 |
| | | | | Max $V_z$ | -3.87 | 0.17 | 6.19 | 0.00 | 29.35 | -0.42 | BC 447 |
| | | | | Min $V_z$ | -31.20 | -0.05 | -5.18 | -0.00 | -24.99 | 0.12 | BC 361 |
| | | | | Max $M_T$ | -27.89 | 0.14 | 6.16 | 0.00 | 29.27 | -0.36 | BC 171 |
| | | | | Min $M_T$ | -43.91 | -0.04 | -5.14 | -0.00 | -24.88 | 0.11 | BC 209 |
| | | | | Max $M_y$ | -3.87 | 0.17 | 6.19 | 0.00 | 29.35 | -0.42 | BC 447 |
| | | | | Min $M_y$ | -27.43 | -0.05 | -5.18 | -0.00 | -24.99 | 0.11 | BC 357 |
| | | | | Max $M_z$ | -56.40 | -0.06 | -5.16 | -0.00 | -24.94 | 0.16 | BC 273 |
| | | | | Min $M_z$ | -28.74 | 0.18 | 6.17 | 0.00 | 29.28 | -0.46 | BC 207 |
| | | | 2500 | Max N | -1.82 | 0.18 | 6.19 | 0.00 | 29.35 | -0.44 | BC 415 |
| | | | Rechts | Min N | -115.06 | 0.10 | 3.28 | -0.00 | 15.72 | -0.24 | BC 234 |
| | | | | Max $V_y$ | -28.74 | 0.18 | 6.16 | 0.00 | 29.28 | -0.46 | BC 207 |
| | | | | Min $V_y$ | -56.40 | -0.06 | -5.16 | -0.00 | -24.94 | 0.16 | BC 273 |
| | | | | Max $V_z$ | -3.87 | 0.17 | 6.19 | 0.00 | 29.35 | -0.42 | BC 447 |
| | | | | Min $V_z$ | -31.20 | -0.05 | -5.18 | -0.00 | -24.99 | 0.12 | BC 361 |
| | | | | Max $M_T$ | -27.89 | 0.14 | 6.16 | 0.00 | 29.27 | -0.36 | BC 171 |
| | | | | Min $M_T$ | -43.91 | -0.04 | -5.14 | -0.00 | -24.88 | 0.11 | BC 209 |
| | | | | Max $M_y$ | -3.87 | 0.17 | 6.19 | 0.00 | 29.35 | -0.42 | BC 447 |
| | | | | Min $M_y$ | -27.43 | -0.05 | -5.18 | -0.00 | -24.99 | 0.11 | BC 357 |
| | | | | Max $M_z$ | -56.40 | -0.06 | -5.16 | -0.00 | -24.94 | 0.16 | BC 273 |
| | | | | Min $M_z$ | -28.74 | 0.18 | 6.16 | 0.00 | 29.28 | -0.46 | BC 207 |
| | | | 4345 | Max N | 1.84 | 0.18 | -1.99 | 0.00 | 33.22 | -0.76 | BC 415 |
| | | | Links | Min N | -109.69 | 0.10 | -1.16 | -0.00 | 17.68 | -0.42 | BC 234 |
| | | | | Max $V_y$ | -23.37 | 0.18 | -2.02 | 0.00 | 33.10 | -0.79 | BC 207 |
| | | | | Min $V_y$ | -51.03 | -0.06 | 1.94 | -0.00 | -27.91 | 0.27 | BC 273 |
| | | | | Max $V_z$ | -39.01 | -0.05 | 1.96 | -0.00 | -27.80 | 0.20 | BC 269 |
| | | | | Min $V_z$ | -35.49 | 0.14 | -2.04 | 0.00 | 33.02 | -0.63 | BC 175 |
| | | | | Max $M_T$ | -22.52 | 0.14 | -2.03 | 0.00 | 33.08 | -0.62 | BC 171 |
| | | | | Min $M_T$ | -38.53 | -0.04 | 1.96 | -0.00 | -27.81 | 0.19 | BC 209 |
| | | | | Max $M_y$ | -0.20 | 0.17 | -1.99 | 0.00 | 33.23 | -0.73 | BC 447 |
| | | | | Min $M_y$ | -27.54 | -0.05 | 1.92 | -0.00 | -28.00 | 0.22 | BC 361 |
| | | | | Max $M_z$ | -51.03 | -0.06 | 1.94 | -0.00 | -27.91 | 0.27 | BC 273 |
| | | | | Min $M_z$ | -23.37 | 0.18 | -2.02 | 0.00 | 33.10 | -0.79 | BC 207 |
| | | 78 | 4345 | Max N | 1.84 | 0.18 | -1.99 | 0.00 | 33.22 | -0.76 | BC 415 |
| | | | Rechts | Min N | -109.69 | 0.10 | -1.16 | -0.00 | 17.68 | -0.42 | BC 234 |
| | | | | Max $V_y$ | -23.37 | 0.18 | -2.02 | 0.00 | 33.10 | -0.79 | BC 207 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 22 | RC1 | | | Min $V_y$ | -51.03 | -0.06 | 1.94 | -0.00 | -27.91 | 0.27 | BC 273 |
| | | | | Max $V_z$ | -39.01 | -0.05 | 1.96 | -0.00 | -27.80 | 0.20 | BC 269 |
| | | | | Min $V_z$ | -35.49 | 0.14 | -2.04 | 0.00 | 33.02 | -0.63 | BC 175 |
| | | | | Max $M_T$ | -22.52 | 0.14 | -2.03 | 0.00 | 33.08 | -0.62 | BC 171 |
| | | | | Min $M_T$ | -38.53 | -0.04 | 1.96 | -0.00 | -27.81 | 0.19 | BC 209 |
| | | | | Max $M_y$ | -0.20 | 0.17 | -1.99 | 0.00 | 33.23 | -0.73 | BC 447 |
| | | | | Min $M_y$ | -27.54 | -0.05 | 1.92 | -0.00 | -28.00 | 0.22 | BC 361 |
| | | | | Max $M_z$ | -51.03 | -0.06 | 1.94 | -0.00 | -27.91 | 0.27 | BC 273 |
| | | | | Min $M_z$ | -23.37 | 0.18 | -2.02 | 0.00 | 33.10 | -0.79 | BC 207 |
| 23 | RC1 | 55 | 0 | Max N | 12.08 | -0.02 | 31.00 | -0.18 | -0.00 | 0.00 | BC 450 |
| | | | | Min N | -25.42 | -0.01 | 54.26 | 0.01 | -0.00 | 0.00 | BC 392 |
| | | | | Max $V_y$ | 6.84 | 0.06 | 44.74 | 0.08 | 0.00 | 0.00 | BC 161 |
| | | | | Min $V_y$ | 0.58 | -0.06 | 68.55 | 0.02 | -0.00 | 0.00 | BC 247 |
| | | | | Max $V_z$ | -2.43 | -0.04 | 134.13 | 0.00 | 0.00 | 0.00 | BC 134 |
| | | | | Min $V_z$ | 5.85 | 0.06 | 30.30 | 0.09 | -0.00 | 0.00 | BC 473 |
| | | | | Max $M_T$ | 5.64 | 0.06 | 68.10 | 0.11 | 0.00 | 0.00 | BC 241 |
| | | | | Min $M_T$ | 12.04 | -0.00 | 30.98 | -0.19 | 0.00 | 0.00 | BC 446 |
| | | | | Max $M_y$ | 1.52 | -0.05 | 68.50 | 0.03 | 0.00 | 0.00 | BC 271 |
| | | | | Min $M_y$ | -24.73 | -0.00 | 68.62 | -0.02 | -0.00 | 0.00 | BC 204 |
| | | | | Max $M_z$ | -0.94 | -0.02 | 50.96 | -0.03 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -24.42 | -0.00 | 68.61 | -0.02 | 0.00 | -0.00 | BC 264 |
| | | 146 | 3201 | Max N | 12.34 | -0.02 | 16.71 | -0.18 | 76.35 | 0.05 | BC 450 |
| | | | | Min N | -24.94 | -0.01 | 28.35 | 0.01 | 132.21 | 0.02 | BC 392 |
| | | | | Max $V_y$ | 7.24 | 0.06 | 23.77 | 0.08 | 109.63 | -0.20 | BC 161 |
| | | | | Min $V_y$ | 1.19 | -0.06 | 35.96 | 0.02 | 167.24 | 0.18 | BC 247 |
| | | | | Max $V_z$ | -1.21 | -0.04 | 69.03 | 0.00 | 325.11 | 0.12 | BC 134 |
| | | | | Min $V_z$ | 6.12 | 0.06 | 16.01 | 0.09 | 74.11 | -0.19 | BC 473 |
| | | | | Max $M_T$ | 6.25 | 0.06 | 35.52 | 0.11 | 165.83 | -0.18 | BC 241 |
| | | | | Min $M_T$ | 12.31 | -0.00 | 16.68 | -0.19 | 76.28 | 0.01 | BC 446 |
| | | | | Max $M_y$ | -1.21 | -0.04 | 69.03 | 0.00 | 325.11 | 0.12 | BC 134 |
| | | | | Min $M_y$ | 6.12 | 0.06 | 16.01 | 0.09 | 74.11 | -0.19 | BC 473 |
| | | | | Max $M_z$ | 1.19 | -0.06 | 35.96 | 0.02 | 167.24 | 0.18 | BC 247 |
| | | | | Min $M_z$ | 7.24 | 0.06 | 23.77 | 0.08 | 109.63 | -0.20 | BC 161 |
| 24 | RC1 | 65 | 0 | Max N | 9.46 | 0.03 | 13.78 | -0.00 | 0.00 | 0.00 | BC 362 |
| | | | | Min N | -26.33 | 0.03 | 32.06 | -0.01 | 0.00 | 0.00 | BC 269 |
| | | | | Max $V_y$ | 8.68 | 0.04 | 32.06 | -0.00 | 0.00 | 0.00 | BC 234 |
| | | | | Min $V_y$ | -4.16 | -0.00 | 20.21 | 0.01 | 0.00 | 0.00 | BC 171 |
| | | | | Max $V_z$ | -10.87 | 0.02 | 65.23 | 0.00 | -0.00 | 0.00 | BC 154 |
| | | | | Min $V_z$ | -20.28 | 0.02 | 13.78 | -0.01 | -0.00 | 0.00 | BC 389 |
| | | | | Max $M_T$ | -5.08 | 0.01 | 32.06 | 0.01 | 0.00 | 0.00 | BC 243 |
| | | | | Min $M_T$ | -20.41 | 0.02 | 13.78 | -0.01 | 0.00 | 0.00 | BC 449 |
| | | | | Max $M_y$ | -7.27 | 0.01 | 32.06 | 0.00 | 0.00 | 0.00 | BC 91 |
| | | | | Min $M_y$ | -9.48 | 0.02 | 53.38 | 0.00 | -0.00 | 0.00 | BC 136 |
| | | | | Max $M_z$ | -0.85 | 0.01 | 22.82 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -20.43 | 0.02 | 13.78 | -0.01 | 0.00 | -0.00 | BC 353 |
| | | 158 | 3267 | Max N | 9.95 | 0.03 | 0.55 | -0.00 | 23.41 | -0.10 | BC 362 |
| | | | | Min N | -25.17 | 0.03 | 0.82 | -0.01 | 53.71 | -0.09 | BC 269 |
| | | | | Max $V_y$ | 9.84 | 0.04 | 0.81 | -0.00 | 53.69 | -0.12 | BC 234 |
| | | | | Min $V_y$ | -3.43 | -0.00 | 0.81 | 0.01 | 34.35 | 0.01 | BC 171 |
| | | | | Max $V_z$ | -5.82 | 0.01 | 0.92 | 0.00 | 58.14 | -0.04 | BC 27 |
| | | | | Min $V_z$ | -19.79 | 0.02 | 0.55 | -0.01 | 23.41 | -0.06 | BC 389 |
| | | | | Max $M_T$ | -3.92 | 0.01 | 0.82 | 0.01 | 53.72 | -0.02 | BC 243 |
| | | | | Min $M_T$ | -19.92 | 0.02 | 0.55 | -0.01 | 23.41 | -0.06 | BC 449 |
| | | | | Max $M_y$ | -8.47 | 0.02 | 0.82 | 0.00 | 107.89 | -0.07 | BC 154 |
| | | | | Min $M_y$ | -19.79 | 0.02 | 0.55 | -0.01 | 23.41 | -0.06 | BC 389 |
| | | | | Max $M_z$ | -3.43 | -0.00 | 0.81 | 0.01 | 34.35 | 0.01 | BC 171 |
| | | | | Min $M_z$ | 9.84 | 0.04 | 0.81 | -0.00 | 53.69 | -0.12 | BC 234 |
| 25 | RC1 | 8 | 0 | Max N | -23.58 | 5.04 | -5.13 | -0.00 | 0.00 | 0.00 | BC 447 |
| | | | Links | Min N | -56.21 | 0.00 | -0.15 | 0.00 | 0.00 | 0.00 | BC 138 |
| | | | | Max $V_y$ | -40.28 | 5.06 | -5.17 | -0.00 | 0.00 | 0.00 | BC 211 |
| | | | | Min $V_y$ | -29.39 | -6.85 | 4.27 | 0.00 | 0.00 | 0.00 | BC 464 |
| | | | | Max $V_z$ | -23.72 | -6.84 | 4.29 | 0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Min $V_z$ | -40.28 | 5.05 | -5.18 | -0.00 | 0.00 | 0.00 | BC 243 |
| | | | | Max $M_T$ | -34.76 | -6.83 | 4.29 | 0.00 | 0.00 | 0.00 | BC 168 |
| | | | | Min $M_T$ | -23.58 | 5.04 | -5.13 | -0.00 | 0.00 | 0.00 | BC 475 |
| | | | | Max $M_y$ | -45.17 | 0.00 | -0.16 | 0.00 | 0.00 | 0.00 | BC 333 |
| | | | | Min $M_y$ | -39.16 | 0.02 | -0.05 | 0.00 | -0.00 | 0.00 | BC 2 |
| | | | | Max $M_z$ | -40.35 | 0.01 | -0.16 | 0.00 | 0.00 | 0.00 | BC 91 |
| | | | | Min $M_z$ | -40.64 | -0.03 | -0.17 | 0.00 | 0.00 | -0.00 | BC 299 |
| | | | 0 | Max N | -23.58 | 5.04 | -5.13 | -0.00 | -0.00 | -0.00 | BC 447 |
| | | | Rechts | Min N | -56.21 | 0.00 | -0.15 | 0.00 | -0.00 | -0.00 | BC 138 |
| | | | | Max $V_y$ | -40.28 | 5.06 | -5.17 | -0.00 | -0.00 | -0.00 | BC 211 |
| | | | | Min $V_y$ | -29.39 | -6.85 | 4.27 | 0.00 | 0.00 | 0.00 | BC 464 |
| | | | | Max $V_z$ | -23.72 | -6.84 | 4.29 | 0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Min $V_z$ | -40.28 | 5.05 | -5.18 | -0.00 | -0.00 | -0.00 | BC 243 |
| | | | | Max $M_T$ | -34.76 | -6.83 | 4.29 | 0.00 | 0.00 | 0.00 | BC 168 |
| | | | | Min $M_T$ | -23.58 | 5.04 | -5.13 | -0.00 | -0.00 | -0.00 | BC 475 |
| | | | | Max $M_y$ | -23.72 | -6.84 | 4.29 | 0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Min $M_y$ | -40.28 | 5.05 | -5.18 | -0.00 | -0.00 | -0.00 | BC 243 |
| | | | | Max $M_z$ | -29.39 | -6.85 | 4.27 | 0.00 | 0.00 | 0.00 | BC 464 |
| | | | | Min $M_z$ | -40.28 | 5.06 | -5.17 | -0.00 | -0.00 | -0.00 | BC 211 |
| | | | 2500 | Max N | -21.59 | -2.00 | 1.82 | -0.00 | -4.14 | -3.80 | BC 447 |
| | | | Links | Min N | -53.29 | 0.00 | -0.15 | 0.00 | -0.37 | -0.01 | BC 138 |
| | | | | Max $V_y$ | -31.83 | 2.96 | -0.45 | 0.00 | 4.74 | 4.82 | BC 220 |
| | | | | Min $V_y$ | -21.59 | -2.02 | 1.87 | -0.00 | -4.01 | -3.75 | BC 423 |
| | | | | Max $V_z$ | -21.59 | -2.01 | 1.88 | -0.00 | -4.00 | -3.76 | BC 363 |
| | | | | Min $V_z$ | -37.50 | 2.94 | -0.47 | 0.00 | 4.70 | 4.86 | BC 240 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 25 | RC1 | | | Max $M_T$ | -31.84 | 2.94 | -0.42 | 0.00 | 4.84 | 4.86 | BC 168 |
| | | | | Min $M_T$ | -21.59 | -1.99 | 1.82 | -0.00 | -4.14 | -3.81 | BC 475 |
| | | | | Max $M_y$ | -21.73 | 2.94 | -0.41 | 0.00 | 4.85 | 4.87 | BC 360 |
| | | | | Min $M_y$ | -37.37 | 1.64 | -0.28 | 0.00 | -4.38 | 2.67 | BC 269 |
| | | | | Max $M_z$ | -27.39 | 2.92 | -0.43 | 0.00 | 4.80 | 4.91 | BC 464 |
| | | | | Min $M_z$ | -37.36 | -1.98 | 1.78 | -0.00 | -4.23 | -3.85 | BC 211 |
| | | | 2500 | Max N | -21.59 | -2.00 | 1.82 | -0.00 | -4.14 | -3.80 | BC 447 |
| | | | Rechts | Min N | -53.29 | 0.00 | -0.15 | 0.00 | -0.37 | -0.01 | BC 138 |
| | | | | Max $V_y$ | -31.83 | 2.96 | -0.45 | 0.00 | 4.74 | 4.82 | BC 220 |
| | | | | Min $V_y$ | -21.59 | -2.02 | 1.87 | -0.00 | -4.01 | -3.75 | BC 423 |
| | | | | Max $V_z$ | -21.59 | -2.01 | 1.88 | -0.00 | -4.00 | -3.76 | BC 363 |
| | | | | Min $V_z$ | -37.50 | 2.94 | -0.47 | 0.00 | 4.70 | 4.86 | BC 240 |
| | | | | Max $M_T$ | -31.84 | 2.94 | -0.42 | 0.00 | 4.84 | 4.86 | BC 168 |
| | | | | Min $M_T$ | -21.59 | -1.99 | 1.82 | -0.00 | -4.14 | -3.81 | BC 475 |
| | | | | Max $M_y$ | -21.73 | 2.94 | -0.41 | 0.00 | 4.85 | 4.87 | BC 360 |
| | | | | Min $M_y$ | -37.37 | 1.64 | -0.28 | 0.00 | -4.38 | 2.67 | BC 269 |
| | | | | Max $M_z$ | -27.39 | 2.92 | -0.43 | 0.00 | 4.80 | 4.91 | BC 464 |
| | | | | Min $M_z$ | -37.36 | -1.98 | 1.78 | -0.00 | -4.23 | -3.85 | BC 211 |
| | | | 4345 | Max N | -17.44 | -7.19 | 6.95 | -0.00 | 3.94 | 4.68 | BC 447 |
| | | | Links | Min N | -47.21 | 0.00 | -0.15 | 0.00 | -0.64 | -0.02 | BC 138 |
| | | | | Max $V_y$ | -25.76 | 10.17 | -3.92 | 0.00 | 0.70 | -7.30 | BC 220 |
| | | | | Min $V_y$ | -17.45 | -7.21 | 7.00 | -0.00 | 4.18 | 4.76 | BC 423 |
| | | | | Max $V_z$ | -17.45 | -7.20 | 7.01 | -0.00 | 4.20 | 4.74 | BC 363 |
| | | | | Min $V_z$ | -31.42 | 10.16 | -3.94 | 0.00 | 0.63 | -7.23 | BC 240 |
| | | | | Max $M_T$ | -25.76 | 10.16 | -3.89 | 0.00 | 0.87 | -7.22 | BC 168 |
| | | | | Min $M_T$ | -17.44 | -7.18 | 6.95 | -0.00 | 3.95 | 4.65 | BC 475 |
| | | | | Max $M_y$ | -17.45 | -7.20 | 7.01 | -0.00 | 4.20 | 4.74 | BC 363 |
| | | | | Min $M_y$ | -31.30 | 5.63 | 1.88 | 0.00 | -2.91 | -4.04 | BC 269 |
| | | | | Max $M_z$ | -17.45 | -7.21 | 7.00 | -0.00 | 4.18 | 4.76 | BC 423 |
| | | | | Min $M_z$ | -25.76 | 10.17 | -3.92 | 0.00 | 0.70 | -7.30 | BC 220 |
| | | 16 | 4345 | Max N | -17.44 | -7.19 | 6.95 | -0.00 | 3.94 | 4.68 | BC 447 |
| | | | Rechts | Min N | -47.21 | 0.00 | -0.15 | 0.00 | -0.64 | -0.02 | BC 138 |
| | | | | Max $V_y$ | -25.76 | 10.17 | -3.92 | 0.00 | 0.70 | -7.30 | BC 220 |
| | | | | Min $V_y$ | -17.45 | -7.21 | 7.00 | -0.00 | 4.18 | 4.76 | BC 423 |
| | | | | Max $V_z$ | -17.45 | -7.20 | 7.01 | -0.00 | 4.20 | 4.74 | BC 363 |
| | | | | Min $V_z$ | -31.42 | 10.16 | -3.94 | 0.00 | 0.63 | -7.23 | BC 240 |
| | | | | Max $M_T$ | -25.76 | 10.16 | -3.89 | 0.00 | 0.87 | -7.22 | BC 168 |
| | | | | Min $M_T$ | -17.44 | -7.18 | 6.95 | -0.00 | 3.95 | 4.65 | BC 475 |
| | | | | Max $M_y$ | -17.45 | -7.20 | 7.01 | -0.00 | 4.20 | 4.74 | BC 363 |
| | | | | Min $M_y$ | -31.30 | 5.63 | 1.88 | 0.00 | -2.91 | -4.04 | BC 269 |
| | | | | Max $M_z$ | -17.45 | -7.21 | 7.00 | -0.00 | 4.18 | 4.76 | BC 423 |
| | | | | Min $M_z$ | -25.76 | 10.17 | -3.92 | 0.00 | 0.70 | -7.30 | BC 220 |
| 26 | RC1 | 7 | 0 | Max N | -6.36 | -6.97 | -4.99 | -0.00 | 0.00 | 0.00 | BC 445 |
| | | | | Min N | -53.69 | 0.02 | -0.46 | -0.00 | 0.00 | 0.00 | BC 138 |
| | | | | Max $V_y$ | -33.83 | 5.20 | 4.34 | 0.00 | 0.00 | -0.00 | BC 207 |
| | | | | Min $V_y$ | -11.51 | -6.98 | -5.04 | -0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Max $V_z$ | -22.63 | 5.16 | 4.80 | 0.00 | -0.00 | 0.00 | BC 359 |
| | | | | Min $V_z$ | -21.51 | -6.97 | -5.16 | -0.00 | 0.00 | -0.00 | BC 241 |
| | | | | Max $M_T$ | -32.10 | 5.17 | 4.65 | 0.00 | 0.00 | 0.00 | BC 231 |
| | | | | Min $M_T$ | -21.59 | -6.97 | -5.16 | -0.00 | 0.00 | -0.00 | BC 269 |
| | | | | Max $M_y$ | -7.32 | -6.97 | -4.93 | -0.00 | 0.00 | -0.00 | BC 381 |
| | | | | Min $M_y$ | -26.86 | -3.18 | 1.44 | -0.00 | -0.00 | -0.00 | BC 190 |
| | | | | Max $M_z$ | -44.17 | -3.87 | 2.34 | -0.00 | 0.00 | 0.00 | BC 268 |
| | | | | Min $M_z$ | -26.86 | -3.18 | 1.44 | -0.00 | -0.00 | -0.00 | BC 190 |
| | | | 2500 | Max N | -4.36 | 3.01 | -0.28 | -0.00 | -6.59 | 4.95 | BC 445 |
| | | | Links | Min N | -50.76 | 0.02 | -0.46 | -0.00 | -1.15 | -0.06 | BC 138 |
| | | | | Max $V_y$ | -14.47 | 3.03 | -0.34 | -0.00 | -6.73 | 4.91 | BC 217 |
| | | | | Min $V_y$ | -19.79 | -2.06 | -2.20 | 0.00 | 3.19 | -3.87 | BC 451 |
| | | | | Max $V_z$ | -10.67 | 3.02 | 0.14 | -0.00 | -5.52 | 4.92 | BC 357 |
| | | | | Min $V_z$ | -29.76 | -2.03 | -2.68 | 0.00 | 1.98 | -3.95 | BC 243 |
| | | | | Max $M_T$ | -29.85 | -2.05 | -2.25 | 0.00 | 3.06 | -3.90 | BC 171 |
| | | | | Min $M_T$ | -18.66 | 3.01 | -0.46 | -0.00 | -7.02 | 4.95 | BC 269 |
| | | | | Max $M_y$ | -20.63 | -2.05 | -2.15 | 0.00 | 3.32 | -3.89 | BC 359 |
| | | | | Min $M_y$ | -18.58 | 3.01 | -0.46 | -0.00 | -7.02 | 4.96 | BC 241 |
| | | | | Max $M_z$ | -9.51 | 3.00 | -0.34 | -0.00 | -6.73 | 4.97 | BC 433 |
| | | | | Min $M_z$ | -30.90 | -2.02 | -2.61 | 0.00 | 2.16 | -3.97 | BC 207 |
| | | | 2500 | Max N | -4.36 | 3.01 | -0.28 | -0.00 | -6.59 | 4.95 | BC 445 |
| | | | Rechts | Min N | -50.76 | 0.02 | -0.46 | -0.00 | -1.15 | -0.06 | BC 138 |
| | | | | Max $V_y$ | -14.47 | 3.03 | -0.34 | -0.00 | -6.73 | 4.91 | BC 217 |
| | | | | Min $V_y$ | -19.79 | -2.06 | -2.20 | 0.00 | 3.19 | -3.87 | BC 451 |
| | | | | Max $V_z$ | -10.67 | 3.02 | 0.14 | -0.00 | -5.52 | 4.92 | BC 357 |
| | | | | Min $V_z$ | -29.76 | -2.03 | -2.68 | 0.00 | 1.98 | -3.95 | BC 243 |
| | | | | Max $M_T$ | -29.18 | -2.05 | -2.30 | 0.00 | 2.94 | -3.90 | BC 231 |
| | | | | Min $M_T$ | -18.66 | 3.01 | -0.46 | -0.00 | -7.02 | 4.95 | BC 269 |
| | | | | Max $M_y$ | -20.63 | -2.05 | -2.15 | 0.00 | 3.32 | -3.89 | BC 359 |
| | | | | Min $M_y$ | -18.58 | 3.01 | -0.46 | -0.00 | -7.02 | 4.96 | BC 241 |
| | | | | Max $M_z$ | -9.51 | 3.00 | -0.34 | -0.00 | -6.73 | 4.97 | BC 433 |
| | | | | Min $M_z$ | -30.90 | -2.02 | -2.61 | 0.00 | 2.16 | -3.97 | BC 207 |
| | | | 4345 | Max N | -0.19 | 10.38 | 3.19 | -0.00 | -3.91 | -7.41 | BC 445 |
| | | | Links | Min N | -44.64 | 0.02 | -0.46 | -0.00 | -1.99 | -0.11 | BC 138 |
| | | | | Max $V_y$ | -8.35 | 10.40 | 3.13 | -0.00 | -4.15 | -7.47 | BC 217 |
| | | | | Min $V_y$ | -15.61 | -7.39 | -7.33 | 0.00 | -5.61 | 4.85 | BC 451 |
| | | | | Max $V_z$ | -6.49 | 10.39 | 3.61 | -0.00 | -2.06 | -7.46 | BC 357 |
| | | | | Min $V_z$ | -23.63 | -7.35 | -7.81 | 0.00 | -7.70 | 4.71 | BC 243 |
| | | | | Max $M_T$ | -23.05 | -7.37 | -7.43 | 0.00 | -6.04 | 4.79 | BC 231 |
| | | | | Min $M_T$ | -12.53 | 10.38 | 3.01 | -0.00 | -4.66 | -7.41 | BC 269 |
| | | | | Max $M_y$ | -29.00 | 5.83 | -2.41 | -0.00 | 0.61 | -4.25 | BC 360 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 26 | RC1 | | | Min $M_y$ | -23.63 | -7.35 | -7.81 | 0.00 | -7.70 | 4.71 | BC 243 |
| | | | | Max $M_z$ | -15.61 | -7.39 | -7.33 | 0.00 | -5.61 | 4.85 | BC 451 |
| | | | | Min $M_z$ | -8.35 | 10.40 | 3.13 | -0.00 | -4.15 | -7.47 | BC 217 |
| | | 17 | 4345 | Max N | -0.19 | 10.38 | 3.19 | -0.00 | -3.91 | -7.41 | BC 445 |
| | | | Rechts | Min N | -44.64 | 0.02 | -0.46 | -0.00 | -1.99 | -0.11 | BC 138 |
| | | | | Max $V_y$ | -8.35 | 10.40 | 3.13 | -0.00 | -4.15 | -7.47 | BC 217 |
| | | | | Min $V_y$ | -15.61 | -7.39 | -7.33 | 0.00 | -5.61 | 4.85 | BC 451 |
| | | | | Max $V_z$ | -6.49 | 10.39 | 3.61 | -0.00 | -2.06 | -7.46 | BC 357 |
| | | | | Min $V_z$ | -23.63 | -7.35 | -7.81 | 0.00 | -7.70 | 4.71 | BC 243 |
| | | | | Max $M_T$ | -23.05 | -7.37 | -7.43 | 0.00 | -6.04 | 4.79 | BC 231 |
| | | | | Min $M_T$ | -12.53 | 10.38 | 3.01 | -0.00 | -4.66 | -7.41 | BC 269 |
| | | | | Max $M_y$ | -29.00 | 5.83 | -2.41 | -0.00 | 0.61 | -4.25 | BC 360 |
| | | | | Min $M_y$ | -23.63 | -7.35 | -7.81 | 0.00 | -7.70 | 4.71 | BC 243 |
| | | | | Max $M_z$ | -15.61 | -7.39 | -7.33 | 0.00 | -5.61 | 4.85 | BC 451 |
| | | | | Min $M_z$ | -8.35 | 10.40 | 3.13 | -0.00 | -4.15 | -7.47 | BC 217 |
| 27 | RC1 | 56 | 0 | Max N | 3.74 | -0.14 | 7.09 | -0.02 | 0.00 | 0.00 | BC 447 |
| | | | | Min N | -3.97 | -0.02 | 16.07 | 0.01 | -0.00 | 0.00 | BC 172 |
| | | | | Max $V_y$ | 2.76 | 0.19 | 10.41 | 0.03 | 0.00 | 0.00 | BC 253 |
| | | | | Min $V_y$ | 3.52 | -0.16 | 16.07 | -0.02 | 0.00 | 0.00 | BC 175 |
| | | | | Max $V_z$ | -0.40 | -0.04 | 31.92 | -0.00 | 0.00 | 0.00 | BC 141 |
| | | | | Min $V_z$ | -3.77 | -0.00 | 7.09 | 0.02 | 0.00 | 0.00 | BC 440 |
| | | | | Max $M_T$ | 2.76 | 0.19 | 10.41 | 0.03 | 0.00 | 0.00 | BC 253 |
| | | | | Min $M_T$ | 3.52 | -0.16 | 16.07 | -0.02 | 0.00 | 0.00 | BC 175 |
| | | | | Max $M_y$ | -0.20 | -0.03 | 16.07 | -0.00 | 0.00 | 0.00 | BC 70 |
| | | | | Min $M_y$ | 1.39 | -0.02 | 10.41 | 0.01 | -0.00 | 0.00 | BC 226 |
| | | | | Max $M_z$ | -0.15 | -0.03 | 11.75 | -0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.15 | -0.03 | 11.75 | -0.00 | -0.00 | 0.00 | BC 1 |
| | | 145 | 3201 | Max N | 3.92 | -0.15 | 0.13 | -0.02 | 25.92 | 0.49 | BC 243 |
| | | | | Min N | -3.68 | -0.02 | 0.10 | 0.01 | 11.51 | 0.06 | BC 360 |
| | | | | Max $V_y$ | 2.95 | 0.19 | 0.14 | 0.03 | 16.88 | -0.60 | BC 253 |
| | | | | Min $V_y$ | 3.82 | -0.16 | 0.13 | -0.02 | 25.92 | 0.53 | BC 175 |
| | | | | Max $V_z$ | 0.07 | -0.03 | 0.16 | -0.00 | 19.06 | 0.10 | BC 17 |
| | | | | Min $V_z$ | 0.22 | -0.03 | 0.05 | -0.00 | 45.86 | 0.09 | BC 339 |
| | | | | Max $M_T$ | 2.95 | 0.19 | 0.14 | 0.03 | 16.88 | -0.60 | BC 253 |
| | | | | Min $M_T$ | 3.82 | -0.16 | 0.13 | -0.02 | 25.92 | 0.53 | BC 175 |
| | | | | Max $M_y$ | 0.19 | -0.04 | 0.10 | -0.00 | 51.24 | 0.14 | BC 141 |
| | | | | Min $M_y$ | -3.64 | -0.00 | 0.09 | 0.02 | 11.50 | 0.01 | BC 440 |
| | | | | Max $M_z$ | 3.82 | -0.16 | 0.13 | -0.02 | 25.92 | 0.53 | BC 175 |
| | | | | Min $M_z$ | 2.95 | 0.19 | 0.14 | 0.03 | 16.88 | -0.60 | BC 253 |
| 28 | RC1 | 57 | 0 | Max N | 3.19 | 0.01 | 7.25 | 0.01 | 0.00 | 0.00 | BC 359 |
| | | | | Min N | -16.97 | -0.00 | 7.25 | -0.01 | -0.00 | 0.00 | BC 356 |
| | | | | Max $V_y$ | -4.89 | 0.03 | 16.42 | -0.01 | 0.00 | 0.00 | BC 269 |
| | | | | Min $V_y$ | -16.97 | -0.00 | 7.25 | -0.01 | -0.00 | 0.00 | BC 356 |
| | | | | Max $V_z$ | -1.73 | 0.01 | 32.63 | 0.00 | -0.00 | 0.00 | BC 141 |
| | | | | Min $V_z$ | -6.52 | -0.00 | 7.25 | -0.01 | 0.00 | 0.00 | BC 440 |
| | | | | Max $M_T$ | 2.33 | 0.02 | 16.42 | 0.01 | 0.00 | 0.00 | BC 243 |
| | | | | Min $M_T$ | -16.97 | -0.00 | 7.25 | -0.01 | -0.00 | 0.00 | BC 356 |
| | | | | Max $M_y$ | -3.34 | 0.00 | 16.42 | -0.01 | 0.00 | 0.00 | BC 268 |
| | | | | Min $M_y$ | -12.94 | 0.00 | 16.42 | -0.01 | -0.00 | 0.00 | BC 232 |
| | | | | Max $M_z$ | -0.80 | 0.01 | 12.01 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.80 | 0.01 | 12.01 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 157 | 3267 | Max N | 3.45 | 0.01 | 0.12 | 0.01 | 12.04 | -0.04 | BC 359 |
| | | | | Min N | -16.71 | -0.00 | 0.11 | -0.01 | 12.04 | 0.02 | BC 356 |
| | | | | Max $V_y$ | -4.29 | 0.03 | 0.17 | -0.01 | 27.10 | -0.09 | BC 269 |
| | | | | Min $V_y$ | -16.71 | -0.00 | 0.11 | -0.01 | 12.04 | 0.02 | BC 356 |
| | | | | Max $V_z$ | -0.33 | 0.01 | 0.19 | 0.00 | 19.93 | -0.03 | BC 17 |
| | | | | Min $V_z$ | -5.23 | -0.00 | 0.11 | -0.01 | 21.48 | 0.00 | BC 428 |
| | | | | Max $M_T$ | 2.93 | 0.02 | 0.17 | 0.01 | 27.10 | -0.06 | BC 243 |
| | | | | Min $M_T$ | -16.71 | -0.00 | 0.11 | -0.01 | 12.04 | 0.02 | BC 356 |
| | | | | Max $M_y$ | -0.52 | 0.01 | 0.17 | 0.00 | 53.58 | -0.05 | BC 141 |
| | | | | Min $M_y$ | -6.25 | -0.00 | 0.11 | -0.01 | 12.03 | 0.01 | BC 440 |
| | | | | Max $M_z$ | -16.71 | -0.00 | 0.11 | -0.01 | 12.04 | 0.02 | BC 356 |
| | | | | Min $M_z$ | -4.29 | 0.03 | 0.17 | -0.01 | 27.10 | -0.09 | BC 269 |
| 29 | RC1 | 44 | 0 | Max N | -10.36 | 0.17 | -23.79 | 0.00 | 0.00 | 0.00 | BC 356 |
| | | | Links | Min N | -123.30 | 0.27 | -21.77 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Max $V_y$ | -107.29 | 0.27 | -21.77 | 0.00 | 0.00 | 0.00 | BC 437 |
| | | | | Min $V_y$ | -62.37 | -0.01 | 22.36 | -0.00 | -0.00 | 0.00 | BC 182 |
| | | | | Max $V_z$ | -34.52 | -0.01 | 22.36 | -0.00 | -0.00 | 0.00 | BC 358 |
| | | | | Min $V_z$ | -23.07 | 0.17 | -23.80 | 0.00 | -0.00 | 0.00 | BC 432 |
| | | | | Max $M_T$ | -11.04 | 0.17 | -23.80 | 0.00 | 0.00 | 0.00 | BC 412 |
| | | | | Min $M_T$ | -62.27 | -0.01 | 22.36 | -0.00 | 0.00 | 0.00 | BC 234 |
| | | | | Max $M_y$ | -94.16 | 0.25 | -21.77 | 0.00 | 0.00 | 0.00 | BC 381 |
| | | | | Min $M_y$ | -38.87 | 0.18 | -23.80 | 0.00 | -0.00 | 0.00 | BC 268 |
| | | | | Max $M_z$ | -50.40 | 0.01 | -13.98 | 0.00 | 0.00 | 0.00 | BC 163 |
| | | | | Min $M_z$ | -95.27 | 0.03 | -0.00 | -0.00 | 0.00 | -0.00 | BC 155 |
| | | | 0 | Max N | -10.36 | 0.17 | -23.79 | 0.00 | -0.00 | -0.00 | BC 356 |
| | | | Rechts | Min N | -123.30 | 0.27 | -21.77 | 0.00 | -0.00 | -0.00 | BC 241 |
| | | | | Max $V_y$ | -107.29 | 0.27 | -21.77 | 0.00 | -0.00 | -0.00 | BC 437 |
| | | | | Min $V_y$ | -62.37 | -0.01 | 22.36 | -0.00 | 0.00 | 0.00 | BC 182 |
| | | | | Max $V_z$ | -34.52 | -0.01 | 22.36 | -0.00 | 0.00 | 0.00 | BC 358 |
| | | | | Min $V_z$ | -23.07 | 0.17 | -23.80 | 0.00 | -0.00 | -0.00 | BC 432 |
| | | | | Max $M_T$ | -11.04 | 0.17 | -23.80 | 0.00 | -0.00 | -0.00 | BC 412 |
| | | | | Min $M_T$ | -62.27 | -0.01 | 22.36 | -0.00 | 0.00 | 0.00 | BC 234 |
| | | | | Max $M_y$ | -50.64 | -0.01 | 22.36 | -0.00 | 0.00 | 0.00 | BC 162 |
| | | | | Min $M_y$ | -38.87 | 0.18 | -23.80 | 0.00 | -0.00 | -0.00 | BC 268 |
| | | | | Max $M_z$ | -62.37 | -0.01 | 22.36 | -0.00 | 0.00 | 0.00 | BC 182 |
| | | | | Min $M_z$ | -107.43 | 0.27 | -21.77 | 0.00 | -0.00 | -0.00 | BC 433 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 29 | RC1 | | 2500 | Max N | -8.36 | 0.17 | -8.70 | 0.00 | -40.61 | -0.43 | BC 356 |
| | | | Links | Min N | -120.38 | 0.27 | -8.02 | 0.00 | -37.24 | -0.66 | BC 241 |
| | | | | Max $V_y$ | -105.30 | 0.27 | -8.02 | 0.00 | -37.24 | -0.67 | BC 437 |
| | | | | Min $V_y$ | -59.44 | -0.01 | 8.24 | -0.00 | 38.25 | 0.03 | BC 182 |
| | | | | Max $V_z$ | -32.52 | -0.01 | 8.24 | -0.00 | 38.25 | 0.03 | BC 358 |
| | | | | Min $V_z$ | -21.07 | 0.17 | -8.70 | 0.00 | -40.63 | -0.43 | BC 432 |
| | | | | Max $M_T$ | -9.04 | 0.17 | -8.70 | 0.00 | -40.62 | -0.42 | BC 412 |
| | | | | Min $M_T$ | -59.34 | -0.01 | 8.24 | -0.00 | 38.25 | 0.02 | BC 234 |
| | | | | Max $M_y$ | -32.52 | -0.01 | 8.24 | -0.00 | 38.25 | 0.03 | BC 358 |
| | | | | Min $M_y$ | -21.07 | 0.17 | -8.70 | 0.00 | -40.63 | -0.43 | BC 432 |
| | | | | Max $M_z$ | -59.44 | -0.01 | 8.24 | -0.00 | 38.25 | 0.03 | BC 182 |
| | | | | Min $M_z$ | -105.30 | 0.27 | -8.02 | 0.00 | -37.24 | -0.67 | BC 437 |
| | | | 2500 | Max N | -8.36 | 0.17 | -8.70 | 0.00 | -40.61 | -0.43 | BC 356 |
| | | | Rechts | Min N | -120.38 | 0.27 | -8.02 | 0.00 | -37.24 | -0.66 | BC 241 |
| | | | | Max $V_y$ | -105.30 | 0.27 | -8.02 | 0.00 | -37.24 | -0.67 | BC 437 |
| | | | | Min $V_y$ | -59.44 | -0.01 | 8.24 | -0.00 | 38.25 | 0.03 | BC 182 |
| | | | | Max $V_z$ | -32.52 | -0.01 | 8.24 | -0.00 | 38.25 | 0.03 | BC 358 |
| | | | | Min $V_z$ | -21.07 | 0.17 | -8.70 | 0.00 | -40.63 | -0.43 | BC 432 |
| | | | | Max $M_T$ | -9.04 | 0.17 | -8.70 | 0.00 | -40.62 | -0.42 | BC 412 |
| | | | | Min $M_T$ | -59.34 | -0.01 | 8.24 | -0.00 | 38.25 | 0.02 | BC 234 |
| | | | | Max $M_y$ | -32.52 | -0.01 | 8.24 | -0.00 | 38.25 | 0.03 | BC 358 |
| | | | | Min $M_y$ | -21.07 | 0.17 | -8.70 | 0.00 | -40.63 | -0.43 | BC 432 |
| | | | | Max $M_z$ | -59.44 | -0.01 | 8.24 | -0.00 | 38.25 | 0.03 | BC 182 |
| | | | | Min $M_z$ | -105.30 | 0.27 | -8.02 | 0.00 | -37.24 | -0.67 | BC 437 |
| | | | 4345 | Max N | -3.68 | 0.17 | 2.45 | 0.00 | -46.38 | -0.74 | BC 356 |
| | | | Links | Min N | -113.51 | 0.27 | 2.12 | 0.00 | -42.69 | -1.15 | BC 241 |
| | | | | Max $V_y$ | -100.62 | 0.27 | 2.12 | 0.00 | -42.69 | -1.16 | BC 437 |
| | | | | Min $V_y$ | -52.57 | -0.01 | -2.18 | -0.00 | 43.84 | 0.06 | BC 182 |
| | | | | Max $V_z$ | -16.48 | 0.18 | 2.45 | 0.00 | -46.37 | -0.76 | BC 164 |
| | | | | Min $V_z$ | -52.60 | -0.01 | -2.18 | -0.00 | 43.84 | 0.06 | BC 242 |
| | | | | Max $M_T$ | -4.36 | 0.17 | 2.44 | 0.00 | -46.39 | -0.73 | BC 412 |
| | | | | Min $M_T$ | -52.48 | -0.01 | -2.18 | -0.00 | 43.84 | 0.03 | BC 234 |
| | | | | Max $M_y$ | -27.84 | -0.01 | -2.18 | -0.00 | 43.85 | 0.05 | BC 358 |
| | | | | Min $M_y$ | -16.39 | 0.17 | 2.44 | 0.00 | -46.41 | -0.75 | BC 432 |
| | | | | Max $M_z$ | -52.57 | -0.01 | -2.18 | -0.00 | 43.84 | 0.06 | BC 182 |
| | | | | Min $M_z$ | -100.62 | 0.27 | 2.12 | 0.00 | -42.69 | -1.16 | BC 437 |
| | | 69 | 4345 | Max N | -3.68 | 0.17 | 2.45 | 0.00 | -46.38 | -0.74 | BC 356 |
| | | | Rechts | Min N | -113.51 | 0.27 | 2.12 | 0.00 | -42.69 | -1.15 | BC 241 |
| | | | | Max $V_y$ | -100.62 | 0.27 | 2.12 | 0.00 | -42.69 | -1.16 | BC 437 |
| | | | | Min $V_y$ | -52.57 | -0.01 | -2.18 | -0.00 | 43.84 | 0.06 | BC 182 |
| | | | | Max $V_z$ | -16.48 | 0.18 | 2.45 | 0.00 | -46.37 | -0.76 | BC 164 |
| | | | | Min $V_z$ | -52.60 | -0.01 | -2.18 | -0.00 | 43.84 | 0.06 | BC 242 |
| | | | | Max $M_T$ | -4.36 | 0.17 | 2.44 | 0.00 | -46.39 | -0.73 | BC 412 |
| | | | | Min $M_T$ | -52.48 | -0.01 | -2.18 | -0.00 | 43.84 | 0.03 | BC 234 |
| | | | | Max $M_y$ | -27.84 | -0.01 | -2.18 | -0.00 | 43.85 | 0.05 | BC 358 |
| | | | | Min $M_y$ | -16.39 | 0.17 | 2.44 | 0.00 | -46.41 | -0.75 | BC 432 |
| | | | | Max $M_z$ | -52.57 | -0.01 | -2.18 | -0.00 | 43.84 | 0.06 | BC 182 |
| | | | | Min $M_z$ | -100.62 | 0.27 | 2.12 | 0.00 | -42.69 | -1.16 | BC 437 |
| 30 | RC1 | 47 | 0 | Max N | -11.92 | -0.19 | -24.18 | -0.00 | 0.00 | 0.00 | BC 445 |
| | | | Links | Min N | -122.90 | -0.26 | -22.18 | -0.00 | -0.00 | 0.00 | BC 200 |
| | | | | Max $V_y$ | -52.00 | 0.01 | 22.76 | 0.00 | -0.00 | 0.00 | BC 218 |
| | | | | Min $V_y$ | -112.52 | -0.26 | -22.18 | -0.00 | 0.00 | 0.00 | BC 164 |
| | | | | Max $V_z$ | -35.44 | 0.01 | 22.76 | 0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Min $V_z$ | -28.94 | -0.19 | -24.18 | -0.00 | 0.00 | 0.00 | BC 165 |
| | | | | Max $M_T$ | -63.30 | 0.00 | 22.76 | 0.00 | 0.00 | 0.00 | BC 214 |
| | | | | Min $M_T$ | -122.21 | -0.25 | -22.18 | -0.00 | -0.00 | 0.00 | BC 264 |
| | | | | Max $M_y$ | -121.64 | -0.25 | -22.18 | -0.00 | 0.00 | 0.00 | BC 268 |
| | | | | Min $M_y$ | -95.64 | -0.26 | -22.18 | -0.00 | -0.00 | 0.00 | BC 356 |
| | | | | Max $M_z$ | -52.37 | -0.00 | -14.23 | -0.00 | -0.00 | 0.00 | BC 163 |
| | | | | Min $M_z$ | -62.98 | -0.02 | -0.00 | -0.00 | 0.00 | -0.00 | BC 85 |
| | | | 0 | Max N | -11.92 | -0.19 | -24.18 | -0.00 | -0.00 | 0.00 | BC 445 |
| | | | Rechts | Min N | -122.90 | -0.26 | -22.18 | -0.00 | -0.00 | 0.00 | BC 200 |
| | | | | Max $V_y$ | -52.00 | 0.01 | 22.76 | 0.00 | 0.00 | -0.00 | BC 218 |
| | | | | Min $V_y$ | -112.52 | -0.26 | -22.18 | -0.00 | -0.00 | 0.00 | BC 164 |
| | | | | Max $V_z$ | -35.44 | 0.01 | 22.76 | 0.00 | 0.00 | -0.00 | BC 446 |
| | | | | Min $V_z$ | -28.94 | -0.19 | -24.18 | -0.00 | -0.00 | 0.00 | BC 165 |
| | | | | Max $M_T$ | -63.30 | 0.00 | 22.76 | 0.00 | 0.00 | -0.00 | BC 214 |
| | | | | Min $M_T$ | -122.21 | -0.25 | -22.18 | -0.00 | -0.00 | 0.00 | BC 264 |
| | | | | Max $M_y$ | -52.05 | 0.01 | 22.76 | 0.00 | 0.00 | -0.00 | BC 166 |
| | | | | Min $M_y$ | -12.22 | -0.19 | -24.18 | -0.00 | -0.00 | 0.00 | BC 381 |
| | | | | Max $M_z$ | -112.52 | -0.26 | -22.18 | -0.00 | -0.00 | 0.00 | BC 164 |
| | | | | Min $M_z$ | -51.96 | 0.01 | 22.76 | 0.00 | 0.00 | -0.00 | BC 190 |
| | | | 2500 | Max N | -9.93 | -0.19 | -9.07 | -0.00 | -41.56 | 0.48 | BC 445 |
| | | | Links | Min N | -119.98 | -0.26 | -8.39 | -0.00 | -38.21 | 0.65 | BC 200 |
| | | | | Max $V_y$ | -49.07 | 0.01 | 8.61 | 0.00 | 39.21 | -0.03 | BC 218 |
| | | | | Min $V_y$ | -109.59 | -0.26 | -8.39 | -0.00 | -38.20 | 0.66 | BC 164 |
| | | | | Max $V_z$ | -44.85 | 0.00 | 8.61 | 0.00 | 39.21 | -0.01 | BC 434 |
| | | | | Min $V_z$ | -26.01 | -0.19 | -9.08 | -0.00 | -41.57 | 0.48 | BC 165 |
| | | | | Max $M_T$ | -60.37 | 0.00 | 8.61 | 0.00 | 39.21 | -0.01 | BC 214 |
| | | | | Min $M_T$ | -119.29 | -0.25 | -8.39 | -0.00 | -38.21 | 0.64 | BC 264 |
| | | | | Max $M_y$ | -33.44 | 0.01 | 8.61 | 0.00 | 39.21 | -0.02 | BC 446 |
| | | | | Min $M_y$ | -26.01 | -0.19 | -9.08 | -0.00 | -41.57 | 0.48 | BC 165 |
| | | | | Max $M_z$ | -109.59 | -0.26 | -8.39 | -0.00 | -38.20 | 0.66 | BC 164 |
| | | | | Min $M_z$ | -49.07 | 0.01 | 8.61 | 0.00 | 39.21 | -0.03 | BC 218 |
| | | | 2500 | Max N | -9.93 | -0.19 | -9.07 | -0.00 | -41.56 | 0.48 | BC 445 |
| | | | Rechts | Min N | -119.98 | -0.26 | -8.39 | -0.00 | -38.21 | 0.65 | BC 200 |
| | | | | Max $V_y$ | -49.07 | 0.01 | 8.61 | 0.00 | 39.21 | -0.03 | BC 218 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 30 | RC1 | | | Min $V_y$ | -109.59 | -0.26 | -8.39 | -0.00 | -38.20 | 0.66 | BC 164 |
| | | | | Max $V_z$ | -44.85 | 0.00 | 8.61 | 0.00 | 39.21 | -0.01 | BC 434 |
| | | | | Min $V_z$ | -26.01 | -0.19 | -9.08 | -0.00 | -41.57 | 0.48 | BC 165 |
| | | | | Max $M_T$ | -60.37 | 0.00 | 8.61 | 0.00 | 39.21 | -0.01 | BC 214 |
| | | | | Min $M_T$ | -119.29 | -0.25 | -8.39 | -0.00 | -38.21 | 0.64 | BC 264 |
| | | | | Max $M_y$ | -33.44 | 0.01 | 8.61 | 0.00 | 39.21 | -0.02 | BC 446 |
| | | | | Min $M_y$ | -26.01 | -0.19 | -9.08 | -0.00 | -41.57 | 0.48 | BC 165 |
| | | | | Max $M_z$ | -109.59 | -0.26 | -8.39 | -0.00 | -38.20 | 0.66 | BC 164 |
| | | | | Min $M_z$ | -49.07 | 0.01 | 8.61 | 0.00 | 39.21 | -0.03 | BC 218 |
| | | | 4345 | Max N | -5.24 | -0.19 | 2.07 | -0.00 | -48.02 | 0.83 | BC 445 |
| | | | Links | Min N | -113.11 | -0.26 | 1.78 | -0.00 | -44.30 | 1.13 | BC 200 |
| | | | | Max $V_y$ | -42.20 | 0.01 | -1.84 | 0.00 | 45.46 | -0.06 | BC 218 |
| | | | | Min $V_y$ | -102.72 | -0.26 | 1.79 | -0.00 | -44.30 | 1.14 | BC 164 |
| | | | | Max $V_z$ | -16.33 | -0.20 | 2.07 | -0.00 | -48.01 | 0.85 | BC 433 |
| | | | | Min $V_z$ | -42.25 | 0.01 | -1.84 | 0.00 | 45.46 | -0.05 | BC 166 |
| | | | | Max $M_T$ | -53.50 | 0.00 | -1.84 | 0.00 | 45.46 | -0.02 | BC 214 |
| | | | | Min $M_T$ | -112.42 | -0.25 | 1.78 | -0.00 | -44.30 | 1.11 | BC 264 |
| | | | | Max $M_y$ | -28.76 | 0.01 | -1.84 | 0.00 | 45.46 | -0.04 | BC 446 |
| | | | | Min $M_y$ | -19.14 | -0.19 | 2.07 | -0.00 | -48.04 | 0.84 | BC 165 |
| | | | | Max $M_z$ | -102.72 | -0.26 | 1.79 | -0.00 | -44.30 | 1.14 | BC 164 |
| | | | | Min $M_z$ | -42.20 | 0.01 | -1.84 | 0.00 | 45.46 | -0.06 | BC 218 |
| | | 70 | 4345 | Max N | -5.24 | -0.19 | 2.07 | -0.00 | -48.02 | 0.83 | BC 445 |
| | | | Rechts | Min N | -113.11 | -0.26 | 1.78 | -0.00 | -44.30 | 1.13 | BC 200 |
| | | | | Max $V_y$ | -42.20 | 0.01 | -1.84 | 0.00 | 45.46 | -0.06 | BC 218 |
| | | | | Min $V_y$ | -102.72 | -0.26 | 1.79 | -0.00 | -44.30 | 1.14 | BC 164 |
| | | | | Max $V_z$ | -16.33 | -0.20 | 2.07 | -0.00 | -48.01 | 0.85 | BC 433 |
| | | | | Min $V_z$ | -42.25 | 0.01 | -1.84 | 0.00 | 45.46 | -0.05 | BC 166 |
| | | | | Max $M_T$ | -53.50 | 0.00 | -1.84 | 0.00 | 45.46 | -0.02 | BC 214 |
| | | | | Min $M_T$ | -112.42 | -0.25 | 1.78 | -0.00 | -44.30 | 1.11 | BC 264 |
| | | | | Max $M_y$ | -28.76 | 0.01 | -1.84 | 0.00 | 45.46 | -0.04 | BC 446 |
| | | | | Min $M_y$ | -19.14 | -0.19 | 2.07 | -0.00 | -48.04 | 0.84 | BC 165 |
| | | | | Max $M_z$ | -102.72 | -0.26 | 1.79 | -0.00 | -44.30 | 1.14 | BC 164 |
| | | | | Min $M_z$ | -42.20 | 0.01 | -1.84 | 0.00 | 45.46 | -0.06 | BC 218 |
| 31 | RC1 | 58 | 0 | Max N | -15.77 | 0.35 | 23.81 | -0.00 | 0.00 | 0.00 | BC 468 |
| | | | Links | Min N | -91.79 | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | BC 134 |
| | | | | Max $V_y$ | -19.09 | 0.39 | 23.79 | -0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Min $V_y$ | -70.73 | -0.37 | 21.76 | -0.00 | 0.00 | 0.00 | BC 269 |
| | | | | Max $V_z$ | -42.05 | 0.32 | 23.81 | -0.00 | -0.00 | 0.00 | BC 240 |
| | | | | Min $V_z$ | -46.61 | -0.07 | -22.36 | 0.00 | -0.00 | 0.00 | BC 167 |
| | | | | Max $M_T$ | -32.04 | -0.06 | -22.36 | 0.00 | -0.00 | 0.00 | BC 363 |
| | | | | Min $M_T$ | -59.01 | -0.36 | 21.76 | -0.00 | 0.00 | 0.00 | BC 281 |
| | | | | Max $M_y$ | -40.98 | -0.08 | 13.95 | -0.00 | 0.00 | 0.00 | BC 278 |
| | | | | Min $M_y$ | -42.03 | 0.32 | 23.81 | -0.00 | -0.00 | 0.00 | BC 268 |
| | | | | Max $M_z$ | -52.25 | -0.04 | -0.00 | 0.00 | 0.00 | 0.00 | BC 2 |
| | | | | Min $M_z$ | -77.20 | -0.08 | 0.00 | 0.00 | 0.00 | -0.00 | BC 326 |
| | | | 0 | Max N | -15.77 | 0.35 | 23.81 | -0.00 | 0.00 | -0.00 | BC 468 |
| | | | Rechts | Min N | -91.79 | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | BC 134 |
| | | | | Max $V_y$ | -19.09 | 0.39 | 23.79 | -0.00 | 0.00 | -0.00 | BC 360 |
| | | | | Min $V_y$ | -70.73 | -0.37 | 21.76 | -0.00 | 0.00 | 0.00 | BC 269 |
| | | | | Max $V_z$ | -42.05 | 0.32 | 23.81 | -0.00 | 0.00 | -0.00 | BC 240 |
| | | | | Min $V_z$ | -46.61 | -0.07 | -22.36 | 0.00 | -0.00 | 0.00 | BC 167 |
| | | | | Max $M_T$ | -32.04 | -0.06 | -22.36 | 0.00 | -0.00 | 0.00 | BC 363 |
| | | | | Min $M_T$ | -59.01 | -0.36 | 21.76 | -0.00 | 0.00 | 0.00 | BC 281 |
| | | | | Max $M_y$ | -41.83 | 0.33 | 23.81 | -0.00 | 0.00 | -0.00 | BC 264 |
| | | | | Min $M_y$ | -46.61 | -0.07 | -22.36 | 0.00 | -0.00 | 0.00 | BC 167 |
| | | | | Max $M_z$ | -70.67 | -0.37 | 21.76 | -0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min $M_z$ | -19.13 | 0.39 | 23.79 | -0.00 | 0.00 | -0.00 | BC 356 |
| | | | 2500 | Max N | -13.78 | 0.35 | 8.71 | -0.00 | 40.64 | -0.87 | BC 468 |
| | | | Links | Min N | -88.86 | -0.09 | 0.00 | 0.00 | 0.00 | 0.24 | BC 134 |
| | | | | Max $V_y$ | -17.09 | 0.39 | 8.70 | -0.00 | 40.61 | -0.97 | BC 360 |
| | | | | Min $V_y$ | -67.80 | -0.37 | 8.02 | -0.00 | 37.23 | 0.92 | BC 269 |
| | | | | Max $V_z$ | -39.12 | 0.32 | 8.72 | -0.00 | 40.66 | -0.81 | BC 240 |
| | | | | Min $V_z$ | -43.69 | -0.07 | -8.24 | 0.00 | -38.25 | 0.18 | BC 167 |
| | | | | Max $M_T$ | -30.04 | -0.06 | -8.24 | 0.00 | -38.25 | 0.15 | BC 363 |
| | | | | Min $M_T$ | -56.09 | -0.36 | 8.02 | -0.00 | 37.23 | 0.89 | BC 281 |
| | | | | Max $M_y$ | -39.12 | 0.32 | 8.72 | -0.00 | 40.66 | -0.81 | BC 240 |
| | | | | Min $M_y$ | -43.69 | -0.07 | -8.24 | 0.00 | -38.25 | 0.18 | BC 167 |
| | | | | Max $M_z$ | -67.80 | -0.37 | 8.02 | -0.00 | 37.23 | 0.92 | BC 269 |
| | | | | Min $M_z$ | -17.09 | 0.39 | 8.70 | -0.00 | 40.61 | -0.97 | BC 360 |
| | | | 2500 | Max N | -13.78 | 0.35 | 8.71 | -0.00 | 40.64 | -0.87 | BC 468 |
| | | | Rechts | Min N | -88.86 | -0.09 | 0.00 | 0.00 | 0.00 | 0.24 | BC 134 |
| | | | | Max $V_y$ | -17.09 | 0.39 | 8.70 | -0.00 | 40.61 | -0.97 | BC 360 |
| | | | | Min $V_y$ | -67.80 | -0.37 | 8.02 | -0.00 | 37.23 | 0.92 | BC 269 |
| | | | | Max $V_z$ | -39.12 | 0.32 | 8.72 | -0.00 | 40.66 | -0.81 | BC 240 |
| | | | | Min $V_z$ | -43.69 | -0.07 | -8.24 | 0.00 | -38.25 | 0.18 | BC 167 |
| | | | | Max $M_T$ | -30.04 | -0.06 | -8.24 | 0.00 | -38.25 | 0.15 | BC 363 |
| | | | | Min $M_T$ | -56.09 | -0.36 | 8.02 | -0.00 | 37.23 | 0.89 | BC 281 |
| | | | | Max $M_y$ | -39.12 | 0.32 | 8.72 | -0.00 | 40.66 | -0.81 | BC 240 |
| | | | | Min $M_y$ | -43.69 | -0.07 | -8.24 | 0.00 | -38.25 | 0.18 | BC 167 |
| | | | | Max $M_z$ | -67.80 | -0.37 | 8.02 | -0.00 | 37.23 | 0.92 | BC 269 |
| | | | | Min $M_z$ | -17.09 | 0.39 | 8.70 | -0.00 | 40.61 | -0.97 | BC 360 |
| | | | 4345 | Max N | -9.10 | 0.35 | -2.43 | -0.00 | 46.43 | -1.51 | BC 468 |
| | | | Links | Min N | -81.99 | -0.09 | 0.00 | 0.00 | 0.00 | 0.41 | BC 134 |
| | | | | Max $V_y$ | -12.41 | 0.39 | -2.45 | -0.00 | 46.38 | -1.69 | BC 360 |
| | | | | Min $V_y$ | -60.94 | -0.37 | -2.12 | -0.00 | 42.67 | 1.59 | BC 269 |
| | | | | Max $V_z$ | -34.35 | -0.12 | 2.18 | 0.00 | -43.84 | 0.51 | BC 435 |
| | | | | Min $V_z$ | -23.71 | 0.38 | -2.45 | -0.00 | 46.37 | -1.65 | BC 168 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 31 | RC1 | | | Max $M_T$ | -25.36 | -0.06 | 2.18 | 0.00 | -43.84 | 0.26 | BC 363 |
| | | | | Min $M_T$ | -49.22 | -0.36 | -2.12 | -0.00 | 42.67 | 1.55 | BC 281 |
| | | | | Max $M_y$ | -32.26 | 0.32 | -2.43 | -0.00 | 46.46 | -1.40 | BC 240 |
| | | | | Min $M_y$ | -36.82 | -0.07 | 2.18 | 0.00 | -43.85 | 0.31 | BC 167 |
| | | | | Max $M_z$ | -60.94 | -0.37 | -2.12 | -0.00 | 42.67 | 1.59 | BC 269 |
| | | | | Min $M_z$ | -12.41 | 0.39 | -2.45 | -0.00 | 46.38 | -1.69 | BC 360 |
| | | 79 | 4345 | Max N | -9.10 | 0.35 | -2.43 | -0.00 | 46.43 | -1.51 | BC 468 |
| | | | Rechts | Min N | -81.99 | -0.09 | 0.00 | 0.00 | 0.00 | 0.41 | BC 134 |
| | | | | Max $V_y$ | -12.41 | 0.39 | -2.45 | -0.00 | 46.38 | -1.69 | BC 360 |
| | | | | Min $V_y$ | -60.94 | -0.37 | -2.12 | -0.00 | 42.67 | 1.59 | BC 269 |
| | | | | Max $V_z$ | -34.35 | -0.12 | 2.18 | 0.00 | -43.84 | 0.51 | BC 435 |
| | | | | Min $V_z$ | -23.71 | 0.38 | -2.45 | -0.00 | 46.37 | -1.65 | BC 168 |
| | | | | Max $M_T$ | -25.36 | -0.06 | 2.18 | 0.00 | -43.84 | 0.26 | BC 363 |
| | | | | Min $M_T$ | -49.22 | -0.36 | -2.12 | -0.00 | 42.67 | 1.55 | BC 281 |
| | | | | Max $M_y$ | -32.26 | 0.32 | -2.43 | -0.00 | 46.46 | -1.40 | BC 240 |
| | | | | Min $M_y$ | -36.82 | -0.07 | 2.18 | 0.00 | -43.85 | 0.31 | BC 167 |
| | | | | Max $M_z$ | -60.94 | -0.37 | -2.12 | -0.00 | 42.67 | 1.59 | BC 269 |
| | | | | Min $M_z$ | -12.41 | 0.39 | -2.45 | -0.00 | 46.38 | -1.69 | BC 360 |
| 32 | RC1 | 59 | 0 | Max N | -33.75 | 0.02 | -17.34 | -0.00 | 0.00 | 0.00 | BC 419 |
| | | | Links | Min N | -99.63 | -0.27 | 16.81 | 0.00 | -0.00 | 0.00 | BC 172 |
| | | | | Max $V_y$ | -78.50 | 0.42 | 18.55 | 0.00 | -0.00 | 0.00 | BC 433 |
| | | | | Min $V_y$ | -75.53 | -0.30 | 16.83 | 0.00 | -0.00 | 0.00 | BC 360 |
| | | | | Max $V_z$ | -78.08 | 0.42 | 18.55 | 0.00 | -0.00 | 0.00 | BC 461 |
| | | | | Min $V_z$ | -60.98 | 0.03 | -17.36 | -0.00 | 0.00 | 0.00 | BC 187 |
| | | | | Max $M_T$ | -91.33 | -0.28 | 16.81 | 0.00 | -0.00 | 0.00 | BC 164 |
| | | | | Min $M_T$ | -61.66 | 0.03 | -17.36 | -0.00 | 0.00 | 0.00 | BC 235 |
| | | | | Max $M_y$ | -67.63 | 0.41 | 18.55 | 0.00 | 0.00 | -0.00 | BC 381 |
| | | | | Min $M_y$ | -43.69 | 0.02 | -17.34 | -0.00 | -0.00 | 0.00 | BC 379 |
| | | | | Max $M_z$ | -61.18 | 0.07 | -0.05 | -0.00 | 0.00 | 0.00 | BC 3 |
| | | | | Min $M_z$ | -67.63 | 0.41 | 18.55 | 0.00 | 0.00 | -0.00 | BC 381 |
| | | | 0 | Max N | -33.75 | 0.02 | -17.34 | -0.00 | -0.00 | -0.00 | BC 419 |
| | | | Rechts | Min N | -99.63 | -0.27 | 16.81 | 0.00 | 0.00 | 0.00 | BC 172 |
| | | | | Max $V_y$ | -78.50 | 0.42 | 18.55 | 0.00 | 0.00 | -0.00 | BC 433 |
| | | | | Min $V_y$ | -75.53 | -0.30 | 16.83 | 0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Max $V_z$ | -78.08 | 0.42 | 18.55 | 0.00 | 0.00 | -0.00 | BC 461 |
| | | | | Min $V_z$ | -60.98 | 0.03 | -17.36 | -0.00 | -0.00 | -0.00 | BC 187 |
| | | | | Max $M_T$ | -91.33 | -0.28 | 16.81 | 0.00 | 0.00 | 0.00 | BC 164 |
| | | | | Min $M_T$ | -61.66 | 0.03 | -17.36 | -0.00 | -0.00 | -0.00 | BC 235 |
| | | | | Max $M_y$ | -67.63 | 0.41 | 18.55 | 0.00 | 0.00 | -0.00 | BC 381 |
| | | | | Min $M_y$ | -43.69 | 0.02 | -17.34 | -0.00 | -0.00 | -0.00 | BC 379 |
| | | | | Max $M_z$ | -75.53 | -0.30 | 16.83 | 0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Min $M_z$ | -78.50 | 0.42 | 18.55 | 0.00 | 0.00 | -0.00 | BC 433 |
| | | | 2173 | Max N | -32.01 | 0.02 | -5.04 | -0.00 | -24.31 | -0.04 | BC 419 |
| | | | Links | Min N | -97.09 | -0.27 | 4.83 | 0.00 | 23.50 | 0.59 | BC 172 |
| | | | | Max $V_y$ | -76.76 | 0.42 | 5.43 | 0.00 | 26.05 | -0.92 | BC 433 |
| | | | | Min $V_y$ | -73.79 | -0.30 | 4.84 | 0.00 | 23.54 | 0.66 | BC 360 |
| | | | | Max $V_z$ | -76.34 | 0.42 | 5.43 | 0.00 | 26.05 | -0.92 | BC 461 |
| | | | | Min $V_z$ | -58.44 | 0.03 | -5.06 | -0.00 | -24.35 | -0.06 | BC 187 |
| | | | | Max $M_T$ | -88.79 | -0.28 | 4.83 | 0.00 | 23.50 | 0.61 | BC 164 |
| | | | | Min $M_T$ | -59.11 | 0.03 | -5.06 | -0.00 | -24.34 | -0.07 | BC 235 |
| | | | | Max $M_y$ | -76.34 | 0.42 | 5.43 | 0.00 | 26.05 | -0.92 | BC 461 |
| | | | | Min $M_y$ | -58.44 | 0.03 | -5.06 | -0.00 | -24.35 | -0.06 | BC 187 |
| | | | | Max $M_z$ | -73.79 | -0.30 | 4.84 | 0.00 | 23.54 | 0.66 | BC 360 |
| | | | | Min $M_z$ | -76.76 | 0.42 | 5.43 | 0.00 | 26.05 | -0.92 | BC 433 |
| | | 92 | 2173 | Max N | -32.01 | 0.02 | -5.04 | -0.00 | -24.31 | -0.04 | BC 419 |
| | | | Rechts | Min N | -97.09 | -0.27 | 4.83 | 0.00 | 23.50 | 0.59 | BC 172 |
| | | | | Max $V_y$ | -76.76 | 0.42 | 5.43 | 0.00 | 26.05 | -0.92 | BC 433 |
| | | | | Min $V_y$ | -73.79 | -0.30 | 4.84 | 0.00 | 23.54 | 0.66 | BC 360 |
| | | | | Max $V_z$ | -76.34 | 0.42 | 5.43 | 0.00 | 26.05 | -0.92 | BC 461 |
| | | | | Min $V_z$ | -58.44 | 0.03 | -5.06 | -0.00 | -24.35 | -0.06 | BC 187 |
| | | | | Max $M_T$ | -88.79 | -0.28 | 4.83 | 0.00 | 23.50 | 0.61 | BC 164 |
| | | | | Min $M_T$ | -59.11 | 0.03 | -5.06 | -0.00 | -24.34 | -0.07 | BC 235 |
| | | | | Max $M_y$ | -76.34 | 0.42 | 5.43 | 0.00 | 26.05 | -0.92 | BC 461 |
| | | | | Min $M_y$ | -58.44 | 0.03 | -5.06 | -0.00 | -24.35 | -0.06 | BC 187 |
| | | | | Max $M_z$ | -73.79 | -0.30 | 4.84 | 0.00 | 23.54 | 0.66 | BC 360 |
| | | | | Min $M_z$ | -76.76 | 0.42 | 5.43 | 0.00 | 26.05 | -0.92 | BC 433 |
| 33 | RC1 | 101 | 0 | Max N | 20.74 | -0.81 | -8.39 | 0.08 | 1.68 | -0.18 | BC 408 |
| | | | Links | Min N | -12.52 | -0.32 | -18.04 | 0.11 | 3.62 | -0.10 | BC 246 |
| | | | | Max $V_y$ | -7.66 | 0.53 | -34.16 | 0.15 | 6.84 | 0.11 | BC 131 |
| | | | | Min $V_y$ | 7.78 | -0.92 | -8.39 | 0.08 | 1.69 | -0.21 | BC 448 |
| | | | | Max $V_z$ | 11.52 | 0.07 | -8.36 | 0.05 | 1.68 | -0.02 | BC 411 |
| | | | | Min $V_z$ | -8.58 | 0.52 | -34.16 | 0.15 | 6.84 | 0.10 | BC 149 |
| | | | | Max $M_T$ | -2.07 | 0.45 | -34.16 | 0.15 | 6.84 | 0.09 | BC 155 |
| | | | | Min $M_T$ | -1.98 | 0.11 | -8.36 | 0.04 | 1.68 | 0.02 | BC 42 |
| | | | | Max $M_y$ | -2.12 | 0.45 | -34.16 | 0.15 | 6.84 | 0.09 | BC 148 |
| | | | | Min $M_y$ | 11.52 | 0.07 | -8.36 | 0.05 | 1.68 | -0.02 | BC 411 |
| | | | | Max $M_z$ | -7.66 | 0.53 | -34.16 | 0.15 | 6.84 | 0.11 | BC 131 |
| | | | | Min $M_z$ | 7.78 | -0.92 | -8.39 | 0.08 | 1.69 | -0.21 | BC 448 |
| | | | 0 | Max N | 20.74 | -0.81 | -8.39 | 0.08 | 1.68 | -0.18 | BC 408 |
| | | | Rechts | Min N | -12.52 | -0.32 | -18.04 | 0.11 | 3.62 | -0.10 | BC 246 |
| | | | | Max $V_y$ | -7.66 | 0.53 | -34.16 | 0.15 | 6.84 | 0.11 | BC 131 |
| | | | | Min $V_y$ | 7.78 | -0.92 | -8.39 | 0.08 | 1.69 | -0.21 | BC 448 |
| | | | | Max $V_z$ | 11.52 | 0.07 | -8.36 | 0.05 | 1.68 | -0.02 | BC 411 |
| | | | | Min $V_z$ | -8.58 | 0.52 | -34.16 | 0.15 | 6.84 | 0.10 | BC 149 |
| | | | | Max $M_T$ | -2.07 | 0.45 | -34.16 | 0.15 | 6.84 | 0.09 | BC 155 |
| | | | | Min $M_T$ | -1.98 | 0.11 | -8.36 | 0.04 | 1.68 | 0.02 | BC 42 |
| | | | | Max $M_y$ | -2.12 | 0.45 | -34.16 | 0.15 | 6.84 | 0.09 | BC 148 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 33 | RC1 | | | Min $M_y$ | 11.52 | 0.07 | -8.36 | 0.05 | 1.68 | -0.02 | BC 411 |
| | | | | Max $M_z$ | -7.66 | 0.53 | -34.16 | 0.15 | 6.84 | 0.11 | BC 131 |
| | | | | Min $M_z$ | 7.78 | -0.92 | -8.39 | 0.08 | 1.69 | -0.21 | BC 448 |
| | | | 200 | Max N | 20.74 | -1.04 | -8.46 | 0.08 | 0.00 | -0.00 | BC 408 |
| | | | Links | Min N | -12.52 | -0.69 | -18.15 | 0.11 | 0.00 | -0.00 | BC 246 |
| | | | | Max $V_y$ | -7.66 | 0.53 | -34.27 | 0.15 | 0.00 | 0.00 | BC 131 |
| | | | | Min $V_y$ | 7.78 | -1.16 | -8.47 | 0.08 | 0.00 | -0.00 | BC 448 |
| | | | | Max $V_z$ | 11.52 | -0.30 | -8.43 | 0.05 | 0.00 | -0.00 | BC 411 |
| | | | | Min $V_z$ | -8.58 | 0.52 | -34.27 | 0.15 | 0.00 | 0.00 | BC 149 |
| | | | | Max $M_T$ | -2.07 | 0.45 | -34.27 | 0.15 | 0.00 | 0.00 | BC 155 |
| | | | | Min $M_T$ | -1.98 | 0.11 | -8.43 | 0.04 | 0.00 | 0.00 | BC 42 |
| | | | | Max $M_y$ | -8.45 | 0.52 | -34.27 | 0.15 | 0.00 | 0.00 | BC 146 |
| | | | | Min $M_y$ | 6.43 | 0.04 | -8.43 | 0.04 | 0.00 | 0.00 | BC 56 |
| | | | | Max $M_z$ | -7.66 | 0.53 | -34.27 | 0.15 | 0.00 | 0.00 | BC 131 |
| | | | | Min $M_z$ | -2.34 | -1.15 | -8.47 | 0.08 | 0.00 | -0.00 | BC 358 |
| | | 63 | 200 | Max N | 20.74 | -1.04 | -8.46 | 0.08 | 0.00 | 0.00 | BC 408 |
| | | | Rechts | Min N | -12.52 | -0.69 | -18.15 | 0.11 | -0.00 | 0.00 | BC 246 |
| | | | | Max $V_y$ | -7.66 | 0.53 | -34.27 | 0.15 | 0.00 | 0.00 | BC 131 |
| | | | | Min $V_y$ | 7.78 | -1.16 | -8.47 | 0.08 | 0.00 | 0.00 | BC 448 |
| | | | | Max $V_z$ | 11.52 | -0.30 | -8.43 | 0.05 | 0.00 | 0.00 | BC 411 |
| | | | | Min $V_z$ | -8.58 | 0.52 | -34.27 | 0.15 | 0.00 | 0.00 | BC 149 |
| | | | | Max $M_T$ | -2.07 | 0.45 | -34.27 | 0.15 | 0.00 | 0.00 | BC 155 |
| | | | | Min $M_T$ | -1.98 | 0.11 | -8.43 | 0.04 | 0.00 | 0.00 | BC 42 |
| | | | | Max $M_y$ | -8.45 | 0.52 | -34.27 | 0.15 | 0.00 | 0.00 | BC 146 |
| | | | | Min $M_y$ | -7.07 | -0.86 | -14.22 | 0.09 | -0.00 | 0.00 | BC 406 |
| | | | | Max $M_z$ | -9.11 | -0.85 | -14.22 | 0.09 | -0.00 | 0.00 | BC 378 |
| | | | | Min $M_z$ | 9.66 | -1.09 | -8.47 | 0.08 | 0.00 | -0.00 | BC 356 |
| 34 | RC1 | 42 | 0 | Max N | 4.87 | 0.09 | 16.82 | 0.01 | 0.00 | 0.00 | BC 243 |
| | | | | Min N | -41.63 | -0.01 | 11.05 | -0.01 | 0.00 | 0.00 | BC 168 |
| | | | | Max $V_y$ | 4.65 | 0.12 | 7.55 | 0.01 | -0.00 | 0.00 | BC 447 |
| | | | | Min $V_y$ | -20.08 | -0.11 | 7.53 | -0.01 | 0.00 | 0.00 | BC 357 |
| | | | | Max $V_z$ | 0.94 | -0.02 | 32.95 | -0.00 | 0.00 | 0.00 | BC 131 |
| | | | | Min $V_z$ | -19.74 | -0.11 | 7.53 | -0.01 | 0.00 | 0.00 | BC 477 |
| | | | | Max $M_T$ | 4.65 | 0.12 | 7.55 | 0.01 | -0.00 | 0.00 | BC 447 |
| | | | | Min $M_T$ | -20.08 | -0.11 | 7.53 | -0.01 | 0.00 | 0.00 | BC 357 |
| | | | | Max $M_y$ | -40.46 | -0.01 | 16.81 | -0.01 | 0.00 | 0.00 | BC 172 |
| | | | | Min $M_y$ | -5.95 | -0.07 | 11.06 | -0.01 | -0.00 | -0.00 | BC 278 |
| | | | | Max $M_z$ | -36.24 | -0.03 | 13.29 | -0.01 | 0.00 | 0.00 | BC 368 |
| | | | | Min $M_z$ | -41.52 | -0.02 | 7.53 | -0.01 | -0.00 | -0.00 | BC 356 |
| | | 151 | 3256 | Max N | 4.56 | 0.09 | 0.61 | 0.01 | 28.38 | -0.31 | BC 243 |
| | | | | Min N | -41.83 | -0.01 | 0.61 | -0.01 | 18.97 | 0.03 | BC 168 |
| | | | | Max $V_y$ | 4.52 | 0.12 | 0.43 | 0.01 | 12.99 | -0.40 | BC 447 |
| | | | | Min $V_y$ | -20.21 | -0.11 | 0.41 | -0.01 | 12.93 | 0.35 | BC 357 |
| | | | | Max $V_z$ | -1.07 | -0.02 | 0.69 | -0.00 | 21.44 | 0.05 | BC 3 |
| | | | | Min $V_z$ | 0.59 | -0.01 | 0.37 | -0.00 | 48.50 | 0.03 | BC 347 |
| | | | | Max $M_T$ | 4.52 | 0.12 | 0.43 | 0.01 | 12.99 | -0.40 | BC 447 |
| | | | | Min $M_T$ | -20.21 | -0.11 | 0.41 | -0.01 | 12.93 | 0.35 | BC 357 |
| | | | | Max $M_y$ | 0.33 | -0.02 | 0.57 | -0.00 | 54.55 | 0.06 | BC 131 |
| | | | | Min $M_y$ | -19.88 | -0.11 | 0.41 | -0.01 | 12.93 | 0.35 | BC 477 |
| | | | | Max $M_z$ | -20.21 | -0.11 | 0.41 | -0.01 | 12.93 | 0.35 | BC 357 |
| | | | | Min $M_z$ | 4.52 | 0.12 | 0.43 | 0.01 | 12.99 | -0.40 | BC 447 |
| 35 | RC1 | 44 | 0 | Max N | 133.50 | 4.18 | -27.50 | -3.69 | 64.57 | -9.05 | BC 433 |
| | | | | Min N | -177.98 | 12.50 | 19.31 | 9.82 | -35.15 | 4.50 | BC 164 |
| | | | | Max $V_y$ | -120.66 | 15.30 | 27.54 | 8.10 | -5.54 | -4.03 | BC 264 |
| | | | | Min $V_y$ | 75.64 | 1.14 | -35.77 | -2.13 | 35.14 | -0.57 | BC 417 |
| | | | | Max $V_z$ | -102.50 | 12.75 | 33.06 | 6.62 | -6.95 | -4.69 | BC 468 |
| | | | | Min $V_z$ | 61.77 | 3.73 | -41.65 | -0.54 | 37.02 | 0.09 | BC 185 |
| | | | | Max $M_T$ | -175.34 | 13.10 | 15.78 | 10.00 | -33.07 | 4.56 | BC 200 |
| | | | | Min $M_T$ | 131.38 | 3.43 | -23.67 | -3.92 | 62.51 | -9.17 | BC 469 |
| | | | | Max $M_y$ | 133.02 | 4.16 | -27.44 | -3.70 | 64.78 | -9.10 | BC 461 |
| | | | | Min $M_y$ | -176.30 | 12.45 | 19.13 | 9.80 | -35.18 | 4.54 | BC 168 |
| | | | | Max $M_z$ | -173.99 | 13.07 | 15.65 | 9.99 | -33.16 | 4.60 | BC 172 |
| | | | | Min $M_z$ | 132.39 | 3.41 | -23.94 | -3.90 | 62.85 | -9.19 | BC 473 |
| | | | 1505 | Max N | 23.64 | -4.42 | -20.61 | -9.53 | 11.17 | -0.34 | BC 389 |
| | | | | Min N | -129.62 | -7.49 | -31.79 | 19.27 | -15.78 | 1.05 | BC 264 |
| | | | | Max $V_y$ | -121.36 | 8.56 | 23.20 | 7.57 | -20.16 | 2.06 | BC 168 |
| | | | | Min $V_y$ | 16.19 | -20.46 | -75.63 | 2.18 | 15.66 | -1.36 | BC 461 |
| | | | | Max $V_z$ | -104.32 | 8.37 | 24.07 | 7.42 | -17.81 | 1.75 | BC 360 |
| | | | | Min $V_z$ | -0.85 | -20.26 | -76.47 | 2.22 | 13.07 | -1.02 | BC 241 |
| | | | | Max $M_T$ | -126.42 | -7.21 | -30.03 | 19.60 | -14.89 | 0.96 | BC 276 |
| | | | | Min $M_T$ | 21.96 | -4.73 | -22.55 | -9.88 | 10.54 | -0.27 | BC 377 |
| | | | | Max $M_y$ | 22.49 | -18.93 | -69.67 | 1.37 | 16.79 | -1.42 | BC 413 |
| | | | | Min $M_y$ | -125.80 | 7.02 | 17.25 | 8.41 | -21.18 | 2.10 | BC 232 |
| | | | | Max $M_z$ | -122.92 | 8.26 | 21.35 | 7.24 | -20.87 | 2.14 | BC 172 |
| | | | | Min $M_z$ | 19.41 | -20.17 | -73.78 | 2.53 | 16.46 | -1.45 | BC 473 |
| | | | 1505 | Max N | 23.64 | -4.42 | -20.61 | -9.53 | 11.17 | -0.34 | BC 389 |
| | | | | Min N | -129.62 | -7.49 | -31.79 | 19.27 | -15.78 | 1.05 | BC 264 |
| | | | | Max $V_y$ | -121.36 | 8.56 | 23.20 | 7.57 | -20.16 | 2.06 | BC 168 |
| | | | | Min $V_y$ | 16.19 | -20.46 | -75.63 | 2.18 | 15.66 | -1.36 | BC 461 |
| | | | | Max $V_z$ | -104.32 | 8.37 | 24.07 | 7.42 | -17.81 | 1.75 | BC 360 |
| | | | | Min $V_z$ | -0.85 | -20.26 | -76.47 | 2.22 | 13.07 | -1.02 | BC 241 |
| | | | | Max $M_T$ | -126.42 | -7.21 | -30.03 | 19.60 | -14.89 | 0.96 | BC 276 |
| | | | | Min $M_T$ | 21.96 | -4.73 | -22.55 | -9.88 | 10.54 | -0.27 | BC 377 |
| | | | | Max $M_y$ | 22.49 | -18.93 | -69.67 | 1.37 | 16.79 | -1.42 | BC 413 |
| | | | | Min $M_y$ | -125.80 | 7.02 | 17.25 | 8.41 | -21.18 | 2.10 | BC 232 |
| | | | | Max $M_z$ | -122.92 | 8.26 | 21.35 | 7.24 | -20.87 | 2.14 | BC 172 |
| | | | | Min $M_z$ | 19.41 | -20.17 | -73.78 | 2.53 | 16.46 | -1.45 | BC 473 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 35 | RC1 | | 5005 | Max N | 23.57 | 4.48 | 21.33 | 9.85 | 11.80 | -0.39 | BC 360 |
| | | | | Min N | -144.37 | 6.46 | 26.73 | -21.75 | -21.53 | 1.14 | BC 269 |
| | | | | Max $V_y$ | -5.28 | 19.28 | 69.73 | -4.81 | 9.44 | -1.21 | BC 456 |
| | | | | Min $V_y$ | -114.42 | -8.35 | -21.79 | -7.12 | -19.24 | 1.96 | BC 197 |
| | | | | Max $V_z$ | -21.70 | 19.27 | 71.15 | -4.72 | 7.38 | -0.93 | BC 264 |
| | | | | Min $V_z$ | -99.05 | -8.33 | -23.18 | -7.17 | -17.23 | 1.68 | BC 389 |
| | | | | Max $M_T$ | 4.72 | 4.57 | 23.88 | 9.98 | 8.64 | -0.01 | BC 172 |
| | | | | Min $M_T$ | -122.90 | 6.38 | 24.19 | -21.92 | -18.15 | 0.74 | BC 473 |
| | | | | Max $M_y$ | 22.85 | 4.56 | 21.55 | 9.85 | 12.05 | -0.41 | BC 356 |
| | | | | Min $M_y$ | -144.21 | 6.35 | 26.43 | -21.75 | -21.82 | 1.17 | BC 241 |
| | | | | Max $M_z$ | -118.33 | -8.27 | -20.68 | -7.07 | -20.42 | 2.06 | BC 185 |
| | | | | Min $M_z$ | -0.61 | 19.16 | 68.53 | -4.93 | 10.72 | -1.32 | BC 468 |
| | | | 5005 | Max N | 23.57 | 4.48 | 21.33 | 9.85 | 11.80 | -0.39 | BC 360 |
| | | | | Min N | -144.37 | 6.46 | 26.73 | -21.75 | -21.53 | 1.14 | BC 269 |
| | | | | Max $V_y$ | -5.28 | 19.28 | 69.73 | -4.81 | 9.44 | -1.21 | BC 456 |
| | | | | Min $V_y$ | -114.42 | -8.35 | -21.79 | -7.12 | -19.24 | 1.96 | BC 197 |
| | | | | Max $V_z$ | -21.70 | 19.27 | 71.15 | -4.72 | 7.38 | -0.93 | BC 264 |
| | | | | Min $V_z$ | -99.05 | -8.33 | -23.18 | -7.17 | -17.23 | 1.68 | BC 389 |
| | | | | Max $M_T$ | 4.72 | 4.57 | 23.88 | 9.98 | 8.64 | -0.01 | BC 172 |
| | | | | Min $M_T$ | -122.90 | 6.38 | 24.19 | -21.92 | -18.15 | 0.74 | BC 473 |
| | | | | Max $M_y$ | 22.85 | 4.56 | 21.55 | 9.85 | 12.05 | -0.41 | BC 356 |
| | | | | Min $M_y$ | -144.21 | 6.35 | 26.43 | -21.75 | -21.82 | 1.17 | BC 241 |
| | | | | Max $M_z$ | -118.33 | -8.27 | -20.68 | -7.07 | -20.42 | 2.06 | BC 185 |
| | | | | Min $M_z$ | -0.61 | 19.16 | 68.53 | -4.93 | 10.72 | -1.32 | BC 468 |
| | | 47 | 6510 | Max N | 112.40 | -2.69 | 30.24 | 3.87 | 58.10 | -9.14 | BC 468 |
| | | | | Min N | -168.04 | -13.01 | -15.05 | -9.56 | -31.99 | 4.35 | BC 213 |
| | | | | Max $V_y$ | 77.94 | -1.14 | 36.45 | 2.54 | 36.39 | -0.67 | BC 356 |
| | | | | Min $V_y$ | -135.69 | -14.69 | -21.21 | -8.22 | -10.71 | -4.02 | BC 241 |
| | | | | Max $V_z$ | 62.77 | -3.74 | 41.87 | 1.05 | 38.08 | -0.09 | BC 200 |
| | | | | Min $V_z$ | -117.53 | -11.97 | -26.48 | -6.76 | -12.00 | -4.64 | BC 445 |
| | | | | Max $M_T$ | 112.40 | -2.69 | 30.24 | 3.87 | 58.10 | -9.14 | BC 468 |
| | | | | Min $M_T$ | -168.03 | -13.06 | -15.19 | -9.61 | -32.41 | 4.42 | BC 185 |
| | | | | Max $M_y$ | 95.00 | -5.30 | 35.71 | 2.48 | 59.59 | -8.53 | BC 264 |
| | | | | Min $M_y$ | -152.05 | -10.35 | -20.55 | -8.10 | -34.01 | 3.83 | BC 389 |
| | | | | Max $M_z$ | -168.03 | -13.06 | -15.19 | -9.61 | -32.41 | 4.42 | BC 185 |
| | | | | Min $M_z$ | 112.40 | -2.69 | 30.24 | 3.87 | 58.10 | -9.14 | BC 468 |
| 36 | RC1 | 47 | 0 | Max N | 111.47 | -6.85 | -61.59 | 0.15 | 58.52 | -9.19 | BC 468 |
| | | | | Min N | -153.32 | -16.76 | -18.43 | -12.96 | -42.30 | 3.80 | BC 213 |
| | | | | Max $V_y$ | -15.65 | -1.44 | -25.63 | -1.92 | 3.52 | 1.60 | BC 358 |
| | | | | Min $V_y$ | -121.30 | -18.86 | -26.19 | -10.67 | -20.90 | -4.53 | BC 241 |
| | | | | Max $V_z$ | -137.86 | -14.09 | 2.11 | -11.06 | -43.93 | 3.24 | BC 417 |
| | | | | Min $V_z$ | 93.99 | -9.46 | -82.33 | -1.68 | 59.66 | -8.53 | BC 236 |
| | | | | Max $M_T$ | 20.76 | -3.44 | -33.54 | 0.38 | 26.13 | -6.86 | BC 470 |
| | | | | Min $M_T$ | -153.27 | -16.80 | -18.37 | -13.01 | -42.76 | 3.87 | BC 185 |
| | | | | Max $M_y$ | 94.00 | -9.43 | -82.32 | -1.66 | 60.04 | -8.60 | BC 264 |
| | | | | Min $M_y$ | -137.39 | -14.12 | 2.06 | -11.09 | -44.26 | 3.30 | BC 389 |
| | | | | Max $M_z$ | -153.27 | -16.80 | -18.37 | -13.01 | -42.76 | 3.87 | BC 185 |
| | | | | Min $M_z$ | 111.47 | -6.85 | -61.59 | 0.15 | 58.52 | -9.19 | BC 468 |
| | | | 1515 | Max N | -11.02 | -8.12 | -34.91 | -11.51 | -1.94 | 2.23 | BC 360 |
| | | | | Min N | -260.12 | -23.73 | -75.76 | 7.13 | -62.70 | 6.09 | BC 269 |
| | | | | Max $V_y$ | -145.43 | -0.92 | 3.17 | -8.08 | -38.14 | 4.49 | BC 389 |
| | | | | Min $V_y$ | -125.75 | -30.90 | -113.79 | 3.74 | -26.55 | 3.83 | BC 264 |
| | | | | Max $V_z$ | -145.43 | -0.92 | 3.17 | -8.08 | -38.14 | 4.49 | BC 389 |
| | | | | Min $V_z$ | -125.75 | -30.90 | -113.79 | 3.74 | -26.55 | 3.83 | BC 264 |
| | | | | Max $M_T$ | -203.48 | -19.66 | -59.79 | 11.65 | -48.02 | 3.89 | BC 469 |
| | | | | Min $M_T$ | -167.44 | -12.12 | -48.62 | -16.79 | -45.36 | 7.05 | BC 134 |
| | | | | Max $M_y$ | -11.88 | -8.22 | -35.22 | -11.36 | -1.72 | 2.20 | BC 356 |
| | | | | Min $M_y$ | -259.99 | -23.64 | -75.47 | 6.99 | -63.11 | 6.14 | BC 241 |
| | | | | Max $M_z$ | -175.08 | -13.89 | -54.64 | -15.35 | -47.07 | 7.16 | BC 149 |
| | | | | Min $M_z$ | -62.13 | -25.04 | -91.59 | 6.75 | -10.38 | 1.54 | BC 408 |
| | | | 1515 | Max N | -11.02 | -8.12 | -34.91 | -11.51 | -1.94 | 2.23 | BC 360 |
| | | | | Min N | -260.12 | -23.73 | -75.76 | 7.13 | -62.70 | 6.09 | BC 269 |
| | | | | Max $V_y$ | -145.43 | -0.92 | 3.17 | -8.08 | -38.14 | 4.49 | BC 389 |
| | | | | Min $V_y$ | -125.75 | -30.90 | -113.79 | 3.74 | -26.55 | 3.83 | BC 264 |
| | | | | Max $V_z$ | -145.43 | -0.92 | 3.17 | -8.08 | -38.14 | 4.49 | BC 389 |
| | | | | Min $V_z$ | -125.75 | -30.90 | -113.79 | 3.74 | -26.55 | 3.83 | BC 264 |
| | | | | Max $M_T$ | -203.48 | -19.66 | -59.79 | 11.65 | -48.02 | 3.89 | BC 469 |
| | | | | Min $M_T$ | -167.44 | -12.12 | -48.62 | -16.79 | -45.36 | 7.05 | BC 134 |
| | | | | Max $M_y$ | -11.88 | -8.22 | -35.22 | -11.36 | -1.72 | 2.20 | BC 356 |
| | | | | Min $M_y$ | -259.99 | -23.64 | -75.47 | 6.99 | -63.11 | 6.14 | BC 241 |
| | | | | Max $M_z$ | -175.08 | -13.89 | -54.64 | -15.35 | -47.07 | 7.16 | BC 149 |
| | | | | Min $M_z$ | -62.13 | -25.04 | -91.59 | 6.75 | -10.38 | 1.54 | BC 408 |
| | | | 5015 | Max N | -89.66 | 4.40 | 7.28 | -23.58 | -25.74 | 4.86 | BC 362 |
| | | | | Min N | -341.63 | 30.85 | 77.46 | -60.60 | -118.48 | 16.33 | BC 155 |
| | | | | Max $V_y$ | -341.63 | 30.85 | 77.46 | -60.60 | -118.48 | 16.33 | BC 155 |
| | | | | Min $V_y$ | -101.27 | 3.88 | 6.32 | -29.67 | -30.07 | 5.57 | BC 360 |
| | | | | Max $V_z$ | -341.63 | 30.85 | 77.46 | -60.60 | -118.48 | 16.33 | BC 155 |
| | | | | Min $V_z$ | -102.81 | 4.03 | 6.24 | -29.62 | -30.54 | 5.63 | BC 356 |
| | | | | Max $M_T$ | -111.35 | 7.09 | 15.89 | -20.60 | -31.99 | 5.31 | BC 357 |
| | | | | Min $M_T$ | -339.75 | 30.65 | 77.37 | -60.66 | -117.80 | 16.25 | BC 148 |
| | | | | Max $M_y$ | -89.66 | 4.40 | 7.28 | -23.58 | -25.74 | 4.86 | BC 362 |
| | | | | Min $M_y$ | -341.63 | 30.85 | 77.46 | -60.60 | -118.48 | 16.33 | BC 155 |
| | | | | Max $M_z$ | -341.63 | 30.85 | 77.46 | -60.60 | -118.48 | 16.33 | BC 155 |
| | | | | Min $M_z$ | -89.66 | 4.40 | 7.28 | -23.58 | -25.74 | 4.86 | BC 362 |
| | | | 5015 | Max N | -89.66 | 4.40 | 7.28 | -23.58 | -25.74 | 4.86 | BC 362 |
| | | | | Min N | -341.63 | 30.85 | 77.46 | -60.60 | -118.48 | 16.33 | BC 155 |
| | | | | Max $V_y$ | -341.63 | 30.85 | 77.46 | -60.60 | -118.48 | 16.33 | BC 155 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 36 | RC1 | | | Min $V_y$ | -101.27 | 3.88 | 6.32 | -29.67 | -30.07 | 5.57 | BC 360 |
| | | | | Max $V_z$ | -341.63 | 30.85 | 77.46 | -60.60 | -118.48 | 16.33 | BC 155 |
| | | | | Min $V_z$ | -102.81 | 4.03 | 6.24 | -29.62 | -30.54 | 5.63 | BC 356 |
| | | | | Max $M_T$ | -111.35 | 7.09 | 15.89 | -20.60 | -31.99 | 5.31 | BC 357 |
| | | | | Min $M_T$ | -339.75 | 30.65 | 77.37 | -60.66 | -117.80 | 16.25 | BC 148 |
| | | | | Max $M_y$ | -89.66 | 4.40 | 7.28 | -23.58 | -25.74 | 4.86 | BC 362 |
| | | | | Min $M_y$ | -341.63 | 30.85 | 77.46 | -60.60 | -118.48 | 16.33 | BC 155 |
| | | | | Max $M_z$ | -341.63 | 30.85 | 77.46 | -60.60 | -118.48 | 16.33 | BC 155 |
| | | | | Min $M_z$ | -89.66 | 4.40 | 7.28 | -23.58 | -25.74 | 4.86 | BC 362 |
| | | 6 | 6530 | Max N | -30.05 | 17.53 | 17.33 | -25.76 | -23.49 | 2.43 | BC 362 |
| | | | | Min N | -87.09 | 36.10 | 95.68 | -70.14 | -59.83 | 6.31 | BC 155 |
| | | | | Max $V_y$ | -80.98 | 37.79 | 68.87 | -61.87 | -54.91 | 5.85 | BC 156 |
| | | | | Min $V_y$ | -39.71 | 16.01 | 52.39 | -32.17 | -25.93 | 2.72 | BC 381 |
| | | | | Max $V_z$ | -87.09 | 36.10 | 95.68 | -70.14 | -59.83 | 6.31 | BC 155 |
| | | | | Min $V_z$ | -30.05 | 17.53 | 17.33 | -25.76 | -23.49 | 2.43 | BC 362 |
| | | | | Max $M_T$ | -33.86 | 17.48 | 26.93 | -24.18 | -21.12 | 2.28 | BC 361 |
| | | | | Min $M_T$ | -87.09 | 36.10 | 95.68 | -70.14 | -59.83 | 6.31 | BC 155 |
| | | | | Max $M_y$ | -33.86 | 17.48 | 26.93 | -24.18 | -21.12 | 2.28 | BC 361 |
| | | | | Min $M_y$ | -87.09 | 36.10 | 95.68 | -70.14 | -59.83 | 6.31 | BC 155 |
| | | | | Max $M_z$ | -87.09 | 36.10 | 95.68 | -70.14 | -59.83 | 6.31 | BC 155 |
| | | | | Min $M_z$ | -33.86 | 17.48 | 26.93 | -24.18 | -21.12 | 2.28 | BC 361 |
| 37 | RC1 | 102 | 0 | Max N | 34.41 | 0.57 | -18.19 | 0.08 | 3.65 | 0.11 | BC 204 |
| | | | | Min N | -9.40 | -0.29 | -18.22 | 0.11 | 3.65 | -0.06 | BC 247 |
| | | | | Max $V_y$ | 32.07 | 0.93 | -8.41 | 0.01 | 1.69 | 0.19 | BC 448 |
| | | | | Min $V_y$ | 3.40 | -0.53 | -34.52 | 0.22 | 6.91 | -0.11 | BC 131 |
| | | | | Max $V_z$ | 32.07 | 0.93 | -8.41 | 0.01 | 1.69 | 0.19 | BC 448 |
| | | | | Min $V_z$ | 3.65 | -0.52 | -34.52 | 0.22 | 6.91 | -0.10 | BC 138 |
| | | | | Max $M_T$ | 3.40 | -0.53 | -34.52 | 0.22 | 6.91 | -0.11 | BC 131 |
| | | | | Min $M_T$ | 32.07 | 0.93 | -8.41 | 0.01 | 1.69 | 0.19 | BC 448 |
| | | | | Max $M_y$ | 3.65 | -0.52 | -34.52 | 0.22 | 6.91 | -0.10 | BC 138 |
| | | | | Min $M_y$ | 32.07 | 0.93 | -8.41 | 0.01 | 1.69 | 0.19 | BC 448 |
| | | | | Max $M_z$ | 32.07 | 0.93 | -8.41 | 0.01 | 1.69 | 0.19 | BC 448 |
| | | | | Min $M_z$ | 3.40 | -0.53 | -34.52 | 0.22 | 6.91 | -0.11 | BC 131 |
| | | 68 | 200 | Max N | 34.41 | 0.57 | -18.30 | 0.08 | -0.00 | 0.00 | BC 204 |
| | | | | Min N | -9.40 | -0.29 | -18.33 | 0.11 | 0.00 | 0.00 | BC 247 |
| | | | | Max $V_y$ | 32.07 | 0.93 | -8.49 | 0.01 | 0.00 | 0.00 | BC 448 |
| | | | | Min $V_y$ | 3.40 | -0.53 | -34.63 | 0.22 | 0.00 | 0.00 | BC 131 |
| | | | | Max $V_z$ | 32.07 | 0.93 | -8.49 | 0.01 | 0.00 | 0.00 | BC 448 |
| | | | | Min $V_z$ | 3.65 | -0.52 | -34.63 | 0.22 | 0.00 | 0.00 | BC 138 |
| | | | | Max $M_T$ | 3.40 | -0.53 | -34.63 | 0.22 | 0.00 | 0.00 | BC 131 |
| | | | | Min $M_T$ | 32.07 | 0.93 | -8.49 | 0.01 | 0.00 | 0.00 | BC 448 |
| | | | | Max $M_y$ | 4.35 | -0.46 | -34.63 | 0.22 | 0.00 | -0.00 | BC 140 |
| | | | | Min $M_y$ | 2.99 | -0.18 | -18.33 | 0.11 | -0.00 | 0.00 | BC 91 |
| | | | | Max $M_z$ | -0.59 | 0.50 | -14.32 | 0.06 | 0.00 | 0.00 | BC 406 |
| | | | | Min $M_z$ | 33.34 | 0.74 | -14.32 | 0.05 | -0.00 | -0.00 | BC 368 |
| 38 | RC1 | 39 | 0 | Max N | 4.10 | -0.30 | 16.85 | -0.02 | 0.00 | 0.00 | BC 202 |
| | | | | Min N | -41.03 | 0.14 | 11.07 | 0.01 | -0.00 | 0.00 | BC 164 |
| | | | | Max $V_y$ | -39.50 | 0.17 | 7.54 | 0.01 | 0.00 | 0.00 | BC 384 |
| | | | | Min $V_y$ | 3.25 | -0.31 | 7.55 | -0.02 | 0.00 | 0.00 | BC 446 |
| | | | | Max $V_z$ | 0.50 | -0.20 | 33.01 | -0.01 | 0.00 | 0.00 | BC 148 |
| | | | | Min $V_z$ | -40.77 | 0.16 | 7.54 | 0.01 | 0.00 | -0.00 | BC 356 |
| | | | | Max $M_T$ | -39.50 | 0.17 | 7.54 | 0.01 | 0.00 | 0.00 | BC 384 |
| | | | | Min $M_T$ | 3.25 | -0.31 | 7.55 | -0.02 | 0.00 | 0.00 | BC 446 |
| | | | | Max $M_y$ | 0.53 | -0.20 | 33.01 | -0.01 | 0.00 | 0.00 | BC 155 |
| | | | | Min $M_y$ | -38.84 | 0.11 | 16.84 | 0.01 | -0.00 | 0.00 | BC 268 |
| | | | | Max $M_z$ | -39.26 | 0.07 | 16.85 | 0.00 | 0.00 | 0.00 | BC 205 |
| | | | | Min $M_z$ | -40.77 | 0.16 | 7.54 | 0.01 | 0.00 | -0.00 | BC 356 |
| | | 156 | 3256 | Max N | 3.80 | -0.30 | 0.64 | -0.02 | 28.46 | 0.99 | BC 202 |
| | | | | Min N | -41.22 | 0.14 | 0.63 | 0.01 | 19.04 | -0.45 | BC 164 |
| | | | | Max $V_y$ | -39.64 | 0.17 | 0.43 | 0.01 | 12.97 | -0.54 | BC 384 |
| | | | | Min $V_y$ | 3.11 | -0.31 | 0.44 | -0.02 | 13.01 | 1.02 | BC 446 |
| | | | | Max $V_z$ | 0.07 | -0.13 | 0.72 | -0.01 | 30.92 | 0.41 | BC 21 |
| | | | | Min $V_z$ | -39.89 | 0.13 | 0.43 | 0.01 | 22.37 | -0.42 | BC 392 |
| | | | | Max $M_T$ | -39.64 | 0.17 | 0.43 | 0.01 | 12.97 | -0.54 | BC 384 |
| | | | | Min $M_T$ | 3.11 | -0.31 | 0.44 | -0.02 | 13.01 | 1.02 | BC 446 |
| | | | | Max $M_y$ | -0.11 | -0.20 | 0.64 | -0.01 | 54.77 | 0.67 | BC 148 |
| | | | | Min $M_y$ | -40.90 | 0.16 | 0.43 | 0.01 | 12.97 | -0.51 | BC 356 |
| | | | | Max $M_z$ | 3.11 | -0.31 | 0.44 | -0.02 | 13.01 | 1.02 | BC 446 |
| | | | | Min $M_z$ | -39.64 | 0.17 | 0.43 | 0.01 | 12.97 | -0.54 | BC 384 |
| 39 | RC1 | 54 | 0 | Max N | 93.68 | 3.75 | -43.86 | 17.47 | 52.01 | -0.63 | BC 430 |
| | | | | Min N | -138.30 | 7.41 | -1.91 | 21.99 | -24.95 | 5.16 | BC 227 |
| | | | | Max $V_y$ | -73.70 | 12.92 | 11.82 | 27.01 | -2.60 | 3.40 | BC 251 |
| | | | | Min $V_y$ | 6.15 | -0.30 | -44.66 | 10.15 | 21.32 | 1.42 | BC 418 |
| | | | | Max $V_z$ | -63.50 | 11.11 | 19.85 | 23.43 | -4.93 | 2.48 | BC 471 |
| | | | | Min $V_z$ | -4.83 | 5.12 | -71.57 | 29.46 | 29.15 | 3.11 | BC 134 |
| | | | | Max $M_T$ | 50.39 | 5.64 | -64.85 | 37.24 | 48.83 | 1.71 | BC 140 |
| | | | | Min $M_T$ | 25.67 | 1.87 | -43.20 | 7.38 | 27.11 | 0.93 | BC 422 |
| | | | | Max $M_y$ | 89.31 | 6.36 | -55.24 | 28.89 | 54.22 | 0.03 | BC 340 |
| | | | | Min $M_y$ | -138.30 | 7.41 | -1.91 | 21.99 | -24.95 | 5.16 | BC 227 |
| | | | | Max $M_z$ | -137.77 | 7.46 | -1.87 | 21.89 | -24.92 | 5.16 | BC 167 |
| | | | | Min $M_z$ | 93.45 | 3.70 | -44.02 | 17.57 | 52.08 | -0.64 | BC 434 |
| | | 52 | 4500 | Max N | 94.09 | 3.51 | 66.86 | 12.25 | 43.20 | -2.04 | BC 235 |
| | | | | Min N | -134.35 | -13.77 | -21.76 | 11.84 | -24.07 | 3.46 | BC 222 |
| | | | | Max $V_y$ | 91.61 | 4.98 | 70.87 | 10.46 | 43.11 | -2.05 | BC 175 |
| | | | | Min $V_y$ | -116.41 | -16.61 | -28.47 | 13.78 | -23.04 | 3.27 | BC 434 |
| | | | | Max $V_z$ | 56.40 | 3.22 | 81.45 | 12.86 | 31.66 | -0.57 | BC 131 |
| | | | | Min $V_z$ | -123.71 | -16.18 | -37.44 | 12.25 | -26.53 | 3.28 | BC 446 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 39 | RC1 | | | Max $M_T$ | -17.12 | -14.19 | 28.21 | 22.82 | 15.91 | 1.60 | BC 148 |
| | | | | Min $M_T$ | -79.40 | -0.03 | 9.72 | 0.04 | -17.18 | 1.64 | BC 358 |
| | | | | Max $M_y$ | 94.09 | 3.51 | 66.86 | 12.25 | 43.20 | -2.04 | BC 235 |
| | | | | Min $M_y$ | -133.86 | -14.29 | -33.38 | 9.86 | -27.70 | 3.42 | BC 414 |
| | | | | Max $M_z$ | -132.31 | -15.38 | -25.79 | 13.57 | -23.98 | 3.48 | BC 282 |
| | | | | Min $M_z$ | 90.96 | 4.19 | 59.07 | 8.33 | 39.44 | -2.06 | BC 367 |
| 40 | RC1 | 52 | 0 | Max N | 94.06 | 1.07 | -54.88 | 8.23 | 43.26 | -2.03 | BC 235 |
| | | | | Min N | -132.58 | -16.40 | -61.13 | 9.11 | -26.76 | 3.19 | BC 222 |
| | | | | Max $V_y$ | 4.91 | 5.11 | -23.48 | 5.04 | 13.67 | 0.11 | BC 164 |
| | | | | Min $V_y$ | -113.28 | -19.25 | -61.32 | 11.14 | -26.66 | 2.94 | BC 434 |
| | | | | Max $V_z$ | -61.59 | -2.99 | 14.54 | -1.37 | -22.75 | 1.14 | BC 362 |
| | | | | Min $V_z$ | -31.53 | -14.02 | -122.62 | 19.57 | 14.90 | 1.72 | BC 155 |
| | | | | Max $M_T$ | -19.94 | -14.04 | -119.42 | 20.50 | 16.41 | 1.49 | BC 148 |
| | | | | Min $M_T$ | -70.57 | -2.70 | 10.85 | -2.08 | -23.30 | 1.33 | BC 358 |
| | | | | Max $M_y$ | 94.06 | 1.07 | -54.88 | 8.23 | 43.26 | -2.03 | BC 235 |
| | | | | Min $M_y$ | -130.35 | -18.56 | -56.05 | 9.16 | -30.14 | 3.18 | BC 474 |
| | | | | Max $M_z$ | -130.45 | -18.01 | -63.70 | 10.85 | -26.80 | 3.20 | BC 282 |
| | | | | Min $M_z$ | 91.11 | 1.73 | -44.36 | 4.60 | 39.44 | -2.05 | BC 367 |
| | | 50 | 4500 | Max N | 214.74 | 1.92 | 109.25 | 2.36 | 79.55 | -3.42 | BC 146 |
| | | | | Min N | -84.88 | 17.73 | 69.03 | -3.35 | -14.47 | 2.32 | BC 415 |
| | | | | Max $V_y$ | -40.35 | 20.39 | 85.22 | -4.98 | -2.58 | 1.63 | BC 435 |
| | | | | Min $V_y$ | 66.21 | -2.62 | 43.23 | 1.88 | 31.94 | -0.95 | BC 164 |
| | | | | Max $V_z$ | 126.16 | 17.66 | 175.10 | -4.90 | 66.46 | -1.14 | BC 155 |
| | | | | Min $V_z$ | -17.19 | 3.97 | -0.09 | 5.65 | -8.45 | 0.35 | BC 363 |
| | | | | Max $M_T$ | 26.01 | 4.44 | 34.66 | 7.55 | 11.60 | -0.27 | BC 203 |
| | | | | Min $M_T$ | -8.02 | 14.84 | 91.95 | -9.72 | 14.31 | 1.06 | BC 444 |
| | | | | Max $M_y$ | 213.43 | 1.95 | 109.60 | 2.27 | 79.69 | -3.40 | BC 149 |
| | | | | Min $M_y$ | -83.32 | 17.68 | 68.77 | -3.27 | -14.51 | 2.30 | BC 411 |
| | | | | Max $M_z$ | -84.88 | 17.73 | 69.03 | -3.35 | -14.47 | 2.32 | BC 415 |
| | | | | Min $M_z$ | 176.66 | 1.24 | 82.95 | 0.63 | 69.86 | -3.49 | BC 234 |
| 41 | RC1 | 50 | 0 | Max N | 212.09 | 1.89 | -105.25 | -1.27 | 81.27 | -3.35 | BC 146 |
| | | | | Min N | -85.78 | 15.06 | 24.13 | -6.22 | -12.42 | 2.55 | BC 415 |
| | | | | Max $V_y$ | 15.75 | 18.07 | -0.94 | -7.75 | 22.48 | 0.89 | BC 460 |
| | | | | Min $V_y$ | 73.43 | -3.48 | -55.59 | -0.19 | 33.87 | -1.36 | BC 165 |
| | | | | Max $V_z$ | -83.15 | 16.64 | 27.99 | -7.97 | -12.13 | 2.56 | BC 475 |
| | | | | Min $V_z$ | 208.01 | 0.37 | -109.10 | 0.37 | 81.04 | -3.34 | BC 134 |
| | | | | Max $M_T$ | -4.28 | 1.87 | -31.07 | 4.25 | 7.92 | 0.41 | BC 395 |
| | | | | Min $M_T$ | 91.76 | 14.66 | -27.11 | -13.52 | 51.86 | -1.33 | BC 254 |
| | | | | Max $M_y$ | 210.86 | 1.92 | -105.29 | -1.37 | 81.37 | -3.34 | BC 149 |
| | | | | Min $M_y$ | -84.26 | 15.02 | 24.11 | -6.13 | -12.43 | 2.53 | BC 411 |
| | | | | Max $M_z$ | -83.15 | 16.64 | 27.99 | -7.97 | -12.13 | 2.56 | BC 475 |
| | | | | Min $M_z$ | 173.70 | -2.61 | -85.03 | -2.30 | 69.63 | -3.52 | BC 174 |
| | | 48 | 4500 | Max N | 203.00 | -9.60 | 75.25 | -32.01 | 89.10 | -1.52 | BC 339 |
| | | | | Min N | -74.00 | -8.57 | 14.77 | -23.07 | -4.81 | 4.21 | BC 226 |
| | | | | Max $V_y$ | 47.00 | -0.77 | 52.54 | -11.21 | 34.08 | 0.85 | BC 419 |
| | | | | Min $V_y$ | 25.28 | -14.82 | 15.90 | -31.89 | 30.67 | 2.10 | BC 238 |
| | | | | Max $V_z$ | 134.21 | -8.62 | 97.38 | -32.66 | 72.61 | 1.10 | BC 131 |
| | | | | Min $V_z$ | -25.66 | -12.24 | -12.74 | -24.69 | 6.69 | 2.02 | BC 474 |
| | | | | Max $M_T$ | 66.30 | -2.95 | 51.01 | -8.44 | 39.77 | 0.37 | BC 423 |
| | | | | Min $M_T$ | 182.56 | -9.57 | 88.74 | -41.01 | 89.97 | -0.11 | BC 140 |
| | | | | Max $M_y$ | 200.17 | -11.45 | 86.53 | -38.34 | 94.71 | -0.57 | BC 148 |
| | | | | Min $M_y$ | -73.90 | -6.92 | 2.88 | -17.06 | -11.08 | 3.30 | BC 418 |
| | | | | Max $M_z$ | -74.00 | -8.57 | 14.77 | -23.07 | -4.81 | 4.21 | BC 226 |
| | | | | Min $M_z$ | 203.00 | -9.60 | 75.25 | -32.01 | 89.10 | -1.52 | BC 339 |
| 42 | RC1 | 48 | 0 | Max N | 202.58 | -9.81 | -116.73 | -35.37 | 89.28 | -1.48 | BC 339 |
| | | | | Min N | -66.43 | -11.68 | -45.42 | -26.53 | -10.06 | 3.93 | BC 226 |
| | | | | Max $V_y$ | 2.12 | -1.29 | -43.12 | -13.65 | 16.44 | 1.82 | BC 416 |
| | | | | Min $V_y$ | 35.12 | -17.94 | -61.71 | -35.73 | 23.68 | 1.70 | BC 238 |
| | | | | Max $V_z$ | -22.97 | -14.21 | -13.17 | -28.05 | -4.77 | 1.76 | BC 414 |
| | | | | Min $V_z$ | 143.02 | -10.08 | -143.59 | -36.01 | 75.82 | 0.94 | BC 146 |
| | | | | Max $M_T$ | 21.31 | -3.46 | -49.60 | -10.98 | 22.23 | 1.33 | BC 420 |
| | | | | Min $M_T$ | 182.73 | -9.81 | -131.89 | -44.84 | 89.82 | -0.07 | BC 140 |
| | | | | Max $M_y$ | 199.61 | -11.68 | -137.81 | -42.25 | 94.97 | -0.53 | BC 148 |
| | | | | Min $M_y$ | -65.79 | -10.01 | -23.63 | -19.96 | -16.69 | 3.00 | BC 418 |
| | | | | Max $M_z$ | -65.50 | -11.69 | -45.68 | -26.40 | -9.84 | 3.93 | BC 166 |
| | | | | Min $M_z$ | 201.69 | -9.80 | -116.49 | -35.49 | 89.07 | -1.48 | BC 340 |
| | | 5 | 4300 | Max N | -24.75 | 18.51 | 9.61 | -27.99 | -21.67 | 2.29 | BC 356 |
| | | | | Min N | -76.47 | 52.53 | -8.59 | -74.42 | -57.87 | 6.17 | BC 148 |
| | | | | Max $V_y$ | -76.43 | 52.61 | -8.97 | -74.96 | -57.93 | 6.18 | BC 154 |
| | | | | Min $V_y$ | -32.32 | 18.46 | 19.30 | -28.06 | -19.91 | 2.20 | BC 390 |
| | | | | Max $V_z$ | -53.48 | 32.05 | 25.06 | -48.97 | -35.16 | 3.86 | BC 186 |
| | | | | Min $V_z$ | -38.85 | 31.39 | -19.93 | -40.77 | -34.90 | 3.59 | BC 456 |
| | | | | Max $M_T$ | -24.82 | 18.48 | 9.83 | -27.45 | -21.62 | 2.28 | BC 360 |
| | | | | Min $M_T$ | -76.46 | 52.61 | -8.92 | -75.00 | -57.96 | 6.19 | BC 155 |
| | | | | Max $M_y$ | -32.29 | 18.47 | 19.25 | -28.03 | -19.88 | 2.19 | BC 362 |
| | | | | Min $M_y$ | -76.46 | 52.61 | -8.92 | -75.00 | -57.96 | 6.19 | BC 155 |
| | | | | Max $M_z$ | -76.46 | 52.61 | -8.92 | -75.00 | -57.96 | 6.19 | BC 155 |
| | | | | Min $M_z$ | -32.29 | 18.47 | 19.25 | -28.03 | -19.88 | 2.19 | BC 362 |
| 43 | RC1 | 43 | 0 | Max N | -54.57 | -2.83 | 0.47 | 0.00 | 0.00 | 0.00 | BC 473 |
| | | | | Min N | -215.27 | -0.03 | 0.11 | 0.00 | 0.00 | 0.00 | BC 131 |
| | | | | Max $V_y$ | -90.46 | 2.63 | 0.18 | 0.00 | 0.00 | 0.00 | BC 403 |
| | | | | Min $V_y$ | -115.89 | -2.85 | 0.39 | 0.00 | 0.00 | 0.00 | BC 233 |
| | | | | Max $V_z$ | -82.36 | -2.60 | 0.72 | -0.00 | 0.00 | 0.00 | BC 216 |
| | | | | Min $V_z$ | -57.38 | -1.67 | -0.60 | -0.00 | 0.00 | 0.00 | BC 390 |
| | | | | Max $M_T$ | -115.71 | -2.84 | 0.47 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min $M_T$ | -57.18 | -1.67 | -0.55 | -0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Max $M_y$ | -115.71 | -2.84 | 0.47 | 0.00 | 0.00 | 0.00 | BC 177 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 43 | RC1 | | | Min $M_y$ | -117.56 | -2.60 | 0.70 | -0.00 | -0.00 | 0.00 | BC 268 |
| | | | | Max $M_z$ | -92.46 | -1.67 | -0.52 | -0.00 | -0.00 | 0.00 | BC 378 |
| | | | | Min $M_z$ | -54.59 | -2.83 | 0.46 | 0.00 | -0.00 | -0.00 | BC 381 |
| | | 87 | 4345 | Max N | -51.10 | -2.83 | 0.47 | 0.00 | 2.04 | 12.31 | BC 473 |
| | | | | Min N | -210.18 | -0.03 | 0.11 | 0.00 | 0.49 | 0.11 | BC 131 |
| | | | | Max $V_y$ | -86.99 | 2.63 | 0.18 | 0.00 | 0.78 | -11.44 | BC 403 |
| | | | | Min $V_y$ | -110.80 | -2.85 | 0.39 | 0.00 | 1.68 | 12.37 | BC 233 |
| | | | | Max $V_z$ | -77.28 | -2.60 | 0.72 | -0.00 | 3.13 | 11.29 | BC 216 |
| | | | | Min $V_z$ | -53.91 | -1.67 | -0.60 | -0.00 | -2.60 | 7.27 | BC 390 |
| | | | | Max $M_T$ | -110.62 | -2.84 | 0.47 | 0.00 | 2.05 | 12.35 | BC 241 |
| | | | | Min $M_T$ | -53.71 | -1.67 | -0.55 | -0.00 | -2.38 | 7.27 | BC 446 |
| | | | | Max $M_y$ | -77.28 | -2.60 | 0.72 | -0.00 | 3.13 | 11.29 | BC 216 |
| | | | | Min $M_y$ | -53.91 | -1.67 | -0.60 | -0.00 | -2.60 | 7.27 | BC 390 |
| | | | | Max $M_z$ | -110.80 | -2.85 | 0.39 | 0.00 | 1.68 | 12.37 | BC 233 |
| | | | | Min $M_z$ | -86.99 | 2.63 | 0.18 | 0.00 | 0.78 | -11.44 | BC 403 |
| 44 | RC1 | 66 | 0 | Max N | 8.59 | -2.58 | -0.38 | 0.00 | 0.00 | 0.00 | BC 444 |
| | | | | Min N | -203.38 | -0.02 | 1.55 | 0.00 | 0.00 | 0.00 | BC 138 |
| | | | | Max $V_y$ | -75.10 | 2.68 | 0.63 | 0.00 | 0.00 | -0.00 | BC 431 |
| | | | | Min $V_y$ | -171.72 | -2.83 | 2.08 | 0.00 | 0.00 | 0.00 | BC 225 |
| | | | | Max $V_z$ | -199.19 | -2.83 | 2.20 | 0.00 | 0.00 | 0.00 | BC 213 |
| | | | | Min $V_z$ | -6.39 | -2.61 | -0.50 | 0.00 | 0.00 | 0.00 | BC 388 |
| | | | | Max $M_T$ | -54.44 | 2.64 | 0.26 | 0.00 | 0.00 | 0.00 | BC 419 |
| | | | | Min $M_T$ | -146.84 | -2.82 | 1.81 | 0.00 | -0.00 | -0.00 | BC 421 |
| | | | | Max $M_y$ | -72.89 | 0.02 | 0.83 | 0.00 | 0.00 | 0.00 | BC 38 |
| | | | | Min $M_y$ | -91.29 | -0.03 | 0.71 | 0.00 | -0.00 | 0.00 | BC 2 |
| | | | | Max $M_z$ | -80.10 | -1.67 | 0.54 | 0.00 | 0.00 | 0.00 | BC 226 |
| | | | | Min $M_z$ | -69.91 | 2.66 | 0.66 | 0.00 | 0.00 | -0.00 | BC 191 |
| | | 99 | 2173 | Max N | 10.32 | -2.58 | -0.38 | 0.00 | -0.82 | 5.60 | BC 444 |
| | | | | Min N | -200.84 | -0.02 | 1.55 | 0.00 | 3.37 | 0.05 | BC 138 |
| | | | | Max $V_y$ | -73.36 | 2.68 | 0.63 | 0.00 | 1.37 | -5.81 | BC 431 |
| | | | | Min $V_y$ | -169.18 | -2.83 | 2.08 | 0.00 | 4.51 | 6.15 | BC 225 |
| | | | | Max $V_z$ | -196.64 | -2.83 | 2.20 | 0.00 | 4.77 | 6.14 | BC 213 |
| | | | | Min $V_z$ | -4.66 | -2.61 | -0.50 | 0.00 | -1.10 | 5.68 | BC 388 |
| | | | | Max $M_T$ | -52.71 | 2.64 | 0.26 | 0.00 | 0.57 | -5.73 | BC 419 |
| | | | | Min $M_T$ | -145.10 | -2.82 | 1.81 | 0.00 | 3.92 | 6.12 | BC 421 |
| | | | | Max $M_y$ | -196.64 | -2.83 | 2.20 | 0.00 | 4.77 | 6.14 | BC 213 |
| | | | | Min $M_y$ | -4.66 | -2.61 | -0.50 | 0.00 | -1.10 | 5.68 | BC 388 |
| | | | | Max $M_z$ | -169.18 | -2.83 | 2.08 | 0.00 | 4.51 | 6.15 | BC 225 |
| | | | | Min $M_z$ | -73.36 | 2.68 | 0.63 | 0.00 | 1.37 | -5.81 | BC 431 |
| 45 | RC1 | 67 | 0 | Max N | 24.79 | -0.04 | 30.91 | 0.18 | -0.00 | 0.00 | BC 390 |
| | | | | Min N | -24.80 | -0.02 | 45.69 | 0.05 | 0.00 | 0.00 | BC 216 |
| | | | | Max $V_y$ | -12.05 | 0.03 | 31.26 | -0.07 | 0.00 | 0.00 | BC 447 |
| | | | | Min $V_y$ | 19.57 | -0.04 | 45.53 | 0.17 | -0.00 | 0.00 | BC 254 |
| | | | | Max $V_z$ | -8.29 | -0.01 | 134.88 | -0.02 | -0.00 | 0.00 | BC 155 |
| | | | | Min $V_z$ | 24.79 | -0.04 | 30.91 | 0.18 | -0.00 | 0.00 | BC 390 |
| | | | | Max $M_T$ | 22.87 | -0.04 | 30.94 | 0.19 | 0.00 | 0.00 | BC 446 |
| | | | | Min $M_T$ | -8.16 | 0.02 | 54.70 | -0.08 | 0.00 | 0.00 | BC 435 |
| | | | | Max $M_y$ | -7.32 | -0.01 | 69.24 | 0.00 | 0.00 | 0.00 | BC 91 |
| | | | | Min $M_y$ | -22.85 | -0.01 | 69.09 | 0.03 | -0.00 | 0.00 | BC 232 |
| | | | | Max $M_z$ | -23.31 | -0.01 | 69.60 | -0.04 | 0.00 | 0.00 | BC 205 |
| | | | | Min $M_z$ | -18.94 | -0.01 | 46.11 | -0.02 | -0.00 | -0.00 | BC 197 |
| | | 152 | 3256 | Max N | 24.51 | -0.04 | 16.36 | 0.18 | 76.94 | 0.12 | BC 390 |
| | | | | Min N | -25.20 | -0.02 | 24.36 | 0.05 | 114.02 | 0.07 | BC 216 |
| | | | | Max $V_y$ | -12.33 | 0.03 | 16.72 | -0.07 | 78.09 | -0.09 | BC 447 |
| | | | | Min $V_y$ | 19.17 | -0.04 | 24.20 | 0.17 | 113.51 | 0.15 | BC 254 |
| | | | | Max $V_z$ | -9.54 | -0.01 | 68.66 | -0.02 | 331.31 | 0.03 | BC 155 |
| | | | | Min $V_z$ | 24.51 | -0.04 | 16.36 | 0.18 | 76.94 | 0.12 | BC 390 |
| | | | | Max $M_T$ | 22.59 | -0.04 | 16.40 | 0.19 | 77.06 | 0.14 | BC 446 |
| | | | | Min $M_T$ | -8.66 | 0.02 | 28.35 | -0.08 | 135.18 | -0.07 | BC 435 |
| | | | | Max $M_y$ | -9.54 | -0.01 | 68.66 | -0.02 | 331.31 | 0.03 | BC 155 |
| | | | | Min $M_y$ | 24.51 | -0.04 | 16.36 | 0.18 | 76.94 | 0.12 | BC 390 |
| | | | | Max $M_z$ | 19.17 | -0.04 | 24.20 | 0.17 | 113.51 | 0.15 | BC 254 |
| | | | | Min $M_z$ | -12.33 | 0.03 | 16.72 | -0.07 | 78.09 | -0.09 | BC 447 |
| 46 | RC1 | 68 | 0 | Max N | 36.13 | 0.05 | 31.32 | -0.25 | 0.00 | 0.00 | BC 391 |
| | | | | Min N | -32.25 | 0.01 | 70.70 | -0.01 | 0.00 | 0.00 | BC 240 |
| | | | | Max $V_y$ | 32.59 | 0.05 | 31.36 | -0.24 | 0.00 | -0.00 | BC 411 |
| | | | | Min $V_y$ | -3.89 | -0.00 | 55.69 | -0.03 | -0.00 | 0.00 | BC 53 |
| | | | | Max $V_z$ | -4.02 | 0.00 | 137.61 | -0.05 | 0.00 | 0.00 | BC 154 |
| | | | | Min $V_z$ | 36.13 | 0.05 | 31.32 | -0.25 | 0.00 | 0.00 | BC 419 |
| | | | | Max $M_T$ | -9.77 | 0.02 | 55.66 | 0.03 | 0.00 | 0.00 | BC 373 |
| | | | | Min $M_T$ | 36.13 | 0.05 | 31.32 | -0.25 | 0.00 | 0.00 | BC 391 |
| | | | | Max $M_y$ | -4.03 | 0.00 | 118.43 | -0.05 | 0.00 | 0.00 | BC 115 |
| | | | | Min $M_y$ | -9.27 | 0.01 | 31.69 | 0.03 | -0.00 | 0.00 | BC 381 |
| | | | | Max $M_z$ | -8.04 | 0.02 | 70.44 | 0.02 | -0.00 | 0.00 | BC 261 |
| | | | | Min $M_z$ | 32.16 | 0.05 | 31.37 | -0.24 | 0.00 | -0.00 | BC 387 |
| | | 153 | 3256 | Max N | 35.85 | 0.05 | 16.53 | -0.25 | 77.89 | -0.15 | BC 391 |
| | | | | Min N | -32.89 | 0.01 | 36.93 | -0.01 | 175.20 | -0.05 | BC 240 |
| | | | | Max $V_y$ | 32.31 | 0.05 | 16.57 | -0.24 | 78.01 | -0.16 | BC 411 |
| | | | | Min $V_y$ | -4.40 | -0.00 | 28.81 | -0.03 | 137.55 | 0.00 | BC 53 |
| | | | | Max $V_z$ | -5.30 | 0.00 | 70.01 | -0.05 | 337.97 | -0.02 | BC 154 |
| | | | | Min $V_z$ | 35.85 | 0.05 | 16.53 | -0.25 | 77.89 | -0.15 | BC 419 |
| | | | | Max $M_T$ | -10.28 | 0.02 | 28.79 | 0.03 | 137.47 | -0.06 | BC 373 |
| | | | | Min $M_T$ | 35.85 | 0.05 | 16.53 | -0.25 | 77.89 | -0.15 | BC 391 |
| | | | | Max $M_y$ | -5.30 | 0.00 | 70.01 | -0.05 | 337.97 | -0.02 | BC 154 |
| | | | | Min $M_y$ | 35.85 | 0.05 | 16.53 | -0.25 | 77.89 | -0.15 | BC 419 |
| | | | | Max $M_z$ | -4.40 | -0.00 | 28.81 | -0.03 | 137.55 | 0.00 | BC 53 |
| | | | | Min $M_z$ | 32.31 | 0.05 | 16.57 | -0.24 | 78.01 | -0.16 | BC 411 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 47 | RC1 | 9 | 0 | Max N | 13.48 | 0.00 | 1.50 | 0.00 | 0.00 | 0.00 | BC 266 |
| | | | | Min N | -8.19 | 0.00 | 1.02 | -0.00 | 0.00 | 0.00 | BC 356 |
| | | | | Max $V_y$ | 0.27 | 0.00 | 1.70 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.27 | 0.00 | 1.70 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.27 | 0.00 | 1.70 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -8.17 | 0.00 | 1.02 | -0.00 | 0.00 | 0.00 | BC 352 |
| | | | | Max $M_T$ | 13.30 | 0.00 | 1.50 | 0.00 | 0.00 | 0.00 | BC 186 |
| | | | | Min $M_T$ | -8.12 | 0.00 | 1.50 | -0.00 | 0.00 | 0.00 | BC 164 |
| | | | | Max $M_y$ | 0.32 | 0.00 | 1.50 | -0.00 | 0.00 | 0.00 | BC 87 |
| | | | | Min $M_y$ | 5.82 | 0.00 | 1.50 | 0.00 | -0.00 | 0.00 | BC 163 |
| | | | | Max $M_z$ | 0.27 | 0.00 | 1.70 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.27 | 0.00 | 1.70 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | 69 | 6400 | Max N | 13.48 | 0.00 | -1.50 | 0.00 | 0.00 | 0.00 | BC 266 |
| | | | | Min N | -8.19 | 0.00 | -1.02 | -0.00 | 0.00 | 0.00 | BC 356 |
| | | | | Max $V_y$ | 0.27 | 0.00 | -1.70 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.27 | 0.00 | -1.70 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -8.17 | 0.00 | -1.02 | -0.00 | 0.00 | 0.00 | BC 352 |
| | | | | Min $V_z$ | 0.27 | 0.00 | -1.70 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 13.30 | 0.00 | -1.50 | 0.00 | 0.00 | 0.00 | BC 186 |
| | | | | Min $M_T$ | -8.12 | 0.00 | -1.50 | -0.00 | 0.00 | 0.00 | BC 164 |
| | | | | Max $M_y$ | 0.32 | 0.00 | -1.50 | -0.00 | 0.00 | 0.00 | BC 87 |
| | | | | Min $M_y$ | 5.82 | 0.00 | -1.50 | 0.00 | -0.00 | 0.00 | BC 163 |
| | | | | Max $M_z$ | 0.27 | 0.00 | -1.70 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.27 | 0.00 | -1.70 | -0.00 | 0.00 | 0.00 | BC 1 |
| 48 | RC1 | 69 | 0 | Max N | 13.14 | 0.00 | 1.53 | -0.00 | 0.00 | 0.00 | BC 238 |
| | | | | Min N | -47.80 | 0.00 | 1.53 | 0.00 | -0.00 | 0.00 | BC 164 |
| | | | | Max $V_y$ | 0.21 | 0.00 | 1.72 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.21 | 0.00 | 1.72 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.54 | 0.00 | 1.72 | -0.00 | 0.00 | 0.00 | BC 20 |
| | | | | Min $V_z$ | -47.32 | 0.00 | 1.04 | 0.00 | 0.00 | 0.00 | BC 352 |
| | | | | Max $M_T$ | -46.42 | 0.00 | 1.04 | 0.00 | -0.00 | 0.00 | BC 440 |
| | | | | Min $M_T$ | -46.81 | 0.00 | 1.53 | -0.00 | 0.00 | 0.00 | BC 185 |
| | | | | Max $M_y$ | 0.38 | 0.00 | 1.72 | -0.00 | 0.00 | 0.00 | BC 29 |
| | | | | Min $M_y$ | -45.68 | 0.00 | 1.53 | 0.00 | -0.00 | 0.00 | BC 268 |
| | | | | Max $M_z$ | 0.21 | 0.00 | 1.72 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.21 | 0.00 | 1.72 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | 70 | 6510 | Max N | 13.14 | 0.00 | -1.53 | -0.00 | 0.00 | 0.00 | BC 238 |
| | | | | Min N | -47.80 | 0.00 | -1.53 | 0.00 | -0.00 | 0.00 | BC 164 |
| | | | | Max $V_y$ | 0.21 | 0.00 | -1.72 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.21 | 0.00 | -1.72 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -47.32 | 0.00 | -1.04 | 0.00 | 0.00 | 0.00 | BC 352 |
| | | | | Min $V_z$ | 0.54 | 0.00 | -1.72 | -0.00 | 0.00 | 0.00 | BC 20 |
| | | | | Max $M_T$ | -46.42 | 0.00 | -1.04 | 0.00 | -0.00 | 0.00 | BC 440 |
| | | | | Min $M_T$ | -46.81 | 0.00 | -1.53 | -0.00 | 0.00 | 0.00 | BC 185 |
| | | | | Max $M_y$ | 0.38 | 0.00 | -1.72 | -0.00 | 0.00 | 0.00 | BC 29 |
| | | | | Min $M_y$ | -45.68 | 0.00 | -1.53 | 0.00 | -0.00 | 0.00 | BC 268 |
| | | | | Max $M_z$ | 0.21 | 0.00 | -1.72 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.21 | 0.00 | -1.72 | -0.00 | 0.00 | 0.00 | BC 1 |
| 49 | RC1 | 70 | 0 | Max N | 13.45 | 0.00 | 1.53 | 0.00 | 0.00 | 0.00 | BC 242 |
| | | | | Min N | -8.22 | 0.00 | 1.04 | 0.00 | 0.00 | 0.00 | BC 417 |
| | | | | Max $V_y$ | 0.13 | 0.00 | 1.73 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.13 | 0.00 | 1.73 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.34 | 0.00 | 1.73 | 0.00 | 0.00 | 0.00 | BC 5 |
| | | | | Min $V_z$ | -8.21 | 0.00 | 1.04 | 0.00 | 0.00 | 0.00 | BC 353 |
| | | | | Max $M_T$ | -8.00 | 0.00 | 1.53 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min $M_T$ | 5.64 | 0.00 | 1.04 | -0.00 | 0.00 | 0.00 | BC 363 |
| | | | | Max $M_y$ | 5.68 | 0.00 | 1.53 | -0.00 | 0.00 | 0.00 | BC 163 |
| | | | | Min $M_y$ | 0.29 | 0.00 | 1.53 | 0.00 | -0.00 | 0.00 | BC 87 |
| | | | | Max $M_z$ | 0.13 | 0.00 | 1.73 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.13 | 0.00 | 1.73 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 12 | 6530 | Max N | 13.45 | 0.00 | -1.53 | 0.00 | 0.00 | 0.00 | BC 242 |
| | | | | Min N | -8.22 | 0.00 | -1.04 | 0.00 | 0.00 | 0.00 | BC 417 |
| | | | | Max $V_y$ | 0.13 | 0.00 | -1.73 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.13 | 0.00 | -1.73 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -8.21 | 0.00 | -1.04 | 0.00 | 0.00 | 0.00 | BC 353 |
| | | | | Min $V_z$ | 0.34 | 0.00 | -1.73 | 0.00 | 0.00 | 0.00 | BC 5 |
| | | | | Max $M_T$ | -8.00 | 0.00 | -1.53 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min $M_T$ | 5.64 | 0.00 | -1.04 | -0.00 | 0.00 | 0.00 | BC 363 |
| | | | | Max $M_y$ | 5.68 | 0.00 | -1.53 | -0.00 | 0.00 | 0.00 | BC 163 |
| | | | | Min $M_y$ | 0.29 | 0.00 | -1.53 | 0.00 | -0.00 | 0.00 | BC 87 |
| | | | | Max $M_z$ | 0.13 | 0.00 | -1.73 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.13 | 0.00 | -1.73 | 0.00 | 0.00 | 0.00 | BC 1 |
| 50 | RC1 | 16 | 0 | Max N | 12.96 | 0.00 | 1.02 | 0.00 | 0.00 | 0.00 | BC 363 |
| | | | | Min N | -6.93 | 0.00 | 1.50 | 0.00 | 0.00 | 0.00 | BC 240 |
| | | | | Max $V_y$ | -0.12 | 0.00 | 1.70 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.12 | 0.00 | 1.70 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.10 | 0.00 | 1.70 | 0.00 | 0.00 | 0.00 | BC 2 |
| | | | | Min $V_z$ | -6.81 | 0.00 | 1.02 | 0.00 | 0.00 | 0.00 | BC 352 |
| | | | | Max $M_T$ | -6.83 | 0.00 | 1.50 | 0.00 | 0.00 | 0.00 | BC 260 |
| | | | | Min $M_T$ | 5.55 | 0.00 | 1.02 | -0.00 | 0.00 | 0.00 | BC 422 |
| | | | | Max $M_y$ | 5.51 | 0.00 | 1.50 | 0.00 | 0.00 | 0.00 | BC 226 |
| | | | | Min $M_y$ | -0.12 | 0.00 | 1.02 | 0.00 | -0.00 | 0.00 | BC 36 |
| | | | | Max $M_z$ | -0.12 | 0.00 | 1.70 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.12 | 0.00 | 1.70 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 79 | 6400 | Max N | 12.96 | 0.00 | -1.02 | 0.00 | 0.00 | 0.00 | BC 363 |
| | | | | Min N | -6.93 | 0.00 | -1.50 | 0.00 | 0.00 | 0.00 | BC 240 |
| | | | | Max $V_y$ | -0.12 | 0.00 | -1.70 | 0.00 | 0.00 | 0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 50 | RC1 | | | Min $V_y$ | -0.12 | 0.00 | -1.70 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -6.81 | 0.00 | -1.02 | 0.00 | 0.00 | 0.00 | BC 352 |
| | | | | Min $V_z$ | -0.10 | 0.00 | -1.70 | 0.00 | 0.00 | 0.00 | BC 2 |
| | | | | Max $M_T$ | -6.83 | 0.00 | -1.50 | 0.00 | 0.00 | 0.00 | BC 260 |
| | | | | Min $M_T$ | 5.55 | 0.00 | -1.02 | -0.00 | 0.00 | 0.00 | BC 422 |
| | | | | Max $M_y$ | 5.51 | 0.00 | -1.50 | 0.00 | 0.00 | 0.00 | BC 226 |
| | | | | Min $M_y$ | -0.12 | 0.00 | -1.02 | 0.00 | -0.00 | 0.00 | BC 36 |
| | | | | Max $M_z$ | -0.12 | 0.00 | -1.70 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.12 | 0.00 | -1.70 | 0.00 | 0.00 | 0.00 | BC 1 |
| 51 | RC1 | 79 | 0 | Max N | 10.24 | -0.00 | 0.61 | 0.00 | 0.00 | 0.00 | BC 407 |
| | | | | Min N | -38.42 | 0.00 | 0.66 | -0.00 | -0.00 | 0.00 | BC 248 |
| | | | | Max $V_y$ | 2.99 | 0.00 | 1.08 | -0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min $V_y$ | 7.85 | -0.00 | 0.89 | 0.00 | -0.00 | 0.00 | BC 167 |
| | | | | Max $V_z$ | 3.68 | 0.00 | 1.09 | -0.00 | 0.00 | 0.00 | BC 185 |
| | | | | Min $V_z$ | -35.94 | 0.00 | 0.38 | -0.00 | 0.00 | 0.00 | BC 456 |
| | | | | Max $M_T$ | 3.36 | -0.00 | 0.87 | 0.00 | 0.00 | 0.00 | BC 243 |
| | | | | Min $M_T$ | -30.26 | 0.00 | 0.41 | -0.00 | -0.00 | 0.00 | BC 356 |
| | | | | Max $M_y$ | -4.30 | 0.00 | 0.87 | 0.00 | 0.00 | 0.00 | BC 114 |
| | | | | Min $M_y$ | -9.55 | 0.00 | 0.86 | 0.00 | -0.00 | 0.00 | BC 91 |
| | | | | Max $M_z$ | -7.06 | 0.00 | 0.98 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -7.06 | 0.00 | 0.98 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 93 | 4845 | Max N | 10.24 | -0.00 | -0.94 | 0.00 | -0.82 | 0.01 | BC 407 |
| | | | | Min N | -38.42 | 0.00 | -1.62 | -0.00 | -2.32 | -0.01 | BC 248 |
| | | | | Max $V_y$ | 2.99 | 0.00 | -1.20 | -0.00 | -0.29 | -0.01 | BC 241 |
| | | | | Min $V_y$ | 7.85 | -0.00 | -1.39 | 0.00 | -1.21 | 0.01 | BC 167 |
| | | | | Max $V_z$ | 3.93 | 0.00 | -0.74 | -0.00 | 0.17 | -0.01 | BC 377 |
| | | | | Min $V_z$ | -38.19 | 0.00 | -1.62 | -0.00 | -2.34 | -0.01 | BC 264 |
| | | | | Max $M_T$ | 3.36 | -0.00 | -1.41 | 0.00 | -1.31 | 0.01 | BC 243 |
| | | | | Min $M_T$ | -30.26 | 0.00 | -1.14 | -0.00 | -1.79 | -0.01 | BC 356 |
| | | | | Max $M_y$ | 3.93 | 0.00 | -0.74 | -0.00 | 0.17 | -0.01 | BC 377 |
| | | | | Min $M_y$ | -38.19 | 0.00 | -1.62 | -0.00 | -2.34 | -0.01 | BC 264 |
| | | | | Max $M_z$ | 7.85 | -0.00 | -1.39 | 0.00 | -1.21 | 0.01 | BC 167 |
| | | | | Min $M_z$ | 2.99 | 0.00 | -1.20 | -0.00 | -0.29 | -0.01 | BC 241 |
| 52 | RC1 | 80 | 0 | Max N | 8.19 | -0.00 | -0.25 | 0.01 | 0.00 | 0.00 | BC 359 |
| | | | | Min N | -38.02 | 0.00 | -0.72 | -0.01 | -0.00 | 0.00 | BC 241 |
| | | | | Max $V_y$ | -26.72 | 0.00 | -0.31 | -0.01 | 0.00 | 0.00 | BC 377 |
| | | | | Min $V_y$ | -4.16 | -0.00 | -0.72 | 0.01 | 0.00 | 0.00 | BC 267 |
| | | | | Max $V_z$ | 8.19 | -0.00 | -0.25 | 0.01 | 0.00 | 0.00 | BC 359 |
| | | | | Min $V_z$ | -18.35 | -0.00 | -0.91 | 0.00 | 0.00 | 0.00 | BC 155 |
| | | | | Max $M_T$ | -4.16 | -0.00 | -0.72 | 0.01 | 0.00 | 0.00 | BC 267 |
| | | | | Min $M_T$ | -25.98 | 0.00 | -0.27 | -0.01 | 0.00 | 0.00 | BC 389 |
| | | | | Max $M_y$ | -5.34 | 0.00 | -0.52 | -0.00 | 0.00 | 0.00 | BC 258 |
| | | | | Min $M_y$ | -9.34 | -0.00 | -0.62 | 0.00 | -0.00 | 0.00 | BC 114 |
| | | | | Max $M_z$ | -8.59 | -0.00 | -0.54 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -8.59 | -0.00 | -0.54 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | 89 | 1665 | Max N | 8.19 | -0.00 | -0.78 | 0.01 | -0.86 | 0.00 | BC 359 |
| | | | | Min N | -38.02 | 0.00 | -1.50 | -0.01 | -1.85 | -0.00 | BC 241 |
| | | | | Max $V_y$ | -26.72 | 0.00 | -0.85 | -0.01 | -0.97 | -0.00 | BC 377 |
| | | | | Min $V_y$ | -4.16 | -0.00 | -1.50 | 0.01 | -1.85 | 0.00 | BC 267 |
| | | | | Max $V_z$ | 8.19 | -0.00 | -0.78 | 0.01 | -0.86 | 0.00 | BC 359 |
| | | | | Min $V_z$ | -17.66 | -0.00 | -1.72 | 0.00 | -2.13 | 0.00 | BC 21 |
| | | | | Max $M_T$ | -4.16 | -0.00 | -1.50 | 0.01 | -1.85 | 0.00 | BC 267 |
| | | | | Min $M_T$ | -25.98 | 0.00 | -0.81 | -0.01 | -0.90 | -0.00 | BC 389 |
| | | | | Max $M_y$ | 8.19 | -0.00 | -0.78 | 0.01 | -0.86 | 0.00 | BC 359 |
| | | | | Min $M_y$ | -18.35 | -0.00 | -1.69 | 0.00 | -2.16 | 0.00 | BC 155 |
| | | | | Max $M_z$ | -4.16 | -0.00 | -1.50 | 0.01 | -1.85 | 0.00 | BC 267 |
| | | | | Min $M_z$ | -26.72 | 0.00 | -0.85 | -0.01 | -0.97 | -0.00 | BC 377 |
| 53 | RC1 | 9 | 0 | Max N | 18.94 | 0.00 | 0.69 | -0.00 | 0.00 | 0.00 | BC 412 |
| | | | | Min N | -13.46 | 0.00 | 1.01 | 0.00 | 0.00 | 0.00 | BC 234 |
| | | | | Max $V_y$ | -0.02 | 0.00 | 1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.02 | 0.00 | 1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.02 | 0.00 | 1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -13.42 | 0.00 | 0.69 | 0.00 | 0.00 | 0.00 | BC 354 |
| | | | | Max $M_T$ | -13.41 | 0.00 | 1.01 | 0.00 | 0.00 | 0.00 | BC 166 |
| | | | | Min $M_T$ | 18.92 | 0.00 | 0.69 | -0.00 | 0.00 | 0.00 | BC 388 |
| | | | | Max $M_y$ | -0.04 | 0.00 | 1.14 | 0.00 | 0.00 | 0.00 | BC 27 |
| | | | | Min $M_y$ | -0.01 | 0.00 | 1.14 | 0.00 | -0.00 | 0.00 | BC 23 |
| | | | | Max $M_z$ | -0.02 | 0.00 | 1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.02 | 0.00 | 1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 71 | 4300 | Max N | 18.94 | 0.00 | -0.69 | -0.00 | 0.00 | 0.00 | BC 412 |
| | | | | Min N | -13.46 | 0.00 | -1.01 | 0.00 | 0.00 | 0.00 | BC 234 |
| | | | | Max $V_y$ | -0.02 | 0.00 | -1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.02 | 0.00 | -1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -13.42 | 0.00 | -0.69 | 0.00 | 0.00 | 0.00 | BC 354 |
| | | | | Min $V_z$ | -0.02 | 0.00 | -1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -13.41 | 0.00 | -1.01 | 0.00 | 0.00 | 0.00 | BC 166 |
| | | | | Min $M_T$ | 18.92 | 0.00 | -0.69 | -0.00 | 0.00 | 0.00 | BC 388 |
| | | | | Max $M_y$ | -0.04 | 0.00 | -1.14 | 0.00 | 0.00 | 0.00 | BC 27 |
| | | | | Min $M_y$ | -0.01 | 0.00 | -1.14 | 0.00 | -0.00 | 0.00 | BC 23 |
| | | | | Max $M_z$ | -0.02 | 0.00 | -1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.02 | 0.00 | -1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| 54 | RC1 | 71 | 0 | Max N | 14.21 | 0.00 | 0.72 | -0.00 | 0.00 | 0.00 | BC 416 |
| | | | | Min N | -42.56 | 0.00 | 0.72 | -0.00 | 0.00 | 0.00 | BC 414 |
| | | | | Max $V_y$ | -1.90 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -1.90 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -1.90 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -42.56 | 0.00 | 0.72 | -0.00 | 0.00 | 0.00 | BC 414 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 54 | RC1 | | | Max $M_T$ | -11.39 | 0.00 | 1.06 | 0.00 | 0.00 | 0.00 | BC 271 |
| | | | | Min $M_T$ | -28.02 | 0.00 | 0.72 | -0.00 | -0.00 | 0.00 | BC 390 |
| | | | | Max $M_y$ | -5.59 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 27 |
| | | | | Min $M_y$ | -2.77 | 0.00 | 1.06 | 0.00 | -0.00 | 0.00 | BC 104 |
| | | | | Max $M_z$ | -1.90 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -1.90 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 72 | 4500 | Max N | 14.21 | 0.00 | -0.72 | -0.00 | 0.00 | 0.00 | BC 416 |
| | | | | Min N | -42.56 | 0.00 | -0.72 | -0.00 | 0.00 | 0.00 | BC 414 |
| | | | | Max $V_y$ | -1.90 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -1.90 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -42.56 | 0.00 | -0.72 | -0.00 | 0.00 | 0.00 | BC 414 |
| | | | | Min $V_z$ | -1.90 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -11.39 | 0.00 | -1.06 | 0.00 | 0.00 | 0.00 | BC 271 |
| | | | | Min $M_T$ | -28.02 | 0.00 | -0.72 | -0.00 | -0.00 | 0.00 | BC 390 |
| | | | | Max $M_y$ | -5.59 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 27 |
| | | | | Min $M_y$ | -2.77 | 0.00 | -1.06 | 0.00 | -0.00 | 0.00 | BC 104 |
| | | | | Max $M_z$ | -1.90 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -1.90 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| 55 | RC1 | 72 | 0 | Max N | 15.04 | 0.00 | 1.06 | -0.00 | -0.00 | 0.00 | BC 284 |
| | | | | Min N | -2.28 | 0.00 | 1.06 | 0.00 | 0.00 | 0.00 | BC 234 |
| | | | | Max $V_y$ | 0.07 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.07 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.07 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.91 | 0.00 | 0.72 | 0.00 | -0.00 | 0.00 | BC 52 |
| | | | | Max $M_T$ | 8.40 | 0.00 | 1.06 | 0.00 | 0.00 | 0.00 | BC 173 |
| | | | | Min $M_T$ | 13.90 | 0.00 | 1.06 | -0.00 | -0.00 | 0.00 | BC 184 |
| | | | | Max $M_y$ | -1.58 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 27 |
| | | | | Min $M_y$ | -0.88 | 0.00 | 1.06 | 0.00 | -0.00 | 0.00 | BC 76 |
| | | | | Max $M_z$ | 0.07 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.07 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 73 | 4500 | Max N | 15.04 | 0.00 | -1.06 | -0.00 | -0.00 | 0.00 | BC 284 |
| | | | | Min N | -2.28 | 0.00 | -1.06 | 0.00 | 0.00 | 0.00 | BC 234 |
| | | | | Max $V_y$ | 0.07 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.07 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.91 | 0.00 | -0.72 | 0.00 | -0.00 | 0.00 | BC 52 |
| | | | | Min $V_z$ | 0.07 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 8.40 | 0.00 | -1.06 | 0.00 | 0.00 | 0.00 | BC 173 |
| | | | | Min $M_T$ | 13.90 | 0.00 | -1.06 | -0.00 | -0.00 | 0.00 | BC 184 |
| | | | | Max $M_y$ | -1.58 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 27 |
| | | | | Min $M_y$ | -0.88 | 0.00 | -1.06 | 0.00 | -0.00 | 0.00 | BC 76 |
| | | | | Max $M_z$ | 0.07 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.07 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| 56 | RC1 | 73 | 0 | Max N | 15.26 | 0.00 | 1.06 | -0.00 | -0.00 | 0.00 | BC 224 |
| | | | | Min N | -41.89 | 0.00 | 0.72 | 0.00 | 0.00 | 0.00 | BC 411 |
| | | | | Max $V_y$ | -1.66 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -1.66 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.91 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 2 |
| | | | | Min $V_z$ | -41.89 | 0.00 | 0.72 | 0.00 | 0.00 | 0.00 | BC 411 |
| | | | | Max $M_T$ | 8.95 | 0.00 | 1.06 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min $M_T$ | -22.96 | 0.00 | 0.72 | -0.00 | 0.00 | 0.00 | BC 358 |
| | | | | Max $M_y$ | -3.46 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 27 |
| | | | | Min $M_y$ | -3.90 | 0.00 | 1.06 | 0.00 | -0.00 | 0.00 | BC 91 |
| | | | | Max $M_z$ | -1.66 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -1.66 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 74 | 4500 | Max N | 15.26 | 0.00 | -1.06 | -0.00 | -0.00 | 0.00 | BC 224 |
| | | | | Min N | -41.89 | 0.00 | -0.72 | 0.00 | 0.00 | 0.00 | BC 411 |
| | | | | Max $V_y$ | -1.66 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -1.66 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -41.89 | 0.00 | -0.72 | 0.00 | 0.00 | 0.00 | BC 411 |
| | | | | Min $V_z$ | -0.91 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 2 |
| | | | | Max $M_T$ | 8.95 | 0.00 | -1.06 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min $M_T$ | -22.96 | 0.00 | -0.72 | -0.00 | 0.00 | 0.00 | BC 358 |
| | | | | Max $M_y$ | -3.46 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 27 |
| | | | | Min $M_y$ | -3.90 | 0.00 | -1.06 | 0.00 | -0.00 | 0.00 | BC 91 |
| | | | | Max $M_z$ | -1.66 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -1.66 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| 57 | RC1 | 74 | 0 | Max N | 18.98 | 0.00 | 1.01 | 0.00 | 0.00 | 0.00 | BC 220 |
| | | | | Min N | -13.40 | 0.00 | 0.69 | -0.00 | 0.00 | 0.00 | BC 423 |
| | | | | Max $V_y$ | 0.03 | 0.00 | 1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.03 | 0.00 | 1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.03 | 0.00 | 1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -13.39 | 0.00 | 0.69 | -0.00 | 0.00 | 0.00 | BC 355 |
| | | | | Max $M_T$ | 18.94 | 0.00 | 1.01 | 0.00 | 0.00 | 0.00 | BC 240 |
| | | | | Min $M_T$ | -13.36 | 0.00 | 1.01 | -0.00 | 0.00 | 0.00 | BC 167 |
| | | | | Max $M_y$ | 0.02 | 0.00 | 1.14 | 0.00 | 0.00 | 0.00 | BC 23 |
| | | | | Min $M_y$ | 0.01 | 0.00 | 1.14 | 0.00 | -0.00 | 0.00 | BC 27 |
| | | | | Max $M_z$ | 0.03 | 0.00 | 1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.03 | 0.00 | 1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | 16 | 4300 | Max N | 18.98 | 0.00 | -1.01 | 0.00 | 0.00 | 0.00 | BC 220 |
| | | | | Min N | -13.40 | 0.00 | -0.69 | -0.00 | 0.00 | 0.00 | BC 423 |
| | | | | Max $V_y$ | 0.03 | 0.00 | -1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.03 | 0.00 | -1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -13.39 | 0.00 | -0.69 | -0.00 | 0.00 | 0.00 | BC 355 |
| | | | | Min $V_z$ | 0.03 | 0.00 | -1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 18.94 | 0.00 | -1.01 | 0.00 | 0.00 | 0.00 | BC 240 |
| | | | | Min $M_T$ | -13.36 | 0.00 | -1.01 | -0.00 | 0.00 | 0.00 | BC 167 |
| | | | | Max $M_y$ | 0.02 | 0.00 | -1.14 | 0.00 | 0.00 | 0.00 | BC 23 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 57 | RC1 | | | Min $M_y$ | 0.01 | 0.00 | -1.14 | 0.00 | -0.00 | 0.00 | BC 27 |
| | | | | Max $M_z$ | 0.03 | 0.00 | -1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.03 | 0.00 | -1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| 58 | RC1 | 12 | 0 | Max N | 19.35 | 0.00 | 0.69 | 0.00 | 0.00 | 0.00 | BC 409 |
| | | | | Min N | -13.79 | 0.00 | 0.69 | -0.00 | 0.00 | 0.00 | BC 438 |
| | | | | Max $V_y$ | -0.03 | 0.00 | 1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.03 | 0.00 | 1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.03 | 0.00 | 1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -13.75 | 0.00 | 0.69 | -0.00 | 0.00 | 0.00 | BC 354 |
| | | | | Max $M_T$ | -0.17 | 0.00 | 1.01 | 0.00 | 0.00 | 0.00 | BC 139 |
| | | | | Min $M_T$ | -13.76 | 0.00 | 0.69 | -0.00 | 0.00 | 0.00 | BC 390 |
| | | | | Max $M_y$ | 10.81 | 0.00 | 1.01 | 0.00 | 0.00 | 0.00 | BC 268 |
| | | | | Min $M_y$ | -0.21 | 0.00 | 1.01 | 0.00 | -0.00 | 0.00 | BC 147 |
| | | | | Max $M_z$ | -0.03 | 0.00 | 1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.03 | 0.00 | 1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 75 | 4300 | Max N | 19.35 | 0.00 | -0.69 | 0.00 | 0.00 | 0.00 | BC 409 |
| | | | | Min N | -13.79 | 0.00 | -0.69 | -0.00 | 0.00 | 0.00 | BC 438 |
| | | | | Max $V_y$ | -0.03 | 0.00 | -1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.03 | 0.00 | -1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -13.75 | 0.00 | -0.69 | -0.00 | 0.00 | 0.00 | BC 354 |
| | | | | Min $V_z$ | -0.03 | 0.00 | -1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.17 | 0.00 | -1.01 | 0.00 | 0.00 | 0.00 | BC 139 |
| | | | | Min $M_T$ | -13.76 | 0.00 | -0.69 | -0.00 | 0.00 | 0.00 | BC 390 |
| | | | | Max $M_y$ | 10.81 | 0.00 | -1.01 | 0.00 | 0.00 | 0.00 | BC 268 |
| | | | | Min $M_y$ | -0.21 | 0.00 | -1.01 | 0.00 | -0.00 | 0.00 | BC 147 |
| | | | | Max $M_z$ | -0.03 | 0.00 | -1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.03 | 0.00 | -1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| 59 | RC1 | 75 | 0 | Max N | 14.72 | 0.00 | 0.72 | 0.00 | 0.00 | 0.00 | BC 357 |
| | | | | Min N | -44.04 | 0.00 | 0.72 | 0.00 | 0.00 | 0.00 | BC 410 |
| | | | | Max $V_y$ | -0.66 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.66 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.06 | 0.00 | 1.19 | 0.00 | -0.00 | 0.00 | BC 2 |
| | | | | Min $V_z$ | -44.04 | 0.00 | 0.72 | 0.00 | 0.00 | 0.00 | BC 410 |
| | | | | Max $M_T$ | -30.01 | 0.00 | 1.06 | 0.00 | 0.00 | 0.00 | BC 202 |
| | | | | Min $M_T$ | -24.93 | 0.00 | 0.72 | -0.00 | 0.00 | 0.00 | BC 367 |
| | | | | Max $M_y$ | -7.89 | 0.00 | 1.06 | 0.00 | 0.00 | 0.00 | BC 146 |
| | | | | Min $M_y$ | -5.88 | 0.00 | 1.06 | 0.00 | -0.00 | 0.00 | BC 91 |
| | | | | Max $M_z$ | -0.66 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.66 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 76 | 4500 | Max N | 14.72 | 0.00 | -0.72 | 0.00 | 0.00 | 0.00 | BC 357 |
| | | | | Min N | -44.04 | 0.00 | -0.72 | 0.00 | 0.00 | 0.00 | BC 410 |
| | | | | Max $V_y$ | -0.66 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.66 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -44.04 | 0.00 | -0.72 | 0.00 | 0.00 | 0.00 | BC 410 |
| | | | | Min $V_z$ | -0.06 | 0.00 | -1.19 | 0.00 | -0.00 | 0.00 | BC 2 |
| | | | | Max $M_T$ | -30.01 | 0.00 | -1.06 | 0.00 | 0.00 | 0.00 | BC 202 |
| | | | | Min $M_T$ | -24.93 | 0.00 | -0.72 | -0.00 | 0.00 | 0.00 | BC 367 |
| | | | | Max $M_y$ | -7.89 | 0.00 | -1.06 | 0.00 | 0.00 | 0.00 | BC 146 |
| | | | | Min $M_y$ | -5.88 | 0.00 | -1.06 | 0.00 | -0.00 | 0.00 | BC 91 |
| | | | | Max $M_z$ | -0.66 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.66 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| 60 | RC1 | 76 | 0 | Max N | 15.79 | 0.00 | 0.72 | -0.00 | 0.00 | 0.00 | BC 413 |
| | | | | Min N | -2.26 | 0.00 | 1.06 | 0.00 | 0.00 | 0.00 | BC 246 |
| | | | | Max $V_y$ | -0.00 | 0.00 | 1.19 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.00 | 0.00 | 1.19 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.00 | 0.00 | 1.19 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -1.87 | 0.00 | 0.72 | -0.00 | 0.00 | 0.00 | BC 331 |
| | | | | Max $M_T$ | 2.97 | 0.00 | 0.72 | 0.00 | 0.00 | 0.00 | BC 471 |
| | | | | Min $M_T$ | -1.33 | 0.00 | 1.06 | -0.00 | 0.00 | 0.00 | BC 134 |
| | | | | Max $M_y$ | -0.40 | 0.00 | 1.06 | -0.00 | 0.00 | 0.00 | BC 147 |
| | | | | Min $M_y$ | -0.41 | 0.00 | 1.06 | -0.00 | -0.00 | 0.00 | BC 91 |
| | | | | Max $M_z$ | -0.00 | 0.00 | 1.19 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.00 | 0.00 | 1.19 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | 77 | 4500 | Max N | 15.79 | 0.00 | -0.72 | -0.00 | 0.00 | 0.00 | BC 413 |
| | | | | Min N | -2.26 | 0.00 | -1.06 | 0.00 | 0.00 | 0.00 | BC 246 |
| | | | | Max $V_y$ | -0.00 | 0.00 | -1.19 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.00 | 0.00 | -1.19 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -1.87 | 0.00 | -0.72 | -0.00 | 0.00 | 0.00 | BC 331 |
| | | | | Min $V_z$ | -0.00 | 0.00 | -1.19 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 2.97 | 0.00 | -0.72 | 0.00 | 0.00 | 0.00 | BC 471 |
| | | | | Min $M_T$ | -1.33 | 0.00 | -1.06 | -0.00 | 0.00 | 0.00 | BC 134 |
| | | | | Max $M_y$ | -0.40 | 0.00 | -1.06 | -0.00 | 0.00 | 0.00 | BC 147 |
| | | | | Min $M_y$ | -0.41 | 0.00 | -1.06 | -0.00 | -0.00 | 0.00 | BC 91 |
| | | | | Max $M_z$ | -0.00 | 0.00 | -1.19 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.00 | 0.00 | -1.19 | -0.00 | 0.00 | 0.00 | BC 1 |
| 61 | RC1 | 77 | 0 | Max N | 15.07 | 0.00 | 1.06 | 0.00 | 0.00 | 0.00 | BC 213 |
| | | | | Min N | -45.31 | 0.00 | 0.72 | -0.00 | 0.00 | 0.00 | BC 415 |
| | | | | Max $V_y$ | -0.81 | 0.00 | 1.19 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.81 | 0.00 | 1.19 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.13 | 0.00 | 1.19 | -0.00 | 0.00 | 0.00 | BC 17 |
| | | | | Min $V_z$ | -45.27 | 0.00 | 0.72 | -0.00 | 0.00 | 0.00 | BC 411 |
| | | | | Max $M_T$ | 14.38 | 0.00 | 0.72 | 0.00 | 0.00 | 0.00 | BC 361 |
| | | | | Min $M_T$ | -44.05 | 0.00 | 1.06 | -0.00 | -0.00 | 0.00 | BC 283 |
| | | | | Max $M_y$ | -6.15 | 0.00 | 1.06 | -0.00 | 0.00 | 0.00 | BC 146 |
| | | | | Min $M_y$ | -7.96 | 0.00 | 1.06 | -0.00 | -0.00 | 0.00 | BC 87 |
| | | | | Max $M_z$ | -0.81 | 0.00 | 1.19 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.81 | 0.00 | 1.19 | -0.00 | 0.00 | 0.00 | BC 1 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 61 | RC1 | 78 | 4500 | Max N | 15.07 | 0.00 | -1.06 | 0.00 | 0.00 | 0.00 | BC 213 |
| | | | | Min N | -45.31 | 0.00 | -0.72 | -0.00 | 0.00 | 0.00 | BC 415 |
| | | | | Max $V_y$ | -0.81 | 0.00 | -1.19 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.81 | 0.00 | -1.19 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -45.27 | 0.00 | -0.72 | -0.00 | 0.00 | 0.00 | BC 411 |
| | | | | Min $V_z$ | -0.13 | 0.00 | -1.19 | -0.00 | 0.00 | 0.00 | BC 17 |
| | | | | Max $M_T$ | 14.38 | 0.00 | -0.72 | 0.00 | 0.00 | 0.00 | BC 361 |
| | | | | Min $M_T$ | -44.05 | 0.00 | -1.06 | -0.00 | -0.00 | 0.00 | BC 283 |
| | | | | Max $M_y$ | -6.15 | 0.00 | -1.06 | -0.00 | 0.00 | 0.00 | BC 146 |
| | | | | Min $M_y$ | -7.96 | 0.00 | -1.06 | -0.00 | -0.00 | 0.00 | BC 87 |
| | | | | Max $M_z$ | -0.81 | 0.00 | -1.19 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.81 | 0.00 | -1.19 | -0.00 | 0.00 | 0.00 | BC 1 |
| 62 | RC1 | 78 | 0 | Max N | 19.39 | 0.00 | 1.01 | -0.00 | 0.00 | 0.00 | BC 217 |
| | | | | Min N | -13.73 | 0.00 | 0.69 | 0.00 | 0.00 | 0.00 | BC 451 |
| | | | | Max $V_y$ | 0.06 | 0.00 | 1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.06 | 0.00 | 1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.06 | 0.00 | 1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -13.71 | 0.00 | 0.69 | 0.00 | 0.00 | 0.00 | BC 355 |
| | | | | Max $M_T$ | -13.65 | 0.00 | 1.01 | 0.00 | 0.00 | 0.00 | BC 243 |
| | | | | Min $M_T$ | 19.39 | 0.00 | 0.69 | -0.00 | 0.00 | 0.00 | BC 357 |
| | | | | Max $M_y$ | 10.87 | 0.00 | 1.01 | 0.00 | 0.00 | 0.00 | BC 264 |
| | | | | Min $M_y$ | 10.87 | 0.00 | 1.01 | 0.00 | -0.00 | 0.00 | BC 268 |
| | | | | Max $M_z$ | 0.06 | 0.00 | 1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.06 | 0.00 | 1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 17 | 4300 | Max N | 19.39 | 0.00 | -1.01 | -0.00 | 0.00 | 0.00 | BC 217 |
| | | | | Min N | -13.73 | 0.00 | -0.69 | 0.00 | 0.00 | 0.00 | BC 451 |
| | | | | Max $V_y$ | 0.06 | 0.00 | -1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.06 | 0.00 | -1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -13.71 | 0.00 | -0.69 | 0.00 | 0.00 | 0.00 | BC 355 |
| | | | | Min $V_z$ | 0.06 | 0.00 | -1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -13.65 | 0.00 | -1.01 | 0.00 | 0.00 | 0.00 | BC 243 |
| | | | | Min $M_T$ | 19.39 | 0.00 | -0.69 | -0.00 | 0.00 | 0.00 | BC 357 |
| | | | | Max $M_y$ | 10.87 | 0.00 | -1.01 | 0.00 | 0.00 | 0.00 | BC 264 |
| | | | | Min $M_y$ | 10.87 | 0.00 | -1.01 | 0.00 | -0.00 | 0.00 | BC 268 |
| | | | | Max $M_z$ | 0.06 | 0.00 | -1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.06 | 0.00 | -1.14 | 0.00 | 0.00 | 0.00 | BC 1 |
| 63 | RC1 | 45 | 0 | Max N | 5.00 | 0.00 | 1.20 | -0.00 | 0.00 | 0.00 | BC 236 |
| | | | | Min N | -3.58 | 0.00 | 0.82 | 0.01 | 0.00 | 0.00 | BC 414 |
| | | | | Max $V_y$ | 0.03 | 0.00 | 1.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.03 | 0.00 | 1.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.03 | 0.00 | 1.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -3.54 | 0.00 | 0.82 | 0.01 | 0.00 | 0.00 | BC 354 |
| | | | | Max $M_T$ | -3.55 | 0.00 | 1.20 | 0.01 | 0.00 | 0.00 | BC 206 |
| | | | | Min $M_T$ | 4.94 | 0.00 | 0.82 | -0.00 | 0.00 | 0.00 | BC 448 |
| | | | | Max $M_y$ | 4.97 | 0.00 | 0.82 | -0.00 | 0.00 | 0.00 | BC 428 |
| | | | | Min $M_y$ | 0.05 | 0.00 | 1.35 | 0.00 | -0.00 | 0.00 | BC 6 |
| | | | | Max $M_z$ | 0.03 | 0.00 | 1.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.03 | 0.00 | 1.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 49 | 4300 | Max N | 5.00 | 0.00 | -1.20 | -0.00 | 0.00 | 0.00 | BC 236 |
| | | | | Min N | -3.58 | 0.00 | -0.82 | 0.01 | 0.00 | 0.00 | BC 414 |
| | | | | Max $V_y$ | 0.03 | 0.00 | -1.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.03 | 0.00 | -1.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -3.54 | 0.00 | -0.82 | 0.01 | -0.00 | 0.00 | BC 354 |
| | | | | Min $V_z$ | 0.03 | 0.00 | -1.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -3.55 | 0.00 | -1.20 | 0.01 | 0.00 | 0.00 | BC 206 |
| | | | | Min $M_T$ | 4.94 | 0.00 | -0.82 | -0.00 | 0.00 | 0.00 | BC 448 |
| | | | | Max $M_y$ | 0.05 | 0.00 | -1.20 | 0.00 | 0.00 | 0.00 | BC 103 |
| | | | | Min $M_y$ | 0.05 | 0.00 | -1.35 | 0.00 | -0.00 | 0.00 | BC 6 |
| | | | | Max $M_z$ | 0.03 | 0.00 | -1.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.03 | 0.00 | -1.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| 64 | RC1 | 49 | 0 | Max N | -5.89 | 0.00 | 0.86 | 0.00 | 0.00 | 0.00 | BC 477 |
| | | | | Min N | -39.58 | 0.00 | 1.25 | 0.00 | 0.00 | 0.00 | BC 146 |
| | | | | Max $V_y$ | -14.80 | 0.00 | 1.42 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -14.80 | 0.00 | 1.42 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -13.53 | 0.00 | 1.42 | -0.00 | 0.00 | 0.00 | BC 15 |
| | | | | Min $V_z$ | -35.23 | 0.00 | 0.86 | 0.00 | 0.00 | 0.00 | BC 338 |
| | | | | Max $M_T$ | -27.25 | 0.00 | 1.25 | 0.00 | 0.00 | 0.00 | BC 247 |
| | | | | Min $M_T$ | -28.17 | 0.00 | 1.25 | -0.00 | 0.00 | 0.00 | BC 206 |
| | | | | Max $M_y$ | -16.11 | 0.00 | 1.42 | 0.00 | 0.00 | 0.00 | BC 3 |
| | | | | Min $M_y$ | -22.44 | 0.00 | 1.25 | -0.00 | -0.00 | 0.00 | BC 172 |
| | | | | Max $M_z$ | -14.80 | 0.00 | 1.42 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -14.80 | 0.00 | 1.42 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 51 | 4500 | Max N | -5.89 | 0.00 | -0.86 | 0.00 | 0.00 | 0.00 | BC 477 |
| | | | | Min N | -39.58 | 0.00 | -1.25 | 0.00 | 0.00 | 0.00 | BC 146 |
| | | | | Max $V_y$ | -14.80 | 0.00 | -1.42 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -14.80 | 0.00 | -1.42 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -35.23 | 0.00 | -0.86 | 0.00 | 0.00 | 0.00 | BC 338 |
| | | | | Min $V_z$ | -13.53 | 0.00 | -1.42 | -0.00 | 0.00 | 0.00 | BC 15 |
| | | | | Max $M_T$ | -27.25 | 0.00 | -1.25 | 0.00 | 0.00 | 0.00 | BC 247 |
| | | | | Min $M_T$ | -28.17 | 0.00 | -1.25 | -0.00 | 0.00 | 0.00 | BC 206 |
| | | | | Max $M_y$ | -16.11 | 0.00 | -1.42 | 0.00 | 0.00 | 0.00 | BC 3 |
| | | | | Min $M_y$ | -22.44 | 0.00 | -1.25 | -0.00 | -0.00 | 0.00 | BC 172 |
| | | | | Max $M_z$ | -14.80 | 0.00 | -1.42 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -14.80 | 0.00 | -1.42 | 0.00 | 0.00 | 0.00 | BC 1 |
| 65 | RC1 | 51 | 0 | Max N | 22.35 | 0.00 | 0.86 | 0.00 | 0.00 | 0.00 | BC 413 |
| | | | | Min N | -15.52 | 0.00 | 1.25 | 0.00 | 0.00 | 0.00 | BC 234 |
| | | | | Max $V_y$ | -1.89 | 0.00 | 1.42 | -0.00 | 0.00 | 0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 65 | RC1 | | | Min $V_y$ | -1.89 | 0.00 | 1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 7.55 | 0.00 | 1.42 | -0.00 | 0.00 | 0.00 | BC 15 |
| | | | | Min $V_z$ | -12.53 | 0.00 | 0.86 | 0.00 | -0.00 | 0.00 | BC 426 |
| | | | | Max $M_T$ | 4.67 | 0.00 | 0.86 | 0.00 | -0.00 | 0.00 | BC 446 |
| | | | | Min $M_T$ | -5.85 | 0.00 | 1.25 | -0.00 | 0.00 | 0.00 | BC 141 |
| | | | | Max $M_y$ | -3.17 | 0.00 | 1.42 | -0.00 | 0.00 | 0.00 | BC 3 |
| | | | | Min $M_y$ | 4.41 | 0.00 | 1.42 | -0.00 | -0.00 | 0.00 | BC 27 |
| | | | | Max $M_z$ | -1.89 | 0.00 | 1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -1.89 | 0.00 | 1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | 53 | 4500 | Max N | 22.35 | 0.00 | -0.86 | 0.00 | 0.00 | 0.00 | BC 413 |
| | | | | Min N | -15.52 | 0.00 | -1.25 | 0.00 | 0.00 | 0.00 | BC 234 |
| | | | | Max $V_y$ | -1.89 | 0.00 | -1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -1.89 | 0.00 | -1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -12.53 | 0.00 | -0.86 | 0.00 | -0.00 | 0.00 | BC 426 |
| | | | | Min $V_z$ | 7.55 | 0.00 | -1.42 | -0.00 | 0.00 | 0.00 | BC 15 |
| | | | | Max $M_T$ | 4.67 | 0.00 | -0.86 | 0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Min $M_T$ | -5.85 | 0.00 | -1.25 | -0.00 | 0.00 | 0.00 | BC 141 |
| | | | | Max $M_y$ | -3.17 | 0.00 | -1.42 | -0.00 | 0.00 | 0.00 | BC 3 |
| | | | | Min $M_y$ | 4.41 | 0.00 | -1.42 | -0.00 | -0.00 | 0.00 | BC 27 |
| | | | | Max $M_z$ | -1.89 | 0.00 | -1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -1.89 | 0.00 | -1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| 66 | RC1 | 53 | 0 | Max N | 0.72 | 0.00 | 1.25 | -0.00 | 0.00 | 0.00 | BC 237 |
| | | | | Min N | -27.36 | 0.00 | 1.25 | -0.00 | -0.00 | 0.00 | BC 246 |
| | | | | Max $V_y$ | -1.82 | 0.00 | 1.42 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -1.82 | 0.00 | 1.42 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.23 | 0.00 | 1.42 | 0.00 | 0.00 | 0.00 | BC 5 |
| | | | | Min $V_z$ | -26.17 | 0.00 | 0.86 | -0.00 | -0.00 | 0.00 | BC 426 |
| | | | | Max $M_T$ | -19.41 | 0.00 | 0.86 | 0.00 | 0.00 | 0.00 | BC 419 |
| | | | | Min $M_T$ | -12.23 | 0.00 | 0.86 | -0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Max $M_y$ | -3.09 | 0.00 | 1.42 | 0.00 | 0.00 | 0.00 | BC 3 |
| | | | | Min $M_y$ | -0.60 | 0.00 | 0.86 | 0.00 | -0.00 | 0.00 | BC 420 |
| | | | | Max $M_z$ | -1.82 | 0.00 | 1.42 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -1.82 | 0.00 | 1.42 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 55 | 4500 | Max N | 0.72 | 0.00 | -1.25 | -0.00 | 0.00 | 0.00 | BC 237 |
| | | | | Min N | -27.36 | 0.00 | -1.25 | -0.00 | 0.00 | 0.00 | BC 246 |
| | | | | Max $V_y$ | -1.82 | 0.00 | -1.42 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -1.82 | 0.00 | -1.42 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -26.17 | 0.00 | -0.86 | -0.00 | -0.00 | 0.00 | BC 426 |
| | | | | Min $V_z$ | 0.23 | 0.00 | -1.42 | 0.00 | 0.00 | 0.00 | BC 5 |
| | | | | Max $M_T$ | -19.41 | 0.00 | -0.86 | 0.00 | 0.00 | 0.00 | BC 419 |
| | | | | Min $M_T$ | -12.23 | 0.00 | -0.86 | -0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Max $M_y$ | -3.09 | 0.00 | -1.42 | 0.00 | 0.00 | 0.00 | BC 3 |
| | | | | Min $M_y$ | -0.60 | 0.00 | -0.86 | 0.00 | -0.00 | 0.00 | BC 420 |
| | | | | Max $M_z$ | -1.82 | 0.00 | -1.42 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -1.82 | 0.00 | -1.42 | 0.00 | 0.00 | 0.00 | BC 1 |
| 67 | RC1 | 55 | 0 | Max N | 4.96 | 0.00 | 1.20 | 0.00 | 0.00 | 0.00 | BC 200 |
| | | | | Min N | -3.57 | 0.00 | 1.20 | -0.01 | 0.00 | 0.00 | BC 223 |
| | | | | Max $V_y$ | 0.02 | 0.00 | 1.35 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.02 | 0.00 | 1.35 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.02 | 0.00 | 1.35 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -3.53 | 0.00 | 0.82 | -0.01 | 0.00 | 0.00 | BC 355 |
| | | | | Max $M_T$ | 4.92 | 0.00 | 1.20 | 0.00 | 0.00 | 0.00 | BC 240 |
| | | | | Min $M_T$ | -3.53 | 0.00 | 0.82 | -0.01 | 0.00 | 0.00 | BC 359 |
| | | | | Max $M_y$ | 0.01 | 0.00 | 1.35 | 0.00 | 0.00 | 0.00 | BC 27 |
| | | | | Min $M_y$ | 0.00 | 0.00 | 1.35 | 0.00 | -0.00 | 0.00 | BC 23 |
| | | | | Max $M_z$ | 0.02 | 0.00 | 1.35 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.02 | 0.00 | 1.35 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | 56 | 4300 | Max N | 4.96 | 0.00 | -1.20 | 0.00 | 0.00 | 0.00 | BC 200 |
| | | | | Min N | -3.57 | 0.00 | -1.20 | -0.01 | 0.00 | 0.00 | BC 223 |
| | | | | Max $V_y$ | 0.02 | 0.00 | -1.35 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.02 | 0.00 | -1.35 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -3.53 | 0.00 | -0.82 | -0.01 | 0.00 | 0.00 | BC 355 |
| | | | | Min $V_z$ | 0.02 | 0.00 | -1.35 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 4.92 | 0.00 | -1.20 | 0.00 | 0.00 | 0.00 | BC 240 |
| | | | | Min $M_T$ | -3.53 | 0.00 | -0.82 | -0.01 | 0.00 | 0.00 | BC 359 |
| | | | | Max $M_y$ | 0.01 | 0.00 | -1.35 | 0.00 | 0.00 | 0.00 | BC 27 |
| | | | | Min $M_y$ | 0.00 | 0.00 | -1.35 | 0.00 | -0.00 | 0.00 | BC 23 |
| | | | | Max $M_z$ | 0.02 | 0.00 | -1.35 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.02 | 0.00 | -1.35 | -0.00 | 0.00 | 0.00 | BC 1 |
| 68 | RC1 | 46 | 0 | Max N | 5.10 | 0.00 | 1.20 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min N | -3.65 | 0.00 | 0.82 | -0.01 | 0.00 | 0.00 | BC 410 |
| | | | | Max $V_y$ | 0.03 | 0.00 | 1.35 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.03 | 0.00 | 1.35 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.03 | 0.00 | 1.35 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -3.62 | 0.00 | 0.82 | -0.01 | 0.00 | 0.00 | BC 354 |
| | | | | Max $M_T$ | 5.07 | 0.00 | 0.82 | 0.00 | 0.00 | 0.00 | BC 421 |
| | | | | Min $M_T$ | -3.62 | 0.00 | 1.20 | -0.01 | -0.00 | 0.00 | BC 210 |
| | | | | Max $M_y$ | 0.16 | 0.00 | 1.20 | -0.00 | 0.00 | 0.00 | BC 147 |
| | | | | Min $M_y$ | 2.70 | 0.00 | 1.20 | -0.00 | -0.00 | 0.00 | BC 268 |
| | | | | Max $M_z$ | 0.03 | 0.00 | 1.35 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.03 | 0.00 | 1.35 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | 37 | 4300 | Max N | 5.10 | 0.00 | -1.20 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min N | -3.65 | 0.00 | -0.82 | -0.01 | 0.00 | 0.00 | BC 410 |
| | | | | Max $V_y$ | 0.03 | 0.00 | -1.35 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.03 | 0.00 | -1.35 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -3.62 | 0.00 | -0.82 | -0.01 | 0.00 | 0.00 | BC 354 |
| | | | | Min $V_z$ | 0.03 | 0.00 | -1.35 | -0.00 | 0.00 | 0.00 | BC 1 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 68 | RC1 | | | Max $M_T$ | 5.07 | 0.00 | -0.82 | 0.00 | 0.00 | 0.00 | BC 421 |
| | | | | Min $M_T$ | -3.62 | 0.00 | -1.20 | -0.01 | -0.00 | 0.00 | BC 210 |
| | | | | Max $M_y$ | -3.60 | 0.00 | -1.20 | -0.01 | 0.00 | 0.00 | BC 274 |
| | | | | Min $M_y$ | 0.04 | 0.00 | -1.20 | -0.00 | -0.00 | 0.00 | BC 91 |
| | | | | Max $M_z$ | 0.03 | 0.00 | -1.35 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.03 | 0.00 | -1.35 | -0.00 | 0.00 | 0.00 | BC 1 |
| 69 | RC1 | 37 | 0 | Max N | -7.84 | 0.00 | 0.86 | 0.00 | 0.00 | 0.00 | BC 417 |
| | | | | Min N | -40.40 | 0.00 | 1.25 | 0.00 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_y$ | -14.90 | 0.00 | 1.42 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -14.90 | 0.00 | 1.42 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -14.15 | 0.00 | 1.42 | 0.00 | 0.00 | 0.00 | BC 2 |
| | | | | Min $V_z$ | -36.07 | 0.00 | 0.86 | 0.00 | 0.00 | 0.00 | BC 338 |
| | | | | Max $M_T$ | -27.58 | 0.00 | 1.25 | 0.00 | 0.00 | 0.00 | BC 206 |
| | | | | Min $M_T$ | -25.97 | 0.00 | 1.25 | -0.01 | 0.00 | 0.00 | BC 235 |
| | | | | Max $M_y$ | -24.08 | 0.00 | 1.25 | 0.00 | 0.00 | 0.00 | BC 162 |
| | | | | Min $M_y$ | -29.50 | 0.00 | 1.25 | 0.00 | -0.00 | 0.00 | BC 122 |
| | | | | Max $M_z$ | -14.90 | 0.00 | 1.42 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -14.90 | 0.00 | 1.42 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 61 | 4500 | Max N | -7.84 | 0.00 | -0.86 | 0.00 | 0.00 | 0.00 | BC 417 |
| | | | | Min N | -40.40 | 0.00 | -1.25 | 0.00 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_y$ | -14.90 | 0.00 | -1.42 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -14.90 | 0.00 | -1.42 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -36.07 | 0.00 | -0.86 | 0.00 | 0.00 | 0.00 | BC 338 |
| | | | | Min $V_z$ | -14.15 | 0.00 | -1.42 | 0.00 | 0.00 | 0.00 | BC 2 |
| | | | | Max $M_T$ | -27.58 | 0.00 | -1.25 | 0.00 | 0.00 | 0.00 | BC 206 |
| | | | | Min $M_T$ | -25.97 | 0.00 | -1.25 | -0.01 | 0.00 | 0.00 | BC 235 |
| | | | | Max $M_y$ | -24.08 | 0.00 | -1.25 | 0.00 | 0.00 | 0.00 | BC 162 |
| | | | | Min $M_y$ | -29.50 | 0.00 | -1.25 | 0.00 | -0.00 | 0.00 | BC 122 |
| | | | | Max $M_z$ | -14.90 | 0.00 | -1.42 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -14.90 | 0.00 | -1.42 | 0.00 | -0.00 | 0.00 | BC 1 |
| 70 | RC1 | 61 | 0 | Max N | 20.67 | 0.04 | 1.22 | 0.00 | 0.00 | 0.00 | BC 408 |
| | | | | Min N | -12.22 | 0.02 | 2.06 | 0.00 | -0.00 | 0.00 | BC 246 |
| | | | | Max $V_y$ | 7.73 | 0.05 | 1.22 | 0.00 | 0.00 | 0.00 | BC 448 |
| | | | | Min $V_y$ | -7.13 | -0.03 | 2.82 | -0.00 | 0.00 | 0.00 | BC 131 |
| | | | | Max $V_z$ | -1.59 | -0.02 | 2.82 | -0.00 | -0.00 | 0.00 | BC 154 |
| | | | | Min $V_z$ | -1.84 | -0.01 | 1.22 | 0.00 | 0.00 | 0.00 | BC 42 |
| | | | | Max $M_T$ | 10.78 | 0.01 | 1.22 | 0.01 | 0.00 | 0.00 | BC 471 |
| | | | | Min $M_T$ | 2.45 | -0.01 | 1.49 | -0.00 | 0.00 | 0.00 | BC 365 |
| | | | | Max $M_y$ | -7.92 | -0.03 | 2.82 | -0.00 | 0.00 | 0.00 | BC 146 |
| | | | | Min $M_y$ | -6.82 | 0.03 | 1.49 | 0.00 | -0.00 | 0.00 | BC 406 |
| | | | | Max $M_z$ | -6.08 | -0.02 | 2.60 | -0.00 | 0.00 | 0.00 | BC 99 |
| | | | | Min $M_z$ | 9.60 | 0.05 | 1.22 | 0.00 | 0.00 | -0.00 | BC 356 |
| | | 101 | 4300 | Max N | 20.67 | 0.04 | -0.41 | 0.00 | 1.73 | -0.18 | BC 408 |
| | | | | Min N | -12.22 | 0.02 | -0.34 | 0.00 | 3.69 | -0.10 | BC 246 |
| | | | | Max $V_y$ | 7.73 | 0.05 | -0.42 | 0.00 | 1.73 | -0.21 | BC 448 |
| | | | | Min $V_y$ | -7.13 | -0.03 | 0.42 | -0.00 | 6.96 | 0.11 | BC 131 |
| | | | | Max $V_z$ | -0.51 | -0.02 | 0.62 | -0.00 | 6.17 | 0.09 | BC 346 |
| | | | | Min $V_z$ | -2.05 | -0.01 | -0.69 | 0.00 | 2.83 | 0.04 | BC 10 |
| | | | | Max $M_T$ | 10.78 | 0.01 | -0.42 | 0.01 | 1.72 | -0.02 | BC 471 |
| | | | | Min $M_T$ | 2.45 | -0.01 | -0.15 | -0.00 | 2.88 | 0.03 | BC 365 |
| | | | | Max $M_y$ | -1.59 | -0.02 | 0.42 | -0.00 | 6.96 | 0.10 | BC 154 |
| | | | | Min $M_y$ | -1.84 | -0.01 | -0.42 | 0.00 | 1.71 | 0.02 | BC 42 |
| | | | | Max $M_z$ | -7.13 | -0.03 | 0.42 | -0.00 | 6.96 | 0.11 | BC 131 |
| | | | | Min $M_z$ | 7.73 | 0.05 | -0.42 | 0.00 | 1.73 | -0.21 | BC 448 |
| 71 | RC1 | 63 | 0 | Max N | 2.96 | 0.00 | 1.25 | -0.01 | -0.00 | 0.00 | BC 264 |
| | | | | Min N | -26.76 | 0.00 | 1.25 | -0.01 | 0.00 | 0.00 | BC 234 |
| | | | | Max $V_y$ | -0.92 | 0.00 | 1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.92 | 0.00 | 1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.34 | 0.00 | 1.42 | -0.00 | 0.00 | 0.00 | BC 2 |
| | | | | Min $V_z$ | -25.92 | 0.00 | 0.86 | -0.00 | 0.00 | 0.00 | BC 426 |
| | | | | Max $M_T$ | 2.17 | 0.00 | 0.86 | 0.00 | 0.00 | 0.00 | BC 361 |
| | | | | Min $M_T$ | -18.32 | 0.00 | 1.25 | -0.01 | 0.00 | 0.00 | BC 271 |
| | | | | Max $M_y$ | -8.24 | 0.00 | 1.25 | -0.00 | 0.00 | 0.00 | BC 146 |
| | | | | Min $M_y$ | -4.97 | 0.00 | 1.25 | -0.00 | -0.00 | 0.00 | BC 136 |
| | | | | Max $M_z$ | -0.92 | 0.00 | 1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.92 | 0.00 | 1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | 65 | 4500 | Max N | 2.96 | 0.00 | -1.25 | -0.01 | -0.00 | 0.00 | BC 264 |
| | | | | Min N | -26.76 | 0.00 | -1.25 | -0.01 | 0.00 | 0.00 | BC 234 |
| | | | | Max $V_y$ | -0.92 | 0.00 | -1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.92 | 0.00 | -1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -25.92 | 0.00 | -0.86 | -0.00 | 0.00 | 0.00 | BC 426 |
| | | | | Min $V_z$ | -0.34 | 0.00 | -1.42 | -0.00 | 0.00 | 0.00 | BC 2 |
| | | | | Max $M_T$ | 2.17 | 0.00 | -0.86 | 0.00 | 0.00 | 0.00 | BC 361 |
| | | | | Min $M_T$ | -18.32 | 0.00 | -1.25 | -0.01 | 0.00 | 0.00 | BC 271 |
| | | | | Max $M_y$ | -8.24 | 0.00 | -1.25 | -0.00 | 0.00 | 0.00 | BC 146 |
| | | | | Min $M_y$ | -4.95 | 0.00 | -1.25 | -0.00 | -0.00 | 0.00 | BC 115 |
| | | | | Max $M_z$ | -0.92 | 0.00 | -1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.92 | 0.00 | -1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| 72 | RC1 | 65 | 0 | Max N | 5.06 | 0.00 | 0.82 | -0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min N | -3.81 | 0.00 | 1.20 | 0.01 | 0.00 | 0.00 | BC 207 |
| | | | | Max $V_y$ | -0.02 | 0.00 | 1.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.02 | 0.00 | 1.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.02 | 0.00 | 1.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -3.77 | 0.00 | 0.82 | 0.01 | 0.00 | 0.00 | BC 355 |
| | | | | Max $M_T$ | -3.80 | 0.00 | 1.20 | 0.01 | 0.00 | 0.00 | BC 243 |
| | | | | Min $M_T$ | 5.02 | 0.00 | 0.82 | -0.01 | 0.00 | 0.00 | BC 357 |
| | | | | Max $M_y$ | 2.77 | 0.00 | 1.20 | 0.00 | 0.00 | 0.00 | BC 268 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 72 | RC1 | | | Min $M_y$ | 2.78 | 0.00 | 1.20 | 0.00 | -0.00 | 0.00 | BC 176 |
| | | | | Max $M_z$ | -0.02 | 0.00 | 1.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.02 | 0.00 | 1.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 57 | 4300 | Max N | 5.06 | 0.00 | -0.82 | -0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min N | -3.81 | 0.00 | -1.20 | 0.01 | 0.00 | 0.00 | BC 207 |
| | | | | Max $V_y$ | -0.02 | 0.00 | -1.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.02 | 0.00 | -1.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -3.77 | 0.00 | -0.82 | 0.01 | 0.00 | 0.00 | BC 355 |
| | | | | Min $V_z$ | -0.02 | 0.00 | -1.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -3.80 | 0.00 | -1.20 | 0.01 | 0.00 | 0.00 | BC 243 |
| | | | | Min $M_T$ | 5.02 | 0.00 | -0.82 | -0.01 | 0.00 | 0.00 | BC 357 |
| | | | | Max $M_y$ | 2.77 | 0.00 | -1.20 | 0.00 | 0.00 | 0.00 | BC 268 |
| | | | | Min $M_y$ | 0.01 | 0.00 | -1.20 | 0.00 | -0.00 | 0.00 | BC 147 |
| | | | | Max $M_z$ | -0.02 | 0.00 | -1.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.02 | 0.00 | -1.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| 73 | RC1 | 35 | 0 | Max N | 22.31 | 0.00 | 0.33 | 0.28 | 0.00 | 0.00 | BC 241 |
| | | | | Min N | -21.92 | 0.00 | 0.23 | 0.12 | 0.00 | 0.00 | BC 358 |
| | | | | Max $V_y$ | 0.28 | 0.00 | 0.37 | 0.21 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.28 | 0.00 | 0.37 | 0.21 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.44 | 0.00 | 0.37 | 0.29 | 0.00 | 0.00 | BC 4 |
| | | | | Min $V_z$ | -21.91 | 0.00 | 0.23 | 0.12 | 0.00 | 0.00 | BC 354 |
| | | | | Max $M_T$ | 0.94 | 0.00 | 0.33 | 0.49 | 0.00 | 0.00 | BC 155 |
| | | | | Min $M_T$ | -1.01 | 0.00 | 0.23 | 0.09 | 0.00 | 0.00 | BC 356 |
| | | | | Max $M_y$ | 0.03 | 0.00 | 0.33 | 0.23 | 0.00 | 0.00 | BC 264 |
| | | | | Min $M_y$ | 0.34 | 0.00 | 0.33 | 0.23 | -0.00 | 0.00 | BC 268 |
| | | | | Max $M_z$ | 0.28 | 0.00 | 0.37 | 0.21 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.28 | 0.00 | 0.37 | 0.21 | 0.00 | 0.00 | BC 1 |
| | | 81 | 4300 | Max N | 22.31 | 0.00 | -0.33 | 0.28 | 0.00 | 0.00 | BC 241 |
| | | | | Min N | -21.92 | 0.00 | -0.23 | 0.12 | 0.00 | 0.00 | BC 358 |
| | | | | Max $V_y$ | 0.28 | 0.00 | -0.37 | 0.21 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.28 | 0.00 | -0.37 | 0.21 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -21.91 | 0.00 | -0.23 | 0.12 | 0.00 | 0.00 | BC 354 |
| | | | | Min $V_z$ | 0.44 | 0.00 | -0.37 | 0.29 | 0.00 | 0.00 | BC 4 |
| | | | | Max $M_T$ | 0.94 | 0.00 | -0.33 | 0.49 | 0.00 | 0.00 | BC 155 |
| | | | | Min $M_T$ | -1.01 | 0.00 | -0.23 | 0.09 | 0.00 | 0.00 | BC 356 |
| | | | | Max $M_y$ | 0.03 | 0.00 | -0.33 | 0.23 | 0.00 | 0.00 | BC 264 |
| | | | | Min $M_y$ | 0.34 | 0.00 | -0.33 | 0.23 | -0.00 | 0.00 | BC 268 |
| | | | | Max $M_z$ | 0.28 | 0.00 | -0.37 | 0.21 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.28 | 0.00 | -0.37 | 0.21 | 0.00 | 0.00 | BC 1 |
| 74 | RC1 | 89 | 0 | Max N | 10.64 | 0.00 | 0.98 | -0.00 | -0.97 | 0.00 | BC 359 |
| | | | | Min N | -39.11 | -0.00 | 1.78 | 0.00 | -3.13 | -0.00 | BC 241 |
| | | | | Max $V_y$ | 8.73 | 0.00 | 1.47 | -0.00 | -1.59 | 0.00 | BC 203 |
| | | | | Min $V_y$ | -36.71 | -0.00 | 1.31 | 0.00 | -2.57 | -0.00 | BC 429 |
| | | | | Max $V_z$ | -15.02 | 0.00 | 1.81 | -0.00 | -2.56 | 0.00 | BC 21 |
| | | | | Min $V_z$ | 5.07 | -0.00 | 0.83 | 0.00 | -0.25 | -0.00 | BC 360 |
| | | | | Max $M_T$ | -27.15 | -0.00 | 1.18 | 0.00 | -1.97 | -0.00 | BC 393 |
| | | | | Min $M_T$ | 2.36 | 0.00 | 1.09 | -0.00 | -1.53 | 0.00 | BC 475 |
| | | | | Max $M_y$ | 5.07 | -0.00 | 0.83 | 0.00 | -0.25 | -0.00 | BC 360 |
| | | | | Min $M_y$ | -39.11 | -0.00 | 1.78 | 0.00 | -3.13 | -0.00 | BC 241 |
| | | | | Max $M_z$ | 8.73 | 0.00 | 1.47 | -0.00 | -1.59 | 0.00 | BC 203 |
| | | | | Min $M_z$ | -36.71 | -0.00 | 1.31 | 0.00 | -2.57 | -0.00 | BC 429 |
| | | 17 | 4865 | Max N | 10.64 | 0.00 | -0.58 | -0.00 | 0.00 | 0.00 | BC 359 |
| | | | | Min N | -39.11 | -0.00 | -0.50 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Max $V_y$ | 8.73 | 0.00 | -0.82 | -0.00 | 0.00 | 0.00 | BC 203 |
| | | | | Min $V_y$ | -36.71 | -0.00 | -0.25 | 0.00 | 0.00 | 0.00 | BC 429 |
| | | | | Max $V_z$ | -36.99 | -0.00 | -0.25 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min $V_z$ | 5.14 | -0.00 | -0.98 | 0.00 | 0.00 | 0.00 | BC 168 |
| | | | | Max $M_T$ | -27.15 | -0.00 | -0.37 | 0.00 | 0.00 | 0.00 | BC 393 |
| | | | | Min $M_T$ | 2.36 | 0.00 | -0.46 | -0.00 | 0.00 | 0.00 | BC 475 |
| | | | | Max $M_y$ | -8.07 | -0.00 | -0.69 | 0.00 | 0.00 | 0.00 | BC 190 |
| | | | | Min $M_y$ | -12.54 | -0.00 | -0.41 | -0.00 | -0.00 | 0.00 | BC 53 |
| | | | | Max $M_z$ | -5.93 | 0.00 | -0.89 | -0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -5.93 | 0.00 | -0.89 | -0.00 | -0.00 | 0.00 | BC 1 |
| 75 | RC1 | 81 | 0 | Max N | 27.19 | 0.00 | 0.24 | 0.00 | 0.00 | 0.00 | BC 445 |
| | | | | Min N | -26.52 | 0.00 | 0.35 | 0.01 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_y$ | -11.30 | 0.00 | 0.39 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -11.30 | 0.00 | 0.39 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -10.70 | 0.00 | 0.39 | 0.00 | 0.00 | 0.00 | BC 31 |
| | | | | Min $V_z$ | -23.25 | 0.00 | 0.24 | 0.01 | -0.00 | 0.00 | BC 332 |
| | | | | Max $M_T$ | -26.47 | 0.00 | 0.35 | 0.01 | 0.00 | 0.00 | BC 138 |
| | | | | Min $M_T$ | -12.79 | 0.00 | 0.24 | 0.00 | 0.00 | 0.00 | BC 356 |
| | | | | Max $M_y$ | -19.85 | 0.00 | 0.24 | 0.01 | 0.00 | 0.00 | BC 378 |
| | | | | Min $M_y$ | -26.39 | 0.00 | 0.35 | 0.01 | -0.00 | 0.00 | BC 148 |
| | | | | Max $M_z$ | -11.30 | 0.00 | 0.39 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -11.30 | 0.00 | 0.39 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 82 | 4500 | Max N | 27.19 | 0.00 | -0.24 | 0.00 | 0.00 | 0.00 | BC 445 |
| | | | | Min N | -26.52 | 0.00 | -0.35 | 0.01 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_y$ | -11.30 | 0.00 | -0.39 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -11.30 | 0.00 | -0.39 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -23.25 | 0.00 | -0.24 | 0.01 | -0.00 | 0.00 | BC 332 |
| | | | | Min $V_z$ | -10.70 | 0.00 | -0.39 | 0.00 | 0.00 | 0.00 | BC 31 |
| | | | | Max $M_T$ | -26.47 | 0.00 | -0.35 | 0.01 | 0.00 | 0.00 | BC 138 |
| | | | | Min $M_T$ | -12.79 | 0.00 | -0.24 | 0.00 | 0.00 | 0.00 | BC 356 |
| | | | | Max $M_y$ | -19.85 | 0.00 | -0.24 | 0.01 | 0.00 | 0.00 | BC 378 |
| | | | | Min $M_y$ | -26.39 | 0.00 | -0.35 | 0.01 | -0.00 | 0.00 | BC 148 |
| | | | | Max $M_z$ | -11.30 | 0.00 | -0.39 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -11.30 | 0.00 | -0.39 | 0.00 | 0.00 | 0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 76 | RC1 | 93 | 0 | Max N | 8.32 | 0.00 | 0.69 | -0.01 | -0.71 | 0.00 | BC 359 |
| | | | | Min N | -37.50 | -0.00 | 1.16 | 0.01 | -1.29 | -0.00 | BC 248 |
| | | | | Max $V_y$ | -3.79 | 0.00 | 1.16 | -0.01 | -1.27 | 0.00 | BC 271 |
| | | | | Min $V_y$ | -23.01 | -0.00 | 0.63 | 0.01 | -0.61 | -0.00 | BC 357 |
| | | | | Max $V_z$ | -17.27 | 0.00 | 1.31 | 0.00 | -1.44 | 0.00 | BC 20 |
| | | | | Min $V_z$ | -23.34 | -0.00 | 0.63 | 0.01 | -0.61 | -0.00 | BC 417 |
| | | | | Max $M_T$ | -30.49 | -0.00 | 0.76 | 0.01 | -0.81 | -0.00 | BC 433 |
| | | | | Min $M_T$ | 5.97 | 0.00 | 1.03 | -0.01 | -1.06 | 0.00 | BC 167 |
| | | | | Max $M_y$ | -23.34 | -0.00 | 0.63 | 0.01 | -0.61 | -0.00 | BC 417 |
| | | | | Min $M_y$ | -17.27 | 0.00 | 1.31 | 0.00 | -1.44 | 0.00 | BC 20 |
| | | | | Max $M_z$ | -3.79 | 0.00 | 1.16 | -0.01 | -1.27 | 0.00 | BC 271 |
| | | | | Min $M_z$ | -23.01 | -0.00 | 0.63 | 0.01 | -0.61 | -0.00 | BC 357 |
| | | 80 | 1665 | Max N | 8.32 | 0.00 | 0.16 | -0.01 | 0.00 | 0.00 | BC 359 |
| | | | | Min N | -37.50 | -0.00 | 0.38 | 0.01 | 0.00 | 0.00 | BC 248 |
| | | | | Max $V_y$ | -3.79 | 0.00 | 0.37 | -0.01 | 0.00 | 0.00 | BC 271 |
| | | | | Min $V_y$ | -23.01 | -0.00 | 0.10 | 0.01 | 0.00 | 0.00 | BC 357 |
| | | | | Max $V_z$ | -17.95 | 0.00 | 0.47 | 0.00 | -0.00 | 0.00 | BC 147 |
| | | | | Min $V_z$ | -23.34 | -0.00 | 0.10 | 0.01 | -0.00 | 0.00 | BC 417 |
| | | | | Max $M_T$ | -30.49 | -0.00 | 0.22 | 0.01 | 0.00 | 0.00 | BC 433 |
| | | | | Min $M_T$ | 5.97 | 0.00 | 0.25 | -0.01 | 0.00 | 0.00 | BC 167 |
| | | | | Max $M_y$ | -37.29 | -0.00 | 0.41 | 0.01 | 0.00 | 0.00 | BC 264 |
| | | | | Min $M_y$ | -3.79 | -0.00 | 0.28 | 0.01 | -0.00 | 0.00 | BC 198 |
| | | | | Max $M_z$ | -8.20 | 0.00 | 0.31 | -0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -8.20 | 0.00 | 0.31 | -0.00 | -0.00 | 0.00 | BC 1 |
| 77 | RC1 | 82 | 0 | Max N | 25.19 | 0.00 | 0.35 | -0.28 | 0.00 | 0.00 | BC 241 |
| | | | | Min N | -9.51 | 0.00 | 0.35 | -0.28 | 0.00 | 0.00 | BC 263 |
| | | | | Max $V_y$ | 0.40 | 0.00 | 0.39 | -0.22 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.40 | 0.00 | 0.39 | -0.22 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 2.57 | 0.00 | 0.39 | -0.31 | -0.00 | 0.00 | BC 27 |
| | | | | Min $V_z$ | -7.94 | 0.00 | 0.24 | -0.21 | 0.00 | 0.00 | BC 367 |
| | | | | Max $M_T$ | 23.21 | 0.00 | 0.24 | -0.13 | 0.00 | 0.00 | BC 389 |
| | | | | Min $M_T$ | 3.91 | 0.00 | 0.35 | -0.50 | 0.00 | 0.00 | BC 154 |
| | | | | Max $M_y$ | 1.05 | 0.00 | 0.24 | -0.21 | 0.00 | 0.00 | BC 378 |
| | | | | Min $M_y$ | 2.40 | 0.00 | 0.35 | -0.28 | -0.00 | 0.00 | BC 91 |
| | | | | Max $M_z$ | 0.40 | 0.00 | 0.39 | -0.22 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.40 | 0.00 | 0.39 | -0.22 | 0.00 | 0.00 | BC 1 |
| | | 83 | 4500 | Max N | 25.19 | 0.00 | -0.35 | -0.28 | 0.00 | 0.00 | BC 241 |
| | | | | Min N | -9.51 | 0.00 | -0.35 | -0.28 | 0.00 | 0.00 | BC 263 |
| | | | | Max $V_y$ | 0.40 | 0.00 | -0.39 | -0.22 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.40 | 0.00 | -0.39 | -0.22 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -7.94 | 0.00 | -0.24 | -0.21 | 0.00 | 0.00 | BC 367 |
| | | | | Min $V_z$ | 2.57 | 0.00 | -0.39 | -0.31 | -0.00 | 0.00 | BC 27 |
| | | | | Max $M_T$ | 23.21 | 0.00 | -0.24 | -0.13 | 0.00 | 0.00 | BC 389 |
| | | | | Min $M_T$ | 3.91 | 0.00 | -0.35 | -0.50 | 0.00 | 0.00 | BC 154 |
| | | | | Max $M_y$ | 1.05 | 0.00 | -0.24 | -0.21 | 0.00 | 0.00 | BC 378 |
| | | | | Min $M_y$ | 2.40 | 0.00 | -0.35 | -0.28 | -0.00 | 0.00 | BC 91 |
| | | | | Max $M_z$ | 0.40 | 0.00 | -0.39 | -0.22 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.40 | 0.00 | -0.39 | -0.22 | 0.00 | 0.00 | BC 1 |
| 78 | RC1 | 96 | 0 | Max N | 18.02 | -0.00 | 1.91 | 0.00 | -3.72 | -0.00 | BC 268 |
| | | | | Min N | -39.13 | -0.00 | 2.31 | 0.00 | -5.68 | -0.00 | BC 165 |
| | | | | Max $V_y$ | 10.91 | 0.00 | 1.54 | 0.00 | -3.71 | 0.00 | BC 446 |
| | | | | Min $V_y$ | -33.35 | -0.00 | 2.70 | 0.00 | -7.58 | -0.00 | BC 205 |
| | | | | Max $V_z$ | -31.72 | -0.00 | 2.74 | 0.00 | -7.77 | -0.00 | BC 269 |
| | | | | Min $V_z$ | 11.95 | -0.00 | 0.86 | 0.00 | -0.39 | -0.00 | BC 360 |
| | | | | Max $M_T$ | -33.78 | -0.00 | 2.03 | 0.00 | -6.08 | -0.00 | BC 413 |
| | | | | Min $M_T$ | 10.06 | -0.00 | 1.25 | -0.00 | -2.31 | -0.00 | BC 451 |
| | | | | Max $M_y$ | 11.95 | -0.00 | 0.86 | 0.00 | -0.39 | -0.00 | BC 360 |
| | | | | Min $M_y$ | -31.72 | -0.00 | 2.74 | 0.00 | -7.77 | -0.00 | BC 269 |
| | | | | Max $M_z$ | 10.91 | 0.00 | 1.54 | 0.00 | -3.71 | 0.00 | BC 446 |
| | | | | Min $M_z$ | -33.35 | -0.00 | 2.70 | 0.00 | -7.58 | -0.00 | BC 205 |
| | | 77 | 4865 | Max N | 18.02 | -0.00 | -0.38 | 0.00 | 0.00 | 0.00 | BC 268 |
| | | | | Min N | -39.13 | -0.00 | 0.03 | 0.00 | 0.00 | 0.00 | BC 165 |
| | | | | Max $V_y$ | 10.91 | 0.00 | -0.02 | 0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Min $V_y$ | -33.35 | -0.00 | 0.42 | 0.00 | 0.00 | 0.00 | BC 205 |
| | | | | Max $V_z$ | -31.08 | -0.00 | 0.57 | 0.00 | 0.00 | 0.00 | BC 461 |
| | | | | Min $V_z$ | 13.56 | -0.00 | -0.81 | 0.00 | 0.00 | 0.00 | BC 168 |
| | | | | Max $M_T$ | -33.78 | -0.00 | 0.47 | 0.00 | 0.00 | 0.00 | BC 413 |
| | | | | Min $M_T$ | 10.06 | -0.00 | -0.30 | -0.00 | 0.00 | 0.00 | BC 451 |
| | | | | Max $M_y$ | 2.79 | -0.00 | 0.12 | 0.00 | 0.00 | 0.00 | BC 44 |
| | | | | Min $M_y$ | 6.03 | 0.00 | -0.44 | 0.00 | -0.00 | 0.00 | BC 162 |
| | | | | Max $M_z$ | -2.19 | -0.00 | -0.40 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -2.19 | -0.00 | -0.40 | 0.00 | 0.00 | 0.00 | BC 1 |
| 79 | RC1 | 83 | 0 | Max N | 25.07 | 0.00 | 0.24 | 0.01 | 0.00 | 0.00 | BC 433 |
| | | | | Min N | -19.99 | 0.00 | 0.35 | 0.00 | 0.00 | 0.00 | BC 167 |
| | | | | Max $V_y$ | -1.89 | 0.00 | 0.39 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -1.89 | 0.00 | 0.39 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.37 | 0.00 | 0.39 | 0.01 | -0.00 | 0.00 | BC 27 |
| | | | | Min $V_z$ | -19.94 | 0.00 | 0.24 | 0.00 | -0.00 | 0.00 | BC 359 |
| | | | | Max $M_T$ | -18.49 | 0.00 | 0.24 | 0.02 | -0.00 | 0.00 | BC 459 |
| | | | | Min $M_T$ | -1.43 | 0.00 | 0.24 | -0.01 | 0.00 | 0.00 | BC 390 |
| | | | | Max $M_y$ | 0.58 | 0.00 | 0.24 | -0.00 | 0.00 | 0.00 | BC 406 |
| | | | | Min $M_y$ | -19.47 | 0.00 | 0.35 | 0.00 | -0.00 | 0.00 | BC 259 |
| | | | | Max $M_z$ | -1.89 | 0.00 | 0.39 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -1.89 | 0.00 | 0.39 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 84 | 4500 | Max N | 25.07 | 0.00 | -0.24 | 0.01 | 0.00 | 0.00 | BC 433 |
| | | | | Min N | -19.99 | 0.00 | -0.35 | 0.00 | 0.00 | 0.00 | BC 167 |
| | | | | Max $V_y$ | -1.89 | 0.00 | -0.39 | 0.00 | 0.00 | 0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 79 | RC1 | | | Min $V_y$ | -1.89 | 0.00 | -0.39 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -19.94 | 0.00 | -0.24 | 0.00 | -0.00 | 0.00 | BC 359 |
| | | | | Min $V_z$ | -0.37 | 0.00 | -0.39 | 0.01 | -0.00 | 0.00 | BC 27 |
| | | | | Max $M_T$ | -18.49 | 0.00 | -0.24 | 0.02 | -0.00 | 0.00 | BC 459 |
| | | | | Min $M_T$ | -1.43 | 0.00 | -0.24 | -0.01 | 0.00 | 0.00 | BC 390 |
| | | | | Max $M_y$ | 0.58 | 0.00 | -0.24 | -0.00 | 0.00 | 0.00 | BC 406 |
| | | | | Min $M_y$ | -19.47 | 0.00 | -0.35 | 0.00 | -0.00 | 0.00 | BC 259 |
| | | | | Max $M_z$ | -1.89 | 0.00 | -0.39 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -1.89 | 0.00 | -0.39 | 0.00 | 0.00 | 0.00 | BC 1 |
| 80 | RC1 | 17 | 0 | Max N | -16.34 | 6.32 | 6.79 | 0.00 | -7.03 | 4.78 | BC 447 |
| | | | Links | Min N | -46.20 | -0.03 | 0.62 | -0.00 | -1.99 | -0.11 | BC 138 |
| | | | | Max $V_y$ | -16.39 | 6.34 | 6.37 | 0.00 | -5.61 | 4.85 | BC 451 |
| | | | | Min $V_y$ | -24.15 | -9.00 | -1.96 | -0.00 | -4.15 | -7.47 | BC 217 |
| | | | | Max $V_z$ | -29.83 | 6.30 | 6.99 | 0.00 | -7.70 | 4.71 | BC 243 |
| | | | | Min $V_z$ | -16.51 | -8.99 | -2.58 | -0.00 | -2.06 | -7.46 | BC 357 |
| | | | | Max $M_T$ | -24.09 | 6.32 | 6.50 | 0.00 | -6.04 | 4.79 | BC 231 |
| | | | | Min $M_T$ | -29.93 | -8.98 | -1.81 | -0.00 | -4.66 | -7.41 | BC 269 |
| | | | | Max $M_y$ | -26.98 | -5.05 | 2.44 | -0.00 | 0.61 | -4.25 | BC 360 |
| | | | | Min $M_y$ | -29.83 | 6.30 | 6.99 | 0.00 | -7.70 | 4.71 | BC 243 |
| | | | | Max $M_z$ | -16.39 | 6.34 | 6.37 | 0.00 | -5.61 | 4.85 | BC 451 |
| | | | | Min $M_z$ | -24.15 | -9.00 | -1.96 | -0.00 | -4.15 | -7.47 | BC 217 |
| | | | 0 | Max N | -16.34 | 6.32 | 6.79 | 0.00 | -7.03 | 4.78 | BC 447 |
| | | | Rechts | Min N | -46.20 | -0.03 | 0.62 | -0.00 | -1.99 | -0.11 | BC 138 |
| | | | | Max $V_y$ | -16.39 | 6.34 | 6.37 | 0.00 | -5.61 | 4.85 | BC 451 |
| | | | | Min $V_y$ | -24.15 | -9.00 | -1.96 | -0.00 | -4.15 | -7.47 | BC 217 |
| | | | | Max $V_z$ | -29.83 | 6.30 | 6.99 | 0.00 | -7.70 | 4.71 | BC 243 |
| | | | | Min $V_z$ | -16.51 | -8.99 | -2.58 | -0.00 | -2.06 | -7.46 | BC 357 |
| | | | | Max $M_T$ | -24.09 | 6.32 | 6.50 | 0.00 | -6.04 | 4.79 | BC 231 |
| | | | | Min $M_T$ | -29.93 | -8.98 | -1.81 | -0.00 | -4.66 | -7.41 | BC 269 |
| | | | | Max $M_y$ | -26.98 | -5.05 | 2.44 | -0.00 | 0.61 | -4.25 | BC 360 |
| | | | | Min $M_y$ | -29.83 | 6.30 | 6.99 | 0.00 | -7.70 | 4.71 | BC 243 |
| | | | | Max $M_z$ | -16.39 | 6.34 | 6.37 | 0.00 | -5.61 | 4.85 | BC 451 |
| | | | | Min $M_z$ | -24.15 | -9.00 | -1.96 | -0.00 | -4.15 | -7.47 | BC 217 |
| | | | 3505 | Max N | -8.35 | -3.80 | -2.96 | 0.00 | -0.32 | 0.35 | BC 447 |
| | | | Links | Min N | -34.49 | -0.03 | 0.62 | -0.00 | 0.20 | 0.00 | BC 138 |
| | | | | Max $V_y$ | -14.24 | 5.03 | 4.63 | -0.00 | 0.53 | -0.47 | BC 433 |
| | | | | Min $V_y$ | -18.13 | -3.83 | -2.84 | 0.00 | -0.27 | 0.36 | BC 207 |
| | | | | Max $V_z$ | -18.21 | 5.02 | 4.79 | -0.00 | 0.56 | -0.47 | BC 241 |
| | | | | Min $V_z$ | -8.41 | -3.79 | -3.44 | 0.00 | -0.36 | 0.35 | BC 359 |
| | | | | Max $M_T$ | -12.38 | -3.79 | -3.24 | 0.00 | -0.33 | 0.35 | BC 231 |
| | | | | Min $M_T$ | -18.21 | 5.02 | 4.79 | -0.00 | 0.56 | -0.47 | BC 269 |
| | | | | Max $M_y$ | -19.02 | 2.77 | -1.67 | -0.00 | 1.95 | -0.25 | BC 356 |
| | | | | Min $M_y$ | -8.41 | -3.79 | -3.44 | 0.00 | -0.36 | 0.35 | BC 359 |
| | | | | Max $M_z$ | -18.13 | -3.83 | -2.84 | 0.00 | -0.27 | 0.36 | BC 207 |
| | | | | Min $M_z$ | -14.24 | 5.03 | 4.63 | -0.00 | 0.53 | -0.47 | BC 433 |
| | | 57 | 3505 | Max N | -8.35 | -3.80 | -2.96 | 0.00 | -0.32 | 0.35 | BC 447 |
| | | | Rechts | Min N | -34.49 | -0.03 | 0.62 | -0.00 | 0.20 | 0.00 | BC 138 |
| | | | | Max $V_y$ | -14.24 | 5.03 | 4.63 | -0.00 | 0.53 | -0.47 | BC 433 |
| | | | | Min $V_y$ | -18.13 | -3.83 | -2.84 | 0.00 | -0.27 | 0.36 | BC 207 |
| | | | | Max $V_z$ | -18.21 | 5.02 | 4.79 | -0.00 | 0.56 | -0.47 | BC 241 |
| | | | | Min $V_z$ | -8.41 | -3.79 | -3.44 | 0.00 | -0.36 | 0.35 | BC 359 |
| | | | | Max $M_T$ | -12.38 | -3.79 | -3.24 | 0.00 | -0.33 | 0.35 | BC 231 |
| | | | | Min $M_T$ | -18.21 | 5.02 | 4.79 | -0.00 | 0.56 | -0.47 | BC 269 |
| | | | | Max $M_y$ | -19.02 | 2.77 | -1.67 | -0.00 | 1.95 | -0.25 | BC 356 |
| | | | | Min $M_y$ | -8.41 | -3.79 | -3.44 | 0.00 | -0.36 | 0.35 | BC 359 |
| | | | | Max $M_z$ | -18.13 | -3.83 | -2.84 | 0.00 | -0.27 | 0.36 | BC 207 |
| | | | | Min $M_z$ | -14.24 | 5.03 | 4.63 | -0.00 | 0.53 | -0.47 | BC 433 |
| 81 | RC1 | 84 | 0 | Max N | 21.89 | 0.00 | 0.23 | 0.01 | 0.00 | 0.00 | BC 433 |
| | | | | Min N | -22.60 | 0.00 | 0.33 | 0.02 | -0.00 | 0.00 | BC 167 |
| | | | | Max $V_y$ | -0.75 | 0.00 | 0.37 | 0.03 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.75 | 0.00 | 0.37 | 0.03 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.02 | 0.00 | 0.37 | 0.02 | -0.00 | 0.00 | BC 16 |
| | | | | Min $V_z$ | -22.31 | 0.00 | 0.23 | 0.01 | 0.00 | 0.00 | BC 355 |
| | | | | Max $M_T$ | -0.35 | 0.00 | 0.33 | 0.04 | 0.00 | 0.00 | BC 160 |
| | | | | Min $M_T$ | 21.89 | 0.00 | 0.23 | 0.01 | 0.00 | 0.00 | BC 369 |
| | | | | Max $M_y$ | 0.07 | 0.00 | 0.33 | 0.04 | 0.00 | 0.00 | BC 172 |
| | | | | Min $M_y$ | 8.80 | 0.00 | 0.33 | 0.03 | -0.00 | 0.00 | BC 278 |
| | | | | Max $M_z$ | -0.75 | 0.00 | 0.37 | 0.03 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.75 | 0.00 | 0.37 | 0.03 | 0.00 | 0.00 | BC 1 |
| | | 41 | 4300 | Max N | 21.89 | 0.00 | -0.23 | 0.01 | 0.00 | 0.00 | BC 433 |
| | | | | Min N | -22.60 | 0.00 | -0.33 | 0.02 | -0.00 | 0.00 | BC 167 |
| | | | | Max $V_y$ | -0.75 | 0.00 | -0.37 | 0.03 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.75 | 0.00 | -0.37 | 0.03 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -22.31 | 0.00 | -0.23 | 0.01 | 0.00 | 0.00 | BC 355 |
| | | | | Min $V_z$ | 0.02 | 0.00 | -0.37 | 0.02 | -0.00 | 0.00 | BC 16 |
| | | | | Max $M_T$ | -0.35 | 0.00 | -0.33 | 0.04 | 0.00 | 0.00 | BC 160 |
| | | | | Min $M_T$ | 21.89 | 0.00 | -0.23 | 0.01 | 0.00 | 0.00 | BC 369 |
| | | | | Max $M_y$ | 0.07 | 0.00 | -0.33 | 0.04 | 0.00 | 0.00 | BC 172 |
| | | | | Min $M_y$ | 8.77 | 0.00 | -0.33 | 0.03 | -0.00 | 0.00 | BC 190 |
| | | | | Max $M_z$ | -0.75 | 0.00 | -0.37 | 0.03 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.75 | 0.00 | -0.37 | 0.03 | 0.00 | 0.00 | BC 1 |
| 82 | RC1 | 39 | 0 | Max N | 22.59 | 0.00 | 0.33 | -0.27 | 0.00 | 0.00 | BC 264 |
| | | | | Min N | -22.22 | 0.00 | 0.23 | -0.20 | 0.00 | 0.00 | BC 434 |
| | | | | Max $V_y$ | 0.36 | 0.00 | 0.37 | -0.20 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.36 | 0.00 | 0.37 | -0.20 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.41 | 0.00 | 0.37 | -0.28 | 0.00 | 0.00 | BC 4 |
| | | | | Min $V_z$ | -22.17 | 0.00 | 0.23 | -0.12 | 0.00 | 0.00 | BC 362 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 82 | RC1 | | | Max $M_T$ | 0.04 | 0.00 | 0.23 | -0.08 | 0.00 | 0.00 | BC 445 |
| | | | | Min $M_T$ | 0.52 | 0.00 | 0.33 | -0.47 | 0.00 | 0.00 | BC 131 |
| | | | | Max $M_y$ | 0.41 | 0.00 | 0.33 | -0.39 | 0.00 | 0.00 | BC 150 |
| | | | | Min $M_y$ | 0.39 | 0.00 | 0.23 | -0.08 | -0.00 | 0.00 | BC 381 |
| | | | | Max $M_z$ | 0.36 | 0.00 | 0.37 | -0.20 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.36 | 0.00 | 0.37 | -0.20 | 0.00 | 0.00 | BC 1 |
| | | 85 | 4300 | Max N | 22.59 | 0.00 | -0.33 | -0.27 | 0.00 | 0.00 | BC 264 |
| | | | | Min N | -22.22 | 0.00 | -0.23 | -0.20 | 0.00 | 0.00 | BC 434 |
| | | | | Max $V_y$ | 0.36 | 0.00 | -0.37 | -0.20 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.36 | 0.00 | -0.37 | -0.20 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -22.17 | 0.00 | -0.23 | -0.12 | 0.00 | 0.00 | BC 362 |
| | | | | Min $V_z$ | 0.41 | 0.00 | -0.37 | -0.28 | 0.00 | 0.00 | BC 4 |
| | | | | Max $M_T$ | 0.04 | 0.00 | -0.23 | -0.08 | 0.00 | 0.00 | BC 445 |
| | | | | Min $M_T$ | 0.52 | 0.00 | -0.33 | -0.47 | 0.00 | 0.00 | BC 131 |
| | | | | Max $M_y$ | 0.41 | 0.00 | -0.33 | -0.39 | 0.00 | 0.00 | BC 150 |
| | | | | Min $M_y$ | 0.39 | 0.00 | -0.23 | -0.08 | -0.00 | 0.00 | BC 381 |
| | | | | Max $M_z$ | 0.36 | 0.00 | -0.37 | -0.20 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.36 | 0.00 | -0.37 | -0.20 | 0.00 | 0.00 | BC 1 |
| 83 | RC1 | 85 | 0 | Max N | 49.36 | -1.13 | 36.35 | -0.40 | 502.29 | -4.51 | BC 235 |
| | | | | Min N | -19.96 | 0.71 | 16.77 | -0.01 | 241.68 | 1.48 | BC 408 |
| | | | | Max $V_y$ | -19.96 | 0.71 | 16.77 | -0.01 | 241.68 | 1.48 | BC 408 |
| | | | | Min $V_y$ | 0.41 | -1.83 | 69.78 | -0.64 | 914.51 | -6.81 | BC 138 |
| | | | | Max $V_z$ | -0.97 | -1.81 | 69.80 | -0.63 | 914.26 | -6.73 | BC 139 |
| | | | | Min $V_z$ | 41.10 | -0.72 | 16.73 | -0.25 | 239.54 | -3.17 | BC 363 |
| | | | | Max $M_T$ | -14.70 | -0.54 | 18.19 | 0.05 | 230.60 | -2.22 | BC 469 |
| | | | | Min $M_T$ | 0.41 | -1.83 | 69.78 | -0.64 | 914.51 | -6.81 | BC 138 |
| | | | | Max $M_y$ | 0.94 | -1.82 | 69.77 | -0.64 | 914.61 | -6.78 | BC 149 |
| | | | | Min $M_y$ | -14.76 | -0.54 | 18.19 | 0.05 | 230.58 | -2.22 | BC 409 |
| | | | | Max $M_z$ | -19.96 | 0.71 | 16.77 | -0.01 | 241.68 | 1.48 | BC 408 |
| | | | | Min $M_z$ | 0.41 | -1.83 | 69.78 | -0.64 | 914.51 | -6.81 | BC 138 |
| | | 155 | 3256 | Max N | 48.66 | -1.13 | -0.30 | -0.40 | 560.96 | -0.82 | BC 235 |
| | | | | Min N | -20.28 | 0.71 | -0.17 | -0.01 | 268.70 | -0.83 | BC 408 |
| | | | | Max $V_y$ | -20.28 | 0.71 | -0.17 | -0.01 | 268.70 | -0.83 | BC 408 |
| | | | | Min $V_y$ | -0.91 | -1.83 | 0.06 | -0.64 | 1028.19 | -0.84 | BC 138 |
| | | | | Max $V_z$ | -14.87 | -0.75 | 1.52 | -0.03 | 385.12 | -0.60 | BC 221 |
| | | | | Min $V_z$ | 45.40 | -0.95 | -0.50 | -0.34 | 436.89 | -0.84 | BC 427 |
| | | | | Max $M_T$ | -15.02 | -0.54 | 1.26 | 0.05 | 262.27 | -0.47 | BC 469 |
| | | | | Min $M_T$ | -0.91 | -1.83 | 0.06 | -0.64 | 1028.19 | -0.84 | BC 138 |
| | | | | Max $M_y$ | -0.38 | -1.82 | 0.04 | -0.64 | 1028.25 | -0.84 | BC 149 |
| | | | | Min $M_y$ | -15.08 | -0.54 | 1.26 | 0.05 | 262.25 | -0.47 | BC 409 |
| | | | | Max $M_z$ | -16.93 | -0.57 | 0.90 | -0.19 | 558.43 | 0.74 | BC 242 |
| | | | | Min $M_z$ | -17.84 | 0.13 | -0.12 | -0.20 | 560.60 | -1.13 | BC 184 |
| 84 | RC1 | 85 | 0 | Max N | 28.87 | 0.00 | 0.24 | -0.00 | 0.00 | 0.00 | BC 408 |
| | | | | Min N | -27.23 | 0.00 | 0.35 | -0.01 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_y$ | -11.85 | 0.00 | 0.39 | -0.01 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -11.85 | 0.00 | 0.39 | -0.01 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -11.21 | 0.00 | 0.39 | -0.01 | 0.00 | 0.00 | BC 9 |
| | | | | Min $V_z$ | -23.96 | 0.00 | 0.24 | -0.01 | 0.00 | 0.00 | BC 323 |
| | | | | Max $M_T$ | 28.47 | 0.00 | 0.24 | -0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Min $M_T$ | -26.83 | 0.00 | 0.35 | -0.01 | 0.00 | 0.00 | BC 140 |
| | | | | Max $M_y$ | -20.27 | 0.00 | 0.35 | -0.01 | 0.00 | 0.00 | BC 162 |
| | | | | Min $M_y$ | -12.21 | 0.00 | 0.24 | -0.00 | -0.00 | 0.00 | BC 381 |
| | | | | Max $M_z$ | -11.85 | 0.00 | 0.39 | -0.01 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -11.85 | 0.00 | 0.39 | -0.01 | 0.00 | 0.00 | BC 1 |
| | | 86 | 4500 | Max N | 28.87 | 0.00 | -0.24 | -0.00 | 0.00 | 0.00 | BC 408 |
| | | | | Min N | -27.23 | 0.00 | -0.35 | -0.01 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_y$ | -11.85 | 0.00 | -0.39 | -0.01 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -11.85 | 0.00 | -0.39 | -0.01 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -23.96 | 0.00 | -0.24 | -0.01 | 0.00 | 0.00 | BC 323 |
| | | | | Min $V_z$ | -11.21 | 0.00 | -0.39 | -0.01 | 0.00 | 0.00 | BC 9 |
| | | | | Max $M_T$ | 28.47 | 0.00 | -0.24 | -0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Min $M_T$ | -26.83 | 0.00 | -0.35 | -0.01 | 0.00 | 0.00 | BC 140 |
| | | | | Max $M_y$ | -20.27 | 0.00 | -0.35 | -0.01 | 0.00 | 0.00 | BC 162 |
| | | | | Min $M_y$ | -12.21 | 0.00 | -0.24 | -0.00 | -0.00 | 0.00 | BC 381 |
| | | | | Max $M_z$ | -11.85 | 0.00 | -0.39 | -0.01 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -11.85 | 0.00 | -0.39 | -0.01 | 0.00 | 0.00 | BC 1 |
| 85 | RC1 | 86 | 0 | Max N | 53.66 | 0.50 | 36.52 | 0.24 | 516.70 | 3.30 | BC 206 |
| | | | | Min N | -18.63 | 0.36 | 37.89 | 0.00 | 508.35 | 2.14 | BC 235 |
| | | | | Max $V_y$ | 3.47 | 0.87 | 70.71 | 0.39 | 937.71 | 5.40 | BC 149 |
| | | | | Min $V_y$ | -11.65 | -1.30 | 17.21 | 0.19 | 241.32 | -5.31 | BC 356 |
| | | | | Max $V_z$ | 3.56 | 0.87 | 70.71 | 0.39 | 937.70 | 5.38 | BC 146 |
| | | | | Min $V_z$ | 46.18 | 0.50 | 16.63 | 0.17 | 247.18 | 3.10 | BC 410 |
| | | | | Max $M_T$ | 4.93 | 0.84 | 70.68 | 0.39 | 937.88 | 5.32 | BC 148 |
| | | | | Min $M_T$ | -16.80 | 0.54 | 18.16 | -0.02 | 236.51 | 1.95 | BC 357 |
| | | | | Max $M_y$ | 5.22 | 0.84 | 70.68 | 0.39 | 937.89 | 5.30 | BC 140 |
| | | | | Min $M_y$ | -17.10 | 0.55 | 18.16 | -0.02 | 236.49 | 1.99 | BC 421 |
| | | | | Max $M_z$ | 3.47 | 0.87 | 70.71 | 0.39 | 937.71 | 5.40 | BC 149 |
| | | | | Min $M_z$ | -10.26 | -1.29 | 17.16 | 0.20 | 241.78 | -5.34 | BC 408 |
| | | 154 | 3256 | Max N | 52.96 | 0.50 | -0.77 | 0.24 | 574.90 | 1.67 | BC 206 |
| | | | | Min N | -19.34 | 0.36 | 0.61 | 0.00 | 571.02 | 0.99 | BC 235 |
| | | | | Max $V_y$ | 2.12 | 0.87 | -0.40 | 0.39 | 1052.16 | 2.56 | BC 149 |
| | | | | Min $V_y$ | -11.98 | -1.30 | 0.03 | 0.19 | 269.38 | -1.08 | BC 356 |
| | | | | Max $V_z$ | -17.20 | 0.67 | 1.12 | 0.03 | 393.34 | 0.42 | BC 169 |
| | | | | Min $V_z$ | 49.98 | 0.51 | -0.85 | 0.22 | 447.94 | 1.59 | BC 398 |
| | | | | Max $M_T$ | 3.59 | 0.84 | -0.43 | 0.39 | 1052.22 | 2.58 | BC 148 |
| | | | | Min $M_T$ | -17.12 | 0.54 | 0.97 | -0.02 | 267.66 | 0.18 | BC 357 |
| | | | | Max $M_y$ | 3.80 | 0.84 | -0.44 | 0.39 | 1052.22 | 2.57 | BC 155 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 85 | RC1 | | | Min $M_y$ | -17.36 | 0.56 | 0.97 | -0.02 | 267.63 | 0.20 | BC 449 |
| | | | | Max $M_z$ | 3.59 | 0.84 | -0.43 | 0.39 | 1052.22 | 2.58 | BC 148 |
| | | | | Min $M_z$ | -10.59 | -1.29 | -0.02 | 0.20 | 269.69 | -1.13 | BC 408 |
| 86 | RC1 | 86 | 0 | Max N | 34.49 | -0.03 | 2.03 | 0.02 | -0.00 | 0.00 | BC 204 |
| | | | | Min N | -9.19 | 0.01 | 2.03 | 0.01 | 0.00 | 0.00 | BC 247 |
| | | | | Max $V_y$ | 3.93 | 0.03 | 2.77 | 0.02 | 0.00 | 0.00 | BC 131 |
| | | | | Min $V_y$ | 32.02 | -0.04 | 1.20 | 0.01 | 0.00 | 0.00 | BC 448 |
| | | | | Max $V_z$ | 3.79 | 0.03 | 2.77 | 0.02 | 0.00 | 0.00 | BC 134 |
| | | | | Min $V_z$ | -1.89 | -0.03 | 1.20 | 0.01 | 0.00 | 0.00 | BC 470 |
| | | | | Max $M_T$ | 4.93 | 0.02 | 2.77 | 0.02 | 0.00 | 0.00 | BC 154 |
| | | | | Min $M_T$ | -0.48 | -0.01 | 1.20 | 0.01 | -0.00 | 0.00 | BC 361 |
| | | | | Max $M_y$ | -0.49 | -0.02 | 1.46 | 0.01 | 0.00 | 0.00 | BC 378 |
| | | | | Min $M_y$ | 0.34 | -0.01 | 1.20 | 0.01 | -0.00 | 0.00 | BC 381 |
| | | | | Max $M_z$ | -0.49 | -0.02 | 1.46 | 0.01 | 0.00 | 0.00 | BC 378 |
| | | | | Min $M_z$ | 1.54 | 0.01 | 1.99 | 0.01 | 0.00 | 0.00 | BC 1 |
| | | 102 | 4300 | Max N | 34.49 | -0.03 | -0.37 | 0.02 | 3.56 | 0.11 | BC 204 |
| | | | | Min N | -9.19 | 0.01 | -0.37 | 0.01 | 3.57 | -0.06 | BC 247 |
| | | | | Max $V_y$ | 3.93 | 0.03 | 0.37 | 0.02 | 6.75 | -0.11 | BC 131 |
| | | | | Min $V_y$ | 32.02 | -0.04 | -0.43 | 0.01 | 1.65 | 0.18 | BC 448 |
| | | | | Max $V_z$ | 3.18 | 0.02 | 0.57 | 0.02 | 5.98 | -0.10 | BC 326 |
| | | | | Min $V_z$ | 2.97 | 0.01 | -0.72 | 0.01 | 2.73 | -0.02 | BC 30 |
| | | | | Max $M_T$ | 4.93 | 0.02 | 0.37 | 0.02 | 6.75 | -0.10 | BC 154 |
| | | | | Min $M_T$ | -0.48 | -0.01 | -0.43 | 0.01 | 1.65 | 0.03 | BC 361 |
| | | | | Max $M_y$ | 3.79 | 0.03 | 0.37 | 0.02 | 6.75 | -0.11 | BC 134 |
| | | | | Min $M_y$ | -1.89 | -0.03 | -0.44 | 0.01 | 1.64 | 0.14 | BC 470 |
| | | | | Max $M_z$ | 32.02 | -0.04 | -0.43 | 0.01 | 1.65 | 0.18 | BC 448 |
| | | | | Min $M_z$ | 3.93 | 0.03 | 0.37 | 0.02 | 6.75 | -0.11 | BC 131 |
| 87 | RC1 | 68 | 0 | Max N | 30.32 | 0.00 | 1.25 | -0.00 | -0.00 | 0.00 | BC 164 |
| | | | | Min N | -21.21 | 0.00 | 1.25 | -0.00 | -0.00 | 0.00 | BC 243 |
| | | | | Max $V_y$ | -1.16 | 0.00 | 1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -1.16 | 0.00 | 1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -1.16 | 0.00 | 1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -21.11 | 0.00 | 0.86 | -0.00 | -0.00 | 0.00 | BC 435 |
| | | | | Max $M_T$ | -4.55 | 0.00 | 0.86 | 0.00 | 0.00 | 0.00 | BC 362 |
| | | | | Min $M_T$ | -8.06 | 0.00 | 1.25 | -0.01 | 0.00 | 0.00 | BC 269 |
| | | | | Max $M_y$ | -5.25 | 0.00 | 1.25 | -0.00 | 0.00 | 0.00 | BC 91 |
| | | | | Min $M_y$ | -18.42 | 0.00 | 1.25 | -0.00 | -0.00 | 0.00 | BC 219 |
| | | | | Max $M_z$ | -1.16 | 0.00 | 1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -1.16 | 0.00 | 1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | 67 | 4500 | Max N | 30.32 | 0.00 | -1.25 | -0.00 | -0.00 | 0.00 | BC 164 |
| | | | | Min N | -21.21 | 0.00 | -1.25 | -0.00 | -0.00 | 0.00 | BC 243 |
| | | | | Max $V_y$ | -1.16 | 0.00 | -1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -1.16 | 0.00 | -1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -21.11 | 0.00 | -0.86 | -0.00 | -0.00 | 0.00 | BC 435 |
| | | | | Min $V_z$ | -1.16 | 0.00 | -1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -4.55 | 0.00 | -0.86 | 0.00 | 0.00 | 0.00 | BC 362 |
| | | | | Min $M_T$ | -8.06 | 0.00 | -1.25 | -0.01 | 0.00 | 0.00 | BC 269 |
| | | | | Max $M_y$ | -5.25 | 0.00 | -1.25 | -0.00 | 0.00 | 0.00 | BC 91 |
| | | | | Min $M_y$ | -18.42 | 0.00 | -1.25 | -0.00 | -0.00 | 0.00 | BC 219 |
| | | | | Max $M_z$ | -1.16 | 0.00 | -1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -1.16 | 0.00 | -1.42 | -0.00 | 0.00 | 0.00 | BC 1 |
| 88 | RC1 | 67 | 0 | Max N | 16.63 | 0.00 | 1.20 | -0.00 | 0.00 | 0.00 | BC 172 |
| | | | | Min N | -19.60 | 0.00 | 0.82 | 0.00 | 0.00 | 0.00 | BC 435 |
| | | | | Max $V_y$ | -0.34 | 0.00 | 1.35 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.34 | 0.00 | 1.35 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.34 | 0.00 | 1.35 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -19.60 | 0.00 | 0.82 | 0.00 | 0.00 | 0.00 | BC 435 |
| | | | | Max $M_T$ | -10.99 | 0.00 | 1.20 | 0.00 | 0.00 | 0.00 | BC 269 |
| | | | | Min $M_T$ | 6.44 | 0.00 | 0.82 | -0.00 | 0.00 | 0.00 | BC 358 |
| | | | | Max $M_y$ | 16.63 | 0.00 | 1.20 | -0.00 | 0.00 | 0.00 | BC 172 |
| | | | | Min $M_y$ | -3.98 | 0.00 | 0.82 | 0.00 | -0.00 | 0.00 | BC 53 |
| | | | | Max $M_z$ | -0.34 | 0.00 | 1.35 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.34 | 0.00 | 1.35 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | 42 | 4300 | Max N | 16.63 | 0.00 | -1.20 | -0.00 | 0.00 | 0.00 | BC 172 |
| | | | | Min N | -19.60 | 0.00 | -0.82 | 0.00 | 0.00 | 0.00 | BC 435 |
| | | | | Max $V_y$ | -0.34 | 0.00 | -1.35 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.34 | 0.00 | -1.35 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -19.60 | 0.00 | -0.82 | 0.00 | 0.00 | 0.00 | BC 435 |
| | | | | Min $V_z$ | -0.34 | 0.00 | -1.35 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -10.99 | 0.00 | -1.20 | 0.00 | 0.00 | 0.00 | BC 269 |
| | | | | Min $M_T$ | 6.44 | 0.00 | -0.82 | -0.00 | 0.00 | 0.00 | BC 358 |
| | | | | Max $M_y$ | 16.63 | 0.00 | -1.20 | -0.00 | 0.00 | 0.00 | BC 172 |
| | | | | Min $M_y$ | -3.98 | 0.00 | -0.82 | 0.00 | -0.00 | 0.00 | BC 53 |
| | | | | Max $M_z$ | -0.34 | 0.00 | -1.35 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.34 | 0.00 | -1.35 | 0.00 | -0.00 | 0.00 | BC 1 |
| 89 | RC1 | 35 | 0 | Max N | 46.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 164 |
| | | | | Min N | -1.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 148 |
| | | | | Max $V_u$ | -0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 89 | RC1 | 27 | 3901 | Max N | 46.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 164 |
| | | | | Min N | -1.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 148 |
| | | | | Max $V_u$ | -0.28 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.28 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.28 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.28 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.28 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.28 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.28 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.28 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.28 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.28 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 90 | RC1 | 81 | 0 | Max N | 44.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min N | -1.93 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 200 |
| | | | | Max $V_u$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 27 | 3901 | Max N | 44.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min N | -1.92 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 200 |
| | | | | Max $V_u$ | -0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 91 | RC1 | 49 | 0 | Max N | 57.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 139 |
| | | | | Min N | -0.61 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 451 |
| | | | | Max $V_u$ | 22.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 22.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 22.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 22.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 22.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 22.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 22.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 22.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 22.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 22.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 23 | 3912 | Max N | 57.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 139 |
| | | | | Min N | -0.60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 451 |
| | | | | Max $V_u$ | 22.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 22.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 22.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 22.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 22.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 22.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 22.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 22.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 22.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 22.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 92 | RC1 | 51 | 0 | Max N | 55.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 134 |
| | | | | Min N | -0.69 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 410 |
| | | | | Max $V_u$ | 22.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 22.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 22.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 22.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 22.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 22.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 22.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 22.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 22.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 22.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 23 | 3912 | Max N | 55.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 134 |
| | | | | Min N | -0.68 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 410 |
| | | | | Max $V_u$ | 22.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 22.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 22.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 22.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 22.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 22.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 22.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 22.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 22.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 22.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 93 | RC1 | 82 | 0 | Max N | 18.23 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 165 |
| | | | | Min N | -1.59 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 268 |
| | | | | Max $V_u$ | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 93 | RC1 | | | Min $V_u$ | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 31 | 3957 | Max N | 18.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 165 |
| | | | | Min N | -1.58 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 268 |
| | | | | Max $V_u$ | -0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 94 | RC1 | 83 | 0 | Max N | 18.58 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 432 |
| | | | | Min N | -0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 173 |
| | | | | Max $V_u$ | -0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 31 | 3957 | Max N | 18.59 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 432 |
| | | | | Min N | -0.48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 173 |
| | | | | Max $V_u$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 95 | RC1 | 53 | 0 | Max N | 29.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Min N | -1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 411 |
| | | | | Max $V_u$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 26 | 3912 | Max N | 29.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Min N | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 411 |
| | | | | Max $V_u$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 96 | RC1 | 55 | 0 | Max N | 27.85 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 419 |
| | | | | Min N | -0.98 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 450 |
| | | | | Max $V_u$ | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 26 | 3912 | Max N | 27.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 419 |
| | | | | Min N | -0.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 450 |
| | | | | Max $V_u$ | -0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 96 | RC1 | | | Max $M_T$ | -0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 97 | RC1 | 84 | 0 | Max N | 51.73 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min N | -0.48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Max $V_u$ | 1.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 1.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 1.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 1.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 1.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 1.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 1.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 1.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 1.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 1.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 33 | 3901 | Max N | 51.74 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min N | -0.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Max $V_u$ | 1.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 1.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 1.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 1.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 1.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 1.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 1.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 1.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 1.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 1.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 98 | RC1 | 41 | 0 | Max N | 45.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 168 |
| | | | | Min N | -0.57 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 435 |
| | | | | Max $V_u$ | 1.39 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 1.39 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 1.39 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 1.39 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 1.39 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 1.39 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 1.39 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 1.39 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 1.39 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 1.39 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 33 | 3901 | Max N | 45.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 168 |
| | | | | Min N | -0.56 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 435 |
| | | | | Max $V_u$ | 1.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 1.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 1.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 1.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 1.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 1.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 1.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 1.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 1.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 1.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 99 | RC1 | 88 | 0 | Max N | 6.21 | 0.00 | 1.06 | 0.00 | 0.00 | 0.00 | BC 225 |
| | | | | Min N | -5.89 | 0.00 | 0.72 | 0.00 | 0.00 | 0.00 | BC 471 |
| | | | | Max $V_y$ | 0.04 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.04 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.04 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -5.82 | 0.00 | 0.72 | 0.00 | 0.00 | 0.00 | BC 355 |
| | | | | Max $M_T$ | 6.13 | 0.00 | 1.06 | 0.00 | 0.00 | 0.00 | BC 265 |
| | | | | Min $M_T$ | 5.72 | 0.00 | 0.72 | -0.00 | 0.00 | 0.00 | BC 416 |
| | | | | Max $M_y$ | 0.04 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.04 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.04 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.04 | 0.00 | 1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 87 | 4500 | Max N | 6.21 | 0.00 | -1.06 | 0.00 | 0.00 | 0.00 | BC 225 |
| | | | | Min N | -5.89 | 0.00 | -0.72 | 0.00 | 0.00 | 0.00 | BC 471 |
| | | | | Max $V_y$ | 0.04 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.04 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -5.82 | 0.00 | -0.72 | 0.00 | 0.00 | 0.00 | BC 355 |
| | | | | Min $V_z$ | 0.04 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 6.13 | 0.00 | -1.06 | 0.00 | 0.00 | 0.00 | BC 265 |
| | | | | Min $M_T$ | 5.72 | 0.00 | -0.72 | -0.00 | 0.00 | 0.00 | BC 416 |
| | | | | Max $M_y$ | 0.04 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.04 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.04 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.04 | 0.00 | -1.19 | 0.00 | 0.00 | 0.00 | BC 1 |
| 100 | RC1 | 87 | 0 | Max N | -49.69 | 3.36 | 0.47 | 0.00 | 2.04 | 12.31 | BC 473 |
| | | | | Min N | -208.12 | 0.03 | 0.11 | 0.00 | 0.49 | 0.11 | BC 131 |
| | | | | Max $V_y$ | -73.47 | 3.38 | 0.39 | 0.00 | 1.68 | 12.36 | BC 229 |
| | | | | Min $V_y$ | -85.58 | -3.15 | 0.18 | 0.00 | 0.77 | -11.44 | BC 375 |
| | | | | Max $V_z$ | -75.21 | 3.13 | 0.72 | -0.00 | 3.13 | 11.29 | BC 216 |
| | | | | Min $V_z$ | -52.50 | 2.02 | -0.60 | -0.00 | -2.60 | 7.27 | BC 390 |
| | | | | Max $M_T$ | -108.55 | 3.37 | 0.47 | 0.00 | 2.05 | 12.35 | BC 241 |
| | | | | Min $M_T$ | -52.30 | 2.02 | -0.55 | -0.00 | -2.38 | 7.27 | BC 446 |
| | | | | Max $M_y$ | -75.21 | 3.13 | 0.72 | -0.00 | 3.13 | 11.29 | BC 216 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 100 | RC1 | | | Min $M_y$ | -52.50 | 2.02 | -0.60 | -0.00 | -2.60 | 7.27 | BC 390 |
| | | | | Max $M_z$ | -108.74 | 3.38 | 0.39 | 0.00 | 1.68 | 12.37 | BC 233 |
| | | | | Min $M_z$ | -85.58 | -3.15 | 0.18 | 0.00 | 0.78 | -11.44 | BC 403 |
| | | 67 | 3748 | Max N | -46.70 | 3.36 | 0.47 | 0.00 | 3.80 | -0.30 | BC 473 |
| | | | | Min N | -203.73 | 0.03 | 0.11 | 0.00 | 0.91 | 0.01 | BC 131 |
| | | | | Max $V_y$ | -69.09 | 3.38 | 0.39 | 0.00 | 3.13 | -0.31 | BC 229 |
| | | | | Min $V_y$ | -82.59 | -3.15 | 0.18 | 0.00 | 1.44 | 0.37 | BC 375 |
| | | | | Max $V_z$ | -70.82 | 3.13 | 0.72 | -0.00 | 5.84 | -0.44 | BC 216 |
| | | | | Min $V_z$ | -49.51 | 2.02 | -0.60 | -0.00 | -4.83 | -0.28 | BC 390 |
| | | | | Max $M_T$ | -104.17 | 3.37 | 0.47 | 0.00 | 3.81 | -0.28 | BC 241 |
| | | | | Min $M_T$ | -49.31 | 2.02 | -0.55 | -0.00 | -4.43 | -0.30 | BC 446 |
| | | | | Max $M_y$ | -70.82 | 3.13 | 0.72 | -0.00 | 5.84 | -0.44 | BC 216 |
| | | | | Min $M_y$ | -49.51 | 2.02 | -0.60 | -0.00 | -4.83 | -0.28 | BC 390 |
| | | | | Max $M_z$ | -82.59 | -3.15 | 0.18 | 0.00 | 1.46 | 0.38 | BC 435 |
| | | | | Min $M_z$ | -70.81 | 3.13 | 0.72 | -0.00 | 5.81 | -0.44 | BC 276 |
| 101 | RC1 | 88 | 0 | Max N | -52.45 | 3.10 | 0.96 | 0.00 | 1.55 | 11.35 | BC 448 |
| | | | | Min N | -219.66 | 0.03 | 4.69 | 0.00 | -17.36 | 0.09 | BC 138 |
| | | | | Max $V_y$ | -131.80 | 3.38 | 6.56 | 0.00 | -25.23 | 12.29 | BC 213 |
| | | | | Min $V_y$ | -63.18 | -3.22 | 0.74 | 0.00 | -10.52 | -11.62 | BC 471 |
| | | | | Max $V_z$ | -131.48 | 3.34 | 8.92 | 0.00 | -33.36 | 12.12 | BC 269 |
| | | | | Min $V_z$ | -62.18 | -3.18 | -1.89 | 0.00 | -1.52 | -11.46 | BC 363 |
| | | | | Max $M_T$ | -62.12 | -3.18 | -1.65 | 0.00 | -2.39 | -11.46 | BC 419 |
| | | | | Min $M_T$ | -69.78 | 3.36 | 4.97 | 0.00 | -19.19 | 12.25 | BC 421 |
| | | | | Max $M_y$ | -52.50 | 3.10 | 0.65 | 0.00 | 2.46 | 11.35 | BC 360 |
| | | | | Min $M_y$ | -131.48 | 3.34 | 8.92 | 0.00 | -33.36 | 12.12 | BC 269 |
| | | | | Max $M_z$ | -96.45 | 3.38 | 6.04 | 0.00 | -23.51 | 12.29 | BC 225 |
| | | | | Min $M_z$ | -98.35 | -3.21 | 1.12 | 0.00 | -11.57 | -11.63 | BC 431 |
| | | 68 | 3748 | Max N | -49.46 | 3.10 | 0.96 | 0.00 | 5.14 | -0.29 | BC 448 |
| | | | | Min N | -215.27 | 0.03 | 4.69 | 0.00 | 0.21 | -0.01 | BC 138 |
| | | | | Max $V_y$ | -127.41 | 3.38 | 6.56 | 0.00 | -0.63 | -0.37 | BC 213 |
| | | | | Min $V_y$ | -60.19 | -3.22 | 0.74 | 0.00 | -7.73 | 0.43 | BC 471 |
| | | | | Max $V_z$ | -127.10 | 3.34 | 8.92 | 0.00 | 0.06 | -0.39 | BC 269 |
| | | | | Min $V_z$ | -59.19 | -3.18 | -1.89 | 0.00 | -8.60 | 0.46 | BC 363 |
| | | | | Max $M_T$ | -59.13 | -3.18 | -1.65 | 0.00 | -8.58 | 0.46 | BC 419 |
| | | | | Min $M_T$ | -66.78 | 3.36 | 4.97 | 0.00 | -0.58 | -0.36 | BC 421 |
| | | | | Max $M_y$ | -109.57 | 3.08 | 4.64 | 0.00 | 6.10 | -0.31 | BC 240 |
| | | | | Min $M_y$ | -59.51 | -3.18 | -1.77 | 0.00 | -8.64 | 0.46 | BC 359 |
| | | | | Max $M_z$ | -58.81 | -3.18 | -1.76 | 0.00 | -8.54 | 0.46 | BC 391 |
| | | | | Min $M_z$ | -101.85 | 3.33 | 7.85 | 0.00 | 0.10 | -0.39 | BC 461 |
| 102 | RC1 | 87 | 0 | Max N | 12.43 | 0.00 | 1.01 | 0.00 | 0.00 | 0.00 | BC 169 |
| | | | | Min N | -11.67 | 0.00 | 0.69 | -0.00 | 0.00 | 0.00 | BC 475 |
| | | | | Max $V_y$ | 0.11 | 0.00 | 1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.11 | 0.00 | 1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.11 | 0.00 | 1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -11.67 | 0.00 | 0.69 | -0.00 | 0.00 | 0.00 | BC 371 |
| | | | | Max $M_T$ | 12.39 | 0.00 | 0.69 | 0.00 | 0.00 | 0.00 | BC 377 |
| | | | | Min $M_T$ | 11.43 | 0.00 | 0.69 | -0.00 | 0.00 | 0.00 | BC 356 |
| | | | | Max $M_y$ | 0.11 | 0.00 | 1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.11 | 0.00 | 1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.11 | 0.00 | 1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.11 | 0.00 | 1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | 80 | 4300 | Max N | 12.43 | 0.00 | -1.01 | 0.00 | 0.00 | 0.00 | BC 169 |
| | | | | Min N | -11.67 | 0.00 | -0.69 | -0.00 | 0.00 | 0.00 | BC 475 |
| | | | | Max $V_y$ | 0.11 | 0.00 | -1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.11 | 0.00 | -1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -11.67 | 0.00 | -0.69 | -0.00 | 0.00 | 0.00 | BC 371 |
| | | | | Min $V_z$ | 0.11 | 0.00 | -1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 12.39 | 0.00 | -0.69 | 0.00 | 0.00 | 0.00 | BC 377 |
| | | | | Min $M_T$ | 11.43 | 0.00 | -0.69 | -0.00 | 0.00 | 0.00 | BC 356 |
| | | | | Max $M_y$ | 0.11 | 0.00 | -1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.11 | 0.00 | -1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.11 | 0.00 | -1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.11 | 0.00 | -1.14 | -0.00 | 0.00 | 0.00 | BC 1 |
| 103 | RC1 | 80 | 0 | Max N | -29.96 | 0.07 | 0.04 | -0.00 | -0.14 | 0.24 | BC 49 |
| | | | Links | Min N | -97.09 | 0.00 | 0.01 | -0.00 | -0.01 | 0.78 | BC 154 |
| | | | | Max $V_y$ | -68.01 | 1.02 | 4.28 | 0.00 | 21.13 | -0.03 | BC 236 |
| | | | | Min $V_y$ | -70.07 | -0.16 | 4.64 | 0.00 | 23.55 | 2.10 | BC 237 |
| | | | | Max $V_z$ | -52.04 | 0.09 | 4.68 | 0.00 | 23.36 | 1.93 | BC 197 |
| | | | | Min $V_z$ | -38.22 | 0.03 | -4.38 | -0.00 | -21.75 | 0.43 | BC 471 |
| | | | | Max $M_T$ | -52.72 | 0.66 | 4.32 | 0.00 | 21.00 | -0.73 | BC 164 |
| | | | | Min $M_T$ | -57.41 | 0.07 | -4.31 | -0.00 | -21.99 | 0.34 | BC 235 |
| | | | | Max $M_y$ | -56.35 | -0.10 | 4.62 | 0.00 | 23.62 | 2.06 | BC 461 |
| | | | | Min $M_y$ | -56.23 | 0.06 | -4.31 | -0.00 | -21.99 | 0.30 | BC 187 |
| | | | | Max $M_z$ | -70.16 | -0.15 | 4.64 | 0.00 | 23.55 | 2.12 | BC 269 |
| | | | | Min $M_z$ | -39.07 | 0.54 | 4.30 | 0.00 | 21.06 | -0.92 | BC 360 |
| | | | 0 | Max N | -29.96 | 0.07 | 0.04 | -0.00 | -0.14 | 0.24 | BC 49 |
| | | | Rechts | Min N | -97.09 | 0.00 | 0.01 | -0.00 | -0.01 | 0.78 | BC 154 |
| | | | | Max $V_y$ | -68.01 | 1.02 | 4.28 | 0.00 | 21.13 | -0.03 | BC 236 |
| | | | | Min $V_y$ | -70.07 | -0.16 | 4.64 | 0.00 | 23.55 | 2.10 | BC 237 |
| | | | | Max $V_z$ | -52.04 | 0.09 | 4.68 | 0.00 | 23.36 | 1.93 | BC 197 |
| | | | | Min $V_z$ | -38.22 | 0.03 | -4.38 | -0.00 | -21.75 | 0.43 | BC 471 |
| | | | | Max $M_T$ | -52.72 | 0.66 | 4.32 | 0.00 | 21.00 | -0.73 | BC 164 |
| | | | | Min $M_T$ | -57.41 | 0.07 | -4.31 | -0.00 | -21.99 | 0.34 | BC 235 |
| | | | | Max $M_y$ | -56.35 | -0.10 | 4.62 | 0.00 | 23.62 | 2.06 | BC 461 |
| | | | | Min $M_y$ | -56.23 | 0.06 | -4.31 | -0.00 | -21.99 | 0.30 | BC 187 |
| | | | | Max $M_z$ | -70.16 | -0.15 | 4.64 | 0.00 | 23.55 | 2.12 | BC 269 |
| | | | | Min $M_z$ | -39.07 | 0.54 | 4.30 | 0.00 | 21.06 | -0.92 | BC 360 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 103 | RC1 | | 3627 | Max N | -20.67 | 0.07 | 0.04 | -0.00 | 0.00 | -0.00 | BC 49 |
| | | | Links | Min N | -83.47 | 0.00 | 0.01 | -0.00 | 0.04 | 0.78 | BC 154 |
| | | | | Max $V_y$ | -54.39 | 1.02 | -15.72 | 0.00 | 0.39 | -3.73 | BC 236 |
| | | | | Min $V_y$ | -56.44 | -0.16 | -17.26 | 0.00 | 0.66 | 2.69 | BC 237 |
| | | | | Max $V_z$ | -42.61 | 0.06 | 16.22 | -0.00 | -0.41 | 0.09 | BC 187 |
| | | | | Min $V_z$ | -46.89 | -0.10 | -17.28 | 0.00 | 0.66 | 2.40 | BC 457 |
| | | | | Max $M_T$ | -39.10 | 0.66 | -15.68 | 0.00 | 0.39 | -3.11 | BC 164 |
| | | | | Min $M_T$ | -43.79 | 0.07 | 16.22 | -0.00 | -0.41 | 0.08 | BC 235 |
| | | | | Max $M_y$ | -47.21 | -0.10 | -17.28 | 0.00 | 0.66 | 2.43 | BC 433 |
| | | | | Min $M_y$ | -20.68 | 0.04 | 16.20 | -0.00 | -0.41 | 0.00 | BC 359 |
| | | | | Max $M_z$ | -56.62 | -0.16 | -17.26 | 0.00 | 0.66 | 2.70 | BC 241 |
| | | | | Min $M_z$ | -42.94 | 1.01 | -15.72 | 0.00 | 0.39 | -3.75 | BC 248 |
| | | | 3627 | Max N | -20.67 | 0.07 | 0.04 | -0.00 | 0.00 | -0.00 | BC 49 |
| | | | Rechts | Min N | -83.47 | 0.00 | 0.01 | -0.00 | 0.04 | 0.78 | BC 154 |
| | | | | Max $V_y$ | -54.39 | 1.02 | -15.72 | 0.00 | 0.39 | -3.73 | BC 236 |
| | | | | Min $V_y$ | -56.44 | -0.16 | -17.26 | 0.00 | 0.66 | 2.69 | BC 237 |
| | | | | Max $V_z$ | -42.61 | 0.06 | 16.22 | -0.00 | -0.41 | 0.09 | BC 187 |
| | | | | Min $V_z$ | -46.89 | -0.10 | -17.28 | 0.00 | 0.66 | 2.40 | BC 457 |
| | | | | Max $M_T$ | -39.10 | 0.66 | -15.68 | 0.00 | 0.39 | -3.11 | BC 164 |
| | | | | Min $M_T$ | -43.79 | 0.07 | 16.22 | -0.00 | -0.41 | 0.08 | BC 235 |
| | | | | Max $M_y$ | -47.21 | -0.10 | -17.28 | 0.00 | 0.66 | 2.43 | BC 433 |
| | | | | Min $M_y$ | -20.68 | 0.04 | 16.20 | -0.00 | -0.41 | 0.00 | BC 359 |
| | | | | Max $M_z$ | -56.62 | -0.16 | -17.26 | 0.00 | 0.66 | 2.70 | BC 241 |
| | | | | Min $M_z$ | -42.94 | 1.01 | -15.72 | 0.00 | 0.39 | -3.75 | BC 248 |
| | | | 3686 | Max N | -20.53 | 0.07 | 0.04 | -0.00 | 0.00 | -0.01 | BC 49 |
| | | | Links | Min N | -83.26 | 0.00 | 0.01 | -0.00 | 0.04 | 0.78 | BC 154 |
| | | | | Max $V_y$ | -54.18 | 1.02 | -16.05 | 0.00 | -0.56 | -3.79 | BC 236 |
| | | | | Min $V_y$ | -56.24 | -0.16 | -17.63 | 0.00 | -0.39 | 2.70 | BC 237 |
| | | | | Max $V_z$ | -42.40 | 0.06 | 16.56 | -0.00 | 0.57 | 0.08 | BC 187 |
| | | | | Min $V_z$ | -46.75 | -0.10 | -17.64 | 0.00 | -0.39 | 2.40 | BC 457 |
| | | | | Max $M_T$ | -38.89 | 0.66 | -16.01 | 0.00 | -0.56 | -3.15 | BC 164 |
| | | | | Min $M_T$ | -43.58 | 0.07 | 16.55 | -0.00 | 0.57 | 0.07 | BC 235 |
| | | | | Max $M_y$ | -50.57 | 0.02 | 16.51 | -0.00 | 0.59 | 0.52 | BC 243 |
| | | | | Min $M_y$ | -32.89 | 0.84 | -16.07 | 0.00 | -0.56 | -3.46 | BC 408 |
| | | | | Max $M_z$ | -56.41 | -0.16 | -17.63 | 0.00 | -0.38 | 2.71 | BC 241 |
| | | | | Min $M_z$ | -42.74 | 1.01 | -16.05 | 0.00 | -0.56 | -3.82 | BC 248 |
| | | | 3686 | Max N | -20.53 | 0.07 | 0.04 | -0.00 | 0.00 | -0.01 | BC 49 |
| | | | Rechts | Min N | -83.26 | 0.00 | 0.01 | -0.00 | 0.04 | 0.78 | BC 154 |
| | | | | Max $V_y$ | -54.18 | 1.02 | -16.05 | 0.00 | -0.56 | -3.79 | BC 236 |
| | | | | Min $V_y$ | -56.24 | -0.16 | -17.63 | 0.00 | -0.39 | 2.70 | BC 237 |
| | | | | Max $V_z$ | -42.40 | 0.06 | 16.56 | -0.00 | 0.58 | 0.08 | BC 187 |
| | | | | Min $V_z$ | -46.75 | -0.10 | -17.64 | 0.00 | -0.39 | 2.40 | BC 457 |
| | | | | Max $M_T$ | -38.89 | 0.66 | -16.01 | 0.00 | -0.56 | -3.15 | BC 164 |
| | | | | Min $M_T$ | -43.58 | 0.07 | 16.56 | -0.00 | 0.57 | 0.07 | BC 235 |
| | | | | Max $M_y$ | -50.57 | 0.02 | 16.51 | -0.00 | 0.60 | 0.52 | BC 243 |
| | | | | Min $M_y$ | -32.89 | 0.84 | -16.07 | 0.00 | -0.56 | -3.46 | BC 408 |
| | | | | Max $M_z$ | -56.41 | -0.16 | -17.63 | 0.00 | -0.38 | 2.71 | BC 241 |
| | | | | Min $M_z$ | -42.74 | 1.01 | -16.05 | 0.00 | -0.56 | -3.82 | BC 248 |
| | | | 3748 | Max N | -20.44 | 0.07 | 0.04 | -0.00 | 0.01 | -0.01 | BC 49 |
| | | | Links | Min N | -83.12 | 0.00 | 0.01 | -0.00 | 0.04 | 0.78 | BC 154 |
| | | | | Max $V_y$ | -54.05 | 1.02 | -16.39 | 0.00 | -1.56 | -3.85 | BC 236 |
| | | | | Min $V_y$ | -56.10 | -0.16 | -18.00 | 0.00 | -1.48 | 2.70 | BC 237 |
| | | | | Max $V_z$ | -42.27 | 0.06 | 16.90 | -0.00 | 1.60 | 0.08 | BC 187 |
| | | | | Min $V_z$ | -46.66 | -0.10 | -18.02 | 0.00 | -1.48 | 2.41 | BC 457 |
| | | | | Max $M_T$ | -38.76 | 0.66 | -16.35 | 0.00 | -1.56 | -3.19 | BC 164 |
| | | | | Min $M_T$ | -43.45 | 0.07 | 16.90 | -0.00 | 1.60 | 0.07 | BC 235 |
| | | | | Max $M_y$ | -50.44 | 0.02 | 16.86 | -0.00 | 1.62 | 0.52 | BC 243 |
| | | | | Min $M_y$ | -32.80 | 0.84 | -16.41 | 0.00 | -1.56 | -3.51 | BC 408 |
| | | | | Max $M_z$ | -56.28 | -0.16 | -18.00 | 0.00 | -1.48 | 2.72 | BC 241 |
| | | | | Min $M_z$ | -42.60 | 1.01 | -16.39 | 0.00 | -1.56 | -3.88 | BC 248 |
| | | 42 | 3748 | Max N | -20.44 | 0.07 | 0.04 | -0.00 | 0.01 | -0.01 | BC 49 |
| | | | Rechts | Min N | -83.12 | 0.00 | 0.01 | -0.00 | 0.04 | 0.78 | BC 154 |
| | | | | Max $V_y$ | -54.05 | 1.02 | -16.39 | 0.00 | -1.56 | -3.85 | BC 236 |
| | | | | Min $V_y$ | -56.10 | -0.16 | -18.00 | 0.00 | -1.48 | 2.70 | BC 237 |
| | | | | Max $V_z$ | -42.27 | 0.06 | 16.90 | -0.00 | 1.60 | 0.08 | BC 187 |
| | | | | Min $V_z$ | -46.66 | -0.10 | -18.02 | 0.00 | -1.48 | 2.41 | BC 457 |
| | | | | Max $M_T$ | -38.76 | 0.66 | -16.35 | 0.00 | -1.56 | -3.19 | BC 164 |
| | | | | Min $M_T$ | -43.45 | 0.07 | 16.90 | -0.00 | 1.60 | 0.07 | BC 235 |
| | | | | Max $M_y$ | -50.44 | 0.02 | 16.86 | -0.00 | 1.62 | 0.52 | BC 243 |
| | | | | Min $M_y$ | -32.80 | 0.84 | -16.41 | 0.00 | -1.56 | -3.51 | BC 408 |
| | | | | Max $M_z$ | -56.28 | -0.16 | -18.00 | 0.00 | -1.48 | 2.72 | BC 241 |
| | | | | Min $M_z$ | -42.60 | 1.01 | -16.39 | 0.00 | -1.56 | -3.88 | BC 248 |
| 104 | RC1 | 59 | 0 | Max N | 62.82 | 6.57 | -2.77 | 3.56 | 35.04 | -8.07 | BC 435 |
| | | | | Min N | -26.93 | -8.76 | -54.39 | -10.46 | 7.99 | 0.85 | BC 164 |
| | | | | Max $V_y$ | 49.01 | 18.08 | 30.55 | 15.29 | 40.88 | -8.36 | BC 241 |
| | | | | Min $V_y$ | -22.52 | -10.19 | -50.83 | -11.56 | 4.77 | 0.72 | BC 356 |
| | | | | Max $V_z$ | 49.94 | 15.79 | 36.44 | 13.49 | 34.75 | -8.25 | BC 445 |
| | | | | Min $V_z$ | -20.80 | -8.25 | -56.74 | -9.89 | 10.43 | 0.64 | BC 172 |
| | | | | Max $M_T$ | 4.64 | 16.30 | 20.25 | 16.17 | 20.08 | -0.38 | BC 245 |
| | | | | Min $M_T$ | 24.74 | -9.51 | -39.96 | -12.93 | 24.38 | -7.29 | BC 408 |
| | | | | Max $M_y$ | 53.39 | 9.11 | -14.74 | 5.00 | 45.13 | -8.69 | BC 155 |
| | | | | Min $M_y$ | -20.10 | 1.62 | -11.67 | 0.53 | 3.93 | 1.03 | BC 362 |
| | | | | Max $M_z$ | -24.29 | 3.03 | -15.87 | 1.57 | 7.43 | 1.15 | BC 170 |
| | | | | Min $M_z$ | 56.87 | 7.71 | -9.88 | 3.99 | 41.21 | -8.78 | BC 347 |
| | | | 1505 | Max N | 77.87 | -11.89 | -6.39 | 21.87 | 43.35 | -2.85 | BC 433 |
| | | | | Min N | -123.74 | -8.18 | -49.24 | -10.98 | -34.15 | 2.02 | BC 164 |
| | | | | Max $V_y$ | 71.07 | 5.97 | 39.08 | 7.61 | 37.98 | -1.81 | BC 389 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 104 | RC1 | | | Min $V_y$ | -114.60 | -25.41 | -94.11 | 3.42 | -29.96 | 1.04 | BC 264 |
| | | | | Max $V_z$ | 71.07 | 5.97 | 39.08 | 7.61 | 37.98 | -1.81 | BC 389 |
| | | | | Min $V_z$ | -114.60 | -25.41 | -94.11 | 3.42 | -29.96 | 1.04 | BC 264 |
| | | | | Max $M_T$ | 69.57 | -12.33 | -8.42 | 22.10 | 44.07 | -2.83 | BC 269 |
| | | | | Min $M_T$ | -115.95 | -7.81 | -47.34 | -11.25 | -34.84 | 2.01 | BC 360 |
| | | | | Max $M_y$ | 69.57 | -12.33 | -8.42 | 22.10 | 44.07 | -2.83 | BC 269 |
| | | | | Min $M_y$ | -115.95 | -7.81 | -47.34 | -11.25 | -34.84 | 2.01 | BC 360 |
| | | | | Max $M_z$ | -122.76 | -8.16 | -49.33 | -11.07 | -34.35 | 2.04 | BC 168 |
| | | | | Min $M_z$ | 76.92 | -11.96 | -6.59 | 21.91 | 43.35 | -2.86 | BC 461 |
| | | | 1505 | Max N | 77.87 | -11.89 | -6.39 | 21.87 | 43.35 | -2.85 | BC 433 |
| | | | | Min N | -123.74 | -8.18 | -49.24 | -10.98 | -34.15 | 2.02 | BC 164 |
| | | | | Max $V_y$ | 71.07 | 5.97 | 39.08 | 7.61 | 37.98 | -1.81 | BC 389 |
| | | | | Min $V_y$ | -114.60 | -25.41 | -94.11 | 3.42 | -29.96 | 1.04 | BC 264 |
| | | | | Max $V_z$ | 71.07 | 5.97 | 39.08 | 7.61 | 37.98 | -1.81 | BC 389 |
| | | | | Min $V_z$ | -114.60 | -25.41 | -94.11 | 3.42 | -29.96 | 1.04 | BC 264 |
| | | | | Max $M_T$ | 69.57 | -12.33 | -8.42 | 22.10 | 44.07 | -2.83 | BC 269 |
| | | | | Min $M_T$ | -115.95 | -7.81 | -47.34 | -11.25 | -34.84 | 2.01 | BC 360 |
| | | | | Max $M_y$ | 69.57 | -12.33 | -8.42 | 22.10 | 44.07 | -2.83 | BC 269 |
| | | | | Min $M_y$ | -115.95 | -7.81 | -47.34 | -11.25 | -34.84 | 2.01 | BC 360 |
| | | | | Max $M_z$ | -122.76 | -8.16 | -49.33 | -11.07 | -34.35 | 2.04 | BC 168 |
| | | | | Min $M_z$ | 76.92 | -11.96 | -6.59 | 21.91 | 43.35 | -2.86 | BC 461 |
| | | | 1665 | Max N | 91.33 | 3.45 | 44.77 | 7.05 | 40.35 | -2.19 | BC 377 |
| | | | | Min N | -156.48 | -26.82 | -99.00 | 4.27 | -33.31 | 3.06 | BC 276 |
| | | | | Max $V_y$ | 88.63 | 3.91 | 45.11 | 6.35 | 38.98 | -2.04 | BC 389 |
| | | | | Min $V_y$ | -154.56 | -27.11 | -99.17 | 5.04 | -32.00 | 2.90 | BC 264 |
| | | | | Max $V_z$ | 88.63 | 3.91 | 45.11 | 6.35 | 38.98 | -2.04 | BC 389 |
| | | | | Min $V_z$ | -154.56 | -27.11 | -99.17 | 5.04 | -32.00 | 2.90 | BC 264 |
| | | | | Max $M_T$ | 63.02 | -17.16 | -10.37 | 21.70 | 45.21 | -1.85 | BC 269 |
| | | | | Min $M_T$ | -130.10 | -7.18 | -44.30 | -10.70 | -37.75 | 2.83 | BC 360 |
| | | | | Max $M_y$ | 63.02 | -17.16 | -10.37 | 21.70 | 45.21 | -1.85 | BC 269 |
| | | | | Min $M_y$ | -130.10 | -7.18 | -44.30 | -10.70 | -37.75 | 2.83 | BC 360 |
| | | | | Max $M_z$ | -155.37 | -26.72 | -98.73 | 4.23 | -33.30 | 3.07 | BC 248 |
| | | | | Min $M_z$ | 89.90 | 3.37 | 44.51 | 7.11 | 40.34 | -2.19 | BC 405 |
| | | | 1665 | Max N | 87.05 | 3.18 | -30.04 | 6.13 | 41.72 | -2.58 | BC 377 |
| | | | | Min N | -140.74 | -25.75 | -42.86 | 5.75 | -40.63 | 3.22 | BC 276 |
| | | | | Max $V_y$ | 84.35 | 3.64 | -26.68 | 5.45 | 40.33 | -2.44 | BC 389 |
| | | | | Min $V_y$ | -139.19 | -26.03 | -46.35 | 6.47 | -39.08 | 3.07 | BC 264 |
| | | | | Max $V_z$ | -115.37 | -7.53 | 22.24 | -10.04 | -45.67 | 2.97 | BC 360 |
| | | | | Min $V_z$ | 61.74 | -16.07 | -94.97 | 21.58 | 45.84 | -2.26 | BC 269 |
| | | | | Max $M_T$ | 61.74 | -16.07 | -94.97 | 21.58 | 45.84 | -2.26 | BC 269 |
| | | | | Min $M_T$ | -115.37 | -7.53 | 22.24 | -10.04 | -45.67 | 2.97 | BC 360 |
| | | | | Max $M_y$ | 61.74 | -16.07 | -94.97 | 21.58 | 45.84 | -2.26 | BC 269 |
| | | | | Min $M_y$ | -115.37 | -7.53 | 22.24 | -10.04 | -45.67 | 2.97 | BC 360 |
| | | | | Max $M_z$ | -139.69 | -25.67 | -42.91 | 5.69 | -40.59 | 3.22 | BC 248 |
| | | | | Min $M_z$ | 85.64 | 3.12 | -30.01 | 6.18 | 41.70 | -2.58 | BC 405 |
| | | | 5005 | Max N | 15.42 | -3.92 | -8.83 | 0.27 | 4.25 | 0.31 | BC 389 |
| | | | | Min N | -127.76 | 14.18 | 50.25 | -12.05 | -18.18 | 1.07 | BC 264 |
| | | | | Max $V_y$ | -109.35 | 14.59 | 50.28 | -11.63 | -15.49 | 0.67 | BC 456 |
| | | | | Min $V_y$ | -1.91 | -4.30 | -8.76 | -0.17 | 1.70 | 0.70 | BC 197 |
| | | | | Max $V_z$ | -109.35 | 14.59 | 50.28 | -11.63 | -15.49 | 0.67 | BC 456 |
| | | | | Min $V_z$ | 15.42 | -3.92 | -8.83 | 0.27 | 4.25 | 0.31 | BC 389 |
| | | | | Max $M_T$ | -36.25 | -1.08 | 2.88 | 2.35 | -6.76 | 1.36 | BC 323 |
| | | | | Min $M_T$ | -55.11 | 12.31 | 42.61 | -14.32 | -6.29 | 0.06 | BC 283 |
| | | | | Max $M_y$ | -5.69 | 9.20 | 32.48 | -12.27 | 4.42 | -0.65 | BC 413 |
| | | | | Min $M_y$ | -126.98 | 14.11 | 50.06 | -12.02 | -18.35 | 1.09 | BC 236 |
| | | | | Max $M_z$ | -100.94 | 0.01 | 5.70 | 1.81 | -17.74 | 2.05 | BC 172 |
| | | | | Min $M_z$ | -9.04 | 10.34 | 36.12 | -13.57 | 4.03 | -0.69 | BC 473 |
| | | | 5005 | Max N | 15.42 | -3.92 | -8.83 | 0.27 | 4.25 | 0.31 | BC 389 |
| | | | | Min N | -127.76 | 14.18 | 50.25 | -12.05 | -18.18 | 1.07 | BC 264 |
| | | | | Max $V_y$ | -109.35 | 14.59 | 50.28 | -11.63 | -15.49 | 0.67 | BC 456 |
| | | | | Min $V_y$ | -1.91 | -4.30 | -8.76 | -0.17 | 1.70 | 0.70 | BC 197 |
| | | | | Max $V_z$ | -109.35 | 14.59 | 50.28 | -11.63 | -15.49 | 0.67 | BC 456 |
| | | | | Min $V_z$ | 15.42 | -3.92 | -8.83 | 0.27 | 4.25 | 0.31 | BC 389 |
| | | | | Max $M_T$ | -36.25 | -1.08 | 2.88 | 2.35 | -6.76 | 1.36 | BC 323 |
| | | | | Min $M_T$ | -55.11 | 12.31 | 42.61 | -14.32 | -6.29 | 0.06 | BC 283 |
| | | | | Max $M_y$ | -5.69 | 9.20 | 32.48 | -12.27 | 4.42 | -0.65 | BC 413 |
| | | | | Min $M_y$ | -126.98 | 14.11 | 50.06 | -12.02 | -18.35 | 1.09 | BC 236 |
| | | | | Max $M_z$ | -100.94 | 0.01 | 5.70 | 1.81 | -17.74 | 2.05 | BC 172 |
| | | | | Min $M_z$ | -9.04 | 10.34 | 36.12 | -13.57 | 4.03 | -0.69 | BC 473 |
| | | 58 | 6510 | Max N | 18.16 | -6.93 | -21.88 | -3.57 | 30.78 | -6.73 | BC 385 |
| | | | | Min N | -96.03 | -3.45 | -8.54 | -2.99 | -8.99 | 1.89 | BC 160 |
| | | | | Max $V_y$ | -74.71 | -1.40 | -2.63 | -1.30 | -10.57 | 1.95 | BC 356 |
| | | | | Min $V_y$ | -4.24 | -9.55 | -29.67 | -5.59 | 35.16 | -6.70 | BC 241 |
| | | | | Max $V_z$ | -74.71 | -1.40 | -2.63 | -1.30 | -10.57 | 1.95 | BC 356 |
| | | | | Min $V_z$ | -4.92 | -9.54 | -29.67 | -5.53 | 35.45 | -6.76 | BC 269 |
| | | | | Max $M_T$ | -53.70 | -3.62 | -10.77 | 1.28 | 12.62 | -6.60 | BC 468 |
| | | | | Min $M_T$ | -22.97 | -7.31 | -21.41 | -8.24 | 12.13 | 1.82 | BC 185 |
| | | | | Max $M_y$ | -4.92 | -9.54 | -29.67 | -5.53 | 35.45 | -6.76 | BC 269 |
| | | | | Min $M_y$ | -74.18 | -1.42 | -2.68 | -1.34 | -10.92 | 2.02 | BC 360 |
| | | | | Max $M_z$ | -83.74 | -5.76 | -16.78 | -5.53 | -3.28 | 2.84 | BC 174 |
| | | | | Min $M_z$ | 17.59 | -7.26 | -22.97 | -3.48 | 32.51 | -7.45 | BC 473 |
| 105 | RC1 | 58 | 0 | Max N | 18.16 | -6.93 | -21.88 | -3.57 | 30.78 | -6.73 | BC 385 |
| | | | | Min N | -96.03 | -3.45 | -8.54 | -2.99 | -8.99 | 1.89 | BC 160 |
| | | | | Max $V_y$ | -74.71 | -1.40 | -2.63 | -1.30 | -10.57 | 1.95 | BC 356 |
| | | | | Min $V_y$ | -4.24 | -9.55 | -29.67 | -5.59 | 35.16 | -6.70 | BC 241 |
| | | | | Max $V_z$ | -74.71 | -1.40 | -2.63 | -1.30 | -10.57 | 1.95 | BC 356 |
| | | | | Min $V_z$ | -4.92 | -9.54 | -29.67 | -5.53 | 35.45 | -6.76 | BC 269 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 105 | RC1 | | | Max $M_T$ | -53.70 | -3.62 | -10.77 | 1.28 | 12.62 | -6.60 | BC 468 |
| | | | | Min $M_T$ | -22.97 | -7.31 | -21.41 | -8.24 | 12.13 | 1.82 | BC 185 |
| | | | | Max $M_y$ | -4.92 | -9.54 | -29.67 | -5.53 | 35.45 | -6.76 | BC 269 |
| | | | | Min $M_y$ | -74.18 | -1.42 | -2.68 | -1.34 | -10.92 | 2.02 | BC 360 |
| | | | | Max $M_z$ | -83.74 | -5.76 | -16.78 | -5.53 | -3.28 | 2.84 | BC 174 |
| | | | | Min $M_z$ | 17.59 | -7.26 | -22.97 | -3.48 | 32.51 | -7.45 | BC 473 |
| | | | 1450 | Max N | -55.15 | -3.54 | -12.42 | -9.20 | -12.60 | 2.51 | BC 391 |
| | | | | Min N | -209.16 | -28.54 | -102.34 | 1.91 | -46.21 | 5.90 | BC 154 |
| | | | | Max $V_y$ | -92.45 | -1.54 | -6.69 | -6.18 | -18.27 | 3.12 | BC 360 |
| | | | | Min $V_y$ | -208.85 | -28.56 | -102.48 | 1.80 | -46.17 | 5.90 | BC 155 |
| | | | | Max $V_z$ | -92.45 | -1.54 | -6.69 | -6.18 | -18.27 | 3.12 | BC 360 |
| | | | | Min $V_z$ | -208.85 | -28.56 | -102.48 | 1.80 | -46.17 | 5.90 | BC 155 |
| | | | | Max $M_T$ | -145.50 | -19.44 | -66.75 | 13.21 | -28.51 | 2.80 | BC 468 |
| | | | | Min $M_T$ | -109.10 | -9.30 | -35.24 | -18.25 | -25.48 | 4.91 | BC 185 |
| | | | | Max $M_y$ | -55.47 | -3.59 | -12.56 | -9.04 | -12.27 | 2.47 | BC 419 |
| | | | | Min $M_y$ | -207.79 | -28.51 | -102.20 | 1.73 | -46.35 | 5.93 | BC 147 |
| | | | | Max $M_z$ | -158.81 | -12.45 | -48.04 | -16.38 | -36.89 | 6.27 | BC 149 |
| | | | | Min $M_z$ | -98.44 | -19.71 | -66.70 | 8.89 | -20.54 | 2.00 | BC 415 |
| | | | 1450 | Max N | -55.15 | -3.54 | -12.42 | -9.20 | -12.60 | 2.51 | BC 391 |
| | | | | Min N | -209.16 | -28.54 | -102.34 | 1.91 | -46.21 | 5.90 | BC 154 |
| | | | | Max $V_y$ | -92.45 | -1.54 | -6.69 | -6.18 | -18.27 | 3.12 | BC 360 |
| | | | | Min $V_y$ | -208.85 | -28.56 | -102.48 | 1.80 | -46.17 | 5.90 | BC 155 |
| | | | | Max $V_z$ | -92.45 | -1.54 | -6.69 | -6.18 | -18.27 | 3.12 | BC 360 |
| | | | | Min $V_z$ | -208.85 | -28.56 | -102.48 | 1.80 | -46.17 | 5.90 | BC 155 |
| | | | | Max $M_T$ | -145.50 | -19.44 | -66.75 | 13.21 | -28.51 | 2.80 | BC 468 |
| | | | | Min $M_T$ | -109.10 | -9.30 | -35.24 | -18.25 | -25.48 | 4.91 | BC 185 |
| | | | | Max $M_y$ | -55.47 | -3.59 | -12.56 | -9.04 | -12.27 | 2.47 | BC 419 |
| | | | | Min $M_y$ | -207.79 | -28.51 | -102.20 | 1.73 | -46.35 | 5.93 | BC 147 |
| | | | | Max $M_z$ | -158.81 | -12.45 | -48.04 | -16.38 | -36.89 | 6.27 | BC 149 |
| | | | | Min $M_z$ | -98.44 | -19.71 | -66.70 | 8.89 | -20.54 | 2.00 | BC 415 |
| | | | 4950 | Max N | -81.43 | 4.78 | 6.70 | -22.54 | -21.64 | 4.36 | BC 391 |
| | | | | Min N | -305.60 | 30.23 | 72.67 | -56.16 | -101.05 | 14.36 | BC 155 |
| | | | | Max $V_y$ | -305.60 | 30.23 | 72.67 | -56.16 | -101.05 | 14.36 | BC 155 |
| | | | | Min $V_y$ | -81.43 | 4.78 | 6.70 | -22.54 | -21.64 | 4.36 | BC 391 |
| | | | | Max $V_z$ | -304.18 | 30.06 | 72.76 | -56.27 | -100.64 | 14.30 | BC 148 |
| | | | | Min $V_z$ | -82.55 | 4.90 | 6.48 | -22.43 | -21.90 | 4.41 | BC 419 |
| | | | | Max $M_T$ | -93.71 | 5.64 | 10.23 | -20.44 | -24.53 | 4.77 | BC 356 |
| | | | | Min $M_T$ | -304.18 | 30.06 | 72.76 | -56.27 | -100.64 | 14.30 | BC 148 |
| | | | | Max $M_y$ | -81.43 | 4.78 | 6.70 | -22.54 | -21.64 | 4.36 | BC 391 |
| | | | | Min $M_y$ | -305.60 | 30.23 | 72.67 | -56.16 | -101.05 | 14.36 | BC 155 |
| | | | | Max $M_z$ | -305.60 | 30.23 | 72.67 | -56.16 | -101.05 | 14.36 | BC 155 |
| | | | | Min $M_z$ | -81.43 | 4.78 | 6.70 | -22.54 | -21.64 | 4.36 | BC 391 |
| | | | 4950 | Max N | -81.43 | 4.78 | 6.70 | -22.54 | -21.64 | 4.36 | BC 391 |
| | | | | Min N | -305.60 | 30.23 | 72.67 | -56.16 | -101.05 | 14.36 | BC 155 |
| | | | | Max $V_y$ | -305.60 | 30.23 | 72.67 | -56.16 | -101.05 | 14.36 | BC 155 |
| | | | | Min $V_y$ | -81.43 | 4.78 | 6.70 | -22.54 | -21.64 | 4.36 | BC 391 |
| | | | | Max $V_z$ | -304.18 | 30.06 | 72.76 | -56.27 | -100.64 | 14.30 | BC 148 |
| | | | | Min $V_z$ | -82.55 | 4.90 | 6.48 | -22.43 | -21.90 | 4.41 | BC 419 |
| | | | | Max $M_T$ | -93.71 | 5.64 | 10.23 | -20.44 | -24.53 | 4.77 | BC 356 |
| | | | | Min $M_T$ | -304.18 | 30.06 | 72.76 | -56.27 | -100.64 | 14.30 | BC 148 |
| | | | | Max $M_y$ | -81.43 | 4.78 | 6.70 | -22.54 | -21.64 | 4.36 | BC 391 |
| | | | | Min $M_y$ | -305.60 | 30.23 | 72.67 | -56.16 | -101.05 | 14.36 | BC 155 |
| | | | | Max $M_z$ | -305.60 | 30.23 | 72.67 | -56.16 | -101.05 | 14.36 | BC 155 |
| | | | | Min $M_z$ | -81.43 | 4.78 | 6.70 | -22.54 | -21.64 | 4.36 | BC 391 |
| | | 8 | 6400 | Max N | -24.60 | 16.62 | 13.12 | -24.15 | -22.71 | 2.25 | BC 363 |
| | | | | Min N | -70.71 | 33.73 | 80.64 | -64.05 | -56.55 | 5.71 | BC 155 |
| | | | | Max $V_y$ | -65.02 | 35.36 | 54.09 | -55.91 | -51.07 | 5.21 | BC 156 |
| | | | | Min $V_y$ | -29.99 | 15.24 | 38.06 | -31.90 | -28.01 | 2.72 | BC 383 |
| | | | | Max $V_z$ | -70.71 | 33.73 | 80.64 | -64.05 | -56.55 | 5.71 | BC 155 |
| | | | | Min $V_z$ | -24.62 | 16.64 | 13.08 | -24.19 | -22.74 | 2.25 | BC 391 |
| | | | | Max $M_T$ | -29.14 | 17.28 | 19.11 | -22.94 | -20.35 | 2.11 | BC 360 |
| | | | | Min $M_T$ | -70.71 | 33.73 | 80.64 | -64.05 | -56.55 | 5.71 | BC 155 |
| | | | | Max $M_y$ | -29.14 | 17.28 | 19.11 | -22.94 | -20.35 | 2.11 | BC 360 |
| | | | | Min $M_y$ | -70.71 | 33.73 | 80.64 | -64.05 | -56.55 | 5.71 | BC 155 |
| | | | | Max $M_z$ | -70.71 | 33.73 | 80.64 | -64.05 | -56.55 | 5.71 | BC 155 |
| | | | | Min $M_z$ | -29.14 | 17.28 | 19.11 | -22.94 | -20.35 | 2.11 | BC 360 |
| 106 | RC1 | 88 | 0 | Max N | 1.23 | -0.00 | -0.86 | 0.01 | -0.00 | 0.00 | BC 363 |
| | | | | Min N | -37.77 | 0.00 | -1.93 | -0.01 | 0.00 | 0.00 | BC 165 |
| | | | | Max $V_y$ | -34.15 | 0.00 | -2.76 | -0.01 | 0.00 | 0.00 | BC 217 |
| | | | | Min $V_y$ | -4.06 | -0.00 | -1.71 | 0.01 | 0.00 | 0.00 | BC 247 |
| | | | | Max $V_z$ | -17.31 | 0.00 | -0.37 | -0.01 | 0.00 | 0.00 | BC 360 |
| | | | | Min $V_z$ | -19.93 | -0.00 | -3.29 | 0.00 | 0.00 | 0.00 | BC 155 |
| | | | | Max $M_T$ | -9.96 | -0.00 | -2.54 | 0.01 | -0.00 | 0.00 | BC 243 |
| | | | | Min $M_T$ | -35.76 | 0.00 | -2.14 | -0.01 | 0.00 | 0.00 | BC 201 |
| | | | | Max $M_y$ | -10.84 | 0.00 | -2.24 | -0.00 | 0.00 | 0.00 | BC 278 |
| | | | | Min $M_y$ | -13.07 | -0.00 | -2.10 | 0.00 | -0.00 | 0.00 | BC 53 |
| | | | | Max $M_z$ | -10.40 | 0.00 | -1.75 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -10.40 | 0.00 | -1.75 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | 96 | 1665 | Max N | 1.23 | -0.00 | -1.39 | 0.01 | -1.87 | 0.00 | BC 363 |
| | | | | Min N | -37.77 | 0.00 | -2.71 | -0.01 | -3.86 | -0.00 | BC 165 |
| | | | | Max $V_y$ | -34.15 | 0.00 | -3.54 | -0.01 | -5.25 | -0.00 | BC 217 |
| | | | | Min $V_y$ | -4.06 | -0.00 | -2.49 | 0.01 | -3.50 | 0.00 | BC 247 |
| | | | | Max $V_z$ | -17.31 | 0.00 | -0.90 | -0.01 | -1.06 | -0.00 | BC 360 |
| | | | | Min $V_z$ | -19.93 | -0.00 | -4.08 | 0.00 | -6.13 | 0.00 | BC 155 |
| | | | | Max $M_T$ | -9.96 | -0.00 | -3.33 | 0.01 | -4.89 | 0.00 | BC 243 |
| | | | | Min $M_T$ | -35.76 | 0.00 | -2.92 | -0.01 | -4.21 | -0.00 | BC 201 |
| | | | | Max $M_y$ | -17.31 | 0.00 | -0.90 | -0.01 | -1.06 | -0.00 | BC 360 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 106 | RC1 | | | Min $M_y$ | -19.93 | -0.00 | -4.08 | 0.00 | -6.13 | 0.00 | BC 155 |
| | | | | Max $M_z$ | -4.06 | -0.00 | -2.49 | 0.01 | -3.50 | 0.00 | BC 247 |
| | | | | Min $M_z$ | -34.15 | 0.00 | -3.54 | -0.01 | -5.25 | -0.00 | BC 217 |
| 107 | RC1 | 77 | 0 | Max N | -25.47 | 0.15 | 10.88 | -0.00 | -10.65 | 0.38 | BC 362 |
| | | | Links | Min N | -87.50 | 0.14 | 6.08 | -0.00 | -20.15 | 0.10 | BC 140 |
| | | | | Max $V_y$ | -51.37 | 1.01 | 11.79 | 0.00 | -17.78 | 0.32 | BC 415 |
| | | | | Min $V_y$ | -26.08 | 0.01 | 2.16 | -0.00 | -7.20 | 0.03 | BC 64 |
| | | | | Max $V_z$ | -49.96 | 0.12 | 14.24 | -0.00 | -22.41 | 0.34 | BC 270 |
| | | | | Min $V_z$ | -27.54 | 0.08 | -4.01 | -0.00 | -8.35 | 0.11 | BC 361 |
| | | | | Max $M_T$ | -50.20 | 0.45 | 10.27 | 0.00 | -12.61 | 0.02 | BC 439 |
| | | | | Min $M_T$ | -66.80 | 0.31 | 8.91 | -0.00 | -13.50 | 0.22 | BC 204 |
| | | | | Max $M_y$ | -36.65 | 0.04 | 5.80 | -0.00 | -2.64 | 0.09 | BC 360 |
| | | | | Min $M_y$ | -73.75 | 0.92 | 13.22 | 0.00 | -22.50 | 0.25 | BC 271 |
| | | | | Max $M_z$ | -49.72 | 0.15 | 12.32 | -0.00 | -15.78 | 0.45 | BC 246 |
| | | | | Min $M_z$ | -61.78 | 0.42 | 11.11 | 0.00 | -15.41 | -0.01 | BC 235 |
| | | | 0 | Max N | -25.47 | 0.15 | 10.88 | -0.00 | -10.65 | 0.38 | BC 362 |
| | | | Rechts | Min N | -87.50 | 0.14 | 6.08 | -0.00 | -20.15 | 0.10 | BC 140 |
| | | | | Max $V_y$ | -51.37 | 1.01 | 11.79 | 0.00 | -17.78 | 0.32 | BC 415 |
| | | | | Min $V_y$ | -26.08 | 0.01 | 2.16 | -0.00 | -7.20 | 0.03 | BC 64 |
| | | | | Max $V_z$ | -49.96 | 0.12 | 14.24 | -0.00 | -22.41 | 0.34 | BC 270 |
| | | | | Min $V_z$ | -27.54 | 0.08 | -4.01 | -0.00 | -8.35 | 0.11 | BC 361 |
| | | | | Max $M_T$ | -50.20 | 0.45 | 10.27 | 0.00 | -12.61 | 0.02 | BC 439 |
| | | | | Min $M_T$ | -66.80 | 0.31 | 8.91 | -0.00 | -13.50 | 0.22 | BC 204 |
| | | | | Max $M_y$ | -36.65 | 0.04 | 5.80 | -0.00 | -2.64 | 0.09 | BC 360 |
| | | | | Min $M_y$ | -73.75 | 0.92 | 13.22 | 0.00 | -22.50 | 0.25 | BC 271 |
| | | | | Max $M_z$ | -49.72 | 0.15 | 12.32 | -0.00 | -15.78 | 0.45 | BC 246 |
| | | | | Min $M_z$ | -61.78 | 0.42 | 11.11 | 0.00 | -15.41 | -0.01 | BC 235 |
| | | | 3505 | Max N | -18.41 | 0.15 | -4.28 | -0.00 | 0.85 | -0.13 | BC 362 |
| | | | Links | Min N | -77.15 | 0.14 | 6.08 | -0.00 | 1.15 | -0.40 | BC 140 |
| | | | | Max $V_y$ | -44.31 | 1.01 | -1.71 | 0.00 | -0.18 | -3.21 | BC 415 |
| | | | | Min $V_y$ | -19.02 | 0.01 | 2.16 | -0.00 | 0.36 | 0.00 | BC 64 |
| | | | | Max $V_z$ | -50.45 | 0.47 | 13.17 | -0.00 | 1.90 | -1.28 | BC 269 |
| | | | | Min $V_z$ | -18.41 | 0.15 | -4.28 | -0.00 | 0.85 | -0.13 | BC 362 |
| | | | | Max $M_T$ | -43.14 | 0.45 | -3.23 | 0.00 | -0.32 | -1.55 | BC 439 |
| | | | | Min $M_T$ | -56.45 | 0.31 | 0.48 | -0.00 | 2.92 | -0.88 | BC 204 |
| | | | | Max $M_y$ | -48.73 | 0.25 | -0.20 | -0.00 | 3.39 | -0.70 | BC 432 |
| | | | | Min $M_y$ | -32.68 | 0.52 | -3.86 | 0.00 | -0.47 | -1.75 | BC 363 |
| | | | | Max $M_z$ | -40.14 | 0.03 | 11.16 | -0.00 | 1.63 | 0.01 | BC 245 |
| | | | | Min $M_z$ | -44.31 | 1.01 | -1.71 | 0.00 | -0.18 | -3.21 | BC 415 |
| | | 63 | 3505 | Max N | -18.41 | 0.15 | -4.28 | -0.00 | 0.85 | -0.13 | BC 362 |
| | | | Rechts | Min N | -77.15 | 0.14 | 6.08 | -0.00 | 1.15 | -0.40 | BC 140 |
| | | | | Max $V_y$ | -44.31 | 1.01 | -1.71 | 0.00 | -0.18 | -3.21 | BC 415 |
| | | | | Min $V_y$ | -19.02 | 0.01 | 2.16 | -0.00 | 0.36 | 0.00 | BC 64 |
| | | | | Max $V_z$ | -50.45 | 0.47 | 13.17 | -0.00 | 1.90 | -1.28 | BC 269 |
| | | | | Min $V_z$ | -18.41 | 0.15 | -4.28 | -0.00 | 0.85 | -0.13 | BC 362 |
| | | | | Max $M_T$ | -43.14 | 0.45 | -3.23 | 0.00 | -0.32 | -1.55 | BC 439 |
| | | | | Min $M_T$ | -56.45 | 0.31 | 0.48 | -0.00 | 2.92 | -0.88 | BC 204 |
| | | | | Max $M_y$ | -48.73 | 0.25 | -0.20 | -0.00 | 3.39 | -0.70 | BC 432 |
| | | | | Min $M_y$ | -32.68 | 0.52 | -3.86 | 0.00 | -0.47 | -1.75 | BC 363 |
| | | | | Max $M_z$ | -40.14 | 0.03 | 11.16 | -0.00 | 1.63 | 0.01 | BC 245 |
| | | | | Min $M_z$ | -44.31 | 1.01 | -1.71 | 0.00 | -0.18 | -3.21 | BC 415 |
| 108 | RC1 | 62 | 0 | Max N | 59.76 | -2.53 | -40.31 | -9.37 | 28.52 | -1.63 | BC 451 |
| | | | | Min N | -182.73 | 13.92 | 29.29 | -16.62 | -39.25 | 4.24 | BC 206 |
| | | | | Max $V_y$ | -152.81 | 16.28 | 47.01 | -13.80 | -36.47 | 3.68 | BC 442 |
| | | | | Min $V_y$ | -34.74 | -5.63 | -48.05 | -9.57 | 4.58 | 0.20 | BC 200 |
| | | | | Max $V_z$ | -161.99 | 16.11 | 47.43 | -13.22 | -37.87 | 3.88 | BC 470 |
| | | | | Min $V_z$ | -29.02 | -5.49 | -59.65 | -18.61 | 2.98 | 0.64 | BC 134 |
| | | | | Max $M_T$ | -119.23 | 0.51 | -0.05 | -0.82 | -29.39 | 2.26 | BC 358 |
| | | | | Min $M_T$ | -93.27 | 12.08 | -6.44 | -29.24 | -10.37 | 2.62 | BC 148 |
| | | | | Max $M_y$ | 50.55 | -3.47 | -49.74 | -12.18 | 29.00 | -1.48 | BC 259 |
| | | | | Min $M_y$ | -171.42 | 14.60 | 38.21 | -14.01 | -39.30 | 4.06 | BC 398 |
| | | | | Max $M_z$ | -182.73 | 13.92 | 29.29 | -16.62 | -39.25 | 4.24 | BC 206 |
| | | | | Min $M_z$ | 59.76 | -2.53 | -40.31 | -9.37 | 28.52 | -1.63 | BC 451 |
| | | 64 | 4500 | Max N | 55.34 | -2.90 | 30.77 | -15.15 | 36.46 | 0.03 | BC 434 |
| | | | | Min N | -184.96 | -7.33 | -10.74 | -19.75 | -41.53 | 6.08 | BC 167 |
| | | | | Max $V_y$ | -19.08 | 0.86 | 46.26 | -10.10 | 14.62 | 2.02 | BC 394 |
| | | | | Min $V_y$ | -114.57 | -12.92 | -25.40 | -25.49 | -18.41 | 4.16 | BC 255 |
| | | | | Max $V_z$ | -42.15 | -1.20 | 51.33 | -13.31 | 12.87 | 3.19 | BC 174 |
| | | | | Min $V_z$ | -90.93 | -11.28 | -29.88 | -22.38 | -15.85 | 2.98 | BC 475 |
| | | | | Max $M_T$ | -1.06 | -1.32 | 37.12 | -5.56 | 17.47 | 1.50 | BC 422 |
| | | | | Min $M_T$ | -49.34 | -4.24 | 33.74 | -31.71 | 12.06 | 3.29 | BC 140 |
| | | | | Max $M_y$ | 55.34 | -2.90 | 30.77 | -15.15 | 36.46 | 0.03 | BC 434 |
| | | | | Min $M_y$ | -184.96 | -7.33 | -10.74 | -19.75 | -41.53 | 6.08 | BC 167 |
| | | | | Max $M_z$ | -184.94 | -6.99 | -3.31 | -21.76 | -39.41 | 6.14 | BC 203 |
| | | | | Min $M_z$ | 53.75 | -3.03 | 22.93 | -13.10 | 33.59 | -0.00 | BC 446 |
| 109 | RC1 | 36 | 0 | Max N | 229.80 | 10.59 | -72.90 | 28.96 | 96.40 | -2.02 | BC 340 |
| | | | | Min N | -73.88 | 8.00 | 1.47 | 16.32 | -11.91 | 3.40 | BC 358 |
| | | | | Max $V_y$ | 39.08 | 15.76 | -12.48 | 29.95 | 34.26 | 1.83 | BC 238 |
| | | | | Min $V_y$ | 53.12 | 1.43 | -50.97 | 10.30 | 35.44 | 0.83 | BC 359 |
| | | | | Max $V_z$ | -16.97 | 12.88 | 15.03 | 23.49 | 9.02 | 1.81 | BC 470 |
| | | | | Min $V_z$ | 155.70 | 9.93 | -92.46 | 29.55 | 77.28 | 0.86 | BC 134 |
| | | | | Max $M_T$ | 217.13 | 10.58 | -86.70 | 37.00 | 99.29 | -0.73 | BC 140 |
| | | | | Min $M_T$ | 71.36 | 3.45 | -49.78 | 7.71 | 41.00 | 0.35 | BC 423 |
| | | | | Max $M_y$ | 228.87 | 12.68 | -83.15 | 34.89 | 102.19 | -1.07 | BC 148 |
| | | | | Min $M_y$ | -73.88 | 8.00 | 1.47 | 16.32 | -11.91 | 3.40 | BC 358 |
| | | | | Max $M_z$ | -72.18 | 9.87 | -9.60 | 22.00 | -5.29 | 4.29 | BC 166 |
| | | | | Min $M_z$ | 229.80 | 10.59 | -72.90 | 28.96 | 96.40 | -2.02 | BC 340 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 109 | RC1 | 60 | 4500 | Max N | 244.81 | -3.74 | 102.51 | -6.71 | 91.04 | -4.01 | BC 149 |
| | | | | Min N | -77.42 | -15.46 | -26.96 | 4.24 | -10.67 | 2.42 | BC 411 |
| | | | | Max $V_y$ | 60.67 | 2.46 | 39.77 | -1.03 | 25.91 | -1.15 | BC 388 |
| | | | | Min $V_y$ | 154.70 | -19.64 | 50.11 | 0.78 | 72.22 | -1.55 | BC 154 |
| | | | | Max $V_z$ | 242.17 | -2.30 | 106.44 | -8.42 | 91.19 | -4.05 | BC 131 |
| | | | | Min $V_z$ | -74.71 | -16.91 | -30.87 | 5.95 | -10.77 | 2.46 | BC 475 |
| | | | | Max $M_T$ | 84.59 | -15.28 | 10.44 | 10.96 | 45.12 | -1.17 | BC 446 |
| | | | | Min $M_T$ | 233.91 | -2.16 | 106.18 | -9.01 | 90.12 | -3.88 | BC 138 |
| | | | | Max $M_y$ | 244.34 | -3.74 | 102.61 | -6.75 | 91.27 | -4.03 | BC 146 |
| | | | | Min $M_y$ | -76.71 | -15.45 | -27.00 | 4.29 | -10.83 | 2.44 | BC 415 |
| | | | | Max $M_z$ | -74.71 | -16.91 | -30.87 | 5.95 | -10.77 | 2.46 | BC 475 |
| | | | | Min $M_z$ | 199.86 | 1.25 | 85.56 | -2.43 | 78.48 | -4.05 | BC 174 |
| 110 | RC1 | 60 | 0 | Max N | 247.61 | -2.41 | -113.01 | -10.45 | 89.33 | -4.05 | BC 149 |
| | | | | Min N | -76.55 | -18.01 | -71.23 | 1.01 | -12.74 | 2.35 | BC 411 |
| | | | | Max $V_y$ | 89.41 | 2.46 | -44.79 | -4.94 | 37.07 | -1.41 | BC 225 |
| | | | | Min $V_y$ | -27.01 | -20.53 | -87.31 | 1.22 | 0.54 | 1.58 | BC 431 |
| | | | | Max $V_z$ | -7.38 | -4.52 | -0.79 | -8.34 | -6.00 | 0.25 | BC 363 |
| | | | | Min $V_z$ | 150.81 | -18.12 | -178.82 | -3.13 | 73.36 | -1.51 | BC 154 |
| | | | | Max $M_T$ | 8.36 | -14.26 | -92.64 | 7.79 | 16.65 | 0.91 | BC 445 |
| | | | | Min $M_T$ | 235.66 | -0.80 | -114.82 | -12.84 | 89.08 | -3.90 | BC 138 |
| | | | | Max $M_y$ | 244.83 | -0.97 | -110.82 | -12.19 | 89.63 | -4.09 | BC 131 |
| | | | | Min $M_y$ | -73.70 | -19.46 | -73.47 | 2.75 | -13.00 | 2.38 | BC 475 |
| | | | | Max $M_z$ | -73.70 | -19.46 | -73.47 | 2.75 | -13.00 | 2.38 | BC 475 |
| | | | | Min $M_z$ | 244.83 | -0.97 | -110.82 | -12.19 | 89.63 | -4.09 | BC 131 |
| | | 62 | 4500 | Max N | 59.76 | -2.00 | 27.37 | -7.42 | 28.57 | -1.62 | BC 451 |
| | | | | Min N | -180.71 | 14.13 | 49.15 | -15.64 | -42.18 | 4.16 | BC 206 |
| | | | | Max $V_y$ | -150.73 | 16.94 | 41.57 | -13.09 | -39.37 | 3.60 | BC 442 |
| | | | | Min $V_y$ | -37.44 | -7.12 | 23.58 | -17.12 | 0.92 | 0.82 | BC 141 |
| | | | | Max $V_z$ | -19.31 | 12.41 | 104.93 | -21.48 | 21.00 | 0.59 | BC 271 |
| | | | | Min $V_z$ | -99.35 | 1.86 | -28.91 | -0.78 | -35.06 | 1.86 | BC 362 |
| | | | | Max $M_T$ | -109.47 | 1.65 | -25.19 | -0.17 | -35.93 | 2.06 | BC 358 |
| | | | | Min $M_T$ | -97.42 | 10.18 | 87.08 | -28.42 | -9.17 | 2.67 | BC 148 |
| | | | | Max $M_y$ | 50.51 | -3.24 | 30.96 | -10.11 | 29.06 | -1.47 | BC 259 |
| | | | | Min $M_y$ | -180.71 | 14.13 | 49.15 | -15.64 | -42.18 | 4.16 | BC 206 |
| | | | | Max $M_z$ | -180.71 | 14.13 | 49.15 | -15.64 | -42.18 | 4.16 | BC 206 |
| | | | | Min $M_z$ | 57.07 | -3.34 | 24.78 | -5.61 | 28.38 | -1.62 | BC 391 |
| 111 | RC1 | 64 | 0 | Max N | 54.61 | -4.48 | -40.82 | -17.70 | 36.74 | 0.02 | BC 434 |
| | | | | Min N | -176.37 | -9.97 | -14.20 | -24.36 | -45.40 | 5.78 | BC 203 |
| | | | | Max $V_y$ | -47.80 | 0.38 | -22.04 | -14.46 | -2.29 | 2.52 | BC 393 |
| | | | | Min $V_y$ | -102.69 | -15.89 | -3.47 | -27.64 | -26.89 | 3.62 | BC 255 |
| | | | | Max $V_z$ | -89.30 | -13.16 | 13.20 | -24.79 | -28.39 | 2.66 | BC 411 |
| | | | | Min $V_z$ | -32.41 | -3.95 | -62.15 | -15.81 | 16.40 | 2.96 | BC 234 |
| | | | | Max $M_T$ | -1.61 | -2.90 | -45.09 | -8.22 | 17.71 | 1.50 | BC 422 |
| | | | | Min $M_T$ | -48.79 | -4.22 | -45.36 | -33.06 | 11.58 | 3.26 | BC 140 |
| | | | | Max $M_y$ | 54.61 | -4.48 | -40.82 | -17.70 | 36.74 | 0.02 | BC 434 |
| | | | | Min $M_y$ | -176.03 | -10.31 | -8.21 | -22.14 | -47.77 | 5.70 | BC 167 |
| | | | | Max $M_z$ | -151.66 | -3.88 | -39.23 | -19.60 | -26.14 | 5.97 | BC 200 |
| | | | | Min $M_z$ | 53.02 | -4.62 | -34.58 | -15.41 | 33.87 | -0.01 | BC 446 |
| | | 7 | 4300 | Max N | -22.24 | 15.48 | 6.79 | -23.20 | -19.75 | 1.97 | BC 361 |
| | | | | Min N | -60.99 | 41.55 | 1.18 | -54.31 | -44.48 | 4.57 | BC 154 |
| | | | | Max $V_y$ | -60.99 | 41.55 | 1.18 | -54.31 | -44.48 | 4.57 | BC 154 |
| | | | | Min $V_y$ | -22.24 | 15.48 | 6.79 | -23.20 | -19.75 | 1.97 | BC 361 |
| | | | | Max $V_z$ | -47.66 | 30.49 | 40.97 | -42.31 | -33.42 | 3.54 | BC 172 |
| | | | | Min $V_z$ | -29.81 | 23.30 | -26.19 | -29.67 | -28.50 | 2.75 | BC 473 |
| | | | | Max $M_T$ | -29.07 | 15.81 | 24.14 | -22.70 | -16.49 | 1.77 | BC 363 |
| | | | | Min $M_T$ | -60.98 | 41.54 | 1.03 | -54.33 | -44.49 | 4.57 | BC 155 |
| | | | | Max $M_y$ | -29.07 | 15.81 | 24.14 | -22.70 | -16.49 | 1.77 | BC 363 |
| | | | | Min $M_y$ | -60.98 | 41.54 | 1.03 | -54.33 | -44.49 | 4.57 | BC 155 |
| | | | | Max $M_z$ | -60.98 | 41.54 | 1.03 | -54.33 | -44.49 | 4.57 | BC 155 |
| | | | | Min $M_z$ | -29.07 | 15.81 | 24.14 | -22.70 | -16.49 | 1.77 | BC 363 |
| 112 | RC1 | 83 | 0 | Max N | 11.46 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 268 |
| | | | | Min N | -0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 361 |
| | | | | Max $V_u$ | 4.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 4.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 4.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 4.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 4.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 4.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 4.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 4.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 4.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 4.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 32 | 3957 | Max N | 11.48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 268 |
| | | | | Min N | -0.10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 361 |
| | | | | Max $V_u$ | 4.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 4.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 4.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 4.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 4.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 4.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 4.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 4.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 4.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 4.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 113 | RC1 | 84 | 0 | Max N | 15.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 277 |
| | | | | Min N | 0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 184 |
| | | | | Max $V_u$ | 3.82 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 113 | RC1 | | | Min $V_u$ | 3.82 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 3.82 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 3.82 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 3.82 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 3.82 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 3.82 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 3.82 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 3.82 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 3.82 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 32 | 3957 | Max N | 15.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 277 |
| | | | | Min N | 0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 184 |
| | | | | Max $V_u$ | 3.84 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 3.84 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 3.84 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 3.84 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 3.84 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 3.84 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 3.84 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 3.84 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 3.84 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 3.84 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 114 | RC1 | 68 | 0 | Max N | 33.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 447 |
| | | | | Min N | -0.46 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 362 |
| | | | | Max $V_u$ | -0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 164 | 3967 | Max N | 33.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 447 |
| | | | | Min N | -0.48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 362 |
| | | | | Max $V_u$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 115 | RC1 | 67 | 0 | Max N | 35.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 358 |
| | | | | Min N | -0.46 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 447 |
| | | | | Max $V_u$ | 0.57 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 0.57 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 0.57 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 0.57 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.57 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.57 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 0.57 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 0.57 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 0.57 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 0.57 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 164 | 3967 | Max N | 35.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 358 |
| | | | | Min N | -0.48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 447 |
| | | | | Max $V_u$ | 0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 116 | RC1 | 81 | 0 | Max N | -0.23 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 413 |
| | | | | Min N | -2.39 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_u$ | -1.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -1.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -1.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -1.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -1.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -1.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -1.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -1.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -1.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -1.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 28 | 3957 | Max N | -0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 413 |
| | | | | Min N | -2.37 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_u$ | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 116 | RC1 | | | Max $M_T$ | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 117 | RC1 | 82 | 0 | Max N | -0.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 440 |
| | | | | Min N | -2.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 139 |
| | | | | Max $V_u$ | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 28 | 3957 | Max N | -0.46 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 440 |
| | | | | Min N | -2.28 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 139 |
| | | | | Max $V_u$ | -0.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 118 | RC1 | 85 | 0 | Max N | 56.81 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 146 |
| | | | | Min N | -0.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 474 |
| | | | | Max $V_u$ | 25.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 25.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 25.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 25.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 25.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 25.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 25.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 25.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 25.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 25.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 38 | 3967 | Max N | 56.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 146 |
| | | | | Min N | -0.73 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 474 |
| | | | | Max $V_u$ | 25.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 25.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 25.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 25.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 25.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 25.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 25.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 25.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 25.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 25.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 119 | RC1 | 86 | 0 | Max N | 60.73 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 139 |
| | | | | Min N | -0.56 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 451 |
| | | | | Max $V_u$ | 25.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 25.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 25.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 25.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 25.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 25.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 25.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 25.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 25.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 25.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 38 | 3967 | Max N | 60.70 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 139 |
| | | | | Min N | -0.58 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 451 |
| | | | | Max $V_u$ | 25.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 25.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 25.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 25.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 25.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 25.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 25.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 25.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 25.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 25.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 120 | RC1 | 48 | 0 | Max N | 63.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 414 |
| | | | | Min N | -1.26 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 235 |
| | | | | Max $V_y$ | -0.68 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.68 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.68 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.68 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.68 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.68 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.68 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 120 | RC1 | | | Min $M_y$ | -0.68 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.68 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.68 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 72 | 6255 | Max N | 63.75 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 414 |
| | | | | Min N | -0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 427 |
| | | | | Max $V_y$ | 0.23 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.23 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.23 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.23 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.23 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.23 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.23 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.23 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.23 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.23 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 121 | RC1 | 50 | 0 | Max N | 53.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 235 |
| | | | | Min N | -1.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 210 |
| | | | | Max $V_y$ | 2.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 2.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 2.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 2.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 2.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 2.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 2.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 2.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 2.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 2.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 71 | 6255 | Max N | 53.85 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 235 |
| | | | | Min N | -0.65 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 402 |
| | | | | Max $V_y$ | 3.13 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 3.13 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 3.13 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 3.13 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 3.13 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 3.13 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 3.13 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 3.13 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 3.13 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 3.13 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 122 | RC1 | 71 | 0 | Max N | 38.14 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 414 |
| | | | | Min N | -0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 235 |
| | | | | Max $V_y$ | -0.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 51 | 5704 | Max N | 38.58 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 414 |
| | | | | Min N | -0.39 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 427 |
| | | | | Max $V_y$ | 0.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 123 | RC1 | 72 | 0 | Max N | 36.60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 235 |
| | | | | Min N | -1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 210 |
| | | | | Max $V_y$ | 2.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 2.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 2.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 2.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 2.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 2.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 2.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 2.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 2.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 2.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 49 | 5704 | Max N | 37.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 235 |
| | | | | Min N | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 402 |
| | | | | Max $V_y$ | 2.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 2.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 2.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 2.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 2.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 2.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 2.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 2.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 2.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 2.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 124 | RC1 | 36 | 0 | Max N | 65.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 410 |
| | | | | Min N | -1.23 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 247 |
| | | | | Max $V_y$ | -0.66 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.66 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.66 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.66 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.66 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.66 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.66 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.66 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.66 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.66 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 76 | 6255 | Max N | 65.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 410 |
| | | | | Min N | -0.48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 439 |
| | | | | Max $V_y$ | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 125 | RC1 | 60 | 0 | Max N | 49.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 247 |
| | | | | Min N | -1.39 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 206 |
| | | | | Max $V_y$ | 0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 75 | 6255 | Max N | 50.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 247 |
| | | | | Min N | -0.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 398 |
| | | | | Max $V_y$ | 1.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 1.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 1.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 1.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 1.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 1.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 1.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 1.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 1.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 1.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 126 | RC1 | 75 | 0 | Max N | 39.63 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 410 |
| | | | | Min N | -0.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 247 |
| | | | | Max $V_y$ | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 61 | 5704 | Max N | 40.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 410 |
| | | | | Min N | -0.37 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 439 |
| | | | | Max $V_y$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 127 | RC1 | 76 | 0 | Max N | 34.65 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 247 |
| | | | | Min N | -1.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 206 |
| | | | | Max $V_y$ | 0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 37 | 5704 | Max N | 35.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 247 |
| | | | | Min N | -0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 398 |
| | | | | Max $V_y$ | 1.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 127 | RC1 | | | Min $V_y$ | 1.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 1.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 1.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 1.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 1.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 1.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 1.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 1.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 1.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 128 | RC1 | 52 | 0 | Max N | 56.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 246 |
| | | | | Min N | -1.27 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 219 |
| | | | | Max $V_y$ | 2.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 2.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 2.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 2.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 2.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 2.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 2.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 2.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 2.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 2.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 74 | 6255 | Max N | 56.84 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 246 |
| | | | | Min N | -0.58 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 415 |
| | | | | Max $V_y$ | 2.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 2.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 2.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 2.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 2.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 2.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 2.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 2.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 2.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 2.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 129 | RC1 | 54 | 0 | Max N | 63.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 415 |
| | | | | Min N | -1.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 246 |
| | | | | Max $V_y$ | -0.60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 73 | 6255 | Max N | 63.85 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 415 |
| | | | | Min N | -0.46 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 438 |
| | | | | Max $V_y$ | 0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 130 | RC1 | 73 | 0 | Max N | 36.72 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 246 |
| | | | | Min N | -0.91 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 219 |
| | | | | Max $V_y$ | 1.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 1.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 1.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 1.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 1.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 1.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 1.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 1.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 1.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 1.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 55 | 5704 | Max N | 37.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 246 |
| | | | | Min N | -0.36 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 411 |
| | | | | Max $V_y$ | 2.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 2.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 2.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 2.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 2.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 2.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 2.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 2.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 2.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 2.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 131 | RC1 | 74 | 0 | Max N | 37.27 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 415 |
| | | | | Min N | -0.95 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 246 |
| | | | | Max $V_y$ | -0.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 131 | RC1 | | | Max $M_T$ | -0.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 53 | 5704 | Max N | 37.72 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 415 |
| | | | | Min N | -0.36 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 438 |
| | | | | Max $V_y$ | 0.26 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.26 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.26 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.26 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.26 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.26 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.26 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.26 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.26 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.26 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 132 | RC1 | 62 | 0 | Max N | 55.27 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 234 |
| | | | | Min N | -1.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 223 |
| | | | | Max $V_y$ | 0.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 78 | 6255 | Max N | 56.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 234 |
| | | | | Min N | -0.61 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 415 |
| | | | | Max $V_y$ | 1.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 1.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 1.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 1.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 1.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 1.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 1.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 1.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 1.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 1.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 133 | RC1 | 64 | 0 | Max N | 69.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 415 |
| | | | | Min N | -1.12 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 234 |
| | | | | Max $V_y$ | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 77 | 6255 | Max N | 69.81 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 415 |
| | | | | Min N | -0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 426 |
| | | | | Max $V_y$ | 0.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 134 | RC1 | 77 | 0 | Max N | 35.63 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 234 |
| | | | | Min N | -0.95 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 223 |
| | | | | Max $V_y$ | 0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 65 | 5704 | Max N | 36.29 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 234 |
| | | | | Min N | -0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 415 |
| | | | | Max $V_y$ | 1.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 1.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 1.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 1.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 1.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 1.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 1.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 134 | RC1 | | | Min $M_y$ | 1.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 1.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 1.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 135 | RC1 | 78 | 0 | Max N | 41.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 415 |
| | | | | Min N | -0.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 234 |
| | | | | Max $V_y$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 63 | 5704 | Max N | 41.68 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 415 |
| | | | | Min N | -0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 426 |
| | | | | Max $V_y$ | 0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 136 | RC1 | 44 | 0 | Max N | 67.48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 164 |
| | | | | Min N | -1.29 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Max $V_y$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 70 | 7827 | Max N | 68.29 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 164 |
| | | | | Min N | -0.60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Max $V_y$ | 0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 137 | RC1 | 69 | 0 | Max N | 47.14 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 164 |
| | | | | Min N | -1.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Max $V_y$ | -0.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 39 | 7512 | Max N | 47.84 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 164 |
| | | | | Min N | -0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Max $V_y$ | 0.63 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.63 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.63 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.63 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.63 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.63 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.63 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.63 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.63 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.63 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 138 | RC1 | 47 | 0 | Max N | 67.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min N | -1.29 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 164 |
| | | | | Max $V_y$ | -0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 138 | RC1 | 69 | 7827 | Max N | 67.73 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min N | -0.59 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 356 |
| | | | | Max $V_y$ | 0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 139 | RC1 | 70 | 0 | Max N | 46.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min N | -1.10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 164 |
| | | | | Max $V_y$ | -0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 35 | 7451 | Max N | 46.88 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min N | -0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 356 |
| | | | | Max $V_y$ | 0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 140 | RC1 | 16 | 0 | Max N | -15.73 | 6.17 | -5.88 | -0.00 | 3.94 | 4.68 | BC 447 |
| | | | Links | Min N | -44.70 | -0.01 | 0.17 | 0.00 | -0.64 | -0.02 | BC 138 |
| | | | | Max $V_y$ | -15.74 | 6.19 | -5.95 | -0.00 | 4.18 | 4.76 | BC 423 |
| | | | | Min $V_y$ | -23.25 | -8.81 | 2.97 | 0.00 | 0.70 | -7.30 | BC 220 |
| | | | | Max $V_z$ | -28.91 | -8.79 | 2.99 | 0.00 | 0.63 | -7.23 | BC 240 |
| | | | | Min $V_z$ | -15.74 | 6.19 | -5.95 | -0.00 | 4.20 | 4.74 | BC 363 |
| | | | | Max $M_T$ | -23.25 | -8.78 | 2.92 | 0.00 | 0.87 | -7.22 | BC 168 |
| | | | | Min $M_T$ | -15.73 | 6.16 | -5.88 | -0.00 | 3.95 | 4.65 | BC 475 |
| | | | | Max $M_y$ | -15.74 | 6.19 | -5.95 | -0.00 | 4.20 | 4.74 | BC 363 |
| | | | | Min $M_y$ | -28.79 | -4.88 | -1.14 | 0.00 | -2.91 | -4.04 | BC 269 |
| | | | | Max $M_z$ | -15.74 | 6.19 | -5.95 | -0.00 | 4.18 | 4.76 | BC 423 |
| | | | | Min $M_z$ | -23.25 | -8.81 | 2.97 | 0.00 | 0.70 | -7.30 | BC 220 |
| | | | 0 | Max N | -15.73 | 6.17 | -5.88 | -0.00 | 3.94 | 4.68 | BC 447 |
| | | | Rechts | Min N | -44.70 | -0.01 | 0.17 | 0.00 | -0.64 | -0.02 | BC 138 |
| | | | | Max $V_y$ | -15.74 | 6.19 | -5.95 | -0.00 | 4.18 | 4.76 | BC 423 |
| | | | | Min $V_y$ | -23.25 | -8.81 | 2.97 | 0.00 | 0.70 | -7.30 | BC 220 |
| | | | | Max $V_z$ | -28.91 | -8.79 | 2.99 | 0.00 | 0.63 | -7.23 | BC 240 |
| | | | | Min $V_z$ | -15.74 | 6.19 | -5.95 | -0.00 | 4.20 | 4.74 | BC 363 |
| | | | | Max $M_T$ | -23.25 | -8.78 | 2.92 | 0.00 | 0.87 | -7.22 | BC 168 |
| | | | | Min $M_T$ | -15.73 | 6.16 | -5.88 | -0.00 | 3.95 | 4.65 | BC 475 |
| | | | | Max $M_y$ | -15.74 | 6.19 | -5.95 | -0.00 | 4.20 | 4.74 | BC 363 |
| | | | | Min $M_y$ | -28.79 | -4.88 | -1.14 | 0.00 | -2.91 | -4.04 | BC 269 |
| | | | | Max $M_z$ | -15.74 | 6.19 | -5.95 | -0.00 | 4.18 | 4.76 | BC 423 |
| | | | | Min $M_z$ | -23.25 | -8.81 | 2.97 | 0.00 | 0.70 | -7.30 | BC 220 |
| | | | 3505 | Max N | -7.84 | -3.69 | 3.87 | -0.00 | 0.42 | 0.33 | BC 447 |
| | | | Links | Min N | -33.13 | -0.01 | 0.17 | 0.00 | -0.05 | -0.00 | BC 138 |
| | | | | Max $V_y$ | -13.65 | 4.94 | -3.65 | 0.00 | -0.44 | -0.45 | BC 464 |
| | | | | Min $V_y$ | -17.20 | -3.72 | 3.90 | -0.00 | 0.41 | 0.33 | BC 211 |
| | | | | Max $V_z$ | -17.20 | -3.70 | 3.92 | -0.00 | 0.41 | 0.33 | BC 243 |
| | | | | Min $V_z$ | -7.98 | 4.93 | -3.67 | 0.00 | -0.43 | -0.45 | BC 360 |
| | | | | Max $M_T$ | -11.68 | 4.92 | -3.67 | 0.00 | -0.44 | -0.45 | BC 168 |
| | | | | Min $M_T$ | -7.84 | -3.70 | 3.86 | -0.00 | 0.42 | 0.33 | BC 475 |
| | | | | Max $M_y$ | -7.84 | -3.69 | 3.87 | -0.00 | 0.42 | 0.33 | BC 447 |
| | | | | Min $M_y$ | -17.34 | 4.92 | -3.66 | 0.00 | -0.45 | -0.45 | BC 172 |
| | | | | Max $M_z$ | -11.53 | -3.71 | 3.88 | -0.00 | 0.41 | 0.33 | BC 223 |
| | | | | Min $M_z$ | -13.65 | 4.94 | -3.66 | 0.00 | -0.44 | -0.45 | BC 392 |
| | | 56 | 3505 | Max N | -7.84 | -3.69 | 3.87 | -0.00 | 0.42 | 0.33 | BC 447 |
| | | | Rechts | Min N | -33.13 | -0.01 | 0.17 | 0.00 | -0.05 | -0.00 | BC 138 |
| | | | | Max $V_y$ | -13.65 | 4.94 | -3.65 | 0.00 | -0.44 | -0.45 | BC 464 |
| | | | | Min $V_y$ | -17.20 | -3.72 | 3.90 | -0.00 | 0.41 | 0.33 | BC 211 |
| | | | | Max $V_z$ | -17.20 | -3.70 | 3.92 | -0.00 | 0.41 | 0.33 | BC 243 |
| | | | | Min $V_z$ | -7.98 | 4.93 | -3.67 | 0.00 | -0.43 | -0.45 | BC 360 |
| | | | | Max $M_T$ | -11.68 | 4.92 | -3.67 | 0.00 | -0.44 | -0.45 | BC 168 |
| | | | | Min $M_T$ | -7.84 | -3.70 | 3.86 | -0.00 | 0.42 | 0.33 | BC 475 |
| | | | | Max $M_y$ | -7.84 | -3.69 | 3.87 | -0.00 | 0.42 | 0.33 | BC 447 |
| | | | | Min $M_y$ | -17.34 | 4.92 | -3.66 | 0.00 | -0.45 | -0.45 | BC 172 |
| | | | | Max $M_z$ | -11.53 | -3.71 | 3.88 | -0.00 | 0.41 | 0.33 | BC 223 |
| | | | | Min $M_z$ | -13.65 | 4.94 | -3.66 | 0.00 | -0.44 | -0.45 | BC 392 |
| 141 | RC1 | 79 | 0 | Max N | -24.67 | -0.68 | -2.43 | -0.00 | 46.44 | -1.51 | BC 468 |
| | | | Links | Min N | -80.14 | 0.09 | 0.00 | 0.00 | 0.00 | 0.41 | BC 134 |
| | | | | Max $V_y$ | -48.00 | 0.15 | 2.18 | 0.00 | -43.84 | 0.57 | BC 243 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 141 | RC1 | | | Min $V_y$ | -24.71 | -0.77 | -2.44 | -0.00 | 46.38 | -1.69 | BC 360 |
| | | | | Max $V_z$ | -36.38 | 0.14 | 2.18 | 0.00 | -43.84 | 0.51 | BC 435 |
| | | | | Min $V_z$ | -36.33 | -0.76 | -2.45 | -0.00 | 46.38 | -1.65 | BC 168 |
| | | | | Max $M_T$ | -24.95 | 0.07 | 2.18 | 0.00 | -43.85 | 0.26 | BC 363 |
| | | | | Min $M_T$ | -45.82 | -0.09 | -2.12 | -0.00 | 42.68 | 1.55 | BC 281 |
| | | | | Max $M_y$ | -47.77 | -0.64 | -2.43 | -0.00 | 46.47 | -1.40 | BC 240 |
| | | | | Min $M_y$ | -36.57 | 0.08 | 2.18 | 0.00 | -43.85 | 0.31 | BC 167 |
| | | | | Max $M_z$ | -57.53 | -0.10 | -2.12 | -0.00 | 42.68 | 1.59 | BC 269 |
| | | | | Min $M_z$ | -24.71 | -0.77 | -2.44 | -0.00 | 46.38 | -1.69 | BC 360 |
| | | | 0 | Max N | -24.67 | -0.68 | -2.43 | -0.00 | 46.44 | -1.51 | BC 468 |
| | | | Rechts | Min N | -80.14 | 0.09 | 0.00 | 0.00 | 0.00 | 0.41 | BC 134 |
| | | | | Max $V_y$ | -48.00 | 0.15 | 2.18 | 0.00 | -43.84 | 0.57 | BC 243 |
| | | | | Min $V_y$ | -24.71 | -0.77 | -2.44 | -0.00 | 46.38 | -1.69 | BC 360 |
| | | | | Max $V_z$ | -36.38 | 0.14 | 2.18 | 0.00 | -43.84 | 0.51 | BC 435 |
| | | | | Min $V_z$ | -36.33 | -0.76 | -2.45 | -0.00 | 46.38 | -1.65 | BC 168 |
| | | | | Max $M_T$ | -24.95 | 0.07 | 2.18 | 0.00 | -43.85 | 0.26 | BC 363 |
| | | | | Min $M_T$ | -45.82 | -0.09 | -2.12 | -0.00 | 42.68 | 1.55 | BC 281 |
| | | | | Max $M_y$ | -47.77 | -0.64 | -2.43 | -0.00 | 46.47 | -1.40 | BC 240 |
| | | | | Min $M_y$ | -36.57 | 0.08 | 2.18 | 0.00 | -43.85 | 0.31 | BC 167 |
| | | | | Max $M_z$ | -57.53 | -0.10 | -2.12 | -0.00 | 42.68 | 1.59 | BC 269 |
| | | | | Min $M_z$ | -24.71 | -0.77 | -2.44 | -0.00 | 46.38 | -1.69 | BC 360 |
| | | | 3565 | Max N | -15.58 | -0.68 | -23.96 | -0.00 | -0.61 | 0.92 | BC 468 |
| | | | Links | Min N | -66.80 | 0.09 | 0.00 | 0.00 | 0.00 | 0.11 | BC 134 |
| | | | | Max $V_y$ | -34.66 | 0.15 | 22.31 | 0.00 | -0.19 | 0.02 | BC 243 |
| | | | | Min $V_y$ | -15.62 | -0.77 | -23.97 | -0.00 | -0.71 | 1.05 | BC 360 |
| | | | | Max $V_z$ | -15.82 | 0.13 | 22.31 | 0.00 | -0.19 | -0.01 | BC 447 |
| | | | | Min $V_z$ | -22.99 | -0.76 | -23.97 | -0.00 | -0.71 | 1.06 | BC 168 |
| | | | | Max $M_T$ | -15.86 | 0.07 | 22.31 | 0.00 | -0.20 | 0.01 | BC 363 |
| | | | | Min $M_T$ | -32.48 | -0.09 | -21.71 | -0.00 | 0.20 | 1.88 | BC 281 |
| | | | | Max $M_y$ | -38.05 | -0.21 | -21.71 | -0.00 | 0.20 | 2.20 | BC 433 |
| | | | | Min $M_y$ | -22.99 | -0.76 | -23.97 | -0.00 | -0.71 | 1.06 | BC 168 |
| | | | | Max $M_z$ | -40.82 | -0.48 | -21.71 | -0.00 | 0.20 | 2.76 | BC 377 |
| | | | | Min $M_z$ | -15.81 | 0.12 | 22.31 | 0.00 | -0.19 | -0.01 | BC 443 |
| | | | 3565 | Max N | -15.58 | -0.68 | -23.96 | -0.00 | -0.61 | 0.92 | BC 468 |
| | | | Rechts | Min N | -66.80 | 0.09 | 0.00 | 0.00 | 0.00 | 0.11 | BC 134 |
| | | | | Max $V_y$ | -34.66 | 0.15 | 22.31 | 0.00 | -0.19 | 0.02 | BC 243 |
| | | | | Min $V_y$ | -15.62 | -0.77 | -23.97 | -0.00 | -0.71 | 1.05 | BC 360 |
| | | | | Max $V_z$ | -15.82 | 0.13 | 22.31 | 0.00 | -0.19 | -0.01 | BC 447 |
| | | | | Min $V_z$ | -22.99 | -0.76 | -23.97 | -0.00 | -0.71 | 1.06 | BC 168 |
| | | | | Max $M_T$ | -15.86 | 0.07 | 22.31 | 0.00 | -0.20 | 0.01 | BC 363 |
| | | | | Min $M_T$ | -32.48 | -0.09 | -21.71 | -0.00 | 0.19 | 1.88 | BC 281 |
| | | | | Max $M_y$ | -38.05 | -0.21 | -21.71 | -0.00 | 0.20 | 2.20 | BC 433 |
| | | | | Min $M_y$ | -22.99 | -0.76 | -23.97 | -0.00 | -0.71 | 1.06 | BC 168 |
| | | | | Max $M_z$ | -40.82 | -0.48 | -21.71 | -0.00 | 0.20 | 2.76 | BC 377 |
| | | | | Min $M_z$ | -15.81 | 0.12 | 22.31 | 0.00 | -0.19 | -0.01 | BC 443 |
| | | | 3625 | Max N | -15.45 | -0.68 | -24.32 | -0.00 | -2.06 | 0.96 | BC 468 |
| | | | Links | Min N | -66.61 | 0.09 | 0.00 | 0.00 | 0.00 | 0.10 | BC 134 |
| | | | | Max $V_y$ | -34.48 | 0.15 | 22.65 | 0.00 | 1.16 | 0.01 | BC 243 |
| | | | | Min $V_y$ | -15.49 | -0.77 | -24.34 | -0.00 | -2.16 | 1.09 | BC 360 |
| | | | | Max $V_z$ | -15.69 | 0.13 | 22.65 | 0.00 | 1.16 | -0.02 | BC 447 |
| | | | | Min $V_z$ | -22.80 | -0.76 | -24.34 | -0.00 | -2.16 | 1.10 | BC 168 |
| | | | | Max $M_T$ | -15.73 | 0.07 | 22.65 | 0.00 | 1.15 | 0.01 | BC 363 |
| | | | | Min $M_T$ | -32.29 | -0.09 | -22.04 | -0.00 | -1.12 | 1.88 | BC 281 |
| | | | | Max $M_y$ | -27.16 | 0.14 | 22.65 | 0.00 | 1.16 | 0.01 | BC 435 |
| | | | | Min $M_y$ | -22.80 | -0.76 | -24.34 | -0.00 | -2.16 | 1.10 | BC 168 |
| | | | | Max $M_z$ | -40.70 | -0.48 | -22.04 | -0.00 | -1.12 | 2.79 | BC 377 |
| | | | | Min $M_z$ | -15.69 | 0.13 | 22.65 | 0.00 | 1.16 | -0.02 | BC 447 |
| | | 41 | 3625 | Max N | -15.45 | -0.68 | -24.32 | -0.00 | -2.06 | 0.96 | BC 468 |
| | | | Rechts | Min N | -66.61 | 0.09 | 0.00 | 0.00 | 0.00 | 0.10 | BC 134 |
| | | | | Max $V_y$ | -34.48 | 0.15 | 22.65 | 0.00 | 1.16 | 0.01 | BC 243 |
| | | | | Min $V_y$ | -15.49 | -0.77 | -24.34 | -0.00 | -2.16 | 1.09 | BC 360 |
| | | | | Max $V_z$ | -15.69 | 0.13 | 22.65 | 0.00 | 1.16 | -0.02 | BC 447 |
| | | | | Min $V_z$ | -22.80 | -0.76 | -24.34 | -0.00 | -2.16 | 1.10 | BC 168 |
| | | | | Max $M_T$ | -15.73 | 0.07 | 22.65 | 0.00 | 1.15 | 0.01 | BC 363 |
| | | | | Min $M_T$ | -32.29 | -0.09 | -22.04 | -0.00 | -1.12 | 1.88 | BC 281 |
| | | | | Max $M_y$ | -27.16 | 0.14 | 22.65 | 0.00 | 1.16 | 0.01 | BC 435 |
| | | | | Min $M_y$ | -22.80 | -0.76 | -24.34 | -0.00 | -2.16 | 1.10 | BC 168 |
| | | | | Max $M_z$ | -40.70 | -0.48 | -22.04 | -0.00 | -1.12 | 2.79 | BC 377 |
| | | | | Min $M_z$ | -15.69 | 0.13 | 22.65 | 0.00 | 1.16 | -0.02 | BC 447 |
| 142 | RC1 | 74 | 0 | Max N | -39.34 | -0.25 | 1.90 | 0.00 | -33.62 | -0.74 | BC 415 |
| | | | | Min N | -155.36 | -0.32 | -0.09 | 0.00 | -0.41 | -0.15 | BC 149 |
| | | | | Max $V_y$ | -82.60 | 0.09 | -2.49 | 0.00 | 25.50 | 0.37 | BC 212 |
| | | | | Min $V_y$ | -104.93 | -0.87 | 1.64 | -0.00 | -20.28 | -0.35 | BC 246 |
| | | | | Max $V_z$ | -81.52 | -0.24 | 2.10 | 0.00 | -32.78 | -0.73 | BC 243 |
| | | | | Min $V_z$ | -82.60 | 0.09 | -2.50 | 0.00 | 25.48 | 0.37 | BC 200 |
| | | | | Max $M_T$ | -81.54 | 0.03 | 1.26 | 0.00 | -17.25 | 0.21 | BC 241 |
| | | | | Min $M_T$ | -51.53 | -0.36 | 1.67 | -0.00 | -20.16 | -0.01 | BC 446 |
| | | | | Max $M_y$ | -59.05 | 0.06 | -2.45 | -0.00 | 25.71 | 0.22 | BC 252 |
| | | | | Min $M_y$ | -39.48 | -0.21 | 1.89 | 0.00 | -33.67 | -0.60 | BC 419 |
| | | | | Max $M_z$ | -82.60 | 0.09 | -2.49 | 0.00 | 25.50 | 0.37 | BC 212 |
| | | | | Min $M_z$ | -81.50 | -0.25 | 2.08 | 0.00 | -32.86 | -0.76 | BC 211 |
| | | 55 | 3505 | Max N | -32.38 | -0.25 | 17.46 | 0.00 | 0.31 | 0.15 | BC 415 |
| | | | | Min N | -145.15 | -0.32 | -0.09 | 0.00 | -0.74 | 0.96 | BC 149 |
| | | | | Max $V_y$ | -72.39 | 0.09 | -15.99 | 0.00 | -6.89 | 0.04 | BC 212 |
| | | | | Min $V_y$ | -94.72 | -0.87 | 11.82 | -0.00 | 3.31 | 2.72 | BC 246 |
| | | | | Max $V_z$ | -71.31 | -0.24 | 17.65 | 0.00 | 1.82 | 0.11 | BC 243 |
| | | | | Min $V_z$ | -72.39 | 0.09 | -15.99 | 0.00 | -6.91 | 0.04 | BC 200 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 142 | RC1 | | | Max $M_T$ | -71.33 | 0.03 | 9.69 | 0.00 | 1.93 | 0.10 | BC 241 |
| | | | | Min $M_T$ | -44.56 | -0.36 | 11.85 | -0.00 | 3.55 | 1.24 | BC 446 |
| | | | | Max $M_y$ | -53.34 | -0.76 | 11.85 | -0.00 | 3.55 | 2.36 | BC 450 |
| | | | | Min $M_y$ | -72.39 | 0.09 | -15.99 | 0.00 | -6.91 | 0.04 | BC 200 |
| | | | | Max $M_z$ | -94.72 | -0.87 | 11.82 | -0.00 | 3.31 | 2.72 | BC 246 |
| | | | | Min $M_z$ | -54.72 | -0.01 | -0.04 | -0.00 | -0.28 | -0.03 | BC 15 |
| 143 | RC1 | 72 | 0 | Max N | -63.60 | -0.04 | 0.68 | -0.00 | -20.26 | -0.04 | BC 421 |
| | | | | Min N | -233.71 | 0.26 | -1.71 | -0.02 | -7.44 | 0.34 | BC 140 |
| | | | | Max $V_y$ | -231.63 | 0.33 | -1.71 | -0.02 | -7.45 | 0.34 | BC 147 |
| | | | | Min $V_y$ | -88.57 | -0.66 | 2.33 | -0.01 | -27.02 | -0.10 | BC 414 |
| | | | | Max $V_z$ | -88.40 | -0.66 | 2.33 | -0.01 | -27.02 | -0.09 | BC 410 |
| | | | | Min $V_z$ | -131.04 | 0.03 | -3.53 | -0.01 | 21.81 | -0.03 | BC 244 |
| | | | | Max $M_T$ | -64.98 | -0.05 | -3.05 | -0.00 | 23.91 | -0.08 | BC 360 |
| | | | | Min $M_T$ | -233.71 | 0.26 | -1.71 | -0.02 | -7.44 | 0.34 | BC 140 |
| | | | | Max $M_y$ | -74.19 | -0.42 | -3.01 | -0.00 | 24.07 | -0.23 | BC 408 |
| | | | | Min $M_y$ | -129.55 | -0.14 | 1.03 | -0.00 | -32.46 | -0.40 | BC 247 |
| | | | | Max $M_z$ | -233.08 | 0.29 | -1.71 | -0.02 | -7.43 | 0.37 | BC 154 |
| | | | | Min $M_z$ | -129.55 | -0.14 | 1.03 | -0.00 | -32.46 | -0.40 | BC 235 |
| | | 51 | 3505 | Max N | -56.54 | -0.04 | 9.31 | -0.00 | -2.76 | 0.09 | BC 421 |
| | | | | Min N | -223.36 | 0.26 | -1.71 | -0.02 | -13.44 | -0.56 | BC 140 |
| | | | | Max $V_y$ | -221.28 | 0.33 | -1.71 | -0.02 | -13.46 | -0.82 | BC 147 |
| | | | | Min $V_y$ | -81.52 | -0.66 | 16.13 | -0.01 | 5.34 | 2.23 | BC 414 |
| | | | | Max $V_z$ | -81.34 | -0.66 | 16.13 | -0.01 | 5.35 | 2.21 | BC 410 |
| | | | | Min $V_z$ | -120.70 | 0.03 | -17.33 | -0.01 | -14.76 | -0.14 | BC 244 |
| | | | | Max $M_T$ | -57.92 | -0.05 | -16.85 | -0.00 | -10.95 | 0.09 | BC 360 |
| | | | | Min $M_T$ | -223.36 | 0.26 | -1.71 | -0.02 | -13.44 | -0.56 | BC 140 |
| | | | | Max $M_y$ | -81.34 | -0.66 | 16.13 | -0.01 | 5.35 | 2.21 | BC 410 |
| | | | | Min $M_y$ | -120.70 | 0.03 | -17.33 | -0.01 | -14.76 | -0.14 | BC 244 |
| | | | | Max $M_z$ | -81.52 | -0.66 | 16.13 | -0.01 | 5.34 | 2.23 | BC 414 |
| | | | | Min $M_z$ | -221.00 | 0.30 | -1.73 | -0.02 | -13.56 | -0.84 | BC 138 |
| 144 | RC1 | 90 | 0 | Max N | 28.01 | 0.13 | 0.00 | -0.00 | 0.00 | 0.00 | BC 389 |
| | | | | Min N | -80.69 | -0.08 | 0.00 | -0.00 | 0.00 | 0.00 | BC 264 |
| | | | | Max $V_y$ | 22.54 | 0.17 | 0.00 | -0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min $V_y$ | -70.53 | -0.11 | 0.00 | -0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Max $V_z$ | 27.55 | 0.13 | 0.00 | -0.00 | 0.00 | 0.00 | BC 377 |
| | | | | Min $V_z$ | -15.83 | 0.04 | -0.00 | 0.00 | 0.00 | 0.00 | BC 267 |
| | | | | Max $M_T$ | -12.58 | 0.03 | -0.00 | 0.00 | 0.00 | 0.00 | BC 443 |
| | | | | Min $M_T$ | 24.15 | 0.14 | 0.00 | -0.00 | 0.00 | 0.00 | BC 185 |
| | | | | Max $M_y$ | -12.06 | 0.04 | -0.00 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -12.06 | 0.04 | -0.00 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -11.56 | 0.06 | -0.00 | 0.00 | 0.00 | 0.00 | BC 91 |
| | | | | Min $M_z$ | -7.89 | 0.05 | -0.00 | 0.00 | 0.00 | -0.00 | BC 53 |
| | | 91 | 2173 | Max N | 28.70 | 0.13 | 0.00 | -0.00 | 0.00 | -0.27 | BC 389 |
| | | | | Min N | -79.67 | -0.08 | 0.00 | -0.00 | 0.00 | 0.18 | BC 264 |
| | | | | Max $V_y$ | 23.56 | 0.17 | 0.00 | -0.00 | 0.00 | -0.37 | BC 241 |
| | | | | Min $V_y$ | -69.84 | -0.11 | 0.00 | -0.00 | 0.00 | 0.24 | BC 360 |
| | | | | Max $V_z$ | 28.25 | 0.13 | 0.00 | -0.00 | 0.00 | -0.28 | BC 377 |
| | | | | Min $V_z$ | -14.81 | 0.04 | -0.00 | 0.00 | -0.00 | -0.09 | BC 267 |
| | | | | Max $M_T$ | -11.88 | 0.03 | -0.00 | 0.00 | -0.00 | -0.06 | BC 443 |
| | | | | Min $M_T$ | 25.17 | 0.14 | 0.00 | -0.00 | 0.00 | -0.31 | BC 185 |
| | | | | Max $M_y$ | 28.25 | 0.13 | 0.00 | -0.00 | 0.00 | -0.28 | BC 377 |
| | | | | Min $M_y$ | -14.81 | 0.04 | -0.00 | 0.00 | -0.00 | -0.09 | BC 267 |
| | | | | Max $M_z$ | -69.84 | -0.11 | 0.00 | -0.00 | 0.00 | 0.24 | BC 360 |
| | | | | Min $M_z$ | 23.56 | 0.17 | 0.00 | -0.00 | 0.00 | -0.37 | BC 241 |
| 145 | RC1 | 73 | 0 | Max N | -40.15 | 0.14 | 1.60 | 0.00 | -30.00 | 0.39 | BC 422 |
| | | | | Min N | -150.61 | 0.02 | -0.17 | 0.00 | -0.74 | 0.11 | BC 140 |
| | | | | Max $V_y$ | -63.72 | 0.81 | 2.27 | 0.00 | -27.31 | 0.19 | BC 415 |
| | | | | Min $V_y$ | -67.37 | -0.00 | -0.04 | 0.00 | -0.17 | 0.04 | BC 1 |
| | | | | Max $V_z$ | -63.73 | 0.81 | 2.27 | 0.00 | -27.31 | 0.19 | BC 411 |
| | | | | Min $V_z$ | -83.75 | 0.02 | -2.36 | 0.00 | 26.90 | 0.14 | BC 244 |
| | | | | Max $M_T$ | -54.63 | 0.43 | 2.26 | 0.00 | -27.32 | 0.02 | BC 419 |
| | | | | Min $M_T$ | -45.21 | 0.22 | 0.84 | 0.00 | -19.59 | 0.08 | BC 445 |
| | | | | Max $M_y$ | -51.64 | 0.46 | -2.30 | 0.00 | 27.15 | 0.31 | BC 408 |
| | | | | Min $M_y$ | -40.26 | 0.11 | 1.55 | 0.00 | -30.21 | 0.30 | BC 446 |
| | | | | Max $M_z$ | -83.02 | 0.14 | 1.72 | 0.00 | -29.47 | 0.45 | BC 234 |
| | | | | Min $M_z$ | -93.02 | 0.24 | 2.23 | 0.00 | -27.46 | -0.14 | BC 247 |
| | | 53 | 3505 | Max N | -33.09 | 0.14 | 15.32 | 0.00 | -0.35 | -0.09 | BC 422 |
| | | | | Min N | -140.26 | 0.02 | -0.17 | 0.00 | -1.34 | 0.05 | BC 140 |
| | | | | Max $V_y$ | -56.66 | 0.81 | 16.06 | 0.00 | 4.81 | -2.65 | BC 415 |
| | | | | Min $V_y$ | -55.69 | -0.00 | -0.04 | 0.00 | -0.30 | 0.05 | BC 1 |
| | | | | Max $V_z$ | -56.67 | 0.81 | 16.06 | 0.00 | 4.81 | -2.65 | BC 411 |
| | | | | Min $V_z$ | -73.40 | 0.02 | -16.16 | 0.00 | -5.56 | 0.05 | BC 244 |
| | | | | Max $M_T$ | -47.57 | 0.43 | 16.06 | 0.00 | 4.80 | -1.50 | BC 419 |
| | | | | Min $M_T$ | -38.15 | 0.22 | 9.46 | 0.00 | -1.54 | -0.68 | BC 445 |
| | | | | Max $M_y$ | -56.67 | 0.81 | 16.06 | 0.00 | 4.81 | -2.65 | BC 411 |
| | | | | Min $M_y$ | -73.40 | 0.02 | -16.16 | 0.00 | -5.56 | 0.05 | BC 244 |
| | | | | Max $M_z$ | -140.21 | 0.01 | -0.13 | 0.00 | -1.06 | 0.07 | BC 138 |
| | | | | Min $M_z$ | -56.66 | 0.81 | 16.06 | 0.00 | 4.81 | -2.65 | BC 415 |
| 146 | RC1 | 80 | 0 | Max N | 20.62 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 356 |
| | | | | Min N | -0.90 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Max $V_y$ | -0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 146 | RC1 | | | Min $M_y$ | -0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 57 | 7411 | Max N | 21.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 356 |
| | | | | Min N | -0.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Max $V_y$ | 0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 147 | RC1 | 17 | 0 | Max N | 39.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min N | -0.57 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 168 |
| | | | | Max $V_y$ | 7.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 7.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 7.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 7.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 7.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 7.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 7.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 7.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 7.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 7.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 42 | 7529 | Max N | 39.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min N | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 356 |
| | | | | Max $V_y$ | 8.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 8.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 8.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 8.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 8.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 8.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 8.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 8.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 8.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 8.17 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 148 | RC1 | 92 | 0 | Max N | -0.01 | 0.00 | 0.27 | 0.00 | 0.00 | 0.00 | BC 326 |
| | | | | Min N | -25.76 | 0.00 | 0.39 | 0.00 | -0.00 | 0.00 | BC 264 |
| | | | | Max $V_y$ | -1.31 | 0.00 | 0.44 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -1.31 | 0.00 | 0.44 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.13 | 0.00 | 0.44 | 0.00 | 0.00 | 0.00 | BC 7 |
| | | | | Min $V_z$ | -24.97 | 0.00 | 0.27 | 0.00 | 0.00 | 0.00 | BC 428 |
| | | | | Max $M_T$ | -22.19 | 0.00 | 0.39 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min $M_T$ | -0.42 | 0.00 | 0.27 | -0.00 | 0.00 | 0.00 | BC 391 |
| | | | | Max $M_y$ | -1.54 | 0.00 | 0.44 | 0.00 | 0.00 | 0.00 | BC 2 |
| | | | | Min $M_y$ | -1.31 | 0.00 | 0.44 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -1.31 | 0.00 | 0.44 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -1.31 | 0.00 | 0.44 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | 91 | 1665 | Max N | -0.01 | 0.00 | -0.27 | 0.00 | 0.00 | 0.00 | BC 326 |
| | | | | Min N | -25.76 | 0.00 | -0.39 | 0.00 | -0.00 | 0.00 | BC 264 |
| | | | | Max $V_y$ | -1.31 | 0.00 | -0.44 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -1.31 | 0.00 | -0.44 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -24.97 | 0.00 | -0.27 | 0.00 | 0.00 | 0.00 | BC 428 |
| | | | | Min $V_z$ | -0.13 | 0.00 | -0.44 | 0.00 | 0.00 | 0.00 | BC 7 |
| | | | | Max $M_T$ | -22.19 | 0.00 | -0.39 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min $M_T$ | -0.42 | 0.00 | -0.27 | -0.00 | 0.00 | 0.00 | BC 391 |
| | | | | Max $M_y$ | -1.54 | 0.00 | -0.44 | 0.00 | 0.00 | 0.00 | BC 2 |
| | | | | Min $M_y$ | -1.31 | 0.00 | -0.44 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -1.31 | 0.00 | -0.44 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -1.31 | 0.00 | -0.44 | 0.00 | -0.00 | 0.00 | BC 1 |
| 149 | RC1 | 71 | 0 | Max N | -62.19 | 0.02 | 0.94 | -0.00 | -18.64 | -0.00 | BC 413 |
| | | | | Min N | -232.89 | -0.06 | -1.74 | 0.02 | -7.54 | -0.21 | BC 146 |
| | | | | Max $V_y$ | -151.45 | 0.62 | 1.65 | 0.02 | -20.24 | 0.18 | BC 235 |
| | | | | Min $V_y$ | -226.59 | -0.33 | -1.78 | 0.02 | -7.74 | -0.37 | BC 148 |
| | | | | Max $V_z$ | -84.02 | 0.58 | 1.71 | 0.01 | -19.97 | 0.19 | BC 451 |
| | | | | Min $V_z$ | -128.95 | -0.22 | -3.59 | 0.01 | 20.73 | -0.39 | BC 204 |
| | | | | Max $M_T$ | -232.72 | -0.07 | -1.74 | 0.02 | -7.55 | -0.22 | BC 149 |
| | | | | Min $M_T$ | -62.55 | 0.21 | 1.68 | -0.00 | -34.57 | 0.54 | BC 390 |
| | | | | Max $M_y$ | -66.87 | -0.03 | -3.07 | 0.00 | 23.00 | -0.28 | BC 448 |
| | | | | Min $M_y$ | -127.04 | 0.25 | 1.35 | -0.00 | -36.02 | 0.66 | BC 206 |
| | | | | Max $M_z$ | -62.37 | 0.26 | 1.64 | -0.00 | -34.78 | 0.71 | BC 414 |
| | | | | Min $M_z$ | -128.97 | -0.24 | -3.58 | 0.01 | 20.76 | -0.49 | BC 236 |
| | | 49 | 3505 | Max N | -55.22 | 0.02 | 9.37 | -0.00 | -0.58 | -0.09 | BC 413 |
| | | | | Min N | -222.68 | -0.06 | -1.74 | 0.02 | -13.63 | -0.00 | BC 146 |
| | | | | Max $V_y$ | -141.24 | 0.62 | 11.83 | 0.02 | 3.38 | -2.00 | BC 235 |
| | | | | Min $V_y$ | -216.38 | -0.33 | -1.78 | 0.02 | -13.99 | 0.78 | BC 148 |
| | | | | Max $V_z$ | -55.59 | 0.21 | 17.24 | -0.00 | -1.40 | -0.20 | BC 450 |
| | | | | Min $V_z$ | -118.74 | -0.22 | -17.08 | 0.01 | -15.50 | 0.36 | BC 204 |
| | | | | Max $M_T$ | -222.51 | -0.07 | -1.74 | 0.02 | -13.64 | 0.02 | BC 149 |
| | | | | Min $M_T$ | -55.58 | 0.21 | 17.24 | -0.00 | -1.42 | -0.20 | BC 390 |
| | | | | Max $M_y$ | -77.06 | 0.58 | 11.90 | 0.01 | 3.88 | -1.84 | BC 451 |
| | | | | Min $M_y$ | -118.74 | -0.22 | -17.08 | 0.01 | -15.50 | 0.36 | BC 204 |
| | | | | Max $M_z$ | -216.38 | -0.33 | -1.78 | 0.02 | -13.99 | 0.78 | BC 148 |
| | | | | Min $M_z$ | -141.24 | 0.62 | 11.83 | 0.02 | 3.38 | -2.00 | BC 235 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 150 | RC1 | 9 | 0 | Max N | -15.72 | -6.21 | -6.11 | 0.00 | 4.74 | -4.81 | BC 422 |
| | | | Links | Min N | -44.64 | -0.06 | -0.28 | -0.00 | 0.87 | -0.20 | BC 133 |
| | | | | Max $V_y$ | -15.84 | 8.78 | 3.62 | -0.00 | -1.48 | 7.22 | BC 412 |
| | | | | Min $V_y$ | -28.74 | -6.22 | -6.17 | 0.00 | 4.93 | -4.86 | BC 234 |
| | | | | Max $V_z$ | -15.84 | 8.77 | 3.70 | -0.00 | -1.76 | 7.18 | BC 356 |
| | | | | Min $V_z$ | -28.74 | -6.19 | -6.25 | 0.00 | 5.18 | -4.75 | BC 266 |
| | | | | Max $M_T$ | -15.72 | -6.18 | -6.19 | 0.00 | 5.01 | -4.70 | BC 474 |
| | | | | Min $M_T$ | -28.86 | 8.76 | 3.63 | -0.00 | -1.54 | 7.15 | BC 200 |
| | | | | Max $M_y$ | -23.09 | -6.18 | -6.25 | 0.00 | 5.18 | -4.70 | BC 278 |
| | | | | Min $M_y$ | -15.84 | 8.77 | 3.70 | -0.00 | -1.76 | 7.18 | BC 356 |
| | | | | Max $M_z$ | -15.84 | 8.78 | 3.62 | -0.00 | -1.48 | 7.22 | BC 412 |
| | | | | Min $M_z$ | -28.74 | -6.22 | -6.17 | 0.00 | 4.93 | -4.86 | BC 234 |
| | | | 0 | Max N | -15.72 | -6.21 | -6.11 | 0.00 | 4.74 | -4.81 | BC 422 |
| | | | Rechts | Min N | -44.64 | -0.06 | -0.28 | -0.00 | 0.87 | -0.20 | BC 133 |
| | | | | Max $V_y$ | -15.84 | 8.78 | 3.62 | -0.00 | -1.48 | 7.22 | BC 412 |
| | | | | Min $V_y$ | -28.74 | -6.22 | -6.17 | 0.00 | 4.93 | -4.86 | BC 234 |
| | | | | Max $V_z$ | -15.84 | 8.77 | 3.70 | -0.00 | -1.76 | 7.18 | BC 356 |
| | | | | Min $V_z$ | -28.74 | -6.19 | -6.25 | 0.00 | 5.18 | -4.75 | BC 266 |
| | | | | Max $M_T$ | -15.72 | -6.18 | -6.19 | 0.00 | 5.01 | -4.70 | BC 474 |
| | | | | Min $M_T$ | -28.86 | 8.76 | 3.63 | -0.00 | -1.54 | 7.15 | BC 200 |
| | | | | Max $M_y$ | -23.09 | -6.18 | -6.25 | 0.00 | 5.18 | -4.70 | BC 278 |
| | | | | Min $M_y$ | -15.84 | 8.77 | 3.70 | -0.00 | -1.76 | 7.18 | BC 356 |
| | | | | Max $M_z$ | -15.84 | 8.78 | 3.62 | -0.00 | -1.48 | 7.22 | BC 412 |
| | | | | Min $M_z$ | -28.74 | -6.22 | -6.17 | 0.00 | 4.93 | -4.86 | BC 234 |
| | | | 3505 | Max N | -7.83 | 3.65 | 3.63 | 0.00 | 0.39 | -0.33 | BC 422 |
| | | | Links | Min N | -33.07 | -0.06 | -0.28 | -0.00 | -0.10 | 0.01 | BC 133 |
| | | | | Max $V_y$ | -7.83 | 3.69 | 3.56 | 0.00 | 0.38 | -0.33 | BC 414 |
| | | | | Min $V_y$ | -17.29 | -4.98 | -3.06 | -0.00 | -0.38 | 0.46 | BC 236 |
| | | | | Max $V_z$ | -7.83 | 3.66 | 3.64 | 0.00 | 0.39 | -0.33 | BC 390 |
| | | | | Min $V_z$ | -17.29 | -4.98 | -3.06 | -0.00 | -0.38 | 0.46 | BC 240 |
| | | | | Max $M_T$ | -7.83 | 3.69 | 3.55 | 0.00 | 0.38 | -0.33 | BC 474 |
| | | | | Min $M_T$ | -17.29 | -4.94 | -2.96 | -0.00 | -0.37 | 0.45 | BC 200 |
| | | | | Max $M_y$ | -7.83 | 3.66 | 3.64 | 0.00 | 0.39 | -0.33 | BC 390 |
| | | | | Min $M_y$ | -17.29 | -4.98 | -3.06 | -0.00 | -0.38 | 0.46 | BC 240 |
| | | | | Max $M_z$ | -17.29 | -4.98 | -3.06 | -0.00 | -0.38 | 0.46 | BC 236 |
| | | | | Min $M_z$ | -7.83 | 3.69 | 3.56 | 0.00 | 0.38 | -0.33 | BC 414 |
| | | 45 | 3505 | Max N | -7.83 | 3.65 | 3.63 | 0.00 | 0.39 | -0.33 | BC 422 |
| | | | Rechts | Min N | -33.07 | -0.06 | -0.28 | -0.00 | -0.10 | 0.01 | BC 133 |
| | | | | Max $V_y$ | -7.83 | 3.69 | 3.56 | 0.00 | 0.38 | -0.33 | BC 414 |
| | | | | Min $V_y$ | -17.29 | -4.98 | -3.06 | -0.00 | -0.38 | 0.46 | BC 236 |
| | | | | Max $V_z$ | -7.83 | 3.66 | 3.64 | 0.00 | 0.39 | -0.33 | BC 390 |
| | | | | Min $V_z$ | -17.29 | -4.98 | -3.06 | -0.00 | -0.38 | 0.46 | BC 240 |
| | | | | Max $M_T$ | -7.83 | 3.69 | 3.55 | 0.00 | 0.38 | -0.33 | BC 474 |
| | | | | Min $M_T$ | -17.29 | -4.94 | -2.96 | -0.00 | -0.37 | 0.45 | BC 200 |
| | | | | Max $M_y$ | -7.83 | 3.66 | 3.64 | 0.00 | 0.39 | -0.33 | BC 390 |
| | | | | Min $M_y$ | -17.29 | -4.98 | -3.06 | -0.00 | -0.38 | 0.46 | BC 240 |
| | | | | Max $M_z$ | -17.29 | -4.98 | -3.06 | -0.00 | -0.38 | 0.46 | BC 236 |
| | | | | Min $M_z$ | -7.83 | 3.69 | 3.56 | 0.00 | 0.38 | -0.33 | BC 414 |
| 151 | RC1 | 69 | 0 | Max N | -24.58 | -0.53 | 2.45 | 0.00 | -46.38 | -0.74 | BC 356 |
| | | | Links | Min N | -80.57 | -0.23 | -0.00 | -0.00 | -0.01 | -0.13 | BC 148 |
| | | | | Max $V_y$ | -24.94 | -0.05 | -0.00 | -0.00 | -0.00 | -0.01 | BC 63 |
| | | | | Min $V_y$ | -71.41 | -1.75 | 2.12 | 0.00 | -42.69 | -1.15 | BC 241 |
| | | | | Max $V_z$ | -36.21 | -0.56 | 2.45 | 0.00 | -46.38 | -0.76 | BC 164 |
| | | | | Min $V_z$ | -48.31 | -0.09 | -2.18 | -0.00 | 43.84 | 0.06 | BC 242 |
| | | | | Max $M_T$ | -24.59 | -0.52 | 2.44 | 0.00 | -46.40 | -0.73 | BC 412 |
| | | | | Min $M_T$ | -48.27 | -0.09 | -2.18 | -0.00 | 43.84 | 0.03 | BC 234 |
| | | | | Max $M_y$ | -25.43 | -0.05 | -2.18 | -0.00 | 43.85 | 0.05 | BC 358 |
| | | | | Min $M_y$ | -36.06 | -0.54 | 2.44 | 0.00 | -46.41 | -0.75 | BC 432 |
| | | | | Max $M_z$ | -48.31 | -0.09 | -2.18 | -0.00 | 43.84 | 0.06 | BC 182 |
| | | | | Min $M_z$ | -59.85 | -1.74 | 2.12 | 0.00 | -42.69 | -1.16 | BC 437 |
| | | | 0 | Max N | -24.58 | -0.53 | 2.45 | 0.00 | -46.38 | -0.74 | BC 356 |
| | | | Rechts | Min N | -80.57 | -0.23 | -0.00 | -0.00 | -0.01 | -0.12 | BC 148 |
| | | | | Max $V_y$ | -24.94 | -0.05 | -0.00 | -0.00 | -0.00 | -0.01 | BC 63 |
| | | | | Min $V_y$ | -71.41 | -1.75 | 2.12 | 0.00 | -42.69 | -1.15 | BC 241 |
| | | | | Max $V_z$ | -36.21 | -0.56 | 2.45 | 0.00 | -46.38 | -0.76 | BC 164 |
| | | | | Min $V_z$ | -48.31 | -0.09 | -2.18 | -0.00 | 43.84 | 0.06 | BC 242 |
| | | | | Max $M_T$ | -24.59 | -0.52 | 2.44 | 0.00 | -46.40 | -0.73 | BC 412 |
| | | | | Min $M_T$ | -48.27 | -0.09 | -2.18 | -0.00 | 43.84 | 0.03 | BC 234 |
| | | | | Max $M_y$ | -25.43 | -0.05 | -2.18 | -0.00 | 43.85 | 0.05 | BC 358 |
| | | | | Min $M_y$ | -36.06 | -0.54 | 2.44 | 0.00 | -46.41 | -0.75 | BC 432 |
| | | | | Max $M_z$ | -48.31 | -0.09 | -2.18 | -0.00 | 43.84 | 0.06 | BC 182 |
| | | | | Min $M_z$ | -59.85 | -1.74 | 2.12 | 0.00 | -42.69 | -1.16 | BC 437 |
| | | | 3565 | Max N | -15.48 | -0.53 | 23.97 | 0.00 | 0.71 | 1.14 | BC 356 |
| | | | Links | Min N | -67.23 | -0.23 | -0.00 | -0.00 | -0.03 | 0.69 | BC 148 |
| | | | | Max $V_y$ | -15.85 | -0.05 | -0.00 | -0.00 | -0.00 | 0.15 | BC 63 |
| | | | | Min $V_y$ | -58.08 | -1.75 | 21.71 | 0.00 | -0.22 | 5.09 | BC 241 |
| | | | | Max $V_z$ | -22.87 | -0.56 | 23.97 | 0.00 | 0.72 | 1.22 | BC 164 |
| | | | | Min $V_z$ | -27.74 | -0.08 | -22.31 | -0.00 | 0.19 | 0.33 | BC 434 |
| | | | | Max $M_T$ | -15.49 | -0.52 | 23.97 | 0.00 | 0.68 | 1.11 | BC 412 |
| | | | | Min $M_T$ | -34.93 | -0.09 | -22.31 | -0.00 | 0.19 | 0.36 | BC 234 |
| | | | | Max $M_y$ | -22.87 | -0.56 | 23.97 | 0.00 | 0.72 | 1.22 | BC 164 |
| | | | | Min $M_y$ | -58.08 | -1.75 | 21.71 | 0.00 | -0.22 | 5.09 | BC 241 |
| | | | | Max $M_z$ | -58.08 | -1.75 | 21.71 | 0.00 | -0.22 | 5.09 | BC 241 |
| | | | | Min $M_z$ | -15.84 | -0.05 | -0.00 | -0.00 | -0.00 | 0.15 | BC 64 |
| | | | 3565 | Max N | -15.48 | -0.53 | 23.97 | 0.00 | 0.71 | 1.14 | BC 356 |
| | | | Rechts | Min N | -67.23 | -0.23 | -0.00 | -0.00 | -0.03 | 0.69 | BC 148 |
| | | | | Max $V_y$ | -15.85 | -0.05 | -0.00 | -0.00 | -0.00 | 0.15 | BC 63 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 151 | RC1 | | | Min $V_y$ | -58.08 | -1.75 | 21.71 | 0.00 | -0.21 | 5.09 | BC 241 |
| | | | | Max $V_z$ | -22.87 | -0.56 | 23.97 | 0.00 | 0.72 | 1.22 | BC 164 |
| | | | | Min $V_z$ | -27.74 | -0.08 | -22.31 | -0.00 | 0.19 | 0.33 | BC 434 |
| | | | | Max $M_T$ | -15.49 | -0.52 | 23.97 | 0.00 | 0.68 | 1.11 | BC 412 |
| | | | | Min $M_T$ | -34.93 | -0.09 | -22.31 | -0.00 | 0.19 | 0.36 | BC 234 |
| | | | | Max $M_y$ | -22.87 | -0.56 | 23.97 | 0.00 | 0.72 | 1.22 | BC 164 |
| | | | | Min $M_y$ | -58.08 | -1.75 | 21.71 | 0.00 | -0.21 | 5.09 | BC 241 |
| | | | | Max $M_z$ | -58.08 | -1.75 | 21.71 | 0.00 | -0.21 | 5.09 | BC 241 |
| | | | | Min $M_z$ | -15.84 | -0.05 | -0.00 | -0.00 | -0.00 | 0.15 | BC 64 |
| | | | 3625 | Max N | -15.35 | -0.53 | 24.34 | 0.00 | 2.16 | 1.18 | BC 356 |
| | | | Links | Min N | -67.05 | -0.23 | -0.00 | -0.00 | -0.03 | 0.71 | BC 148 |
| | | | | Max $V_y$ | -15.72 | -0.05 | -0.00 | -0.00 | -0.00 | 0.16 | BC 63 |
| | | | | Min $V_y$ | -57.89 | -1.75 | 22.04 | 0.00 | 1.10 | 5.19 | BC 241 |
| | | | | Max $V_z$ | -22.68 | -0.56 | 24.34 | 0.00 | 2.17 | 1.26 | BC 164 |
| | | | | Min $V_z$ | -27.61 | -0.08 | -22.65 | -0.00 | -1.16 | 0.33 | BC 434 |
| | | | | Max $M_T$ | -15.37 | -0.52 | 24.33 | 0.00 | 2.13 | 1.15 | BC 412 |
| | | | | Min $M_T$ | -34.74 | -0.09 | -22.65 | -0.00 | -1.16 | 0.37 | BC 234 |
| | | | | Max $M_y$ | -22.68 | -0.56 | 24.34 | 0.00 | 2.17 | 1.26 | BC 164 |
| | | | | Min $M_y$ | -34.79 | -0.09 | -22.65 | -0.00 | -1.16 | 0.38 | BC 242 |
| | | | | Max $M_z$ | -57.89 | -1.75 | 22.04 | 0.00 | 1.10 | 5.19 | BC 241 |
| | | | | Min $M_z$ | -15.72 | -0.05 | -0.00 | -0.00 | -0.00 | 0.16 | BC 64 |
| | | 35 | 3625 | Max N | -15.35 | -0.53 | 24.34 | 0.00 | 2.16 | 1.18 | BC 356 |
| | | | Rechts | Min N | -67.05 | -0.23 | -0.00 | -0.00 | -0.03 | 0.71 | BC 148 |
| | | | | Max $V_y$ | -15.72 | -0.05 | -0.00 | -0.00 | -0.00 | 0.16 | BC 63 |
| | | | | Min $V_y$ | -57.89 | -1.75 | 22.04 | 0.00 | 1.10 | 5.19 | BC 241 |
| | | | | Max $V_z$ | -22.68 | -0.56 | 24.34 | 0.00 | 2.17 | 1.26 | BC 164 |
| | | | | Min $V_z$ | -27.61 | -0.08 | -22.65 | -0.00 | -1.16 | 0.33 | BC 434 |
| | | | | Max $M_T$ | -15.37 | -0.52 | 24.33 | 0.00 | 2.13 | 1.15 | BC 412 |
| | | | | Min $M_T$ | -34.74 | -0.09 | -22.65 | -0.00 | -1.16 | 0.37 | BC 234 |
| | | | | Max $M_y$ | -22.68 | -0.56 | 24.34 | 0.00 | 2.17 | 1.26 | BC 164 |
| | | | | Min $M_y$ | -34.79 | -0.09 | -22.65 | -0.00 | -1.16 | 0.38 | BC 242 |
| | | | | Max $M_z$ | -57.89 | -1.75 | 22.04 | 0.00 | 1.10 | 5.19 | BC 241 |
| | | | | Min $M_z$ | -15.72 | -0.05 | -0.00 | -0.00 | -0.00 | 0.16 | BC 64 |
| 152 | RC1 | 70 | 0 | Max N | -24.87 | 0.52 | 2.07 | -0.00 | -48.03 | 0.83 | BC 445 |
| | | | Links | Min N | -81.22 | 0.19 | -0.00 | -0.00 | -0.01 | 0.15 | BC 138 |
| | | | | Max $V_y$ | -60.18 | 1.67 | 1.79 | -0.00 | -44.30 | 1.14 | BC 164 |
| | | | | Min $V_y$ | -25.44 | 0.04 | -0.00 | -0.00 | -0.00 | 0.02 | BC 35 |
| | | | | Max $V_z$ | -36.44 | 0.56 | 2.07 | -0.00 | -48.02 | 0.85 | BC 433 |
| | | | | Min $V_z$ | -37.93 | 0.06 | -1.84 | 0.00 | 45.46 | -0.05 | BC 166 |
| | | | | Max $M_T$ | -49.24 | 0.08 | -1.84 | 0.00 | 45.46 | -0.02 | BC 214 |
| | | | | Min $M_T$ | -70.95 | 1.64 | 1.78 | -0.00 | -44.30 | 1.11 | BC 264 |
| | | | | Max $M_y$ | -37.51 | 0.07 | -1.84 | 0.00 | 45.46 | -0.02 | BC 434 |
| | | | | Min $M_y$ | -36.72 | 0.53 | 2.07 | -0.00 | -48.04 | 0.84 | BC 165 |
| | | | | Max $M_z$ | -60.18 | 1.67 | 1.79 | -0.00 | -44.30 | 1.14 | BC 164 |
| | | | | Min $M_z$ | -37.93 | 0.06 | -1.84 | 0.00 | 45.46 | -0.06 | BC 218 |
| | | | 0 | Max N | -24.87 | 0.52 | 2.07 | -0.00 | -48.03 | 0.83 | BC 445 |
| | | | Rechts | Min N | -81.22 | 0.19 | -0.00 | -0.00 | -0.01 | 0.15 | BC 138 |
| | | | | Max $V_y$ | -60.18 | 1.67 | 1.79 | -0.00 | -44.30 | 1.14 | BC 164 |
| | | | | Min $V_y$ | -25.44 | 0.04 | -0.00 | -0.00 | -0.00 | 0.02 | BC 35 |
| | | | | Max $V_z$ | -36.44 | 0.56 | 2.07 | -0.00 | -48.02 | 0.85 | BC 433 |
| | | | | Min $V_z$ | -37.93 | 0.06 | -1.84 | 0.00 | 45.46 | -0.05 | BC 166 |
| | | | | Max $M_T$ | -49.24 | 0.08 | -1.84 | 0.00 | 45.46 | -0.02 | BC 214 |
| | | | | Min $M_T$ | -70.95 | 1.64 | 1.78 | -0.00 | -44.30 | 1.11 | BC 264 |
| | | | | Max $M_y$ | -37.51 | 0.07 | -1.84 | 0.00 | 45.46 | -0.02 | BC 434 |
| | | | | Min $M_y$ | -36.72 | 0.53 | 2.07 | -0.00 | -48.04 | 0.84 | BC 165 |
| | | | | Max $M_z$ | -60.18 | 1.67 | 1.79 | -0.00 | -44.30 | 1.14 | BC 164 |
| | | | | Min $M_z$ | -37.93 | 0.06 | -1.84 | 0.00 | 45.46 | -0.06 | BC 218 |
| | | | 3627 | Max N | -15.58 | 0.52 | 23.98 | -0.00 | -0.80 | -1.07 | BC 445 |
| | | | Links | Min N | -67.60 | 0.19 | -0.00 | -0.00 | -0.01 | -0.52 | BC 138 |
| | | | | Max $V_y$ | -46.56 | 1.67 | 21.78 | -0.00 | -1.56 | -4.93 | BC 164 |
| | | | | Min $V_y$ | -16.15 | 0.04 | -0.00 | -0.00 | -0.00 | -0.14 | BC 35 |
| | | | | Max $V_z$ | -27.16 | 0.56 | 23.98 | -0.00 | -0.78 | -1.17 | BC 433 |
| | | | | Min $V_z$ | -24.31 | 0.06 | -22.37 | 0.00 | 1.57 | -0.28 | BC 166 |
| | | | | Max $M_T$ | -35.62 | 0.08 | -22.37 | 0.00 | 1.58 | -0.32 | BC 214 |
| | | | | Min $M_T$ | -57.33 | 1.64 | 21.78 | -0.00 | -1.56 | -4.84 | BC 264 |
| | | | | Max $M_y$ | -28.23 | 0.07 | -22.37 | 0.00 | 1.58 | -0.28 | BC 434 |
| | | | | Min $M_y$ | -57.30 | 1.64 | 21.78 | -0.00 | -1.56 | -4.83 | BC 236 |
| | | | | Max $M_z$ | -16.09 | 0.05 | -0.00 | -0.00 | -0.00 | -0.13 | BC 56 |
| | | | | Min $M_z$ | -46.56 | 1.67 | 21.78 | -0.00 | -1.56 | -4.93 | BC 164 |
| | | | 3627 | Max N | -15.58 | 0.52 | 23.98 | -0.00 | -0.80 | -1.07 | BC 445 |
| | | | Rechts | Min N | -67.60 | 0.19 | -0.00 | -0.00 | -0.01 | -0.52 | BC 138 |
| | | | | Max $V_y$ | -46.56 | 1.67 | 21.78 | -0.00 | -1.56 | -4.93 | BC 164 |
| | | | | Min $V_y$ | -16.15 | 0.04 | -0.00 | -0.00 | -0.00 | -0.14 | BC 35 |
| | | | | Max $V_z$ | -27.16 | 0.56 | 23.98 | -0.00 | -0.78 | -1.17 | BC 433 |
| | | | | Min $V_z$ | -24.31 | 0.06 | -22.37 | 0.00 | 1.57 | -0.28 | BC 166 |
| | | | | Max $M_T$ | -35.62 | 0.08 | -22.37 | 0.00 | 1.58 | -0.32 | BC 214 |
| | | | | Min $M_T$ | -57.33 | 1.64 | 21.78 | -0.00 | -1.56 | -4.84 | BC 264 |
| | | | | Max $M_y$ | -28.23 | 0.07 | -22.37 | 0.00 | 1.58 | -0.28 | BC 434 |
| | | | | Min $M_y$ | -57.30 | 1.64 | 21.78 | -0.00 | -1.56 | -4.83 | BC 236 |
| | | | | Max $M_z$ | -16.09 | 0.05 | -0.00 | -0.00 | -0.00 | -0.13 | BC 56 |
| | | | | Min $M_z$ | -46.56 | 1.67 | 21.78 | -0.00 | -1.56 | -4.93 | BC 164 |
| | | | 3686 | Max N | -15.44 | 0.52 | 24.34 | -0.00 | 0.65 | -1.10 | BC 445 |
| | | | Links | Min N | -67.39 | 0.19 | -0.00 | -0.00 | -0.01 | -0.53 | BC 138 |
| | | | | Max $V_y$ | -46.35 | 1.67 | 22.12 | -0.00 | -0.24 | -5.03 | BC 164 |
| | | | | Min $V_y$ | -16.01 | 0.04 | -0.00 | -0.00 | -0.00 | -0.14 | BC 35 |
| | | | | Max $V_z$ | -27.02 | 0.56 | 24.34 | -0.00 | 0.67 | -1.21 | BC 433 |
| | | | | Min $V_z$ | -24.10 | 0.06 | -22.71 | 0.00 | 0.22 | -0.28 | BC 166 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 152 | RC1 | | | Max $M_T$ | -35.41 | 0.08 | -22.71 | 0.00 | 0.22 | -0.32 | BC 214 |
| | | | | Min $M_T$ | -57.13 | 1.64 | 22.11 | -0.00 | -0.25 | -4.94 | BC 264 |
| | | | | Max $M_y$ | -27.02 | 0.56 | 24.34 | -0.00 | 0.67 | -1.21 | BC 433 |
| | | | | Min $M_y$ | -57.09 | 1.64 | 22.11 | -0.00 | -0.25 | -4.93 | BC 236 |
| | | | | Max $M_z$ | -15.95 | 0.05 | -0.00 | -0.00 | -0.00 | -0.13 | BC 56 |
| | | | | Min $M_z$ | -46.35 | 1.67 | 22.12 | -0.00 | -0.24 | -5.03 | BC 164 |
| | | | 3686 | Max N | -15.44 | 0.52 | 24.34 | -0.00 | 0.65 | -1.10 | BC 445 |
| | | | Rechts | Min N | -67.39 | 0.19 | -0.00 | -0.00 | -0.01 | -0.53 | BC 138 |
| | | | | Max $V_y$ | -46.35 | 1.67 | 22.12 | -0.00 | -0.24 | -5.03 | BC 164 |
| | | | | Min $V_y$ | -16.01 | 0.04 | -0.00 | -0.00 | -0.00 | -0.14 | BC 35 |
| | | | | Max $V_z$ | -27.02 | 0.56 | 24.34 | -0.00 | 0.67 | -1.21 | BC 433 |
| | | | | Min $V_z$ | -24.10 | 0.06 | -22.71 | 0.00 | 0.22 | -0.28 | BC 166 |
| | | | | Max $M_T$ | -35.41 | 0.08 | -22.71 | 0.00 | 0.22 | -0.32 | BC 214 |
| | | | | Min $M_T$ | -57.13 | 1.64 | 22.11 | -0.00 | -0.25 | -4.94 | BC 264 |
| | | | | Max $M_y$ | -27.02 | 0.56 | 24.34 | -0.00 | 0.67 | -1.21 | BC 433 |
| | | | | Min $M_y$ | -57.09 | 1.64 | 22.11 | -0.00 | -0.25 | -4.93 | BC 236 |
| | | | | Max $M_z$ | -15.95 | 0.05 | -0.00 | -0.00 | -0.00 | -0.13 | BC 56 |
| | | | | Min $M_z$ | -46.35 | 1.67 | 22.12 | -0.00 | -0.24 | -5.03 | BC 164 |
| | | | 3748 | Max N | -15.35 | 0.52 | 24.71 | -0.00 | 2.16 | -1.13 | BC 445 |
| | | | Links | Min N | -67.26 | 0.19 | -0.00 | -0.00 | -0.01 | -0.54 | BC 138 |
| | | | | Max $V_y$ | -46.22 | 1.67 | 22.45 | -0.00 | 1.13 | -5.13 | BC 164 |
| | | | | Min $V_y$ | -15.92 | 0.04 | -0.00 | -0.00 | -0.00 | -0.15 | BC 35 |
| | | | | Max $V_z$ | -26.93 | 0.56 | 24.71 | -0.00 | 2.18 | -1.24 | BC 433 |
| | | | | Min $V_z$ | -23.97 | 0.06 | -23.05 | 0.00 | -1.18 | -0.29 | BC 166 |
| | | | | Max $M_T$ | -35.28 | 0.08 | -23.05 | 0.00 | -1.18 | -0.33 | BC 214 |
| | | | | Min $M_T$ | -56.99 | 1.64 | 22.45 | -0.00 | 1.12 | -5.04 | BC 264 |
| | | | | Max $M_y$ | -26.93 | 0.56 | 24.71 | -0.00 | 2.18 | -1.24 | BC 433 |
| | | | | Min $M_y$ | -23.97 | 0.06 | -23.05 | 0.00 | -1.18 | -0.29 | BC 166 |
| | | | | Max $M_z$ | -15.85 | 0.05 | -0.00 | -0.00 | -0.00 | -0.13 | BC 56 |
| | | | | Min $M_z$ | -46.22 | 1.67 | 22.45 | -0.00 | 1.13 | -5.13 | BC 164 |
| | | 39 | 3748 | Max N | -15.35 | 0.52 | 24.71 | -0.00 | 2.16 | -1.13 | BC 445 |
| | | | Rechts | Min N | -67.26 | 0.19 | -0.00 | -0.00 | -0.01 | -0.54 | BC 138 |
| | | | | Max $V_y$ | -46.22 | 1.67 | 22.45 | -0.00 | 1.13 | -5.13 | BC 164 |
| | | | | Min $V_y$ | -15.92 | 0.04 | -0.00 | -0.00 | -0.00 | -0.15 | BC 35 |
| | | | | Max $V_z$ | -26.93 | 0.56 | 24.71 | -0.00 | 2.18 | -1.24 | BC 433 |
| | | | | Min $V_z$ | -23.97 | 0.06 | -23.05 | 0.00 | -1.19 | -0.29 | BC 166 |
| | | | | Max $M_T$ | -35.28 | 0.08 | -23.05 | 0.00 | -1.18 | -0.33 | BC 214 |
| | | | | Min $M_T$ | -56.99 | 1.64 | 22.45 | -0.00 | 1.12 | -5.04 | BC 264 |
| | | | | Max $M_y$ | -26.93 | 0.56 | 24.71 | -0.00 | 2.18 | -1.24 | BC 433 |
| | | | | Min $M_y$ | -23.97 | 0.06 | -23.05 | 0.00 | -1.19 | -0.29 | BC 166 |
| | | | | Max $M_z$ | -15.85 | 0.05 | -0.00 | -0.00 | -0.00 | -0.13 | BC 56 |
| | | | | Min $M_z$ | -46.22 | 1.67 | 22.45 | -0.00 | 1.13 | -5.13 | BC 164 |
| 153 | RC1 | 12 | 0 | Max N | -15.89 | -6.35 | 6.09 | -0.00 | -4.64 | -4.88 | BC 358 |
| | | | Links | Min N | -45.44 | -0.11 | 0.27 | 0.00 | -0.79 | -0.37 | BC 155 |
| | | | | Max $V_y$ | -16.13 | 8.98 | -3.65 | 0.00 | 1.61 | 7.39 | BC 409 |
| | | | | Min $V_y$ | -29.14 | -6.38 | 6.17 | -0.00 | -4.89 | -4.97 | BC 246 |
| | | | | Max $V_z$ | -29.14 | -6.36 | 6.24 | -0.00 | -5.10 | -4.91 | BC 242 |
| | | | | Min $V_z$ | -16.13 | 8.95 | -3.71 | 0.00 | 1.82 | 7.30 | BC 417 |
| | | | | Max $M_T$ | -29.38 | 8.93 | -3.65 | 0.00 | 1.63 | 7.25 | BC 245 |
| | | | | Min $M_T$ | -15.89 | -6.36 | 6.09 | -0.00 | -4.65 | -4.90 | BC 362 |
| | | | | Max $M_y$ | -16.13 | 8.95 | -3.71 | 0.00 | 1.82 | 7.30 | BC 417 |
| | | | | Min $M_y$ | -29.14 | -6.36 | 6.24 | -0.00 | -5.10 | -4.91 | BC 242 |
| | | | | Max $M_z$ | -16.13 | 8.98 | -3.65 | 0.00 | 1.61 | 7.39 | BC 413 |
| | | | | Min $M_z$ | -21.66 | -6.38 | 6.13 | -0.00 | -4.77 | -4.97 | BC 438 |
| | | | 0 | Max N | -15.89 | -6.35 | 6.09 | -0.00 | -4.64 | -4.88 | BC 358 |
| | | | Rechts | Min N | -45.44 | -0.11 | 0.27 | 0.00 | -0.79 | -0.37 | BC 155 |
| | | | | Max $V_y$ | -16.13 | 8.98 | -3.65 | 0.00 | 1.61 | 7.39 | BC 409 |
| | | | | Min $V_y$ | -29.14 | -6.38 | 6.17 | -0.00 | -4.89 | -4.97 | BC 246 |
| | | | | Max $V_z$ | -29.14 | -6.36 | 6.24 | -0.00 | -5.10 | -4.91 | BC 242 |
| | | | | Min $V_z$ | -16.13 | 8.95 | -3.71 | 0.00 | 1.82 | 7.30 | BC 417 |
| | | | | Max $M_T$ | -29.38 | 8.93 | -3.65 | 0.00 | 1.63 | 7.25 | BC 245 |
| | | | | Min $M_T$ | -15.89 | -6.36 | 6.09 | -0.00 | -4.65 | -4.90 | BC 362 |
| | | | | Max $M_y$ | -16.13 | 8.95 | -3.71 | 0.00 | 1.82 | 7.30 | BC 417 |
| | | | | Min $M_y$ | -29.14 | -6.36 | 6.24 | -0.00 | -5.10 | -4.91 | BC 242 |
| | | | | Max $M_z$ | -16.13 | 8.98 | -3.65 | 0.00 | 1.61 | 7.39 | BC 413 |
| | | | | Min $M_z$ | -21.66 | -6.38 | 6.13 | -0.00 | -4.77 | -4.97 | BC 438 |
| | | | 3505 | Max N | -7.90 | 3.76 | -3.66 | -0.00 | -0.38 | -0.34 | BC 358 |
| | | | Links | Min N | -33.72 | -0.10 | 0.27 | 0.00 | 0.17 | 0.01 | BC 140 |
| | | | | Max $V_y$ | -7.90 | 3.78 | -3.60 | -0.00 | -0.37 | -0.34 | BC 410 |
| | | | | Min $V_y$ | -17.67 | -5.07 | 3.01 | 0.00 | 0.41 | 0.47 | BC 241 |
| | | | | Max $V_z$ | -17.67 | -5.05 | 3.01 | 0.00 | 0.41 | 0.47 | BC 265 |
| | | | | Min $V_z$ | -7.90 | 3.76 | -3.66 | -0.00 | -0.38 | -0.34 | BC 358 |
| | | | | Max $M_T$ | -17.67 | -5.06 | 2.95 | 0.00 | 0.41 | 0.47 | BC 245 |
| | | | | Min $M_T$ | -7.90 | 3.76 | -3.65 | -0.00 | -0.38 | -0.34 | BC 362 |
| | | | | Max $M_y$ | -17.67 | -5.05 | 3.01 | 0.00 | 0.41 | 0.47 | BC 265 |
| | | | | Min $M_y$ | -7.90 | 3.76 | -3.66 | -0.00 | -0.38 | -0.34 | BC 358 |
| | | | | Max $M_z$ | -17.67 | -5.07 | 3.01 | 0.00 | 0.41 | 0.47 | BC 241 |
| | | | | Min $M_z$ | -7.90 | 3.78 | -3.60 | -0.00 | -0.37 | -0.34 | BC 410 |
| | | 46 | 3505 | Max N | -7.90 | 3.76 | -3.66 | -0.00 | -0.38 | -0.34 | BC 358 |
| | | | Rechts | Min N | -33.72 | -0.11 | 0.27 | 0.00 | 0.17 | 0.01 | BC 155 |
| | | | | Max $V_y$ | -7.90 | 3.78 | -3.60 | -0.00 | -0.37 | -0.34 | BC 410 |
| | | | | Min $V_y$ | -17.67 | -5.07 | 3.01 | 0.00 | 0.41 | 0.47 | BC 241 |
| | | | | Max $V_z$ | -17.67 | -5.05 | 3.01 | 0.00 | 0.41 | 0.47 | BC 265 |
| | | | | Min $V_z$ | -7.90 | 3.76 | -3.66 | -0.00 | -0.38 | -0.34 | BC 358 |
| | | | | Max $M_T$ | -17.67 | -5.06 | 2.95 | 0.00 | 0.41 | 0.47 | BC 245 |
| | | | | Min $M_T$ | -7.90 | 3.76 | -3.65 | -0.00 | -0.38 | -0.34 | BC 362 |
| | | | | Max $M_y$ | -17.67 | -5.05 | 3.01 | 0.00 | 0.41 | 0.47 | BC 265 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 153 | RC1 | | | Min $M_y$ | -7.90 | 3.76 | -3.66 | -0.00 | -0.38 | -0.34 | BC 358 |
| | | | | Max $M_z$ | -17.67 | -5.07 | 3.01 | 0.00 | 0.41 | 0.47 | BC 241 |
| | | | | Min $M_z$ | -7.90 | 3.78 | -3.60 | -0.00 | -0.37 | -0.34 | BC 410 |
| 154 | RC1 | 59 | 0 | Max N | 43.58 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 264 |
| | | | | Min N | -0.75 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 245 |
| | | | | Max $V_y$ | 1.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 1.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 1.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 1.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 1.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 1.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 1.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 1.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 1.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 1.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 91 | 2737 | Max N | 43.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 264 |
| | | | | Min N | -0.39 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 437 |
| | | | | Max $V_y$ | 2.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 2.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 2.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 2.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 2.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 2.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 2.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 2.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 2.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 2.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 155 | RC1 | 90 | 0 | Max N | 49.93 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 377 |
| | | | | Min N | -1.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 264 |
| | | | | Max $V_y$ | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 92 | 2737 | Max N | 50.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 377 |
| | | | | Min N | -0.64 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 456 |
| | | | | Max $V_y$ | 0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 156 | RC1 | 92 | 0 | Max N | 49.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 264 |
| | | | | Min N | -0.75 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Max $V_y$ | 4.44 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 4.44 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 4.44 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 4.44 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 4.44 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 4.44 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 4.44 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 4.44 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 4.44 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 4.44 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 89 | 2737 | Max N | 49.57 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 264 |
| | | | | Min N | -0.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Max $V_y$ | 4.90 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 4.90 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 4.90 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 4.90 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 4.90 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 4.90 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 4.90 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 4.90 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 4.90 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 4.90 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 157 | RC1 | 91 | 0 | Max N | 39.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 389 |
| | | | | Min N | -0.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 264 |
| | | | | Max $V_y$ | -0.37 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.37 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.37 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.37 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.37 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.37 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.37 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.37 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.37 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.37 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 157 | RC1 | 80 | 2737 | Max N | 39.61 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 389 |
| | | | | Min N | -0.59 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 456 |
| | | | | Max $V_y$ | 0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 158 | RC1 | 79 | 0 | Max N | 37.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 248 |
| | | | | Min N | -0.68 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 185 |
| | | | | Max $V_y$ | 7.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 7.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 7.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 7.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 7.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 7.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 7.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 7.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 7.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 7.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 42 | 7512 | Max N | 37.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 248 |
| | | | | Min N | -0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 377 |
| | | | | Max $V_y$ | 8.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 8.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 8.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 8.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 8.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 8.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 8.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 8.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 8.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 8.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 159 | RC1 | 80 | 0 | Max N | 26.61 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 377 |
| | | | | Min N | -0.96 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 264 |
| | | | | Max $V_y$ | -0.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 41 | 7451 | Max N | 27.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 377 |
| | | | | Min N | -0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 456 |
| | | | | Max $V_y$ | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 160 | RC1 | 94 | 0 | Max N | 29.20 | -0.13 | 0.00 | -0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Min N | -90.94 | 0.12 | 0.00 | -0.00 | 0.00 | 0.00 | BC 269 |
| | | | | Max $V_y$ | -87.48 | 0.13 | 0.00 | -0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min $V_y$ | 19.98 | -0.15 | 0.00 | -0.00 | 0.00 | 0.00 | BC 276 |
| | | | | Max $V_z$ | -73.30 | 0.12 | 0.00 | -0.00 | 0.00 | 0.00 | BC 377 |
| | | | | Min $V_z$ | -18.50 | -0.02 | -0.00 | 0.00 | 0.00 | 0.00 | BC 279 |
| | | | | Max $M_T$ | -8.23 | -0.02 | -0.00 | 0.00 | 0.00 | 0.00 | BC 167 |
| | | | | Min $M_T$ | -90.92 | 0.12 | 0.00 | -0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Max $M_y$ | -8.11 | -0.03 | -0.00 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -8.11 | -0.03 | -0.00 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -13.60 | -0.04 | 0.00 | -0.00 | 0.00 | 0.00 | BC 190 |
| | | | | Min $M_z$ | -82.00 | 0.12 | 0.00 | -0.00 | 0.00 | -0.00 | BC 381 |
| | | 95 | 2173 | Max N | 29.90 | -0.13 | 0.00 | -0.00 | 0.01 | 0.28 | BC 360 |
| | | | | Min N | -89.92 | 0.12 | 0.00 | -0.00 | 0.01 | -0.26 | BC 269 |
| | | | | Max $V_y$ | -86.78 | 0.13 | 0.00 | -0.00 | 0.01 | -0.28 | BC 433 |
| | | | | Min $V_y$ | 21.00 | -0.15 | 0.00 | -0.00 | 0.01 | 0.32 | BC 276 |
| | | | | Max $V_z$ | -72.61 | 0.12 | 0.00 | -0.00 | 0.01 | -0.26 | BC 377 |
| | | | | Min $V_z$ | -17.48 | -0.02 | -0.00 | 0.00 | -0.01 | 0.05 | BC 279 |
| | | | | Max $M_T$ | -7.21 | -0.02 | -0.00 | 0.00 | -0.01 | 0.04 | BC 167 |
| | | | | Min $M_T$ | -89.90 | 0.12 | 0.00 | -0.00 | 0.01 | -0.26 | BC 241 |
| | | | | Max $M_y$ | -72.61 | 0.12 | 0.00 | -0.00 | 0.01 | -0.26 | BC 377 |
| | | | | Min $M_y$ | -17.48 | -0.02 | -0.00 | 0.00 | -0.01 | 0.05 | BC 279 |
| | | | | Max $M_z$ | 21.00 | -0.15 | 0.00 | -0.00 | 0.01 | 0.32 | BC 276 |
| | | | | Min $M_z$ | -86.78 | 0.13 | 0.00 | -0.00 | 0.01 | -0.28 | BC 433 |
| 161 | RC1 | 97 | 0 | Max N | 24.10 | 0.17 | 0.00 | -0.00 | 0.00 | 0.00 | BC 357 |
| | | | | Min N | -121.56 | -0.10 | 0.00 | -0.00 | 0.00 | -0.00 | BC 240 |
| | | | | Max $V_y$ | 13.68 | 0.19 | 0.00 | -0.00 | 0.00 | 0.00 | BC 201 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 161 | RC1 | | | Min $V_y$ | -109.52 | -0.12 | 0.00 | -0.00 | 0.00 | 0.00 | BC 444 |
| | | | | Max $V_z$ | 5.27 | 0.18 | 0.00 | -0.00 | 0.00 | 0.00 | BC 217 |
| | | | | Min $V_z$ | -39.31 | 0.04 | -0.00 | 0.00 | 0.00 | 0.00 | BC 247 |
| | | | | Max $M_T$ | -44.29 | 0.02 | -0.00 | 0.00 | 0.00 | 0.00 | BC 415 |
| | | | | Min $M_T$ | 22.19 | 0.16 | 0.00 | -0.00 | 0.00 | 0.00 | BC 417 |
| | | | | Max $M_y$ | -20.20 | 0.06 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -20.20 | 0.06 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -18.48 | 0.05 | 0.00 | 0.00 | 0.00 | 0.00 | BC 2 |
| | | | | Min $M_z$ | -46.07 | 0.04 | 0.00 | 0.00 | 0.00 | -0.00 | BC 91 |
| | | 98 | 2173 | Max N | 24.80 | 0.17 | 0.00 | -0.00 | 0.00 | -0.37 | BC 357 |
| | | | | Min N | -120.54 | -0.10 | 0.00 | -0.00 | 0.00 | 0.22 | BC 240 |
| | | | | Max $V_y$ | 14.70 | 0.19 | 0.00 | -0.00 | 0.00 | -0.42 | BC 201 |
| | | | | Min $V_y$ | -108.83 | -0.12 | 0.00 | -0.00 | 0.00 | 0.26 | BC 444 |
| | | | | Max $V_z$ | 6.29 | 0.18 | 0.00 | -0.00 | 0.00 | -0.38 | BC 217 |
| | | | | Min $V_z$ | -38.29 | 0.04 | -0.00 | 0.00 | -0.00 | -0.09 | BC 247 |
| | | | | Max $M_T$ | -43.60 | 0.02 | -0.00 | 0.00 | -0.00 | -0.05 | BC 415 |
| | | | | Min $M_T$ | 22.88 | 0.16 | 0.00 | -0.00 | 0.00 | -0.36 | BC 417 |
| | | | | Max $M_y$ | 6.29 | 0.18 | 0.00 | -0.00 | 0.00 | -0.38 | BC 217 |
| | | | | Min $M_y$ | -38.29 | 0.04 | -0.00 | 0.00 | -0.00 | -0.09 | BC 247 |
| | | | | Max $M_z$ | -108.83 | -0.12 | 0.00 | -0.00 | 0.00 | 0.26 | BC 444 |
| | | | | Min $M_z$ | 14.70 | 0.19 | 0.00 | -0.00 | 0.00 | -0.42 | BC 201 |
| 162 | RC1 | 95 | 0 | Max N | -0.01 | 0.00 | 0.27 | 0.00 | 0.00 | 0.00 | BC 394 |
| | | | | Min N | -29.81 | 0.00 | 0.39 | 0.00 | 0.00 | 0.00 | BC 269 |
| | | | | Max $V_y$ | -0.09 | 0.00 | 0.44 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.09 | 0.00 | 0.44 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.09 | 0.00 | 0.44 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -29.34 | 0.00 | 0.27 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Max $M_T$ | -22.34 | 0.00 | 0.39 | 0.00 | -0.00 | 0.00 | BC 244 |
| | | | | Min $M_T$ | -3.64 | 0.00 | 0.39 | -0.00 | -0.00 | 0.00 | BC 219 |
| | | | | Max $M_y$ | -5.68 | 0.00 | 0.39 | 0.00 | 0.00 | 0.00 | BC 91 |
| | | | | Min $M_y$ | -0.58 | 0.00 | 0.39 | 0.00 | -0.00 | 0.00 | BC 70 |
| | | | | Max $M_z$ | -0.09 | 0.00 | 0.44 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.09 | 0.00 | 0.44 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 92 | 1665 | Max N | -0.01 | 0.00 | -0.27 | 0.00 | 0.00 | 0.00 | BC 394 |
| | | | | Min N | -29.81 | 0.00 | -0.39 | 0.00 | 0.00 | 0.00 | BC 269 |
| | | | | Max $V_y$ | -0.09 | 0.00 | -0.44 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.09 | 0.00 | -0.44 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -29.34 | 0.00 | -0.27 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min $V_z$ | -0.09 | 0.00 | -0.44 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -22.34 | 0.00 | -0.39 | 0.00 | -0.00 | 0.00 | BC 244 |
| | | | | Min $M_T$ | -3.64 | 0.00 | -0.39 | -0.00 | -0.00 | 0.00 | BC 219 |
| | | | | Max $M_y$ | -5.68 | 0.00 | -0.39 | 0.00 | 0.00 | 0.00 | BC 91 |
| | | | | Min $M_y$ | -0.58 | 0.00 | -0.39 | 0.00 | -0.00 | 0.00 | BC 70 |
| | | | | Max $M_z$ | -0.09 | 0.00 | -0.44 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.09 | 0.00 | -0.44 | 0.00 | 0.00 | 0.00 | BC 1 |
| 163 | RC1 | 94 | 0 | Max N | 51.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Min N | -1.14 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 269 |
| | | | | Max $V_y$ | -0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 92 | 2737 | Max N | 51.28 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Min N | -0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Max $V_y$ | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 164 | RC1 | 59 | 0 | Max N | 50.72 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 269 |
| | | | | Min N | -0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 168 |
| | | | | Max $V_y$ | -0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 95 | 2737 | Max N | 51.12 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 269 |
| | | | | Min N | -0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Max $V_y$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 164 | RC1 | | | Max $M_T$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 165 | RC1 | 95 | 0 | Max N | 40.68 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Min N | -1.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Max $V_y$ | -0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 80 | 2737 | Max N | 40.95 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Min N | -0.69 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Max $V_y$ | 0.12 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.12 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.12 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.12 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.12 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.12 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.12 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.12 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.12 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.12 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 166 | RC1 | 92 | 0 | Max N | 55.70 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min N | -0.77 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 168 |
| | | | | Max $V_y$ | 1.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 1.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 1.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 1.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 1.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 1.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 1.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 1.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 1.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 1.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 93 | 2737 | Max N | 56.10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min N | -0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Max $V_y$ | 2.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 2.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 2.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 2.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 2.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 2.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 2.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 2.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 2.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 2.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 167 | RC1 | 88 | 0 | Max N | 24.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 432 |
| | | | | Min N | -0.88 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 165 |
| | | | | Max $V_y$ | -0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 63 | 7411 | Max N | 24.69 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 432 |
| | | | | Min N | -0.28 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 357 |
| | | | | Max $V_y$ | 0.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 168 | RC1 | 77 | 0 | Max N | 34.96 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 165 |
| | | | | Min N | -0.64 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 240 |
| | | | | Max $V_y$ | 9.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 9.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 9.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 9.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 9.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 9.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 9.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 168 | RC1 | | | Min $M_y$ | 9.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 9.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 9.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 68 | 7529 | Max N | 35.66 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 165 |
| | | | | Min N | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 432 |
| | | | | Max $V_y$ | 9.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 9.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 9.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 9.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 9.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 9.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 9.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 9.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 9.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 9.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 169 | RC1 | 99 | 0 | Max N | -0.12 | 0.00 | 0.27 | 0.00 | -0.00 | 0.00 | BC 34 |
| | | | | Min N | -39.78 | 0.00 | 0.27 | 0.00 | 0.00 | 0.00 | BC 432 |
| | | | | Max $V_y$ | -0.52 | 0.00 | 0.44 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.52 | 0.00 | 0.44 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.23 | 0.00 | 0.44 | 0.00 | -0.00 | 0.00 | BC 2 |
| | | | | Min $V_z$ | -39.78 | 0.00 | 0.27 | 0.00 | 0.00 | 0.00 | BC 432 |
| | | | | Max $M_T$ | -14.47 | 0.00 | 0.39 | 0.00 | 0.00 | 0.00 | BC 245 |
| | | | | Min $M_T$ | -10.50 | 0.00 | 0.27 | -0.00 | -0.00 | 0.00 | BC 411 |
| | | | | Max $M_y$ | -11.73 | 0.00 | 0.39 | 0.00 | 0.00 | 0.00 | BC 278 |
| | | | | Min $M_y$ | -8.08 | 0.00 | 0.27 | -0.00 | -0.00 | 0.00 | BC 53 |
| | | | | Max $M_z$ | -0.52 | 0.00 | 0.44 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.52 | 0.00 | 0.44 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 98 | 1665 | Max N | -0.12 | 0.00 | -0.27 | 0.00 | -0.00 | 0.00 | BC 34 |
| | | | | Min N | -39.78 | 0.00 | -0.27 | 0.00 | 0.00 | 0.00 | BC 432 |
| | | | | Max $V_y$ | -0.52 | 0.00 | -0.44 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.52 | 0.00 | -0.44 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -39.78 | 0.00 | -0.27 | 0.00 | 0.00 | 0.00 | BC 432 |
| | | | | Min $V_z$ | -0.23 | 0.00 | -0.44 | 0.00 | -0.00 | 0.00 | BC 2 |
| | | | | Max $M_T$ | -14.47 | 0.00 | -0.39 | 0.00 | 0.00 | 0.00 | BC 245 |
| | | | | Min $M_T$ | -10.50 | 0.00 | -0.27 | -0.00 | -0.00 | 0.00 | BC 411 |
| | | | | Max $M_y$ | -11.73 | 0.00 | -0.39 | 0.00 | 0.00 | 0.00 | BC 278 |
| | | | | Min $M_y$ | -8.08 | 0.00 | -0.27 | -0.00 | -0.00 | 0.00 | BC 53 |
| | | | | Max $M_z$ | -0.52 | 0.00 | -0.44 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.52 | 0.00 | -0.44 | 0.00 | 0.00 | 0.00 | BC 1 |
| 170 | RC1 | 66 | 0 | Max N | 67.12 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 432 |
| | | | | Min N | -0.98 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 201 |
| | | | | Max $V_y$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 98 | 2737 | Max N | 67.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 432 |
| | | | | Min N | -0.60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 393 |
| | | | | Max $V_y$ | 0.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 171 | RC1 | 97 | 0 | Max N | 58.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 357 |
| | | | | Min N | -1.36 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 240 |
| | | | | Max $V_y$ | -0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 99 | 2737 | Max N | 58.69 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 357 |
| | | | | Min N | -0.98 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 432 |
| | | | | Max $V_y$ | 0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 172 | RC1 | 99 | 0 | Max N | 74.98 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 240 |
| | | | | Min N | -0.75 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 165 |
| | | | | Max $V_y$ | 13.88 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 13.88 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 13.88 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 13.88 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 13.88 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 13.88 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 13.88 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 13.88 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 13.88 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 13.88 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 96 | 2737 | Max N | 75.39 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 240 |
| | | | | Min N | -0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 357 |
| | | | | Max $V_y$ | 14.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 14.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 14.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 14.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 14.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 14.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 14.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 14.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 14.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 14.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 173 | RC1 | 98 | 0 | Max N | 36.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 357 |
| | | | | Min N | -1.32 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 240 |
| | | | | Max $V_y$ | -0.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 88 | 2737 | Max N | 36.58 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 357 |
| | | | | Min N | -0.92 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 240 |
| | | | | Max $V_y$ | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 174 | RC1 | 101 | 0 | Max N | -0.16 | 0.09 | 7.94 | -0.03 | 0.00 | 0.00 | BC 363 |
| | | | | Min N | -1.39 | 0.04 | 13.97 | -0.06 | 0.00 | 0.00 | BC 436 |
| | | | | Max $V_y$ | -0.74 | 0.53 | 34.58 | -0.10 | 0.00 | -0.00 | BC 149 |
| | | | | Min $V_y$ | -1.15 | -0.07 | 7.93 | -0.05 | 0.00 | 0.00 | BC 408 |
| | | | | Max $V_z$ | -0.74 | 0.53 | 34.58 | -0.10 | 0.00 | 0.00 | BC 134 |
| | | | | Min $V_z$ | -1.15 | -0.07 | 7.93 | -0.05 | -0.00 | 0.00 | BC 468 |
| | | | | Max $M_T$ | -1.11 | 0.21 | 7.94 | -0.02 | 0.00 | 0.00 | BC 390 |
| | | | | Min $M_T$ | -0.81 | 0.52 | 34.57 | -0.10 | -0.00 | 0.00 | BC 154 |
| | | | | Max $M_y$ | -0.43 | 0.31 | 20.01 | -0.06 | 0.00 | -0.00 | BC 304 |
| | | | | Min $M_y$ | -1.29 | 0.02 | 13.97 | -0.06 | -0.00 | 0.00 | BC 368 |
| | | | | Max $M_z$ | -0.71 | 0.45 | 29.75 | -0.09 | 0.00 | 0.00 | BC 122 |
| | | | | Min $M_z$ | -0.68 | 0.44 | 28.54 | -0.09 | -0.00 | -0.00 | BC 136 |
| | | 160 | 3267 | Max N | 0.55 | 0.53 | 0.03 | -0.10 | 56.54 | -1.73 | BC 131 |
| | | | | Min N | -0.98 | -0.05 | 0.08 | -0.04 | 13.09 | 0.17 | BC 448 |
| | | | | Max $V_y$ | 0.54 | 0.53 | 0.03 | -0.10 | 56.54 | -1.74 | BC 149 |
| | | | | Min $V_y$ | -0.85 | -0.07 | 0.07 | -0.05 | 13.08 | 0.22 | BC 408 |
| | | | | Max $V_z$ | 0.18 | 0.23 | 0.13 | -0.04 | 21.68 | -0.76 | BC 10 |
| | | | | Min $V_z$ | 0.43 | 0.46 | -0.01 | -0.09 | 50.42 | -1.49 | BC 346 |
| | | | | Max $M_T$ | -0.81 | 0.21 | 0.08 | -0.02 | 13.09 | -0.70 | BC 390 |
| | | | | Min $M_T$ | 0.48 | 0.52 | 0.03 | -0.10 | 56.53 | -1.70 | BC 154 |
| | | | | Max $M_y$ | 0.55 | 0.53 | 0.03 | -0.10 | 56.54 | -1.73 | BC 134 |
| | | | | Min $M_y$ | -0.86 | -0.07 | 0.07 | -0.05 | 13.08 | 0.22 | BC 468 |
| | | | | Max $M_z$ | -0.85 | -0.07 | 0.07 | -0.05 | 13.08 | 0.22 | BC 408 |
| | | | | Min $M_z$ | 0.54 | 0.53 | 0.03 | -0.10 | 56.54 | -1.74 | BC 149 |
| 175 | RC1 | 75 | 0 | Max N | -61.83 | 0.27 | -1.59 | 0.00 | 34.96 | 0.73 | BC 410 |
| | | | | Min N | -232.32 | -0.05 | 2.03 | -0.03 | 8.83 | -0.24 | BC 149 |
| | | | | Max $V_y$ | -120.92 | 0.61 | -1.29 | -0.03 | 17.08 | 0.18 | BC 439 |
| | | | | Min $V_y$ | -226.79 | -0.31 | 2.07 | -0.03 | 8.98 | -0.47 | BC 147 |
| | | | | Max $V_z$ | -128.40 | -0.17 | 3.64 | -0.02 | -20.52 | -0.34 | BC 205 |
| | | | | Min $V_z$ | -62.04 | 0.22 | -1.64 | 0.00 | 34.74 | 0.57 | BC 450 |
| | | | | Max $M_T$ | -61.83 | 0.27 | -1.59 | 0.00 | 34.96 | 0.73 | BC 410 |
| | | | | Min $M_T$ | -232.32 | -0.05 | 2.03 | -0.03 | 8.83 | -0.24 | BC 149 |
| | | | | Max $M_y$ | -126.41 | 0.26 | -1.26 | 0.00 | 36.43 | 0.68 | BC 206 |
| | | | | Min $M_y$ | -66.08 | -0.03 | 3.04 | -0.01 | -23.13 | -0.30 | BC 449 |
| | | | | Max $M_z$ | -61.83 | 0.27 | -1.59 | 0.00 | 34.96 | 0.73 | BC 410 |
| | | | | Min $M_z$ | -226.79 | -0.31 | 2.07 | -0.03 | 8.98 | -0.47 | BC 147 |
| | | 37 | 3505 | Max N | -54.87 | 0.27 | -17.15 | 0.00 | 2.11 | -0.21 | BC 410 |
| | | | | Min N | -222.11 | -0.05 | 2.03 | -0.03 | 15.95 | -0.06 | BC 149 |
| | | | | Max $V_y$ | -113.96 | 0.61 | -9.73 | -0.03 | -2.23 | -1.94 | BC 439 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 175 | RC1 | | | Min $V_y$ | -216.58 | -0.31 | 2.07 | -0.03 | 16.23 | 0.62 | BC 147 |
| | | | | Max $V_z$ | -118.19 | -0.17 | 17.13 | -0.02 | 15.89 | 0.26 | BC 205 |
| | | | | Min $V_z$ | -55.07 | 0.22 | -17.20 | 0.00 | 1.72 | -0.21 | BC 450 |
| | | | | Max $M_T$ | -54.87 | 0.27 | -17.15 | 0.00 | 2.11 | -0.21 | BC 410 |
| | | | | Min $M_T$ | -222.11 | -0.05 | 2.03 | -0.03 | 15.95 | -0.06 | BC 149 |
| | | | | Max $M_y$ | -216.49 | -0.29 | 2.07 | -0.03 | 16.28 | 0.62 | BC 139 |
| | | | | Min $M_y$ | -77.35 | 0.59 | -9.79 | -0.02 | -2.76 | -1.86 | BC 451 |
| | | | | Max $M_z$ | -216.49 | -0.29 | 2.07 | -0.03 | 16.25 | 0.63 | BC 140 |
| | | | | Min $M_z$ | -140.87 | 0.60 | -9.68 | -0.03 | -1.85 | -1.95 | BC 247 |
| 176 | RC1 | 76 | 0 | Max N | -63.36 | -0.11 | -1.54 | 0.00 | 35.11 | -0.35 | BC 423 |
| | | | Links | Min N | -232.87 | 0.23 | 1.98 | 0.03 | 8.62 | 0.25 | BC 139 |
| | | | | Max $V_y$ | -232.33 | 0.25 | 1.98 | 0.03 | 8.61 | 0.22 | BC 155 |
| | | | | Min $V_y$ | -90.37 | -0.72 | -2.32 | 0.02 | 27.23 | -0.12 | BC 410 |
| | | | | Max $V_z$ | -131.33 | 0.09 | 3.75 | 0.02 | -21.04 | 0.01 | BC 201 |
| | | | | Min $V_z$ | -90.22 | -0.71 | -2.32 | 0.03 | 27.23 | -0.12 | BC 414 |
| | | | | Max $M_T$ | -232.01 | 0.24 | 2.01 | 0.03 | 8.72 | 0.17 | BC 134 |
| | | | | Min $M_T$ | -74.53 | -0.66 | -0.60 | -0.02 | 20.70 | -0.33 | BC 408 |
| | | | | Max $M_y$ | -129.36 | -0.10 | -1.20 | 0.01 | 36.59 | -0.35 | BC 235 |
| | | | | Min $M_y$ | -73.15 | -0.29 | 3.16 | 0.01 | -23.58 | -0.13 | BC 473 |
| | | | | Max $M_z$ | -203.44 | 0.19 | 1.74 | 0.03 | 7.57 | 0.28 | BC 332 |
| | | | | Min $M_z$ | -93.46 | -0.11 | -1.39 | 0.01 | 35.76 | -0.35 | BC 231 |
| | | | 0 | Max N | -63.36 | -0.11 | -1.54 | 0.00 | 35.11 | -0.35 | BC 423 |
| | | | Rechts | Min N | -232.87 | 0.23 | 1.98 | 0.03 | 8.62 | 0.25 | BC 139 |
| | | | | Max $V_y$ | -232.33 | 0.25 | 1.98 | 0.03 | 8.61 | 0.22 | BC 155 |
| | | | | Min $V_y$ | -90.37 | -0.72 | -2.32 | 0.02 | 27.23 | -0.12 | BC 410 |
| | | | | Max $V_z$ | -131.33 | 0.09 | 3.75 | 0.02 | -21.04 | 0.01 | BC 201 |
| | | | | Min $V_z$ | -90.22 | -0.71 | -2.32 | 0.03 | 27.23 | -0.12 | BC 414 |
| | | | | Max $M_T$ | -232.01 | 0.24 | 2.01 | 0.03 | 8.72 | 0.17 | BC 134 |
| | | | | Min $M_T$ | -74.53 | -0.66 | -0.60 | -0.02 | 20.70 | -0.33 | BC 408 |
| | | | | Max $M_y$ | -129.36 | -0.10 | -1.20 | 0.01 | 36.59 | -0.35 | BC 235 |
| | | | | Min $M_y$ | -73.15 | -0.29 | 3.16 | 0.01 | -23.58 | -0.13 | BC 473 |
| | | | | Max $M_z$ | -203.44 | 0.19 | 1.74 | 0.03 | 7.57 | 0.28 | BC 332 |
| | | | | Min $M_z$ | -93.46 | -0.11 | -1.39 | 0.01 | 35.76 | -0.35 | BC 231 |
| | | | 3505 | Max N | -56.30 | -0.11 | -16.87 | 0.00 | 2.78 | 0.06 | BC 423 |
| | | | Links | Min N | -222.52 | 0.23 | 1.98 | 0.03 | 15.57 | -0.57 | BC 139 |
| | | | | Max $V_y$ | -221.99 | 0.25 | 1.98 | 0.03 | 15.56 | -0.64 | BC 155 |
| | | | | Min $V_y$ | -83.32 | -0.72 | -15.98 | 0.02 | -4.91 | 2.40 | BC 410 |
| | | | | Max $V_z$ | -120.98 | 0.09 | 17.41 | 0.02 | 16.09 | -0.30 | BC 201 |
| | | | | Min $V_z$ | -56.53 | -0.09 | -16.92 | 0.00 | 2.35 | 0.07 | BC 415 |
| | | | | Max $M_T$ | -221.66 | 0.24 | 2.01 | 0.03 | 15.76 | -0.67 | BC 134 |
| | | | | Min $M_T$ | -67.47 | -0.66 | -9.14 | -0.02 | 3.59 | 1.98 | BC 408 |
| | | | | Max $M_y$ | -120.98 | 0.09 | 17.41 | 0.02 | 16.09 | -0.30 | BC 201 |
| | | | | Min $M_y$ | -83.17 | -0.71 | -15.98 | 0.03 | -4.91 | 2.38 | BC 414 |
| | | | | Max $M_z$ | -83.32 | -0.72 | -15.98 | 0.02 | -4.91 | 2.40 | BC 410 |
| | | | | Min $M_z$ | -221.65 | 0.24 | 2.01 | 0.03 | 15.76 | -0.67 | BC 149 |
| | | 61 | 3505 | Max N | -56.30 | -0.11 | -16.87 | 0.00 | 2.78 | 0.06 | BC 423 |
| | | | Rechts | Min N | -222.52 | 0.23 | 1.98 | 0.03 | 15.57 | -0.57 | BC 139 |
| | | | | Max $V_y$ | -221.99 | 0.25 | 1.98 | 0.03 | 15.56 | -0.64 | BC 155 |
| | | | | Min $V_y$ | -83.32 | -0.72 | -15.98 | 0.02 | -4.91 | 2.40 | BC 410 |
| | | | | Max $V_z$ | -120.98 | 0.09 | 17.41 | 0.02 | 16.09 | -0.30 | BC 201 |
| | | | | Min $V_z$ | -56.53 | -0.09 | -16.92 | 0.00 | 2.35 | 0.07 | BC 415 |
| | | | | Max $M_T$ | -221.66 | 0.24 | 2.01 | 0.03 | 15.76 | -0.67 | BC 134 |
| | | | | Min $M_T$ | -67.47 | -0.66 | -9.14 | -0.02 | 3.59 | 1.98 | BC 408 |
| | | | | Max $M_y$ | -120.98 | 0.09 | 17.41 | 0.02 | 16.09 | -0.30 | BC 201 |
| | | | | Min $M_y$ | -83.17 | -0.71 | -15.98 | 0.03 | -4.91 | 2.38 | BC 414 |
| | | | | Max $M_z$ | -83.32 | -0.72 | -15.98 | 0.02 | -4.91 | 2.40 | BC 410 |
| | | | | Min $M_z$ | -221.65 | 0.24 | 2.01 | 0.03 | 15.76 | -0.67 | BC 149 |
| 177 | RC1 | 78 | 0 | Max N | -22.08 | -0.25 | -1.99 | 0.00 | 33.22 | -0.76 | BC 415 |
| | | | | Min N | -82.85 | -0.18 | 0.07 | -0.00 | 0.30 | -0.10 | BC 146 |
| | | | | Max $V_y$ | -46.30 | 0.07 | 1.94 | -0.00 | -27.91 | 0.27 | BC 273 |
| | | | | Min $V_y$ | -67.49 | -0.91 | -1.16 | -0.00 | 17.68 | -0.42 | BC 234 |
| | | | | Max $V_z$ | -46.20 | 0.04 | 1.96 | -0.00 | -27.80 | 0.20 | BC 269 |
| | | | | Min $V_z$ | -44.87 | -0.20 | -2.04 | 0.00 | 33.02 | -0.63 | BC 175 |
| | | | | Max $M_T$ | -33.01 | -0.20 | -2.03 | 0.00 | 33.08 | -0.62 | BC 171 |
| | | | | Min $M_T$ | -46.19 | 0.04 | 1.96 | -0.00 | -27.81 | 0.19 | BC 209 |
| | | | | Max $M_y$ | -22.11 | -0.24 | -1.99 | 0.00 | 33.23 | -0.73 | BC 447 |
| | | | | Min $M_y$ | -23.68 | 0.05 | 1.92 | -0.00 | -28.00 | 0.22 | BC 361 |
| | | | | Max $M_z$ | -46.30 | 0.07 | 1.94 | -0.00 | -27.91 | 0.27 | BC 273 |
| | | | | Min $M_z$ | -44.73 | -0.25 | -2.02 | 0.00 | 33.10 | -0.79 | BC 207 |
| | | 65 | 3505 | Max N | -15.12 | -0.25 | -17.55 | 0.00 | -1.02 | 0.12 | BC 415 |
| | | | | Min N | -72.64 | -0.18 | 0.07 | -0.00 | 0.55 | 0.52 | BC 146 |
| | | | | Max $V_y$ | -36.09 | 0.07 | 15.43 | -0.00 | 2.52 | 0.04 | BC 273 |
| | | | | Min $V_y$ | -57.28 | -0.91 | -9.59 | -0.00 | -1.16 | 2.78 | BC 234 |
| | | | | Max $V_z$ | -35.98 | 0.04 | 15.46 | -0.00 | 2.72 | 0.05 | BC 269 |
| | | | | Min $V_z$ | -34.66 | -0.20 | -17.59 | 0.00 | -1.39 | 0.08 | BC 175 |
| | | | | Max $M_T$ | -22.80 | -0.20 | -17.58 | 0.00 | -1.28 | 0.10 | BC 171 |
| | | | | Min $M_T$ | -35.98 | 0.04 | 15.45 | -0.00 | 2.71 | 0.05 | BC 209 |
| | | | | Max $M_y$ | -35.98 | 0.04 | 15.46 | -0.00 | 2.72 | 0.05 | BC 269 |
| | | | | Min $M_y$ | -34.66 | -0.20 | -17.59 | 0.00 | -1.39 | 0.08 | BC 175 |
| | | | | Max $M_z$ | -57.28 | -0.91 | -9.59 | -0.00 | -1.16 | 2.78 | BC 234 |
| | | | | Min $M_z$ | -35.09 | 0.02 | -9.59 | -0.00 | -1.14 | -0.00 | BC 204 |
| 178 | RC1 | 92 | 0 | Max N | -36.37 | -0.15 | -0.03 | -0.00 | -0.07 | -0.08 | BC 49 |
| | | | Links | Min N | -105.67 | -0.45 | -0.00 | -0.00 | -0.00 | -0.18 | BC 154 |
| | | | | Max $V_y$ | -67.76 | 0.73 | 4.84 | 0.00 | 23.54 | 0.66 | BC 360 |
| | | | | Min $V_y$ | -97.84 | -1.40 | 5.42 | 0.00 | 26.02 | -0.92 | BC 269 |
| | | | | Max $V_z$ | -81.27 | -1.37 | 5.43 | 0.00 | 26.05 | -0.92 | BC 461 |
| | | | | Min $V_z$ | -65.51 | -0.17 | -5.06 | -0.00 | -24.35 | -0.06 | BC 187 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 178 | RC1 | | | Max $M_T$ | -84.45 | 0.61 | 4.83 | 0.00 | 23.50 | 0.61 | BC 164 |
| | | | | Min $M_T$ | -66.65 | -0.19 | -5.06 | -0.00 | -24.34 | -0.07 | BC 235 |
| | | | | Max $M_y$ | -81.27 | -1.37 | 5.43 | 0.00 | 26.05 | -0.92 | BC 461 |
| | | | | Min $M_y$ | -65.51 | -0.17 | -5.06 | -0.00 | -24.35 | -0.06 | BC 187 |
| | | | | Max $M_z$ | -67.76 | 0.73 | 4.84 | 0.00 | 23.54 | 0.66 | BC 360 |
| | | | | Min $M_z$ | -81.58 | -1.37 | 5.43 | 0.00 | 26.05 | -0.92 | BC 433 |
| | | | 0 | Max N | -36.37 | -0.15 | -0.03 | -0.00 | -0.07 | -0.08 | BC 49 |
| | | | Rechts | Min N | -105.67 | -0.45 | -0.00 | -0.00 | -0.00 | -0.18 | BC 154 |
| | | | | Max $V_y$ | -67.76 | 0.73 | 4.84 | 0.00 | 23.54 | 0.66 | BC 360 |
| | | | | Min $V_y$ | -97.84 | -1.40 | 5.42 | 0.00 | 26.02 | -0.92 | BC 269 |
| | | | | Max $V_z$ | -81.27 | -1.37 | 5.43 | 0.00 | 26.05 | -0.92 | BC 461 |
| | | | | Min $V_z$ | -65.51 | -0.17 | -5.06 | -0.00 | -24.35 | -0.06 | BC 187 |
| | | | | Max $M_T$ | -84.45 | 0.61 | 4.83 | 0.00 | 23.50 | 0.61 | BC 164 |
| | | | | Min $M_T$ | -66.65 | -0.19 | -5.06 | -0.00 | -24.34 | -0.07 | BC 235 |
| | | | | Max $M_y$ | -81.27 | -1.37 | 5.43 | 0.00 | 26.05 | -0.92 | BC 461 |
| | | | | Min $M_y$ | -65.51 | -0.17 | -5.06 | -0.00 | -24.35 | -0.06 | BC 187 |
| | | | | Max $M_z$ | -67.76 | 0.73 | 4.84 | 0.00 | 23.54 | 0.66 | BC 360 |
| | | | | Min $M_z$ | -81.58 | -1.37 | 5.43 | 0.00 | 26.05 | -0.92 | BC 433 |
| | | | 328 | Max N | -36.11 | -0.15 | -0.03 | -0.00 | -0.08 | -0.03 | BC 49 |
| | | | Links | Min N | -105.29 | -0.45 | -0.00 | -0.00 | -0.01 | -0.04 | BC 154 |
| | | | | Max $V_y$ | -67.50 | 0.73 | 3.04 | 0.00 | 24.83 | 0.42 | BC 360 |
| | | | | Min $V_y$ | -97.46 | -1.40 | 3.44 | 0.00 | 27.47 | -0.46 | BC 269 |
| | | | | Max $V_z$ | -81.01 | -1.37 | 3.45 | 0.00 | 27.51 | -0.47 | BC 461 |
| | | | | Min $V_z$ | -65.13 | -0.17 | -3.20 | -0.00 | -25.70 | -0.01 | BC 187 |
| | | | | Max $M_T$ | -84.07 | 0.61 | 3.02 | 0.00 | 24.79 | 0.40 | BC 164 |
| | | | | Min $M_T$ | -66.27 | -0.19 | -3.20 | -0.00 | -25.69 | -0.01 | BC 235 |
| | | | | Max $M_y$ | -81.01 | -1.37 | 3.45 | 0.00 | 27.51 | -0.47 | BC 461 |
| | | | | Min $M_y$ | -65.13 | -0.17 | -3.20 | -0.00 | -25.70 | -0.01 | BC 187 |
| | | | | Max $M_z$ | -67.50 | 0.73 | 3.04 | 0.00 | 24.83 | 0.42 | BC 360 |
| | | | | Min $M_z$ | -81.32 | -1.37 | 3.45 | 0.00 | 27.51 | -0.47 | BC 433 |
| | | | 328 | Max N | -36.11 | -0.15 | -0.03 | -0.00 | -0.08 | -0.03 | BC 49 |
| | | | Rechts | Min N | -105.29 | -0.45 | -0.00 | -0.00 | -0.01 | -0.04 | BC 154 |
| | | | | Max $V_y$ | -67.50 | 0.73 | 3.04 | 0.00 | 24.83 | 0.42 | BC 360 |
| | | | | Min $V_y$ | -97.46 | -1.40 | 3.44 | 0.00 | 27.47 | -0.46 | BC 269 |
| | | | | Max $V_z$ | -81.01 | -1.37 | 3.45 | 0.00 | 27.51 | -0.47 | BC 461 |
| | | | | Min $V_z$ | -65.13 | -0.17 | -3.20 | -0.00 | -25.70 | -0.01 | BC 187 |
| | | | | Max $M_T$ | -84.07 | 0.61 | 3.02 | 0.00 | 24.79 | 0.40 | BC 164 |
| | | | | Min $M_T$ | -66.27 | -0.19 | -3.20 | -0.00 | -25.69 | -0.01 | BC 235 |
| | | | | Max $M_y$ | -81.01 | -1.37 | 3.45 | 0.00 | 27.51 | -0.47 | BC 461 |
| | | | | Min $M_y$ | -65.13 | -0.17 | -3.20 | -0.00 | -25.70 | -0.01 | BC 187 |
| | | | | Max $M_z$ | -67.50 | 0.73 | 3.04 | 0.00 | 24.83 | 0.42 | BC 360 |
| | | | | Min $M_z$ | -81.32 | -1.37 | 3.45 | 0.00 | 27.51 | -0.47 | BC 433 |
| | | | 2172 | Max N | -31.43 | -0.15 | -0.03 | -0.00 | -0.14 | 0.24 | BC 49 |
| | | | Links | Min N | -98.42 | -0.45 | -0.00 | -0.00 | -0.01 | 0.78 | BC 154 |
| | | | | Max $V_y$ | -62.81 | 0.73 | -7.14 | 0.00 | 21.05 | -0.92 | BC 360 |
| | | | | Min $V_y$ | -90.59 | -1.40 | -7.71 | 0.00 | 23.53 | 2.12 | BC 269 |
| | | | | Max $V_z$ | -50.71 | -0.27 | 7.30 | -0.00 | -21.73 | 0.47 | BC 463 |
| | | | | Min $V_z$ | -71.78 | -1.27 | -7.75 | 0.00 | 23.34 | 1.91 | BC 169 |
| | | | | Max $M_T$ | -77.20 | 0.61 | -7.15 | 0.00 | 20.98 | -0.73 | BC 164 |
| | | | | Min $M_T$ | -59.40 | -0.19 | 7.24 | -0.00 | -21.97 | 0.34 | BC 235 |
| | | | | Max $M_y$ | -76.32 | -1.37 | -7.69 | 0.00 | 23.60 | 2.06 | BC 461 |
| | | | | Min $M_y$ | -58.26 | -0.17 | 7.24 | -0.00 | -21.97 | 0.30 | BC 187 |
| | | | | Max $M_z$ | -90.59 | -1.40 | -7.71 | 0.00 | 23.53 | 2.12 | BC 269 |
| | | | | Min $M_z$ | -62.81 | 0.73 | -7.14 | 0.00 | 21.05 | -0.92 | BC 360 |
| | | 80 | 2172 | Max N | -31.43 | -0.15 | -0.03 | -0.00 | -0.14 | 0.24 | BC 49 |
| | | | Rechts | Min N | -98.42 | -0.45 | -0.00 | -0.00 | -0.01 | 0.78 | BC 154 |
| | | | | Max $V_y$ | -62.81 | 0.73 | -7.14 | 0.00 | 21.05 | -0.92 | BC 360 |
| | | | | Min $V_y$ | -90.59 | -1.40 | -7.71 | 0.00 | 23.53 | 2.12 | BC 269 |
| | | | | Max $V_z$ | -50.71 | -0.27 | 7.30 | -0.00 | -21.73 | 0.47 | BC 463 |
| | | | | Min $V_z$ | -71.78 | -1.27 | -7.75 | 0.00 | 23.34 | 1.91 | BC 169 |
| | | | | Max $M_T$ | -77.20 | 0.61 | -7.15 | 0.00 | 20.98 | -0.73 | BC 164 |
| | | | | Min $M_T$ | -59.40 | -0.19 | 7.24 | -0.00 | -21.97 | 0.34 | BC 235 |
| | | | | Max $M_y$ | -76.32 | -1.37 | -7.69 | 0.00 | 23.60 | 2.06 | BC 461 |
| | | | | Min $M_y$ | -58.26 | -0.17 | 7.24 | -0.00 | -21.97 | 0.30 | BC 187 |
| | | | | Max $M_z$ | -90.59 | -1.40 | -7.71 | 0.00 | 23.53 | 2.12 | BC 269 |
| | | | | Min $M_z$ | -62.81 | 0.73 | -7.14 | 0.00 | 21.05 | -0.92 | BC 360 |
| 179 | RC1 | 95 | 0 | Max N | -2.31 | 0.59 | 0.00 | -0.00 | 0.01 | 0.28 | BC 356 |
| | | | | Min N | -47.93 | -0.52 | 0.00 | -0.00 | 0.01 | -0.26 | BC 241 |
| | | | | Max $V_y$ | -3.48 | 0.64 | 0.00 | -0.00 | 0.01 | 0.31 | BC 168 |
| | | | | Min $V_y$ | -45.69 | -0.55 | 0.00 | -0.00 | 0.01 | -0.28 | BC 433 |
| | | | | Max $V_z$ | -39.28 | -0.50 | 0.00 | -0.00 | 0.01 | -0.26 | BC 377 |
| | | | | Min $V_z$ | -11.01 | 0.07 | -0.00 | 0.00 | -0.01 | 0.05 | BC 279 |
| | | | | Max $M_T$ | -6.25 | 0.09 | -0.00 | 0.00 | -0.01 | 0.04 | BC 167 |
| | | | | Min $M_T$ | -47.93 | -0.52 | 0.00 | -0.00 | 0.01 | -0.26 | BC 241 |
| | | | | Max $M_y$ | -44.51 | -0.54 | 0.00 | -0.00 | 0.01 | -0.27 | BC 397 |
| | | | | Min $M_y$ | -8.34 | 0.07 | -0.00 | 0.00 | -0.01 | 0.03 | BC 247 |
| | | | | Max $M_z$ | -3.66 | 0.63 | 0.00 | -0.00 | 0.01 | 0.32 | BC 276 |
| | | | | Min $M_z$ | -45.69 | -0.55 | 0.00 | -0.00 | 0.01 | -0.28 | BC 433 |
| | | 93 | 2173 | Max N | -1.61 | 0.59 | 0.00 | -0.00 | 0.01 | -1.00 | BC 356 |
| | | | | Min N | -46.91 | -0.52 | 0.00 | -0.00 | 0.02 | 0.87 | BC 241 |
| | | | | Max $V_y$ | -2.46 | 0.64 | 0.00 | -0.00 | 0.01 | -1.08 | BC 168 |
| | | | | Min $V_y$ | -44.99 | -0.55 | 0.00 | -0.00 | 0.02 | 0.92 | BC 433 |
| | | | | Max $V_z$ | -38.59 | -0.50 | 0.00 | -0.00 | 0.02 | 0.82 | BC 377 |
| | | | | Min $V_z$ | -9.99 | 0.07 | -0.00 | 0.00 | -0.01 | -0.10 | BC 279 |
| | | | | Max $M_T$ | -5.23 | 0.09 | -0.00 | 0.00 | -0.01 | -0.15 | BC 167 |
| | | | | Min $M_T$ | -46.91 | -0.52 | 0.00 | -0.00 | 0.02 | 0.87 | BC 241 |
| | | | | Max $M_y$ | -44.23 | -0.54 | 0.00 | -0.00 | 0.02 | 0.91 | BC 401 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 179 | RC1 | | | Min $M_y$ | -11.80 | 0.04 | -0.00 | 0.00 | -0.01 | -0.05 | BC 239 |
| | | | | Max $M_z$ | -44.99 | -0.55 | 0.00 | -0.00 | 0.02 | 0.92 | BC 433 |
| | | | | Min $M_z$ | -2.46 | 0.64 | 0.00 | -0.00 | 0.01 | -1.08 | BC 168 |
| 180 | RC1 | 91 | 0 | Max N | -2.42 | -0.59 | 0.00 | -0.00 | 0.01 | -0.27 | BC 389 |
| | | | | Min N | -43.41 | 0.32 | 0.00 | -0.00 | 0.01 | 0.18 | BC 264 |
| | | | | Max $V_y$ | -38.82 | 0.43 | 0.00 | -0.00 | 0.01 | 0.24 | BC 392 |
| | | | | Min $V_y$ | -4.12 | -0.76 | 0.00 | -0.00 | 0.01 | -0.37 | BC 241 |
| | | | | Max $V_z$ | -2.47 | -0.60 | 0.00 | -0.00 | 0.01 | -0.28 | BC 377 |
| | | | | Min $V_z$ | -10.55 | -0.18 | -0.00 | 0.00 | -0.01 | -0.09 | BC 267 |
| | | | | Max $M_T$ | -7.90 | -0.13 | -0.00 | 0.00 | -0.01 | -0.06 | BC 443 |
| | | | | Min $M_T$ | -3.74 | -0.66 | 0.00 | -0.00 | 0.01 | -0.31 | BC 185 |
| | | | | Max $M_y$ | -2.85 | -0.70 | 0.00 | -0.00 | 0.01 | -0.34 | BC 433 |
| | | | | Min $M_y$ | -8.29 | -0.12 | -0.00 | 0.00 | -0.01 | -0.05 | BC 287 |
| | | | | Max $M_z$ | -38.21 | 0.43 | 0.00 | -0.00 | 0.01 | 0.24 | BC 360 |
| | | | | Min $M_z$ | -4.12 | -0.76 | 0.00 | -0.00 | 0.01 | -0.37 | BC 241 |
| | | 89 | 2173 | Max N | -1.73 | -0.59 | 0.00 | -0.00 | 0.01 | 1.00 | BC 389 |
| | | | | Min N | -42.39 | 0.32 | 0.00 | -0.00 | 0.01 | -0.52 | BC 264 |
| | | | | Max $V_y$ | -38.12 | 0.43 | 0.00 | -0.00 | 0.01 | -0.70 | BC 392 |
| | | | | Min $V_y$ | -3.10 | -0.76 | 0.00 | -0.00 | 0.01 | 1.28 | BC 241 |
| | | | | Max $V_z$ | -1.78 | -0.60 | 0.00 | -0.00 | 0.01 | 1.02 | BC 377 |
| | | | | Min $V_z$ | -9.53 | -0.18 | -0.00 | 0.00 | -0.01 | 0.30 | BC 267 |
| | | | | Max $M_T$ | -7.21 | -0.13 | -0.00 | 0.00 | -0.01 | 0.21 | BC 443 |
| | | | | Min $M_T$ | -2.72 | -0.66 | 0.00 | -0.00 | 0.01 | 1.13 | BC 185 |
| | | | | Max $M_y$ | -1.78 | -0.60 | 0.00 | -0.00 | 0.01 | 1.02 | BC 377 |
| | | | | Min $M_y$ | -9.53 | -0.18 | -0.00 | 0.00 | -0.01 | 0.30 | BC 267 |
| | | | | Max $M_z$ | -3.10 | -0.76 | 0.00 | -0.00 | 0.01 | 1.28 | BC 241 |
| | | | | Min $M_z$ | -38.12 | 0.43 | 0.00 | -0.00 | 0.01 | -0.70 | BC 392 |
| 181 | RC1 | 99 | 0 | Max N | -42.60 | -2.58 | -2.25 | 0.00 | -0.82 | 5.60 | BC 444 |
| | | | | Min N | -221.45 | -0.02 | -9.55 | 0.00 | 3.37 | 0.05 | BC 138 |
| | | | | Max $V_y$ | -99.11 | 2.68 | -5.96 | 0.00 | 1.37 | -5.81 | BC 431 |
| | | | | Min $V_y$ | -123.11 | -2.83 | -12.90 | 0.00 | 4.51 | 6.14 | BC 225 |
| | | | | Max $V_z$ | -44.65 | -2.61 | 1.62 | 0.00 | -1.06 | 5.67 | BC 360 |
| | | | | Min $V_z$ | -139.28 | -2.79 | -17.33 | 0.00 | 4.30 | 6.06 | BC 269 |
| | | | | Max $M_T$ | -64.14 | 2.64 | -1.36 | 0.00 | 0.57 | -5.72 | BC 419 |
| | | | | Min $M_T$ | -99.11 | -2.82 | -10.64 | 0.00 | 3.92 | 6.12 | BC 421 |
| | | | | Max $M_y$ | -153.76 | -2.83 | -13.81 | 0.00 | 4.77 | 6.14 | BC 213 |
| | | | | Min $M_y$ | -44.05 | -2.61 | 1.50 | 0.00 | -1.10 | 5.67 | BC 388 |
| | | | | Max $M_z$ | -123.11 | -2.83 | -12.90 | 0.00 | 4.51 | 6.14 | BC 225 |
| | | | | Min $M_z$ | -99.11 | 2.68 | -5.96 | 0.00 | 1.37 | -5.81 | BC 431 |
| | | 88 | 2173 | Max N | -40.86 | -2.58 | -2.25 | 0.00 | -5.71 | 11.20 | BC 444 |
| | | | | Min N | -218.91 | -0.02 | -9.55 | 0.00 | -17.36 | 0.09 | BC 138 |
| | | | | Max $V_y$ | -97.38 | 2.68 | -5.96 | 0.00 | -11.57 | -11.62 | BC 431 |
| | | | | Min $V_y$ | -120.57 | -2.83 | -12.90 | 0.00 | -23.51 | 12.29 | BC 225 |
| | | | | Max $V_z$ | -42.91 | -2.61 | 1.62 | 0.00 | 2.46 | 11.35 | BC 360 |
| | | | | Min $V_z$ | -136.74 | -2.79 | -17.33 | 0.00 | -33.36 | 12.12 | BC 269 |
| | | | | Max $M_T$ | -62.40 | 2.64 | -1.36 | 0.00 | -2.39 | -11.45 | BC 419 |
| | | | | Min $M_T$ | -97.38 | -2.82 | -10.64 | 0.00 | -19.19 | 12.24 | BC 421 |
| | | | | Max $M_y$ | -42.91 | -2.61 | 1.62 | 0.00 | 2.46 | 11.35 | BC 360 |
| | | | | Min $M_y$ | -136.74 | -2.79 | -17.33 | 0.00 | -33.36 | 12.12 | BC 269 |
| | | | | Max $M_z$ | -120.57 | -2.83 | -12.90 | 0.00 | -23.51 | 12.29 | BC 225 |
| | | | | Min $M_z$ | -97.38 | 2.68 | -5.96 | 0.00 | -11.57 | -11.62 | BC 431 |
| 182 | RC1 | 98 | 0 | Max N | -4.03 | -0.89 | 0.00 | -0.00 | 0.01 | -0.37 | BC 361 |
| | | | | Min N | -65.63 | 0.26 | 0.00 | -0.00 | 0.01 | 0.22 | BC 268 |
| | | | | Max $V_y$ | -46.20 | 0.44 | 0.00 | -0.00 | 0.01 | 0.24 | BC 376 |
| | | | | Min $V_y$ | -7.57 | -1.10 | 0.00 | -0.00 | 0.01 | -0.39 | BC 265 |
| | | | | Max $V_z$ | -7.16 | -1.09 | 0.00 | -0.00 | 0.01 | -0.38 | BC 217 |
| | | | | Min $V_z$ | -24.90 | -0.24 | -0.00 | 0.00 | -0.01 | -0.09 | BC 247 |
| | | | | Max $M_T$ | -27.50 | -0.22 | -0.00 | 0.00 | -0.01 | -0.05 | BC 415 |
| | | | | Min $M_T$ | -4.18 | -0.89 | 0.00 | -0.00 | 0.01 | -0.36 | BC 417 |
| | | | | Max $M_y$ | -5.95 | -1.02 | 0.00 | -0.00 | 0.01 | -0.40 | BC 225 |
| | | | | Min $M_y$ | -27.19 | -0.22 | -0.00 | 0.00 | -0.01 | -0.06 | BC 443 |
| | | | | Max $M_z$ | -56.62 | 0.37 | 0.00 | -0.00 | 0.01 | 0.26 | BC 444 |
| | | | | Min $M_z$ | -6.17 | -1.04 | 0.00 | -0.00 | 0.01 | -0.42 | BC 201 |
| | | 96 | 2173 | Max N | -3.33 | -0.89 | 0.00 | -0.00 | 0.01 | 1.56 | BC 361 |
| | | | | Min N | -64.61 | 0.26 | 0.00 | -0.00 | 0.01 | -0.35 | BC 268 |
| | | | | Max $V_y$ | -45.50 | 0.44 | 0.00 | -0.00 | 0.01 | -0.71 | BC 376 |
| | | | | Min $V_y$ | -6.55 | -1.10 | 0.00 | -0.00 | 0.01 | 2.00 | BC 265 |
| | | | | Max $V_z$ | -6.14 | -1.09 | 0.00 | -0.00 | 0.01 | 1.98 | BC 217 |
| | | | | Min $V_z$ | -23.88 | -0.24 | -0.00 | 0.00 | -0.01 | 0.43 | BC 247 |
| | | | | Max $M_T$ | -26.81 | -0.22 | -0.00 | 0.00 | -0.01 | 0.43 | BC 415 |
| | | | | Min $M_T$ | -3.49 | -0.89 | 0.00 | -0.00 | 0.01 | 1.57 | BC 417 |
| | | | | Max $M_y$ | -4.84 | -1.03 | 0.00 | -0.00 | 0.01 | 1.82 | BC 165 |
| | | | | Min $M_y$ | -31.85 | -0.21 | -0.00 | 0.00 | -0.01 | 0.40 | BC 435 |
| | | | | Max $M_z$ | -6.55 | -1.10 | 0.00 | -0.00 | 0.01 | 2.00 | BC 265 |
| | | | | Min $M_z$ | -45.50 | 0.44 | 0.00 | -0.00 | 0.01 | -0.71 | BC 376 |
| 183 | RC1 | 145 | 0 | Max N | 3.92 | 0.15 | -0.20 | -0.00 | 26.16 | 0.49 | BC 243 |
| | | | | Min N | -3.67 | 0.02 | -0.13 | 0.02 | 11.62 | 0.06 | BC 360 |
| | | | | Max $V_y$ | 3.83 | 0.16 | -0.20 | -0.00 | 26.15 | 0.53 | BC 175 |
| | | | | Min $V_y$ | 2.96 | -0.19 | -0.19 | 0.00 | 17.04 | -0.60 | BC 253 |
| | | | | Max $V_z$ | 2.76 | -0.18 | -0.13 | 0.00 | 11.61 | -0.58 | BC 417 |
| | | | | Min $V_z$ | 0.24 | 0.04 | -0.24 | 0.00 | 51.70 | 0.12 | BC 147 |
| | | | | Max $M_T$ | -3.67 | 0.02 | -0.19 | 0.02 | 17.03 | 0.08 | BC 168 |
| | | | | Min $M_T$ | 3.87 | 0.14 | -0.13 | -0.00 | 11.62 | 0.44 | BC 475 |
| | | | | Max $M_y$ | 0.24 | 0.04 | -0.24 | 0.00 | 51.70 | 0.12 | BC 147 |
| | | | | Min $M_y$ | 2.76 | -0.18 | -0.13 | 0.00 | 11.61 | -0.58 | BC 417 |
| | | | | Max $M_z$ | 3.83 | 0.16 | -0.20 | -0.00 | 26.15 | 0.53 | BC 175 |
| | | | | Min $M_z$ | 2.96 | -0.19 | -0.19 | 0.00 | 17.04 | -0.60 | BC 253 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 183 | RC1 | 41 | 3201 | Max N | 4.22 | 0.15 | -16.14 | -0.00 | 0.00 | 0.00 | BC 243 |
| | | | | Min N | -3.54 | 0.02 | -7.13 | 0.02 | 0.00 | 0.00 | BC 360 |
| | | | | Max $V_y$ | 4.13 | 0.16 | -16.14 | -0.00 | 0.00 | 0.00 | BC 175 |
| | | | | Min $V_y$ | 3.15 | -0.19 | -10.46 | 0.00 | 0.00 | 0.00 | BC 253 |
| | | | | Max $V_z$ | 2.89 | -0.18 | -7.13 | 0.00 | -0.00 | 0.00 | BC 417 |
| | | | | Min $V_z$ | 0.84 | 0.04 | -32.07 | 0.00 | -0.00 | 0.00 | BC 147 |
| | | | | Max $M_T$ | -3.48 | 0.02 | -10.45 | 0.02 | -0.00 | 0.00 | BC 168 |
| | | | | Min $M_T$ | 4.00 | 0.14 | -7.13 | -0.00 | 0.00 | 0.00 | BC 475 |
| | | | | Max $M_y$ | 0.40 | 0.03 | -16.14 | 0.00 | 0.00 | 0.00 | BC 70 |
| | | | | Min $M_y$ | 1.78 | 0.02 | -10.45 | 0.01 | -0.00 | 0.00 | BC 226 |
| | | | | Max $M_z$ | 0.29 | 0.03 | -11.80 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.29 | 0.03 | -11.80 | 0.00 | -0.00 | 0.00 | BC 1 |
| 184 | RC1 | 146 | 0 | Max N | 12.38 | 0.21 | 15.60 | -0.12 | 76.25 | 0.05 | BC 450 |
| | | | | Min N | -24.85 | 0.08 | 27.23 | 0.03 | 132.00 | 0.02 | BC 392 |
| | | | | Max $V_y$ | -5.49 | 0.22 | 15.32 | 0.08 | 75.34 | 0.13 | BC 359 |
| | | | | Min $V_y$ | 6.31 | -0.35 | 33.94 | 0.01 | 165.57 | -0.18 | BC 241 |
| | | | | Max $V_z$ | -1.02 | 0.02 | 67.40 | 0.02 | 324.63 | 0.12 | BC 134 |
| | | | | Min $V_z$ | 6.21 | -0.31 | 14.95 | -0.01 | 73.99 | -0.19 | BC 469 |
| | | | | Max $M_T$ | -0.26 | 0.14 | 27.09 | 0.09 | 131.48 | 0.16 | BC 435 |
| | | | | Min $M_T$ | 12.34 | 0.21 | 15.58 | -0.13 | 76.15 | 0.01 | BC 446 |
| | | | | Max $M_y$ | -1.02 | 0.02 | 67.40 | 0.02 | 324.63 | 0.12 | BC 134 |
| | | | | Min $M_y$ | 6.13 | -0.32 | 14.95 | -0.01 | 73.99 | -0.19 | BC 473 |
| | | | | Max $M_z$ | 1.26 | 0.19 | 34.34 | 0.08 | 167.00 | 0.18 | BC 247 |
| | | | | Min $M_z$ | 7.27 | -0.29 | 22.18 | -0.01 | 109.48 | -0.20 | BC 161 |
| | | 84 | 3201 | Max N | 12.64 | 0.21 | 1.31 | -0.12 | 103.30 | -0.63 | BC 450 |
| | | | | Min N | -24.36 | 0.08 | 1.32 | 0.03 | 177.70 | -0.22 | BC 392 |
| | | | | Max $V_y$ | -5.22 | 0.22 | 1.02 | 0.08 | 101.49 | -0.59 | BC 359 |
| | | | | Min $V_y$ | 6.92 | -0.35 | 1.36 | 0.01 | 222.06 | 0.93 | BC 241 |
| | | | | Max $V_z$ | 0.20 | 0.02 | 2.30 | 0.02 | 436.17 | 0.05 | BC 134 |
| | | | | Min $V_z$ | 6.48 | -0.31 | 0.65 | -0.01 | 98.95 | 0.81 | BC 469 |
| | | | | Max $M_T$ | 0.23 | 0.14 | 1.18 | 0.09 | 176.72 | -0.31 | BC 435 |
| | | | | Min $M_T$ | 12.61 | 0.21 | 1.28 | -0.13 | 103.13 | -0.68 | BC 446 |
| | | | | Max $M_y$ | 0.20 | 0.02 | 2.30 | 0.02 | 436.17 | 0.05 | BC 134 |
| | | | | Min $M_y$ | 6.39 | -0.32 | 0.65 | -0.01 | 98.95 | 0.84 | BC 473 |
| | | | | Max $M_z$ | 6.92 | -0.35 | 1.36 | 0.01 | 222.06 | 0.93 | BC 241 |
| | | | | Min $M_z$ | 12.60 | 0.21 | 1.28 | -0.13 | 103.11 | -0.68 | BC 474 |
| 185 | RC1 | 147 | 0 | Max N | 16.59 | -0.27 | 15.88 | 0.17 | 77.80 | 0.11 | BC 411 |
| | | | | Min N | -18.20 | -0.01 | 34.81 | 0.06 | 169.94 | 0.08 | BC 244 |
| | | | | Max $V_y$ | -18.05 | 0.01 | 27.47 | 0.04 | 133.94 | 0.05 | BC 432 |
| | | | | Min $V_y$ | 16.59 | -0.27 | 15.88 | 0.17 | 77.80 | 0.11 | BC 411 |
| | | | | Max $V_z$ | -2.93 | -0.04 | 68.77 | 0.04 | 332.04 | 0.14 | BC 131 |
| | | | | Min $V_z$ | -17.19 | -0.00 | 15.42 | 0.04 | 76.32 | 0.04 | BC 472 |
| | | | | Max $M_T$ | 16.53 | -0.27 | 15.95 | 0.17 | 78.01 | 0.14 | BC 391 |
| | | | | Min $M_T$ | -7.94 | -0.14 | 15.64 | -0.02 | 76.99 | 0.14 | BC 450 |
| | | | | Max $M_y$ | -2.93 | -0.04 | 68.77 | 0.04 | 332.04 | 0.14 | BC 131 |
| | | | | Min $M_y$ | -17.50 | 0.00 | 15.42 | 0.04 | 76.31 | 0.04 | BC 444 |
| | | | | Max $M_z$ | 16.03 | -0.19 | 35.27 | 0.14 | 171.48 | 0.16 | BC 175 |
| | | | | Min $M_z$ | -10.26 | -0.09 | 15.64 | -0.01 | 77.16 | -0.14 | BC 473 |
| | | 83 | 3201 | Max N | 16.86 | -0.27 | 1.34 | 0.17 | 105.35 | 0.97 | BC 411 |
| | | | | Min N | -17.58 | -0.01 | 1.60 | 0.06 | 228.21 | 0.11 | BC 244 |
| | | | | Max $V_y$ | -17.56 | 0.01 | 1.05 | 0.04 | 179.59 | 0.02 | BC 432 |
| | | | | Min $V_y$ | 16.86 | -0.27 | 1.34 | 0.17 | 105.35 | 0.97 | BC 411 |
| | | | | Max $V_z$ | -1.68 | -0.04 | 2.31 | 0.04 | 445.78 | 0.27 | BC 131 |
| | | | | Min $V_z$ | -16.92 | -0.00 | 0.88 | 0.04 | 102.40 | 0.04 | BC 472 |
| | | | | Max $M_T$ | 16.80 | -0.27 | 1.41 | 0.17 | 105.80 | 0.99 | BC 391 |
| | | | | Min $M_T$ | -7.67 | -0.14 | 1.10 | -0.02 | 103.78 | 0.58 | BC 450 |
| | | | | Max $M_y$ | -1.68 | -0.04 | 2.31 | 0.04 | 445.78 | 0.27 | BC 131 |
| | | | | Min $M_y$ | -17.23 | 0.00 | 0.88 | 0.04 | 102.40 | 0.03 | BC 444 |
| | | | | Max $M_z$ | 16.80 | -0.27 | 1.41 | 0.17 | 105.80 | 0.99 | BC 363 |
| | | | | Min $M_z$ | -17.56 | 0.01 | 1.05 | 0.04 | 179.59 | 0.02 | BC 432 |
| 186 | RC1 | 148 | 0 | Max N | 16.02 | 0.41 | 37.84 | -0.59 | 151.55 | -0.05 | BC 410 |
| | | | | Min N | -49.75 | 0.98 | 78.72 | -0.02 | 315.47 | -0.43 | BC 244 |
| | | | | Max $V_y$ | -48.38 | 1.36 | 146.18 | -0.65 | 584.42 | -0.68 | BC 139 |
| | | | | Min $V_y$ | -13.10 | -0.10 | 36.32 | -0.06 | 146.82 | -0.06 | BC 421 |
| | | | | Max $V_z$ | -48.51 | 1.35 | 146.18 | -0.65 | 584.42 | -0.68 | BC 140 |
| | | | | Min $V_z$ | -12.99 | -0.10 | 36.32 | -0.06 | 146.82 | -0.06 | BC 361 |
| | | | | Max $M_T$ | -36.01 | 0.62 | 37.27 | 0.17 | 149.70 | -0.23 | BC 360 |
| | | | | Min $M_T$ | -48.56 | 1.35 | 146.18 | -0.65 | 584.42 | -0.68 | BC 155 |
| | | | | Max $M_y$ | -48.51 | 1.35 | 146.18 | -0.65 | 584.42 | -0.68 | BC 140 |
| | | | | Min $M_y$ | -13.10 | -0.10 | 36.32 | -0.06 | 146.82 | -0.06 | BC 421 |
| | | | | Max $M_z$ | -11.92 | -0.07 | 36.34 | -0.05 | 146.92 | -0.02 | BC 409 |
| | | | | Min $M_z$ | -48.55 | 1.36 | 146.18 | -0.65 | 584.42 | -0.68 | BC 132 |
| | | 82 | 3201 | Max N | 16.34 | 0.41 | 20.95 | -0.59 | 245.62 | -1.35 | BC 410 |
| | | | | Min N | -49.06 | 0.98 | 42.07 | -0.02 | 508.76 | -3.58 | BC 244 |
| | | | | Max $V_y$ | -47.07 | 1.36 | 76.27 | -0.65 | 940.40 | -5.02 | BC 139 |
| | | | | Min $V_y$ | -12.78 | -0.10 | 19.43 | -0.06 | 236.02 | 0.25 | BC 421 |
| | | | | Max $V_z$ | -47.20 | 1.35 | 76.27 | -0.65 | 940.40 | -5.01 | BC 140 |
| | | | | Min $V_z$ | -12.68 | -0.10 | 19.43 | -0.06 | 236.03 | 0.25 | BC 361 |
| | | | | Max $M_T$ | -35.69 | 0.62 | 20.38 | 0.17 | 241.97 | -2.21 | BC 360 |
| | | | | Min $M_T$ | -47.25 | 1.35 | 76.27 | -0.65 | 940.39 | -5.00 | BC 155 |
| | | | | Max $M_y$ | -47.20 | 1.35 | 76.27 | -0.65 | 940.40 | -5.01 | BC 140 |
| | | | | Min $M_y$ | -12.78 | -0.10 | 19.43 | -0.06 | 236.02 | 0.25 | BC 421 |
| | | | | Max $M_z$ | -12.68 | -0.10 | 19.43 | -0.06 | 236.03 | 0.25 | BC 361 |
| | | | | Min $M_z$ | -47.07 | 1.36 | 76.27 | -0.65 | 940.40 | -5.02 | BC 139 |
| 187 | RC1 | 149 | 0 | Max N | 11.74 | -0.42 | 36.96 | 0.55 | 148.23 | -0.05 | BC 451 |
| | | | | Min N | -52.70 | -0.81 | 77.45 | 0.29 | 310.21 | 0.53 | BC 204 |
| | | | | Max $V_y$ | -4.61 | 0.59 | 35.50 | 0.14 | 143.41 | -0.11 | BC 473 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 187 | RC1 | | | Min $V_y$ | -49.32 | -1.24 | 142.90 | 0.64 | 571.31 | 0.62 | BC 149 |
| | | | | Max $V_z$ | -49.32 | -1.24 | 142.90 | 0.64 | 571.31 | 0.62 | BC 149 |
| | | | | Min $V_z$ | -4.72 | 0.59 | 35.50 | 0.14 | 143.41 | -0.11 | BC 413 |
| | | | | Max $M_T$ | -49.64 | -1.23 | 142.89 | 0.64 | 571.29 | 0.62 | BC 141 |
| | | | | Min $M_T$ | -10.58 | -0.60 | 36.03 | -0.23 | 145.26 | 0.04 | BC 450 |
| | | | | Max $M_y$ | -49.32 | -1.24 | 142.90 | 0.64 | 571.31 | 0.62 | BC 149 |
| | | | | Min $M_y$ | -4.72 | 0.59 | 35.50 | 0.14 | 143.41 | -0.11 | BC 413 |
| | | | | Max $M_z$ | -50.67 | -1.23 | 142.88 | 0.64 | 571.21 | 0.63 | BC 148 |
| | | | | Min $M_z$ | -3.33 | 0.58 | 35.53 | 0.15 | 143.52 | -0.12 | BC 449 |
| | | 81 | 3201 | Max N | 12.06 | -0.42 | 20.32 | 0.55 | 239.90 | 1.31 | BC 451 |
| | | | | Min N | -52.03 | -0.81 | 41.42 | 0.29 | 500.43 | 3.11 | BC 204 |
| | | | | Max $V_y$ | -4.30 | 0.59 | 18.86 | 0.14 | 230.40 | -2.01 | BC 473 |
| | | | | Min $V_y$ | -48.03 | -1.24 | 74.35 | 0.64 | 918.97 | 4.58 | BC 149 |
| | | | | Max $V_z$ | -48.03 | -1.24 | 74.35 | 0.64 | 918.97 | 4.58 | BC 149 |
| | | | | Min $V_z$ | -4.40 | 0.59 | 18.86 | 0.14 | 230.40 | -2.01 | BC 413 |
| | | | | Max $M_T$ | -48.36 | -1.23 | 74.34 | 0.64 | 918.91 | 4.55 | BC 141 |
| | | | | Min $M_T$ | -10.27 | -0.60 | 19.39 | -0.23 | 233.95 | 1.95 | BC 450 |
| | | | | Max $M_y$ | -48.03 | -1.24 | 74.35 | 0.64 | 918.97 | 4.58 | BC 149 |
| | | | | Min $M_y$ | -4.40 | 0.59 | 18.86 | 0.14 | 230.40 | -2.01 | BC 413 |
| | | | | Max $M_z$ | -48.03 | -1.24 | 74.35 | 0.64 | 918.97 | 4.58 | BC 149 |
| | | | | Min $M_z$ | -4.13 | 0.59 | 18.86 | 0.14 | 230.42 | -2.01 | BC 445 |
| 188 | RC1 | 150 | 0 | Max N | 3.65 | -0.12 | -0.15 | 0.01 | 11.68 | -0.39 | BC 390 |
| | | | | Min N | -3.05 | -0.02 | -0.24 | -0.02 | 26.29 | -0.05 | BC 240 |
| | | | | Max $V_y$ | 1.29 | 0.11 | -0.15 | -0.01 | 11.68 | 0.36 | BC 409 |
| | | | | Min $V_y$ | 3.58 | -0.13 | -0.24 | 0.01 | 26.28 | -0.42 | BC 234 |
| | | | | Max $V_z$ | 1.37 | 0.11 | -0.15 | -0.01 | 11.67 | 0.35 | BC 417 |
| | | | | Min $V_z$ | -0.28 | -0.05 | -0.31 | -0.00 | 51.91 | -0.14 | BC 148 |
| | | | | Max $M_T$ | 3.56 | -0.11 | -0.15 | 0.01 | 11.68 | -0.36 | BC 474 |
| | | | | Min $M_T$ | -2.96 | -0.02 | -0.24 | -0.02 | 26.28 | -0.06 | BC 200 |
| | | | | Max $M_y$ | -0.28 | -0.05 | -0.31 | -0.00 | 51.91 | -0.14 | BC 148 |
| | | | | Min $M_y$ | 1.37 | 0.11 | -0.15 | -0.01 | 11.67 | 0.35 | BC 417 |
| | | | | Max $M_z$ | 1.29 | 0.11 | -0.15 | -0.01 | 11.68 | 0.36 | BC 409 |
| | | | | Min $M_z$ | 3.58 | -0.13 | -0.24 | 0.01 | 26.28 | -0.42 | BC 234 |
| | | 35 | 3201 | Max N | 3.90 | -0.13 | -16.18 | 0.01 | 0.00 | 0.00 | BC 186 |
| | | | | Min N | -2.85 | -0.00 | -7.15 | -0.02 | 0.00 | 0.00 | BC 444 |
| | | | | Max $V_y$ | 1.42 | 0.11 | -7.15 | -0.01 | 0.00 | 0.00 | BC 409 |
| | | | | Min $V_y$ | 3.87 | -0.13 | -16.18 | 0.01 | 0.00 | 0.00 | BC 234 |
| | | | | Max $V_z$ | 1.50 | 0.11 | -7.15 | -0.01 | 0.00 | 0.00 | BC 417 |
| | | | | Min $V_z$ | 0.31 | -0.05 | -32.14 | -0.00 | 0.00 | 0.00 | BC 148 |
| | | | | Max $M_T$ | 3.69 | -0.11 | -7.15 | 0.01 | 0.00 | 0.00 | BC 474 |
| | | | | Min $M_T$ | -2.66 | -0.02 | -16.18 | -0.02 | 0.00 | 0.00 | BC 200 |
| | | | | Max $M_y$ | 0.24 | -0.03 | -18.54 | -0.00 | 0.00 | 0.00 | BC 304 |
| | | | | Min $M_y$ | 0.11 | -0.03 | -17.53 | -0.00 | -0.00 | 0.00 | BC 21 |
| | | | | Max $M_z$ | 0.07 | -0.02 | -11.83 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.07 | -0.02 | -11.83 | -0.00 | 0.00 | 0.00 | BC 1 |
| 189 | RC1 | 151 | 0 | Max N | 4.61 | -0.09 | -0.69 | -0.00 | 28.62 | -0.31 | BC 243 |
| | | | | Min N | -41.79 | 0.01 | -0.66 | -0.01 | 19.15 | 0.03 | BC 168 |
| | | | | Max $V_y$ | -20.18 | 0.11 | -0.45 | 0.00 | 13.04 | 0.35 | BC 357 |
| | | | | Min $V_y$ | 4.53 | -0.12 | -0.47 | -0.00 | 13.11 | -0.40 | BC 447 |
| | | | | Max $V_z$ | -16.18 | 0.11 | -0.45 | 0.00 | 13.04 | 0.35 | BC 413 |
| | | | | Min $V_z$ | -0.17 | 0.02 | -0.77 | 0.00 | 31.07 | 0.07 | BC 4 |
| | | | | Max $M_T$ | -20.18 | 0.11 | -0.45 | 0.00 | 13.04 | 0.35 | BC 357 |
| | | | | Min $M_T$ | -41.66 | 0.01 | -0.66 | -0.01 | 19.15 | 0.03 | BC 164 |
| | | | | Max $M_y$ | 0.43 | 0.02 | -0.71 | 0.00 | 55.02 | 0.06 | BC 131 |
| | | | | Min $M_y$ | -16.18 | 0.11 | -0.45 | 0.00 | 13.04 | 0.35 | BC 413 |
| | | | | Max $M_z$ | -20.18 | 0.11 | -0.45 | 0.00 | 13.04 | 0.35 | BC 357 |
| | | | | Min $M_z$ | 4.53 | -0.12 | -0.47 | -0.00 | 13.11 | -0.40 | BC 447 |
| | | 41 | 3256 | Max N | 4.40 | -0.12 | -7.59 | -0.00 | -0.00 | 0.00 | BC 447 |
| | | | | Min N | -41.99 | 0.01 | -11.10 | -0.01 | 0.00 | 0.00 | BC 168 |
| | | | | Max $V_y$ | -20.31 | 0.11 | -7.57 | 0.00 | 0.00 | 0.00 | BC 357 |
| | | | | Min $V_y$ | 4.40 | -0.12 | -7.59 | -0.00 | -0.00 | 0.00 | BC 447 |
| | | | | Max $V_z$ | -16.31 | 0.11 | -7.56 | 0.00 | -0.00 | 0.00 | BC 413 |
| | | | | Min $V_z$ | -0.19 | 0.02 | -33.09 | 0.00 | 0.00 | 0.00 | BC 131 |
| | | | | Max $M_T$ | -20.31 | 0.11 | -7.57 | 0.00 | 0.00 | 0.00 | BC 357 |
| | | | | Min $M_T$ | -41.85 | 0.01 | -11.10 | -0.01 | 0.00 | 0.00 | BC 164 |
| | | | | Max $M_y$ | -41.02 | 0.01 | -16.89 | -0.01 | 0.00 | 0.00 | BC 172 |
| | | | | Min $M_y$ | -6.32 | 0.07 | -11.12 | 0.00 | -0.00 | -0.00 | BC 278 |
| | | | | Max $M_z$ | -36.68 | 0.03 | -13.36 | -0.01 | 0.00 | 0.00 | BC 368 |
| | | | | Min $M_z$ | -41.76 | 0.02 | -7.57 | -0.01 | -0.00 | -0.00 | BC 356 |
| 190 | RC1 | 152 | 0 | Max N | 24.58 | -0.15 | 14.66 | 0.15 | 76.81 | 0.12 | BC 390 |
| | | | | Min N | -25.09 | -0.09 | 21.80 | 0.03 | 113.84 | 0.07 | BC 216 |
| | | | | Max $V_y$ | -23.61 | 0.29 | 33.87 | 0.02 | 172.37 | 0.03 | BC 241 |
| | | | | Min $V_y$ | -10.79 | -0.20 | 14.95 | -0.10 | 77.76 | -0.06 | BC 359 |
| | | | | Max $V_z$ | -9.26 | 0.04 | 66.06 | -0.01 | 330.81 | 0.03 | BC 155 |
| | | | | Min $V_z$ | 24.58 | -0.15 | 14.66 | 0.15 | 76.81 | 0.12 | BC 390 |
| | | | | Max $M_T$ | 22.66 | -0.16 | 14.68 | 0.16 | 76.93 | 0.14 | BC 446 |
| | | | | Min $M_T$ | -12.25 | -0.16 | 14.97 | -0.11 | 77.98 | -0.09 | BC 447 |
| | | | | Max $M_y$ | -9.26 | 0.04 | 66.06 | -0.01 | 330.81 | 0.03 | BC 155 |
| | | | | Min $M_y$ | 24.58 | -0.15 | 14.66 | 0.15 | 76.81 | 0.12 | BC 390 |
| | | | | Max $M_z$ | 19.27 | -0.15 | 21.66 | 0.15 | 113.32 | 0.15 | BC 254 |
| | | | | Min $M_z$ | -12.25 | -0.16 | 14.97 | -0.11 | 77.98 | -0.09 | BC 447 |
| | | 84 | 3256 | Max N | 24.31 | -0.15 | 0.12 | 0.15 | 100.85 | 0.62 | BC 390 |
| | | | | Min N | -25.49 | -0.09 | 0.47 | 0.03 | 150.09 | 0.36 | BC 216 |
| | | | | Max $V_y$ | -24.23 | 0.29 | 0.73 | 0.02 | 228.70 | -0.93 | BC 241 |
| | | | | Min $V_y$ | -11.07 | -0.20 | 0.40 | -0.10 | 102.75 | 0.59 | BC 359 |
| | | | | Max $V_z$ | -23.97 | 0.26 | 0.93 | 0.04 | 153.14 | -0.80 | BC 277 |
| | | | | Min $V_z$ | -5.46 | 0.03 | -0.37 | -0.01 | 389.85 | -0.10 | BC 326 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 190 | RC1 | | | Max $M_T$ | 22.39 | -0.16 | 0.14 | 0.16 | 101.06 | 0.67 | BC 446 |
| | | | | Min $M_T$ | -12.53 | -0.16 | 0.43 | -0.11 | 103.05 | 0.42 | BC 447 |
| | | | | Max $M_y$ | -10.51 | 0.04 | -0.16 | -0.01 | 438.09 | -0.10 | BC 155 |
| | | | | Min $M_y$ | 24.31 | -0.15 | 0.12 | 0.15 | 100.85 | 0.62 | BC 390 |
| | | | | Max $M_z$ | 22.20 | -0.16 | 0.14 | 0.16 | 101.08 | 0.67 | BC 474 |
| | | | | Min $M_z$ | -24.23 | 0.29 | 0.73 | 0.02 | 228.70 | -0.93 | BC 241 |
| 191 | RC1 | 153 | 0 | Max N | 35.96 | 0.25 | 14.82 | -0.19 | 77.76 | -0.15 | BC 391 |
| | | | | Min N | -32.77 | 0.01 | 34.34 | -0.01 | 174.90 | -0.05 | BC 240 |
| | | | | Max $V_y$ | 35.95 | 0.26 | 14.82 | -0.19 | 77.76 | -0.15 | BC 363 |
| | | | | Min $V_y$ | -32.10 | -0.01 | 27.26 | -0.01 | 138.01 | -0.05 | BC 432 |
| | | | | Max $V_z$ | -5.03 | 0.09 | 67.45 | -0.03 | 337.41 | -0.02 | BC 154 |
| | | | | Min $V_z$ | 35.95 | 0.26 | 14.82 | -0.19 | 77.76 | -0.15 | BC 363 |
| | | | | Max $M_T$ | -8.85 | 0.17 | 15.14 | 0.04 | 79.02 | -0.05 | BC 450 |
| | | | | Min $M_T$ | 35.96 | 0.25 | 14.82 | -0.19 | 77.76 | -0.15 | BC 391 |
| | | | | Max $M_y$ | -5.03 | 0.09 | 67.45 | -0.03 | 337.41 | -0.02 | BC 154 |
| | | | | Min $M_y$ | 35.96 | 0.25 | 14.82 | -0.19 | 77.75 | -0.15 | BC 419 |
| | | | | Max $M_z$ | -4.29 | 0.07 | 27.06 | -0.02 | 137.31 | 0.00 | BC 53 |
| | | | | Min $M_z$ | 32.42 | 0.25 | 14.89 | -0.19 | 77.85 | -0.16 | BC 411 |
| | | 83 | 3256 | Max N | 35.68 | 0.25 | 0.02 | -0.19 | 101.91 | -0.98 | BC 391 |
| | | | | Min N | -33.40 | 0.01 | 0.56 | -0.01 | 231.71 | -0.07 | BC 240 |
| | | | | Max $V_y$ | 35.67 | 0.26 | 0.02 | -0.19 | 101.92 | -0.98 | BC 363 |
| | | | | Min $V_y$ | -32.61 | -0.01 | 0.39 | -0.01 | 183.03 | -0.02 | BC 432 |
| | | | | Max $V_z$ | -32.37 | 0.01 | 0.74 | -0.01 | 154.29 | -0.07 | BC 252 |
| | | | | Min $V_z$ | -3.42 | 0.05 | -0.36 | -0.02 | 398.10 | -0.19 | BC 323 |
| | | | | Max $M_T$ | -9.13 | 0.17 | 0.35 | 0.04 | 104.22 | -0.58 | BC 450 |
| | | | | Min $M_T$ | 35.68 | 0.25 | 0.02 | -0.19 | 101.91 | -0.98 | BC 391 |
| | | | | Max $M_y$ | -6.31 | 0.09 | -0.15 | -0.03 | 446.96 | -0.32 | BC 154 |
| | | | | Min $M_y$ | 35.68 | 0.25 | 0.02 | -0.19 | 101.91 | -0.98 | BC 391 |
| | | | | Max $M_z$ | -32.61 | -0.01 | 0.39 | -0.01 | 183.03 | -0.02 | BC 432 |
| | | | | Min $M_z$ | 35.67 | 0.26 | 0.02 | -0.19 | 101.92 | -0.98 | BC 363 |
| 192 | RC1 | 154 | 0 | Max N | 53.00 | -0.22 | -3.37 | 0.03 | 575.15 | 1.67 | BC 206 |
| | | | | Min N | -19.28 | -0.09 | -2.01 | -0.13 | 571.25 | 0.99 | BC 235 |
| | | | | Max $V_y$ | -17.41 | 0.13 | -0.80 | -0.14 | 267.75 | 0.19 | BC 421 |
| | | | | Min $V_y$ | -9.83 | -1.23 | -2.69 | 0.25 | 568.48 | -0.40 | BC 204 |
| | | | | Max $V_z$ | -17.33 | 0.13 | -0.80 | -0.14 | 267.75 | 0.18 | BC 361 |
| | | | | Min $V_z$ | 53.00 | -0.22 | -3.37 | 0.03 | 575.15 | 1.67 | BC 206 |
| | | | | Max $M_T$ | -10.68 | -1.02 | -1.80 | 0.28 | 269.83 | -1.12 | BC 468 |
| | | | | Min $M_T$ | -16.24 | -0.17 | -1.74 | -0.19 | 566.40 | 0.85 | BC 185 |
| | | | | Max $M_y$ | 3.87 | -0.74 | -3.04 | -0.07 | 1052.68 | 2.57 | BC 155 |
| | | | | Min $M_y$ | -17.35 | 0.12 | -0.81 | -0.15 | 267.74 | 0.20 | BC 449 |
| | | | | Max $M_z$ | 3.66 | -0.74 | -3.04 | -0.07 | 1052.68 | 2.57 | BC 148 |
| | | | | Min $M_z$ | -10.56 | -1.02 | -1.80 | 0.28 | 269.81 | -1.13 | BC 408 |
| | | 82 | 3256 | Max N | 52.29 | -0.22 | -40.65 | 0.03 | 503.49 | 2.39 | BC 206 |
| | | | | Min N | -19.98 | -0.09 | -39.29 | -0.13 | 504.01 | 1.28 | BC 235 |
| | | | | Max $V_y$ | -17.73 | 0.13 | -17.98 | -0.14 | 237.17 | -0.24 | BC 421 |
| | | | | Min $V_y$ | -10.54 | -1.23 | -39.97 | 0.25 | 499.04 | 3.60 | BC 204 |
| | | | | Max $V_z$ | -17.65 | 0.13 | -17.98 | -0.14 | 237.18 | -0.24 | BC 361 |
| | | | | Min $V_z$ | 2.61 | -0.74 | -74.15 | -0.07 | 927.03 | 4.99 | BC 140 |
| | | | | Max $M_T$ | -11.00 | -1.02 | -18.98 | 0.28 | 236.01 | 2.20 | BC 468 |
| | | | | Min $M_T$ | -16.94 | -0.17 | -39.02 | -0.19 | 500.06 | 1.41 | BC 185 |
| | | | | Max $M_y$ | 0.85 | -0.71 | -74.12 | -0.08 | 927.07 | 4.87 | BC 149 |
| | | | | Min $M_y$ | -12.28 | -1.01 | -18.93 | 0.27 | 235.82 | 2.20 | BC 356 |
| | | | | Max $M_z$ | 2.73 | -0.75 | -74.15 | -0.07 | 927.03 | 5.00 | BC 139 |
| | | | | Min $M_z$ | -17.65 | 0.13 | -17.98 | -0.14 | 237.18 | -0.24 | BC 361 |
| 193 | RC1 | 155 | 0 | Max N | 48.66 | 0.49 | -2.88 | 0.08 | 560.97 | -0.82 | BC 235 |
| | | | | Min N | -20.31 | 0.32 | -1.93 | -0.13 | 268.70 | -0.83 | BC 408 |
| | | | | Max $V_y$ | -0.39 | 1.14 | -2.53 | 0.24 | 1028.26 | -0.84 | BC 149 |
| | | | | Min $V_y$ | -15.07 | -0.76 | -0.50 | -0.01 | 262.31 | -0.46 | BC 473 |
| | | | | Max $V_z$ | -15.12 | -0.76 | -0.50 | -0.01 | 262.29 | -0.46 | BC 413 |
| | | | | Min $V_z$ | 48.66 | 0.49 | -2.88 | 0.08 | 560.97 | -0.82 | BC 235 |
| | | | | Max $M_T$ | -0.39 | 1.14 | -2.53 | 0.24 | 1028.26 | -0.84 | BC 149 |
| | | | | Min $M_T$ | -20.10 | 0.32 | -1.92 | -0.13 | 268.61 | -0.84 | BC 412 |
| | | | | Max $M_y$ | -0.39 | 1.14 | -2.53 | 0.24 | 1028.26 | -0.84 | BC 149 |
| | | | | Min $M_y$ | -15.07 | -0.75 | -0.50 | -0.01 | 262.27 | -0.47 | BC 409 |
| | | | | Max $M_z$ | -16.94 | 0.71 | -1.66 | 0.19 | 558.44 | 0.74 | BC 242 |
| | | | | Min $M_z$ | -17.87 | 0.60 | -2.70 | -0.06 | 560.60 | -1.13 | BC 184 |
| | | 81 | 3256 | Max N | 47.96 | 0.49 | -39.53 | 0.08 | 491.95 | -2.40 | BC 235 |
| | | | | Min N | -20.70 | 0.48 | -30.86 | -0.09 | 383.83 | -2.57 | BC 396 |
| | | | | Max $V_y$ | -1.71 | 1.14 | -72.26 | 0.24 | 906.53 | -4.56 | BC 149 |
| | | | | Min $V_y$ | -15.39 | -0.76 | -17.43 | -0.01 | 233.12 | 2.00 | BC 473 |
| | | | | Max $V_z$ | -15.44 | -0.76 | -17.43 | -0.01 | 233.11 | 2.00 | BC 413 |
| | | | | Min $V_z$ | -1.71 | 1.14 | -72.26 | 0.24 | 906.53 | -4.56 | BC 149 |
| | | | | Max $M_T$ | -1.71 | 1.14 | -72.26 | 0.24 | 906.53 | -4.56 | BC 149 |
| | | | | Min $M_T$ | -20.42 | 0.32 | -18.86 | -0.13 | 234.78 | -1.89 | BC 412 |
| | | | | Max $M_y$ | -1.80 | 1.14 | -72.25 | 0.24 | 906.54 | -4.54 | BC 146 |
| | | | | Min $M_y$ | -1.71 | 0.30 | -18.10 | 0.06 | 231.80 | -1.15 | BC 41 |
| | | | | Max $M_z$ | -15.23 | -0.76 | -17.43 | -0.01 | 233.15 | 2.00 | BC 445 |
| | | | | Min $M_z$ | -1.71 | 1.14 | -72.26 | 0.24 | 906.53 | -4.56 | BC 149 |
| 194 | RC1 | 156 | 0 | Max N | 3.79 | 0.30 | -0.64 | 0.02 | 28.46 | 0.99 | BC 202 |
| | | | | Min N | -41.26 | -0.14 | -0.63 | -0.01 | 19.05 | -0.45 | BC 164 |
| | | | | Max $V_y$ | 3.11 | 0.31 | -0.44 | 0.02 | 13.00 | 1.02 | BC 446 |
| | | | | Min $V_y$ | -39.68 | -0.17 | -0.43 | -0.01 | 12.98 | -0.54 | BC 384 |
| | | | | Max $V_z$ | -40.08 | -0.10 | -0.42 | -0.01 | 22.37 | -0.32 | BC 397 |
| | | | | Min $V_z$ | 0.01 | 0.10 | -0.72 | 0.01 | 21.52 | 0.32 | BC 1 |
| | | | | Max $M_T$ | 3.11 | 0.31 | -0.44 | 0.02 | 13.00 | 1.02 | BC 446 |
| | | | | Min $M_T$ | -39.31 | -0.12 | -0.43 | -0.01 | 12.97 | -0.39 | BC 409 |
| | | | | Max $M_y$ | 0.07 | 0.20 | -0.63 | 0.01 | 54.76 | 0.67 | BC 146 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 194 | RC1 | | | Min $M_y$ | -39.31 | -0.12 | -0.43 | -0.01 | 12.97 | -0.39 | BC 409 |
| | | | | Max $M_z$ | 3.11 | 0.31 | -0.44 | 0.02 | 13.00 | 1.02 | BC 446 |
| | | | | Min $M_z$ | -39.68 | -0.17 | -0.43 | -0.01 | 12.98 | -0.54 | BC 384 |
| | | 35 | 3256 | Max N | 3.49 | 0.30 | -16.85 | 0.02 | 0.00 | 0.00 | BC 202 |
| | | | | Min N | -41.46 | -0.14 | -11.07 | -0.01 | -0.00 | 0.00 | BC 164 |
| | | | | Max $V_y$ | 2.98 | 0.31 | -7.55 | 0.02 | 0.00 | 0.00 | BC 446 |
| | | | | Min $V_y$ | -39.81 | -0.17 | -7.55 | -0.01 | -0.00 | 0.00 | BC 384 |
| | | | | Max $V_z$ | -39.45 | -0.12 | -7.54 | -0.01 | 0.00 | 0.00 | BC 409 |
| | | | | Min $V_z$ | -0.54 | 0.20 | -33.01 | 0.01 | 0.00 | 0.00 | BC 146 |
| | | | | Max $M_T$ | 2.98 | 0.31 | -7.55 | 0.02 | 0.00 | 0.00 | BC 446 |
| | | | | Min $M_T$ | -39.45 | -0.12 | -7.54 | -0.01 | 0.00 | 0.00 | BC 409 |
| | | | | Max $M_y$ | -0.70 | 0.20 | -33.01 | 0.01 | 0.00 | 0.00 | BC 155 |
| | | | | Min $M_y$ | -39.49 | -0.11 | -16.84 | -0.01 | -0.00 | 0.00 | BC 268 |
| | | | | Max $M_z$ | -39.84 | -0.07 | -16.84 | -0.01 | 0.00 | 0.00 | BC 205 |
| | | | | Min $M_z$ | -41.07 | -0.16 | -7.55 | -0.01 | 0.00 | -0.00 | BC 356 |
| 195 | RC1 | 157 | 0 | Max N | 3.46 | -0.01 | -0.11 | 0.01 | 12.02 | -0.04 | BC 359 |
| | | | | Min N | -16.70 | 0.00 | -0.11 | -0.01 | 12.02 | 0.02 | BC 356 |
| | | | | Max $V_y$ | -16.70 | 0.00 | -0.11 | -0.01 | 12.02 | 0.02 | BC 356 |
| | | | | Min $V_y$ | -4.28 | -0.03 | -0.16 | -0.01 | 27.09 | -0.09 | BC 269 |
| | | | | Max $V_z$ | -3.72 | -0.02 | -0.11 | -0.01 | 12.02 | -0.06 | BC 417 |
| | | | | Min $V_z$ | -0.75 | -0.01 | -0.19 | -0.00 | 29.37 | -0.03 | BC 20 |
| | | | | Max $M_T$ | 3.36 | -0.01 | -0.16 | 0.01 | 17.63 | -0.04 | BC 171 |
| | | | | Min $M_T$ | -4.28 | -0.03 | -0.16 | -0.01 | 27.09 | -0.09 | BC 269 |
| | | | | Max $M_y$ | -0.84 | -0.02 | -0.17 | -0.00 | 53.57 | -0.06 | BC 147 |
| | | | | Min $M_y$ | -3.72 | -0.02 | -0.11 | -0.01 | 12.02 | -0.06 | BC 417 |
| | | | | Max $M_z$ | -16.70 | 0.00 | -0.11 | -0.01 | 12.02 | 0.02 | BC 356 |
| | | | | Min $M_z$ | -4.28 | -0.03 | -0.16 | -0.01 | 27.09 | -0.09 | BC 269 |
| | | 42 | 3267 | Max N | 3.92 | -0.01 | -16.42 | 0.01 | 0.00 | 0.00 | BC 203 |
| | | | | Min N | -16.43 | 0.00 | -7.25 | -0.01 | -0.00 | 0.00 | BC 356 |
| | | | | Max $V_y$ | -16.43 | 0.00 | -7.25 | -0.01 | -0.00 | 0.00 | BC 356 |
| | | | | Min $V_y$ | -3.67 | -0.03 | -16.42 | -0.01 | 0.00 | 0.00 | BC 269 |
| | | | | Max $V_z$ | -3.45 | -0.02 | -7.25 | -0.01 | 0.00 | 0.00 | BC 417 |
| | | | | Min $V_z$ | 0.37 | -0.02 | -32.63 | -0.00 | 0.00 | 0.00 | BC 147 |
| | | | | Max $M_T$ | 3.75 | -0.01 | -10.63 | 0.01 | 0.00 | 0.00 | BC 171 |
| | | | | Min $M_T$ | -3.67 | -0.03 | -16.42 | -0.01 | 0.00 | 0.00 | BC 269 |
| | | | | Max $M_y$ | -2.12 | -0.00 | -16.42 | -0.01 | 0.00 | 0.00 | BC 268 |
| | | | | Min $M_y$ | -11.72 | -0.00 | -16.42 | -0.01 | -0.00 | 0.00 | BC 232 |
| | | | | Max $M_z$ | 0.09 | -0.01 | -12.00 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.09 | -0.01 | -12.00 | -0.00 | 0.00 | 0.00 | BC 1 |
| 196 | RC1 | 158 | 0 | Max N | 9.96 | -0.03 | -0.56 | -0.01 | 23.44 | -0.10 | BC 362 |
| | | | | Min N | -25.14 | -0.03 | -0.81 | -0.02 | 53.70 | -0.09 | BC 269 |
| | | | | Max $V_y$ | -3.42 | 0.00 | -0.82 | 0.01 | 34.36 | 0.01 | BC 171 |
| | | | | Min $V_y$ | 9.85 | -0.04 | -0.82 | -0.01 | 53.72 | -0.12 | BC 234 |
| | | | | Max $V_z$ | 9.63 | -0.02 | -0.55 | -0.01 | 42.75 | -0.06 | BC 456 |
| | | | | Min $V_z$ | -0.02 | -0.01 | -0.92 | -0.00 | 38.79 | -0.04 | BC 10 |
| | | | | Max $M_T$ | -3.42 | 0.00 | -0.82 | 0.01 | 34.36 | 0.01 | BC 171 |
| | | | | Min $M_T$ | -25.14 | -0.03 | -0.81 | -0.02 | 53.70 | -0.09 | BC 269 |
| | | | | Max $M_y$ | -4.70 | -0.02 | -0.82 | -0.00 | 107.88 | -0.06 | BC 134 |
| | | | | Min $M_y$ | 9.65 | -0.01 | -0.55 | -0.01 | 23.41 | -0.05 | BC 468 |
| | | | | Max $M_z$ | -3.42 | 0.00 | -0.82 | 0.01 | 34.36 | 0.01 | BC 171 |
| | | | | Min $M_z$ | 9.85 | -0.04 | -0.82 | -0.01 | 53.72 | -0.12 | BC 234 |
| | | 67 | 3267 | Max N | 11.02 | -0.04 | -32.06 | -0.01 | 0.00 | 0.00 | BC 174 |
| | | | | Min N | -23.98 | -0.03 | -32.06 | -0.02 | 0.00 | 0.00 | BC 269 |
| | | | | Max $V_y$ | -2.70 | 0.00 | -20.22 | 0.01 | 0.00 | 0.00 | BC 171 |
| | | | | Min $V_y$ | 11.02 | -0.04 | -32.06 | -0.01 | 0.00 | 0.00 | BC 234 |
| | | | | Max $V_z$ | 10.14 | -0.01 | -13.78 | -0.01 | 0.00 | 0.00 | BC 468 |
| | | | | Min $V_z$ | -2.30 | -0.02 | -65.22 | -0.00 | -0.00 | 0.00 | BC 134 |
| | | | | Max $M_T$ | -2.70 | 0.00 | -20.22 | 0.01 | 0.00 | 0.00 | BC 171 |
| | | | | Min $M_T$ | -23.98 | -0.03 | -32.06 | -0.02 | 0.00 | 0.00 | BC 269 |
| | | | | Max $M_y$ | -4.92 | -0.01 | -32.06 | -0.00 | 0.00 | 0.00 | BC 91 |
| | | | | Min $M_y$ | -5.54 | -0.02 | -53.37 | -0.00 | -0.00 | 0.00 | BC 136 |
| | | | | Max $M_z$ | 0.80 | -0.01 | -22.82 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -19.43 | -0.02 | -13.79 | -0.02 | 0.00 | -0.00 | BC 353 |
| 197 | RC1 | 159 | 0 | Max N | 4.54 | 0.05 | -0.44 | 0.02 | 14.70 | 0.16 | BC 363 |
| | | | | Min N | -29.37 | -0.05 | -0.44 | -0.02 | 25.03 | -0.17 | BC 436 |
| | | | | Max $V_y$ | 2.51 | 0.05 | -0.45 | 0.01 | 14.71 | 0.17 | BC 447 |
| | | | | Min $V_y$ | -24.52 | -0.06 | -0.65 | -0.02 | 31.90 | -0.20 | BC 204 |
| | | | | Max $V_z$ | -22.73 | 0.01 | -0.44 | -0.01 | 14.69 | 0.02 | BC 390 |
| | | | | Min $V_z$ | -5.50 | 0.00 | -0.74 | -0.00 | 34.68 | 0.00 | BC 27 |
| | | | | Max $M_T$ | 4.28 | 0.05 | -0.44 | 0.02 | 14.70 | 0.16 | BC 451 |
| | | | | Min $M_T$ | -24.52 | -0.06 | -0.65 | -0.02 | 31.90 | -0.20 | BC 204 |
| | | | | Max $M_y$ | -6.28 | -0.01 | -0.65 | -0.00 | 60.84 | -0.02 | BC 154 |
| | | | | Min $M_y$ | -22.73 | 0.01 | -0.44 | -0.01 | 14.69 | 0.02 | BC 390 |
| | | | | Max $M_z$ | 2.51 | 0.05 | -0.45 | 0.01 | 14.71 | 0.17 | BC 447 |
| | | | | Min $M_z$ | -24.52 | -0.06 | -0.65 | -0.02 | 31.90 | -0.20 | BC 204 |
| | | 68 | 3267 | Max N | 4.84 | 0.05 | -8.55 | 0.02 | -0.00 | 0.00 | BC 363 |
| | | | | Min N | -28.83 | -0.05 | -14.88 | -0.02 | -0.00 | 0.00 | BC 436 |
| | | | | Max $V_y$ | 2.81 | 0.05 | -8.56 | 0.01 | 0.00 | 0.00 | BC 447 |
| | | | | Min $V_y$ | -23.84 | -0.06 | -18.87 | -0.02 | -0.00 | 0.00 | BC 204 |
| | | | | Max $V_z$ | -22.42 | 0.01 | -8.55 | -0.01 | 0.00 | 0.00 | BC 390 |
| | | | | Min $V_z$ | -4.94 | -0.01 | -36.59 | -0.00 | -0.00 | 0.00 | BC 154 |
| | | | | Max $M_T$ | 4.58 | 0.05 | -8.55 | 0.02 | 0.00 | 0.00 | BC 451 |
| | | | | Min $M_T$ | -23.84 | -0.06 | -18.87 | -0.02 | -0.00 | 0.00 | BC 204 |
| | | | | Max $M_y$ | -2.09 | -0.00 | -21.20 | -0.00 | 0.00 | 0.00 | BC 304 |
| | | | | Min $M_y$ | -19.28 | -0.01 | -12.55 | -0.01 | -0.00 | 0.00 | BC 278 |
| | | | | Max $M_z$ | -9.26 | -0.01 | -8.55 | -0.02 | 0.00 | 0.00 | BC 477 |
| | | | | Min $M_z$ | -12.05 | -0.01 | -18.87 | -0.02 | 0.00 | -0.00 | BC 241 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 198 | RC1 | 160 | 0 | Max N | 0.57 | -0.53 | -0.30 | -0.19 | 57.41 | -1.73 | BC 131 |
| | | | | Min N | -0.97 | 0.05 | -0.15 | -0.04 | 13.33 | 0.17 | BC 448 |
| | | | | Max $V_y$ | -0.84 | 0.07 | -0.15 | -0.04 | 13.34 | 0.22 | BC 408 |
| | | | | Min $V_y$ | 0.56 | -0.53 | -0.30 | -0.19 | 57.41 | -1.73 | BC 149 |
| | | | | Max $V_z$ | -0.14 | -0.13 | -0.15 | -0.05 | 13.32 | -0.44 | BC 389 |
| | | | | Min $V_z$ | 0.49 | -0.52 | -0.30 | -0.19 | 57.41 | -1.70 | BC 154 |
| | | | | Max $M_T$ | -0.90 | 0.06 | -0.15 | -0.03 | 13.33 | 0.19 | BC 356 |
| | | | | Min $M_T$ | 0.49 | -0.52 | -0.30 | -0.19 | 57.41 | -1.70 | BC 154 |
| | | | | Max $M_y$ | 0.49 | -0.52 | -0.30 | -0.19 | 57.41 | -1.70 | BC 154 |
| | | | | Min $M_y$ | -0.14 | -0.13 | -0.15 | -0.05 | 13.32 | -0.44 | BC 389 |
| | | | | Max $M_z$ | -0.84 | 0.07 | -0.15 | -0.04 | 13.34 | 0.22 | BC 408 |
| | | | | Min $M_z$ | 0.56 | -0.53 | -0.30 | -0.19 | 57.41 | -1.73 | BC 149 |
| | | 102 | 3267 | Max N | 1.85 | -0.53 | -34.84 | -0.19 | -0.00 | 0.00 | BC 131 |
| | | | | Min N | -0.67 | 0.05 | -8.01 | -0.04 | -0.00 | 0.00 | BC 448 |
| | | | | Max $V_y$ | -0.55 | 0.07 | -8.01 | -0.04 | 0.00 | 0.00 | BC 408 |
| | | | | Min $V_y$ | 1.84 | -0.53 | -34.84 | -0.19 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_z$ | 0.15 | -0.13 | -8.01 | -0.05 | -0.00 | -0.00 | BC 389 |
| | | | | Min $V_z$ | 1.78 | -0.52 | -34.84 | -0.19 | -0.00 | 0.00 | BC 154 |
| | | | | Max $M_T$ | -0.61 | 0.06 | -8.01 | -0.03 | 0.00 | 0.00 | BC 356 |
| | | | | Min $M_T$ | 1.78 | -0.52 | -34.84 | -0.19 | -0.00 | 0.00 | BC 154 |
| | | | | Max $M_y$ | 1.06 | -0.31 | -20.16 | -0.11 | 0.00 | -0.00 | BC 304 |
| | | | | Min $M_y$ | -0.33 | -0.01 | -11.75 | -0.06 | -0.00 | 0.00 | BC 160 |
| | | | | Max $M_z$ | 1.65 | -0.46 | -31.10 | -0.16 | -0.00 | 0.00 | BC 345 |
| | | | | Min $M_z$ | 1.52 | -0.44 | -28.76 | -0.16 | -0.00 | -0.00 | BC 129 |
| 199 | RC1 | 161 | 0 | Max N | 15.04 | -0.78 | 38.54 | 0.43 | 156.99 | 0.59 | BC 414 |
| | | | | Min N | -54.78 | -1.45 | 145.10 | 0.46 | 592.61 | 0.67 | BC 146 |
| | | | | Max $V_y$ | -15.60 | 1.35 | 36.69 | -0.16 | 150.97 | -0.95 | BC 408 |
| | | | | Min $V_y$ | -54.73 | -1.46 | 145.09 | 0.46 | 592.60 | 0.68 | BC 149 |
| | | | | Max $V_z$ | -53.99 | -1.42 | 145.17 | 0.47 | 592.83 | 0.68 | BC 139 |
| | | | | Min $V_z$ | -15.12 | -0.45 | 36.36 | -0.04 | 149.93 | 0.31 | BC 423 |
| | | | | Max $M_T$ | -54.04 | -1.42 | 145.16 | 0.47 | 592.80 | 0.68 | BC 132 |
| | | | | Min $M_T$ | -16.83 | 1.33 | 36.61 | -0.16 | 150.74 | -0.93 | BC 352 |
| | | | | Max $M_y$ | -53.99 | -1.42 | 145.17 | 0.47 | 592.83 | 0.68 | BC 139 |
| | | | | Min $M_y$ | -15.12 | -0.45 | 36.36 | -0.04 | 149.93 | 0.31 | BC 423 |
| | | | | Max $M_z$ | 13.01 | -0.82 | 79.92 | 0.45 | 325.92 | 0.72 | BC 242 |
| | | | | Min $M_z$ | -15.60 | 1.35 | 36.69 | -0.16 | 150.97 | -0.95 | BC 408 |
| | | 86 | 3267 | Max N | 15.67 | -0.78 | 21.56 | 0.43 | 255.16 | 3.15 | BC 414 |
| | | | | Min N | -52.18 | -1.45 | 75.19 | 0.46 | 952.48 | 5.42 | BC 146 |
| | | | | Max $V_y$ | -14.96 | 1.35 | 19.71 | -0.16 | 243.10 | -5.35 | BC 408 |
| | | | | Min $V_y$ | -52.13 | -1.46 | 75.19 | 0.46 | 952.45 | 5.44 | BC 149 |
| | | | | Max $V_z$ | -51.39 | -1.42 | 75.26 | 0.47 | 952.92 | 5.32 | BC 139 |
| | | | | Min $V_z$ | -14.48 | -0.45 | 19.38 | -0.04 | 241.00 | 1.77 | BC 423 |
| | | | | Max $M_T$ | -51.43 | -1.42 | 75.25 | 0.47 | 952.87 | 5.33 | BC 132 |
| | | | | Min $M_T$ | -16.20 | 1.33 | 19.63 | -0.16 | 242.61 | -5.29 | BC 352 |
| | | | | Max $M_y$ | -51.39 | -1.42 | 75.26 | 0.47 | 952.92 | 5.32 | BC 139 |
| | | | | Min $M_y$ | -14.48 | -0.45 | 19.38 | -0.04 | 241.00 | 1.77 | BC 423 |
| | | | | Max $M_z$ | -52.13 | -1.46 | 75.19 | 0.46 | 952.45 | 5.44 | BC 149 |
| | | | | Min $M_z$ | -14.96 | 1.35 | 19.71 | -0.16 | 243.10 | -5.35 | BC 408 |
| 200 | RC1 | 162 | 0 | Max N | 8.78 | 0.85 | 37.41 | -0.36 | 153.35 | -0.47 | BC 451 |
| | | | | Min N | -56.80 | 1.75 | 141.47 | -0.35 | 580.81 | -1.06 | BC 139 |
| | | | | Max $V_y$ | -56.04 | 1.77 | 141.53 | -0.35 | 581.02 | -1.07 | BC 138 |
| | | | | Min $V_y$ | -9.27 | -0.48 | 36.06 | -0.16 | 148.91 | -0.08 | BC 408 |
| | | | | Max $V_z$ | -55.53 | 1.76 | 141.54 | -0.35 | 581.07 | -1.05 | BC 149 |
| | | | | Min $V_z$ | -12.65 | 0.46 | 35.42 | 0.21 | 146.86 | 0.24 | BC 410 |
| | | | | Max $M_T$ | -12.65 | 0.46 | 35.42 | 0.21 | 146.86 | 0.24 | BC 410 |
| | | | | Min $M_T$ | 6.90 | 1.17 | 77.82 | -0.39 | 319.10 | -0.70 | BC 247 |
| | | | | Max $M_y$ | -55.53 | 1.76 | 141.54 | -0.35 | 581.07 | -1.05 | BC 149 |
| | | | | Min $M_y$ | -12.65 | 0.46 | 35.42 | 0.21 | 146.86 | 0.24 | BC 410 |
| | | | | Max $M_z$ | -21.05 | 0.45 | 75.34 | 0.20 | 311.02 | 0.37 | BC 242 |
| | | | | Min $M_z$ | -56.04 | 1.77 | 141.53 | -0.35 | 581.02 | -1.07 | BC 138 |
| | | 85 | 3267 | Max N | 9.42 | 0.85 | 20.43 | -0.36 | 247.86 | -3.27 | BC 451 |
| | | | | Min N | -54.20 | 1.75 | 71.56 | -0.35 | 928.81 | -6.77 | BC 139 |
| | | | | Max $V_y$ | -53.44 | 1.77 | 71.62 | -0.35 | 929.22 | -6.85 | BC 138 |
| | | | | Min $V_y$ | -8.64 | -0.48 | 19.08 | -0.16 | 238.98 | 1.47 | BC 408 |
| | | | | Max $V_z$ | -52.93 | 1.76 | 71.63 | -0.35 | 929.32 | -6.82 | BC 149 |
| | | | | Min $V_z$ | -12.02 | 0.46 | 18.44 | 0.21 | 234.85 | -1.25 | BC 410 |
| | | | | Max $M_T$ | -12.02 | 0.46 | 18.44 | 0.21 | 234.85 | -1.25 | BC 410 |
| | | | | Min $M_T$ | 8.27 | 1.17 | 41.07 | -0.39 | 513.33 | -4.53 | BC 247 |
| | | | | Max $M_y$ | -52.93 | 1.76 | 71.63 | -0.35 | 929.32 | -6.82 | BC 149 |
| | | | | Min $M_y$ | -12.02 | 0.46 | 18.44 | 0.21 | 234.85 | -1.25 | BC 410 |
| | | | | Max $M_z$ | -8.64 | -0.48 | 19.08 | -0.16 | 238.98 | 1.47 | BC 408 |
| | | | | Min $M_z$ | -53.44 | 1.77 | 71.62 | -0.35 | 929.22 | -6.85 | BC 138 |
| 201 | RC1 | 163 | 0 | Max N | 3.66 | 0.13 | -0.15 | -0.01 | 12.14 | 0.44 | BC 358 |
| | | | | Min N | -3.00 | 0.03 | -0.24 | 0.02 | 27.34 | 0.09 | BC 265 |
| | | | | Max $V_y$ | 3.52 | 0.15 | -0.24 | -0.00 | 27.34 | 0.49 | BC 242 |
| | | | | Min $V_y$ | 1.25 | -0.12 | -0.15 | 0.01 | 12.15 | -0.39 | BC 472 |
| | | | | Max $V_z$ | 3.66 | 0.13 | -0.15 | -0.01 | 12.14 | 0.44 | BC 358 |
| | | | | Min $V_z$ | -0.26 | 0.04 | -0.30 | 0.00 | 54.02 | 0.13 | BC 154 |
| | | | | Max $M_T$ | -2.94 | 0.03 | -0.24 | 0.02 | 27.34 | 0.10 | BC 245 |
| | | | | Min $M_T$ | 3.66 | 0.13 | -0.15 | -0.01 | 12.14 | 0.44 | BC 362 |
| | | | | Max $M_y$ | -0.26 | 0.04 | -0.30 | 0.00 | 54.02 | 0.13 | BC 154 |
| | | | | Min $M_y$ | 3.66 | 0.13 | -0.15 | -0.01 | 12.14 | 0.44 | BC 358 |
| | | | | Max $M_z$ | 3.52 | 0.15 | -0.24 | -0.00 | 27.34 | 0.49 | BC 242 |
| | | | | Min $M_z$ | 1.25 | -0.12 | -0.15 | 0.01 | 12.15 | -0.39 | BC 472 |
| | | 39 | 3267 | Max N | 4.23 | 0.14 | -16.50 | -0.00 | 0.00 | 0.00 | BC 202 |
| | | | | Min N | -2.68 | 0.02 | -7.29 | 0.02 | 0.00 | 0.00 | BC 469 |
| | | | | Max $V_y$ | 4.13 | 0.15 | -16.50 | -0.00 | -0.00 | 0.00 | BC 242 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 201 | RC1 | | | Min $V_y$ | 1.52 | -0.12 | -7.29 | 0.01 | 0.00 | 0.00 | BC 472 |
| | | | | Max $V_z$ | 3.93 | 0.13 | -7.29 | -0.01 | 0.00 | 0.00 | BC 358 |
| | | | | Min $V_z$ | 0.94 | 0.04 | -32.76 | 0.00 | 0.00 | 0.00 | BC 147 |
| | | | | Max $M_T$ | -2.34 | 0.03 | -16.50 | 0.02 | 0.00 | 0.00 | BC 245 |
| | | | | Min $M_T$ | 3.93 | 0.13 | -7.29 | -0.01 | 0.00 | 0.00 | BC 362 |
| | | | | Max $M_y$ | 0.45 | 0.02 | -17.87 | 0.00 | 0.00 | 0.00 | BC 21 |
| | | | | Min $M_y$ | 0.58 | 0.02 | -18.90 | 0.00 | -0.00 | 0.00 | BC 304 |
| | | | | Max $M_z$ | 0.37 | 0.02 | -12.06 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.37 | 0.02 | -12.06 | 0.00 | 0.00 | 0.00 | BC 1 |
| 202 | RC1 | 150 | 0 | Max N | 0.23 | 0.00 | 0.23 | 0.23 | 0.00 | 0.00 | BC 409 |
| | | | | Min N | -0.26 | 0.00 | 0.33 | 0.48 | 0.00 | 0.00 | BC 234 |
| | | | | Max $V_y$ | -0.04 | 0.00 | 0.37 | 0.38 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.04 | 0.00 | 0.37 | 0.38 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.04 | 0.00 | 0.37 | 0.38 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.24 | 0.00 | 0.23 | 0.23 | 0.00 | 0.00 | BC 354 |
| | | | | Max $M_T$ | -0.09 | 0.00 | 0.33 | 0.90 | 0.00 | 0.00 | BC 148 |
| | | | | Min $M_T$ | 0.22 | 0.00 | 0.23 | 0.22 | 0.00 | 0.00 | BC 417 |
| | | | | Max $M_y$ | -0.04 | 0.00 | 0.37 | 0.38 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.04 | 0.00 | 0.37 | 0.38 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.04 | 0.00 | 0.37 | 0.38 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.04 | 0.00 | 0.37 | 0.38 | 0.00 | 0.00 | BC 1 |
| | | 149 | 4300 | Max N | 0.23 | 0.00 | -0.23 | 0.23 | 0.00 | 0.00 | BC 409 |
| | | | | Min N | -0.26 | 0.00 | -0.33 | 0.48 | 0.00 | 0.00 | BC 234 |
| | | | | Max $V_y$ | -0.04 | 0.00 | -0.37 | 0.38 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.04 | 0.00 | -0.37 | 0.38 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.24 | 0.00 | -0.23 | 0.23 | 0.00 | 0.00 | BC 354 |
| | | | | Min $V_z$ | -0.04 | 0.00 | -0.37 | 0.38 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.09 | 0.00 | -0.33 | 0.90 | 0.00 | 0.00 | BC 148 |
| | | | | Min $M_T$ | 0.22 | 0.00 | -0.23 | 0.22 | 0.00 | 0.00 | BC 417 |
| | | | | Max $M_y$ | -0.04 | 0.00 | -0.37 | 0.38 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.04 | 0.00 | -0.37 | 0.38 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.04 | 0.00 | -0.37 | 0.38 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.04 | 0.00 | -0.37 | 0.38 | 0.00 | 0.00 | BC 1 |
| 203 | RC1 | 149 | 0 | Max N | 0.78 | -0.04 | 0.83 | 0.01 | 0.00 | 0.00 | BC 413 |
| | | | | Min N | -1.14 | -0.28 | 1.30 | 0.03 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_y$ | -0.83 | -0.03 | 0.88 | 0.01 | 0.00 | 0.00 | BC 362 |
| | | | | Min $V_y$ | -1.12 | -0.28 | 1.30 | 0.03 | -0.00 | 0.00 | BC 148 |
| | | | | Max $V_z$ | -0.67 | -0.15 | 1.46 | 0.02 | 0.00 | 0.00 | BC 22 |
| | | | | Min $V_z$ | 0.78 | -0.04 | 0.83 | 0.01 | 0.00 | 0.00 | BC 413 |
| | | | | Max $M_T$ | -1.12 | -0.28 | 1.30 | 0.03 | -0.00 | 0.00 | BC 148 |
| | | | | Min $M_T$ | -0.44 | -0.04 | 0.88 | 0.00 | 0.00 | 0.00 | BC 359 |
| | | | | Max $M_y$ | -0.82 | -0.08 | 0.88 | 0.02 | 0.00 | 0.00 | BC 378 |
| | | | | Min $M_y$ | -0.60 | -0.14 | 1.29 | 0.02 | -0.00 | 0.00 | BC 91 |
| | | | | Max $M_z$ | -0.76 | -0.11 | 1.29 | 0.02 | 0.00 | 0.00 | BC 182 |
| | | | | Min $M_z$ | -0.46 | -0.10 | 1.46 | 0.01 | 0.00 | 0.00 | BC 1 |
| | | 23 | 2250 | Max N | 0.78 | -0.04 | 0.60 | 0.01 | 1.61 | 0.09 | BC 413 |
| | | | | Min N | -1.14 | -0.28 | 0.96 | 0.03 | 2.54 | 0.63 | BC 149 |
| | | | | Max $V_y$ | -0.83 | -0.03 | 0.64 | 0.01 | 1.71 | 0.08 | BC 362 |
| | | | | Min $V_y$ | -1.12 | -0.28 | 0.95 | 0.03 | 2.53 | 0.64 | BC 148 |
| | | | | Max $V_z$ | -0.67 | -0.15 | 1.07 | 0.02 | 2.84 | 0.34 | BC 22 |
| | | | | Min $V_z$ | 0.78 | -0.04 | 0.60 | 0.01 | 1.61 | 0.09 | BC 413 |
| | | | | Max $M_T$ | -1.12 | -0.28 | 0.95 | 0.03 | 2.53 | 0.64 | BC 148 |
| | | | | Min $M_T$ | -0.44 | -0.04 | 0.64 | 0.00 | 1.72 | 0.10 | BC 359 |
| | | | | Max $M_y$ | -0.67 | -0.15 | 1.07 | 0.02 | 2.84 | 0.34 | BC 22 |
| | | | | Min $M_y$ | 0.78 | -0.04 | 0.60 | 0.01 | 1.61 | 0.09 | BC 413 |
| | | | | Max $M_z$ | -1.12 | -0.28 | 0.95 | 0.03 | 2.53 | 0.64 | BC 148 |
| | | | | Min $M_z$ | -0.83 | -0.03 | 0.64 | 0.01 | 1.71 | 0.08 | BC 362 |
| 204 | RC1 | 148 | 0 | Max N | 6.30 | 0.00 | 0.24 | -0.12 | 0.00 | 0.00 | BC 413 |
| | | | | Min N | -2.13 | 0.00 | 0.35 | -0.25 | 0.00 | 0.00 | BC 244 |
| | | | | Max $V_y$ | -0.24 | 0.00 | 0.39 | -0.20 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.24 | 0.00 | 0.39 | -0.20 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.03 | 0.00 | 0.39 | -0.21 | -0.00 | 0.00 | BC 16 |
| | | | | Min $V_z$ | -1.87 | 0.00 | 0.24 | -0.19 | 0.00 | 0.00 | BC 364 |
| | | | | Max $M_T$ | 5.21 | 0.00 | 0.24 | -0.12 | 0.00 | 0.00 | BC 389 |
| | | | | Min $M_T$ | -0.44 | 0.00 | 0.35 | -0.42 | 0.00 | 0.00 | BC 154 |
| | | | | Max $M_y$ | -2.13 | 0.00 | 0.35 | -0.25 | 0.00 | 0.00 | BC 244 |
| | | | | Min $M_y$ | -1.01 | 0.00 | 0.35 | -0.25 | -0.00 | 0.00 | BC 264 |
| | | | | Max $M_z$ | -0.24 | 0.00 | 0.39 | -0.20 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.24 | 0.00 | 0.39 | -0.20 | 0.00 | 0.00 | BC 1 |
| | | 147 | 4500 | Max N | 6.30 | 0.00 | -0.24 | -0.12 | 0.00 | 0.00 | BC 413 |
| | | | | Min N | -2.13 | 0.00 | -0.35 | -0.25 | 0.00 | 0.00 | BC 244 |
| | | | | Max $V_y$ | -0.24 | 0.00 | -0.39 | -0.20 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.24 | 0.00 | -0.39 | -0.20 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -1.87 | 0.00 | -0.24 | -0.19 | 0.00 | 0.00 | BC 364 |
| | | | | Min $V_z$ | -0.03 | 0.00 | -0.39 | -0.21 | -0.00 | 0.00 | BC 16 |
| | | | | Max $M_T$ | 5.21 | 0.00 | -0.24 | -0.12 | 0.00 | 0.00 | BC 389 |
| | | | | Min $M_T$ | -0.44 | 0.00 | -0.35 | -0.42 | 0.00 | 0.00 | BC 154 |
| | | | | Max $M_y$ | -2.07 | 0.00 | -0.35 | -0.25 | 0.00 | 0.00 | BC 232 |
| | | | | Min $M_y$ | -1.01 | 0.00 | -0.35 | -0.25 | -0.00 | 0.00 | BC 264 |
| | | | | Max $M_z$ | -0.24 | 0.00 | -0.39 | -0.20 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.24 | 0.00 | -0.39 | -0.20 | 0.00 | 0.00 | BC 1 |
| 205 | RC1 | 147 | 0 | Max N | 6.16 | 0.01 | 0.92 | 0.00 | 0.00 | 0.00 | BC 413 |
| | | | | Min N | -2.12 | -0.08 | 1.27 | 0.00 | 0.00 | 0.00 | BC 244 |
| | | | | Max $V_y$ | 6.04 | 0.01 | 0.92 | 0.00 | 0.00 | 0.00 | BC 445 |
| | | | | Min $V_y$ | -1.13 | -0.16 | 1.28 | -0.00 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_z$ | -0.09 | -0.04 | 1.45 | 0.01 | 0.00 | 0.00 | BC 15 |
| | | | | Min $V_z$ | -2.03 | -0.07 | 0.86 | 0.00 | 0.00 | 0.00 | BC 436 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 205 | RC1 | | | Max $M_T$ | -0.52 | -0.04 | 0.88 | 0.01 | 0.00 | 0.00 | BC 468 |
| | | | | Min $M_T$ | 4.39 | 0.00 | 1.32 | -0.01 | -0.00 | 0.00 | BC 197 |
| | | | | Max $M_y$ | -2.12 | -0.08 | 1.27 | 0.00 | 0.00 | 0.00 | BC 244 |
| | | | | Min $M_y$ | -0.99 | -0.08 | 1.28 | 0.01 | -0.00 | -0.00 | BC 264 |
| | | | | Max $M_z$ | -2.06 | -0.08 | 1.27 | 0.00 | 0.00 | 0.00 | BC 232 |
| | | | | Min $M_z$ | -0.99 | -0.08 | 1.28 | 0.01 | -0.00 | -0.00 | BC 264 |
| | | 26 | 2250 | Max N | 6.16 | 0.01 | 0.69 | 0.00 | 1.81 | -0.03 | BC 413 |
| | | | | Min N | -2.12 | -0.08 | 0.93 | 0.00 | 2.47 | 0.18 | BC 244 |
| | | | | Max $V_y$ | 6.04 | 0.01 | 0.68 | 0.00 | 1.81 | -0.03 | BC 445 |
| | | | | Min $V_y$ | -1.13 | -0.16 | 0.94 | -0.00 | 2.50 | 0.36 | BC 149 |
| | | | | Max $V_z$ | -0.09 | -0.04 | 1.06 | 0.01 | 2.83 | 0.08 | BC 15 |
| | | | | Min $V_z$ | -2.03 | -0.07 | 0.63 | 0.00 | 1.68 | 0.16 | BC 436 |
| | | | | Max $M_T$ | -0.52 | -0.04 | 0.64 | 0.01 | 1.70 | 0.08 | BC 468 |
| | | | | Min $M_T$ | 4.39 | 0.00 | 0.97 | -0.01 | 2.57 | -0.00 | BC 197 |
| | | | | Max $M_y$ | -0.09 | -0.04 | 1.06 | 0.01 | 2.83 | 0.08 | BC 15 |
| | | | | Min $M_y$ | -2.03 | -0.07 | 0.63 | 0.00 | 1.68 | 0.16 | BC 436 |
| | | | | Max $M_z$ | -1.13 | -0.16 | 0.94 | -0.00 | 2.50 | 0.36 | BC 149 |
| | | | | Min $M_z$ | 6.04 | 0.01 | 0.68 | 0.00 | 1.81 | -0.03 | BC 445 |
| 206 | RC1 | 146 | 0 | Max N | 0.38 | 0.00 | 0.33 | -0.16 | 0.00 | 0.00 | BC 253 |
| | | | | Min N | -0.33 | 0.00 | 0.33 | -0.23 | 0.00 | 0.00 | BC 175 |
| | | | | Max $V_y$ | -0.07 | 0.00 | 0.37 | -0.17 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.07 | 0.00 | 0.37 | -0.17 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.04 | 0.00 | 0.37 | -0.26 | 0.00 | 0.00 | BC 5 |
| | | | | Min $V_z$ | -0.30 | 0.00 | 0.23 | -0.10 | 0.00 | 0.00 | BC 355 |
| | | | | Max $M_T$ | 0.36 | 0.00 | 0.23 | -0.10 | 0.00 | 0.00 | BC 417 |
| | | | | Min $M_T$ | -0.07 | 0.00 | 0.33 | -0.47 | 0.00 | 0.00 | BC 147 |
| | | | | Max $M_y$ | -0.07 | 0.00 | 0.37 | -0.17 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.07 | 0.00 | 0.37 | -0.17 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.07 | 0.00 | 0.37 | -0.17 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.07 | 0.00 | 0.37 | -0.17 | 0.00 | 0.00 | BC 1 |
| | | 145 | 4300 | Max N | 0.38 | 0.00 | -0.33 | -0.16 | 0.00 | 0.00 | BC 253 |
| | | | | Min N | -0.33 | 0.00 | -0.33 | -0.23 | 0.00 | 0.00 | BC 175 |
| | | | | Max $V_y$ | -0.07 | 0.00 | -0.37 | -0.17 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.07 | 0.00 | -0.37 | -0.17 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.30 | 0.00 | -0.23 | -0.10 | 0.00 | 0.00 | BC 355 |
| | | | | Min $V_z$ | -0.04 | 0.00 | -0.37 | -0.26 | 0.00 | 0.00 | BC 5 |
| | | | | Max $M_T$ | 0.36 | 0.00 | -0.23 | -0.10 | 0.00 | 0.00 | BC 417 |
| | | | | Min $M_T$ | -0.07 | 0.00 | -0.33 | -0.47 | 0.00 | 0.00 | BC 147 |
| | | | | Max $M_y$ | -0.07 | 0.00 | -0.37 | -0.17 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.07 | 0.00 | -0.37 | -0.17 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.07 | 0.00 | -0.37 | -0.17 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.07 | 0.00 | -0.37 | -0.17 | 0.00 | 0.00 | BC 1 |
| 207 | RC1 | 156 | 0 | Max N | 0.33 | -0.02 | 0.85 | -0.01 | -0.00 | 0.00 | BC 384 |
| | | | | Min N | -0.62 | 0.01 | 0.87 | 0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Max $V_y$ | 0.15 | 0.05 | 1.26 | 0.02 | -0.00 | 0.00 | BC 201 |
| | | | | Min $V_y$ | 0.28 | -0.02 | 0.85 | -0.01 | 0.00 | 0.00 | BC 400 |
| | | | | Max $V_z$ | -0.20 | 0.02 | 1.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.14 | 0.01 | 0.85 | 0.01 | 0.00 | 0.00 | BC 415 |
| | | | | Max $M_T$ | 0.13 | 0.05 | 1.26 | 0.02 | -0.00 | 0.00 | BC 241 |
| | | | | Min $M_T$ | 0.31 | -0.02 | 0.85 | -0.01 | 0.00 | 0.00 | BC 356 |
| | | | | Max $M_y$ | -0.61 | 0.02 | 1.27 | 0.01 | 0.00 | 0.00 | BC 182 |
| | | | | Min $M_y$ | 0.28 | -0.01 | 1.26 | -0.01 | -0.00 | 0.00 | BC 160 |
| | | | | Max $M_z$ | -0.20 | 0.02 | 1.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.20 | 0.02 | 1.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 27 | 2150 | Max N | 0.33 | -0.02 | 0.63 | -0.01 | 1.59 | 0.05 | BC 384 |
| | | | | Min N | -0.62 | 0.01 | 0.64 | 0.00 | 1.63 | -0.03 | BC 446 |
| | | | | Max $V_y$ | 0.15 | 0.05 | 0.93 | 0.02 | 2.35 | -0.11 | BC 201 |
| | | | | Min $V_y$ | 0.28 | -0.02 | 0.63 | -0.01 | 1.59 | 0.05 | BC 400 |
| | | | | Max $V_z$ | -0.20 | 0.02 | 1.06 | 0.00 | 2.68 | -0.05 | BC 1 |
| | | | | Min $V_z$ | 0.14 | 0.01 | 0.63 | 0.01 | 1.59 | -0.01 | BC 415 |
| | | | | Max $M_T$ | 0.13 | 0.05 | 0.93 | 0.02 | 2.35 | -0.10 | BC 241 |
| | | | | Min $M_T$ | 0.31 | -0.02 | 0.63 | -0.01 | 1.59 | 0.04 | BC 356 |
| | | | | Max $M_y$ | -0.20 | 0.02 | 1.06 | 0.00 | 2.68 | -0.05 | BC 1 |
| | | | | Min $M_y$ | 0.14 | 0.01 | 0.63 | 0.01 | 1.59 | -0.01 | BC 415 |
| | | | | Max $M_z$ | 0.28 | -0.02 | 0.63 | -0.01 | 1.59 | 0.05 | BC 400 |
| | | | | Min $M_z$ | 0.15 | 0.05 | 0.93 | 0.02 | 2.35 | -0.11 | BC 201 |
| 208 | RC1 | 155 | 0 | Max N | 2.13 | 0.03 | 0.88 | -0.00 | -0.00 | 0.00 | BC 408 |
| | | | | Min N | -3.36 | 0.02 | 1.30 | -0.00 | -0.00 | 0.00 | BC 148 |
| | | | | Max $V_y$ | 1.19 | 0.04 | 1.30 | -0.00 | 0.00 | 0.00 | BC 204 |
| | | | | Min $V_y$ | 1.53 | 0.00 | 0.88 | 0.00 | -0.00 | 0.00 | BC 449 |
| | | | | Max $V_z$ | -2.09 | 0.03 | 1.47 | -0.00 | -0.00 | 0.00 | BC 11 |
| | | | | Min $V_z$ | 2.13 | 0.03 | 0.88 | -0.00 | -0.00 | 0.00 | BC 408 |
| | | | | Max $M_T$ | -2.41 | 0.02 | 1.30 | 0.00 | -0.00 | 0.00 | BC 166 |
| | | | | Min $M_T$ | -1.31 | 0.02 | 1.30 | -0.00 | -0.00 | 0.00 | BC 243 |
| | | | | Max $M_y$ | -2.32 | 0.01 | 0.89 | 0.00 | 0.00 | -0.00 | BC 378 |
| | | | | Min $M_y$ | 1.69 | 0.04 | 1.30 | -0.00 | -0.00 | 0.00 | BC 160 |
| | | | | Max $M_z$ | 2.12 | 0.03 | 0.88 | -0.00 | -0.00 | 0.00 | BC 384 |
| | | | | Min $M_z$ | -2.32 | 0.01 | 0.89 | 0.00 | 0.00 | -0.00 | BC 378 |
| | | 28 | 2250 | Max N | 2.13 | 0.03 | 0.65 | -0.00 | 1.72 | -0.07 | BC 408 |
| | | | | Min N | -3.36 | 0.02 | 0.95 | -0.00 | 2.54 | -0.05 | BC 148 |
| | | | | Max $V_y$ | 1.19 | 0.04 | 0.95 | -0.00 | 2.53 | -0.08 | BC 204 |
| | | | | Min $V_y$ | 1.53 | 0.00 | 0.65 | 0.00 | 1.72 | -0.00 | BC 449 |
| | | | | Max $V_z$ | -2.09 | 0.03 | 1.08 | -0.00 | 2.86 | -0.06 | BC 11 |
| | | | | Min $V_z$ | 2.13 | 0.03 | 0.65 | -0.00 | 1.72 | -0.07 | BC 408 |
| | | | | Max $M_T$ | -2.41 | 0.02 | 0.95 | 0.00 | 2.53 | -0.05 | BC 166 |
| | | | | Min $M_T$ | -1.31 | 0.02 | 0.95 | -0.00 | 2.54 | -0.05 | BC 243 |
| | | | | Max $M_y$ | -2.09 | 0.03 | 1.08 | -0.00 | 2.86 | -0.06 | BC 11 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 208 | RC1 | | | Min $M_y$ | 2.13 | 0.03 | 0.65 | -0.00 | 1.72 | -0.07 | BC 408 |
| | | | | Max $M_z$ | 1.53 | 0.00 | 0.65 | 0.00 | 1.72 | -0.00 | BC 449 |
| | | | | Min $M_z$ | 1.19 | 0.04 | 0.95 | -0.00 | 2.53 | -0.08 | BC 204 |
| 209 | RC1 | 154 | 0 | Max N | 2.20 | 0.05 | 0.89 | -0.12 | -0.00 | 0.00 | BC 413 |
| | | | | Min N | -2.43 | 0.04 | 0.89 | -0.12 | 0.00 | 0.00 | BC 446 |
| | | | | Max $V_y$ | -2.24 | 0.10 | 1.31 | -0.48 | -0.00 | 0.00 | BC 154 |
| | | | | Min $V_y$ | 1.86 | 0.02 | 0.89 | -0.12 | 0.00 | 0.00 | BC 360 |
| | | | | Max $V_z$ | -1.42 | 0.08 | 1.47 | -0.28 | 0.00 | 0.00 | BC 27 |
| | | | | Min $V_z$ | -2.37 | 0.03 | 0.89 | -0.12 | 0.00 | 0.00 | BC 450 |
| | | | | Max $M_T$ | 2.14 | 0.05 | 0.89 | -0.11 | 0.00 | 0.00 | BC 389 |
| | | | | Min $M_T$ | -2.24 | 0.10 | 1.31 | -0.48 | -0.00 | 0.00 | BC 154 |
| | | | | Max $M_y$ | -1.89 | 0.04 | 0.89 | -0.20 | 0.00 | -0.00 | BC 378 |
| | | | | Min $M_y$ | 1.49 | 0.04 | 1.31 | -0.25 | -0.00 | 0.00 | BC 232 |
| | | | | Max $M_z$ | -1.97 | 0.09 | 1.31 | -0.42 | -0.00 | 0.00 | BC 100 |
| | | | | Min $M_z$ | -1.67 | 0.07 | 1.30 | -0.26 | 0.00 | -0.00 | BC 182 |
| | | 31 | 2250 | Max N | 2.20 | 0.05 | 0.65 | -0.12 | 1.74 | -0.11 | BC 413 |
| | | | | Min N | -2.43 | 0.04 | 0.65 | -0.12 | 1.73 | -0.09 | BC 446 |
| | | | | Max $V_y$ | -2.24 | 0.10 | 0.96 | -0.48 | 2.55 | -0.23 | BC 154 |
| | | | | Min $V_y$ | 1.86 | 0.02 | 0.65 | -0.12 | 1.74 | -0.05 | BC 360 |
| | | | | Max $V_z$ | -1.42 | 0.08 | 1.08 | -0.28 | 2.87 | -0.19 | BC 27 |
| | | | | Min $V_z$ | -2.37 | 0.03 | 0.65 | -0.12 | 1.73 | -0.08 | BC 450 |
| | | | | Max $M_T$ | 2.14 | 0.05 | 0.65 | -0.11 | 1.74 | -0.10 | BC 389 |
| | | | | Min $M_T$ | -2.24 | 0.10 | 0.96 | -0.48 | 2.55 | -0.23 | BC 154 |
| | | | | Max $M_y$ | -1.42 | 0.08 | 1.08 | -0.28 | 2.87 | -0.19 | BC 27 |
| | | | | Min $M_y$ | -2.37 | 0.03 | 0.65 | -0.12 | 1.73 | -0.08 | BC 450 |
| | | | | Max $M_z$ | 1.86 | 0.02 | 0.65 | -0.12 | 1.74 | -0.05 | BC 360 |
| | | | | Min $M_z$ | -2.24 | 0.10 | 0.96 | -0.48 | 2.55 | -0.23 | BC 154 |
| 210 | RC1 | 153 | 0 | Max N | 1.46 | 0.04 | 0.88 | -0.00 | -0.00 | 0.00 | BC 417 |
| | | | | Min N | -8.26 | 0.11 | 1.27 | 0.01 | 0.00 | -0.00 | BC 279 |
| | | | | Max $V_y$ | -3.60 | 0.21 | 1.27 | 0.01 | 0.00 | 0.00 | BC 154 |
| | | | | Min $V_y$ | 1.46 | 0.04 | 0.88 | -0.00 | 0.00 | 0.00 | BC 389 |
| | | | | Max $V_z$ | -2.14 | 0.11 | 1.46 | -0.00 | 0.00 | -0.00 | BC 3 |
| | | | | Min $V_z$ | -3.11 | 0.18 | 0.86 | 0.01 | 0.00 | -0.00 | BC 347 |
| | | | | Max $M_T$ | -3.11 | 0.18 | 0.86 | 0.01 | 0.00 | 0.00 | BC 346 |
| | | | | Min $M_T$ | 1.17 | 0.08 | 1.30 | -0.00 | -0.00 | 0.00 | BC 197 |
| | | | | Max $M_y$ | -8.19 | 0.11 | 1.27 | 0.01 | 0.00 | -0.00 | BC 219 |
| | | | | Min $M_y$ | 0.27 | 0.13 | 1.30 | 0.00 | -0.00 | 0.00 | BC 232 |
| | | | | Max $M_z$ | 0.29 | 0.13 | 1.30 | 0.00 | -0.00 | 0.00 | BC 172 |
| | | | | Min $M_z$ | -8.19 | 0.11 | 1.27 | 0.01 | 0.00 | -0.00 | BC 219 |
| | | 32 | 2250 | Max N | 1.46 | 0.04 | 0.65 | -0.00 | 1.72 | -0.10 | BC 417 |
| | | | | Min N | -8.26 | 0.11 | 0.92 | 0.01 | 2.46 | -0.24 | BC 279 |
| | | | | Max $V_y$ | -3.60 | 0.21 | 0.92 | 0.01 | 2.46 | -0.48 | BC 154 |
| | | | | Min $V_y$ | 1.46 | 0.04 | 0.65 | -0.00 | 1.72 | -0.10 | BC 389 |
| | | | | Max $V_z$ | -2.14 | 0.11 | 1.06 | -0.00 | 2.84 | -0.24 | BC 3 |
| | | | | Min $V_z$ | -3.11 | 0.18 | 0.62 | 0.01 | 1.66 | -0.41 | BC 347 |
| | | | | Max $M_T$ | -3.11 | 0.18 | 0.62 | 0.01 | 1.66 | -0.41 | BC 346 |
| | | | | Min $M_T$ | 1.17 | 0.08 | 0.95 | -0.00 | 2.53 | -0.17 | BC 197 |
| | | | | Max $M_y$ | -2.14 | 0.11 | 1.06 | -0.00 | 2.84 | -0.24 | BC 3 |
| | | | | Min $M_y$ | -3.11 | 0.18 | 0.62 | 0.01 | 1.66 | -0.41 | BC 347 |
| | | | | Max $M_z$ | 1.46 | 0.04 | 0.65 | -0.00 | 1.72 | -0.10 | BC 389 |
| | | | | Min $M_z$ | -3.60 | 0.21 | 0.92 | 0.01 | 2.46 | -0.48 | BC 154 |
| 211 | RC1 | 152 | 0 | Max N | 1.20 | 0.05 | 0.87 | 0.11 | 0.00 | 0.00 | BC 413 |
| | | | | Min N | -5.55 | 0.06 | 0.82 | 0.12 | 0.00 | -0.00 | BC 355 |
| | | | | Max $V_y$ | -1.33 | 0.12 | 1.26 | 0.47 | 0.00 | 0.00 | BC 138 |
| | | | | Min $V_y$ | -4.03 | 0.03 | 0.83 | 0.11 | 0.00 | -0.00 | BC 447 |
| | | | | Max $V_z$ | 0.07 | 0.06 | 1.43 | 0.19 | -0.00 | 0.00 | BC 16 |
| | | | | Min $V_z$ | -5.55 | 0.06 | 0.82 | 0.12 | 0.00 | -0.00 | BC 355 |
| | | | | Max $M_T$ | -0.99 | 0.12 | 1.26 | 0.47 | 0.00 | -0.00 | BC 156 |
| | | | | Min $M_T$ | 1.19 | 0.05 | 0.87 | 0.11 | -0.00 | 0.00 | BC 381 |
| | | | | Max $M_y$ | -5.20 | 0.07 | 1.23 | 0.17 | 0.00 | -0.00 | BC 259 |
| | | | | Min $M_y$ | -0.23 | 0.08 | 1.27 | 0.26 | -0.00 | 0.00 | BC 200 |
| | | | | Max $M_z$ | -0.24 | 0.08 | 1.27 | 0.26 | -0.00 | 0.00 | BC 172 |
| | | | | Min $M_z$ | -5.20 | 0.07 | 1.23 | 0.17 | 0.00 | -0.00 | BC 259 |
| | | 33 | 2150 | Max N | 1.20 | 0.05 | 0.65 | 0.11 | 1.63 | -0.11 | BC 413 |
| | | | | Min N | -5.55 | 0.06 | 0.59 | 0.12 | 1.52 | -0.12 | BC 355 |
| | | | | Max $V_y$ | -1.33 | 0.12 | 0.92 | 0.47 | 2.34 | -0.26 | BC 138 |
| | | | | Min $V_y$ | -4.03 | 0.03 | 0.61 | 0.11 | 1.55 | -0.07 | BC 447 |
| | | | | Max $V_z$ | 0.07 | 0.06 | 1.06 | 0.19 | 2.68 | -0.14 | BC 16 |
| | | | | Min $V_z$ | -5.55 | 0.06 | 0.59 | 0.12 | 1.52 | -0.12 | BC 355 |
| | | | | Max $M_T$ | -0.99 | 0.12 | 0.93 | 0.47 | 2.35 | -0.26 | BC 156 |
| | | | | Min $M_T$ | 1.19 | 0.05 | 0.65 | 0.11 | 1.63 | -0.11 | BC 381 |
| | | | | Max $M_y$ | 0.07 | 0.06 | 1.06 | 0.19 | 2.68 | -0.14 | BC 16 |
| | | | | Min $M_y$ | -5.55 | 0.06 | 0.59 | 0.12 | 1.52 | -0.12 | BC 355 |
| | | | | Max $M_z$ | -4.03 | 0.03 | 0.61 | 0.11 | 1.55 | -0.07 | BC 447 |
| | | | | Min $M_z$ | -1.33 | 0.12 | 0.92 | 0.47 | 2.34 | -0.26 | BC 138 |
| 212 | RC1 | 163 | 0 | Max N | 0.24 | 0.00 | 0.23 | -0.24 | 0.00 | 0.00 | BC 472 |
| | | | | Min N | -0.30 | 0.00 | 0.33 | -0.49 | 0.00 | 0.00 | BC 242 |
| | | | | Max $V_y$ | -0.04 | 0.00 | 0.37 | -0.38 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.04 | 0.00 | 0.37 | -0.38 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.04 | 0.00 | 0.37 | -0.38 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.27 | 0.00 | 0.23 | -0.23 | 0.00 | 0.00 | BC 354 |
| | | | | Max $M_T$ | -0.27 | 0.00 | 0.23 | -0.23 | 0.00 | 0.00 | BC 358 |
| | | | | Min $M_T$ | -0.08 | 0.00 | 0.33 | -0.89 | 0.00 | 0.00 | BC 154 |
| | | | | Max $M_y$ | -0.28 | 0.00 | 0.33 | -0.34 | 0.00 | 0.00 | BC 162 |
| | | | | Min $M_y$ | -0.28 | 0.00 | 0.33 | -0.33 | -0.00 | 0.00 | BC 198 |
| | | | | Max $M_z$ | -0.04 | 0.00 | 0.37 | -0.38 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.04 | 0.00 | 0.37 | -0.38 | 0.00 | 0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 212 | RC1 | 162 | 4300 | Max N | 0.24 | 0.00 | -0.23 | -0.24 | 0.00 | 0.00 | BC 472 |
| | | | | Min N | -0.30 | 0.00 | -0.33 | -0.49 | 0.00 | 0.00 | BC 242 |
| | | | | Max $V_y$ | -0.04 | 0.00 | -0.37 | -0.38 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.04 | 0.00 | -0.37 | -0.38 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.27 | 0.00 | -0.23 | -0.23 | 0.00 | 0.00 | BC 354 |
| | | | | Min $V_z$ | -0.04 | 0.00 | -0.37 | -0.38 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.27 | 0.00 | -0.23 | -0.23 | 0.00 | 0.00 | BC 358 |
| | | | | Min $M_T$ | -0.08 | 0.00 | -0.33 | -0.89 | 0.00 | 0.00 | BC 154 |
| | | | | Max $M_y$ | -0.28 | 0.00 | -0.33 | -0.34 | 0.00 | 0.00 | BC 162 |
| | | | | Min $M_y$ | -0.28 | 0.00 | -0.33 | -0.33 | -0.00 | 0.00 | BC 198 |
| | | | | Max $M_z$ | -0.04 | 0.00 | -0.37 | -0.38 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.04 | 0.00 | -0.37 | -0.38 | 0.00 | 0.00 | BC 1 |
| 213 | RC1 | 162 | 0 | Max N | 0.74 | 0.02 | 0.88 | -0.00 | 0.00 | 0.00 | BC 408 |
| | | | | Min N | -1.53 | 0.26 | 1.32 | -0.03 | 0.00 | 0.00 | BC 146 |
| | | | | Max $V_y$ | -1.52 | 0.26 | 1.32 | -0.03 | 0.00 | 0.00 | BC 138 |
| | | | | Min $V_y$ | -0.80 | 0.02 | 0.89 | -0.01 | 0.00 | 0.00 | BC 446 |
| | | | | Max $V_z$ | -0.90 | 0.13 | 1.48 | -0.02 | 0.00 | 0.00 | BC 22 |
| | | | | Min $V_z$ | 0.72 | 0.02 | 0.88 | -0.00 | 0.00 | 0.00 | BC 356 |
| | | | | Max $M_T$ | -0.66 | 0.02 | 0.89 | -0.00 | 0.00 | 0.00 | BC 363 |
| | | | | Min $M_T$ | -1.50 | 0.26 | 1.32 | -0.03 | 0.00 | 0.00 | BC 139 |
| | | | | Max $M_y$ | -0.82 | 0.04 | 1.30 | -0.02 | 0.00 | -0.00 | BC 162 |
| | | | | Min $M_y$ | -0.83 | 0.04 | 1.30 | -0.02 | -0.00 | 0.00 | BC 198 |
| | | | | Max $M_z$ | -0.67 | 0.08 | 1.47 | -0.01 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.82 | 0.04 | 1.30 | -0.02 | 0.00 | -0.00 | BC 162 |
| | | 38 | 2250 | Max N | 0.74 | 0.02 | 0.65 | -0.00 | 1.72 | -0.05 | BC 408 |
| | | | | Min N | -1.53 | 0.26 | 0.97 | -0.03 | 2.57 | -0.59 | BC 146 |
| | | | | Max $V_y$ | -1.52 | 0.26 | 0.97 | -0.03 | 2.57 | -0.59 | BC 138 |
| | | | | Min $V_y$ | -0.80 | 0.02 | 0.65 | -0.01 | 1.73 | -0.04 | BC 446 |
| | | | | Max $V_z$ | -0.90 | 0.13 | 1.09 | -0.02 | 2.88 | -0.29 | BC 22 |
| | | | | Min $V_z$ | 0.72 | 0.02 | 0.65 | -0.00 | 1.72 | -0.06 | BC 356 |
| | | | | Max $M_T$ | -0.66 | 0.02 | 0.65 | -0.00 | 1.73 | -0.05 | BC 363 |
| | | | | Min $M_T$ | -1.50 | 0.26 | 0.97 | -0.03 | 2.57 | -0.59 | BC 139 |
| | | | | Max $M_y$ | -0.90 | 0.13 | 1.09 | -0.02 | 2.88 | -0.29 | BC 22 |
| | | | | Min $M_y$ | 0.72 | 0.02 | 0.65 | -0.00 | 1.72 | -0.06 | BC 356 |
| | | | | Max $M_z$ | -0.80 | 0.02 | 0.65 | -0.01 | 1.73 | -0.04 | BC 446 |
| | | | | Min $M_z$ | -1.52 | 0.26 | 0.97 | -0.03 | 2.57 | -0.59 | BC 138 |
| 214 | RC1 | 161 | 0 | Max N | 0.14 | 0.00 | 0.23 | 0.26 | 0.00 | 0.00 | BC 408 |
| | | | | Min N | -1.06 | 0.00 | 0.33 | 0.87 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_y$ | -0.46 | 0.00 | 0.37 | 0.39 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.46 | 0.00 | 0.37 | 0.39 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.46 | 0.00 | 0.37 | 0.39 | 0.00 | 0.00 | BC 2 |
| | | | | Min $V_z$ | -0.93 | 0.00 | 0.23 | 0.76 | 0.00 | 0.00 | BC 323 |
| | | | | Max $M_T$ | -1.04 | 0.00 | 0.33 | 0.88 | 0.00 | 0.00 | BC 154 |
| | | | | Min $M_T$ | -0.27 | 0.00 | 0.23 | 0.22 | 0.00 | 0.00 | BC 389 |
| | | | | Max $M_y$ | -0.50 | 0.00 | 0.33 | 0.35 | 0.00 | 0.00 | BC 198 |
| | | | | Min $M_y$ | -0.57 | 0.00 | 0.33 | 0.50 | -0.00 | 0.00 | BC 182 |
| | | | | Max $M_z$ | -0.46 | 0.00 | 0.37 | 0.39 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.46 | 0.00 | 0.37 | 0.39 | 0.00 | 0.00 | BC 1 |
| | | 160 | 4300 | Max N | 0.14 | 0.00 | -0.23 | 0.26 | 0.00 | 0.00 | BC 408 |
| | | | | Min N | -1.06 | 0.00 | -0.33 | 0.87 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_y$ | -0.46 | 0.00 | -0.37 | 0.39 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.46 | 0.00 | -0.37 | 0.39 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.93 | 0.00 | -0.23 | 0.76 | 0.00 | 0.00 | BC 323 |
| | | | | Min $V_z$ | -0.46 | 0.00 | -0.37 | 0.39 | 0.00 | 0.00 | BC 2 |
| | | | | Max $M_T$ | -1.04 | 0.00 | -0.33 | 0.88 | 0.00 | 0.00 | BC 154 |
| | | | | Min $M_T$ | -0.27 | 0.00 | -0.23 | 0.22 | 0.00 | 0.00 | BC 389 |
| | | | | Max $M_y$ | -0.50 | 0.00 | -0.33 | 0.35 | 0.00 | 0.00 | BC 198 |
| | | | | Min $M_y$ | -0.57 | 0.00 | -0.33 | 0.50 | -0.00 | 0.00 | BC 182 |
| | | | | Max $M_z$ | -0.46 | 0.00 | -0.37 | 0.39 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.46 | 0.00 | -0.37 | 0.39 | 0.00 | 0.00 | BC 1 |
| 215 | RC1 | 159 | 0 | Max N | 0.12 | -0.05 | 1.30 | -0.03 | 0.00 | 0.00 | BC 204 |
| | | | | Min N | -0.10 | -0.03 | 0.89 | -0.02 | 0.00 | 0.00 | BC 447 |
| | | | | Max $V_y$ | 0.03 | -0.02 | 0.89 | -0.02 | 0.00 | 0.00 | BC 461 |
| | | | | Min $V_y$ | 0.02 | -0.05 | 1.47 | -0.00 | -0.00 | 0.00 | BC 18 |
| | | | | Max $V_z$ | 0.02 | -0.05 | 1.47 | -0.00 | 0.00 | 0.00 | BC 11 |
| | | | | Min $V_z$ | -0.10 | -0.04 | 0.89 | -0.00 | 0.00 | 0.00 | BC 391 |
| | | | | Max $M_T$ | -0.01 | -0.03 | 0.89 | 0.01 | 0.00 | 0.00 | BC 390 |
| | | | | Min $M_T$ | -0.09 | -0.05 | 1.30 | -0.03 | 0.00 | 0.00 | BC 267 |
| | | | | Max $M_y$ | 0.03 | -0.03 | 0.89 | 0.01 | 0.00 | 0.00 | BC 361 |
| | | | | Min $M_y$ | -0.00 | -0.04 | 1.30 | -0.02 | -0.00 | 0.00 | BC 91 |
| | | | | Max $M_z$ | 0.02 | -0.05 | 1.47 | -0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.02 | -0.05 | 1.47 | -0.00 | -0.00 | 0.00 | BC 1 |
| | | 164 | 2250 | Max N | 0.12 | -0.05 | 0.95 | -0.03 | 2.54 | 0.11 | BC 204 |
| | | | | Min N | -0.10 | -0.03 | 0.65 | -0.02 | 1.73 | 0.08 | BC 447 |
| | | | | Max $V_y$ | 0.03 | -0.02 | 0.65 | -0.02 | 1.73 | 0.05 | BC 461 |
| | | | | Min $V_y$ | 0.02 | -0.05 | 1.08 | -0.00 | 2.86 | 0.11 | BC 18 |
| | | | | Max $V_z$ | 0.02 | -0.05 | 1.08 | -0.00 | 2.86 | 0.11 | BC 11 |
| | | | | Min $V_z$ | -0.10 | -0.04 | 0.65 | -0.00 | 1.72 | 0.08 | BC 391 |
| | | | | Max $M_T$ | -0.01 | -0.03 | 0.65 | 0.01 | 1.73 | 0.08 | BC 390 |
| | | | | Min $M_T$ | -0.09 | -0.05 | 0.95 | -0.03 | 2.53 | 0.10 | BC 267 |
| | | | | Max $M_y$ | 0.02 | -0.05 | 1.08 | -0.00 | 2.86 | 0.11 | BC 11 |
| | | | | Min $M_y$ | -0.10 | -0.04 | 0.65 | -0.00 | 1.72 | 0.08 | BC 391 |
| | | | | Max $M_z$ | 0.02 | -0.05 | 1.08 | -0.00 | 2.86 | 0.11 | BC 18 |
| | | | | Min $M_z$ | 0.03 | -0.02 | 0.65 | -0.02 | 1.73 | 0.05 | BC 461 |
| 216 | RC1 | 158 | 0 | Max N | 0.01 | 0.00 | 0.23 | -0.01 | 0.00 | 0.00 | BC 356 |
| | | | | Min N | -0.05 | 0.00 | 0.33 | -0.01 | 0.00 | 0.00 | BC 269 |
| | | | | Max $V_y$ | -0.02 | 0.00 | 0.37 | -0.02 | 0.00 | 0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 216 | RC1 | | | Min $V_y$ | -0.02 | 0.00 | 0.37 | -0.02 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.02 | 0.00 | 0.37 | -0.02 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.01 | 0.00 | 0.23 | -0.01 | 0.00 | 0.00 | BC 33 |
| | | | | Max $M_T$ | 0.00 | 0.00 | 0.23 | 0.01 | 0.00 | 0.00 | BC 428 |
| | | | | Min $M_T$ | -0.04 | 0.00 | 0.33 | -0.03 | 0.00 | 0.00 | BC 225 |
| | | | | Max $M_y$ | -0.02 | 0.00 | 0.33 | -0.00 | 0.00 | 0.00 | BC 91 |
| | | | | Min $M_y$ | -0.02 | 0.00 | 0.37 | -0.02 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.02 | 0.00 | 0.37 | -0.02 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.02 | 0.00 | 0.37 | -0.02 | 0.00 | 0.00 | BC 1 |
| | | 157 | 4300 | Max N | 0.01 | 0.00 | -0.23 | -0.01 | 0.00 | 0.00 | BC 356 |
| | | | | Min N | -0.05 | 0.00 | -0.33 | -0.01 | 0.00 | 0.00 | BC 269 |
| | | | | Max $V_y$ | -0.02 | 0.00 | -0.37 | -0.02 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.02 | 0.00 | -0.37 | -0.02 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.01 | 0.00 | -0.23 | -0.01 | 0.00 | 0.00 | BC 33 |
| | | | | Min $V_z$ | -0.02 | 0.00 | -0.37 | -0.02 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.00 | 0.00 | -0.23 | 0.01 | 0.00 | 0.00 | BC 428 |
| | | | | Min $M_T$ | -0.04 | 0.00 | -0.33 | -0.03 | 0.00 | 0.00 | BC 225 |
| | | | | Max $M_y$ | -0.02 | 0.00 | -0.33 | -0.00 | 0.00 | 0.00 | BC 91 |
| | | | | Min $M_y$ | -0.02 | 0.00 | -0.37 | -0.02 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.02 | 0.00 | -0.37 | -0.02 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.02 | 0.00 | -0.37 | -0.02 | 0.00 | 0.00 | BC 1 |
| 217 | RC1 | 23 | 0 | Max N | 57.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 139 |
| | | | | Min N | -0.44 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 451 |
| | | | | Max $V_u$ | 22.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 22.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 22.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 22.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 22.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 22.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 22.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 22.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 22.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 22.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 82 | 3912 | Max N | 57.10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 139 |
| | | | | Min N | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 451 |
| | | | | Max $V_u$ | 22.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 22.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 22.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 22.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 22.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 22.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 22.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 22.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 22.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 22.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 218 | RC1 | 23 | 0 | Max N | 53.70 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 149 |
| | | | | Min N | -0.68 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 358 |
| | | | | Max $V_u$ | 22.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 22.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 22.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 22.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 22.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 22.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 22.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 22.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 22.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 22.41 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 81 | 3912 | Max N | 53.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 149 |
| | | | | Min N | -0.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 358 |
| | | | | Max $V_u$ | 22.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 22.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 22.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 22.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 22.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 22.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 22.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 22.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 22.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 22.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 219 | RC1 | 23 | 0 | Max N | 6.37 | 0.04 | -0.69 | 0.00 | 1.81 | 0.09 | BC 413 |
| | | | | Min N | -2.98 | 0.15 | -0.92 | -0.00 | 2.47 | 0.34 | BC 244 |
| | | | | Max $V_y$ | -1.61 | 0.28 | -0.94 | 0.01 | 2.51 | 0.64 | BC 148 |
| | | | | Min $V_y$ | -0.83 | 0.03 | -0.64 | 0.01 | 1.71 | 0.08 | BC 362 |
| | | | | Max $V_z$ | -2.75 | 0.12 | -0.63 | -0.00 | 1.67 | 0.27 | BC 436 |
| | | | | Min $V_z$ | -0.51 | 0.10 | -1.06 | 0.00 | 2.83 | 0.23 | BC 31 |
| | | | | Max $M_T$ | -0.80 | 0.11 | -0.94 | 0.01 | 2.51 | 0.24 | BC 202 |
| | | | | Min $M_T$ | -1.97 | 0.07 | -0.63 | -0.00 | 1.68 | 0.16 | BC 356 |
| | | | | Max $M_y$ | -0.51 | 0.10 | -1.06 | 0.00 | 2.83 | 0.23 | BC 31 |
| | | | | Min $M_y$ | -2.75 | 0.12 | -0.63 | -0.00 | 1.67 | 0.27 | BC 436 |
| | | | | Max $M_z$ | -1.61 | 0.28 | -0.94 | 0.01 | 2.51 | 0.64 | BC 148 |
| | | | | Min $M_z$ | -0.83 | 0.03 | -0.64 | 0.01 | 1.71 | 0.08 | BC 362 |
| | | 148 | 2250 | Max N | 6.37 | 0.04 | -0.92 | 0.00 | 0.00 | 0.00 | BC 413 |
| | | | | Min N | -2.98 | 0.15 | -1.27 | -0.00 | 0.00 | 0.00 | BC 244 |
| | | | | Max $V_y$ | -1.61 | 0.28 | -1.29 | 0.01 | 0.00 | 0.00 | BC 148 |
| | | | | Min $V_y$ | -0.83 | 0.03 | -0.88 | 0.01 | 0.00 | 0.00 | BC 362 |
| | | | | Max $V_z$ | -2.75 | 0.12 | -0.86 | -0.00 | 0.00 | 0.00 | BC 436 |
| | | | | Min $V_z$ | -0.51 | 0.10 | -1.46 | 0.00 | 0.00 | 0.00 | BC 31 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 219 | RC1 | | | Max $M_T$ | -0.80 | 0.11 | -1.29 | 0.01 | 0.00 | 0.00 | BC 202 |
| | | | | Min $M_T$ | -1.97 | 0.07 | -0.87 | -0.00 | -0.00 | 0.00 | BC 356 |
| | | | | Max $M_y$ | -2.98 | 0.15 | -1.27 | -0.00 | 0.00 | 0.00 | BC 244 |
| | | | | Min $M_y$ | -1.88 | 0.15 | -1.28 | -0.00 | -0.00 | -0.00 | BC 264 |
| | | | | Max $M_z$ | -2.92 | 0.15 | -1.27 | -0.00 | 0.00 | 0.00 | BC 232 |
| | | | | Min $M_z$ | -1.88 | 0.15 | -1.28 | -0.00 | -0.00 | -0.00 | BC 264 |
| 220 | RC1 | 26 | 0 | Max N | 29.34 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min N | -1.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 359 |
| | | | | Max $V_u$ | -0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 84 | 3912 | Max N | 29.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min N | -1.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 359 |
| | | | | Max $V_u$ | -0.14 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.14 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.14 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.14 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.14 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.14 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.14 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.14 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.14 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.14 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 221 | RC1 | 26 | 0 | Max N | 27.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 419 |
| | | | | Min N | -0.79 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 282 |
| | | | | Max $V_u$ | -0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 83 | 3912 | Max N | 27.98 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 419 |
| | | | | Min N | -0.77 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 282 |
| | | | | Max $V_u$ | -0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 222 | RC1 | 26 | 0 | Max N | 0.77 | 0.03 | -0.90 | -0.00 | 2.42 | 0.06 | BC 241 |
| | | | | Min N | -0.59 | 0.04 | -0.94 | -0.00 | 2.51 | 0.09 | BC 175 |
| | | | | Max $V_y$ | -0.16 | 0.16 | -0.95 | -0.01 | 2.53 | 0.36 | BC 149 |
| | | | | Min $V_y$ | 0.76 | -0.01 | -0.60 | 0.00 | 1.61 | -0.03 | BC 445 |
| | | | | Max $V_z$ | 0.75 | -0.01 | -0.60 | 0.00 | 1.61 | -0.03 | BC 413 |
| | | | | Min $V_z$ | -0.15 | 0.08 | -1.07 | -0.01 | 2.84 | 0.17 | BC 22 |
| | | | | Max $M_T$ | -0.50 | 0.00 | -0.64 | 0.01 | 1.71 | 0.01 | BC 471 |
| | | | | Min $M_T$ | -0.15 | 0.16 | -0.95 | -0.01 | 2.53 | 0.36 | BC 134 |
| | | | | Max $M_y$ | -0.15 | 0.08 | -1.07 | -0.01 | 2.84 | 0.17 | BC 22 |
| | | | | Min $M_y$ | 0.75 | -0.01 | -0.60 | 0.00 | 1.61 | -0.03 | BC 413 |
| | | | | Max $M_z$ | -0.16 | 0.16 | -0.95 | -0.01 | 2.53 | 0.36 | BC 149 |
| | | | | Min $M_z$ | 0.76 | -0.01 | -0.60 | 0.00 | 1.61 | -0.03 | BC 445 |
| | | 146 | 2250 | Max N | 0.77 | 0.03 | -1.25 | -0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min N | -0.59 | 0.04 | -1.29 | -0.00 | 0.00 | 0.00 | BC 175 |
| | | | | Max $V_y$ | -0.16 | 0.16 | -1.30 | -0.01 | 0.00 | 0.00 | BC 149 |
| | | | | Min $V_y$ | 0.76 | -0.01 | -0.83 | 0.00 | 0.00 | 0.00 | BC 445 |
| | | | | Max $V_z$ | 0.75 | -0.01 | -0.83 | 0.00 | 0.00 | 0.00 | BC 413 |
| | | | | Min $V_z$ | -0.15 | 0.08 | -1.46 | -0.01 | 0.00 | 0.00 | BC 22 |
| | | | | Max $M_T$ | -0.50 | 0.00 | -0.88 | 0.01 | -0.00 | 0.00 | BC 471 |
| | | | | Min $M_T$ | -0.15 | 0.16 | -1.30 | -0.01 | 0.00 | 0.00 | BC 134 |
| | | | | Max $M_y$ | -0.13 | 0.08 | -1.30 | 0.01 | 0.00 | 0.00 | BC 264 |
| | | | | Min $M_y$ | -0.14 | 0.08 | -1.30 | -0.01 | -0.00 | 0.00 | BC 172 |
| | | | | Max $M_z$ | -0.17 | 0.04 | -1.46 | -0.01 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.17 | 0.04 | -1.46 | -0.01 | 0.00 | 0.00 | BC 1 |
| 223 | RC1 | 27 | 0 | Max N | 44.73 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 164 |
| | | | | Min N | -1.83 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 185 |
| | | | | Max $V_u$ | -0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 223 | RC1 | | | Min $M_u$ | -0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 85 | 3901 | Max N | 44.75 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 164 |
| | | | | Min N | -1.81 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 185 |
| | | | | Max $V_u$ | -0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 224 | RC1 | 27 | 0 | Max N | 45.44 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min N | -0.90 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 166 |
| | | | | Max $V_u$ | -0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 39 | 3901 | Max N | 45.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min N | -0.89 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 166 |
| | | | | Max $V_u$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 225 | RC1 | 27 | 0 | Max N | 1.75 | 0.02 | -0.65 | -0.01 | 1.65 | 0.05 | BC 412 |
| | | | | Min N | -1.26 | -0.01 | -0.63 | 0.00 | 1.61 | -0.03 | BC 446 |
| | | | | Max $V_y$ | 1.74 | 0.02 | -0.65 | -0.01 | 1.65 | 0.05 | BC 400 |
| | | | | Min $V_y$ | 1.42 | -0.05 | -0.95 | 0.02 | 2.39 | -0.11 | BC 201 |
| | | | | Max $V_z$ | -1.26 | -0.01 | -0.63 | 0.00 | 1.61 | -0.03 | BC 446 |
| | | | | Min $V_z$ | -0.26 | -0.02 | -1.06 | 0.01 | 2.68 | -0.05 | BC 12 |
| | | | | Max $M_T$ | 1.32 | -0.05 | -0.95 | 0.02 | 2.39 | -0.10 | BC 241 |
| | | | | Min $M_T$ | 1.69 | 0.02 | -0.65 | -0.01 | 1.64 | 0.04 | BC 356 |
| | | | | Max $M_y$ | -0.26 | -0.02 | -1.06 | 0.01 | 2.68 | -0.05 | BC 12 |
| | | | | Min $M_y$ | -1.26 | -0.01 | -0.63 | 0.00 | 1.61 | -0.03 | BC 446 |
| | | | | Max $M_z$ | 1.74 | 0.02 | -0.65 | -0.01 | 1.65 | 0.05 | BC 400 |
| | | | | Min $M_z$ | 1.42 | -0.05 | -0.95 | 0.02 | 2.39 | -0.11 | BC 201 |
| | | 155 | 2150 | Max N | 1.75 | 0.02 | -0.88 | -0.01 | -0.00 | 0.00 | BC 412 |
| | | | | Min N | -1.26 | -0.01 | -0.86 | 0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Max $V_y$ | 1.74 | 0.02 | -0.88 | -0.01 | 0.00 | 0.00 | BC 400 |
| | | | | Min $V_y$ | 1.42 | -0.05 | -1.28 | 0.02 | -0.00 | 0.00 | BC 201 |
| | | | | Max $V_z$ | -1.26 | -0.01 | -0.86 | 0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Min $V_z$ | -0.26 | -0.02 | -1.43 | 0.01 | 0.00 | 0.00 | BC 12 |
| | | | | Max $M_T$ | 1.32 | -0.05 | -1.28 | 0.02 | -0.00 | 0.00 | BC 241 |
| | | | | Min $M_T$ | 1.69 | 0.02 | -0.88 | -0.01 | 0.00 | 0.00 | BC 356 |
| | | | | Max $M_y$ | -1.03 | -0.01 | -0.86 | 0.00 | 0.00 | 0.00 | BC 426 |
| | | | | Min $M_y$ | 1.60 | -0.01 | -0.88 | 0.00 | -0.00 | 0.00 | BC 415 |
| | | | | Max $M_z$ | -0.24 | -0.02 | -1.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.24 | -0.02 | -1.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| 226 | RC1 | 28 | 0 | Max N | -0.39 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 413 |
| | | | | Min N | -1.92 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_u$ | -0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 86 | 3957 | Max N | -0.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 413 |
| | | | | Min N | -1.91 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_u$ | -0.74 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.74 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.74 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.74 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.74 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.74 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.74 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.74 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.74 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.74 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 227 | RC1 | 28 | 0 | Max N | -0.27 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 440 |
| | | | | Min N | -2.69 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 132 |
| | | | | Max $V_u$ | -1.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -1.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -1.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -1.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -1.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -1.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -1.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -1.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -1.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -1.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 85 | 3957 | Max N | -0.26 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 440 |
| | | | | Min N | -2.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 132 |
| | | | | Max $V_u$ | -1.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -1.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -1.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -1.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -1.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -1.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -1.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -1.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -1.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -1.16 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 228 | RC1 | 28 | 0 | Max N | 2.33 | -0.03 | -0.65 | 0.00 | 1.73 | -0.07 | BC 408 |
| | | | | Min N | -3.85 | -0.02 | -0.95 | -0.00 | 2.52 | -0.05 | BC 149 |
| | | | | Max $V_y$ | 1.70 | -0.00 | -0.65 | -0.00 | 1.73 | -0.00 | BC 449 |
| | | | | Min $V_y$ | 1.25 | -0.04 | -0.95 | -0.00 | 2.53 | -0.08 | BC 204 |
| | | | | Max $V_z$ | -3.34 | -0.02 | -0.64 | -0.00 | 1.72 | -0.04 | BC 338 |
| | | | | Min $V_z$ | -1.69 | -0.02 | -1.07 | -0.00 | 2.85 | -0.06 | BC 16 |
| | | | | Max $M_T$ | -2.61 | -0.02 | -0.95 | 0.00 | 2.53 | -0.05 | BC 166 |
| | | | | Min $M_T$ | -1.70 | -0.02 | -0.95 | -0.00 | 2.52 | -0.05 | BC 243 |
| | | | | Max $M_y$ | -1.69 | -0.02 | -1.07 | -0.00 | 2.85 | -0.06 | BC 16 |
| | | | | Min $M_y$ | -3.34 | -0.02 | -0.64 | -0.00 | 1.72 | -0.04 | BC 338 |
| | | | | Max $M_z$ | 1.70 | -0.00 | -0.65 | -0.00 | 1.73 | -0.00 | BC 449 |
| | | | | Min $M_z$ | 1.25 | -0.04 | -0.95 | -0.00 | 2.53 | -0.08 | BC 204 |
| | | 154 | 2250 | Max N | 2.33 | -0.03 | -0.89 | 0.00 | -0.00 | 0.00 | BC 408 |
| | | | | Min N | -3.85 | -0.02 | -1.29 | -0.00 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_y$ | 1.70 | -0.00 | -0.89 | -0.00 | -0.00 | 0.00 | BC 449 |
| | | | | Min $V_y$ | 1.25 | -0.04 | -1.30 | -0.00 | 0.00 | 0.00 | BC 204 |
| | | | | Max $V_z$ | -3.34 | -0.02 | -0.88 | -0.00 | 0.00 | 0.00 | BC 338 |
| | | | | Min $V_z$ | -1.69 | -0.02 | -1.46 | -0.00 | -0.00 | 0.00 | BC 16 |
| | | | | Max $M_T$ | -2.61 | -0.02 | -1.30 | 0.00 | -0.00 | 0.00 | BC 166 |
| | | | | Min $M_T$ | -1.70 | -0.02 | -1.29 | -0.00 | -0.00 | 0.00 | BC 243 |
| | | | | Max $M_y$ | -2.51 | -0.01 | -0.88 | 0.00 | 0.00 | -0.00 | BC 378 |
| | | | | Min $M_y$ | 1.25 | -0.04 | -1.30 | -0.00 | -0.00 | 0.00 | BC 232 |
| | | | | Max $M_z$ | 2.31 | -0.03 | -0.89 | 0.00 | 0.00 | 0.00 | BC 384 |
| | | | | Min $M_z$ | 1.81 | -0.04 | -1.30 | 0.00 | 0.00 | -0.00 | BC 160 |
| 229 | RC1 | 31 | 0 | Max N | 19.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 217 |
| | | | | Min N | -0.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 184 |
| | | | | Max $V_u$ | 0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 0.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 68 | 3957 | Max N | 19.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 217 |
| | | | | Min N | -0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 184 |
| | | | | Max $V_u$ | 0.56 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 0.56 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 0.56 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 0.56 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.56 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.56 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 0.56 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 0.56 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 0.56 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 0.56 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 230 | RC1 | 31 | 0 | Max N | 17.72 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 432 |
| | | | | Min N | -1.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 205 |
| | | | | Max $V_u$ | -0.83 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.83 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.83 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.83 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.83 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.83 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.83 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.83 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.83 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.83 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 86 | 3957 | Max N | 17.73 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 432 |
| | | | | Min N | -1.48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 205 |
| | | | | Max $V_u$ | -0.81 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 230 | RC1 | | | Min $V_u$ | -0.81 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.81 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.81 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.81 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.81 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.81 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.81 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.81 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.81 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 231 | RC1 | 31 | 0 | Max N | 1.50 | -0.05 | -0.64 | -0.11 | 1.71 | -0.10 | BC 417 |
| | | | | Min N | -8.06 | -0.08 | -0.89 | -0.18 | 2.38 | -0.18 | BC 279 |
| | | | | Max $V_y$ | 1.19 | -0.02 | -0.64 | -0.12 | 1.71 | -0.05 | BC 360 |
| | | | | Min $V_y$ | -3.51 | -0.10 | -0.94 | -0.48 | 2.50 | -0.23 | BC 154 |
| | | | | Max $V_z$ | -7.56 | -0.06 | -0.58 | -0.12 | 1.56 | -0.13 | BC 471 |
| | | | | Min $V_z$ | -1.97 | -0.07 | -1.07 | -0.19 | 2.84 | -0.15 | BC 25 |
| | | | | Max $M_T$ | 1.50 | -0.05 | -0.64 | -0.11 | 1.71 | -0.10 | BC 389 |
| | | | | Min $M_T$ | -3.51 | -0.10 | -0.94 | -0.48 | 2.50 | -0.23 | BC 154 |
| | | | | Max $M_y$ | -1.97 | -0.07 | -1.07 | -0.19 | 2.84 | -0.15 | BC 25 |
| | | | | Min $M_y$ | -7.56 | -0.06 | -0.58 | -0.12 | 1.56 | -0.13 | BC 471 |
| | | | | Max $M_z$ | 1.19 | -0.02 | -0.64 | -0.12 | 1.71 | -0.05 | BC 360 |
| | | | | Min $M_z$ | -3.51 | -0.10 | -0.94 | -0.48 | 2.50 | -0.23 | BC 154 |
| | | 153 | 2250 | Max N | 1.50 | -0.05 | -0.88 | -0.11 | -0.00 | 0.00 | BC 417 |
| | | | | Min N | -8.06 | -0.08 | -1.23 | -0.18 | 0.00 | -0.00 | BC 279 |
| | | | | Max $V_y$ | 1.19 | -0.02 | -0.88 | -0.12 | 0.00 | 0.00 | BC 360 |
| | | | | Min $V_y$ | -3.51 | -0.10 | -1.29 | -0.48 | 0.00 | 0.00 | BC 154 |
| | | | | Max $V_z$ | -7.56 | -0.06 | -0.81 | -0.12 | 0.00 | -0.00 | BC 471 |
| | | | | Min $V_z$ | -1.97 | -0.07 | -1.46 | -0.19 | 0.00 | 0.00 | BC 25 |
| | | | | Max $M_T$ | 1.50 | -0.05 | -0.88 | -0.11 | 0.00 | 0.00 | BC 389 |
| | | | | Min $M_T$ | -3.51 | -0.10 | -1.29 | -0.48 | 0.00 | 0.00 | BC 154 |
| | | | | Max $M_y$ | -8.06 | -0.08 | -1.23 | -0.18 | 0.00 | -0.00 | BC 279 |
| | | | | Min $M_y$ | 0.26 | -0.04 | -1.29 | -0.25 | -0.00 | 0.00 | BC 232 |
| | | | | Max $M_z$ | 0.38 | -0.10 | -1.29 | -0.25 | -0.00 | 0.00 | BC 205 |
| | | | | Min $M_z$ | -7.99 | -0.08 | -1.23 | -0.18 | 0.00 | -0.00 | BC 219 |
| 232 | RC1 | 32 | 0 | Max N | 11.83 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 268 |
| | | | | Min N | -0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 359 |
| | | | | Max $V_u$ | 3.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 3.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 3.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 3.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 3.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 3.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 3.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 3.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 3.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 3.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 67 | 3957 | Max N | 11.85 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 268 |
| | | | | Min N | -0.23 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 359 |
| | | | | Max $V_u$ | 3.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 3.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 3.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 3.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 3.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 3.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 3.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 3.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 3.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 3.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 233 | RC1 | 32 | 0 | Max N | 15.94 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 265 |
| | | | | Min N | -0.12 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 388 |
| | | | | Max $V_u$ | 4.85 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 4.85 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 4.85 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 4.85 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 4.85 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 4.85 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 4.85 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 4.85 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 4.85 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 4.85 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 68 | 3957 | Max N | 15.95 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 265 |
| | | | | Min N | -0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 388 |
| | | | | Max $V_u$ | 4.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 4.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 4.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 4.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 4.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 4.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 4.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 4.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 4.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 4.86 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 234 | RC1 | 32 | 0 | Max N | 1.48 | -0.05 | -0.65 | 0.01 | 1.73 | -0.11 | BC 413 |
| | | | | Min N | -5.77 | -0.08 | -0.65 | 0.01 | 1.73 | -0.18 | BC 355 |
| | | | | Max $V_y$ | 1.44 | -0.04 | -0.65 | -0.00 | 1.72 | -0.10 | BC 389 |
| | | | | Min $V_y$ | 0.01 | -0.21 | -0.98 | 0.03 | 2.59 | -0.48 | BC 154 |
| | | | | Max $V_z$ | -0.05 | -0.07 | -0.64 | 0.02 | 1.70 | -0.16 | BC 380 |
| | | | | Min $V_z$ | 0.05 | -0.14 | -1.09 | 0.02 | 2.90 | -0.31 | BC 27 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 234 | RC1 | | | Max $M_T$ | 0.01 | -0.21 | -0.98 | 0.03 | 2.59 | -0.48 | BC 154 |
| | | | | Min $M_T$ | 1.44 | -0.04 | -0.65 | -0.00 | 1.72 | -0.10 | BC 389 |
| | | | | Max $M_y$ | 0.05 | -0.14 | -1.09 | 0.02 | 2.90 | -0.31 | BC 27 |
| | | | | Min $M_y$ | -0.05 | -0.07 | -0.64 | 0.02 | 1.70 | -0.16 | BC 380 |
| | | | | Max $M_z$ | 1.44 | -0.04 | -0.65 | -0.00 | 1.72 | -0.10 | BC 389 |
| | | | | Min $M_z$ | 0.01 | -0.21 | -0.98 | 0.03 | 2.59 | -0.48 | BC 154 |
| | | 152 | 2250 | Max N | 1.48 | -0.05 | -0.89 | 0.01 | 0.00 | 0.00 | BC 413 |
| | | | | Min N | -5.77 | -0.08 | -0.89 | 0.01 | 0.00 | -0.00 | BC 355 |
| | | | | Max $V_y$ | 1.44 | -0.04 | -0.88 | -0.00 | 0.00 | 0.00 | BC 389 |
| | | | | Min $V_y$ | 0.01 | -0.21 | -1.32 | 0.03 | 0.00 | 0.00 | BC 154 |
| | | | | Max $V_z$ | -0.05 | -0.07 | -0.87 | 0.02 | 0.00 | -0.00 | BC 380 |
| | | | | Min $V_z$ | 0.05 | -0.14 | -1.49 | 0.02 | 0.00 | 0.00 | BC 27 |
| | | | | Max $M_T$ | 0.01 | -0.21 | -1.32 | 0.03 | 0.00 | 0.00 | BC 154 |
| | | | | Min $M_T$ | 1.44 | -0.04 | -0.88 | -0.00 | 0.00 | 0.00 | BC 389 |
| | | | | Max $M_y$ | -5.38 | -0.10 | -1.30 | 0.01 | 0.00 | -0.00 | BC 259 |
| | | | | Min $M_y$ | -0.29 | -0.13 | -1.29 | 0.01 | -0.00 | 0.00 | BC 200 |
| | | | | Max $M_z$ | -0.30 | -0.13 | -1.29 | 0.01 | -0.00 | 0.00 | BC 172 |
| | | | | Min $M_z$ | -5.38 | -0.10 | -1.30 | 0.01 | 0.00 | -0.00 | BC 259 |
| 235 | RC1 | 33 | 0 | Max N | 52.60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min N | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 172 |
| | | | | Max $V_u$ | 0.48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 0.48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 0.48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 0.48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 0.48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 0.48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 0.48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 0.48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 42 | 3901 | Max N | 52.61 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min N | -0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 172 |
| | | | | Max $V_u$ | 0.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 0.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 0.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 0.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 0.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 0.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 0.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 0.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 236 | RC1 | 33 | 0 | Max N | 45.56 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 168 |
| | | | | Min N | -0.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 445 |
| | | | | Max $V_u$ | 2.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 2.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 2.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 2.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 2.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 2.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 2.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 2.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 2.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 2.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 67 | 3901 | Max N | 45.57 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 168 |
| | | | | Min N | -0.96 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 445 |
| | | | | Max $V_u$ | 2.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 2.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 2.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 2.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 2.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 2.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 2.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 2.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 2.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 2.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 237 | RC1 | 33 | 0 | Max N | 0.22 | -0.05 | -0.63 | 0.12 | 1.60 | -0.11 | BC 357 |
| | | | | Min N | -0.24 | -0.03 | -0.67 | 0.12 | 1.69 | -0.07 | BC 447 |
| | | | | Max $V_y$ | -0.24 | -0.03 | -0.67 | 0.12 | 1.69 | -0.07 | BC 447 |
| | | | | Min $V_y$ | 0.04 | -0.12 | -0.95 | 0.48 | 2.39 | -0.26 | BC 138 |
| | | | | Max $V_z$ | 0.21 | -0.05 | -0.63 | 0.11 | 1.60 | -0.11 | BC 413 |
| | | | | Min $V_z$ | 0.04 | -0.08 | -1.07 | 0.28 | 2.71 | -0.18 | BC 4 |
| | | | | Max $M_T$ | 0.04 | -0.12 | -0.95 | 0.48 | 2.39 | -0.26 | BC 153 |
| | | | | Min $M_T$ | 0.21 | -0.05 | -0.63 | 0.11 | 1.60 | -0.11 | BC 381 |
| | | | | Max $M_y$ | 0.04 | -0.08 | -1.07 | 0.28 | 2.71 | -0.18 | BC 4 |
| | | | | Min $M_y$ | 0.21 | -0.05 | -0.63 | 0.11 | 1.60 | -0.11 | BC 413 |
| | | | | Max $M_z$ | -0.24 | -0.03 | -0.67 | 0.12 | 1.69 | -0.07 | BC 447 |
| | | | | Min $M_z$ | 0.04 | -0.12 | -0.95 | 0.48 | 2.39 | -0.26 | BC 138 |
| | | 151 | 2150 | Max N | 0.22 | -0.05 | -0.86 | 0.12 | -0.00 | 0.00 | BC 357 |
| | | | | Min N | -0.24 | -0.03 | -0.90 | 0.12 | 0.00 | 0.00 | BC 447 |
| | | | | Max $V_y$ | -0.24 | -0.03 | -0.90 | 0.12 | 0.00 | 0.00 | BC 447 |
| | | | | Min $V_y$ | 0.04 | -0.12 | -1.28 | 0.48 | 0.00 | 0.00 | BC 138 |
| | | | | Max $V_z$ | 0.21 | -0.05 | -0.86 | 0.11 | 0.00 | 0.00 | BC 413 |
| | | | | Min $V_z$ | 0.04 | -0.08 | -1.45 | 0.28 | 0.00 | 0.00 | BC 4 |
| | | | | Max $M_T$ | 0.04 | -0.12 | -1.28 | 0.48 | 0.00 | 0.00 | BC 153 |
| | | | | Min $M_T$ | 0.21 | -0.05 | -0.86 | 0.11 | 0.00 | 0.00 | BC 381 |
| | | | | Max $M_y$ | 0.02 | -0.06 | -1.27 | 0.18 | 0.00 | 0.00 | BC 160 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 237 | RC1 | | | Min $M_y$ | -0.20 | -0.07 | -1.31 | 0.17 | -0.00 | 0.00 | BC 287 |
| | | | | Max $M_z$ | 0.03 | -0.07 | -1.44 | 0.20 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.02 | -0.08 | -1.27 | 0.26 | 0.00 | -0.00 | BC 172 |
| 238 | RC1 | 38 | 0 | Max N | 57.81 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 146 |
| | | | | Min N | -0.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 414 |
| | | | | Max $V_u$ | 25.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 25.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 25.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 25.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 25.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 25.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 25.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 25.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 25.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 25.71 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 61 | 3967 | Max N | 57.78 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 146 |
| | | | | Min N | -0.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 414 |
| | | | | Max $V_u$ | 25.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 25.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 25.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 25.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 25.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 25.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 25.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 25.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 25.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 25.67 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 239 | RC1 | 38 | 0 | Max N | 60.39 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 139 |
| | | | | Min N | -0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 451 |
| | | | | Max $V_u$ | 25.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 25.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 25.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 25.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 25.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 25.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 25.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 25.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 25.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 25.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 37 | 3967 | Max N | 60.36 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 139 |
| | | | | Min N | -0.44 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 451 |
| | | | | Max $V_u$ | 25.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 25.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 25.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 25.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 25.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 25.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 25.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 25.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 25.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 25.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 240 | RC1 | 38 | 0 | Max N | 1.19 | -0.02 | -0.65 | 0.00 | 1.74 | -0.05 | BC 408 |
| | | | | Min N | -2.31 | -0.26 | -0.96 | -0.01 | 2.54 | -0.59 | BC 149 |
| | | | | Max $V_y$ | -1.02 | -0.02 | -0.65 | -0.01 | 1.73 | -0.04 | BC 446 |
| | | | | Min $V_y$ | -2.29 | -0.26 | -0.96 | -0.01 | 2.54 | -0.59 | BC 138 |
| | | | | Max $V_z$ | -1.03 | -0.02 | -0.65 | -0.01 | 1.73 | -0.04 | BC 450 |
| | | | | Min $V_z$ | -1.31 | -0.13 | -1.08 | -0.01 | 2.87 | -0.29 | BC 12 |
| | | | | Max $M_T$ | -0.53 | -0.02 | -0.65 | 0.00 | 1.73 | -0.05 | BC 363 |
| | | | | Min $M_T$ | -1.16 | -0.08 | -0.95 | -0.01 | 2.54 | -0.19 | BC 270 |
| | | | | Max $M_y$ | -1.31 | -0.13 | -1.08 | -0.01 | 2.87 | -0.29 | BC 12 |
| | | | | Min $M_y$ | -1.03 | -0.02 | -0.65 | -0.01 | 1.73 | -0.04 | BC 450 |
| | | | | Max $M_z$ | -1.02 | -0.02 | -0.65 | -0.01 | 1.73 | -0.04 | BC 446 |
| | | | | Min $M_z$ | -2.29 | -0.26 | -0.96 | -0.01 | 2.54 | -0.59 | BC 138 |
| | | 161 | 2250 | Max N | 1.19 | -0.02 | -0.89 | 0.00 | 0.00 | 0.00 | BC 408 |
| | | | | Min N | -2.31 | -0.26 | -1.30 | -0.01 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_y$ | -1.02 | -0.02 | -0.89 | -0.01 | 0.00 | 0.00 | BC 446 |
| | | | | Min $V_y$ | -2.29 | -0.26 | -1.30 | -0.01 | 0.00 | 0.00 | BC 138 |
| | | | | Max $V_z$ | -1.03 | -0.02 | -0.89 | -0.01 | 0.00 | 0.00 | BC 450 |
| | | | | Min $V_z$ | -1.31 | -0.13 | -1.47 | -0.01 | 0.00 | 0.00 | BC 12 |
| | | | | Max $M_T$ | -0.53 | -0.02 | -0.89 | 0.00 | 0.00 | 0.00 | BC 363 |
| | | | | Min $M_T$ | -1.16 | -0.08 | -1.30 | -0.01 | -0.00 | 0.00 | BC 270 |
| | | | | Max $M_y$ | -1.09 | -0.04 | -1.30 | -0.01 | 0.00 | -0.00 | BC 198 |
| | | | | Min $M_y$ | -1.16 | -0.08 | -1.30 | -0.01 | -0.00 | 0.00 | BC 182 |
| | | | | Max $M_z$ | -1.16 | -0.08 | -1.30 | -0.01 | -0.00 | 0.00 | BC 182 |
| | | | | Min $M_z$ | -1.09 | -0.04 | -1.30 | -0.01 | 0.00 | -0.00 | BC 198 |
| 241 | RC1 | 164 | 0 | Max N | 33.10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 447 |
| | | | | Min N | -0.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 362 |
| | | | | Max $V_u$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 241 | RC1 | 65 | 3967 | Max N | 33.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 447 |
| | | | | Min N | -0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 362 |
| | | | | Max $V_u$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | -0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 242 | RC1 | 164 | 0 | Max N | 34.92 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 358 |
| | | | | Min N | -0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 475 |
| | | | | Max $V_u$ | 0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 63 | 3967 | Max N | 34.90 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 358 |
| | | | | Min N | -0.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 475 |
| | | | | Max $V_u$ | 0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_u$ | 0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_v$ | 0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_v$ | 0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_u$ | 0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_u$ | 0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_v$ | 0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_v$ | 0.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 243 | RC1 | 164 | 0 | Max N | -0.01 | 0.03 | -0.65 | 0.00 | 1.73 | 0.07 | BC 57 |
| | | | | Min N | -0.11 | 0.05 | -0.95 | 0.01 | 2.53 | 0.11 | BC 234 |
| | | | | Max $V_y$ | -0.05 | 0.05 | -1.07 | 0.00 | 2.86 | 0.11 | BC 18 |
| | | | | Min $V_y$ | -0.11 | 0.02 | -0.65 | -0.02 | 1.72 | 0.05 | BC 461 |
| | | | | Max $V_z$ | -0.04 | 0.04 | -0.65 | -0.03 | 1.72 | 0.08 | BC 460 |
| | | | | Min $V_z$ | -0.03 | 0.05 | -1.07 | -0.02 | 2.86 | 0.11 | BC 9 |
| | | | | Max $M_T$ | -0.10 | 0.05 | -0.95 | 0.01 | 2.53 | 0.11 | BC 198 |
| | | | | Min $M_T$ | -0.05 | 0.05 | -0.95 | -0.03 | 2.53 | 0.10 | BC 267 |
| | | | | Max $M_y$ | -0.03 | 0.05 | -1.07 | -0.02 | 2.86 | 0.11 | BC 9 |
| | | | | Min $M_y$ | -0.04 | 0.04 | -0.65 | -0.03 | 1.72 | 0.08 | BC 460 |
| | | | | Max $M_z$ | -0.05 | 0.05 | -1.07 | 0.00 | 2.86 | 0.11 | BC 18 |
| | | | | Min $M_z$ | -0.11 | 0.02 | -0.65 | -0.02 | 1.72 | 0.05 | BC 461 |
| | | 158 | 2250 | Max N | -0.01 | 0.03 | -0.89 | 0.00 | 0.00 | 0.00 | BC 57 |
| | | | | Min N | -0.11 | 0.05 | -1.30 | 0.01 | 0.00 | 0.00 | BC 234 |
| | | | | Max $V_y$ | -0.05 | 0.05 | -1.47 | 0.00 | 0.00 | 0.00 | BC 18 |
| | | | | Min $V_y$ | -0.11 | 0.02 | -0.89 | -0.02 | 0.00 | 0.00 | BC 461 |
| | | | | Max $V_z$ | -0.04 | 0.04 | -0.88 | -0.03 | 0.00 | 0.00 | BC 460 |
| | | | | Min $V_z$ | -0.03 | 0.05 | -1.47 | -0.02 | 0.00 | 0.00 | BC 9 |
| | | | | Max $M_T$ | -0.10 | 0.05 | -1.30 | 0.01 | 0.00 | 0.00 | BC 198 |
| | | | | Min $M_T$ | -0.05 | 0.05 | -1.30 | -0.03 | 0.00 | 0.00 | BC 267 |
| | | | | Max $M_y$ | -0.04 | 0.04 | -1.30 | -0.02 | 0.00 | 0.00 | BC 91 |
| | | | | Min $M_y$ | -0.07 | 0.03 | -0.89 | 0.01 | -0.00 | 0.00 | BC 361 |
| | | | | Max $M_z$ | -0.05 | 0.05 | -1.47 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.05 | 0.05 | -1.47 | -0.00 | 0.00 | 0.00 | BC 1 |

## 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | **Doorgaande staven No. 1: Doorgaande staven 1** | | | | | | | | | | |
| 5 | RC1 | 5 | 0 | Max N | ▷ -23.57 | -5.01 | -4.95 | 0.00 | 0.00 | 0.00 | BC 422 |
| | | | Links | Min N | ▷ -56.15 | 0.05 | 0.20 | -0.00 | 0.00 | 0.00 | BC 133 |
| | | | | Max $V_y$ | -40.37 | ▷ 6.88 | 3.81 | -0.00 | 0.00 | 0.00 | BC 236 |
| | | | | Min $V_y$ | -23.57 | ▷ -5.03 | -4.90 | 0.00 | 0.00 | 0.00 | BC 414 |
| | | | | Max $V_z$ | -40.37 | 6.88 | ▷ 3.81 | -0.00 | 0.00 | 0.00 | BC 240 |
| | | | | Min $V_z$ | -23.57 | -5.01 | ▷ -4.96 | 0.00 | 0.00 | 0.00 | BC 390 |
| | | | | Max $M_T$ | -23.57 | -5.03 | -4.89 | ▷ 0.00 | 0.00 | 0.00 | BC 474 |
| | | | | Min $M_T$ | -40.37 | 6.85 | 3.73 | ▷ -0.00 | 0.00 | 0.00 | BC 200 |
| | | | | Max $M_y$ | -29.22 | -5.02 | -4.89 | 0.00 | ▷ 0.00 | 0.00 | BC 374 |
| | | | | Min $M_y$ | -34.64 | 3.09 | -2.00 | -0.00 | ▷ -0.00 | 0.00 | BC 163 |
| | | | | Max $M_z$ | -40.32 | 0.01 | 0.15 | -0.00 | 0.00 | ▷ 0.00 | BC 91 |
| | | | | Min $M_z$ | -29.34 | 6.86 | 3.77 | -0.00 | 0.00 | ▷ -0.00 | BC 428 |
| | | | 0 | Max N | ▷ -23.57 | -5.01 | -4.95 | 0.00 | -0.00 | 0.00 | BC 422 |
| | | | Rechts | Min N | ▷ -56.15 | 0.05 | 0.20 | -0.00 | 0.00 | -0.00 | BC 133 |
| | | | | Max $V_y$ | -40.37 | ▷ 6.88 | 3.81 | -0.00 | 0.00 | -0.00 | BC 236 |
| | | | | Min $V_y$ | -23.57 | ▷ -5.03 | -4.90 | 0.00 | -0.00 | 0.00 | BC 414 |
| | | | | Max $V_z$ | -40.37 | 6.88 | ▷ 3.81 | -0.00 | 0.00 | -0.00 | BC 240 |
| | | | | Min $V_z$ | -23.57 | -5.01 | ▷ -4.96 | 0.00 | -0.00 | 0.00 | BC 390 |
| | | | | Max $M_T$ | -23.57 | -5.03 | -4.89 | ▷ 0.00 | -0.00 | 0.00 | BC 474 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 5 | RC1 | | | Min $M_T$ | -40.37 | 6.85 | 3.73 | ▷ -0.00 | 0.00 | -0.00 | BC 200 |
| | | | | Max $M_y$ | -40.37 | 6.88 | 3.81 | -0.00 | ▷ 0.00 | -0.00 | BC 240 |
| | | | | Min $M_y$ | -23.57 | -5.01 | -4.96 | 0.00 | ▷ -0.00 | 0.00 | BC 390 |
| | | | | Max $M_z$ | -34.60 | -5.03 | -4.86 | 0.00 | -0.00 | ▷ 0.00 | BC 218 |
| | | | | Min $M_z$ | -40.37 | 6.88 | 3.81 | -0.00 | 0.00 | ▷ -0.00 | BC 236 |
| | | | 2500 | Max N | ▷ -21.57 | 2.03 | 2.00 | 0.00 | -3.68 | 3.72 | BC 422 |
| | | | Links | Min N | ▷ -53.23 | 0.05 | 0.20 | -0.00 | 0.50 | -0.12 | BC 133 |
| | | | | Max $V_y$ | -37.33 | ▷ 2.04 | 2.04 | 0.00 | -3.58 | 3.69 | BC 234 |
| | | | | Min $V_y$ | -21.69 | ▷ -2.94 | -0.96 | -0.00 | 3.49 | -4.87 | BC 412 |
| | | | | Max $V_z$ | -31.67 | 2.00 | ▷ 2.10 | 0.00 | -3.43 | 3.78 | BC 278 |
| | | | | Min $V_z$ | -21.69 | -2.93 | ▷ -1.02 | -0.00 | 3.33 | -4.89 | BC 356 |
| | | | | Max $M_T$ | -21.57 | 2.00 | 2.06 | ▷ 0.00 | -3.53 | 3.79 | BC 474 |
| | | | | Min $M_T$ | -37.45 | -2.93 | -0.97 | ▷ -0.00 | 3.45 | -4.90 | BC 200 |
| | | | | Max $M_y$ | -37.45 | -2.90 | -0.90 | -0.00 | ▷ 3.64 | -4.98 | BC 240 |
| | | | | Min $M_y$ | -21.57 | 2.03 | 1.99 | 0.00 | ▷ -3.71 | 3.73 | BC 390 |
| | | | | Max $M_z$ | -21.57 | 2.00 | 2.06 | 0.00 | -3.55 | ▷ 3.79 | BC 414 |
| | | | | Min $M_z$ | -37.45 | -2.90 | -0.90 | -0.00 | 3.64 | ▷ -4.98 | BC 236 |
| | | | 2500 | Max N | ▷ -21.57 | 2.03 | 2.00 | 0.00 | -3.68 | 3.72 | BC 422 |
| | | | Rechts | Min N | ▷ -53.23 | 0.05 | 0.20 | -0.00 | 0.50 | -0.12 | BC 133 |
| | | | | Max $V_y$ | -37.33 | ▷ 2.04 | 2.05 | 0.00 | -3.58 | 3.69 | BC 234 |
| | | | | Min $V_y$ | -21.69 | ▷ -2.94 | -0.96 | -0.00 | 3.49 | -4.87 | BC 412 |
| | | | | Max $V_z$ | -31.67 | 2.00 | ▷ 2.10 | 0.00 | -3.43 | 3.78 | BC 278 |
| | | | | Min $V_z$ | -21.69 | -2.93 | ▷ -1.02 | -0.00 | 3.33 | -4.89 | BC 356 |
| | | | | Max $M_T$ | -21.57 | 2.00 | 2.06 | ▷ 0.00 | -3.53 | 3.79 | BC 474 |
| | | | | Min $M_T$ | -37.45 | -2.93 | -0.97 | ▷ -0.00 | 3.45 | -4.90 | BC 200 |
| | | | | Max $M_y$ | -37.45 | -2.90 | -0.90 | -0.00 | ▷ 3.64 | -4.98 | BC 240 |
| | | | | Min $M_y$ | -21.57 | 2.03 | 1.99 | 0.00 | ▷ -3.71 | 3.73 | BC 390 |
| | | | | Max $M_z$ | -21.57 | 2.00 | 2.06 | 0.00 | -3.55 | ▷ 3.79 | BC 414 |
| | | | | Min $M_z$ | -37.45 | -2.90 | -0.90 | -0.00 | 3.64 | ▷ -4.98 | BC 236 |
| | | | 4345 | Max N | ▷ -17.43 | 7.22 | 7.13 | 0.00 | 4.74 | -4.81 | BC 422 |
| | | | Links | Min N | ▷ -47.15 | 0.05 | 0.20 | -0.00 | 0.87 | -0.20 | BC 133 |
| | | | | Max $V_y$ | -31.25 | ▷ 7.23 | 7.17 | 0.00 | 4.93 | -4.86 | BC 234 |
| | | | | Min $V_y$ | -17.55 | ▷ -10.16 | -4.43 | -0.00 | -1.48 | 7.22 | BC 412 |
| | | | | Max $V_z$ | -25.60 | 7.20 | ▷ 7.23 | 0.00 | 5.18 | -4.70 | BC 278 |
| | | | | Min $V_z$ | -17.55 | -10.15 | ▷ -4.49 | -0.00 | -1.76 | 7.18 | BC 356 |
| | | | | Max $M_T$ | -17.43 | 7.19 | 7.19 | ▷ 0.00 | 5.01 | -4.70 | BC 474 |
| | | | | Min $M_T$ | -31.37 | -10.14 | -4.44 | ▷ -0.00 | -1.54 | 7.15 | BC 200 |
| | | | | Max $M_y$ | -25.60 | 7.20 | 7.23 | 0.00 | ▷ 5.18 | -4.70 | BC 278 |
| | | | | Min $M_y$ | -17.55 | -10.15 | -4.49 | -0.00 | ▷ -1.76 | 7.18 | BC 356 |
| | | | | Max $M_z$ | -17.55 | -10.16 | -4.43 | -0.00 | -1.48 | ▷ 7.22 | BC 412 |
| | | | | Min $M_z$ | -31.25 | 7.23 | 7.17 | 0.00 | 4.93 | ▷ -4.86 | BC 234 |
| | | 9 | 4345 | Max N | ▷ -17.43 | 7.22 | 7.13 | 0.00 | 4.74 | -4.81 | BC 422 |
| | | | Rechts | Min N | ▷ -47.15 | 0.05 | 0.20 | -0.00 | 0.87 | -0.20 | BC 133 |
| | | | | Max $V_y$ | -31.25 | ▷ 7.23 | 7.17 | 0.00 | 4.93 | -4.86 | BC 234 |
| | | | | Min $V_y$ | -17.55 | ▷ -10.16 | -4.43 | -0.00 | -1.48 | 7.22 | BC 412 |
| | | | | Max $V_z$ | -25.60 | 7.20 | ▷ 7.23 | 0.00 | 5.18 | -4.70 | BC 278 |
| | | | | Min $V_z$ | -17.55 | -10.15 | ▷ -4.49 | -0.00 | -1.76 | 7.18 | BC 356 |
| | | | | Max $M_T$ | -17.43 | 7.19 | 7.19 | ▷ 0.00 | 5.01 | -4.70 | BC 474 |
| | | | | Min $M_T$ | -31.37 | -10.14 | -4.44 | ▷ -0.00 | -1.54 | 7.15 | BC 200 |
| | | | | Max $M_y$ | -25.60 | 7.20 | 7.23 | 0.00 | ▷ 5.18 | -4.70 | BC 278 |
| | | | | Min $M_y$ | -17.55 | -10.15 | -4.49 | -0.00 | ▷ -1.76 | 7.18 | BC 356 |
| | | | | Max $M_z$ | -17.55 | -10.16 | -4.43 | -0.00 | -1.48 | ▷ 7.22 | BC 412 |
| | | | | Min $M_z$ | -31.25 | 7.23 | 7.17 | 0.00 | 4.93 | ▷ -4.86 | BC 234 |
| | | 9 | 4345 | Max N | ▷ -17.43 | 7.22 | 7.13 | 0.00 | 4.74 | -4.81 | BC 422 |
| | | 5 | 0 | Min N | ▷ -56.15 | 0.05 | 0.20 | -0.00 | 0.00 | 0.00 | BC 133 |
| | | 9 | 4345 | Max $V_y$ | -31.25 | ▷ 7.23 | 7.17 | 0.00 | 4.93 | -4.86 | BC 234 |
| | | 9 | 4345 | Min $V_y$ | -17.55 | ▷ -10.16 | -4.43 | -0.00 | -1.48 | 7.22 | BC 412 |
| | | 9 | 4345 | Max $V_z$ | -25.60 | 7.20 | ▷ 7.23 | 0.00 | 5.18 | -4.70 | BC 278 |
| | | 5 | 0 | Min $V_z$ | -23.57 | -5.01 | ▷ -4.96 | 0.00 | 0.00 | 0.00 | BC 390 |
| | | | 2500 | Max $M_T$ | -21.57 | 2.00 | 2.06 | ▷ 0.00 | -3.53 | 3.79 | BC 474 |
| | | | 2500 | Min $M_T$ | -37.45 | -2.93 | -0.97 | ▷ -0.00 | 3.45 | -4.90 | BC 200 |
| | | 9 | 4345 | Max $M_y$ | -25.60 | 7.20 | 7.23 | 0.00 | ▷ 5.18 | -4.70 | BC 278 |
| | | | 1731 | Min $M_y$ | -22.19 | -0.14 | -0.15 | 0.00 | ▷ -4.42 | 4.45 | BC 390 |
| | | 9 | 4345 | Max $M_z$ | -17.55 | -10.16 | -4.43 | -0.00 | -1.48 | ▷ 7.22 | BC 412 |
| | | | 1731 | Min $M_z$ | -38.35 | 0.11 | 0.55 | -0.00 | 3.77 | ▷ -6.05 | BC 236 |
| 150 | RC1 | 9 | 0 | Max N | ▷ -15.72 | -6.21 | -6.11 | 0.00 | 4.74 | -4.81 | BC 422 |
| | | | Links | Min N | ▷ -44.64 | -0.06 | -0.28 | -0.00 | 0.87 | -0.20 | BC 133 |
| | | | | Max $V_y$ | -15.84 | ▷ 8.78 | 3.62 | -0.00 | -1.48 | 7.22 | BC 412 |
| | | | | Min $V_y$ | -28.74 | ▷ -6.22 | -6.17 | 0.00 | 4.93 | -4.86 | BC 234 |
| | | | | Max $V_z$ | -15.84 | 8.77 | ▷ 3.70 | -0.00 | -1.76 | 7.18 | BC 356 |
| | | | | Min $V_z$ | -28.74 | -6.19 | ▷ -6.25 | 0.00 | 5.18 | -4.75 | BC 266 |
| | | | | Max $M_T$ | -15.72 | -6.18 | -6.19 | ▷ 0.00 | 5.01 | -4.70 | BC 474 |
| | | | | Min $M_T$ | -28.86 | 8.76 | 3.63 | ▷ -0.00 | -1.54 | 7.15 | BC 200 |
| | | | | Max $M_y$ | -23.09 | -6.18 | -6.25 | 0.00 | ▷ 5.18 | -4.70 | BC 278 |
| | | | | Min $M_y$ | -15.84 | 8.77 | 3.70 | -0.00 | ▷ -1.76 | 7.18 | BC 356 |
| | | | | Max $M_z$ | -15.84 | 8.78 | 3.62 | -0.00 | -1.48 | ▷ 7.22 | BC 412 |
| | | | | Min $M_z$ | -28.74 | -6.22 | -6.17 | 0.00 | 4.93 | ▷ -4.86 | BC 234 |
| | | | 0 | Max N | ▷ -15.72 | -6.21 | -6.11 | 0.00 | 4.74 | -4.81 | BC 422 |
| | | | Rechts | Min N | ▷ -44.64 | -0.06 | -0.28 | -0.00 | 0.87 | -0.20 | BC 133 |
| | | | | Max $V_y$ | -15.84 | ▷ 8.78 | 3.62 | -0.00 | -1.48 | 7.22 | BC 412 |
| | | | | Min $V_y$ | -28.74 | ▷ -6.22 | -6.17 | 0.00 | 4.93 | -4.86 | BC 234 |
| | | | | Max $V_z$ | -15.84 | 8.77 | ▷ 3.70 | -0.00 | -1.76 | 7.18 | BC 356 |
| | | | | Min $V_z$ | -28.74 | -6.19 | ▷ -6.25 | 0.00 | 5.18 | -4.75 | BC 266 |
| | | | | Max $M_T$ | -15.72 | -6.18 | -6.19 | ▷ 0.00 | 5.01 | -4.70 | BC 474 |
| | | | | Min $M_T$ | -28.86 | 8.76 | 3.63 | ▷ -0.00 | -1.54 | 7.15 | BC 200 |
| | | | | Max $M_y$ | -23.09 | -6.18 | -6.25 | 0.00 | ▷ 5.18 | -4.70 | BC 278 |
| | | | | Min $M_y$ | -15.84 | 8.77 | 3.70 | -0.00 | ▷ -1.76 | 7.18 | BC 356 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 150 | RC1 | | | Max $M_z$ | -15.84 | 8.78 | 3.62 | -0.00 | -1.48 | ▷ 7.22 | BC 412 |
| | | | | Min $M_z$ | -28.74 | -6.22 | -6.17 | 0.00 | 4.93 | ▷ -4.86 | BC 234 |
| | | | 3505 | Max N | ▷ -7.83 | 3.65 | 3.63 | 0.00 | 0.39 | -0.33 | BC 422 |
| | | | Links | Min N | ▷ -33.07 | -0.06 | -0.28 | -0.00 | -0.10 | 0.01 | BC 133 |
| | | | | Max $V_y$ | -7.83 | ▷ 3.69 | 3.56 | 0.00 | 0.38 | -0.33 | BC 414 |
| | | | | Min $V_y$ | -17.29 | ▷ -4.98 | -3.06 | -0.00 | -0.38 | 0.46 | BC 236 |
| | | | | Max $V_z$ | -7.83 | 3.66 | ▷ 3.64 | 0.00 | 0.39 | -0.33 | BC 390 |
| | | | | Min $V_z$ | -17.29 | -4.98 | ▷ -3.06 | -0.00 | -0.38 | 0.46 | BC 240 |
| | | | | Max $M_T$ | -7.83 | 3.69 | 3.55 | ▷ 0.00 | 0.38 | -0.33 | BC 474 |
| | | | | Min $M_T$ | -17.29 | -4.94 | -2.96 | ▷ -0.00 | -0.37 | 0.45 | BC 200 |
| | | | | Max $M_y$ | -7.83 | 3.66 | 3.64 | 0.00 | ▷ 0.39 | -0.33 | BC 390 |
| | | | | Min $M_y$ | -17.29 | -4.98 | -3.06 | -0.00 | ▷ -0.38 | 0.46 | BC 240 |
| | | | | Max $M_z$ | -17.29 | -4.98 | -3.06 | -0.00 | -0.38 | ▷ 0.46 | BC 236 |
| | | | | Min $M_z$ | -7.83 | 3.69 | 3.56 | 0.00 | 0.38 | ▷ -0.33 | BC 414 |
| | | 45 | 3505 | Max N | ▷ -7.83 | 3.65 | 3.63 | 0.00 | 0.39 | -0.33 | BC 422 |
| | | | Rechts | Min N | ▷ -33.07 | -0.06 | -0.28 | -0.00 | -0.10 | 0.01 | BC 133 |
| | | | | Max $V_y$ | -7.83 | ▷ 3.69 | 3.56 | 0.00 | 0.38 | -0.33 | BC 414 |
| | | | | Min $V_y$ | -17.29 | ▷ -4.98 | -3.06 | -0.00 | -0.38 | 0.46 | BC 236 |
| | | | | Max $V_z$ | -7.83 | 3.66 | ▷ 3.64 | 0.00 | 0.39 | -0.33 | BC 390 |
| | | | | Min $V_z$ | -17.29 | -4.98 | ▷ -3.06 | -0.00 | -0.38 | 0.46 | BC 240 |
| | | | | Max $M_T$ | -7.83 | 3.69 | 3.55 | ▷ 0.00 | 0.38 | -0.33 | BC 474 |
| | | | | Min $M_T$ | -17.29 | -4.94 | -2.96 | ▷ -0.00 | -0.37 | 0.45 | BC 200 |
| | | | | Max $M_y$ | -7.83 | 3.66 | 3.64 | 0.00 | ▷ 0.39 | -0.33 | BC 390 |
| | | | | Min $M_y$ | -17.29 | -4.98 | -3.06 | -0.00 | ▷ -0.38 | 0.46 | BC 240 |
| | | | | Max $M_z$ | -17.29 | -4.98 | -3.06 | -0.00 | -0.38 | ▷ 0.46 | BC 236 |
| | | | | Min $M_z$ | -7.83 | 3.69 | 3.56 | 0.00 | 0.38 | ▷ -0.33 | BC 414 |
| | | 45 | 3505 | Max N | ▷ -7.83 | 3.65 | 3.63 | 0.00 | 0.39 | -0.33 | BC 422 |
| | | 9 | 0 | Min N | ▷ -44.64 | -0.06 | -0.28 | -0.00 | 0.87 | -0.20 | BC 133 |
| | | 9 | 0 | Max $V_y$ | -15.84 | ▷ 8.78 | 3.62 | -0.00 | -1.48 | 7.22 | BC 412 |
| | | 9 | 0 | Min $V_y$ | -28.74 | ▷ -6.22 | -6.17 | 0.00 | 4.93 | -4.86 | BC 234 |
| | | 9 | 0 | Max $V_z$ | -15.84 | 8.77 | ▷ 3.70 | -0.00 | -1.76 | 7.18 | BC 356 |
| | | 9 | 0 | Min $V_z$ | -28.74 | -6.19 | ▷ -6.25 | 0.00 | 5.18 | -4.75 | BC 266 |
| | | 9 | 0 | Max $M_T$ | -15.72 | -6.18 | -6.19 | ▷ 0.00 | 5.01 | -4.70 | BC 474 |
| | | 9 | 0 | Min $M_T$ | -28.86 | 8.76 | 3.63 | ▷ -0.00 | -1.54 | 7.15 | BC 200 |
| | | 9 | 0 | Max $M_y$ | -23.09 | -6.18 | -6.25 | 0.00 | ▷ 5.18 | -4.70 | BC 278 |
| | | | 2142 | Min $M_y$ | -10.90 | -0.18 | -0.15 | 0.00 | ▷ -1.99 | 2.04 | BC 390 |
| | | 9 | 0 | Max $M_z$ | -15.84 | 8.78 | 3.62 | -0.00 | -1.48 | ▷ 7.22 | BC 412 |
| | | 9 | 0 | Min $M_z$ | -28.74 | -6.22 | -6.17 | 0.00 | 4.93 | ▷ -4.86 | BC 234 |
| 150 | RC1 | 45 | 3505 | MAX N | ▷ -7.83 | 3.65 | 3.63 | 0.00 | 0.39 | -0.33 | BC 422 |
| 5 | RC1 | 5 | 0 | MIN N | ▷ -56.15 | 0.05 | 0.20 | 0.00 | 0.00 | 0.00 | BC 133 |
| 150 | RC1 | 9 | 0 | MAX $V_y$ | -15.84 | ▷ 8.78 | 3.62 | 0.00 | -1.48 | 7.22 | BC 412 |
| 5 | RC1 | 9 | 4345 | MIN $V_y$ | -17.55 | ▷ -10.16 | -4.43 | 0.00 | -1.48 | 7.22 | BC 412 |
| 5 | RC1 | 9 | 4345 | MAX $V_z$ | -25.60 | 7.20 | ▷ 7.23 | 0.00 | 5.18 | -4.70 | BC 278 |
| 150 | RC1 | 9 | 0 | MIN $V_z$ | -28.74 | -6.19 | ▷ -6.25 | 0.00 | 5.18 | -4.75 | BC 266 |
| 5 | RC1 | | 2500 | MAX $M_T$ | -21.57 | 2.00 | 2.06 | ▷ 0.00 | -3.53 | 3.79 | BC 474 |
| 5 | RC1 | | 2500 | MIN $M_T$ | -37.45 | -2.93 | -0.97 | ▷ 0.00 | 3.45 | -4.90 | BC 200 |
| 150 | RC1 | 9 | 0 | MAX $M_y$ | -23.09 | -6.18 | -6.25 | 0.00 | ▷ 5.18 | -4.70 | BC 278 |
| 5 | RC1 | | 1731 | MIN $M_y$ | -22.19 | -0.14 | -0.15 | 0.00 | ▷ -4.42 | 4.45 | BC 390 |
| 150 | RC1 | 9 | 0 | MAX $M_z$ | -15.84 | 8.78 | 3.62 | 0.00 | -1.48 | ▷ 7.22 | BC 412 |
| 5 | RC1 | | 1731 | MIN $M_z$ | -38.35 | 0.11 | 0.55 | 0.00 | 3.77 | ▷ -6.05 | BC 236 |
| | **Doorgaande staven No. 2: Doorgaande staven 2** | | | | | | | | | | |
| 6 | RC1 | 6 | 0 | Max N | ▷ -23.80 | -5.15 | 4.97 | -0.00 | 0.00 | 0.00 | BC 358 |
| | | | | Min N | ▷ -57.03 | 0.09 | -0.18 | 0.00 | -0.00 | 0.00 | BC 155 |
| | | | | Max $V_y$ | -40.98 | ▷ 7.01 | -3.76 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min $V_y$ | -34.97 | ▷ -5.16 | 4.92 | -0.00 | 0.00 | 0.00 | BC 218 |
| | | | | Max $V_z$ | -23.80 | -5.15 | ▷ 4.97 | -0.00 | 0.00 | 0.00 | BC 358 |
| | | | | Min $V_z$ | -40.98 | 7.00 | ▷ -3.76 | 0.00 | 0.00 | 0.00 | BC 265 |
| | | | | Max $M_T$ | -40.98 | 7.01 | -3.71 | ▷ 0.00 | 0.00 | 0.00 | BC 245 |
| | | | | Min $M_T$ | -23.80 | -5.14 | 4.97 | ▷ -0.00 | 0.00 | 0.00 | BC 362 |
| | | | | Max $M_y$ | -29.57 | -5.14 | 4.90 | -0.00 | ▷ 0.00 | 0.00 | BC 374 |
| | | | | Min $M_y$ | -35.04 | 3.17 | 2.06 | 0.00 | ▷ -0.00 | 0.00 | BC 163 |
| | | | | Max $M_z$ | -40.82 | 3.90 | 1.84 | 0.00 | -0.00 | ▷ 0.00 | BC 268 |
| | | | | Min $M_z$ | -24.04 | 7.00 | -3.67 | 0.00 | 0.00 | ▷ -0.00 | BC 353 |
| | | | 2500 | Max N | ▷ -21.80 | 2.07 | -1.98 | -0.00 | 3.74 | 3.85 | BC 358 |
| | | | Links | Min N | ▷ -54.10 | 0.09 | -0.18 | 0.00 | -0.46 | -0.22 | BC 155 |
| | | | | Max $V_y$ | -27.57 | ▷ 2.09 | -2.01 | -0.00 | 3.67 | 3.79 | BC 438 |
| | | | | Min $V_y$ | -22.04 | ▷ -3.01 | 0.99 | 0.00 | -3.41 | -4.96 | BC 413 |
| | | | | Max $V_z$ | -22.04 | -2.99 | ▷ 1.04 | 0.00 | -3.29 | -5.01 | BC 417 |
| | | | | Min $V_z$ | -37.81 | 2.07 | ▷ -2.08 | -0.00 | 3.48 | 3.83 | BC 242 |
| | | | | Max $M_T$ | -38.05 | -2.98 | 0.99 | ▷ 0.00 | -3.40 | -5.04 | BC 245 |
| | | | | Min $M_T$ | -21.80 | 2.07 | -1.98 | ▷ -0.00 | 3.74 | 3.84 | BC 362 |
| | | | | Max $M_y$ | -21.80 | 2.07 | -1.98 | -0.00 | ▷ 3.74 | 3.85 | BC 358 |
| | | | | Min $M_y$ | -38.05 | -2.98 | 0.94 | 0.00 | ▷ -3.52 | -5.02 | BC 265 |
| | | | | Max $M_z$ | -32.04 | 2.05 | -2.03 | -0.00 | 3.61 | ▷ 3.89 | BC 218 |
| | | | | Min $M_z$ | -38.05 | -2.97 | 0.94 | 0.00 | -3.52 | ▷ -5.06 | BC 241 |
| | | | 2500 | Max N | ▷ -21.80 | 2.07 | -1.98 | -0.00 | 3.74 | 3.85 | BC 358 |
| | | | Rechts | Min N | ▷ -54.10 | 0.09 | -0.18 | 0.00 | -0.46 | -0.22 | BC 155 |
| | | | | Max $V_y$ | -27.57 | ▷ 2.09 | -2.01 | -0.00 | 3.67 | 3.79 | BC 438 |
| | | | | Min $V_y$ | -22.04 | ▷ -3.01 | 0.99 | 0.00 | -3.41 | -4.96 | BC 413 |
| | | | | Max $V_z$ | -22.04 | -2.99 | ▷ 1.04 | 0.00 | -3.29 | -5.01 | BC 417 |
| | | | | Min $V_z$ | -37.81 | 2.07 | ▷ -2.08 | -0.00 | 3.48 | 3.83 | BC 242 |
| | | | | Max $M_T$ | -38.05 | -2.98 | 0.99 | ▷ 0.00 | -3.40 | -5.04 | BC 245 |
| | | | | Min $M_T$ | -21.80 | 2.07 | -1.98 | ▷ -0.00 | 3.74 | 3.84 | BC 362 |
| | | | | Max $M_y$ | -21.80 | 2.07 | -1.98 | -0.00 | ▷ 3.74 | 3.85 | BC 358 |
| | | | | Min $M_y$ | -38.05 | -2.98 | 0.94 | 0.00 | ▷ -3.52 | -5.02 | BC 265 |
| | | | | Max $M_z$ | -32.04 | 2.05 | -2.03 | -0.00 | 3.61 | ▷ 3.89 | BC 218 |
| | | | | Min $M_z$ | -38.05 | -2.97 | 0.94 | 0.00 | -3.52 | ▷ -5.06 | BC 241 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 6 | RC1 | | 4345 | Max N | ▷ -17.62 | 7.39 | -7.11 | -0.00 | -4.64 | -4.88 | BC 358 |
| | | | Links | Min N | ▷ -47.98 | 0.09 | -0.18 | 0.00 | -0.79 | -0.38 | BC 154 |
| | | | | Max $V_y$ | -23.39 | ▷ 7.41 | -7.14 | -0.00 | -4.77 | -4.97 | BC 438 |
| | | | | Min $V_y$ | -17.87 | ▷ -10.38 | 4.46 | 0.00 | 1.61 | 7.39 | BC 413 |
| | | | | Max $V_z$ | -17.86 | -10.36 | ▷ 4.51 | 0.00 | 1.82 | 7.30 | BC 417 |
| | | | | Min $V_z$ | -31.68 | 7.40 | ▷ -7.21 | -0.00 | -5.10 | -4.91 | BC 242 |
| | | | | Max $M_T$ | -31.92 | -10.34 | 4.46 | ▷ 0.00 | 1.63 | 7.25 | BC 245 |
| | | | | Min $M_T$ | -17.62 | 7.40 | -7.11 | ▷ -0.00 | -4.65 | -4.90 | BC 362 |
| | | | | Max $M_y$ | -17.86 | -10.36 | 4.51 | 0.00 | ▷ 1.82 | 7.30 | BC 417 |
| | | | | Min $M_y$ | -31.68 | 7.40 | -7.21 | -0.00 | ▷ -5.10 | -4.91 | BC 242 |
| | | | | Max $M_z$ | -17.87 | -10.38 | 4.46 | 0.00 | 1.61 | ▷ 7.39 | BC 413 |
| | | | | Min $M_z$ | -23.39 | 7.41 | -7.14 | -0.00 | -4.77 | ▷ -4.97 | BC 438 |
| | | 12 | 4345 | Max N | ▷ -17.62 | 7.39 | -7.11 | -0.00 | -4.64 | -4.88 | BC 358 |
| | | | Rechts | Min N | ▷ -47.98 | 0.09 | -0.18 | 0.00 | -0.79 | -0.37 | BC 155 |
| | | | | Max $V_y$ | -23.39 | ▷ 7.41 | -7.14 | -0.00 | -4.77 | -4.97 | BC 438 |
| | | | | Min $V_y$ | -17.87 | ▷ -10.38 | 4.46 | 0.00 | 1.61 | 7.39 | BC 413 |
| | | | | Max $V_z$ | -17.86 | -10.36 | ▷ 4.51 | 0.00 | 1.82 | 7.30 | BC 417 |
| | | | | Min $V_z$ | -31.68 | 7.40 | ▷ -7.21 | -0.00 | -5.10 | -4.91 | BC 242 |
| | | | | Max $M_T$ | -31.92 | -10.34 | 4.46 | ▷ 0.00 | 1.63 | 7.25 | BC 245 |
| | | | | Min $M_T$ | -17.62 | 7.40 | -7.11 | ▷ -0.00 | -4.65 | -4.90 | BC 362 |
| | | | | Max $M_y$ | -17.86 | -10.36 | 4.51 | 0.00 | ▷ 1.82 | 7.30 | BC 417 |
| | | | | Min $M_y$ | -31.68 | 7.40 | -7.21 | -0.00 | ▷ -5.10 | -4.91 | BC 242 |
| | | | | Max $M_z$ | -17.87 | -10.38 | 4.46 | 0.00 | 1.61 | ▷ 7.39 | BC 413 |
| | | | | Min $M_z$ | -23.39 | 7.41 | -7.14 | -0.00 | -4.77 | ▷ -4.97 | BC 438 |
| | | 12 | 4345 | Max N | ▷ -17.62 | 7.39 | -7.11 | -0.00 | -4.64 | -4.88 | BC 358 |
| | | 6 | 0 | Min N | ▷ -57.03 | 0.09 | -0.18 | 0.00 | -0.00 | 0.00 | BC 155 |
| | | 12 | 4345 | Max $V_y$ | -23.39 | ▷ 7.41 | -7.14 | -0.00 | -4.77 | -4.97 | BC 438 |
| | | 12 | 4345 | Min $V_y$ | -17.87 | ▷ -10.38 | 4.46 | 0.00 | 1.61 | 7.39 | BC 413 |
| | | 6 | 0 | Max $V_z$ | -23.80 | -5.15 | ▷ 4.97 | -0.00 | 0.00 | 0.00 | BC 358 |
| | | 12 | 4345 | Min $V_z$ | -31.68 | 7.40 | ▷ -7.21 | -0.00 | -5.10 | -4.91 | BC 242 |
| | | | 2308 | Max $M_T$ | -38.28 | -2.21 | 0.63 | ▷ 0.00 | -3.56 | -5.54 | BC 245 |
| | | | 2308 | Min $M_T$ | -21.95 | 1.52 | -1.45 | ▷ -0.00 | 4.07 | 4.18 | BC 362 |
| | | | 1731 | Max $M_y$ | -22.41 | -0.15 | 0.16 | -0.00 | ▷ 4.44 | 4.59 | BC 358 |
| | | 12 | 4345 | Min $M_y$ | -31.68 | 7.40 | -7.21 | -0.00 | ▷ -5.10 | -4.91 | BC 242 |
| | | 12 | 4345 | Max $M_z$ | -17.87 | -10.38 | 4.46 | 0.00 | 1.61 | ▷ 7.39 | BC 413 |
| | | | 1731 | Min $M_z$ | -38.95 | 0.10 | -0.50 | 0.00 | -3.69 | ▷ -6.16 | BC 241 |
| 153 | RC1 | 12 | 0 | Max N | ▷ -15.89 | -6.35 | 6.09 | -0.00 | -4.64 | -4.88 | BC 358 |
| | | | Links | Min N | ▷ -45.44 | -0.11 | 0.27 | 0.00 | -0.79 | -0.37 | BC 155 |
| | | | | Max $V_y$ | -16.13 | ▷ 8.98 | -3.65 | 0.00 | 1.61 | 7.39 | BC 409 |
| | | | | Min $V_y$ | -29.14 | ▷ -6.38 | 6.17 | -0.00 | -4.89 | -4.97 | BC 246 |
| | | | | Max $V_z$ | -29.14 | -6.36 | ▷ 6.24 | -0.00 | -5.10 | -4.91 | BC 242 |
| | | | | Min $V_z$ | -16.13 | 8.95 | ▷ -3.71 | 0.00 | 1.82 | 7.30 | BC 417 |
| | | | | Max $M_T$ | -29.38 | 8.93 | -3.65 | ▷ 0.00 | 1.63 | 7.25 | BC 245 |
| | | | | Min $M_T$ | -15.89 | -6.36 | 6.09 | ▷ -0.00 | -4.65 | -4.90 | BC 362 |
| | | | | Max $M_y$ | -16.13 | 8.95 | -3.71 | 0.00 | ▷ 1.82 | 7.30 | BC 417 |
| | | | | Min $M_y$ | -29.14 | -6.36 | 6.24 | -0.00 | ▷ -5.10 | -4.91 | BC 242 |
| | | | | Max $M_z$ | -16.13 | 8.98 | -3.65 | 0.00 | 1.61 | ▷ 7.39 | BC 413 |
| | | | | Min $M_z$ | -21.66 | -6.38 | 6.13 | -0.00 | -4.77 | ▷ -4.97 | BC 438 |
| | | | 0 | Max N | ▷ -15.89 | -6.35 | 6.09 | -0.00 | -4.64 | -4.88 | BC 358 |
| | | | Rechts | Min N | ▷ -45.44 | -0.11 | 0.27 | 0.00 | -0.79 | -0.37 | BC 155 |
| | | | | Max $V_y$ | -16.13 | ▷ 8.98 | -3.65 | 0.00 | 1.61 | 7.39 | BC 409 |
| | | | | Min $V_y$ | -29.14 | ▷ -6.38 | 6.17 | -0.00 | -4.89 | -4.97 | BC 246 |
| | | | | Max $V_z$ | -29.14 | -6.36 | ▷ 6.24 | -0.00 | -5.10 | -4.91 | BC 242 |
| | | | | Min $V_z$ | -16.13 | 8.95 | ▷ -3.71 | 0.00 | 1.82 | 7.30 | BC 417 |
| | | | | Max $M_T$ | -29.38 | 8.93 | -3.65 | ▷ 0.00 | 1.63 | 7.25 | BC 245 |
| | | | | Min $M_T$ | -15.89 | -6.36 | 6.09 | ▷ -0.00 | -4.65 | -4.90 | BC 362 |
| | | | | Max $M_y$ | -16.13 | 8.95 | -3.71 | 0.00 | ▷ 1.82 | 7.30 | BC 417 |
| | | | | Min $M_y$ | -29.14 | -6.36 | 6.24 | -0.00 | ▷ -5.10 | -4.91 | BC 242 |
| | | | | Max $M_z$ | -16.13 | 8.98 | -3.65 | 0.00 | 1.61 | ▷ 7.39 | BC 413 |
| | | | | Min $M_z$ | -21.66 | -6.38 | 6.13 | -0.00 | -4.77 | ▷ -4.97 | BC 438 |
| | | | 3505 | Max N | ▷ -7.90 | 3.76 | -3.66 | -0.00 | -0.38 | -0.34 | BC 358 |
| | | | Links | Min N | ▷ -33.72 | -0.10 | 0.27 | 0.00 | 0.17 | 0.01 | BC 140 |
| | | | | Max $V_y$ | -7.90 | ▷ 3.78 | -3.60 | -0.00 | -0.37 | -0.34 | BC 410 |
| | | | | Min $V_y$ | -17.67 | ▷ -5.07 | 3.01 | 0.00 | 0.41 | 0.47 | BC 241 |
| | | | | Max $V_z$ | -17.67 | -5.05 | ▷ 3.01 | 0.00 | 0.41 | 0.47 | BC 265 |
| | | | | Min $V_z$ | -7.90 | 3.76 | ▷ -3.66 | -0.00 | -0.38 | -0.34 | BC 358 |
| | | | | Max $M_T$ | -17.67 | -5.06 | 2.95 | ▷ 0.00 | 0.41 | 0.47 | BC 245 |
| | | | | Min $M_T$ | -7.90 | 3.76 | -3.65 | ▷ -0.00 | -0.38 | -0.34 | BC 362 |
| | | | | Max $M_y$ | -17.67 | -5.05 | 3.01 | 0.00 | ▷ 0.41 | 0.47 | BC 265 |
| | | | | Min $M_y$ | -7.90 | 3.76 | -3.66 | -0.00 | ▷ -0.38 | -0.34 | BC 358 |
| | | | | Max $M_z$ | -17.67 | -5.07 | 3.01 | 0.00 | 0.41 | ▷ 0.47 | BC 241 |
| | | | | Min $M_z$ | -7.90 | 3.78 | -3.60 | -0.00 | -0.37 | ▷ -0.34 | BC 410 |
| | | 46 | 3505 | Max N | ▷ -7.90 | 3.76 | -3.66 | -0.00 | -0.38 | -0.34 | BC 358 |
| | | | Rechts | Min N | ▷ -33.72 | -0.11 | 0.27 | 0.00 | 0.17 | 0.01 | BC 155 |
| | | | | Max $V_y$ | -7.90 | ▷ 3.78 | -3.60 | -0.00 | -0.37 | -0.34 | BC 410 |
| | | | | Min $V_y$ | -17.67 | ▷ -5.07 | 3.01 | 0.00 | 0.41 | 0.47 | BC 241 |
| | | | | Max $V_z$ | -17.67 | -5.05 | ▷ 3.01 | 0.00 | 0.41 | 0.47 | BC 265 |
| | | | | Min $V_z$ | -7.90 | 3.76 | ▷ -3.66 | -0.00 | -0.38 | -0.34 | BC 358 |
| | | | | Max $M_T$ | -17.67 | -5.06 | 2.95 | ▷ 0.00 | 0.41 | 0.47 | BC 245 |
| | | | | Min $M_T$ | -7.90 | 3.76 | -3.65 | ▷ -0.00 | -0.38 | -0.34 | BC 362 |
| | | | | Max $M_y$ | -17.67 | -5.05 | 3.01 | 0.00 | ▷ 0.41 | 0.47 | BC 265 |
| | | | | Min $M_y$ | -7.90 | 3.76 | -3.66 | -0.00 | ▷ -0.38 | -0.34 | BC 358 |
| | | | | Max $M_z$ | -17.67 | -5.07 | 3.01 | 0.00 | 0.41 | ▷ 0.47 | BC 241 |
| | | | | Min $M_z$ | -7.90 | 3.78 | -3.60 | -0.00 | -0.37 | ▷ -0.34 | BC 410 |
| | | 46 | 3505 | Max N | ▷ -7.90 | 3.76 | -3.66 | -0.00 | -0.38 | -0.34 | BC 358 |
| | | 12 | 0 | Min N | ▷ -45.44 | -0.11 | 0.27 | 0.00 | -0.79 | -0.37 | BC 155 |
| | | 12 | 0 | Max $V_y$ | -16.13 | ▷ 8.98 | -3.65 | 0.00 | 1.61 | 7.39 | BC 409 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 153 | RC1 | 12 | 0 | Min $V_y$ | -29.14 | ▷ -6.38 | 6.17 | -0.00 | -4.89 | -4.97 | BC 246 |
| | | 12 | 0 | Max $V_z$ | -29.14 | ▷ -6.36 | ▷ 6.24 | -0.00 | -5.10 | -4.91 | BC 242 |
| | | 12 | 0 | Min $V_z$ | -16.13 | 8.95 | ▷ -3.71 | 0.00 | 1.82 | 7.30 | BC 417 |
| | | 12 | 0 | Max $M_T$ | -29.38 | 8.93 | -3.65 | ▷ 0.00 | 1.63 | 7.25 | BC 245 |
| | | 12 | 0 | Min $M_T$ | -15.89 | -6.36 | 6.09 | ▷ -0.00 | -4.65 | -4.90 | BC 362 |
| | | | 2142 | Max $M_y$ | -11.02 | -0.17 | 0.13 | -0.00 | ▷ 2.02 | 2.11 | BC 358 |
| | | 12 | 0 | Min $M_y$ | -29.14 | -6.36 | 6.24 | -0.00 | ▷ -5.10 | -4.91 | BC 242 |
| | | 12 | 0 | Max $M_z$ | -16.13 | 8.98 | -3.65 | 0.00 | 1.61 | ▷ 7.39 | BC 413 |
| | | 12 | 0 | Min $M_z$ | -21.66 | -6.38 | 6.13 | -0.00 | -4.77 | ▷ -4.97 | BC 438 |
| 153 | RC1 | 46 | 3505 | MAX N | ▷ -7.90 | 3.76 | -3.66 | 0.00 | -0.38 | -0.34 | BC 358 |
| 6 | RC1 | 6 | 0 | MIN N | ▷ -57.03 | 0.09 | -0.18 | 0.00 | 0.00 | 0.00 | BC 155 |
| 153 | RC1 | 12 | 0 | MAX $V_y$ | -16.13 | ▷ 8.98 | -3.65 | 0.00 | 1.61 | 7.39 | BC 409 |
| 6 | RC1 | 12 | 4345 | MIN $V_y$ | -17.87 | ▷ -10.38 | 4.46 | 0.00 | 1.61 | 7.39 | BC 413 |
| 153 | RC1 | 12 | 0 | MAX $V_z$ | -29.14 | -6.36 | ▷ 6.24 | 0.00 | -5.10 | -4.91 | BC 242 |
| 6 | RC1 | 12 | 4345 | MIN $V_z$ | -31.68 | 7.40 | ▷ -7.21 | 0.00 | -5.10 | -4.91 | BC 242 |
| 6 | RC1 | | 2308 | MAX $M_T$ | -38.28 | -2.21 | 0.63 | ▷ 0.00 | -3.56 | -5.54 | BC 245 |
| 6 | RC1 | | 2308 | MIN $M_T$ | -21.95 | 1.52 | -1.45 | ▷ 0.00 | 4.07 | 4.18 | BC 362 |
| 6 | RC1 | | 1731 | MAX $M_y$ | -22.41 | -0.15 | 0.16 | 0.00 | ▷ 4.44 | 4.59 | BC 358 |
| 153 | RC1 | 12 | 0 | MIN $M_y$ | -29.14 | -6.36 | 6.24 | 0.00 | ▷ -5.10 | -4.91 | BC 242 |
| 153 | RC1 | 12 | 0 | MAX $M_z$ | -16.13 | 8.98 | -3.65 | 0.00 | 1.61 | ▷ 7.39 | BC 413 |
| 6 | RC1 | | 1731 | MIN $M_z$ | -38.95 | 0.10 | -0.50 | 0.00 | -3.69 | ▷ -6.16 | BC 241 |
| | **Doorgaande staven No. 3: Doorgaande staven 3** | | | | | | | | | | |
| 9 | RC1 | 48 | 0 | Max N | ▷ -46.00 | -0.16 | -17.65 | -0.00 | 0.00 | 0.00 | BC 414 |
| | | | | Min N | ▷ -253.15 | 0.05 | -1.74 | 0.02 | -0.00 | 0.00 | BC 146 |
| | | | | Max $V_y$ | -136.16 | ▷ 0.11 | 13.14 | 0.01 | 0.00 | 0.00 | BC 236 |
| | | | | Min $V_y$ | -46.00 | ▷ -0.16 | -17.65 | -0.00 | 0.00 | 0.00 | BC 414 |
| | | | | Max $V_z$ | -82.18 | 0.07 | ▷ 13.66 | 0.00 | 0.00 | 0.00 | BC 448 |
| | | | | Min $V_z$ | -116.73 | -0.15 | ▷ -17.93 | -0.00 | 0.00 | 0.00 | BC 206 |
| | | | | Max $M_T$ | -252.74 | 0.05 | -1.74 | ▷ 0.02 | -0.00 | 0.00 | BC 149 |
| | | | | Min $M_T$ | -58.01 | -0.12 | -17.60 | ▷ -0.00 | -0.00 | 0.00 | BC 390 |
| | | | | Max $M_y$ | -101.88 | 0.09 | 13.33 | 0.01 | ▷ 0.00 | -0.00 | BC 428 |
| | | | | Min $M_y$ | -77.12 | 0.08 | 13.64 | 0.00 | ▷ -0.00 | -0.00 | BC 356 |
| | | | | Max $M_z$ | -134.13 | 0.03 | -0.97 | 0.01 | 0.00 | ▷ 0.00 | BC 91 |
| | | | | Min $M_z$ | -101.82 | 0.09 | 13.33 | 0.01 | 0.00 | ▷ -0.00 | BC 432 |
| | | | 2500 | Max N | ▷ -44.01 | -0.16 | -6.55 | -0.00 | -30.25 | 0.41 | BC 414 |
| | | | Links | Min N | ▷ -250.22 | 0.05 | -1.74 | 0.02 | -4.34 | -0.12 | BC 146 |
| | | | | Max $V_y$ | -133.23 | ▷ 0.11 | 3.52 | 0.01 | 20.82 | -0.28 | BC 236 |
| | | | | Min $V_y$ | -44.01 | ▷ -0.16 | -6.55 | -0.00 | -30.25 | 0.41 | BC 414 |
| | | | | Max $V_z$ | -80.18 | 0.07 | ▷ 4.03 | 0.00 | 22.11 | -0.16 | BC 448 |
| | | | | Min $V_z$ | -113.80 | -0.15 | ▷ -6.84 | -0.00 | -30.96 | 0.38 | BC 206 |
| | | | | Max $M_T$ | -249.82 | 0.05 | -1.74 | ▷ 0.02 | -4.34 | -0.12 | BC 149 |
| | | | | Min $M_T$ | -56.02 | -0.12 | -6.50 | ▷ -0.00 | -30.13 | 0.31 | BC 390 |
| | | | | Max $M_y$ | -80.18 | 0.07 | 4.03 | 0.00 | ▷ 22.11 | -0.16 | BC 448 |
| | | | | Min $M_y$ | -113.80 | -0.15 | -6.84 | -0.00 | ▷ -30.96 | 0.38 | BC 206 |
| | | | | Max $M_z$ | -44.01 | -0.16 | -6.55 | -0.00 | -30.25 | ▷ 0.41 | BC 414 |
| | | | | Min $M_z$ | -133.23 | 0.11 | 3.52 | 0.01 | 20.82 | ▷ -0.28 | BC 236 |
| | | | 2500 | Max N | ▷ -44.01 | -0.16 | -6.55 | -0.00 | -30.25 | 0.41 | BC 414 |
| | | | Rechts | Min N | ▷ -250.22 | 0.05 | -1.74 | 0.02 | -4.34 | -0.12 | BC 146 |
| | | | | Max $V_y$ | -133.23 | ▷ 0.11 | 3.52 | 0.01 | 20.82 | -0.28 | BC 236 |
| | | | | Min $V_y$ | -44.01 | ▷ -0.16 | -6.55 | -0.00 | -30.25 | 0.41 | BC 414 |
| | | | | Max $V_z$ | -80.18 | 0.07 | ▷ 4.03 | 0.00 | 22.11 | -0.16 | BC 448 |
| | | | | Min $V_z$ | -113.80 | -0.15 | ▷ -6.84 | -0.00 | -30.96 | 0.38 | BC 206 |
| | | | | Max $M_T$ | -249.82 | 0.05 | -1.74 | ▷ 0.02 | -4.34 | -0.12 | BC 149 |
| | | | | Min $M_T$ | -56.02 | -0.12 | -6.50 | ▷ -0.00 | -30.13 | 0.31 | BC 390 |
| | | | | Max $M_y$ | -80.18 | 0.07 | 4.03 | 0.00 | ▷ 22.11 | -0.16 | BC 448 |
| | | | | Min $M_y$ | -113.80 | -0.15 | -6.84 | -0.00 | ▷ -30.96 | 0.38 | BC 206 |
| | | | | Max $M_z$ | -44.01 | -0.16 | -6.55 | -0.00 | -30.25 | ▷ 0.41 | BC 414 |
| | | | | Min $M_z$ | -133.23 | 0.11 | 3.52 | 0.01 | 20.82 | ▷ -0.28 | BC 236 |
| | | | 4345 | Max N | ▷ -40.34 | -0.16 | 1.63 | -0.00 | -34.78 | 0.71 | BC 414 |
| | | | Links | Min N | ▷ -244.85 | 0.05 | -1.74 | 0.02 | -7.54 | -0.21 | BC 146 |
| | | | | Max $V_y$ | -127.86 | ▷ 0.11 | -3.58 | 0.01 | 20.76 | -0.49 | BC 236 |
| | | | | Min $V_y$ | -40.34 | ▷ -0.16 | 1.63 | -0.00 | -34.78 | 0.71 | BC 414 |
| | | | | Max $V_z$ | -120.39 | -0.04 | ▷ 1.71 | 0.01 | -19.97 | 0.19 | BC 451 |
| | | | | Min $V_z$ | -125.74 | 0.09 | ▷ -3.59 | 0.01 | 20.73 | -0.39 | BC 204 |
| | | | | Max $M_T$ | -244.44 | 0.05 | -1.74 | ▷ 0.02 | -7.55 | -0.22 | BC 149 |
| | | | | Min $M_T$ | -52.35 | -0.12 | 1.68 | ▷ -0.00 | -34.57 | 0.54 | BC 390 |
| | | | | Max $M_y$ | -76.52 | 0.07 | -3.07 | 0.00 | ▷ 23.00 | -0.28 | BC 448 |
| | | | | Min $M_y$ | -108.43 | -0.15 | 1.35 | -0.00 | ▷ -36.02 | 0.66 | BC 206 |
| | | | | Max $M_z$ | -40.34 | -0.16 | 1.63 | -0.00 | -34.78 | ▷ 0.71 | BC 414 |
| | | | | Min $M_z$ | -127.86 | 0.11 | -3.58 | 0.01 | 20.76 | ▷ -0.49 | BC 236 |
| | | 71 | 4345 | Max N | ▷ -40.34 | -0.16 | 1.64 | -0.00 | -34.78 | 0.71 | BC 414 |
| | | | Rechts | Min N | ▷ -244.85 | 0.05 | -1.74 | 0.02 | -7.55 | -0.21 | BC 146 |
| | | | | Max $V_y$ | -127.86 | ▷ 0.11 | -3.58 | 0.01 | 20.76 | -0.49 | BC 236 |
| | | | | Min $V_y$ | -40.34 | ▷ -0.16 | 1.64 | -0.00 | -34.78 | 0.71 | BC 414 |
| | | | | Max $V_z$ | -120.39 | -0.04 | ▷ 1.71 | 0.01 | -19.97 | 0.19 | BC 451 |
| | | | | Min $V_z$ | -125.74 | 0.09 | ▷ -3.59 | 0.01 | 20.73 | -0.39 | BC 204 |
| | | | | Max $M_T$ | -244.44 | 0.05 | -1.74 | ▷ 0.02 | -7.55 | -0.22 | BC 149 |
| | | | | Min $M_T$ | -52.35 | -0.12 | 1.68 | ▷ -0.00 | -34.57 | 0.54 | BC 390 |
| | | | | Max $M_y$ | -76.52 | 0.07 | -3.07 | 0.00 | ▷ 23.00 | -0.28 | BC 448 |
| | | | | Min $M_y$ | -108.43 | -0.15 | 1.35 | -0.00 | ▷ -36.02 | 0.66 | BC 206 |
| | | | | Max $M_z$ | -40.34 | -0.16 | 1.64 | -0.00 | -34.78 | ▷ 0.71 | BC 414 |
| | | | | Min $M_z$ | -127.86 | 0.11 | -3.58 | 0.01 | 20.76 | ▷ -0.49 | BC 236 |
| | | 71 | 4345 | Max N | ▷ -40.34 | -0.16 | 1.64 | -0.00 | -34.78 | 0.71 | BC 414 |
| | | 48 | 0 | Min N | ▷ -253.15 | 0.05 | -1.74 | 0.02 | -0.00 | 0.00 | BC 146 |
| | | 48 | 0 | Max $V_y$ | -136.16 | ▷ 0.11 | 13.14 | 0.01 | 0.00 | 0.00 | BC 236 |
| | | 48 | 0 | Min $V_y$ | -46.00 | ▷ -0.16 | -17.65 | -0.00 | 0.00 | 0.00 | BC 414 |
| | | 48 | 0 | Max $V_z$ | -82.18 | 0.07 | ▷ 13.66 | 0.00 | 0.00 | 0.00 | BC 448 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 9 | RC1 | 48 | 0 | Min $V_z$ | -116.73 | -0.15 | ▷ -17.93 | -0.00 | 0.00 | 0.00 | BC 206 |
| | | 48 | 0 | Max $M_T$ | -252.74 | 0.05 | -1.74 | ▷ 0.02 | -0.00 | 0.00 | BC 149 |
| | | 48 | 0 | Min $M_T$ | -58.01 | -0.12 | -17.60 | ▷ -0.00 | -0.00 | 0.00 | BC 390 |
| | | | 3555 | Max $M_y$ | -78.09 | 0.07 | -0.03 | 0.00 | ▷ 24.22 | -0.23 | BC 448 |
| | | | 3950 | Min $M_y$ | -109.58 | -0.15 | -0.40 | -0.00 | ▷ -36.21 | 0.60 | BC 206 |
| | | 71 | 4345 | Max $M_z$ | -40.34 | -0.16 | 1.64 | -0.00 | -34.78 | ▷ 0.71 | BC 414 |
| | | 71 | 4345 | Min $M_z$ | -127.86 | 0.11 | -3.58 | 0.01 | 20.76 | ▷ -0.49 | BC 236 |
| 149 | RC1 | 71 | 0 | Max N | ▷ -62.19 | 0.02 | 0.94 | -0.00 | -18.64 | -0.00 | BC 413 |
| | | | | Min N | ▷ -232.89 | -0.06 | -1.74 | 0.02 | -7.54 | -0.21 | BC 146 |
| | | | | Max $V_y$ | -151.45 | ▷ 0.62 | 1.65 | 0.02 | -20.24 | 0.18 | BC 235 |
| | | | | Min $V_y$ | -226.59 | ▷ -0.33 | -1.78 | 0.02 | -7.74 | -0.37 | BC 148 |
| | | | | Max $V_z$ | -84.02 | 0.58 | ▷ 1.71 | 0.01 | -19.97 | 0.19 | BC 451 |
| | | | | Min $V_z$ | -128.95 | -0.22 | ▷ -3.59 | 0.01 | 20.73 | -0.39 | BC 204 |
| | | | | Max $M_T$ | -232.72 | -0.07 | -1.74 | ▷ 0.02 | -7.55 | -0.22 | BC 149 |
| | | | | Min $M_T$ | -62.55 | 0.21 | 1.68 | ▷ -0.00 | -34.57 | 0.54 | BC 390 |
| | | | | Max $M_y$ | -66.87 | -0.03 | -3.07 | 0.00 | ▷ 23.00 | -0.28 | BC 448 |
| | | | | Min $M_y$ | -127.04 | 0.25 | 1.35 | -0.00 | ▷ -36.02 | 0.66 | BC 206 |
| | | | | Max $M_z$ | -62.37 | 0.26 | 1.64 | -0.00 | -34.78 | ▷ 0.71 | BC 414 |
| | | | | Min $M_z$ | -128.97 | -0.24 | -3.58 | 0.01 | 20.76 | ▷ -0.49 | BC 236 |
| | | 49 | 3505 | Max N | ▷ -55.22 | 0.02 | 9.37 | -0.00 | -0.58 | -0.09 | BC 413 |
| | | | | Min N | ▷ -222.68 | -0.06 | -1.74 | 0.02 | -13.63 | -0.00 | BC 146 |
| | | | | Max $V_y$ | -141.24 | ▷ 0.62 | 11.83 | 0.02 | 3.38 | -2.00 | BC 235 |
| | | | | Min $V_y$ | -216.38 | ▷ -0.33 | -1.78 | 0.02 | -13.99 | 0.78 | BC 148 |
| | | | | Max $V_z$ | -55.59 | 0.21 | ▷ 17.24 | -0.00 | -1.40 | -0.20 | BC 450 |
| | | | | Min $V_z$ | -118.74 | -0.22 | ▷ -17.08 | 0.01 | -15.50 | 0.36 | BC 204 |
| | | | | Max $M_T$ | -222.51 | -0.07 | -1.74 | ▷ 0.02 | -13.64 | 0.02 | BC 149 |
| | | | | Min $M_T$ | -55.58 | 0.21 | 17.24 | ▷ -0.00 | -1.42 | -0.20 | BC 390 |
| | | | | Max $M_y$ | -77.06 | 0.58 | 11.90 | 0.01 | ▷ 3.88 | -1.84 | BC 451 |
| | | | | Min $M_y$ | -118.74 | -0.22 | -17.08 | 0.01 | ▷ -15.50 | 0.36 | BC 204 |
| | | | | Max $M_z$ | -216.38 | -0.33 | -1.78 | 0.02 | -13.99 | ▷ 0.78 | BC 148 |
| | | | | Min $M_z$ | -141.24 | 0.62 | 11.83 | 0.02 | 3.38 | ▷ -2.00 | BC 235 |
| | | 49 | 3505 | Max N | ▷ -55.22 | 0.02 | 9.37 | -0.00 | -0.58 | -0.09 | BC 413 |
| | | 71 | 0 | Min N | ▷ -232.89 | -0.06 | -1.74 | 0.02 | -7.54 | -0.21 | BC 146 |
| | | 71 | 0 | Max $V_y$ | -151.45 | ▷ 0.62 | 1.65 | 0.02 | -20.24 | 0.18 | BC 235 |
| | | 71 | 0 | Min $V_y$ | -226.59 | ▷ -0.33 | -1.78 | 0.02 | -7.74 | -0.37 | BC 148 |
| | | 49 | 3505 | Max $V_z$ | -55.59 | 0.21 | ▷ 17.24 | -0.00 | -1.40 | -0.20 | BC 450 |
| | | 49 | 3505 | Min $V_z$ | -118.74 | -0.22 | ▷ -17.08 | 0.01 | -15.50 | 0.36 | BC 204 |
| | | 71 | 0 | Max $M_T$ | -232.72 | -0.07 | -1.74 | ▷ 0.02 | -7.55 | -0.22 | BC 149 |
| | | 71 | 0 | Min $M_T$ | -62.55 | 0.21 | 1.68 | ▷ -0.00 | -34.57 | 0.54 | BC 390 |
| | | 71 | 0 | Max $M_y$ | -66.87 | -0.03 | -3.07 | 0.00 | ▷ 23.00 | -0.28 | BC 448 |
| | | 71 | 0 | Min $M_y$ | -127.04 | 0.25 | 1.35 | -0.00 | ▷ -36.02 | 0.66 | BC 206 |
| | | 49 | 3505 | Max $M_z$ | -216.38 | -0.33 | -1.78 | 0.02 | -13.99 | ▷ 0.78 | BC 148 |
| | | 49 | 3505 | Min $M_z$ | -141.24 | 0.62 | 11.83 | 0.02 | 3.38 | ▷ -2.00 | BC 235 |
| 9 | RC1 | 71 | 4345 | MAX N | ▷ -40.34 | -0.16 | 1.64 | 0.00 | -34.78 | 0.71 | BC 414 |
| 9 | RC1 | 48 | 0 | MIN N | ▷ -253.15 | 0.05 | -1.74 | 0.02 | 0.00 | 0.00 | BC 146 |
| 149 | RC1 | 71 | 0 | MAX $V_y$ | -151.45 | ▷ 0.62 | 1.65 | 0.02 | -20.24 | 0.18 | BC 235 |
| 149 | RC1 | 71 | 0 | MIN $V_y$ | -226.59 | ▷ -0.33 | -1.78 | 0.02 | -7.74 | -0.37 | BC 148 |
| 149 | RC1 | 49 | 3505 | MAX $V_z$ | -55.59 | 0.21 | ▷ 17.24 | 0.00 | -1.40 | -0.20 | BC 450 |
| 9 | RC1 | 48 | 0 | MIN $V_z$ | -116.73 | -0.15 | ▷ -17.93 | 0.00 | 0.00 | 0.00 | BC 206 |
| 9 | RC1 | 48 | 0 | MAX $M_T$ | -252.74 | 0.05 | -1.74 | ▷ 0.02 | 0.00 | 0.00 | BC 149 |
| 9 | RC1 | 48 | 0 | MIN $M_T$ | -58.01 | -0.12 | -17.60 | ▷ 0.00 | 0.00 | 0.00 | BC 390 |
| 9 | RC1 | | 3555 | MAX $M_y$ | -78.09 | 0.07 | -0.03 | 0.00 | ▷ 24.22 | -0.23 | BC 448 |
| 9 | RC1 | | 3950 | MIN $M_y$ | -109.58 | -0.15 | -0.40 | 0.00 | ▷ -36.21 | 0.60 | BC 206 |
| 149 | RC1 | 49 | 3505 | MAX $M_z$ | -216.38 | -0.33 | -1.78 | 0.02 | -13.99 | ▷ 0.78 | BC 148 |
| 149 | RC1 | 49 | 3505 | MIN $M_z$ | -141.24 | 0.62 | 11.83 | 0.02 | 3.38 | ▷ -2.00 | BC 235 |
| | **Doorgaande staven No. 4: Doorgaande staven 4** | | | | | | | | | | |
| 10 | RC1 | 36 | 0 | Max N | ▷ -44.53 | -0.17 | 17.69 | 0.00 | 0.00 | 0.00 | BC 410 |
| | | | | Min N | ▷ -252.00 | 0.06 | 2.03 | -0.03 | 0.00 | -0.00 | BC 149 |
| | | | | Max $V_y$ | -238.20 | ▷ 0.11 | 2.07 | -0.03 | 0.00 | -0.00 | BC 147 |
| | | | | Min $V_y$ | -44.53 | ▷ -0.17 | 17.69 | 0.00 | 0.00 | 0.00 | BC 410 |
| | | | | Max $V_z$ | -114.84 | -0.16 | ▷ 18.02 | 0.00 | 0.00 | 0.00 | BC 206 |
| | | | | Min $V_z$ | -81.51 | 0.07 | ▷ -13.69 | -0.01 | -0.00 | 0.00 | BC 449 |
| | | | | Max $M_T$ | -44.53 | -0.17 | 17.69 | ▷ 0.00 | 0.00 | 0.00 | BC 410 |
| | | | | Min $M_T$ | -252.00 | 0.06 | 2.03 | ▷ -0.03 | 0.00 | -0.00 | BC 149 |
| | | | | Max $M_y$ | -70.19 | 0.04 | 9.66 | -0.00 | ▷ 0.00 | 0.00 | BC 356 |
| | | | | Min $M_y$ | -81.43 | 0.07 | -13.68 | -0.01 | ▷ -0.00 | 0.00 | BC 421 |
| | | | | Max $M_z$ | -131.91 | 0.04 | 10.29 | -0.01 | 0.00 | ▷ 0.00 | BC 268 |
| | | | | Min $M_z$ | -77.35 | 0.08 | -13.67 | -0.01 | 0.00 | ▷ -0.00 | BC 353 |
| | | | 2500 | Max N | ▷ -42.53 | -0.17 | 6.59 | 0.00 | 30.35 | 0.42 | BC 410 |
| | | | Links | Min N | ▷ -249.08 | 0.06 | 2.03 | -0.03 | 5.08 | -0.14 | BC 149 |
| | | | | Max $V_y$ | -235.28 | ▷ 0.11 | 2.07 | -0.03 | 5.17 | -0.27 | BC 147 |
| | | | | Min $V_y$ | -42.53 | ▷ -0.17 | 6.59 | 0.00 | 30.35 | 0.42 | BC 410 |
| | | | | Max $V_z$ | -111.91 | -0.16 | ▷ 6.93 | 0.00 | 31.19 | 0.39 | BC 206 |
| | | | | Min $V_z$ | -79.51 | 0.07 | ▷ -4.06 | -0.01 | -22.18 | -0.17 | BC 449 |
| | | | | Max $M_T$ | -42.53 | -0.17 | 6.59 | ▷ 0.00 | 30.35 | 0.42 | BC 410 |
| | | | | Min $M_T$ | -249.08 | 0.06 | 2.03 | ▷ -0.03 | 5.08 | -0.14 | BC 149 |
| | | | | Max $M_y$ | -111.91 | -0.16 | 6.93 | 0.00 | ▷ 31.19 | 0.39 | BC 206 |
| | | | | Min $M_y$ | -79.51 | 0.07 | -4.06 | -0.01 | ▷ -22.18 | -0.17 | BC 449 |
| | | | | Max $M_z$ | -42.53 | -0.17 | 6.59 | 0.00 | 30.35 | ▷ 0.42 | BC 410 |
| | | | | Min $M_z$ | -235.28 | 0.11 | 2.07 | -0.03 | 5.17 | ▷ -0.27 | BC 147 |
| | | | 2500 | Max N | ▷ -42.53 | -0.17 | 6.59 | 0.00 | 30.35 | 0.42 | BC 410 |
| | | | Rechts | Min N | ▷ -249.08 | 0.06 | 2.03 | -0.03 | 5.08 | -0.14 | BC 149 |
| | | | | Max $V_y$ | -235.28 | ▷ 0.11 | 2.07 | -0.03 | 5.17 | -0.27 | BC 147 |
| | | | | Min $V_y$ | -42.53 | ▷ -0.17 | 6.59 | 0.00 | 30.35 | 0.42 | BC 410 |
| | | | | Max $V_z$ | -111.91 | -0.16 | ▷ 6.93 | 0.00 | 31.19 | 0.39 | BC 206 |
| | | | | Min $V_z$ | -79.51 | 0.07 | ▷ -4.06 | -0.01 | -22.18 | -0.17 | BC 449 |
| | | | | Max $M_T$ | -42.53 | -0.17 | 6.59 | ▷ 0.00 | 30.35 | 0.42 | BC 410 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 10 | RC1 | | | Min $M_T$ | -249.08 | 0.06 | 2.03 | ▷ -0.03 | 5.08 | -0.14 | BC 149 |
| | | | | Max $M_y$ | -111.91 | -0.16 | 6.93 | 0.00 | ▷ 31.19 | 0.39 | BC 206 |
| | | | | Min $M_y$ | -79.51 | 0.07 | -4.06 | -0.01 | ▷ -22.18 | -0.17 | BC 449 |
| | | | | Max $M_z$ | -42.53 | -0.17 | 6.59 | 0.00 | 30.35 | ▷ 0.42 | BC 410 |
| | | | | Min $M_z$ | -235.28 | 0.11 | 2.07 | -0.03 | 5.17 | ▷ -0.27 | BC 147 |
| | | | 4345 | Max N | ▷ -38.87 | -0.17 | -1.59 | 0.00 | 34.96 | 0.73 | BC 410 |
| | | | Links | Min N | ▷ -243.70 | 0.06 | 2.03 | -0.03 | 8.83 | -0.24 | BC 149 |
| | | | | Max $V_y$ | -229.90 | ▷ 0.11 | 2.07 | -0.03 | 8.98 | -0.47 | BC 147 |
| | | | | Min $V_y$ | -38.87 | ▷ -0.17 | -1.59 | 0.00 | 34.96 | 0.73 | BC 410 |
| | | | | Max $V_z$ | -125.23 | 0.08 | ▷ 3.64 | -0.02 | -20.51 | -0.34 | BC 205 |
| | | | | Min $V_z$ | -50.72 | -0.13 | ▷ -1.64 | 0.00 | 34.74 | 0.57 | BC 450 |
| | | | | Max $M_T$ | -38.87 | -0.17 | -1.59 | ▷ 0.00 | 34.96 | 0.73 | BC 410 |
| | | | | Min $M_T$ | -243.70 | 0.06 | 2.03 | ▷ -0.03 | 8.83 | -0.24 | BC 149 |
| | | | | Max $M_y$ | -106.54 | -0.16 | -1.26 | 0.00 | ▷ 36.43 | 0.68 | BC 206 |
| | | | | Min $M_y$ | -75.85 | 0.07 | 3.04 | -0.01 | ▷ -23.13 | -0.30 | BC 449 |
| | | | | Max $M_z$ | -38.87 | -0.17 | -1.59 | 0.00 | 34.96 | ▷ 0.73 | BC 410 |
| | | | | Min $M_z$ | -229.90 | 0.11 | 2.07 | -0.03 | 8.98 | ▷ -0.47 | BC 147 |
| | | 75 | 4345 | Max N | ▷ -38.87 | -0.17 | -1.59 | 0.00 | 34.96 | 0.73 | BC 410 |
| | | | Rechts | Min N | ▷ -243.70 | 0.06 | 2.03 | -0.03 | 8.83 | -0.24 | BC 149 |
| | | | | Max $V_y$ | -229.90 | ▷ 0.11 | 2.07 | -0.03 | 8.98 | -0.47 | BC 147 |
| | | | | Min $V_y$ | -38.87 | ▷ -0.17 | -1.59 | 0.00 | 34.96 | 0.73 | BC 410 |
| | | | | Max $V_z$ | -125.23 | 0.08 | ▷ 3.64 | -0.02 | -20.51 | -0.34 | BC 205 |
| | | | | Min $V_z$ | -50.72 | -0.13 | ▷ -1.64 | 0.00 | 34.74 | 0.57 | BC 450 |
| | | | | Max $M_T$ | -38.87 | -0.17 | -1.59 | ▷ 0.00 | 34.96 | 0.73 | BC 410 |
| | | | | Min $M_T$ | -243.70 | 0.06 | 2.03 | ▷ -0.03 | 8.83 | -0.24 | BC 149 |
| | | | | Max $M_y$ | -106.54 | -0.16 | -1.26 | 0.00 | ▷ 36.43 | 0.68 | BC 206 |
| | | | | Min $M_y$ | -75.85 | 0.07 | 3.04 | -0.01 | ▷ -23.13 | -0.30 | BC 449 |
| | | | | Max $M_z$ | -38.87 | -0.17 | -1.59 | 0.00 | 34.96 | ▷ 0.73 | BC 410 |
| | | | | Min $M_z$ | -229.90 | 0.11 | 2.07 | -0.03 | 8.98 | ▷ -0.47 | BC 147 |
| | | 75 | 4345 | Max N | ▷ -38.87 | -0.17 | -1.59 | 0.00 | 34.96 | 0.73 | BC 410 |
| | | 36 | 0 | Min N | ▷ -252.00 | 0.06 | 2.03 | -0.03 | 0.00 | -0.00 | BC 149 |
| | | 36 | 0 | Max $V_y$ | -238.20 | ▷ 0.11 | 2.07 | -0.03 | 0.00 | -0.00 | BC 147 |
| | | 36 | 0 | Min $V_y$ | -44.53 | ▷ -0.17 | 17.69 | 0.00 | 0.00 | 0.00 | BC 410 |
| | | 36 | 0 | Max $V_z$ | -114.84 | -0.16 | ▷ 18.02 | 0.00 | 0.00 | 0.00 | BC 206 |
| | | 36 | 0 | Min $V_z$ | -81.51 | 0.07 | ▷ -13.69 | -0.01 | -0.00 | 0.00 | BC 449 |
| | | 36 | 0 | Max $M_T$ | -44.53 | -0.17 | 17.69 | ▷ 0.00 | 0.00 | 0.00 | BC 410 |
| | | 36 | 0 | Min $M_T$ | -252.00 | 0.06 | 2.03 | ▷ -0.03 | 0.00 | -0.00 | BC 149 |
| | | | 4148 | Max $M_y$ | -107.11 | -0.16 | -0.38 | 0.00 | ▷ 36.59 | 0.65 | BC 206 |
| | | | 3555 | Min $M_y$ | -77.42 | 0.07 | -0.00 | -0.01 | ▷ -24.33 | -0.25 | BC 449 |
| | | 75 | 4345 | Max $M_z$ | -38.87 | -0.17 | -1.59 | 0.00 | 34.96 | ▷ 0.73 | BC 410 |
| | | 75 | 4345 | Min $M_z$ | -229.90 | 0.11 | 2.07 | -0.03 | 8.98 | ▷ -0.47 | BC 147 |
| 175 | RC1 | 75 | 0 | Max N | ▷ -61.83 | 0.27 | -1.59 | 0.00 | 34.96 | 0.73 | BC 410 |
| | | | | Min N | ▷ -232.32 | -0.05 | 2.03 | -0.03 | 8.83 | -0.24 | BC 149 |
| | | | | Max $V_y$ | -120.92 | ▷ 0.61 | -1.29 | -0.03 | 17.08 | 0.18 | BC 439 |
| | | | | Min $V_y$ | -226.79 | ▷ -0.31 | 2.07 | -0.03 | 8.98 | -0.47 | BC 147 |
| | | | | Max $V_z$ | -128.40 | -0.17 | ▷ 3.64 | -0.02 | -20.52 | -0.34 | BC 205 |
| | | | | Min $V_z$ | -62.04 | 0.22 | ▷ -1.64 | 0.00 | 34.74 | 0.57 | BC 450 |
| | | | | Max $M_T$ | -61.83 | 0.27 | -1.59 | ▷ 0.00 | 34.96 | 0.73 | BC 410 |
| | | | | Min $M_T$ | -232.32 | -0.05 | 2.03 | ▷ -0.03 | 8.83 | -0.24 | BC 149 |
| | | | | Max $M_y$ | -126.41 | 0.26 | -1.26 | 0.00 | ▷ 36.43 | 0.68 | BC 206 |
| | | | | Min $M_y$ | -66.08 | -0.03 | 3.04 | -0.01 | ▷ -23.13 | -0.30 | BC 449 |
| | | | | Max $M_z$ | -61.83 | 0.27 | -1.59 | 0.00 | 34.96 | ▷ 0.73 | BC 410 |
| | | | | Min $M_z$ | -226.79 | -0.31 | 2.07 | -0.03 | 8.98 | ▷ -0.47 | BC 147 |
| | | 37 | 3505 | Max N | ▷ -54.87 | 0.27 | -17.15 | 0.00 | 2.11 | -0.21 | BC 410 |
| | | | | Min N | ▷ -222.11 | -0.05 | 2.03 | -0.03 | 15.95 | -0.06 | BC 149 |
| | | | | Max $V_y$ | -113.96 | ▷ 0.61 | -9.73 | -0.03 | -2.23 | -1.94 | BC 439 |
| | | | | Min $V_y$ | -216.58 | ▷ -0.31 | 2.07 | -0.03 | 16.23 | 0.62 | BC 147 |
| | | | | Max $V_z$ | -118.19 | -0.17 | ▷ 17.13 | -0.02 | 15.89 | 0.26 | BC 205 |
| | | | | Min $V_z$ | -55.07 | 0.22 | ▷ -17.20 | 0.00 | 1.72 | -0.21 | BC 450 |
| | | | | Max $M_T$ | -54.87 | 0.27 | -17.15 | ▷ 0.00 | 2.11 | -0.21 | BC 410 |
| | | | | Min $M_T$ | -222.11 | -0.05 | 2.03 | ▷ -0.03 | 15.95 | -0.06 | BC 149 |
| | | | | Max $M_y$ | -216.49 | -0.29 | 2.07 | -0.03 | ▷ 16.28 | 0.62 | BC 139 |
| | | | | Min $M_y$ | -77.35 | 0.59 | -9.79 | -0.02 | ▷ -2.76 | -1.86 | BC 451 |
| | | | | Max $M_z$ | -216.49 | -0.29 | 2.07 | -0.03 | 16.25 | ▷ 0.63 | BC 140 |
| | | | | Min $M_z$ | -140.87 | 0.60 | -9.68 | -0.03 | -1.85 | ▷ -1.95 | BC 247 |
| | | 37 | 3505 | Max N | ▷ -54.87 | 0.27 | -17.15 | 0.00 | 2.11 | -0.21 | BC 410 |
| | | 75 | 0 | Min N | ▷ -232.32 | -0.05 | 2.03 | -0.03 | 8.83 | -0.24 | BC 149 |
| | | 75 | 0 | Max $V_y$ | -120.92 | ▷ 0.61 | -1.29 | -0.03 | 17.08 | 0.18 | BC 439 |
| | | 75 | 0 | Min $V_y$ | -226.79 | ▷ -0.31 | 2.07 | -0.03 | 8.98 | -0.47 | BC 147 |
| | | 37 | 3505 | Max $V_z$ | -118.19 | -0.17 | ▷ 17.13 | -0.02 | 15.89 | 0.26 | BC 205 |
| | | 37 | 3505 | Min $V_z$ | -55.07 | 0.22 | ▷ -17.20 | 0.00 | 1.72 | -0.21 | BC 450 |
| | | 75 | 0 | Max $M_T$ | -61.83 | 0.27 | -1.59 | ▷ 0.00 | 34.96 | 0.73 | BC 410 |
| | | 75 | 0 | Min $M_T$ | -232.32 | -0.05 | 2.03 | ▷ -0.03 | 8.83 | -0.24 | BC 149 |
| | | 75 | 0 | Max $M_y$ | -126.41 | 0.26 | -1.26 | 0.00 | ▷ 36.43 | 0.68 | BC 206 |
| | | 75 | 0 | Min $M_y$ | -66.08 | -0.03 | 3.04 | -0.01 | ▷ -23.13 | -0.30 | BC 449 |
| | | 75 | 0 | Max $M_z$ | -61.83 | 0.27 | -1.59 | 0.00 | 34.96 | ▷ 0.73 | BC 410 |
| | | 37 | 3505 | Min $M_z$ | -140.87 | 0.60 | -9.68 | -0.03 | -1.85 | ▷ -1.95 | BC 247 |
| 10 | RC1 | 75 | 4345 | MAX N | ▷ -38.87 | -0.17 | -1.59 | 0.00 | 34.96 | 0.73 | BC 410 |
| 10 | RC1 | 36 | 0 | MIN N | ▷ -252.00 | 0.06 | 2.03 | -0.03 | 0.00 | 0.00 | BC 149 |
| 175 | RC1 | 75 | 0 | MAX $V_y$ | -120.92 | ▷ 0.61 | -1.29 | -0.03 | 17.08 | 0.18 | BC 439 |
| 175 | RC1 | 75 | 0 | MIN $V_y$ | -226.79 | ▷ -0.31 | 2.07 | -0.03 | 8.98 | -0.47 | BC 147 |
| 10 | RC1 | 36 | 0 | MAX $V_z$ | -114.84 | -0.16 | ▷ 18.02 | 0.00 | 0.00 | 0.00 | BC 206 |
| 175 | RC1 | 37 | 3505 | MIN $V_z$ | -55.07 | 0.22 | ▷ -17.20 | 0.00 | 1.72 | -0.21 | BC 450 |
| 10 | RC1 | 36 | 0 | MAX $M_T$ | -44.53 | -0.17 | 17.69 | ▷ 0.00 | 0.00 | 0.00 | BC 410 |
| 10 | RC1 | 36 | 0 | MIN $M_T$ | -252.00 | 0.06 | 2.03 | ▷ -0.03 | 0.00 | 0.00 | BC 149 |
| 10 | RC1 | | 4148 | MAX $M_y$ | -107.11 | -0.16 | -0.38 | 0.00 | ▷ 36.59 | 0.65 | BC 206 |
| 10 | RC1 | | 3555 | MIN $M_y$ | -77.42 | 0.07 | 0.00 | -0.01 | ▷ -24.33 | -0.25 | BC 449 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 10 | RC1 | 75 | 4345 | MAX $M_z$ | -38.87 | -0.17 | -1.59 | 0.00 | 34.96 | ▷ 0.73 | BC 410 |
| 175 | RC1 | 37 | 3505 | MIN $M_z$ | -140.87 | 0.60 | -9.68 | -0.03 | -1.85 | ▷ -1.95 | BC 247 |
| | **Doorgaande staven No. 5: Doorgaande staven 5** | | | | | | | | | | |
| 13 | RC1 | 50 | 0 | Max N | ▷ -50.85 | 0.09 | -15.67 | -0.00 | 0.00 | 0.00 | BC 451 |
| | | | | Min N | ▷ -247.28 | -0.08 | -1.71 | -0.02 | 0.00 | 0.00 | BC 140 |
| | | | | Max $V_y$ | -117.86 | ▷ 0.09 | -15.97 | -0.00 | -0.00 | 0.00 | BC 235 |
| | | | | Min $V_y$ | -245.67 | ▷ -0.09 | -1.71 | -0.02 | 0.00 | 0.00 | BC 154 |
| | | | | Max $V_z$ | -90.25 | 0.05 | ▷ 14.09 | -0.00 | 0.00 | 0.00 | BC 408 |
| | | | | Min $V_z$ | -118.01 | 0.09 | ▷ -15.97 | -0.00 | 0.00 | 0.00 | BC 247 |
| | | | | Max $M_T$ | -70.66 | 0.02 | 14.06 | ▷ -0.00 | -0.00 | 0.00 | BC 360 |
| | | | | Min $M_T$ | -247.28 | -0.08 | -1.71 | ▷ -0.02 | 0.00 | 0.00 | BC 140 |
| | | | | Max $M_y$ | -115.89 | 0.03 | 13.88 | -0.00 | ▷ 0.00 | 0.00 | BC 252 |
| | | | | Min $M_y$ | -70.66 | 0.02 | 14.06 | -0.00 | ▷ -0.00 | 0.00 | BC 360 |
| | | | | Max $M_z$ | -152.61 | -0.02 | -0.90 | -0.01 | -0.00 | ▷ 0.00 | BC 91 |
| | | | | Min $M_z$ | -115.84 | 0.02 | 13.80 | -0.00 | 0.00 | ▷ -0.00 | BC 432 |
| | | | 2500 | Max N | ▷ -48.85 | 0.09 | -5.89 | -0.00 | -26.95 | -0.21 | BC 451 |
| | | | Links | Min N | ▷ -244.35 | -0.08 | -1.71 | -0.02 | -4.28 | 0.20 | BC 140 |
| | | | | Max $V_y$ | -114.94 | ▷ 0.09 | -6.19 | -0.00 | -27.70 | -0.23 | BC 235 |
| | | | | Min $V_y$ | -242.75 | ▷ -0.09 | -1.71 | -0.02 | -4.27 | 0.21 | BC 154 |
| | | | | Max $V_z$ | -88.25 | 0.05 | ▷ 4.25 | -0.00 | 22.93 | -0.13 | BC 408 |
| | | | | Min $V_z$ | -115.09 | 0.09 | ▷ -6.19 | -0.00 | -27.70 | -0.23 | BC 247 |
| | | | | Max $M_T$ | -68.66 | 0.02 | 4.21 | ▷ -0.00 | 22.84 | -0.05 | BC 360 |
| | | | | Min $M_T$ | -244.35 | -0.08 | -1.71 | ▷ -0.02 | -4.28 | 0.20 | BC 140 |
| | | | | Max $M_y$ | -88.25 | 0.05 | 4.25 | -0.00 | ▷ 22.93 | -0.13 | BC 408 |
| | | | | Min $M_y$ | -115.09 | 0.09 | -6.19 | -0.00 | ▷ -27.70 | -0.23 | BC 247 |
| | | | | Max $M_z$ | -242.75 | -0.09 | -1.71 | -0.02 | -4.27 | ▷ 0.21 | BC 154 |
| | | | | Min $M_z$ | -114.94 | 0.09 | -6.19 | -0.00 | -27.70 | ▷ -0.23 | BC 235 |
| | | | 2500 | Max N | ▷ -48.85 | 0.09 | -5.89 | -0.00 | -26.95 | -0.21 | BC 451 |
| | | | Rechts | Min N | ▷ -244.35 | -0.08 | -1.71 | -0.02 | -4.28 | 0.20 | BC 140 |
| | | | | Max $V_y$ | -114.94 | ▷ 0.09 | -6.19 | -0.00 | -27.70 | -0.23 | BC 235 |
| | | | | Min $V_y$ | -242.75 | ▷ -0.09 | -1.71 | -0.02 | -4.27 | 0.21 | BC 154 |
| | | | | Max $V_z$ | -88.25 | 0.05 | ▷ 4.25 | -0.00 | 22.93 | -0.13 | BC 408 |
| | | | | Min $V_z$ | -115.09 | 0.09 | ▷ -6.19 | -0.00 | -27.70 | -0.23 | BC 247 |
| | | | | Max $M_T$ | -68.66 | 0.02 | 4.21 | ▷ -0.00 | 22.84 | -0.05 | BC 360 |
| | | | | Min $M_T$ | -244.35 | -0.08 | -1.71 | ▷ -0.02 | -4.28 | 0.20 | BC 140 |
| | | | | Max $M_y$ | -88.25 | 0.05 | 4.25 | -0.00 | ▷ 22.93 | -0.13 | BC 408 |
| | | | | Min $M_y$ | -115.09 | 0.09 | -6.19 | -0.00 | ▷ -27.70 | -0.23 | BC 247 |
| | | | | Max $M_z$ | -242.75 | -0.09 | -1.71 | -0.02 | -4.27 | ▷ 0.21 | BC 154 |
| | | | | Min $M_z$ | -114.94 | 0.09 | -6.19 | -0.00 | -27.70 | ▷ -0.23 | BC 235 |
| | | | 4345 | Max N | ▷ -45.14 | 0.09 | 1.33 | -0.00 | -31.16 | -0.37 | BC 451 |
| | | | Links | Min N | ▷ -238.91 | -0.08 | -1.71 | -0.02 | -7.44 | 0.34 | BC 140 |
| | | | | Max $V_y$ | -109.49 | ▷ 0.09 | 1.03 | -0.00 | -32.46 | -0.40 | BC 235 |
| | | | | Min $V_y$ | -237.30 | ▷ -0.09 | -1.71 | -0.02 | -7.43 | 0.37 | BC 154 |
| | | | | Max $V_z$ | -134.83 | 0.02 | ▷ 2.33 | -0.01 | -27.02 | -0.09 | BC 410 |
| | | | | Min $V_z$ | -130.20 | 0.01 | ▷ -3.53 | -0.01 | 21.81 | -0.03 | BC 244 |
| | | | | Max $M_T$ | -64.95 | 0.02 | -3.05 | ▷ -0.00 | 23.91 | -0.08 | BC 360 |
| | | | | Min $M_T$ | -238.91 | -0.08 | -1.71 | ▷ -0.02 | -7.44 | 0.34 | BC 140 |
| | | | | Max $M_y$ | -84.54 | 0.05 | -3.01 | -0.00 | ▷ 24.07 | -0.23 | BC 408 |
| | | | | Min $M_y$ | -109.64 | 0.09 | 1.03 | -0.00 | ▷ -32.46 | -0.40 | BC 247 |
| | | | | Max $M_z$ | -237.30 | -0.09 | -1.71 | -0.02 | -7.43 | ▷ 0.37 | BC 154 |
| | | | | Min $M_z$ | -109.49 | 0.09 | 1.03 | -0.00 | -32.46 | ▷ -0.40 | BC 235 |
| | | 72 | 4345 | Max N | ▷ -45.14 | 0.09 | 1.33 | -0.00 | -31.16 | -0.37 | BC 451 |
| | | | Rechts | Min N | ▷ -238.91 | -0.08 | -1.71 | -0.02 | -7.44 | 0.34 | BC 140 |
| | | | | Max $V_y$ | -109.49 | ▷ 0.09 | 1.03 | -0.00 | -32.46 | -0.40 | BC 235 |
| | | | | Min $V_y$ | -237.30 | ▷ -0.09 | -1.71 | -0.02 | -7.43 | 0.37 | BC 154 |
| | | | | Max $V_z$ | -134.83 | 0.02 | ▷ 2.33 | -0.01 | -27.02 | -0.09 | BC 410 |
| | | | | Min $V_z$ | -130.20 | 0.01 | ▷ -3.53 | -0.01 | 21.81 | -0.03 | BC 244 |
| | | | | Max $M_T$ | -64.95 | 0.02 | -3.05 | ▷ -0.00 | 23.91 | -0.08 | BC 360 |
| | | | | Min $M_T$ | -238.91 | -0.08 | -1.71 | ▷ -0.02 | -7.44 | 0.34 | BC 140 |
| | | | | Max $M_y$ | -84.54 | 0.05 | -3.01 | -0.00 | ▷ 24.07 | -0.23 | BC 408 |
| | | | | Min $M_y$ | -109.64 | 0.09 | 1.03 | -0.00 | ▷ -32.46 | -0.40 | BC 247 |
| | | | | Max $M_z$ | -237.30 | -0.09 | -1.71 | -0.02 | -7.43 | ▷ 0.37 | BC 154 |
| | | | | Min $M_z$ | -109.49 | 0.09 | 1.03 | -0.00 | -32.46 | ▷ -0.40 | BC 235 |
| | | 72 | 4345 | Max N | ▷ -45.14 | 0.09 | 1.33 | -0.00 | -31.16 | -0.37 | BC 451 |
| | | 50 | 0 | Min N | ▷ -247.28 | -0.08 | -1.71 | -0.02 | 0.00 | 0.00 | BC 140 |
| | | 50 | 0 | Max $V_y$ | -117.86 | ▷ 0.09 | -15.97 | -0.00 | -0.00 | 0.00 | BC 235 |
| | | 50 | 0 | Min $V_y$ | -245.67 | ▷ -0.09 | -1.71 | -0.02 | 0.00 | 0.00 | BC 154 |
| | | 50 | 0 | Max $V_z$ | -90.25 | 0.05 | ▷ 14.09 | -0.00 | 0.00 | 0.00 | BC 408 |
| | | 50 | 0 | Min $V_z$ | -118.01 | 0.09 | ▷ -15.97 | -0.00 | 0.00 | 0.00 | BC 247 |
| | | 50 | 0 | Max $M_T$ | -70.66 | 0.02 | 14.06 | ▷ -0.00 | -0.00 | 0.00 | BC 360 |
| | | 50 | 0 | Min $M_T$ | -247.28 | -0.08 | -1.71 | ▷ -0.02 | 0.00 | 0.00 | BC 140 |
| | | | 3555 | Max $M_y$ | -86.13 | 0.05 | 0.10 | -0.00 | ▷ 25.22 | -0.19 | BC 408 |
| | | | 4148 | Min $M_y$ | -110.22 | 0.09 | 0.26 | -0.00 | ▷ -32.59 | -0.38 | BC 247 |
| | | 72 | 4345 | Max $M_z$ | -237.30 | -0.09 | -1.71 | -0.02 | -7.43 | ▷ 0.37 | BC 154 |
| | | 72 | 4345 | Min $M_z$ | -109.49 | 0.09 | 1.03 | -0.00 | -32.46 | ▷ -0.40 | BC 235 |
| 143 | RC1 | 72 | 0 | Max N | ▷ -63.60 | -0.04 | 0.68 | -0.00 | -20.26 | -0.04 | BC 421 |
| | | | | Min N | ▷ -233.71 | 0.26 | -1.71 | -0.02 | -7.44 | 0.34 | BC 140 |
| | | | | Max $V_y$ | -231.63 | ▷ 0.33 | -1.71 | -0.02 | -7.45 | 0.34 | BC 147 |
| | | | | Min $V_y$ | -88.57 | ▷ -0.66 | 2.33 | -0.01 | -27.02 | -0.10 | BC 414 |
| | | | | Max $V_z$ | -88.40 | -0.66 | ▷ 2.33 | -0.01 | -27.02 | -0.09 | BC 410 |
| | | | | Min $V_z$ | -131.04 | 0.03 | ▷ -3.53 | -0.01 | 21.81 | -0.03 | BC 244 |
| | | | | Max $M_T$ | -64.98 | -0.05 | -3.05 | ▷ -0.00 | 23.91 | -0.08 | BC 360 |
| | | | | Min $M_T$ | -233.71 | 0.26 | -1.71 | ▷ -0.02 | -7.44 | 0.34 | BC 140 |
| | | | | Max $M_y$ | -74.19 | -0.42 | -3.01 | -0.00 | ▷ 24.07 | -0.23 | BC 408 |
| | | | | Min $M_y$ | -129.55 | -0.14 | 1.03 | -0.00 | ▷ -32.46 | -0.40 | BC 247 |
| | | | | Max $M_z$ | -233.08 | 0.29 | -1.71 | -0.02 | -7.43 | ▷ 0.37 | BC 154 |
| | | | | Min $M_z$ | -129.55 | -0.14 | 1.03 | -0.00 | -32.46 | ▷ -0.40 | BC 235 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 143 | RC1 | 51 | 3505 | Max N | ▷ -56.54 | -0.04 | 9.31 | -0.00 | -2.76 | 0.09 | BC 421 |
| | | | | Min N | ▷ -223.36 | 0.26 | -1.71 | -0.02 | -13.44 | -0.56 | BC 140 |
| | | | | Max $V_y$ | -221.28 | ▷ 0.33 | -1.71 | -0.02 | -13.46 | -0.82 | BC 147 |
| | | | | Min $V_y$ | -81.52 | ▷ -0.66 | 16.13 | -0.01 | 5.34 | 2.23 | BC 414 |
| | | | | Max $V_z$ | -81.34 | -0.66 | ▷ 16.13 | -0.01 | 5.35 | 2.21 | BC 410 |
| | | | | Min $V_z$ | -120.70 | 0.03 | ▷ -17.33 | -0.01 | -14.76 | -0.14 | BC 244 |
| | | | | Max $M_T$ | -57.92 | -0.05 | -16.85 | ▷ -0.00 | -10.95 | 0.09 | BC 360 |
| | | | | Min $M_T$ | -223.36 | 0.26 | -1.71 | ▷ -0.02 | -13.44 | -0.56 | BC 140 |
| | | | | Max $M_y$ | -81.34 | -0.66 | 16.13 | -0.01 | ▷ 5.35 | 2.21 | BC 410 |
| | | | | Min $M_y$ | -120.70 | 0.03 | -17.33 | -0.01 | ▷ -14.76 | -0.14 | BC 244 |
| | | | | Max $M_z$ | -81.52 | -0.66 | 16.13 | -0.01 | 5.34 | ▷ 2.23 | BC 414 |
| | | | | Min $M_z$ | -221.00 | 0.30 | -1.73 | -0.02 | -13.56 | ▷ -0.84 | BC 138 |
| | | 51 | 3505 | Max N | ▷ -56.54 | -0.04 | 9.31 | -0.00 | -2.76 | 0.09 | BC 421 |
| | | 72 | 0 | Min N | ▷ -233.71 | 0.26 | -1.71 | -0.02 | -7.44 | 0.34 | BC 140 |
| | | 72 | 0 | Max $V_y$ | -231.63 | ▷ 0.33 | -1.71 | -0.02 | -7.45 | 0.34 | BC 147 |
| | | 72 | 0 | Min $V_y$ | -88.57 | ▷ -0.66 | 2.33 | -0.01 | -27.02 | -0.10 | BC 414 |
| | | 51 | 3505 | Max $V_z$ | -81.34 | -0.66 | ▷ 16.13 | -0.01 | 5.35 | 2.21 | BC 410 |
| | | 51 | 3505 | Min $V_z$ | -120.70 | 0.03 | ▷ -17.33 | -0.01 | -14.76 | -0.14 | BC 244 |
| | | 72 | 0 | Max $M_T$ | -64.98 | -0.05 | -3.05 | ▷ -0.00 | 23.91 | -0.08 | BC 360 |
| | | 72 | 0 | Min $M_T$ | -233.71 | 0.26 | -1.71 | ▷ -0.02 | -7.44 | 0.34 | BC 140 |
| | | 72 | 0 | Max $M_y$ | -74.19 | -0.42 | -3.01 | -0.00 | ▷ 24.07 | -0.23 | BC 408 |
| | | 72 | 0 | Min $M_y$ | -129.55 | -0.14 | 1.03 | -0.00 | ▷ -32.46 | -0.40 | BC 247 |
| | | 51 | 3505 | Max $M_z$ | -81.52 | -0.66 | 16.13 | -0.01 | 5.34 | ▷ 2.23 | BC 414 |
| | | 51 | 3505 | Min $M_z$ | -221.00 | 0.30 | -1.73 | -0.02 | -13.56 | ▷ -0.84 | BC 138 |
| 13 | RC1 | 72 | 4345 | MAX N | ▷ -45.14 | 0.09 | 1.33 | 0.00 | -31.16 | -0.37 | BC 451 |
| 13 | RC1 | 50 | 0 | MIN N | ▷ -247.28 | -0.08 | -1.71 | -0.02 | 0.00 | 0.00 | BC 140 |
| 143 | RC1 | 72 | 0 | MAX $V_y$ | -231.63 | ▷ 0.33 | -1.71 | -0.02 | -7.45 | 0.34 | BC 147 |
| 143 | RC1 | 72 | 0 | MIN $V_y$ | -88.57 | ▷ -0.66 | 2.33 | -0.01 | -27.02 | -0.10 | BC 414 |
| 143 | RC1 | 51 | 3505 | MAX $V_z$ | -81.34 | -0.66 | ▷ 16.13 | -0.01 | 5.35 | 2.21 | BC 410 |
| 143 | RC1 | 51 | 3505 | MIN $V_z$ | -120.70 | 0.03 | ▷ -17.33 | -0.01 | -14.76 | -0.14 | BC 244 |
| 13 | RC1 | 50 | 0 | MAX $M_T$ | -70.66 | 0.02 | 14.06 | ▷ 0.00 | 0.00 | 0.00 | BC 360 |
| 13 | RC1 | 50 | 0 | MIN $M_T$ | -247.28 | -0.08 | -1.71 | ▷ -0.02 | 0.00 | 0.00 | BC 140 |
| 13 | RC1 | | 3555 | MAX $M_y$ | -86.13 | 0.05 | 0.10 | 0.00 | ▷ 25.22 | -0.19 | BC 408 |
| 13 | RC1 | | 4148 | MIN $M_y$ | -110.22 | 0.09 | 0.26 | 0.00 | ▷ -32.59 | -0.38 | BC 247 |
| 143 | RC1 | 51 | 3505 | MAX $M_z$ | -81.52 | -0.66 | 16.13 | -0.01 | 5.34 | ▷ 2.23 | BC 414 |
| 143 | RC1 | 51 | 3505 | MIN $M_z$ | -221.00 | 0.30 | -1.73 | -0.02 | -13.56 | ▷ -0.84 | BC 138 |
| | **Doorgaande staven No. 6: Doorgaande staven 6** | | | | | | | | | | |
| 14 | RC1 | 60 | 0 | Max N | ▷ -50.92 | 0.08 | 17.76 | 0.00 | -0.00 | 0.00 | BC 423 |
| | | | Links | Min N | ▷ -244.65 | -0.06 | 1.98 | 0.03 | 0.00 | 0.00 | BC 139 |
| | | | | Max $V_y$ | -84.22 | ▷ 0.08 | 17.91 | 0.01 | -0.00 | 0.00 | BC 231 |
| | | | | Min $V_y$ | -211.55 | ▷ -0.06 | 1.74 | 0.03 | 0.00 | 0.00 | BC 332 |
| | | | | Max $V_z$ | -119.01 | 0.08 | ▷ 18.10 | 0.01 | -0.00 | 0.00 | BC 235 |
| | | | | Min $V_z$ | -87.80 | 0.03 | ▷ -14.07 | 0.01 | -0.00 | 0.00 | BC 473 |
| | | | | Max $M_T$ | -238.56 | -0.04 | 2.01 | ▷ 0.03 | -0.00 | 0.00 | BC 134 |
| | | | | Min $M_T$ | -95.49 | 0.08 | 10.17 | ▷ -0.02 | -0.00 | 0.00 | BC 408 |
| | | | | Max $M_y$ | -156.81 | 0.04 | 10.76 | -0.01 | ▷ 0.00 | 0.00 | BC 264 |
| | | | | Min $M_y$ | -174.79 | 0.01 | 14.96 | 0.03 | ▷ -0.00 | 0.00 | BC 278 |
| | | | | Max $M_z$ | -156.77 | 0.04 | 10.75 | -0.01 | 0.00 | ▷ 0.00 | BC 268 |
| | | | | Min $M_z$ | -143.32 | -0.02 | 1.18 | 0.02 | -0.00 | ▷ -0.00 | BC 289 |
| | | | 0 | Max N | ▷ -50.92 | 0.08 | 17.76 | 0.00 | 0.00 | -0.00 | BC 423 |
| | | | Rechts | Min N | ▷ -244.65 | -0.06 | 1.98 | 0.03 | 0.00 | 0.00 | BC 139 |
| | | | | Max $V_y$ | -84.22 | ▷ 0.08 | 17.91 | 0.01 | 0.00 | -0.00 | BC 231 |
| | | | | Min $V_y$ | -211.55 | ▷ -0.06 | 1.74 | 0.03 | 0.00 | 0.00 | BC 332 |
| | | | | Max $V_z$ | -119.01 | 0.08 | ▷ 18.10 | 0.01 | 0.00 | -0.00 | BC 235 |
| | | | | Min $V_z$ | -87.80 | 0.03 | ▷ -14.07 | 0.01 | -0.00 | -0.00 | BC 473 |
| | | | | Max $M_T$ | -238.56 | -0.04 | 2.01 | ▷ 0.03 | 0.00 | 0.00 | BC 134 |
| | | | | Min $M_T$ | -95.49 | 0.08 | 10.17 | ▷ -0.02 | 0.00 | -0.00 | BC 408 |
| | | | | Max $M_y$ | -119.58 | 0.08 | 18.10 | 0.01 | ▷ 0.00 | -0.00 | BC 175 |
| | | | | Min $M_y$ | -72.30 | 0.01 | -14.04 | 0.01 | ▷ -0.00 | -0.00 | BC 353 |
| | | | | Max $M_z$ | -211.55 | -0.06 | 1.74 | 0.03 | 0.00 | ▷ 0.00 | BC 332 |
| | | | | Min $M_z$ | -84.22 | 0.08 | 17.91 | 0.01 | 0.00 | ▷ -0.00 | BC 231 |
| | | | 2500 | Max N | ▷ -48.92 | 0.08 | 6.61 | 0.00 | 30.44 | -0.20 | BC 423 |
| | | | Links | Min N | ▷ -241.72 | -0.06 | 1.98 | 0.03 | 4.96 | 0.14 | BC 139 |
| | | | | Max $V_y$ | -81.29 | ▷ 0.08 | 6.76 | 0.01 | 30.82 | -0.20 | BC 231 |
| | | | | Min $V_y$ | -209.55 | ▷ -0.06 | 1.74 | 0.03 | 4.35 | 0.16 | BC 332 |
| | | | | Max $V_z$ | -116.08 | 0.08 | ▷ 6.95 | 0.01 | 31.29 | -0.20 | BC 235 |
| | | | | Min $V_z$ | -85.80 | 0.03 | ▷ -4.11 | 0.01 | -22.71 | -0.07 | BC 473 |
| | | | | Max $M_T$ | -235.63 | -0.04 | 2.01 | ▷ 0.03 | 5.02 | 0.10 | BC 134 |
| | | | | Min $M_T$ | -93.50 | 0.08 | 3.94 | ▷ -0.02 | 17.63 | -0.19 | BC 408 |
| | | | | Max $M_y$ | -116.08 | 0.08 | 6.95 | 0.01 | ▷ 31.29 | -0.20 | BC 235 |
| | | | | Min $M_y$ | -85.80 | 0.03 | -4.11 | 0.01 | ▷ -22.71 | -0.07 | BC 473 |
| | | | | Max $M_z$ | -209.55 | -0.06 | 1.74 | 0.03 | 4.35 | ▷ 0.16 | BC 332 |
| | | | | Min $M_z$ | -81.29 | 0.08 | 6.76 | 0.01 | 30.82 | ▷ -0.20 | BC 231 |
| | | | 2500 | Max N | ▷ -48.92 | 0.08 | 6.61 | 0.00 | 30.44 | -0.20 | BC 423 |
| | | | Rechts | Min N | ▷ -241.72 | -0.06 | 1.98 | 0.03 | 4.96 | 0.14 | BC 139 |
| | | | | Max $V_y$ | -81.29 | ▷ 0.08 | 6.76 | 0.01 | 30.82 | -0.20 | BC 231 |
| | | | | Min $V_y$ | -209.55 | ▷ -0.06 | 1.74 | 0.03 | 4.35 | 0.16 | BC 332 |
| | | | | Max $V_z$ | -116.08 | 0.08 | ▷ 6.95 | 0.01 | 31.29 | -0.20 | BC 235 |
| | | | | Min $V_z$ | -85.80 | 0.03 | ▷ -4.11 | 0.01 | -22.71 | -0.07 | BC 473 |
| | | | | Max $M_T$ | -235.63 | -0.04 | 2.01 | ▷ 0.03 | 5.02 | 0.10 | BC 134 |
| | | | | Min $M_T$ | -93.50 | 0.08 | 3.94 | ▷ -0.02 | 17.63 | -0.19 | BC 408 |
| | | | | Max $M_y$ | -116.08 | 0.08 | 6.95 | 0.01 | ▷ 31.29 | -0.20 | BC 235 |
| | | | | Min $M_y$ | -85.80 | 0.03 | -4.11 | 0.01 | ▷ -22.71 | -0.07 | BC 473 |
| | | | | Max $M_z$ | -209.55 | -0.06 | 1.74 | 0.03 | 4.35 | ▷ 0.16 | BC 332 |
| | | | | Min $M_z$ | -81.29 | 0.08 | 6.76 | 0.01 | 30.82 | ▷ -0.20 | BC 231 |
| | | | 4345 | Max N | ▷ -45.21 | 0.08 | -1.54 | 0.00 | 35.11 | -0.35 | BC 423 |
| | | | Links | Min N | ▷ -236.28 | -0.06 | 1.98 | 0.03 | 8.62 | 0.25 | BC 139 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 14 | RC1 | | | Max $V_y$ | -75.84 | ▷ 0.08 | -1.39 | 0.01 | 35.76 | -0.35 | BC 231 |
| | | | | Min $V_y$ | -205.84 | ▷ -0.06 | 1.74 | 0.03 | 7.57 | 0.28 | BC 332 |
| | | | | Max $V_z$ | -133.06 | -0.00 | ▷ 3.75 | 0.02 | -21.04 | 0.01 | BC 201 |
| | | | | Min $V_z$ | -138.18 | 0.03 | ▷ -2.32 | 0.03 | 27.23 | -0.12 | BC 414 |
| | | | | Max $M_T$ | -230.18 | -0.04 | 2.01 | ▷ 0.03 | 8.72 | 0.17 | BC 134 |
| | | | | Min $M_T$ | -89.78 | 0.08 | -0.60 | ▷ -0.02 | 20.70 | -0.33 | BC 408 |
| | | | | Max $M_y$ | -110.63 | 0.08 | -1.20 | 0.01 | ▷ 36.59 | -0.35 | BC 235 |
| | | | | Min $M_y$ | -82.09 | 0.03 | 3.16 | 0.01 | ▷ -23.58 | -0.13 | BC 473 |
| | | | | Max $M_z$ | -205.84 | -0.06 | 1.74 | 0.03 | 7.57 | ▷ 0.28 | BC 332 |
| | | | | Min $M_z$ | -75.84 | 0.08 | -1.39 | 0.01 | 35.76 | ▷ -0.35 | BC 231 |
| | | 76 | 4345 | Max N | ▷ -45.21 | 0.08 | -1.54 | 0.00 | 35.11 | -0.35 | BC 423 |
| | | | Rechts | Min N | ▷ -236.27 | -0.06 | 1.98 | 0.03 | 8.62 | 0.25 | BC 139 |
| | | | | Max $V_y$ | -75.84 | ▷ 0.08 | -1.39 | 0.01 | 35.76 | -0.35 | BC 231 |
| | | | | Min $V_y$ | -205.84 | ▷ -0.06 | 1.74 | 0.03 | 7.57 | 0.28 | BC 332 |
| | | | | Max $V_z$ | -133.06 | -0.00 | ▷ 3.75 | 0.02 | -21.04 | 0.01 | BC 201 |
| | | | | Min $V_z$ | -138.18 | 0.03 | ▷ -2.32 | 0.03 | 27.23 | -0.12 | BC 414 |
| | | | | Max $M_T$ | -230.18 | -0.04 | 2.01 | ▷ 0.03 | 8.72 | 0.17 | BC 134 |
| | | | | Min $M_T$ | -89.78 | 0.08 | -0.60 | ▷ -0.02 | 20.70 | -0.33 | BC 408 |
| | | | | Max $M_y$ | -110.63 | 0.08 | -1.20 | 0.01 | ▷ 36.59 | -0.35 | BC 235 |
| | | | | Min $M_y$ | -82.09 | 0.03 | 3.16 | 0.01 | ▷ -23.58 | -0.13 | BC 473 |
| | | | | Max $M_z$ | -205.84 | -0.06 | 1.74 | 0.03 | 7.57 | ▷ 0.28 | BC 332 |
| | | | | Min $M_z$ | -75.84 | 0.08 | -1.39 | 0.01 | 35.76 | ▷ -0.35 | BC 231 |
| | | 76 | 4345 | Max N | ▷ -45.21 | 0.08 | -1.54 | 0.00 | 35.11 | -0.35 | BC 423 |
| | | 60 | 0 | Min N | ▷ -244.65 | -0.06 | 1.98 | 0.03 | 0.00 | 0.00 | BC 139 |
| | | 60 | 0 | Max $V_y$ | -84.22 | ▷ 0.08 | 17.91 | 0.01 | -0.00 | 0.00 | BC 231 |
| | | 60 | 0 | Min $V_y$ | -211.55 | ▷ -0.06 | 1.74 | 0.03 | 0.00 | 0.00 | BC 332 |
| | | 60 | 0 | Max $V_z$ | -119.01 | 0.08 | ▷ 18.10 | 0.01 | -0.00 | 0.00 | BC 235 |
| | | 60 | 0 | Min $V_z$ | -87.80 | 0.03 | ▷ -14.07 | 0.01 | -0.00 | 0.00 | BC 473 |
| | | 60 | 0 | Max $M_T$ | -238.56 | -0.04 | 2.01 | ▷ 0.03 | -0.00 | 0.00 | BC 134 |
| | | 60 | 0 | Min $M_T$ | -95.49 | 0.08 | 10.17 | ▷ -0.02 | -0.00 | 0.00 | BC 408 |
| | | | 4148 | Max $M_y$ | -111.21 | 0.08 | -0.33 | 0.01 | ▷ 36.74 | -0.33 | BC 235 |
| | | | 3555 | Min $M_y$ | -83.68 | 0.03 | 0.06 | 0.01 | ▷ -24.85 | -0.10 | BC 473 |
| | | 76 | 4345 | Max $M_z$ | -205.84 | -0.06 | 1.74 | 0.03 | 7.57 | ▷ 0.28 | BC 332 |
| | | 76 | 4345 | Min $M_z$ | -75.84 | 0.08 | -1.39 | 0.01 | 35.76 | ▷ -0.35 | BC 231 |
| 176 | RC1 | 76 | 0 | Max N | ▷ -63.36 | -0.11 | -1.54 | 0.00 | 35.11 | -0.35 | BC 423 |
| | | | Links | Min N | ▷ -232.87 | 0.23 | 1.98 | 0.03 | 8.62 | 0.25 | BC 139 |
| | | | | Max $V_y$ | -232.33 | ▷ 0.25 | 1.98 | 0.03 | 8.61 | 0.22 | BC 155 |
| | | | | Min $V_y$ | -90.37 | ▷ -0.72 | -2.32 | 0.02 | 27.23 | -0.12 | BC 410 |
| | | | | Max $V_z$ | -131.33 | 0.09 | ▷ 3.75 | 0.02 | -21.04 | 0.01 | BC 201 |
| | | | | Min $V_z$ | -90.22 | -0.71 | ▷ -2.32 | 0.03 | 27.23 | -0.12 | BC 414 |
| | | | | Max $M_T$ | -232.01 | 0.24 | 2.01 | ▷ 0.03 | 8.72 | 0.17 | BC 134 |
| | | | | Min $M_T$ | -74.53 | -0.66 | -0.60 | ▷ -0.02 | 20.70 | -0.33 | BC 408 |
| | | | | Max $M_y$ | -129.36 | -0.10 | -1.20 | 0.01 | ▷ 36.59 | -0.35 | BC 235 |
| | | | | Min $M_y$ | -73.15 | -0.29 | 3.16 | 0.01 | ▷ -23.58 | -0.13 | BC 473 |
| | | | | Max $M_z$ | -203.44 | 0.19 | 1.74 | 0.03 | 7.57 | ▷ 0.28 | BC 332 |
| | | | | Min $M_z$ | -93.46 | -0.11 | -1.39 | 0.01 | 35.76 | ▷ -0.35 | BC 231 |
| | | | 0 | Max N | ▷ -63.36 | -0.11 | -1.54 | 0.00 | 35.11 | -0.35 | BC 423 |
| | | | Rechts | Min N | ▷ -232.87 | 0.23 | 1.98 | 0.03 | 8.62 | 0.25 | BC 139 |
| | | | | Max $V_y$ | -232.33 | ▷ 0.25 | 1.98 | 0.03 | 8.61 | 0.22 | BC 155 |
| | | | | Min $V_y$ | -90.37 | ▷ -0.72 | -2.32 | 0.02 | 27.23 | -0.12 | BC 410 |
| | | | | Max $V_z$ | -131.33 | 0.09 | ▷ 3.75 | 0.02 | -21.04 | 0.01 | BC 201 |
| | | | | Min $V_z$ | -90.22 | -0.71 | ▷ -2.32 | 0.03 | 27.23 | -0.12 | BC 414 |
| | | | | Max $M_T$ | -232.01 | 0.24 | 2.01 | ▷ 0.03 | 8.72 | 0.17 | BC 134 |
| | | | | Min $M_T$ | -74.53 | -0.66 | -0.60 | ▷ -0.02 | 20.70 | -0.33 | BC 408 |
| | | | | Max $M_y$ | -129.36 | -0.10 | -1.20 | 0.01 | ▷ 36.59 | -0.35 | BC 235 |
| | | | | Min $M_y$ | -73.15 | -0.29 | 3.16 | 0.01 | ▷ -23.58 | -0.13 | BC 473 |
| | | | | Max $M_z$ | -203.44 | 0.19 | 1.74 | 0.03 | 7.57 | ▷ 0.28 | BC 332 |
| | | | | Min $M_z$ | -93.46 | -0.11 | -1.39 | 0.01 | 35.76 | ▷ -0.35 | BC 231 |
| | | | 3505 | Max N | ▷ -56.30 | -0.11 | -16.87 | 0.00 | 2.78 | 0.06 | BC 423 |
| | | | Links | Min N | ▷ -222.52 | 0.23 | 1.98 | 0.03 | 15.57 | -0.57 | BC 139 |
| | | | | Max $V_y$ | -221.99 | ▷ 0.25 | 1.98 | 0.03 | 15.56 | -0.64 | BC 155 |
| | | | | Min $V_y$ | -83.32 | ▷ -0.72 | -15.98 | 0.02 | -4.91 | 2.40 | BC 410 |
| | | | | Max $V_z$ | -120.98 | 0.09 | ▷ 17.41 | 0.02 | 16.09 | -0.30 | BC 201 |
| | | | | Min $V_z$ | -56.53 | -0.09 | ▷ -16.92 | 0.00 | 2.35 | 0.07 | BC 415 |
| | | | | Max $M_T$ | -221.66 | 0.24 | 2.01 | ▷ 0.03 | 15.76 | -0.67 | BC 134 |
| | | | | Min $M_T$ | -67.47 | -0.66 | -9.14 | ▷ -0.02 | 3.59 | 1.98 | BC 408 |
| | | | | Max $M_y$ | -120.98 | 0.09 | 17.41 | 0.02 | ▷ 16.09 | -0.30 | BC 201 |
| | | | | Min $M_y$ | -83.17 | -0.71 | -15.98 | 0.03 | ▷ -4.91 | 2.38 | BC 414 |
| | | | | Max $M_z$ | -83.32 | -0.72 | -15.98 | 0.02 | -4.91 | ▷ 2.40 | BC 410 |
| | | | | Min $M_z$ | -221.65 | 0.24 | 2.01 | 0.03 | 15.76 | ▷ -0.67 | BC 149 |
| | | 61 | 3505 | Max N | ▷ -56.30 | -0.11 | -16.87 | 0.00 | 2.78 | 0.06 | BC 423 |
| | | | Rechts | Min N | ▷ -222.52 | 0.23 | 1.98 | 0.03 | 15.57 | -0.57 | BC 139 |
| | | | | Max $V_y$ | -221.99 | ▷ 0.25 | 1.98 | 0.03 | 15.56 | -0.64 | BC 155 |
| | | | | Min $V_y$ | -83.32 | ▷ -0.72 | -15.98 | 0.02 | -4.91 | 2.40 | BC 410 |
| | | | | Max $V_z$ | -120.98 | 0.09 | ▷ 17.41 | 0.02 | 16.09 | -0.30 | BC 201 |
| | | | | Min $V_z$ | -56.53 | -0.09 | ▷ -16.92 | 0.00 | 2.35 | 0.07 | BC 415 |
| | | | | Max $M_T$ | -221.66 | 0.24 | 2.01 | ▷ 0.03 | 15.76 | -0.67 | BC 134 |
| | | | | Min $M_T$ | -67.47 | -0.66 | -9.14 | ▷ -0.02 | 3.59 | 1.98 | BC 408 |
| | | | | Max $M_y$ | -120.98 | 0.09 | 17.41 | 0.02 | ▷ 16.09 | -0.30 | BC 201 |
| | | | | Min $M_y$ | -83.17 | -0.71 | -15.98 | 0.03 | ▷ -4.91 | 2.38 | BC 414 |
| | | | | Max $M_z$ | -83.32 | -0.72 | -15.98 | 0.02 | -4.91 | ▷ 2.40 | BC 410 |
| | | | | Min $M_z$ | -221.65 | 0.24 | 2.01 | 0.03 | 15.76 | ▷ -0.67 | BC 149 |
| | | 61 | 3505 | Max N | ▷ -56.30 | -0.11 | -16.87 | 0.00 | 2.78 | 0.06 | BC 423 |
| | | 76 | 0 | Min N | ▷ -232.87 | 0.23 | 1.98 | 0.03 | 8.62 | 0.25 | BC 139 |
| | | 76 | 0 | Max $V_y$ | -232.33 | ▷ 0.25 | 1.98 | 0.03 | 8.61 | 0.22 | BC 155 |
| | | 76 | 0 | Min $V_y$ | -90.37 | ▷ -0.72 | -2.32 | 0.02 | 27.23 | -0.12 | BC 410 |
| | | 61 | 3505 | Max $V_z$ | -120.98 | 0.09 | ▷ 17.41 | 0.02 | 16.09 | -0.30 | BC 201 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 176 | RC1 | 61 | 3505 | Min $V_z$ | -56.53 | -0.09 | ▷ -16.92 | 0.00 | 2.35 | 0.07 | BC 415 |
| | | 76 | 0 | Max $M_T$ | -232.01 | 0.24 | 2.01 | ▷ 0.03 | 8.72 | 0.17 | BC 134 |
| | | 76 | 0 | Min $M_T$ | -74.53 | -0.66 | -0.60 | ▷ -0.02 | 20.70 | -0.33 | BC 408 |
| | | 76 | 0 | Max $M_y$ | -129.36 | -0.10 | -1.20 | 0.01 | ▷ 36.59 | -0.35 | BC 235 |
| | | 76 | 0 | Min $M_y$ | -73.15 | -0.29 | 3.16 | 0.01 | ▷ -23.58 | -0.13 | BC 473 |
| | | 61 | 3505 | Max $M_z$ | -83.32 | -0.72 | -15.98 | 0.02 | -4.91 | ▷ 2.40 | BC 410 |
| | | 61 | 3505 | Min $M_z$ | -221.65 | 0.24 | 2.01 | 0.03 | 15.76 | ▷ -0.67 | BC 149 |
| 14 | RC1 | 76 | 4345 | MAX N | ▷ -45.21 | 0.08 | -1.54 | 0.00 | 35.11 | -0.35 | BC 423 |
| 14 | RC1 | 60 | 0 | MIN N | ▷ -244.65 | -0.06 | 1.98 | 0.03 | 0.00 | 0.00 | BC 139 |
| 176 | RC1 | 76 | 0 | MAX $V_y$ | -232.33 | ▷ 0.25 | 1.98 | 0.03 | 8.61 | 0.22 | BC 155 |
| 176 | RC1 | 76 | 0 | MIN $V_y$ | -90.37 | ▷ -0.72 | -2.32 | 0.02 | 27.23 | -0.12 | BC 410 |
| 14 | RC1 | 60 | 0 | MAX $V_z$ | -119.01 | 0.08 | ▷ 18.10 | 0.01 | 0.00 | 0.00 | BC 235 |
| 176 | RC1 | 61 | 3505 | MIN $V_z$ | -56.53 | -0.09 | ▷ -16.92 | 0.00 | 2.35 | 0.07 | BC 415 |
| 14 | RC1 | 60 | 0 | MAX $M_T$ | -238.56 | -0.04 | 2.01 | ▷ 0.03 | 0.00 | 0.00 | BC 134 |
| 14 | RC1 | 60 | 0 | MIN $M_T$ | -95.49 | 0.08 | 10.17 | ▷ -0.02 | 0.00 | 0.00 | BC 408 |
| 14 | RC1 | | 4148 | MAX $M_y$ | -111.21 | 0.08 | -0.33 | 0.01 | ▷ 36.74 | -0.33 | BC 235 |
| 14 | RC1 | | 3555 | MIN $M_y$ | -83.68 | 0.03 | 0.06 | 0.01 | ▷ -24.85 | -0.10 | BC 473 |
| 176 | RC1 | 61 | 3505 | MAX $M_z$ | -83.32 | -0.72 | -15.98 | 0.02 | -4.91 | ▷ 2.40 | BC 410 |
| 176 | RC1 | 61 | 3505 | MIN $M_z$ | -221.65 | 0.24 | 2.01 | 0.03 | 15.76 | ▷ -0.67 | BC 149 |
| | **Doorgaande staven No. 7: Doorgaande staven 7** | | | | | | | | | | |
| 17 | RC1 | 52 | 0 | Max N | ▷ -27.41 | -0.09 | -15.42 | 0.00 | 0.00 | 0.00 | BC 450 |
| | | | | Min N | ▷ -161.78 | -0.02 | -0.15 | 0.00 | 0.00 | 0.00 | BC 139 |
| | | | | Max $V_y$ | -128.58 | ▷ 0.03 | -14.87 | 0.00 | 0.00 | 0.00 | BC 247 |
| | | | | Min $V_y$ | -71.38 | ▷ -0.10 | -15.29 | 0.00 | -0.00 | 0.00 | BC 234 |
| | | | | Max $V_z$ | -69.74 | -0.07 | ▷ 14.80 | 0.00 | -0.00 | 0.00 | BC 408 |
| | | | | Min $V_z$ | -36.42 | -0.07 | ▷ -15.45 | 0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Max $M_T$ | -93.06 | -0.00 | -14.84 | ▷ 0.00 | 0.00 | 0.00 | BC 419 |
| | | | | Min $M_T$ | -57.43 | -0.02 | -9.85 | ▷ 0.00 | -0.00 | 0.00 | BC 445 |
| | | | | Max $M_y$ | -105.68 | -0.05 | 14.76 | 0.00 | ▷ 0.00 | 0.00 | BC 268 |
| | | | | Min $M_y$ | -82.65 | -0.05 | 14.76 | 0.00 | ▷ -0.00 | -0.00 | BC 432 |
| | | | | Max $M_z$ | -101.39 | -0.01 | -0.09 | 0.00 | 0.00 | ▷ 0.00 | BC 91 |
| | | | | Min $M_z$ | -82.65 | -0.05 | 14.76 | 0.00 | -0.00 | ▷ -0.00 | BC 432 |
| | | | 2500 | Max N | ▷ -25.42 | -0.09 | -5.64 | 0.00 | -26.32 | 0.23 | BC 450 |
| | | | Links | Min N | ▷ -158.85 | -0.02 | -0.15 | 0.00 | -0.39 | 0.06 | BC 139 |
| | | | | Max $V_y$ | -125.66 | ▷ 0.03 | -5.03 | 0.00 | -24.88 | -0.08 | BC 247 |
| | | | | Min $V_y$ | -68.45 | ▷ -0.10 | -5.50 | 0.00 | -25.98 | 0.26 | BC 234 |
| | | | | Max $V_z$ | -67.74 | -0.07 | ▷ 4.96 | 0.00 | 24.70 | 0.18 | BC 408 |
| | | | | Min $V_z$ | -34.42 | -0.07 | ▷ -5.67 | 0.00 | -26.41 | 0.17 | BC 446 |
| | | | | Max $M_T$ | -91.06 | -0.00 | -5.00 | ▷ 0.00 | -24.80 | 0.01 | BC 419 |
| | | | | Min $M_T$ | -55.43 | -0.02 | -3.70 | ▷ 0.00 | -16.95 | 0.05 | BC 445 |
| | | | | Max $M_y$ | -67.74 | -0.07 | 4.96 | 0.00 | ▷ 24.70 | 0.18 | BC 408 |
| | | | | Min $M_y$ | -34.42 | -0.07 | -5.67 | 0.00 | ▷ -26.41 | 0.17 | BC 446 |
| | | | | Max $M_z$ | -68.45 | -0.10 | -5.50 | 0.00 | -25.98 | ▷ 0.26 | BC 234 |
| | | | | Min $M_z$ | -125.66 | 0.03 | -5.03 | 0.00 | -24.88 | ▷ -0.08 | BC 247 |
| | | | 2500 | Max N | ▷ -25.42 | -0.09 | -5.64 | 0.00 | -26.32 | 0.23 | BC 450 |
| | | | Rechts | Min N | ▷ -158.85 | -0.02 | -0.15 | 0.00 | -0.39 | 0.06 | BC 139 |
| | | | | Max $V_y$ | -125.66 | ▷ 0.03 | -5.03 | 0.00 | -24.88 | -0.08 | BC 247 |
| | | | | Min $V_y$ | -68.45 | ▷ -0.10 | -5.50 | 0.00 | -25.98 | 0.26 | BC 234 |
| | | | | Max $V_z$ | -67.74 | -0.07 | ▷ 4.96 | 0.00 | 24.70 | 0.18 | BC 408 |
| | | | | Min $V_z$ | -34.42 | -0.07 | ▷ -5.67 | 0.00 | -26.41 | 0.17 | BC 446 |
| | | | | Max $M_T$ | -91.06 | -0.00 | -5.00 | ▷ 0.00 | -24.80 | 0.01 | BC 419 |
| | | | | Min $M_T$ | -55.43 | -0.02 | -3.70 | ▷ 0.00 | -16.95 | 0.05 | BC 445 |
| | | | | Max $M_y$ | -67.74 | -0.07 | 4.96 | 0.00 | ▷ 24.70 | 0.18 | BC 408 |
| | | | | Min $M_y$ | -34.42 | -0.07 | -5.67 | 0.00 | ▷ -26.41 | 0.17 | BC 446 |
| | | | | Max $M_z$ | -68.45 | -0.10 | -5.50 | 0.00 | -25.98 | ▷ 0.26 | BC 234 |
| | | | | Min $M_z$ | -125.66 | 0.03 | -5.03 | 0.00 | -24.88 | ▷ -0.08 | BC 247 |
| | | | 4345 | Max N | ▷ -21.70 | -0.09 | 1.58 | 0.00 | -30.06 | 0.39 | BC 450 |
| | | | Links | Min N | ▷ -153.40 | -0.02 | -0.15 | 0.00 | -0.67 | 0.11 | BC 139 |
| | | | | Max $V_y$ | -120.21 | ▷ 0.03 | 2.23 | 0.00 | -27.46 | -0.14 | BC 247 |
| | | | | Min $V_y$ | -63.01 | ▷ -0.10 | 1.72 | 0.00 | -29.47 | 0.45 | BC 234 |
| | | | | Max $V_z$ | -110.44 | -0.04 | ▷ 2.27 | 0.00 | -27.31 | 0.19 | BC 411 |
| | | | | Min $V_z$ | -85.42 | -0.03 | ▷ -2.36 | 0.00 | 26.90 | 0.14 | BC 244 |
| | | | | Max $M_T$ | -87.35 | -0.00 | 2.26 | ▷ 0.00 | -27.32 | 0.02 | BC 419 |
| | | | | Min $M_T$ | -51.72 | -0.02 | 0.84 | ▷ 0.00 | -19.59 | 0.08 | BC 445 |
| | | | | Max $M_y$ | -64.03 | -0.07 | -2.30 | 0.00 | ▷ 27.15 | 0.31 | BC 408 |
| | | | | Min $M_y$ | -30.71 | -0.07 | 1.55 | 0.00 | ▷ -30.21 | 0.30 | BC 446 |
| | | | | Max $M_z$ | -63.01 | -0.10 | 1.72 | 0.00 | -29.47 | ▷ 0.45 | BC 234 |
| | | | | Min $M_z$ | -120.21 | 0.03 | 2.23 | 0.00 | -27.46 | ▷ -0.14 | BC 247 |
| | | 73 | 4345 | Max N | ▷ -21.70 | -0.09 | 1.58 | 0.00 | -30.06 | 0.39 | BC 450 |
| | | | Rechts | Min N | ▷ -153.40 | -0.02 | -0.15 | 0.00 | -0.67 | 0.11 | BC 139 |
| | | | | Max $V_y$ | -120.21 | ▷ 0.03 | 2.23 | 0.00 | -27.46 | -0.14 | BC 247 |
| | | | | Min $V_y$ | -63.01 | ▷ -0.10 | 1.72 | 0.00 | -29.47 | 0.45 | BC 234 |
| | | | | Max $V_z$ | -110.44 | -0.04 | ▷ 2.27 | 0.00 | -27.31 | 0.19 | BC 411 |
| | | | | Min $V_z$ | -85.42 | -0.03 | ▷ -2.36 | 0.00 | 26.90 | 0.14 | BC 244 |
| | | | | Max $M_T$ | -87.35 | -0.00 | 2.26 | ▷ 0.00 | -27.32 | 0.02 | BC 419 |
| | | | | Min $M_T$ | -51.72 | -0.02 | 0.84 | ▷ 0.00 | -19.59 | 0.08 | BC 445 |
| | | | | Max $M_y$ | -64.03 | -0.07 | -2.30 | 0.00 | ▷ 27.15 | 0.31 | BC 408 |
| | | | | Min $M_y$ | -30.71 | -0.07 | 1.55 | 0.00 | ▷ -30.21 | 0.30 | BC 446 |
| | | | | Max $M_z$ | -63.01 | -0.10 | 1.72 | 0.00 | -29.47 | ▷ 0.45 | BC 234 |
| | | | | Min $M_z$ | -120.21 | 0.03 | 2.23 | 0.00 | -27.46 | ▷ -0.14 | BC 247 |
| | | 73 | 4345 | Max N | ▷ -21.70 | -0.09 | 1.58 | 0.00 | -30.06 | 0.39 | BC 450 |
| | | 52 | 0 | Min N | ▷ -161.78 | -0.02 | -0.15 | 0.00 | 0.00 | 0.00 | BC 139 |
| | | 52 | 0 | Max $V_y$ | -128.58 | ▷ 0.03 | -14.87 | 0.00 | 0.00 | 0.00 | BC 247 |
| | | 52 | 0 | Min $V_y$ | -71.38 | ▷ -0.10 | -15.29 | 0.00 | -0.00 | 0.00 | BC 234 |
| | | 52 | 0 | Max $V_z$ | -69.74 | -0.07 | ▷ 14.80 | 0.00 | -0.00 | 0.00 | BC 408 |
| | | 52 | 0 | Min $V_z$ | -36.42 | -0.07 | ▷ -15.45 | 0.00 | 0.00 | 0.00 | BC 446 |
| | | 52 | 0 | Max $M_T$ | -93.06 | -0.00 | -14.84 | ▷ 0.00 | 0.00 | 0.00 | BC 419 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 17 | RC1 | 52 | 0 | Min $M_T$ | -57.43 | -0.02 | -9.85 | ▷ 0.00 | -0.00 | 0.00 | BC 445 |
| | | | 3753 | Max $M_y$ | -65.22 | -0.07 | 0.03 | 0.00 | ▷ 27.83 | 0.27 | BC 408 |
| | | | 3950 | Min $M_y$ | -31.50 | -0.07 | 0.00 | 0.00 | ▷ -30.51 | 0.27 | BC 446 |
| | | 73 | 4345 | Max $M_z$ | -63.01 | -0.10 | 1.72 | 0.00 | -29.47 | ▷ 0.45 | BC 234 |
| | | 73 | 4345 | Min $M_z$ | -120.21 | 0.03 | 2.23 | 0.00 | -27.46 | ▷ -0.14 | BC 247 |
| 145 | RC1 | 73 | 0 | Max N | ▷ -40.15 | 0.14 | 1.60 | 0.00 | -30.00 | 0.39 | BC 422 |
| | | | | Min N | ▷ -150.61 | 0.02 | -0.17 | 0.00 | -0.74 | 0.11 | BC 140 |
| | | | | Max $V_y$ | -63.72 | ▷ 0.81 | 2.27 | 0.00 | -27.31 | 0.19 | BC 415 |
| | | | | Min $V_y$ | -67.37 | ▷ -0.00 | -0.04 | 0.00 | -0.17 | 0.04 | BC 1 |
| | | | | Max $V_z$ | -63.73 | 0.81 | ▷ 2.27 | 0.00 | -27.31 | 0.19 | BC 411 |
| | | | | Min $V_z$ | -83.75 | 0.02 | ▷ -2.36 | 0.00 | 26.90 | 0.14 | BC 244 |
| | | | | Max $M_T$ | -54.63 | 0.43 | 2.26 | ▷ 0.00 | -27.32 | 0.02 | BC 419 |
| | | | | Min $M_T$ | -45.21 | 0.22 | 0.84 | ▷ 0.00 | -19.59 | 0.08 | BC 445 |
| | | | | Max $M_y$ | -51.64 | 0.46 | -2.30 | 0.00 | ▷ 27.15 | 0.31 | BC 408 |
| | | | | Min $M_y$ | -40.26 | 0.11 | 1.55 | 0.00 | ▷ -30.21 | 0.30 | BC 446 |
| | | | | Max $M_z$ | -83.02 | 0.14 | 1.72 | 0.00 | -29.47 | ▷ 0.45 | BC 234 |
| | | | | Min $M_z$ | -93.02 | 0.24 | 2.23 | 0.00 | -27.46 | ▷ -0.14 | BC 247 |
| | | 53 | 3505 | Max N | ▷ -33.09 | 0.14 | 15.32 | 0.00 | -0.35 | -0.09 | BC 422 |
| | | | | Min N | ▷ -140.26 | 0.02 | -0.17 | 0.00 | -1.34 | 0.05 | BC 140 |
| | | | | Max $V_y$ | -56.66 | ▷ 0.81 | 16.06 | 0.00 | 4.81 | -2.65 | BC 415 |
| | | | | Min $V_y$ | -55.69 | ▷ -0.00 | -0.04 | 0.00 | -0.30 | 0.05 | BC 1 |
| | | | | Max $V_z$ | -56.67 | 0.81 | ▷ 16.06 | 0.00 | 4.81 | -2.65 | BC 411 |
| | | | | Min $V_z$ | -73.40 | 0.02 | ▷ -16.16 | 0.00 | -5.56 | 0.05 | BC 244 |
| | | | | Max $M_T$ | -47.57 | 0.43 | 16.06 | ▷ 0.00 | 4.80 | -1.50 | BC 419 |
| | | | | Min $M_T$ | -38.15 | 0.22 | 9.46 | ▷ 0.00 | -1.54 | -0.68 | BC 445 |
| | | | | Max $M_y$ | -56.67 | 0.81 | 16.06 | 0.00 | ▷ 4.81 | -2.65 | BC 411 |
| | | | | Min $M_y$ | -73.40 | 0.02 | -16.16 | 0.00 | ▷ -5.56 | 0.05 | BC 244 |
| | | | | Max $M_z$ | -140.21 | 0.01 | -0.13 | 0.00 | -1.06 | ▷ 0.07 | BC 138 |
| | | | | Min $M_z$ | -56.66 | 0.81 | 16.06 | 0.00 | 4.81 | ▷ -2.65 | BC 415 |
| | | 53 | 3505 | Max N | ▷ -33.09 | 0.14 | 15.32 | 0.00 | -0.35 | -0.09 | BC 422 |
| | | 73 | 0 | Min N | ▷ -150.61 | 0.02 | -0.17 | 0.00 | -0.74 | 0.11 | BC 140 |
| | | 73 | 0 | Max $V_y$ | -63.72 | ▷ 0.81 | 2.27 | 0.00 | -27.31 | 0.19 | BC 415 |
| | | 73 | 0 | Min $V_y$ | -67.37 | ▷ -0.00 | -0.04 | 0.00 | -0.17 | 0.04 | BC 1 |
| | | 53 | 3505 | Max $V_z$ | -56.67 | 0.81 | ▷ 16.06 | 0.00 | 4.81 | -2.65 | BC 411 |
| | | 53 | 3505 | Min $V_z$ | -73.40 | 0.02 | ▷ -16.16 | 0.00 | -5.56 | 0.05 | BC 244 |
| | | 73 | 0 | Max $M_T$ | -54.63 | 0.43 | 2.26 | ▷ 0.00 | -27.32 | 0.02 | BC 419 |
| | | 73 | 0 | Min $M_T$ | -45.21 | 0.22 | 0.84 | ▷ 0.00 | -19.59 | 0.08 | BC 445 |
| | | 73 | 0 | Max $M_y$ | -51.64 | 0.46 | -2.30 | 0.00 | ▷ 27.15 | 0.31 | BC 408 |
| | | 73 | 0 | Min $M_y$ | -40.26 | 0.11 | 1.55 | 0.00 | ▷ -30.21 | 0.30 | BC 446 |
| | | 73 | 0 | Max $M_z$ | -83.02 | 0.14 | 1.72 | 0.00 | -29.47 | ▷ 0.45 | BC 234 |
| | | 53 | 3505 | Min $M_z$ | -56.66 | 0.81 | 16.06 | 0.00 | 4.81 | ▷ -2.65 | BC 415 |
| 17 | RC1 | 73 | 4345 | MAX N | ▷ -21.70 | -0.09 | 1.58 | 0.00 | -30.06 | 0.39 | BC 450 |
| 17 | RC1 | 52 | 0 | MIN N | ▷ -161.78 | -0.02 | -0.15 | 0.00 | 0.00 | 0.00 | BC 139 |
| 145 | RC1 | 73 | 0 | MAX $V_y$ | -63.72 | ▷ 0.81 | 2.27 | 0.00 | -27.31 | 0.19 | BC 415 |
| 17 | RC1 | 52 | 0 | MIN $V_y$ | -71.38 | ▷ -0.10 | -15.29 | 0.00 | 0.00 | 0.00 | BC 234 |
| 145 | RC1 | 53 | 3505 | MAX $V_z$ | -56.67 | 0.81 | ▷ 16.06 | 0.00 | 4.81 | -2.65 | BC 411 |
| 145 | RC1 | 53 | 3505 | MIN $V_z$ | -73.40 | 0.02 | ▷ -16.16 | 0.00 | -5.56 | 0.05 | BC 244 |
| 17 | RC1 | 52 | 0 | MAX $M_T$ | -93.06 | 0.00 | -14.84 | ▷ 0.00 | 0.00 | 0.00 | BC 419 |
| 17 | RC1 | 52 | 0 | MIN $M_T$ | -57.43 | -0.02 | -9.85 | ▷ 0.00 | 0.00 | 0.00 | BC 445 |
| 17 | RC1 | | 3753 | MAX $M_y$ | -65.22 | -0.07 | 0.03 | 0.00 | ▷ 27.83 | 0.27 | BC 408 |
| 17 | RC1 | | 3950 | MIN $M_y$ | -31.50 | -0.07 | 0.00 | 0.00 | ▷ -30.51 | 0.27 | BC 446 |
| 17 | RC1 | 73 | 4345 | MAX $M_z$ | -63.01 | -0.10 | 1.72 | 0.00 | -29.47 | ▷ 0.45 | BC 234 |
| 145 | RC1 | 53 | 3505 | MIN $M_z$ | -56.66 | 0.81 | 16.06 | 0.00 | 4.81 | ▷ -2.65 | BC 415 |
| **Doorgaande staven No. 8: Doorgaande staven 8** | | | | | | | | | | | |
| 18 | RC1 | 62 | 0 | Max N | ▷ -4.02 | -0.09 | 7.02 | -0.00 | 0.00 | 0.00 | BC 422 |
| | | | Links | Min N | ▷ -125.42 | -0.06 | 3.49 | 0.00 | -0.00 | 0.00 | BC 211 |
| | | | | Max $V_y$ | -95.04 | ▷ 0.00 | 5.00 | 0.00 | 0.00 | 0.00 | BC 235 |
| | | | | Min $V_y$ | -30.26 | ▷ -0.10 | 5.95 | -0.00 | -0.00 | 0.00 | BC 246 |
| | | | | Max $V_z$ | -4.39 | -0.09 | ▷ 7.13 | -0.00 | 0.00 | 0.00 | BC 362 |
| | | | | Min $V_z$ | -64.94 | -0.08 | ▷ -13.31 | -0.00 | -0.00 | 0.00 | BC 269 |
| | | | | Max $M_T$ | -81.63 | -0.00 | 5.65 | ▷ 0.00 | -0.00 | 0.00 | BC 439 |
| | | | | Min $M_T$ | -86.38 | -0.05 | 2.24 | ▷ -0.00 | 0.00 | 0.00 | BC 204 |
| | | | | Max $M_y$ | -43.34 | -0.02 | 4.74 | -0.00 | ▷ 0.00 | 0.00 | BC 360 |
| | | | | Min $M_y$ | -74.18 | -0.04 | -4.04 | -0.00 | ▷ -0.00 | 0.00 | BC 91 |
| | | | | Max $M_z$ | -85.60 | -0.05 | 2.06 | -0.00 | -0.00 | ▷ 0.00 | BC 268 |
| | | | | Min $M_z$ | -55.53 | -0.01 | -1.99 | -0.00 | 0.00 | ▷ -0.00 | BC 289 |
| | | | 0 | Max N | ▷ -4.02 | -0.09 | 7.02 | -0.00 | 0.00 | 0.00 | BC 422 |
| | | | Rechts | Min N | ▷ -125.42 | -0.06 | 3.49 | 0.00 | 0.00 | 0.00 | BC 211 |
| | | | | Max $V_y$ | -95.04 | ▷ 0.00 | 5.00 | 0.00 | 0.00 | -0.00 | BC 235 |
| | | | | Min $V_y$ | -30.26 | ▷ -0.10 | 5.95 | -0.00 | 0.00 | 0.00 | BC 246 |
| | | | | Max $V_z$ | -4.39 | -0.09 | ▷ 7.13 | -0.00 | 0.00 | 0.00 | BC 362 |
| | | | | Min $V_z$ | -64.94 | -0.08 | ▷ -13.31 | -0.00 | -0.00 | 0.00 | BC 269 |
| | | | | Max $M_T$ | -81.63 | -0.00 | 5.65 | ▷ 0.00 | 0.00 | 0.00 | BC 439 |
| | | | | Min $M_T$ | -86.38 | -0.05 | 2.24 | ▷ -0.00 | 0.00 | 0.00 | BC 204 |
| | | | | Max $M_y$ | -4.39 | -0.09 | 7.13 | -0.00 | ▷ 0.00 | 0.00 | BC 362 |
| | | | | Min $M_y$ | -64.94 | -0.08 | -13.31 | -0.00 | ▷ -0.00 | 0.00 | BC 269 |
| | | | | Max $M_z$ | -30.26 | -0.10 | 5.95 | -0.00 | 0.00 | ▷ 0.00 | BC 246 |
| | | | | Min $M_z$ | -95.04 | 0.00 | 5.00 | 0.00 | 0.00 | ▷ -0.00 | BC 235 |
| | | | 2500 | Max N | ▷ -2.02 | -0.09 | -4.02 | -0.00 | 3.72 | 0.22 | BC 422 |
| | | | Links | Min N | ▷ -122.50 | -0.06 | -6.36 | 0.00 | -3.62 | 0.16 | BC 211 |
| | | | | Max $V_y$ | -92.11 | ▷ 0.00 | -4.84 | 0.00 | 0.18 | -0.00 | BC 235 |
| | | | | Min $V_y$ | -27.34 | ▷ -0.10 | -5.08 | -0.00 | 1.06 | 0.26 | BC 246 |
| | | | | Max $V_z$ | -18.06 | -0.03 | ▷ -0.62 | -0.00 | -13.85 | 0.06 | BC 361 |
| | | | | Min $V_z$ | -38.86 | -0.08 | ▷ -6.61 | -0.00 | -2.76 | 0.20 | BC 270 |
| | | | | Max $M_T$ | -79.64 | -0.00 | -4.20 | ▷ 0.00 | 1.79 | 0.01 | BC 439 |
| | | | | Min $M_T$ | -83.45 | -0.05 | -3.92 | ▷ -0.00 | -2.11 | 0.13 | BC 204 |
| | | | | Max $M_y$ | -41.35 | -0.02 | -1.42 | -0.00 | ▷ 4.13 | 0.05 | BC 360 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 18 | RC1 | | | Min $M_y$ | -62.01 | -0.08 | -3.46 | -0.00 | ▷ -20.94 | 0.21 | BC 269 |
| | | | | Max $M_z$ | -27.34 | -0.10 | -5.08 | -0.00 | 1.06 | ▷ 0.26 | BC 246 |
| | | | | Min $M_z$ | -92.11 | 0.00 | -4.84 | 0.00 | 0.18 | ▷ -0.00 | BC 235 |
| | | | 2500 | Max N | ▷ -2.02 | -0.09 | -4.02 | -0.00 | 3.72 | 0.22 | BC 422 |
| | | | Rechts | Min N | ▷ -122.50 | -0.06 | -6.36 | 0.00 | -3.62 | 0.16 | BC 211 |
| | | | | Max $V_y$ | -92.11 | ▷ 0.00 | -4.84 | 0.00 | 0.18 | -0.00 | BC 235 |
| | | | | Min $V_y$ | -27.34 | ▷ -0.10 | -5.08 | -0.00 | 1.06 | 0.26 | BC 246 |
| | | | | Max $V_z$ | -18.06 | -0.03 | ▷ -0.62 | -0.00 | -13.85 | 0.06 | BC 361 |
| | | | | Min $V_z$ | -38.86 | -0.08 | ▷ -6.61 | -0.00 | -2.76 | 0.20 | BC 270 |
| | | | | Max $M_T$ | -79.64 | -0.00 | -4.20 | ▷ 0.00 | 1.79 | 0.01 | BC 439 |
| | | | | Min $M_T$ | -83.45 | -0.05 | -3.92 | ▷ -0.00 | -2.11 | 0.13 | BC 204 |
| | | | | Max $M_y$ | -41.35 | -0.02 | -1.42 | -0.00 | ▷ 4.13 | 0.05 | BC 360 |
| | | | | Min $M_y$ | -62.01 | -0.08 | -3.46 | -0.00 | ▷ -20.94 | 0.21 | BC 269 |
| | | | | Max $M_z$ | -27.34 | -0.10 | -5.08 | -0.00 | 1.06 | ▷ 0.26 | BC 246 |
| | | | | Min $M_z$ | -92.11 | 0.00 | -4.84 | 0.00 | 0.18 | ▷ -0.00 | BC 235 |
| | | | 4345 | Max N | ▷ 1.69 | -0.09 | -12.09 | -0.00 | -11.15 | 0.39 | BC 422 |
| | | | Links | Min N | ▷ -117.05 | -0.06 | -13.56 | 0.00 | -22.00 | 0.27 | BC 211 |
| | | | | Max $V_y$ | -86.66 | ▷ 0.00 | -12.04 | 0.00 | -15.41 | -0.00 | BC 235 |
| | | | | Min $V_y$ | -21.89 | ▷ -0.10 | -13.16 | -0.00 | -15.78 | 0.45 | BC 246 |
| | | | | Max $V_z$ | -14.34 | -0.03 | ▷ 6.57 | -0.00 | -8.35 | 0.11 | BC 361 |
| | | | | Min $V_z$ | -33.41 | -0.08 | ▷ -14.68 | -0.00 | -22.41 | 0.34 | BC 270 |
| | | | | Max $M_T$ | -75.92 | -0.00 | -11.39 | ▷ 0.00 | -12.60 | 0.02 | BC 439 |
| | | | | Min $M_T$ | -78.00 | -0.05 | -8.41 | ▷ -0.00 | -13.50 | 0.22 | BC 204 |
| | | | | Max $M_y$ | -37.63 | -0.02 | -5.92 | -0.00 | ▷ -2.64 | 0.09 | BC 360 |
| | | | | Min $M_y$ | -115.95 | -0.06 | -13.67 | 0.00 | ▷ -22.50 | 0.25 | BC 271 |
| | | | | Max $M_z$ | -21.89 | -0.10 | -13.16 | -0.00 | -15.78 | ▷ 0.45 | BC 246 |
| | | | | Min $M_z$ | -86.66 | 0.00 | -12.04 | 0.00 | -15.41 | ▷ -0.00 | BC 235 |
| | | 77 | 4345 | Max N | ▷ 1.69 | -0.09 | -12.09 | -0.00 | -11.16 | 0.39 | BC 422 |
| | | | Rechts | Min N | ▷ -117.05 | -0.06 | -13.56 | 0.00 | -22.00 | 0.27 | BC 211 |
| | | | | Max $V_y$ | -86.66 | ▷ 0.00 | -12.04 | 0.00 | -15.41 | -0.00 | BC 235 |
| | | | | Min $V_y$ | -21.89 | ▷ -0.10 | -13.16 | -0.00 | -15.78 | 0.45 | BC 246 |
| | | | | Max $V_z$ | -14.34 | -0.03 | ▷ 6.57 | -0.00 | -8.35 | 0.11 | BC 361 |
| | | | | Min $V_z$ | -33.41 | -0.08 | ▷ -14.68 | -0.00 | -22.41 | 0.34 | BC 270 |
| | | | | Max $M_T$ | -75.92 | -0.00 | -11.39 | ▷ 0.00 | -12.60 | 0.02 | BC 439 |
| | | | | Min $M_T$ | -78.00 | -0.05 | -8.41 | ▷ -0.00 | -13.50 | 0.22 | BC 204 |
| | | | | Max $M_y$ | -37.63 | -0.02 | -5.92 | -0.00 | ▷ -2.64 | 0.09 | BC 360 |
| | | | | Min $M_y$ | -115.95 | -0.06 | -13.67 | 0.00 | ▷ -22.50 | 0.25 | BC 271 |
| | | | | Max $M_z$ | -21.89 | -0.10 | -13.16 | -0.00 | -15.78 | ▷ 0.45 | BC 246 |
| | | | | Min $M_z$ | -86.66 | 0.00 | -12.04 | 0.00 | -15.41 | ▷ -0.00 | BC 235 |
| | | 77 | 4345 | Max N | ▷ 1.69 | -0.09 | -12.09 | -0.00 | -11.16 | 0.39 | BC 422 |
| | | 62 | 0 | Min N | ▷ -125.42 | -0.06 | 3.49 | 0.00 | -0.00 | 0.00 | BC 211 |
| | | 62 | 0 | Max $V_y$ | -95.04 | ▷ 0.00 | 5.00 | 0.00 | 0.00 | 0.00 | BC 235 |
| | | 62 | 0 | Min $V_y$ | -30.26 | ▷ -0.10 | 5.95 | -0.00 | -0.00 | 0.00 | BC 246 |
| | | 62 | 0 | Max $V_z$ | -4.39 | -0.09 | ▷ 7.13 | -0.00 | 0.00 | 0.00 | BC 362 |
| | | 77 | 4345 | Min $V_z$ | -33.41 | -0.08 | ▷ -14.68 | -0.00 | -22.41 | 0.34 | BC 270 |
| | | 62 | 0 | Max $M_T$ | -81.63 | -0.00 | 5.65 | ▷ 0.00 | -0.00 | 0.00 | BC 439 |
| | | 62 | 0 | Min $M_T$ | -86.38 | -0.05 | 2.24 | ▷ -0.00 | 0.00 | 0.00 | BC 204 |
| | | | 1580 | Max $M_y$ | -3.12 | -0.09 | 0.14 | -0.00 | ▷ 5.74 | 0.14 | BC 362 |
| | | 77 | 4345 | Min $M_y$ | -115.95 | -0.06 | -13.67 | 0.00 | ▷ -22.50 | 0.25 | BC 271 |
| | | 77 | 4345 | Max $M_z$ | -21.89 | -0.10 | -13.16 | -0.00 | -15.78 | ▷ 0.45 | BC 246 |
| | | 77 | 4345 | Min $M_z$ | -86.66 | 0.00 | -12.04 | 0.00 | -15.41 | ▷ -0.00 | BC 235 |
| 107 | RC1 | 77 | 0 | Max N | ▷ -25.47 | 0.15 | 10.88 | -0.00 | -10.65 | 0.38 | BC 362 |
| | | | Links | Min N | ▷ -87.50 | 0.14 | 6.08 | -0.00 | -20.15 | 0.10 | BC 140 |
| | | | | Max $V_y$ | -51.37 | ▷ 1.01 | 11.79 | 0.00 | -17.78 | 0.32 | BC 415 |
| | | | | Min $V_y$ | -26.08 | ▷ 0.01 | 2.16 | -0.00 | -7.20 | 0.03 | BC 64 |
| | | | | Max $V_z$ | -49.96 | 0.12 | ▷ 14.24 | -0.00 | -22.41 | 0.34 | BC 270 |
| | | | | Min $V_z$ | -27.54 | 0.08 | ▷ -4.01 | -0.00 | -8.35 | 0.11 | BC 361 |
| | | | | Max $M_T$ | -50.20 | 0.45 | 10.27 | ▷ 0.00 | -12.61 | 0.02 | BC 439 |
| | | | | Min $M_T$ | -66.80 | 0.31 | 8.91 | ▷ -0.00 | -13.50 | 0.22 | BC 204 |
| | | | | Max $M_y$ | -36.65 | 0.04 | 5.80 | -0.00 | ▷ -2.64 | 0.09 | BC 360 |
| | | | | Min $M_y$ | -73.75 | 0.92 | 13.22 | 0.00 | ▷ -22.50 | 0.25 | BC 271 |
| | | | | Max $M_z$ | -49.72 | 0.15 | 12.32 | -0.00 | -15.78 | ▷ 0.45 | BC 246 |
| | | | | Min $M_z$ | -61.78 | 0.42 | 11.11 | 0.00 | -15.41 | ▷ -0.01 | BC 235 |
| | | | 0 | Max N | ▷ -25.47 | 0.15 | 10.88 | -0.00 | -10.65 | 0.38 | BC 362 |
| | | | Rechts | Min N | ▷ -87.50 | 0.14 | 6.08 | -0.00 | -20.15 | 0.10 | BC 140 |
| | | | | Max $V_y$ | -51.37 | ▷ 1.01 | 11.79 | 0.00 | -17.78 | 0.32 | BC 415 |
| | | | | Min $V_y$ | -26.08 | ▷ 0.01 | 2.16 | -0.00 | -7.20 | 0.03 | BC 64 |
| | | | | Max $V_z$ | -49.96 | 0.12 | ▷ 14.24 | -0.00 | -22.41 | 0.34 | BC 270 |
| | | | | Min $V_z$ | -27.54 | 0.08 | ▷ -4.01 | -0.00 | -8.35 | 0.11 | BC 361 |
| | | | | Max $M_T$ | -50.20 | 0.45 | 10.27 | ▷ 0.00 | -12.61 | 0.02 | BC 439 |
| | | | | Min $M_T$ | -66.80 | 0.31 | 8.91 | ▷ -0.00 | -13.50 | 0.22 | BC 204 |
| | | | | Max $M_y$ | -36.65 | 0.04 | 5.80 | -0.00 | ▷ -2.64 | 0.09 | BC 360 |
| | | | | Min $M_y$ | -73.75 | 0.92 | 13.22 | 0.00 | ▷ -22.50 | 0.25 | BC 271 |
| | | | | Max $M_z$ | -49.72 | 0.15 | 12.32 | -0.00 | -15.78 | ▷ 0.45 | BC 246 |
| | | | | Min $M_z$ | -61.78 | 0.42 | 11.11 | 0.00 | -15.41 | ▷ -0.01 | BC 235 |
| | | | 3505 | Max N | ▷ -18.41 | 0.15 | -4.28 | -0.00 | 0.85 | -0.13 | BC 362 |
| | | | Links | Min N | ▷ -77.15 | 0.14 | 6.08 | -0.00 | 1.15 | -0.40 | BC 140 |
| | | | | Max $V_y$ | -44.31 | ▷ 1.01 | -1.71 | 0.00 | -0.18 | -3.21 | BC 415 |
| | | | | Min $V_y$ | -19.02 | ▷ 0.01 | 2.16 | -0.00 | 0.36 | 0.00 | BC 64 |
| | | | | Max $V_z$ | -50.45 | 0.47 | ▷ 13.17 | -0.00 | 1.90 | -1.28 | BC 269 |
| | | | | Min $V_z$ | -18.41 | 0.15 | ▷ -4.28 | -0.00 | 0.85 | -0.13 | BC 362 |
| | | | | Max $M_T$ | -43.14 | 0.45 | -3.23 | ▷ 0.00 | -0.32 | -1.55 | BC 439 |
| | | | | Min $M_T$ | -56.45 | 0.31 | 0.48 | ▷ -0.00 | 2.92 | -0.88 | BC 204 |
| | | | | Max $M_y$ | -48.73 | 0.25 | -0.20 | -0.00 | ▷ 3.39 | -0.70 | BC 432 |
| | | | | Min $M_y$ | -32.68 | 0.52 | -3.86 | 0.00 | ▷ -0.47 | -1.75 | BC 363 |
| | | | | Max $M_z$ | -40.14 | 0.03 | 11.16 | -0.00 | 1.63 | ▷ 0.01 | BC 245 |
| | | | | Min $M_z$ | -44.31 | 1.01 | -1.71 | 0.00 | -0.18 | ▷ -3.21 | BC 415 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 107 | RC1 | 63 | 3505 | Max N | ▷ -18.41 | 0.15 | -4.28 | -0.00 | 0.85 | -0.13 | BC 362 |
| | | | Rechts | Min N | ▷ -77.15 | 0.14 | 6.08 | -0.00 | 1.15 | -0.40 | BC 140 |
| | | | | Max $V_y$ | -44.31 | ▷ 1.01 | -1.71 | 0.00 | -0.18 | -3.21 | BC 415 |
| | | | | Min $V_y$ | -19.02 | ▷ 0.01 | 2.16 | -0.00 | 0.36 | 0.00 | BC 64 |
| | | | | Max $V_z$ | -50.45 | 0.47 | ▷ 13.17 | -0.00 | 1.90 | -1.28 | BC 269 |
| | | | | Min $V_z$ | -18.41 | 0.15 | ▷ -4.28 | -0.00 | 0.85 | -0.13 | BC 362 |
| | | | | Max $M_T$ | -43.14 | 0.45 | -3.23 | ▷ 0.00 | -0.32 | -1.55 | BC 439 |
| | | | | Min $M_T$ | -56.45 | 0.31 | 0.48 | ▷ -0.00 | 2.92 | -0.88 | BC 204 |
| | | | | Max $M_y$ | -48.73 | 0.25 | -0.20 | -0.00 | ▷ 3.39 | -0.70 | BC 432 |
| | | | | Min $M_y$ | -32.68 | 0.52 | -3.86 | 0.00 | ▷ -0.47 | -1.75 | BC 363 |
| | | | | Max $M_z$ | -40.14 | 0.03 | 11.16 | -0.00 | 1.63 | ▷ 0.01 | BC 245 |
| | | | | Min $M_z$ | -44.31 | 1.01 | -1.71 | 0.00 | -0.18 | ▷ -3.21 | BC 415 |
| | | 63 | 3505 | Max N | ▷ -18.41 | 0.15 | -4.28 | -0.00 | 0.85 | -0.13 | BC 362 |
| | | 77 | 0 | Min N | ▷ -87.50 | 0.14 | 6.08 | -0.00 | -20.15 | 0.10 | BC 140 |
| | | 77 | 0 | Max $V_y$ | -51.37 | ▷ 1.01 | 11.79 | 0.00 | -17.78 | 0.32 | BC 415 |
| | | 77 | 0 | Min $V_y$ | -26.08 | ▷ 0.01 | 2.16 | -0.00 | -7.20 | 0.03 | BC 64 |
| | | 77 | 0 | Max $V_z$ | -49.96 | 0.12 | ▷ 14.24 | -0.00 | -22.41 | 0.34 | BC 270 |
| | | 63 | 3505 | Min $V_z$ | -18.41 | 0.15 | ▷ -4.28 | -0.00 | 0.85 | -0.13 | BC 362 |
| | | 77 | 0 | Max $M_T$ | -50.20 | 0.45 | 10.27 | ▷ 0.00 | -12.61 | 0.02 | BC 439 |
| | | 77 | 0 | Min $M_T$ | -66.80 | 0.31 | 8.91 | ▷ -0.00 | -13.50 | 0.22 | BC 204 |
| | | | 2337 | Max $M_y$ | -31.95 | 0.04 | 0.16 | -0.00 | ▷ 4.31 | -0.01 | BC 360 |
| | | 77 | 0 | Min $M_y$ | -73.75 | 0.92 | 13.22 | 0.00 | ▷ -22.50 | 0.25 | BC 271 |
| | | 77 | 0 | Max $M_z$ | -49.72 | 0.15 | 12.32 | -0.00 | -15.78 | ▷ 0.45 | BC 246 |
| | | 63 | 3505 | Min $M_z$ | -44.31 | 1.01 | -1.71 | 0.00 | -0.18 | ▷ -3.21 | BC 415 |
| 18 | RC1 | 77 | 4345 | MAX N | ▷ 1.69 | -0.09 | -12.09 | 0.00 | -11.16 | 0.39 | BC 422 |
| 18 | RC1 | 62 | 0 | MIN N | ▷ -125.42 | -0.06 | 3.49 | 0.00 | 0.00 | 0.00 | BC 211 |
| 107 | RC1 | 77 | 0 | MAX $V_y$ | -51.37 | ▷ 1.01 | 11.79 | 0.00 | -17.78 | 0.32 | BC 415 |
| 18 | RC1 | 62 | 0 | MIN $V_y$ | -30.26 | ▷ -0.10 | 5.95 | 0.00 | 0.00 | 0.00 | BC 246 |
| 107 | RC1 | 77 | 0 | MAX $V_z$ | -49.96 | 0.12 | ▷ 14.24 | 0.00 | -22.41 | 0.34 | BC 270 |
| 18 | RC1 | 77 | 4345 | MIN $V_z$ | -33.41 | -0.08 | ▷ -14.68 | 0.00 | -22.41 | 0.34 | BC 270 |
| 18 | RC1 | 62 | 0 | MAX $M_T$ | -81.63 | 0.00 | 5.65 | ▷ 0.00 | 0.00 | 0.00 | BC 439 |
| 18 | RC1 | 62 | 0 | MIN $M_T$ | -86.38 | -0.05 | 2.24 | ▷ 0.00 | 0.00 | 0.00 | BC 204 |
| 18 | RC1 | | 1580 | MAX $M_y$ | -3.12 | -0.09 | 0.14 | 0.00 | ▷ 5.74 | 0.14 | BC 362 |
| 107 | RC1 | 77 | 0 | MIN $M_y$ | -73.75 | 0.92 | 13.22 | 0.00 | ▷ -22.50 | 0.25 | BC 271 |
| 107 | RC1 | 77 | 0 | MAX $M_z$ | -49.72 | 0.15 | 12.32 | 0.00 | -15.78 | ▷ 0.45 | BC 246 |
| 107 | RC1 | 63 | 3505 | MIN $M_z$ | -44.31 | 1.01 | -1.71 | 0.00 | -0.18 | ▷ -3.21 | BC 415 |
| | **Doorgaande staven No. 9: Doorgaande staven 9** | | | | | | | | | | |
| 21 | RC1 | 54 | 0 | Max N | ▷ -23.54 | 0.17 | -17.38 | 0.00 | -0.00 | 0.00 | BC 415 |
| | | | | Min N | ▷ -177.50 | 0.03 | -0.09 | 0.00 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_y$ | -71.97 | ▷ 0.18 | -17.20 | 0.00 | 0.00 | 0.00 | BC 211 |
| | | | | Min $V_y$ | -97.47 | ▷ -0.09 | 14.23 | 0.00 | 0.00 | 0.00 | BC 212 |
| | | | | Max $V_z$ | -62.84 | -0.05 | ▷ 14.28 | -0.00 | 0.00 | 0.00 | BC 252 |
| | | | | Min $V_z$ | -33.03 | 0.14 | ▷ -17.39 | 0.00 | 0.00 | 0.00 | BC 419 |
| | | | | Max $M_T$ | -91.83 | -0.05 | -9.20 | ▷ 0.00 | -0.00 | 0.00 | BC 241 |
| | | | | Min $M_T$ | -80.60 | 0.00 | -10.95 | ▷ -0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Max $M_y$ | -51.39 | -0.07 | 14.25 | 0.00 | ▷ 0.00 | 0.00 | BC 360 |
| | | | | Min $M_y$ | -53.29 | -0.00 | -9.16 | 0.00 | ▷ -0.00 | 0.00 | BC 357 |
| | | | | Max $M_z$ | -90.25 | 0.01 | -0.05 | -0.00 | 0.00 | ▷ 0.00 | BC 91 |
| | | | | Min $M_z$ | -94.17 | -0.02 | -0.06 | 0.00 | -0.00 | ▷ -0.00 | BC 310 |
| | | | 2500 | Max N | ▷ -21.54 | 0.17 | -6.28 | 0.00 | -29.58 | -0.43 | BC 415 |
| | | | Links | Min N | ▷ -174.58 | 0.03 | -0.09 | 0.00 | -0.24 | -0.08 | BC 149 |
| | | | | Max $V_y$ | -69.04 | ▷ 0.18 | -6.11 | 0.00 | -29.14 | -0.44 | BC 211 |
| | | | | Min $V_y$ | -94.54 | ▷ -0.09 | 4.61 | 0.00 | 23.55 | 0.21 | BC 212 |
| | | | | Max $V_z$ | -59.91 | -0.05 | ▷ 4.66 | -0.00 | 23.67 | 0.13 | BC 252 |
| | | | | Min $V_z$ | -31.04 | 0.14 | ▷ -6.30 | 0.00 | -29.60 | -0.34 | BC 419 |
| | | | | Max $M_T$ | -88.90 | -0.05 | -3.18 | ▷ 0.00 | -15.47 | 0.12 | BC 241 |
| | | | | Min $M_T$ | -78.61 | 0.00 | -3.69 | ▷ -0.00 | -18.30 | -0.01 | BC 446 |
| | | | | Max $M_y$ | -59.91 | -0.05 | 4.66 | -0.00 | ▷ 23.67 | 0.13 | BC 252 |
| | | | | Min $M_y$ | -31.04 | 0.14 | -6.30 | 0.00 | ▷ -29.60 | -0.34 | BC 419 |
| | | | | Max $M_z$ | -94.54 | -0.09 | 4.61 | 0.00 | 23.55 | ▷ 0.21 | BC 212 |
| | | | | Min $M_z$ | -69.04 | 0.18 | -6.11 | 0.00 | -29.14 | ▷ -0.44 | BC 211 |
| | | | 2500 | Max N | ▷ -21.54 | 0.17 | -6.28 | 0.00 | -29.58 | -0.43 | BC 415 |
| | | | Rechts | Min N | ▷ -174.58 | 0.03 | -0.09 | 0.00 | -0.24 | -0.08 | BC 149 |
| | | | | Max $V_y$ | -69.04 | ▷ 0.18 | -6.11 | 0.00 | -29.14 | -0.44 | BC 211 |
| | | | | Min $V_y$ | -94.54 | ▷ -0.09 | 4.61 | 0.00 | 23.55 | 0.21 | BC 212 |
| | | | | Max $V_z$ | -59.91 | -0.05 | ▷ 4.66 | -0.00 | 23.67 | 0.13 | BC 252 |
| | | | | Min $V_z$ | -31.04 | 0.14 | ▷ -6.30 | 0.00 | -29.60 | -0.34 | BC 419 |
| | | | | Max $M_T$ | -88.90 | -0.05 | -3.18 | ▷ 0.00 | -15.47 | 0.12 | BC 241 |
| | | | | Min $M_T$ | -78.61 | 0.00 | -3.69 | ▷ -0.00 | -18.30 | -0.01 | BC 446 |
| | | | | Max $M_y$ | -59.91 | -0.05 | 4.66 | -0.00 | ▷ 23.67 | 0.13 | BC 252 |
| | | | | Min $M_y$ | -31.04 | 0.14 | -6.30 | 0.00 | ▷ -29.60 | -0.34 | BC 419 |
| | | | | Max $M_z$ | -94.54 | -0.09 | 4.61 | 0.00 | 23.55 | ▷ 0.21 | BC 212 |
| | | | | Min $M_z$ | -69.04 | 0.18 | -6.11 | 0.00 | -29.14 | ▷ -0.44 | BC 211 |
| | | | 4345 | Max N | ▷ -17.88 | 0.17 | 1.90 | 0.00 | -33.62 | -0.74 | BC 415 |
| | | | Links | Min N | ▷ -169.20 | 0.03 | -0.09 | 0.00 | -0.41 | -0.15 | BC 149 |
| | | | | Max $V_y$ | -63.67 | ▷ 0.18 | 2.08 | 0.00 | -32.86 | -0.76 | BC 211 |
| | | | | Min $V_y$ | -89.17 | ▷ -0.09 | -2.49 | 0.00 | 25.50 | 0.37 | BC 212 |
| | | | | Max $V_z$ | -65.88 | 0.17 | ▷ 2.10 | 0.00 | -32.78 | -0.73 | BC 243 |
| | | | | Min $V_z$ | -89.27 | -0.08 | ▷ -2.50 | 0.00 | 25.48 | 0.37 | BC 200 |
| | | | | Max $M_T$ | -83.53 | -0.05 | 1.26 | ▷ 0.00 | -17.25 | 0.21 | BC 241 |
| | | | | Min $M_T$ | -74.94 | 0.00 | 1.67 | ▷ -0.00 | -20.15 | -0.01 | BC 446 |
| | | | | Max $M_y$ | -54.53 | -0.05 | -2.45 | -0.00 | ▷ 25.71 | 0.22 | BC 252 |
| | | | | Min $M_y$ | -27.37 | 0.14 | 1.89 | 0.00 | ▷ -33.67 | -0.60 | BC 419 |
| | | | | Max $M_z$ | -89.17 | -0.09 | -2.49 | 0.00 | 25.50 | ▷ 0.37 | BC 212 |
| | | | | Min $M_z$ | -63.67 | 0.18 | 2.08 | 0.00 | -32.86 | ▷ -0.76 | BC 211 |
| | | 74 | 4345 | Max N | ▷ -17.88 | 0.17 | 1.90 | 0.00 | -33.62 | -0.74 | BC 415 |
| | | | Rechts | Min N | ▷ -169.20 | 0.03 | -0.09 | 0.00 | -0.41 | -0.15 | BC 149 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 21 | RC1 | | | Max $V_y$ | -63.67 | ▷ 0.18 | 2.08 | 0.00 | -32.86 | -0.76 | BC 211 |
| | | | | Min $V_y$ | -89.17 | ▷ -0.09 | -2.49 | 0.00 | 25.50 | 0.37 | BC 212 |
| | | | | Max $V_z$ | -65.88 | 0.17 | ▷ 2.10 | 0.00 | -32.78 | -0.73 | BC 243 |
| | | | | Min $V_z$ | -89.27 | -0.08 | ▷ -2.50 | 0.00 | 25.48 | 0.37 | BC 200 |
| | | | | Max $M_T$ | -83.53 | -0.05 | 1.26 | ▷ 0.00 | -17.25 | 0.21 | BC 241 |
| | | | | Min $M_T$ | -74.94 | 0.00 | 1.67 | ▷ -0.00 | -20.15 | -0.01 | BC 446 |
| | | | | Max $M_y$ | -54.53 | -0.05 | -2.45 | -0.00 | ▷ 25.71 | 0.22 | BC 252 |
| | | | | Min $M_y$ | -27.37 | 0.14 | 1.89 | 0.00 | ▷ -33.67 | -0.60 | BC 419 |
| | | | | Max $M_z$ | -89.17 | -0.09 | -2.49 | 0.00 | 25.50 | ▷ 0.37 | BC 212 |
| | | | | Min $M_z$ | -63.67 | 0.18 | 2.08 | 0.00 | -32.86 | ▷ -0.76 | BC 211 |
| | | 74 | 4345 | Max N | ▷ -17.88 | 0.17 | 1.90 | 0.00 | -33.62 | -0.74 | BC 415 |
| | | 54 | 0 | Min N | ▷ -177.50 | 0.03 | -0.09 | 0.00 | 0.00 | 0.00 | BC 149 |
| | | 54 | 0 | Max $V_y$ | -71.97 | ▷ 0.18 | -17.20 | 0.00 | 0.00 | 0.00 | BC 211 |
| | | 54 | 0 | Min $V_y$ | -97.47 | ▷ -0.09 | 14.23 | 0.00 | 0.00 | 0.00 | BC 212 |
| | | 54 | 0 | Max $V_z$ | -62.84 | -0.05 | ▷ 14.28 | -0.00 | 0.00 | 0.00 | BC 252 |
| | | 54 | 0 | Min $V_z$ | -33.03 | 0.14 | ▷ -17.39 | 0.00 | 0.00 | 0.00 | BC 419 |
| | | 54 | 0 | Max $M_T$ | -91.83 | -0.05 | -9.20 | ▷ 0.00 | -0.00 | 0.00 | BC 241 |
| | | 54 | 0 | Min $M_T$ | -80.60 | 0.00 | -10.95 | ▷ -0.00 | 0.00 | 0.00 | BC 446 |
| | | | 3753 | Max $M_y$ | -56.26 | -0.05 | -0.17 | -0.00 | ▷ 26.48 | 0.19 | BC 252 |
| | | | 3950 | Min $M_y$ | -28.16 | 0.14 | 0.14 | 0.00 | ▷ -34.07 | -0.54 | BC 419 |
| | | 74 | 4345 | Max $M_z$ | -89.17 | -0.09 | -2.49 | 0.00 | 25.50 | ▷ 0.37 | BC 212 |
| | | 74 | 4345 | Min $M_z$ | -63.67 | 0.18 | 2.08 | 0.00 | -32.86 | ▷ -0.76 | BC 211 |
| 142 | RC1 | 74 | 0 | Max N | ▷ -39.34 | -0.25 | 1.90 | 0.00 | -33.62 | -0.74 | BC 415 |
| | | | | Min N | ▷ -155.36 | -0.32 | -0.09 | 0.00 | -0.41 | -0.15 | BC 149 |
| | | | | Max $V_y$ | -82.60 | ▷ 0.09 | -2.49 | 0.00 | 25.50 | 0.37 | BC 212 |
| | | | | Min $V_y$ | -104.93 | ▷ -0.87 | 1.64 | -0.00 | -20.28 | -0.35 | BC 246 |
| | | | | Max $V_z$ | -81.52 | -0.24 | ▷ 2.10 | 0.00 | -32.78 | -0.73 | BC 243 |
| | | | | Min $V_z$ | -82.60 | 0.09 | ▷ -2.50 | 0.00 | 25.48 | 0.37 | BC 200 |
| | | | | Max $M_T$ | -81.54 | 0.03 | 1.26 | ▷ 0.00 | -17.25 | 0.21 | BC 241 |
| | | | | Min $M_T$ | -51.53 | -0.36 | 1.67 | ▷ -0.00 | -20.16 | -0.01 | BC 446 |
| | | | | Max $M_y$ | -59.05 | 0.06 | -2.45 | -0.00 | ▷ 25.71 | 0.22 | BC 252 |
| | | | | Min $M_y$ | -39.48 | -0.21 | 1.89 | 0.00 | ▷ -33.67 | -0.60 | BC 419 |
| | | | | Max $M_z$ | -82.60 | 0.09 | -2.49 | 0.00 | 25.50 | ▷ 0.37 | BC 212 |
| | | | | Min $M_z$ | -81.50 | -0.25 | 2.08 | 0.00 | -32.86 | ▷ -0.76 | BC 211 |
| | | 55 | 3505 | Max N | ▷ -32.38 | -0.25 | 17.46 | 0.00 | 0.31 | 0.15 | BC 415 |
| | | | | Min N | ▷ -145.15 | -0.32 | -0.09 | 0.00 | -0.74 | 0.96 | BC 149 |
| | | | | Max $V_y$ | -72.39 | ▷ 0.09 | -15.99 | 0.00 | -6.89 | 0.04 | BC 212 |
| | | | | Min $V_y$ | -94.72 | ▷ -0.87 | 11.82 | -0.00 | 3.31 | 2.72 | BC 246 |
| | | | | Max $V_z$ | -71.31 | -0.24 | ▷ 17.65 | 0.00 | 1.82 | 0.11 | BC 243 |
| | | | | Min $V_z$ | -72.39 | 0.09 | ▷ -15.99 | 0.00 | -6.91 | 0.04 | BC 200 |
| | | | | Max $M_T$ | -71.33 | 0.03 | 9.69 | ▷ 0.00 | 1.93 | 0.10 | BC 241 |
| | | | | Min $M_T$ | -44.56 | -0.36 | 11.85 | ▷ -0.00 | 3.55 | 1.24 | BC 446 |
| | | | | Max $M_y$ | -53.34 | -0.76 | 11.85 | -0.00 | ▷ 3.55 | 2.36 | BC 450 |
| | | | | Min $M_y$ | -72.39 | 0.09 | -15.99 | 0.00 | ▷ -6.91 | 0.04 | BC 200 |
| | | | | Max $M_z$ | -94.72 | -0.87 | 11.82 | -0.00 | 3.31 | ▷ 2.72 | BC 246 |
| | | | | Min $M_z$ | -54.72 | -0.01 | -0.04 | -0.00 | -0.28 | ▷ -0.03 | BC 15 |
| | | 55 | 3505 | Max N | ▷ -32.38 | -0.25 | 17.46 | 0.00 | 0.31 | 0.15 | BC 415 |
| | | 74 | 0 | Min N | ▷ -155.36 | -0.32 | -0.09 | 0.00 | -0.41 | -0.15 | BC 149 |
| | | 74 | 0 | Max $V_y$ | -82.60 | ▷ 0.09 | -2.49 | 0.00 | 25.50 | 0.37 | BC 212 |
| | | 74 | 0 | Min $V_y$ | -104.93 | ▷ -0.87 | 1.64 | -0.00 | -20.28 | -0.35 | BC 246 |
| | | 55 | 3505 | Max $V_z$ | -71.31 | -0.24 | ▷ 17.65 | 0.00 | 1.82 | 0.11 | BC 243 |
| | | 55 | 3505 | Min $V_z$ | -72.39 | 0.09 | ▷ -15.99 | 0.00 | -6.91 | 0.04 | BC 200 |
| | | 74 | 0 | Max $M_T$ | -81.54 | 0.03 | 1.26 | ▷ 0.00 | -17.25 | 0.21 | BC 241 |
| | | 74 | 0 | Min $M_T$ | -51.53 | -0.36 | 1.67 | ▷ -0.00 | -20.16 | -0.01 | BC 446 |
| | | 74 | 0 | Max $M_y$ | -59.05 | 0.06 | -2.45 | -0.00 | ▷ 25.71 | 0.22 | BC 252 |
| | | 74 | 0 | Min $M_y$ | -39.48 | -0.21 | 1.89 | 0.00 | ▷ -33.67 | -0.60 | BC 419 |
| | | 55 | 3505 | Max $M_z$ | -94.72 | -0.87 | 11.82 | -0.00 | 3.31 | ▷ 2.72 | BC 246 |
| | | 74 | 0 | Min $M_z$ | -81.50 | -0.25 | 2.08 | 0.00 | -32.86 | ▷ -0.76 | BC 211 |
| 21 | RC1 | 74 | 4345 | MAX N | ▷ -17.88 | 0.17 | 1.90 | 0.00 | -33.62 | -0.74 | BC 415 |
| 21 | RC1 | 54 | 0 | MIN N | ▷ -177.50 | 0.03 | -0.09 | 0.00 | 0.00 | 0.00 | BC 149 |
| 21 | RC1 | 54 | 0 | MAX $V_y$ | -71.97 | ▷ 0.18 | -17.20 | 0.00 | 0.00 | 0.00 | BC 211 |
| 142 | RC1 | 74 | 0 | MIN $V_y$ | -104.93 | ▷ -0.87 | 1.64 | 0.00 | -20.28 | -0.35 | BC 246 |
| 142 | RC1 | 55 | 3505 | MAX $V_z$ | -71.31 | -0.24 | ▷ 17.65 | 0.00 | 1.82 | 0.11 | BC 243 |
| 21 | RC1 | 54 | 0 | MIN $V_z$ | -33.03 | 0.14 | ▷ -17.39 | 0.00 | 0.00 | 0.00 | BC 419 |
| 21 | RC1 | 54 | 0 | MAX $M_T$ | -91.83 | -0.05 | -9.20 | ▷ 0.00 | 0.00 | 0.00 | BC 241 |
| 21 | RC1 | 54 | 0 | MIN $M_T$ | -80.60 | 0.00 | -10.95 | ▷ 0.00 | 0.00 | 0.00 | BC 446 |
| 21 | RC1 | | 3753 | MAX $M_y$ | -56.26 | -0.05 | -0.17 | 0.00 | ▷ 26.48 | 0.19 | BC 252 |
| 21 | RC1 | | 3950 | MIN $M_y$ | -28.16 | 0.14 | 0.14 | 0.00 | ▷ -34.07 | -0.54 | BC 419 |
| 142 | RC1 | 55 | 3505 | MAX $M_z$ | -94.72 | -0.87 | 11.82 | 0.00 | 3.31 | ▷ 2.72 | BC 246 |
| 21 | RC1 | 74 | 4345 | MIN $M_z$ | -63.67 | 0.18 | 2.08 | 0.00 | -32.86 | ▷ -0.76 | BC 211 |
| **Doorgaande staven No. 10: Doorgaande staven 10** | | | | | | | | | | | |
| 22 | RC1 | 64 | 0 | Max N | ▷ -3.82 | 0.18 | 17.29 | 0.00 | -0.00 | 0.00 | BC 415 |
| | | | | Min N | ▷ -117.99 | 0.10 | 9.30 | -0.00 | 0.00 | 0.00 | BC 234 |
| | | | | Max $V_y$ | -31.67 | ▷ 0.18 | 17.26 | 0.00 | -0.00 | 0.00 | BC 207 |
| | | | | Min $V_y$ | -59.33 | ▷ -0.06 | -14.79 | -0.00 | -0.00 | 0.00 | BC 273 |
| | | | | Max $V_z$ | -5.86 | 0.17 | ▷ 17.29 | 0.00 | 0.00 | 0.00 | BC 447 |
| | | | | Min $V_z$ | -33.20 | -0.05 | ▷ -14.81 | -0.00 | 0.00 | 0.00 | BC 361 |
| | | | | Max $M_T$ | -30.82 | 0.14 | 17.25 | ▷ 0.00 | -0.00 | 0.00 | BC 171 |
| | | | | Min $M_T$ | -46.83 | -0.04 | -14.76 | ▷ -0.00 | -0.00 | 0.00 | BC 209 |
| | | | | Max $M_y$ | -37.77 | -0.01 | 9.29 | -0.00 | ▷ 0.00 | 0.00 | BC 388 |
| | | | | Min $M_y$ | -73.35 | 0.00 | 9.29 | -0.00 | ▷ -0.00 | 0.00 | BC 278 |
| | | | | Max $M_z$ | -50.48 | -0.02 | 9.30 | -0.00 | 0.00 | ▷ 0.00 | BC 268 |
| | | | | Min $M_z$ | -57.25 | 0.01 | 0.04 | -0.00 | 0.00 | ▷ -0.00 | BC 289 |
| | | | 2500 | Max N | ▷ -1.82 | 0.18 | 6.19 | 0.00 | 29.35 | -0.44 | BC 415 |
| | | | Links | Min N | ▷ -115.06 | 0.10 | 3.28 | -0.00 | 15.72 | -0.24 | BC 234 |
| | | | | Max $V_y$ | -28.74 | ▷ 0.18 | 6.17 | 0.00 | 29.28 | -0.46 | BC 207 |
| | | | | Min $V_y$ | -56.40 | ▷ -0.06 | -5.16 | -0.00 | -24.94 | 0.16 | BC 273 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 22 | RC1 | | | Max $V_z$ | -3.87 | 0.17 | ▷ 6.19 | 0.00 | 29.35 | -0.42 | BC 447 |
| | | | | Min $V_z$ | -31.20 | -0.05 | ▷ -5.18 | -0.00 | -24.99 | 0.12 | BC 361 |
| | | | | Max $M_T$ | -27.89 | 0.14 | 6.16 | ▷ 0.00 | 29.27 | -0.36 | BC 171 |
| | | | | Min $M_T$ | -43.91 | -0.04 | -5.14 | ▷ -0.00 | -24.88 | 0.11 | BC 209 |
| | | | | Max $M_y$ | -3.87 | 0.17 | 6.19 | 0.00 | ▷ 29.35 | -0.42 | BC 447 |
| | | | | Min $M_y$ | -27.43 | -0.05 | -5.18 | -0.00 | ▷ -24.99 | 0.11 | BC 357 |
| | | | | Max $M_z$ | -56.40 | -0.06 | -5.16 | -0.00 | -24.94 | ▷ 0.16 | BC 273 |
| | | | | Min $M_z$ | -28.74 | 0.18 | 6.17 | 0.00 | 29.28 | ▷ -0.46 | BC 207 |
| | | | 2500 | Max N | ▷ -1.82 | 0.18 | 6.19 | 0.00 | 29.35 | -0.44 | BC 415 |
| | | | Rechts | Min N | ▷ -115.06 | 0.10 | 3.28 | -0.00 | 15.72 | -0.24 | BC 234 |
| | | | | Max $V_y$ | -28.74 | ▷ 0.18 | 6.16 | 0.00 | 29.28 | -0.46 | BC 207 |
| | | | | Min $V_y$ | -56.40 | ▷ -0.06 | -5.16 | -0.00 | -24.94 | 0.16 | BC 273 |
| | | | | Max $V_z$ | -3.87 | 0.17 | ▷ 6.19 | 0.00 | 29.35 | -0.42 | BC 447 |
| | | | | Min $V_z$ | -31.20 | -0.05 | ▷ -5.18 | -0.00 | -24.99 | 0.12 | BC 361 |
| | | | | Max $M_T$ | -27.89 | 0.14 | 6.16 | ▷ 0.00 | 29.27 | -0.36 | BC 171 |
| | | | | Min $M_T$ | -43.91 | -0.04 | -5.14 | ▷ -0.00 | -24.88 | 0.11 | BC 209 |
| | | | | Max $M_y$ | -3.87 | 0.17 | 6.19 | 0.00 | ▷ 29.35 | -0.42 | BC 447 |
| | | | | Min $M_y$ | -27.43 | -0.05 | -5.18 | -0.00 | ▷ -24.99 | 0.11 | BC 357 |
| | | | | Max $M_z$ | -56.40 | -0.06 | -5.16 | -0.00 | -24.94 | ▷ 0.16 | BC 273 |
| | | | | Min $M_z$ | -28.74 | 0.18 | 6.16 | 0.00 | 29.28 | ▷ -0.46 | BC 207 |
| | | | 4345 | Max N | ▷ 1.84 | 0.18 | -1.99 | 0.00 | 33.22 | -0.76 | BC 415 |
| | | | Links | Min N | ▷ -109.69 | 0.10 | -1.16 | -0.00 | 17.68 | -0.42 | BC 234 |
| | | | | Max $V_y$ | -23.37 | ▷ 0.18 | -2.02 | 0.00 | 33.10 | -0.79 | BC 207 |
| | | | | Min $V_y$ | -51.03 | ▷ -0.06 | 1.94 | -0.00 | -27.91 | 0.27 | BC 273 |
| | | | | Max $V_z$ | -39.01 | -0.05 | ▷ 1.96 | -0.00 | -27.80 | 0.20 | BC 269 |
| | | | | Min $V_z$ | -35.49 | 0.14 | ▷ -2.04 | 0.00 | 33.02 | -0.63 | BC 175 |
| | | | | Max $M_T$ | -22.52 | 0.14 | -2.03 | ▷ 0.00 | 33.08 | -0.62 | BC 171 |
| | | | | Min $M_T$ | -38.53 | -0.04 | 1.96 | ▷ -0.00 | -27.81 | 0.19 | BC 209 |
| | | | | Max $M_y$ | -0.20 | 0.17 | -1.99 | 0.00 | ▷ 33.23 | -0.73 | BC 447 |
| | | | | Min $M_y$ | -27.54 | -0.05 | 1.92 | -0.00 | ▷ -28.00 | 0.22 | BC 361 |
| | | | | Max $M_z$ | -51.03 | -0.06 | 1.94 | -0.00 | -27.91 | ▷ 0.27 | BC 273 |
| | | | | Min $M_z$ | -23.37 | 0.18 | -2.02 | 0.00 | 33.10 | ▷ -0.79 | BC 207 |
| | | 78 | 4345 | Max N | ▷ 1.84 | 0.18 | -1.99 | 0.00 | 33.22 | -0.76 | BC 415 |
| | | | Rechts | Min N | ▷ -109.69 | 0.10 | -1.16 | -0.00 | 17.68 | -0.42 | BC 234 |
| | | | | Max $V_y$ | -23.37 | ▷ 0.18 | -2.02 | 0.00 | 33.10 | -0.79 | BC 207 |
| | | | | Min $V_y$ | -51.03 | ▷ -0.06 | 1.94 | -0.00 | -27.91 | 0.27 | BC 273 |
| | | | | Max $V_z$ | -39.01 | -0.05 | ▷ 1.96 | -0.00 | -27.80 | 0.20 | BC 269 |
| | | | | Min $V_z$ | -35.49 | 0.14 | ▷ -2.04 | 0.00 | 33.02 | -0.63 | BC 175 |
| | | | | Max $M_T$ | -22.52 | 0.14 | -2.03 | ▷ 0.00 | 33.08 | -0.62 | BC 171 |
| | | | | Min $M_T$ | -38.53 | -0.04 | 1.96 | ▷ -0.00 | -27.81 | 0.19 | BC 209 |
| | | | | Max $M_y$ | -0.20 | 0.17 | -1.99 | 0.00 | ▷ 33.23 | -0.73 | BC 447 |
| | | | | Min $M_y$ | -27.54 | -0.05 | 1.92 | -0.00 | ▷ -28.00 | 0.22 | BC 361 |
| | | | | Max $M_z$ | -51.03 | -0.06 | 1.94 | -0.00 | -27.91 | ▷ 0.27 | BC 273 |
| | | | | Min $M_z$ | -23.37 | 0.18 | -2.02 | 0.00 | 33.10 | ▷ -0.79 | BC 207 |
| | | 78 | 4345 | Max N | ▷ 1.84 | 0.18 | -1.99 | 0.00 | 33.22 | -0.76 | BC 415 |
| | | 64 | 0 | Min N | ▷ -117.99 | 0.10 | 9.30 | -0.00 | 0.00 | 0.00 | BC 234 |
| | | 64 | 0 | Max $V_y$ | -31.67 | ▷ 0.18 | 17.26 | 0.00 | -0.00 | 0.00 | BC 207 |
| | | 64 | 0 | Min $V_y$ | -59.33 | ▷ -0.06 | -14.79 | -0.00 | -0.00 | 0.00 | BC 273 |
| | | 64 | 0 | Max $V_z$ | -5.86 | 0.17 | ▷ 17.29 | 0.00 | 0.00 | 0.00 | BC 447 |
| | | 64 | 0 | Min $V_z$ | -33.20 | -0.05 | ▷ -14.81 | -0.00 | 0.00 | 0.00 | BC 361 |
| | | 64 | 0 | Max $M_T$ | -30.82 | 0.14 | 17.25 | ▷ 0.00 | -0.00 | 0.00 | BC 171 |
| | | 64 | 0 | Min $M_T$ | -46.83 | -0.04 | -14.76 | ▷ -0.00 | -0.00 | 0.00 | BC 209 |
| | | | 3950 | Max $M_y$ | -0.99 | 0.17 | -0.24 | 0.00 | ▷ 33.67 | -0.66 | BC 447 |
| | | | 3753 | Min $M_y$ | -28.71 | -0.05 | -0.36 | -0.00 | ▷ -28.46 | 0.19 | BC 361 |
| | | 78 | 4345 | Max $M_z$ | -51.03 | -0.06 | 1.94 | -0.00 | -27.91 | ▷ 0.27 | BC 273 |
| | | 78 | 4345 | Min $M_z$ | -23.37 | 0.18 | -2.02 | 0.00 | 33.10 | ▷ -0.79 | BC 207 |
| 177 | RC1 | 78 | 0 | Max N | ▷ -22.08 | -0.25 | -1.99 | 0.00 | 33.22 | -0.76 | BC 415 |
| | | | | Min N | ▷ -82.85 | -0.18 | 0.07 | -0.00 | 0.30 | -0.10 | BC 146 |
| | | | | Max $V_y$ | -46.30 | ▷ 0.07 | 1.94 | -0.00 | -27.91 | 0.27 | BC 273 |
| | | | | Min $V_y$ | -67.49 | ▷ -0.91 | -1.16 | -0.00 | 17.68 | -0.42 | BC 234 |
| | | | | Max $V_z$ | -46.20 | 0.04 | ▷ 1.96 | -0.00 | -27.80 | 0.20 | BC 269 |
| | | | | Min $V_z$ | -44.87 | -0.20 | ▷ -2.04 | 0.00 | 33.02 | -0.63 | BC 175 |
| | | | | Max $M_T$ | -33.01 | -0.20 | -2.03 | ▷ 0.00 | 33.08 | -0.62 | BC 171 |
| | | | | Min $M_T$ | -46.19 | 0.04 | 1.96 | ▷ -0.00 | -27.81 | 0.19 | BC 209 |
| | | | | Max $M_y$ | -22.11 | -0.24 | -1.99 | 0.00 | ▷ 33.23 | -0.73 | BC 447 |
| | | | | Min $M_y$ | -23.68 | 0.05 | 1.92 | -0.00 | ▷ -28.00 | 0.22 | BC 361 |
| | | | | Max $M_z$ | -46.30 | 0.07 | 1.94 | -0.00 | -27.91 | ▷ 0.27 | BC 273 |
| | | | | Min $M_z$ | -44.73 | -0.25 | -2.02 | 0.00 | 33.10 | ▷ -0.79 | BC 207 |
| | | 65 | 3505 | Max N | ▷ -15.12 | -0.25 | -17.55 | 0.00 | -1.02 | 0.12 | BC 415 |
| | | | | Min N | ▷ -72.64 | -0.18 | 0.07 | -0.00 | 0.55 | 0.52 | BC 146 |
| | | | | Max $V_y$ | -36.09 | ▷ 0.07 | 15.43 | -0.00 | 2.52 | 0.04 | BC 273 |
| | | | | Min $V_y$ | -57.28 | ▷ -0.91 | -9.59 | -0.00 | -1.16 | 2.78 | BC 234 |
| | | | | Max $V_z$ | -35.98 | 0.04 | ▷ 15.46 | -0.00 | 2.72 | 0.05 | BC 269 |
| | | | | Min $V_z$ | -34.66 | -0.20 | ▷ -17.59 | 0.00 | -1.39 | 0.08 | BC 175 |
| | | | | Max $M_T$ | -22.80 | -0.20 | -17.58 | ▷ 0.00 | -1.28 | 0.10 | BC 171 |
| | | | | Min $M_T$ | -35.98 | 0.04 | 15.45 | ▷ -0.00 | 2.71 | 0.05 | BC 209 |
| | | | | Max $M_y$ | -35.98 | 0.04 | 15.46 | -0.00 | ▷ 2.72 | 0.05 | BC 269 |
| | | | | Min $M_y$ | -34.66 | -0.20 | -17.59 | 0.00 | ▷ -1.39 | 0.08 | BC 175 |
| | | | | Max $M_z$ | -57.28 | -0.91 | -9.59 | -0.00 | -1.16 | ▷ 2.78 | BC 234 |
| | | | | Min $M_z$ | -35.09 | 0.02 | -9.59 | -0.00 | -1.14 | ▷ -0.00 | BC 204 |
| | | 65 | 3505 | Max N | ▷ -15.12 | -0.25 | -17.55 | 0.00 | -1.02 | 0.12 | BC 415 |
| | | 78 | 0 | Min N | ▷ -82.85 | -0.18 | 0.07 | -0.00 | 0.30 | -0.10 | BC 146 |
| | | 78 | 0 | Max $V_y$ | -46.30 | ▷ 0.07 | 1.94 | -0.00 | -27.91 | 0.27 | BC 273 |
| | | 78 | 0 | Min $V_y$ | -67.49 | ▷ -0.91 | -1.16 | -0.00 | 17.68 | -0.42 | BC 234 |
| | | 65 | 3505 | Max $V_z$ | -35.98 | 0.04 | ▷ 15.46 | -0.00 | 2.72 | 0.05 | BC 269 |
| | | 65 | 3505 | Min $V_z$ | -34.66 | -0.20 | ▷ -17.59 | 0.00 | -1.39 | 0.08 | BC 175 |
| | | 78 | 0 | Max $M_T$ | -33.01 | -0.20 | -2.03 | ▷ 0.00 | 33.08 | -0.62 | BC 171 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 177 | RC1 | 78 | 0 | Min $M_T$ | -46.19 | 0.04 | 1.96 | ▷ -0.00 | -27.81 | 0.19 | BC 209 |
| | | 78 | 0 | Max $M_y$ | -22.11 | -0.24 | -1.99 | 0.00 | ▷ 33.23 | -0.73 | BC 447 |
| | | 78 | 0 | Min $M_y$ | -23.68 | 0.05 | 1.92 | -0.00 | ▷ -28.00 | 0.22 | BC 361 |
| | | 65 | 3505 | Max $M_z$ | -57.28 | -0.91 | -9.59 | -0.00 | -1.16 | ▷ 2.78 | BC 234 |
| | | 78 | 0 | Min $M_z$ | -44.73 | -0.25 | -2.02 | 0.00 | 33.10 | ▷ -0.79 | BC 207 |
| 22 | RC1 | 78 | 4345 | MAX N | ▷ 1.84 | 0.18 | -1.99 | 0.00 | 33.22 | -0.76 | BC 415 |
| 22 | RC1 | 64 | 0 | MIN N | ▷ -117.99 | 0.10 | 9.30 | 0.00 | 0.00 | 0.00 | BC 234 |
| 22 | RC1 | 64 | 0 | MAX $V_y$ | -31.67 | ▷ 0.18 | 17.26 | 0.00 | 0.00 | 0.00 | BC 207 |
| 177 | RC1 | 78 | 0 | MIN $V_y$ | -67.49 | ▷ -0.91 | -1.16 | 0.00 | 17.68 | -0.42 | BC 234 |
| 22 | RC1 | 64 | 0 | MAX $V_z$ | -5.86 | 0.17 | ▷ 17.29 | 0.00 | 0.00 | 0.00 | BC 447 |
| 177 | RC1 | 65 | 3505 | MIN $V_z$ | -34.66 | -0.20 | ▷ -17.59 | 0.00 | -1.39 | 0.08 | BC 175 |
| 22 | RC1 | 64 | 0 | MAX $M_T$ | -30.82 | 0.14 | 17.25 | ▷ 0.00 | 0.00 | 0.00 | BC 171 |
| 22 | RC1 | 64 | 0 | MIN $M_T$ | -46.83 | -0.04 | -14.76 | ▷ 0.00 | 0.00 | 0.00 | BC 209 |
| 22 | RC1 | | 3950 | MAX $M_y$ | -0.99 | 0.17 | -0.24 | 0.00 | ▷ 33.67 | -0.66 | BC 447 |
| 22 | RC1 | | 3753 | MIN $M_y$ | -28.71 | -0.05 | -0.36 | 0.00 | ▷ -28.46 | 0.19 | BC 361 |
| 177 | RC1 | 65 | 3505 | MAX $M_z$ | -57.28 | -0.91 | -9.59 | 0.00 | -1.16 | ▷ 2.78 | BC 234 |
| 22 | RC1 | 78 | 4345 | MIN $M_z$ | -23.37 | 0.18 | -2.02 | 0.00 | 33.10 | ▷ -0.79 | BC 207 |
| | **Doorgaande staven No. 11: Doorgaande staven 11** | | | | | | | | | | |
| 25 | RC1 | 8 | 0 | Max N | ▷ -23.58 | 5.04 | -5.13 | -0.00 | 0.00 | 0.00 | BC 447 |
| | | | Links | Min N | ▷ -56.21 | 0.00 | -0.15 | 0.00 | 0.00 | 0.00 | BC 138 |
| | | | | Max $V_y$ | -40.28 | ▷ 5.06 | -5.17 | -0.00 | 0.00 | 0.00 | BC 211 |
| | | | | Min $V_y$ | -29.39 | ▷ -6.85 | 4.27 | 0.00 | 0.00 | 0.00 | BC 464 |
| | | | | Max $V_z$ | -23.72 | -6.84 | ▷ 4.29 | 0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Min $V_z$ | -40.28 | 5.05 | ▷ -5.18 | -0.00 | 0.00 | 0.00 | BC 243 |
| | | | | Max $M_T$ | -34.76 | -6.83 | 4.29 | ▷ 0.00 | 0.00 | 0.00 | BC 168 |
| | | | | Min $M_T$ | -23.58 | 5.04 | -5.13 | ▷ -0.00 | 0.00 | 0.00 | BC 475 |
| | | | | Max $M_y$ | -45.17 | 0.00 | -0.16 | 0.00 | ▷ 0.00 | 0.00 | BC 333 |
| | | | | Min $M_y$ | -39.16 | 0.02 | -0.05 | 0.00 | ▷ -0.00 | 0.00 | BC 2 |
| | | | | Max $M_z$ | -40.35 | 0.01 | -0.16 | 0.00 | 0.00 | ▷ 0.00 | BC 91 |
| | | | | Min $M_z$ | -40.64 | -0.03 | -0.17 | 0.00 | 0.00 | ▷ -0.00 | BC 299 |
| | | | 0 | Max N | ▷ -23.58 | 5.04 | -5.13 | -0.00 | -0.00 | -0.00 | BC 447 |
| | | | Rechts | Min N | ▷ -56.21 | 0.00 | -0.15 | 0.00 | -0.00 | -0.00 | BC 138 |
| | | | | Max $V_y$ | -40.28 | ▷ 5.06 | -5.17 | -0.00 | -0.00 | -0.00 | BC 211 |
| | | | | Min $V_y$ | -29.39 | ▷ -6.85 | 4.27 | 0.00 | 0.00 | 0.00 | BC 464 |
| | | | | Max $V_z$ | -23.72 | -6.84 | ▷ 4.29 | 0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Min $V_z$ | -40.28 | 5.05 | ▷ -5.18 | -0.00 | -0.00 | 0.00 | BC 243 |
| | | | | Max $M_T$ | -34.76 | -6.83 | 4.29 | ▷ 0.00 | 0.00 | 0.00 | BC 168 |
| | | | | Min $M_T$ | -23.58 | 5.04 | -5.13 | ▷ -0.00 | -0.00 | -0.00 | BC 475 |
| | | | | Max $M_y$ | -23.72 | -6.84 | 4.29 | 0.00 | ▷ 0.00 | 0.00 | BC 360 |
| | | | | Min $M_y$ | -40.28 | 5.05 | -5.18 | -0.00 | ▷ -0.00 | -0.00 | BC 243 |
| | | | | Max $M_z$ | -29.39 | -6.85 | 4.27 | 0.00 | 0.00 | ▷ 0.00 | BC 464 |
| | | | | Min $M_z$ | -40.28 | 5.06 | -5.17 | -0.00 | -0.00 | ▷ -0.00 | BC 211 |
| | | | 2500 | Max N | ▷ -21.59 | -2.00 | 1.82 | -0.00 | -4.14 | -3.80 | BC 447 |
| | | | Links | Min N | ▷ -53.29 | 0.00 | -0.15 | 0.00 | -0.37 | -0.01 | BC 138 |
| | | | | Max $V_y$ | -31.83 | ▷ 2.96 | -0.45 | 0.00 | 4.74 | 4.82 | BC 220 |
| | | | | Min $V_y$ | -21.59 | ▷ -2.02 | 1.87 | -0.00 | -4.01 | -3.75 | BC 423 |
| | | | | Max $V_z$ | -21.59 | -2.01 | ▷ 1.88 | -0.00 | -4.00 | -3.76 | BC 363 |
| | | | | Min $V_z$ | -37.50 | 2.94 | ▷ -0.47 | 0.00 | 4.70 | 4.86 | BC 240 |
| | | | | Max $M_T$ | -31.84 | 2.94 | -0.42 | ▷ 0.00 | 4.84 | 4.86 | BC 168 |
| | | | | Min $M_T$ | -21.59 | -1.99 | 1.82 | ▷ -0.00 | -4.14 | -3.81 | BC 475 |
| | | | | Max $M_y$ | -21.73 | 2.94 | -0.41 | 0.00 | ▷ 4.85 | 4.87 | BC 360 |
| | | | | Min $M_y$ | -37.37 | 1.64 | -0.28 | 0.00 | ▷ -4.38 | 2.67 | BC 269 |
| | | | | Max $M_z$ | -27.39 | 2.92 | -0.43 | 0.00 | 4.80 | ▷ 4.91 | BC 464 |
| | | | | Min $M_z$ | -37.36 | -1.98 | 1.78 | -0.00 | -4.23 | ▷ -3.85 | BC 211 |
| | | | 2500 | Max N | ▷ -21.59 | -2.00 | 1.82 | -0.00 | -4.14 | -3.80 | BC 447 |
| | | | Rechts | Min N | ▷ -53.29 | 0.00 | -0.15 | 0.00 | -0.37 | -0.01 | BC 138 |
| | | | | Max $V_y$ | -31.83 | ▷ 2.96 | -0.45 | 0.00 | 4.74 | 4.82 | BC 220 |
| | | | | Min $V_y$ | -21.59 | ▷ -2.02 | 1.87 | -0.00 | -4.01 | -3.75 | BC 423 |
| | | | | Max $V_z$ | -21.59 | -2.01 | ▷ 1.88 | -0.00 | -4.00 | -3.76 | BC 363 |
| | | | | Min $V_z$ | -37.50 | 2.94 | ▷ -0.47 | 0.00 | 4.70 | 4.86 | BC 240 |
| | | | | Max $M_T$ | -31.84 | 2.94 | -0.42 | ▷ 0.00 | 4.84 | 4.86 | BC 168 |
| | | | | Min $M_T$ | -21.59 | -1.99 | 1.82 | ▷ -0.00 | -4.14 | -3.81 | BC 475 |
| | | | | Max $M_y$ | -21.73 | 2.94 | -0.41 | 0.00 | ▷ 4.85 | 4.87 | BC 360 |
| | | | | Min $M_y$ | -37.37 | 1.64 | -0.28 | 0.00 | ▷ -4.38 | 2.67 | BC 269 |
| | | | | Max $M_z$ | -27.39 | 2.92 | -0.43 | 0.00 | 4.80 | ▷ 4.91 | BC 464 |
| | | | | Min $M_z$ | -37.36 | -1.98 | 1.78 | -0.00 | -4.23 | ▷ -3.85 | BC 211 |
| | | | 4345 | Max N | ▷ -17.44 | -7.19 | 6.95 | -0.00 | 3.94 | 4.68 | BC 447 |
| | | | Links | Min N | ▷ -47.21 | 0.00 | -0.15 | 0.00 | -0.64 | -0.02 | BC 138 |
| | | | | Max $V_y$ | -25.76 | ▷ 10.17 | -3.92 | 0.00 | 0.70 | -7.30 | BC 220 |
| | | | | Min $V_y$ | -17.45 | ▷ -7.21 | 7.00 | -0.00 | 4.18 | 4.76 | BC 423 |
| | | | | Max $V_z$ | -17.45 | -7.20 | ▷ 7.01 | -0.00 | 4.20 | 4.74 | BC 363 |
| | | | | Min $V_z$ | -31.42 | 10.16 | ▷ -3.94 | 0.00 | 0.63 | -7.23 | BC 240 |
| | | | | Max $M_T$ | -25.76 | 10.16 | -3.89 | ▷ 0.00 | 0.87 | -7.22 | BC 168 |
| | | | | Min $M_T$ | -17.44 | -7.18 | 6.95 | ▷ -0.00 | 3.95 | 4.65 | BC 475 |
| | | | | Max $M_y$ | -17.45 | -7.20 | 7.01 | -0.00 | ▷ 4.20 | 4.74 | BC 363 |
| | | | | Min $M_y$ | -31.30 | 5.63 | 1.88 | 0.00 | ▷ -2.91 | -4.04 | BC 269 |
| | | | | Max $M_z$ | -17.45 | -7.21 | 7.00 | -0.00 | 4.18 | ▷ 4.76 | BC 423 |
| | | | | Min $M_z$ | -25.76 | 10.17 | -3.92 | 0.00 | 0.70 | ▷ -7.30 | BC 220 |
| | | 16 | 4345 | Max N | ▷ -17.44 | -7.19 | 6.95 | -0.00 | 3.94 | 4.68 | BC 447 |
| | | | Rechts | Min N | ▷ -47.21 | 0.00 | -0.15 | 0.00 | -0.64 | -0.02 | BC 138 |
| | | | | Max $V_y$ | -25.76 | ▷ 10.17 | -3.92 | 0.00 | 0.70 | -7.30 | BC 220 |
| | | | | Min $V_y$ | -17.45 | ▷ -7.21 | 7.00 | -0.00 | 4.18 | 4.76 | BC 423 |
| | | | | Max $V_z$ | -17.45 | -7.20 | ▷ 7.01 | -0.00 | 4.20 | 4.74 | BC 363 |
| | | | | Min $V_z$ | -31.42 | 10.16 | ▷ -3.94 | 0.00 | 0.63 | -7.23 | BC 240 |
| | | | | Max $M_T$ | -25.76 | 10.16 | -3.89 | ▷ 0.00 | 0.87 | -7.22 | BC 168 |
| | | | | Min $M_T$ | -17.44 | -7.18 | 6.95 | ▷ -0.00 | 3.95 | 4.65 | BC 475 |
| | | | | Max $M_y$ | -17.45 | -7.20 | 7.01 | -0.00 | ▷ 4.20 | 4.74 | BC 363 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 25 | RC1 | | | Min $M_y$ | -31.30 | 5.63 | 1.88 | 0.00 | ▷ -2.91 | -4.04 | BC 269 |
| | | | | Max $M_z$ | -17.45 | -7.21 | 7.00 | -0.00 | 4.18 | ▷ 4.76 | BC 423 |
| | | | | Min $M_z$ | -25.76 | 10.17 | -3.92 | 0.00 | 0.70 | ▷ -7.30 | BC 220 |
| | | 16 | 4345 | Max N | ▷ -17.44 | -7.19 | 6.95 | -0.00 | 3.94 | 4.68 | BC 447 |
| | | 8 | 0 | Min N | ▷ -56.21 | 0.00 | -0.15 | 0.00 | 0.00 | 0.00 | BC 138 |
| | | 16 | 4345 | Max $V_y$ | -25.76 | ▷ 10.17 | -3.92 | 0.00 | 0.70 | -7.30 | BC 220 |
| | | 16 | 4345 | Min $V_y$ | -17.45 | ▷ -7.21 | 7.00 | -0.00 | 4.18 | 4.76 | BC 423 |
| | | 16 | 4345 | Max $V_z$ | -17.45 | -7.20 | ▷ 7.01 | -0.00 | 4.20 | 4.74 | BC 363 |
| | | 8 | 0 | Min $V_z$ | -40.28 | 5.05 | ▷ -5.18 | -0.00 | 0.00 | 0.00 | BC 243 |
| | | | 2500 | Max $M_T$ | -31.84 | 2.94 | -0.42 | ▷ 0.00 | 4.84 | 4.86 | BC 168 |
| | | | 2500 | Min $M_T$ | -21.59 | -1.99 | 1.82 | ▷ -0.00 | -4.14 | -3.81 | BC 475 |
| | | | 2308 | Max $M_y$ | -21.88 | 2.19 | -0.05 | 0.00 | ▷ 4.89 | 5.36 | BC 360 |
| | | | 1923 | Min $M_y$ | -38.03 | -0.36 | 0.17 | -0.00 | ▷ -4.81 | -4.50 | BC 243 |
| | | | 1731 | Max $M_z$ | -28.01 | -0.08 | 1.01 | 0.00 | 4.57 | ▷ 6.00 | BC 464 |
| | | 16 | 4345 | Min $M_z$ | -25.76 | 10.17 | -3.92 | 0.00 | 0.70 | ▷ -7.30 | BC 220 |
| 140 | RC1 | 16 | 0 | Max N | ▷ -15.73 | 6.17 | -5.88 | -0.00 | 3.94 | 4.68 | BC 447 |
| | | | Links | Min N | ▷ -44.70 | -0.01 | 0.17 | 0.00 | -0.64 | -0.02 | BC 138 |
| | | | | Max $V_y$ | -15.74 | ▷ 6.19 | -5.95 | -0.00 | 4.18 | 4.76 | BC 423 |
| | | | | Min $V_y$ | -23.25 | ▷ -8.81 | 2.97 | 0.00 | 0.70 | -7.30 | BC 220 |
| | | | | Max $V_z$ | -28.91 | -8.79 | ▷ 2.99 | 0.00 | 0.63 | -7.23 | BC 240 |
| | | | | Min $V_z$ | -15.74 | 6.19 | ▷ -5.95 | -0.00 | 4.20 | 4.74 | BC 363 |
| | | | | Max $M_T$ | -23.25 | -8.78 | 2.92 | ▷ 0.00 | 0.87 | -7.22 | BC 168 |
| | | | | Min $M_T$ | -15.73 | 6.16 | -5.88 | ▷ -0.00 | 3.95 | 4.65 | BC 475 |
| | | | | Max $M_y$ | -15.74 | 6.19 | -5.95 | -0.00 | ▷ 4.20 | 4.74 | BC 363 |
| | | | | Min $M_y$ | -28.79 | -4.88 | -1.14 | 0.00 | ▷ -2.91 | -4.04 | BC 269 |
| | | | | Max $M_z$ | -15.74 | 6.19 | -5.95 | -0.00 | 4.18 | ▷ 4.76 | BC 423 |
| | | | | Min $M_z$ | -23.25 | -8.81 | 2.97 | 0.00 | 0.70 | ▷ -7.30 | BC 220 |
| | | | 0 | Max N | ▷ -15.73 | 6.17 | -5.88 | -0.00 | 3.94 | 4.68 | BC 447 |
| | | | Rechts | Min N | ▷ -44.70 | -0.01 | 0.17 | 0.00 | -0.64 | -0.02 | BC 138 |
| | | | | Max $V_y$ | -15.74 | ▷ 6.19 | -5.95 | -0.00 | 4.18 | 4.76 | BC 423 |
| | | | | Min $V_y$ | -23.25 | ▷ -8.81 | 2.97 | 0.00 | 0.70 | -7.30 | BC 220 |
| | | | | Max $V_z$ | -28.91 | -8.79 | ▷ 2.99 | 0.00 | 0.63 | -7.23 | BC 240 |
| | | | | Min $V_z$ | -15.74 | 6.19 | ▷ -5.95 | -0.00 | 4.20 | 4.74 | BC 363 |
| | | | | Max $M_T$ | -23.25 | -8.78 | 2.92 | ▷ 0.00 | 0.87 | -7.22 | BC 168 |
| | | | | Min $M_T$ | -15.73 | 6.16 | -5.88 | ▷ -0.00 | 3.95 | 4.65 | BC 475 |
| | | | | Max $M_y$ | -15.74 | 6.19 | -5.95 | -0.00 | ▷ 4.20 | 4.74 | BC 363 |
| | | | | Min $M_y$ | -28.79 | -4.88 | -1.14 | 0.00 | ▷ -2.91 | -4.04 | BC 269 |
| | | | | Max $M_z$ | -15.74 | 6.19 | -5.95 | -0.00 | 4.18 | ▷ 4.76 | BC 423 |
| | | | | Min $M_z$ | -23.25 | -8.81 | 2.97 | 0.00 | 0.70 | ▷ -7.30 | BC 220 |
| | | | 3505 | Max N | ▷ -7.84 | -3.69 | 3.87 | -0.00 | 0.42 | 0.33 | BC 447 |
| | | | Links | Min N | ▷ -33.13 | -0.01 | 0.17 | 0.00 | -0.05 | -0.00 | BC 138 |
| | | | | Max $V_y$ | -13.65 | ▷ 4.94 | -3.65 | 0.00 | -0.44 | -0.45 | BC 464 |
| | | | | Min $V_y$ | -17.20 | ▷ -3.72 | 3.90 | -0.00 | 0.41 | 0.33 | BC 211 |
| | | | | Max $V_z$ | -17.20 | -3.70 | ▷ 3.92 | -0.00 | 0.41 | 0.33 | BC 243 |
| | | | | Min $V_z$ | -7.98 | 4.93 | ▷ -3.67 | 0.00 | -0.43 | -0.45 | BC 360 |
| | | | | Max $M_T$ | -11.68 | 4.92 | -3.67 | ▷ 0.00 | -0.44 | -0.45 | BC 168 |
| | | | | Min $M_T$ | -7.84 | -3.70 | 3.86 | ▷ -0.00 | 0.42 | 0.33 | BC 475 |
| | | | | Max $M_y$ | -7.84 | -3.69 | 3.87 | -0.00 | ▷ 0.42 | 0.33 | BC 447 |
| | | | | Min $M_y$ | -17.34 | 4.92 | -3.66 | 0.00 | ▷ -0.45 | -0.45 | BC 172 |
| | | | | Max $M_z$ | -11.53 | -3.71 | 3.88 | -0.00 | 0.41 | ▷ 0.33 | BC 223 |
| | | | | Min $M_z$ | -13.65 | 4.94 | -3.66 | 0.00 | -0.44 | ▷ -0.45 | BC 392 |
| | | 56 | 3505 | Max N | ▷ -7.84 | -3.69 | 3.87 | -0.00 | 0.42 | 0.33 | BC 447 |
| | | | Rechts | Min N | ▷ -33.13 | -0.01 | 0.17 | 0.00 | -0.05 | -0.00 | BC 138 |
| | | | | Max $V_y$ | -13.65 | ▷ 4.94 | -3.65 | 0.00 | -0.44 | -0.45 | BC 464 |
| | | | | Min $V_y$ | -17.20 | ▷ -3.72 | 3.90 | -0.00 | 0.41 | 0.33 | BC 211 |
| | | | | Max $V_z$ | -17.20 | -3.70 | ▷ 3.92 | -0.00 | 0.41 | 0.33 | BC 243 |
| | | | | Min $V_z$ | -7.98 | 4.93 | ▷ -3.67 | 0.00 | -0.43 | -0.45 | BC 360 |
| | | | | Max $M_T$ | -11.68 | 4.92 | -3.67 | ▷ 0.00 | -0.44 | -0.45 | BC 168 |
| | | | | Min $M_T$ | -7.84 | -3.70 | 3.86 | ▷ -0.00 | 0.42 | 0.33 | BC 475 |
| | | | | Max $M_y$ | -7.84 | -3.69 | 3.87 | -0.00 | ▷ 0.42 | 0.33 | BC 447 |
| | | | | Min $M_y$ | -17.34 | 4.92 | -3.66 | 0.00 | ▷ -0.45 | -0.45 | BC 172 |
| | | | | Max $M_z$ | -11.53 | -3.71 | 3.88 | -0.00 | 0.41 | ▷ 0.33 | BC 223 |
| | | | | Min $M_z$ | -13.65 | 4.94 | -3.66 | 0.00 | -0.44 | ▷ -0.45 | BC 392 |
| | | 56 | 3505 | Max N | ▷ -7.84 | -3.69 | 3.87 | -0.00 | 0.42 | 0.33 | BC 447 |
| | | 16 | 0 | Min N | ▷ -44.70 | -0.01 | 0.17 | 0.00 | -0.64 | -0.02 | BC 138 |
| | | 16 | 0 | Max $V_y$ | -15.74 | ▷ 6.19 | -5.95 | -0.00 | 4.18 | 4.76 | BC 423 |
| | | 16 | 0 | Min $V_y$ | -23.25 | ▷ -8.81 | 2.97 | 0.00 | 0.70 | -7.30 | BC 220 |
| | | 56 | 3505 | Max $V_z$ | -17.20 | -3.70 | ▷ 3.92 | -0.00 | 0.41 | 0.33 | BC 243 |
| | | 16 | 0 | Min $V_z$ | -15.74 | 6.19 | ▷ -5.95 | -0.00 | 4.20 | 4.74 | BC 363 |
| | | 16 | 0 | Max $M_T$ | -23.25 | -8.78 | 2.92 | ▷ 0.00 | 0.87 | -7.22 | BC 168 |
| | | 16 | 0 | Min $M_T$ | -15.73 | 6.16 | -5.88 | ▷ -0.00 | 3.95 | 4.65 | BC 475 |
| | | 16 | 0 | Max $M_y$ | -15.74 | 6.19 | -5.95 | -0.00 | ▷ 4.20 | 4.74 | BC 363 |
| | | | 974 | Min $M_y$ | -25.58 | -2.77 | 0.00 | 0.00 | ▷ -3.46 | -0.32 | BC 269 |
| | | 16 | 0 | Max $M_z$ | -15.74 | 6.19 | -5.95 | -0.00 | 4.18 | ▷ 4.76 | BC 423 |
| | | 16 | 0 | Min $M_z$ | -23.25 | -8.81 | 2.97 | 0.00 | 0.70 | ▷ -7.30 | BC 220 |
| 140 | RC1 | 56 | 3505 | MAX N | ▷ -7.84 | -3.69 | 3.87 | 0.00 | 0.42 | 0.33 | BC 447 |
| 25 | RC1 | 8 | 0 | MIN N | ▷ -56.21 | 0.00 | -0.15 | 0.00 | 0.00 | 0.00 | BC 138 |
| 25 | RC1 | 16 | 4345 | MAX $V_y$ | -25.76 | ▷ 10.17 | -3.92 | 0.00 | 0.70 | -7.30 | BC 220 |
| 140 | RC1 | 16 | 0 | MIN $V_y$ | -23.25 | ▷ -8.81 | 2.97 | 0.00 | 0.70 | -7.30 | BC 220 |
| 25 | RC1 | 16 | 4345 | MAX $V_z$ | -17.45 | -7.20 | ▷ 7.01 | 0.00 | 4.20 | 4.74 | BC 363 |
| 140 | RC1 | 16 | 0 | MIN $V_z$ | -15.74 | 6.19 | ▷ -5.95 | 0.00 | 4.20 | 4.74 | BC 363 |
| 25 | RC1 | | 2500 | MAX $M_T$ | -31.84 | 2.94 | -0.42 | ▷ 0.00 | 4.84 | 4.86 | BC 168 |
| 25 | RC1 | | 2500 | MIN $M_T$ | -21.59 | -1.99 | 1.82 | ▷ 0.00 | -4.14 | -3.81 | BC 475 |
| 25 | RC1 | | 2308 | MAX $M_y$ | -21.88 | 2.19 | -0.05 | 0.00 | ▷ 4.89 | 5.36 | BC 360 |
| 25 | RC1 | | 1923 | MIN $M_y$ | -38.03 | -0.36 | 0.17 | 0.00 | ▷ -4.81 | -4.50 | BC 243 |
| 25 | RC1 | | 1731 | MAX $M_z$ | -28.01 | -0.08 | 1.01 | 0.00 | 4.57 | ▷ 6.00 | BC 464 |
| 140 | RC1 | 16 | 0 | MIN $M_z$ | -23.25 | -8.81 | 2.97 | 0.00 | 0.70 | ▷ -7.30 | BC 220 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| **140** | **Doorgaande staven No. 12: Doorgaande staven 12** | | | | | | | | | | |
| 26 | RC1 | 7 | 0 | Max N | ▷ -6.36 | -6.97 | -4.99 | -0.00 | 0.00 | 0.00 | BC 445 |
| | | | | Min N | ▷ -53.69 | 0.02 | -0.46 | -0.00 | 0.00 | 0.00 | BC 138 |
| | | | | Max $V_y$ | -33.83 | ▷ 5.20 | 4.34 | 0.00 | 0.00 | -0.00 | BC 207 |
| | | | | Min $V_y$ | -11.51 | ▷ -6.98 | -5.04 | -0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Max $V_z$ | -22.63 | 5.16 | ▷ 4.80 | 0.00 | -0.00 | 0.00 | BC 359 |
| | | | | Min $V_z$ | -21.51 | -6.97 | ▷ -5.16 | -0.00 | 0.00 | -0.00 | BC 241 |
| | | | | Max $M_T$ | -32.10 | 5.17 | 4.65 | ▷ 0.00 | 0.00 | 0.00 | BC 231 |
| | | | | Min $M_T$ | -21.59 | -6.97 | -5.16 | ▷ -0.00 | 0.00 | -0.00 | BC 269 |
| | | | | Max $M_y$ | -7.32 | -6.97 | -4.93 | -0.00 | ▷ 0.00 | -0.00 | BC 381 |
| | | | | Min $M_y$ | -26.86 | -3.18 | 1.44 | -0.00 | ▷ -0.00 | -0.00 | BC 190 |
| | | | | Max $M_z$ | -44.17 | -3.87 | 2.34 | -0.00 | 0.00 | ▷ 0.00 | BC 268 |
| | | | | Min $M_z$ | -26.86 | -3.18 | 1.44 | -0.00 | -0.00 | ▷ -0.00 | BC 190 |
| | | | 2500 | Max N | ▷ -4.36 | 3.01 | -0.28 | -0.00 | -6.59 | 4.95 | BC 445 |
| | | | Links | Min N | ▷ -50.76 | 0.02 | -0.46 | -0.00 | -1.15 | -0.06 | BC 138 |
| | | | | Max $V_y$ | -14.47 | ▷ 3.03 | -0.34 | -0.00 | -6.73 | 4.91 | BC 217 |
| | | | | Min $V_y$ | -19.79 | ▷ -2.06 | -2.20 | 0.00 | 3.19 | -3.87 | BC 451 |
| | | | | Max $V_z$ | -10.67 | 3.02 | ▷ 0.14 | -0.00 | -5.52 | 4.92 | BC 357 |
| | | | | Min $V_z$ | -29.76 | -2.03 | ▷ -2.68 | 0.00 | 1.98 | -3.95 | BC 243 |
| | | | | Max $M_T$ | -29.85 | -2.05 | -2.25 | ▷ 0.00 | 3.06 | -3.90 | BC 171 |
| | | | | Min $M_T$ | -18.66 | 3.01 | -0.46 | ▷ -0.00 | -7.02 | 4.95 | BC 269 |
| | | | | Max $M_y$ | -20.63 | -2.05 | -2.15 | 0.00 | ▷ 3.32 | -3.89 | BC 359 |
| | | | | Min $M_y$ | -18.58 | 3.01 | -0.46 | -0.00 | ▷ -7.02 | 4.96 | BC 241 |
| | | | | Max $M_z$ | -9.51 | 3.00 | -0.34 | -0.00 | -6.73 | ▷ 4.97 | BC 433 |
| | | | | Min $M_z$ | -30.90 | -2.02 | -2.61 | 0.00 | 2.16 | ▷ -3.97 | BC 207 |
| | | | 2500 | Max N | ▷ -4.36 | 3.01 | -0.28 | -0.00 | -6.59 | 4.95 | BC 445 |
| | | | Rechts | Min N | ▷ -50.76 | 0.02 | -0.46 | -0.00 | -1.15 | -0.06 | BC 138 |
| | | | | Max $V_y$ | -14.47 | ▷ 3.03 | -0.34 | -0.00 | -6.73 | 4.91 | BC 217 |
| | | | | Min $V_y$ | -19.79 | ▷ -2.06 | -2.20 | 0.00 | 3.19 | -3.87 | BC 451 |
| | | | | Max $V_z$ | -10.67 | 3.02 | ▷ 0.14 | -0.00 | -5.52 | 4.92 | BC 357 |
| | | | | Min $V_z$ | -29.76 | -2.03 | ▷ -2.68 | 0.00 | 1.98 | -3.95 | BC 243 |
| | | | | Max $M_T$ | -29.18 | -2.05 | -2.30 | ▷ 0.00 | 2.94 | -3.90 | BC 231 |
| | | | | Min $M_T$ | -18.66 | 3.01 | -0.46 | ▷ -0.00 | -7.02 | 4.95 | BC 269 |
| | | | | Max $M_y$ | -20.63 | -2.05 | -2.15 | 0.00 | ▷ 3.32 | -3.89 | BC 359 |
| | | | | Min $M_y$ | -18.58 | 3.01 | -0.46 | -0.00 | ▷ -7.02 | 4.96 | BC 241 |
| | | | | Max $M_z$ | -9.51 | 3.00 | -0.34 | -0.00 | -6.73 | ▷ 4.97 | BC 433 |
| | | | | Min $M_z$ | -30.90 | -2.02 | -2.61 | 0.00 | 2.16 | ▷ -3.97 | BC 207 |
| | | | 4345 | Max N | ▷ -0.19 | 10.38 | 3.19 | -0.00 | -3.91 | -7.41 | BC 445 |
| | | | Links | Min N | ▷ -44.64 | 0.02 | -0.46 | -0.00 | -1.99 | -0.11 | BC 138 |
| | | | | Max $V_y$ | -8.35 | ▷ 10.40 | 3.13 | -0.00 | -4.15 | -7.47 | BC 217 |
| | | | | Min $V_y$ | -15.61 | ▷ -7.39 | -7.33 | 0.00 | -5.61 | 4.85 | BC 451 |
| | | | | Max $V_z$ | -6.49 | 10.39 | ▷ 3.61 | -0.00 | -2.06 | -7.46 | BC 357 |
| | | | | Min $V_z$ | -23.63 | -7.35 | ▷ -7.81 | 0.00 | -7.70 | 4.71 | BC 243 |
| | | | | Max $M_T$ | -23.05 | -7.37 | -7.43 | ▷ 0.00 | -6.04 | 4.79 | BC 231 |
| | | | | Min $M_T$ | -12.53 | 10.38 | 3.01 | ▷ -0.00 | -4.66 | -7.41 | BC 269 |
| | | | | Max $M_y$ | -29.00 | 5.83 | -2.41 | -0.00 | ▷ 0.61 | -4.25 | BC 360 |
| | | | | Min $M_y$ | -23.63 | -7.35 | -7.81 | 0.00 | ▷ -7.70 | 4.71 | BC 243 |
| | | | | Max $M_z$ | -15.61 | -7.39 | -7.33 | 0.00 | -5.61 | ▷ 4.85 | BC 451 |
| | | | | Min $M_z$ | -8.35 | 10.40 | 3.13 | -0.00 | -4.15 | ▷ -7.47 | BC 217 |
| | | 17 | 4345 | Max N | ▷ -0.19 | 10.38 | 3.19 | -0.00 | -3.91 | -7.41 | BC 445 |
| | | | Rechts | Min N | ▷ -44.64 | 0.02 | -0.46 | -0.00 | -1.99 | -0.11 | BC 138 |
| | | | | Max $V_y$ | -8.35 | ▷ 10.40 | 3.13 | -0.00 | -4.15 | -7.47 | BC 217 |
| | | | | Min $V_y$ | -15.61 | ▷ -7.39 | -7.33 | 0.00 | -5.61 | 4.85 | BC 451 |
| | | | | Max $V_z$ | -6.49 | 10.39 | ▷ 3.61 | -0.00 | -2.06 | -7.46 | BC 357 |
| | | | | Min $V_z$ | -23.63 | -7.35 | ▷ -7.81 | 0.00 | -7.70 | 4.71 | BC 243 |
| | | | | Max $M_T$ | -23.05 | -7.37 | -7.43 | ▷ 0.00 | -6.04 | 4.79 | BC 231 |
| | | | | Min $M_T$ | -12.53 | 10.38 | 3.01 | ▷ -0.00 | -4.66 | -7.41 | BC 269 |
| | | | | Max $M_y$ | -29.00 | 5.83 | -2.41 | -0.00 | ▷ 0.61 | -4.25 | BC 360 |
| | | | | Min $M_y$ | -23.63 | -7.35 | -7.81 | 0.00 | ▷ -7.70 | 4.71 | BC 243 |
| | | | | Max $M_z$ | -15.61 | -7.39 | -7.33 | 0.00 | -5.61 | ▷ 4.85 | BC 451 |
| | | | | Min $M_z$ | -8.35 | 10.40 | 3.13 | -0.00 | -4.15 | ▷ -7.47 | BC 217 |
| | | 17 | 4345 | Max N | ▷ -0.19 | 10.38 | 3.19 | -0.00 | -3.91 | -7.41 | BC 445 |
| | | 7 | 0 | Min N | ▷ -53.69 | 0.02 | -0.46 | -0.00 | 0.00 | 0.00 | BC 138 |
| | | 17 | 4345 | Max $V_y$ | -8.35 | ▷ 10.40 | 3.13 | -0.00 | -4.15 | -7.47 | BC 217 |
| | | 17 | 4345 | Min $V_y$ | -15.61 | ▷ -7.39 | -7.33 | 0.00 | -5.61 | 4.85 | BC 451 |
| | | 7 | 0 | Max $V_z$ | -22.63 | 5.16 | ▷ 4.80 | 0.00 | -0.00 | 0.00 | BC 359 |
| | | 17 | 4345 | Min $V_z$ | -23.63 | -7.35 | ▷ -7.81 | 0.00 | -7.70 | 4.71 | BC 243 |
| | | | 2308 | Max $M_T$ | -30.08 | -1.49 | -1.72 | ▷ 0.00 | 3.44 | -4.24 | BC 171 |
| | | | 2308 | Min $M_T$ | -18.88 | 2.24 | -0.82 | ▷ -0.00 | -6.90 | 5.45 | BC 269 |
| | | | 1731 | Max $M_y$ | -21.24 | 0.17 | -0.01 | 0.00 | ▷ 4.15 | -4.61 | BC 359 |
| | | 17 | 4345 | Min $M_y$ | -23.63 | -7.35 | -7.81 | 0.00 | ▷ -7.70 | 4.71 | BC 243 |
| | | | 1731 | Max $M_z$ | -10.12 | -0.07 | -1.79 | -0.00 | -5.91 | ▷ 6.10 | BC 433 |
| | | 17 | 4345 | Min $M_z$ | -8.35 | 10.40 | 3.13 | -0.00 | -4.15 | ▷ -7.47 | BC 217 |
| 80 | RC1 | 17 | 0 | Max N | ▷ -16.34 | 6.32 | 6.79 | 0.00 | -7.03 | 4.78 | BC 447 |
| | | | Links | Min N | ▷ -46.20 | -0.03 | 0.62 | -0.00 | -1.99 | -0.11 | BC 138 |
| | | | | Max $V_y$ | -16.39 | ▷ 6.34 | 6.37 | 0.00 | -5.61 | 4.85 | BC 451 |
| | | | | Min $V_y$ | -24.15 | ▷ -9.00 | -1.96 | -0.00 | -4.15 | -7.47 | BC 217 |
| | | | | Max $V_z$ | -29.83 | 6.30 | ▷ 6.99 | 0.00 | -7.70 | 4.71 | BC 243 |
| | | | | Min $V_z$ | -16.51 | -8.99 | ▷ -2.58 | -0.00 | -2.06 | -7.46 | BC 357 |
| | | | | Max $M_T$ | -24.09 | 6.32 | 6.50 | ▷ 0.00 | -6.04 | 4.79 | BC 231 |
| | | | | Min $M_T$ | -29.93 | -8.98 | -1.81 | ▷ -0.00 | -4.66 | -7.41 | BC 269 |
| | | | | Max $M_y$ | -26.98 | -5.05 | 2.44 | -0.00 | ▷ 0.61 | -4.25 | BC 360 |
| | | | | Min $M_y$ | -29.83 | 6.30 | 6.99 | 0.00 | ▷ -7.70 | 4.71 | BC 243 |
| | | | | Max $M_z$ | -16.39 | 6.34 | 6.37 | 0.00 | -5.61 | ▷ 4.85 | BC 451 |
| | | | | Min $M_z$ | -24.15 | -9.00 | -1.96 | -0.00 | -4.15 | ▷ -7.47 | BC 217 |
| | | | 0 | Max N | ▷ -16.34 | 6.32 | 6.79 | 0.00 | -7.03 | 4.78 | BC 447 |
| | | | Rechts | Min N | ▷ -46.20 | -0.03 | 0.62 | -0.00 | -1.99 | -0.11 | BC 138 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 80 | RC1 | | | Max $V_y$ | -16.39 | ▷ 6.34 | 6.37 | 0.00 | -5.61 | 4.85 | BC 451 |
| | | | | Min $V_y$ | -24.15 | ▷ -9.00 | -1.96 | -0.00 | -4.15 | -7.47 | BC 217 |
| | | | | Max $V_z$ | -29.83 | 6.30 | ▷ 6.99 | 0.00 | -7.70 | 4.71 | BC 243 |
| | | | | Min $V_z$ | -16.51 | -8.99 | ▷ -2.58 | -0.00 | -2.06 | -7.46 | BC 357 |
| | | | | Max $M_T$ | -24.09 | 6.32 | 6.50 | ▷ 0.00 | -6.04 | 4.79 | BC 231 |
| | | | | Min $M_T$ | -29.93 | -8.98 | -1.81 | ▷ -0.00 | -4.66 | -7.41 | BC 269 |
| | | | | Max $M_y$ | -26.98 | -5.05 | 2.44 | -0.00 | ▷ 0.61 | -4.25 | BC 360 |
| | | | | Min $M_y$ | -29.83 | 6.30 | 6.99 | 0.00 | ▷ -7.70 | 4.71 | BC 243 |
| | | | | Max $M_z$ | -16.39 | 6.34 | 6.37 | 0.00 | -5.61 | ▷ 4.85 | BC 451 |
| | | | | Min $M_z$ | -24.15 | -9.00 | -1.96 | -0.00 | -4.15 | ▷ -7.47 | BC 217 |
| | | | 3505 | Max N | ▷ -8.35 | -3.80 | -2.96 | 0.00 | -0.32 | 0.35 | BC 447 |
| | | | Links | Min N | ▷ -34.49 | -0.03 | 0.62 | -0.00 | 0.20 | 0.00 | BC 138 |
| | | | | Max $V_y$ | -14.24 | ▷ 5.03 | 4.63 | -0.00 | 0.53 | -0.47 | BC 433 |
| | | | | Min $V_y$ | -18.13 | ▷ -3.83 | -2.84 | 0.00 | -0.27 | 0.36 | BC 207 |
| | | | | Max $V_z$ | -18.21 | 5.02 | ▷ 4.79 | -0.00 | 0.56 | -0.47 | BC 241 |
| | | | | Min $V_z$ | -8.41 | -3.79 | ▷ -3.44 | 0.00 | -0.36 | 0.35 | BC 359 |
| | | | | Max $M_T$ | -12.38 | -3.79 | -3.24 | ▷ 0.00 | -0.33 | 0.35 | BC 231 |
| | | | | Min $M_T$ | -18.21 | 5.02 | 4.79 | ▷ -0.00 | 0.56 | -0.47 | BC 269 |
| | | | | Max $M_y$ | -19.02 | 2.77 | -1.67 | -0.00 | ▷ 1.95 | -0.25 | BC 356 |
| | | | | Min $M_y$ | -8.41 | -3.79 | -3.44 | 0.00 | ▷ -0.36 | 0.35 | BC 359 |
| | | | | Max $M_z$ | -18.13 | -3.83 | -2.84 | 0.00 | -0.27 | ▷ 0.36 | BC 207 |
| | | | | Min $M_z$ | -14.24 | 5.03 | 4.63 | -0.00 | 0.53 | ▷ -0.47 | BC 433 |
| | | 57 | 3505 | Max N | ▷ -8.35 | -3.80 | -2.96 | 0.00 | -0.32 | 0.35 | BC 447 |
| | | | Rechts | Min N | ▷ -34.49 | -0.03 | 0.62 | -0.00 | 0.20 | 0.00 | BC 138 |
| | | | | Max $V_y$ | -14.24 | ▷ 5.03 | 4.63 | -0.00 | 0.53 | -0.47 | BC 433 |
| | | | | Min $V_y$ | -18.13 | ▷ -3.83 | -2.84 | 0.00 | -0.27 | 0.36 | BC 207 |
| | | | | Max $V_z$ | -18.21 | 5.02 | ▷ 4.79 | -0.00 | 0.56 | -0.47 | BC 241 |
| | | | | Min $V_z$ | -8.41 | -3.79 | ▷ -3.44 | 0.00 | -0.36 | 0.35 | BC 359 |
| | | | | Max $M_T$ | -12.38 | -3.79 | -3.24 | ▷ 0.00 | -0.33 | 0.35 | BC 231 |
| | | | | Min $M_T$ | -18.21 | 5.02 | 4.79 | ▷ -0.00 | 0.56 | -0.47 | BC 269 |
| | | | | Max $M_y$ | -19.02 | 2.77 | -1.67 | -0.00 | ▷ 1.95 | -0.25 | BC 356 |
| | | | | Min $M_y$ | -8.41 | -3.79 | -3.44 | 0.00 | ▷ -0.36 | 0.35 | BC 359 |
| | | | | Max $M_z$ | -18.13 | -3.83 | -2.84 | 0.00 | -0.27 | ▷ 0.36 | BC 207 |
| | | | | Min $M_z$ | -14.24 | 5.03 | 4.63 | -0.00 | 0.53 | ▷ -0.47 | BC 433 |
| | | 57 | 3505 | Max N | ▷ -8.35 | -3.80 | -2.96 | 0.00 | -0.32 | 0.35 | BC 447 |
| | | 17 | 0 | Min N | ▷ -46.20 | -0.03 | 0.62 | -0.00 | -1.99 | -0.11 | BC 138 |
| | | 17 | 0 | Max $V_y$ | -16.39 | ▷ 6.34 | 6.37 | 0.00 | -5.61 | 4.85 | BC 451 |
| | | 17 | 0 | Min $V_y$ | -24.15 | ▷ -9.00 | -1.96 | -0.00 | -4.15 | -7.47 | BC 217 |
| | | 17 | 0 | Max $V_z$ | -29.83 | 6.30 | ▷ 6.99 | 0.00 | -7.70 | 4.71 | BC 243 |
| | | 57 | 3505 | Min $V_z$ | -8.41 | -3.79 | ▷ -3.44 | 0.00 | -0.36 | 0.35 | BC 359 |
| | | 17 | 0 | Max $M_T$ | -24.09 | 6.32 | 6.50 | ▷ 0.00 | -6.04 | 4.79 | BC 231 |
| | | 17 | 0 | Min $M_T$ | -29.93 | -8.98 | -1.81 | ▷ -0.00 | -4.66 | -7.41 | BC 269 |
| | | | 2142 | Max $M_y$ | -22.14 | -0.27 | -0.07 | -0.00 | ▷ 3.14 | 1.45 | BC 356 |
| | | 17 | 0 | Min $M_y$ | -29.83 | 6.30 | 6.99 | 0.00 | ▷ -7.70 | 4.71 | BC 243 |
| | | 17 | 0 | Max $M_z$ | -16.39 | 6.34 | 6.37 | 0.00 | -5.61 | ▷ 4.85 | BC 451 |
| | | 17 | 0 | Min $M_z$ | -24.15 | -9.00 | -1.96 | -0.00 | -4.15 | ▷ -7.47 | BC 217 |
| 26 | RC1 | 17 | 4345 | MAX N | ▷ -0.19 | 10.38 | 3.19 | 0.00 | -3.91 | -7.41 | BC 445 |
| 26 | RC1 | 7 | 0 | MIN N | ▷ -53.69 | 0.02 | -0.46 | 0.00 | 0.00 | 0.00 | BC 138 |
| 26 | RC1 | 17 | 4345 | MAX $V_y$ | -8.35 | ▷ 10.40 | 3.13 | 0.00 | -4.15 | -7.47 | BC 217 |
| 80 | RC1 | 17 | 0 | MIN $V_y$ | -24.15 | ▷ -9.00 | -1.96 | 0.00 | -4.15 | -7.47 | BC 217 |
| 80 | RC1 | 17 | 0 | MAX $V_z$ | -29.83 | 6.30 | ▷ 6.99 | 0.00 | -7.70 | 4.71 | BC 243 |
| 26 | RC1 | 17 | 4345 | MIN $V_z$ | -23.63 | -7.35 | ▷ -7.81 | 0.00 | -7.70 | 4.71 | BC 243 |
| 26 | RC1 | | 2308 | MAX $M_T$ | -30.08 | -1.49 | -1.72 | ▷ 0.00 | 3.44 | -4.24 | BC 171 |
| 26 | RC1 | | 2308 | MIN $M_T$ | -18.88 | 2.24 | -0.82 | ▷ 0.00 | -6.90 | 5.45 | BC 269 |
| 26 | RC1 | | 1731 | MAX $M_y$ | -21.24 | 0.17 | -0.01 | 0.00 | ▷ 4.15 | -4.61 | BC 359 |
| 80 | RC1 | 17 | 0 | MIN $M_y$ | -29.83 | 6.30 | 6.99 | 0.00 | ▷ -7.70 | 4.71 | BC 243 |
| 26 | RC1 | | 1731 | MAX $M_z$ | -10.12 | -0.07 | -1.79 | 0.00 | -5.91 | ▷ 6.10 | BC 433 |
| 26 | RC1 | 17 | 4345 | MIN $M_z$ | -8.35 | 10.40 | 3.13 | 0.00 | -4.15 | ▷ -7.47 | BC 217 |
| | **Doorgaande staven No. 13: Doorgaande staven 15** | | | | | | | | | | |
| 15 | RC1 | 51 | 0 | Max N | ▷ 15.65 | 0.02 | 55.85 | -0.70 | 0.00 | 0.00 | BC 410 |
| | | | | Min N | ▷ -50.84 | 0.20 | 217.68 | -0.98 | 0.00 | 0.00 | BC 134 |
| | | | | Max $V_y$ | -50.18 | ▷ 0.21 | 217.72 | -0.98 | 0.00 | 0.00 | BC 132 |
| | | | | Min $V_y$ | -12.30 | ▷ 0.01 | 54.40 | -0.03 | 0.00 | 0.00 | BC 409 |
| | | | | Max $V_z$ | -50.13 | 0.21 | ▷ 217.72 | -0.99 | 0.00 | 0.00 | BC 140 |
| | | | | Min $V_z$ | -13.48 | 0.02 | ▷ 54.36 | -0.03 | -0.00 | 0.00 | BC 421 |
| | | | | Max $M_T$ | -13.64 | 0.12 | 54.74 | ▷ 0.02 | -0.00 | 0.00 | BC 359 |
| | | | | Min $M_T$ | -50.13 | 0.21 | 217.72 | ▷ -0.99 | 0.00 | 0.00 | BC 140 |
| | | | | Max $M_y$ | 14.66 | 0.08 | 91.96 | -0.72 | ▷ 0.00 | -0.00 | BC 406 |
| | | | | Min $M_y$ | -12.51 | 0.01 | 54.39 | -0.03 | ▷ -0.00 | 0.00 | BC 381 |
| | | | | Max $M_z$ | -21.05 | 0.08 | 91.00 | -0.40 | 0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | 14.65 | 0.08 | 91.96 | -0.72 | 0.00 | ▷ -0.00 | BC 378 |
| | | 148 | 3201 | Max N | ▷ 15.97 | 0.02 | 38.95 | -0.70 | 151.70 | -0.05 | BC 410 |
| | | | | Min N | ▷ -49.93 | 0.13 | 80.33 | -0.27 | 315.77 | -0.43 | BC 244 |
| | | | | Max $V_y$ | -48.87 | ▷ 0.21 | 147.81 | -0.98 | 584.94 | -0.68 | BC 132 |
| | | | | Min $V_y$ | -11.99 | ▷ 0.01 | 37.50 | -0.03 | 147.06 | -0.02 | BC 409 |
| | | | | Max $V_z$ | -48.82 | 0.21 | ▷ 147.81 | -0.99 | 584.95 | -0.68 | BC 140 |
| | | | | Min $V_z$ | -13.16 | 0.02 | ▷ 37.47 | -0.03 | 146.95 | -0.06 | BC 421 |
| | | | | Max $M_T$ | -13.32 | 0.12 | 37.85 | ▷ 0.02 | 148.18 | -0.39 | BC 359 |
| | | | | Min $M_T$ | -48.82 | 0.21 | 147.81 | ▷ -0.99 | 584.95 | -0.68 | BC 140 |
| | | | | Max $M_y$ | -48.82 | 0.21 | 147.81 | -0.99 | ▷ 584.95 | -0.68 | BC 140 |
| | | | | Min $M_y$ | -13.16 | 0.02 | 37.47 | -0.03 | ▷ 146.95 | -0.06 | BC 421 |
| | | | | Max $M_z$ | -11.99 | 0.01 | 37.50 | -0.03 | 147.06 | ▷ -0.02 | BC 409 |
| | | | | Min $M_z$ | -48.87 | 0.21 | 147.81 | -0.98 | 584.94 | ▷ -0.68 | BC 132 |
| | | 148 | 3201 | Max N | ▷ 15.97 | 0.02 | 38.95 | -0.70 | 151.70 | -0.05 | BC 410 |
| | | 51 | 0 | Min N | ▷ -50.84 | 0.20 | 217.68 | -0.98 | 0.00 | 0.00 | BC 134 |
| | | 51 | 0 | Max $V_y$ | -50.18 | ▷ 0.21 | 217.72 | -0.98 | 0.00 | 0.00 | BC 132 |
| | | 51 | 0 | Min $V_y$ | -12.30 | ▷ 0.01 | 54.40 | -0.03 | 0.00 | 0.00 | BC 409 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 15 | RC1 | 51 | 0 | Max $V_z$ | -50.13 | 0.21 | ▷ 217.72 | -0.99 | 0.00 | 0.00 | BC 140 |
| | | 148 | 3201 | Min $V_z$ | -13.16 | 0.02 | ▷ 37.47 | -0.03 | 146.95 | -0.06 | BC 421 |
| | | 51 | 0 | Max $M_T$ | -13.64 | 0.12 | 54.74 | ▷ 0.02 | -0.00 | 0.00 | BC 359 |
| | | 51 | 0 | Min $M_T$ | -50.13 | 0.21 | 217.72 | ▷ -0.99 | 0.00 | 0.00 | BC 140 |
| | | 148 | 3201 | Max $M_y$ | -48.82 | 0.21 | 147.81 | -0.99 | ▷ 584.95 | -0.68 | BC 140 |
| | | 51 | 0 | Min $M_y$ | -12.51 | 0.01 | 54.39 | -0.03 | ▷ -0.00 | 0.00 | BC 381 |
| | | 51 | 0 | Max $M_z$ | -21.05 | 0.08 | 91.00 | -0.40 | 0.00 | ▷ 0.00 | BC 1 |
| | | 148 | 3201 | Min $M_z$ | -48.87 | 0.21 | 147.81 | -0.98 | 584.94 | ▷ -0.68 | BC 132 |
| 186 | RC1 | 148 | 0 | Max N | ▷ 16.02 | 0.41 | 37.84 | -0.59 | 151.55 | -0.05 | BC 410 |
| | | | | Min N | ▷ -49.75 | 0.98 | 78.72 | -0.02 | 315.47 | -0.43 | BC 244 |
| | | | | Max $V_y$ | -48.38 | ▷ 1.36 | 146.18 | -0.65 | 584.42 | -0.68 | BC 139 |
| | | | | Min $V_y$ | -13.10 | ▷ -0.10 | 36.32 | -0.06 | 146.82 | -0.06 | BC 421 |
| | | | | Max $V_z$ | -48.51 | 1.35 | ▷ 146.18 | -0.65 | 584.42 | -0.68 | BC 140 |
| | | | | Min $V_z$ | -12.99 | -0.10 | ▷ 36.32 | -0.06 | 146.82 | -0.06 | BC 361 |
| | | | | Max $M_T$ | -36.01 | 0.62 | 37.27 | ▷ 0.17 | 149.70 | -0.23 | BC 360 |
| | | | | Min $M_T$ | -48.56 | 1.35 | 146.18 | ▷ -0.65 | 584.42 | -0.68 | BC 155 |
| | | | | Max $M_y$ | -48.51 | 1.35 | 146.18 | -0.65 | ▷ 584.42 | -0.68 | BC 140 |
| | | | | Min $M_y$ | -13.10 | -0.10 | 36.32 | -0.06 | ▷ 146.82 | -0.06 | BC 421 |
| | | | | Max $M_z$ | -11.92 | -0.07 | 36.34 | -0.05 | 146.92 | ▷ -0.02 | BC 409 |
| | | | | Min $M_z$ | -48.55 | 1.36 | 146.18 | -0.65 | 584.42 | ▷ -0.68 | BC 132 |
| | | 82 | 3201 | Max N | ▷ 16.34 | 0.41 | 20.95 | -0.59 | 245.62 | -1.35 | BC 410 |
| | | | | Min N | ▷ -49.06 | 0.98 | 42.07 | -0.02 | 508.76 | -3.58 | BC 244 |
| | | | | Max $V_y$ | -47.07 | ▷ 1.36 | 76.27 | -0.65 | 940.40 | -5.02 | BC 139 |
| | | | | Min $V_y$ | -12.78 | ▷ -0.10 | 19.43 | -0.06 | 236.02 | 0.25 | BC 421 |
| | | | | Max $V_z$ | -47.20 | 1.35 | ▷ 76.27 | -0.65 | 940.40 | -5.01 | BC 140 |
| | | | | Min $V_z$ | -12.68 | -0.10 | ▷ 19.43 | -0.06 | 236.03 | 0.25 | BC 361 |
| | | | | Max $M_T$ | -35.69 | 0.62 | 20.38 | ▷ 0.17 | 241.97 | -2.21 | BC 360 |
| | | | | Min $M_T$ | -47.25 | 1.35 | 76.27 | ▷ -0.65 | 940.39 | -5.00 | BC 155 |
| | | | | Max $M_y$ | -47.20 | 1.35 | 76.27 | -0.65 | ▷ 940.40 | -5.01 | BC 140 |
| | | | | Min $M_y$ | -12.78 | -0.10 | 19.43 | -0.06 | ▷ 236.02 | 0.25 | BC 421 |
| | | | | Max $M_z$ | -12.68 | -0.10 | 19.43 | -0.06 | 236.03 | ▷ 0.25 | BC 361 |
| | | | | Min $M_z$ | -47.07 | 1.36 | 76.27 | -0.65 | 940.40 | ▷ -5.02 | BC 139 |
| | | 82 | 3201 | Max N | ▷ 16.34 | 0.41 | 20.95 | -0.59 | 245.62 | -1.35 | BC 410 |
| | | 148 | 0 | Min N | ▷ -49.75 | 0.98 | 78.72 | -0.02 | 315.47 | -0.43 | BC 244 |
| | | 148 | 0 | Max $V_y$ | -48.38 | ▷ 1.36 | 146.18 | -0.65 | 584.42 | -0.68 | BC 139 |
| | | 148 | 0 | Min $V_y$ | -13.10 | ▷ -0.10 | 36.32 | -0.06 | 146.82 | -0.06 | BC 421 |
| | | 148 | 0 | Max $V_z$ | -48.51 | 1.35 | ▷ 146.18 | -0.65 | 584.42 | -0.68 | BC 140 |
| | | 82 | 3201 | Min $V_z$ | -12.68 | -0.10 | ▷ 19.43 | -0.06 | 236.03 | 0.25 | BC 361 |
| | | 148 | 0 | Max $M_T$ | -36.01 | 0.62 | 37.27 | ▷ 0.17 | 149.70 | -0.23 | BC 360 |
| | | 148 | 0 | Min $M_T$ | -48.56 | 1.35 | 146.18 | ▷ -0.65 | 584.42 | -0.68 | BC 155 |
| | | 82 | 3201 | Max $M_y$ | -47.20 | 1.35 | 76.27 | -0.65 | ▷ 940.40 | -5.01 | BC 140 |
| | | 148 | 0 | Min $M_y$ | -13.10 | -0.10 | 36.32 | -0.06 | ▷ 146.82 | -0.06 | BC 421 |
| | | 82 | 3201 | Max $M_z$ | -12.68 | -0.10 | 19.43 | -0.06 | 236.03 | ▷ 0.25 | BC 361 |
| | | 82 | 3201 | Min $M_z$ | -47.07 | 1.36 | 76.27 | -0.65 | 940.40 | ▷ -5.02 | BC 139 |
| 192 | RC1 | 154 | 0 | Max N | ▷ 53.00 | -0.22 | -3.37 | 0.03 | 575.15 | 1.67 | BC 206 |
| | | | | Min N | ▷ -19.28 | -0.09 | -2.01 | -0.13 | 571.25 | 0.99 | BC 235 |
| | | | | Max $V_y$ | -17.41 | ▷ 0.13 | -0.80 | -0.14 | 267.75 | 0.19 | BC 421 |
| | | | | Min $V_y$ | -9.83 | ▷ -1.23 | -2.69 | 0.25 | 568.48 | -0.40 | BC 204 |
| | | | | Max $V_z$ | -17.33 | 0.13 | ▷ -0.80 | -0.14 | 267.75 | 0.18 | BC 361 |
| | | | | Min $V_z$ | 53.00 | -0.22 | ▷ -3.37 | 0.03 | 575.15 | 1.67 | BC 206 |
| | | | | Max $M_T$ | -10.68 | -1.02 | -1.80 | ▷ 0.28 | 269.83 | -1.12 | BC 468 |
| | | | | Min $M_T$ | -16.24 | -0.17 | -1.74 | ▷ -0.19 | 566.40 | 0.85 | BC 185 |
| | | | | Max $M_y$ | 3.87 | -0.74 | -3.04 | -0.07 | ▷ 1052.68 | 2.57 | BC 155 |
| | | | | Min $M_y$ | -17.35 | 0.12 | -0.81 | -0.15 | ▷ 267.74 | 0.20 | BC 449 |
| | | | | Max $M_z$ | 3.66 | -0.74 | -3.04 | -0.07 | 1052.68 | ▷ 2.57 | BC 148 |
| | | | | Min $M_z$ | -10.56 | -1.02 | -1.80 | 0.28 | 269.81 | ▷ -1.13 | BC 408 |
| | | 82 | 3256 | Max N | ▷ 52.29 | -0.22 | -40.65 | 0.03 | 503.49 | 2.39 | BC 206 |
| | | | | Min N | ▷ -19.98 | -0.09 | -39.29 | -0.13 | 504.01 | 1.28 | BC 235 |
| | | | | Max $V_y$ | -17.73 | ▷ 0.13 | -17.98 | -0.14 | 237.17 | -0.24 | BC 421 |
| | | | | Min $V_y$ | -10.54 | ▷ -1.23 | -39.97 | 0.25 | 499.04 | 3.60 | BC 204 |
| | | | | Max $V_z$ | -17.65 | 0.13 | ▷ -17.98 | -0.14 | 237.18 | -0.24 | BC 361 |
| | | | | Min $V_z$ | 2.61 | -0.74 | ▷ -74.15 | -0.07 | 927.03 | 4.99 | BC 140 |
| | | | | Max $M_T$ | -11.00 | -1.02 | -18.98 | ▷ 0.28 | 236.01 | 2.20 | BC 468 |
| | | | | Min $M_T$ | -16.94 | -0.17 | -39.02 | ▷ -0.19 | 500.06 | 1.41 | BC 185 |
| | | | | Max $M_y$ | 0.85 | -0.71 | -74.12 | -0.08 | ▷ 927.07 | 4.87 | BC 149 |
| | | | | Min $M_y$ | -12.28 | -1.01 | -18.93 | 0.27 | ▷ 235.82 | 2.20 | BC 356 |
| | | | | Max $M_z$ | 2.73 | -0.75 | -74.15 | -0.07 | 927.03 | ▷ 5.00 | BC 139 |
| | | | | Min $M_z$ | -17.65 | 0.13 | -17.98 | -0.14 | 237.18 | ▷ -0.24 | BC 361 |
| | | 154 | 0 | Max N | ▷ 53.00 | -0.22 | -3.37 | 0.03 | 575.15 | 1.67 | BC 206 |
| | | 82 | 3256 | Min N | ▷ -19.98 | -0.09 | -39.29 | -0.13 | 504.01 | 1.28 | BC 235 |
| | | 154 | 0 | Max $V_y$ | -17.41 | ▷ 0.13 | -0.80 | -0.14 | 267.75 | 0.19 | BC 421 |
| | | 154 | 0 | Min $V_y$ | -9.83 | ▷ -1.23 | -2.69 | 0.25 | 568.48 | -0.40 | BC 204 |
| | | 154 | 0 | Max $V_z$ | -17.33 | 0.13 | ▷ -0.80 | -0.14 | 267.75 | 0.18 | BC 361 |
| | | 82 | 3256 | Min $V_z$ | 2.61 | -0.74 | ▷ -74.15 | -0.07 | 927.03 | 4.99 | BC 140 |
| | | 154 | 0 | Max $M_T$ | -10.68 | -1.02 | -1.80 | ▷ 0.28 | 269.83 | -1.12 | BC 468 |
| | | 154 | 0 | Min $M_T$ | -16.24 | -0.17 | -1.74 | ▷ -0.19 | 566.40 | 0.85 | BC 185 |
| | | 154 | 0 | Max $M_y$ | 3.87 | -0.74 | -3.04 | -0.07 | ▷ 1052.68 | 2.57 | BC 155 |
| | | 82 | 3256 | Min $M_y$ | -12.28 | -1.01 | -18.93 | 0.27 | ▷ 235.82 | 2.20 | BC 356 |
| | | 82 | 3256 | Max $M_z$ | 2.73 | -0.75 | -74.15 | -0.07 | 927.03 | ▷ 5.00 | BC 139 |
| | | 154 | 0 | Min $M_z$ | -10.56 | -1.02 | -1.80 | 0.28 | 269.81 | ▷ -1.13 | BC 408 |
| 85 | RC1 | 86 | 0 | Max N | ▷ 53.66 | 0.50 | 36.52 | 0.24 | 516.70 | 3.30 | BC 206 |
| | | | | Min N | ▷ -18.63 | 0.36 | 37.89 | 0.00 | 508.35 | 2.14 | BC 235 |
| | | | | Max $V_y$ | 3.47 | ▷ 0.87 | 70.71 | 0.39 | 937.71 | 5.40 | BC 149 |
| | | | | Min $V_y$ | -11.65 | ▷ -1.30 | 17.21 | 0.19 | 241.32 | -5.31 | BC 356 |
| | | | | Max $V_z$ | 3.56 | 0.87 | ▷ 70.71 | 0.39 | 937.70 | 5.38 | BC 146 |
| | | | | Min $V_z$ | 46.18 | 0.50 | ▷ 16.63 | 0.17 | 247.18 | 3.10 | BC 410 |
| | | | | Max $M_T$ | 4.93 | 0.84 | 70.68 | ▷ 0.39 | 937.88 | 5.32 | BC 148 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 85 | RC1 | | | Min $M_T$ | -16.80 | 0.54 | 18.16 | ▷ -0.02 | 236.51 | 1.95 | BC 357 |
| | | | | Max $M_y$ | 5.22 | 0.84 | 70.68 | 0.39 | ▷ 937.89 | 5.30 | BC 140 |
| | | | | Min $M_y$ | -17.10 | 0.55 | 18.16 | -0.02 | ▷ 236.49 | 1.99 | BC 421 |
| | | | | Max $M_z$ | 3.47 | 0.87 | 70.71 | 0.39 | 937.71 | ▷ 5.40 | BC 149 |
| | | | | Min $M_z$ | -10.26 | -1.29 | 17.16 | 0.20 | 241.78 | ▷ -5.34 | BC 408 |
| | | 154 | 3256 | Max N | ▷ 52.96 | 0.50 | -0.77 | 0.24 | 574.90 | 1.67 | BC 206 |
| | | | | Min N | ▷ -19.34 | 0.36 | 0.61 | 0.00 | 571.02 | 0.99 | BC 235 |
| | | | | Max $V_y$ | 2.12 | ▷ 0.87 | -0.40 | 0.39 | 1052.16 | 2.56 | BC 149 |
| | | | | Min $V_y$ | -11.98 | ▷ -1.30 | 0.03 | 0.19 | 269.38 | -1.08 | BC 356 |
| | | | | Max $V_z$ | -17.20 | 0.67 | ▷ 1.12 | 0.03 | 393.34 | 0.42 | BC 169 |
| | | | | Min $V_z$ | 49.98 | 0.51 | ▷ -0.85 | 0.22 | 447.94 | 1.59 | BC 398 |
| | | | | Max $M_T$ | 3.59 | 0.84 | -0.43 | ▷ 0.39 | 1052.22 | 2.58 | BC 148 |
| | | | | Min $M_T$ | -17.12 | 0.54 | 0.97 | ▷ -0.02 | 267.66 | 0.18 | BC 357 |
| | | | | Max $M_y$ | 3.80 | 0.84 | -0.44 | 0.39 | ▷ 1052.22 | 2.57 | BC 155 |
| | | | | Min $M_y$ | -17.36 | 0.56 | 0.97 | -0.02 | ▷ 267.63 | 0.20 | BC 449 |
| | | | | Max $M_z$ | 3.59 | 0.84 | -0.43 | 0.39 | 1052.22 | ▷ 2.58 | BC 148 |
| | | | | Min $M_z$ | -10.59 | -1.29 | -0.02 | 0.20 | 269.69 | ▷ -1.13 | BC 408 |
| | | 86 | 0 | Max N | ▷ 53.66 | 0.50 | 36.52 | 0.24 | 516.70 | 3.30 | BC 206 |
| | | 154 | 3256 | Min N | ▷ -19.34 | 0.36 | 0.61 | 0.00 | 571.02 | 0.99 | BC 235 |
| | | 86 | 0 | Max $V_y$ | 3.47 | ▷ 0.87 | 70.71 | 0.39 | 937.71 | 5.40 | BC 149 |
| | | 86 | 0 | Min $V_y$ | -11.65 | ▷ -1.30 | 17.21 | 0.19 | 241.32 | -5.31 | BC 356 |
| | | 86 | 0 | Max $V_z$ | 3.56 | 0.87 | ▷ 70.71 | 0.39 | 937.70 | 5.38 | BC 146 |
| | | 154 | 3256 | Min $V_z$ | 49.98 | 0.51 | ▷ -0.85 | 0.22 | 447.94 | 1.59 | BC 398 |
| | | 86 | 0 | Max $M_T$ | 4.93 | 0.84 | 70.68 | ▷ 0.39 | 937.88 | 5.32 | BC 148 |
| | | 86 | 0 | Min $M_T$ | -16.80 | 0.54 | 18.16 | ▷ -0.02 | 236.51 | 1.95 | BC 357 |
| | | 154 | 3256 | Max $M_y$ | 3.80 | 0.84 | -0.44 | 0.39 | ▷ 1052.22 | 2.57 | BC 155 |
| | | 86 | 0 | Min $M_y$ | -17.10 | 0.55 | 18.16 | -0.02 | ▷ 236.49 | 1.99 | BC 421 |
| | | 86 | 0 | Max $M_z$ | 3.47 | 0.87 | 70.71 | 0.39 | 937.71 | ▷ 5.40 | BC 149 |
| | | 86 | 0 | Min $M_z$ | -10.26 | -1.29 | 17.16 | 0.20 | 241.78 | ▷ -5.34 | BC 408 |
| 199 | RC1 | 161 | 0 | Max N | ▷ 15.04 | -0.78 | 38.54 | 0.43 | 156.99 | 0.59 | BC 414 |
| | | | | Min N | ▷ -54.78 | -1.45 | 145.10 | 0.46 | 592.61 | 0.67 | BC 146 |
| | | | | Max $V_y$ | -15.60 | ▷ 1.35 | 36.69 | -0.16 | 150.97 | -0.95 | BC 408 |
| | | | | Min $V_y$ | -54.73 | ▷ -1.46 | 145.09 | 0.46 | 592.60 | 0.68 | BC 149 |
| | | | | Max $V_z$ | -53.99 | -1.42 | ▷ 145.17 | 0.47 | 592.83 | 0.68 | BC 139 |
| | | | | Min $V_z$ | -15.12 | -0.45 | ▷ 36.36 | -0.04 | 149.93 | 0.31 | BC 423 |
| | | | | Max $M_T$ | -54.04 | -1.42 | 145.16 | ▷ 0.47 | 592.80 | 0.68 | BC 132 |
| | | | | Min $M_T$ | -16.83 | 1.33 | 36.61 | ▷ -0.16 | 150.74 | -0.93 | BC 352 |
| | | | | Max $M_y$ | -53.99 | -1.42 | 145.17 | 0.47 | ▷ 592.83 | 0.68 | BC 139 |
| | | | | Min $M_y$ | -15.12 | -0.45 | 36.36 | -0.04 | ▷ 149.93 | 0.31 | BC 423 |
| | | | | Max $M_z$ | 13.01 | -0.82 | 79.92 | 0.45 | 325.92 | ▷ 0.72 | BC 242 |
| | | | | Min $M_z$ | -15.60 | 1.35 | 36.69 | -0.16 | 150.97 | ▷ -0.95 | BC 408 |
| | | 86 | 3267 | Max N | ▷ 15.67 | -0.78 | 21.56 | 0.43 | 255.16 | 3.15 | BC 414 |
| | | | | Min N | ▷ -52.18 | -1.45 | 75.19 | 0.46 | 952.48 | 5.42 | BC 146 |
| | | | | Max $V_y$ | -14.96 | ▷ 1.35 | 19.71 | -0.16 | 243.10 | -5.35 | BC 408 |
| | | | | Min $V_y$ | -52.13 | ▷ -1.46 | 75.19 | 0.46 | 952.45 | 5.44 | BC 149 |
| | | | | Max $V_z$ | -51.39 | -1.42 | ▷ 75.26 | 0.47 | 952.92 | 5.32 | BC 139 |
| | | | | Min $V_z$ | -14.48 | -0.45 | ▷ 19.38 | -0.04 | 241.00 | 1.77 | BC 423 |
| | | | | Max $M_T$ | -51.43 | -1.42 | 75.25 | ▷ 0.47 | 952.87 | 5.33 | BC 132 |
| | | | | Min $M_T$ | -16.20 | 1.33 | 19.63 | ▷ -0.16 | 242.61 | -5.29 | BC 352 |
| | | | | Max $M_y$ | -51.39 | -1.42 | 75.26 | 0.47 | ▷ 952.92 | 5.32 | BC 139 |
| | | | | Min $M_y$ | -14.48 | -0.45 | 19.38 | -0.04 | ▷ 241.00 | 1.77 | BC 423 |
| | | | | Max $M_z$ | -52.13 | -1.46 | 75.19 | 0.46 | 952.45 | ▷ 5.44 | BC 149 |
| | | | | Min $M_z$ | -14.96 | 1.35 | 19.71 | -0.16 | 243.10 | ▷ -5.35 | BC 408 |
| | | 86 | 3267 | Max N | ▷ 15.67 | -0.78 | 21.56 | 0.43 | 255.16 | 3.15 | BC 414 |
| | | 161 | 0 | Min N | ▷ -54.78 | -1.45 | 145.10 | 0.46 | 592.61 | 0.67 | BC 146 |
| | | 161 | 0 | Max $V_y$ | -15.60 | ▷ 1.35 | 36.69 | -0.16 | 150.97 | -0.95 | BC 408 |
| | | 161 | 0 | Min $V_y$ | -54.73 | ▷ -1.46 | 145.09 | 0.46 | 592.60 | 0.68 | BC 149 |
| | | 161 | 0 | Max $V_z$ | -53.99 | -1.42 | ▷ 145.17 | 0.47 | 592.83 | 0.68 | BC 139 |
| | | 86 | 3267 | Min $V_z$ | -14.48 | -0.45 | ▷ 19.38 | -0.04 | 241.00 | 1.77 | BC 423 |
| | | 161 | 0 | Max $M_T$ | -54.04 | -1.42 | 145.16 | ▷ 0.47 | 592.80 | 0.68 | BC 132 |
| | | 161 | 0 | Min $M_T$ | -16.83 | 1.33 | 36.61 | ▷ -0.16 | 150.74 | -0.93 | BC 352 |
| | | 86 | 3267 | Max $M_y$ | -51.39 | -1.42 | 75.26 | 0.47 | ▷ 952.92 | 5.32 | BC 139 |
| | | 161 | 0 | Min $M_y$ | -15.12 | -0.45 | 36.36 | -0.04 | ▷ 149.93 | 0.31 | BC 423 |
| | | 86 | 3267 | Max $M_z$ | -52.13 | -1.46 | 75.19 | 0.46 | 952.45 | ▷ 5.44 | BC 149 |
| | | 86 | 3267 | Min $M_z$ | -14.96 | 1.35 | 19.71 | -0.16 | 243.10 | ▷ -5.35 | BC 408 |
| 16 | RC1 | 61 | 0 | Max N | ▷ 14.35 | -0.18 | 56.63 | 0.61 | 0.00 | 0.00 | BC 414 |
| | | | | Min N | ▷ -57.70 | -0.21 | 216.63 | 0.83 | -0.00 | 0.00 | BC 146 |
| | | | | Max $V_y$ | -16.29 | ▷ 0.29 | 54.78 | -0.47 | -0.00 | 0.00 | BC 408 |
| | | | | Min $V_y$ | 11.50 | ▷ -0.22 | 118.30 | 0.63 | 0.00 | 0.00 | BC 242 |
| | | | | Max $V_z$ | -56.92 | -0.21 | ▷ 216.70 | 0.82 | 0.00 | 0.00 | BC 139 |
| | | | | Min $V_z$ | -15.81 | -0.10 | ▷ 54.46 | 0.06 | -0.00 | 0.00 | BC 423 |
| | | | | Max $M_T$ | -57.64 | -0.21 | 216.63 | ▷ 0.83 | -0.00 | 0.00 | BC 134 |
| | | | | Min $M_T$ | -17.59 | 0.29 | 54.71 | ▷ -0.47 | 0.00 | 0.00 | BC 356 |
| | | | | Max $M_y$ | 12.67 | -0.21 | 92.51 | 0.61 | ▷ 0.00 | 0.00 | BC 466 |
| | | | | Min $M_y$ | -38.41 | -0.07 | 54.66 | 0.19 | ▷ -0.00 | 0.00 | BC 381 |
| | | | | Max $M_z$ | 13.13 | -0.20 | 82.32 | 0.61 | 0.00 | ▷ 0.00 | BC 162 |
| | | | | Min $M_z$ | -25.44 | -0.09 | 90.96 | 0.35 | -0.00 | ▷ 0.00 | BC 1 |
| | | 161 | 3267 | Max N | ▷ 14.98 | -0.18 | 39.65 | 0.61 | 157.27 | 0.59 | BC 414 |
| | | | | Min N | ▷ -55.10 | -0.21 | 146.72 | 0.83 | 593.59 | 0.67 | BC 146 |
| | | | | Max $V_y$ | -15.66 | ▷ 0.29 | 37.80 | -0.47 | 151.25 | -0.95 | BC 408 |
| | | | | Min $V_y$ | 12.86 | ▷ -0.22 | 81.55 | 0.63 | 326.48 | 0.72 | BC 242 |
| | | | | Max $V_z$ | -54.32 | -0.21 | ▷ 146.79 | 0.82 | 593.82 | 0.68 | BC 139 |
| | | | | Min $V_z$ | -15.18 | -0.10 | ▷ 37.48 | 0.06 | 150.18 | 0.31 | BC 423 |
| | | | | Max $M_T$ | -55.04 | -0.21 | 146.72 | ▷ 0.83 | 593.59 | 0.68 | BC 134 |
| | | | | Min $M_T$ | -16.96 | 0.29 | 37.73 | ▷ -0.47 | 151.00 | -0.93 | BC 356 |
| | | | | Max $M_y$ | -54.32 | -0.21 | 146.79 | 0.82 | ▷ 593.82 | 0.68 | BC 139 |
| | | | | Min $M_y$ | -15.18 | -0.10 | 37.48 | 0.06 | ▷ 150.18 | 0.31 | BC 423 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 16 | RC1 | | | Max $M_z$ | 12.86 | -0.22 | 81.55 | 0.63 | 326.48 | ▷ 0.72 | BC 242 |
| | | | | Min $M_z$ | -15.66 | 0.29 | 37.80 | -0.47 | 151.25 | ▷ -0.95 | BC 408 |
| | | 161 | 3267 | Max N | ▷ 14.98 | -0.18 | 39.65 | 0.61 | 157.27 | 0.59 | BC 414 |
| | | 61 | 0 | Min N | ▷ -57.70 | -0.21 | 216.63 | 0.83 | -0.00 | 0.00 | BC 146 |
| | | 61 | 0 | Max $V_y$ | -16.29 | ▷ 0.29 | 54.78 | -0.47 | -0.00 | 0.00 | BC 408 |
| | | 61 | 0 | Min $V_y$ | 11.50 | ▷ -0.22 | 118.30 | 0.63 | 0.00 | 0.00 | BC 242 |
| | | 61 | 0 | Max $V_z$ | -56.92 | -0.21 | ▷ 216.70 | 0.82 | 0.00 | 0.00 | BC 139 |
| | | 161 | 3267 | Min $V_z$ | -15.18 | -0.10 | ▷ 37.48 | 0.06 | 150.18 | 0.31 | BC 423 |
| | | 61 | 0 | Max $M_T$ | -57.64 | -0.21 | 216.63 | ▷ 0.83 | -0.00 | 0.00 | BC 134 |
| | | 61 | 0 | Min $M_T$ | -17.59 | 0.29 | 54.71 | ▷ -0.47 | 0.00 | 0.00 | BC 356 |
| | | 161 | 3267 | Max $M_y$ | -54.32 | -0.21 | 146.79 | 0.82 | ▷ 593.82 | 0.68 | BC 139 |
| | | 61 | 0 | Min $M_y$ | -38.41 | -0.07 | 54.66 | 0.19 | ▷ -0.00 | 0.00 | BC 381 |
| | | 161 | 3267 | Max $M_z$ | 12.86 | -0.22 | 81.55 | 0.63 | 326.48 | ▷ 0.72 | BC 242 |
| | | 161 | 3267 | Min $M_z$ | -15.66 | 0.29 | 37.80 | -0.47 | 151.25 | ▷ -0.95 | BC 408 |
| 85 | RC1 | 86 | 0 | MAX N | ▷ 53.66 | 0.50 | 36.52 | 0.24 | 516.70 | 3.30 | BC 206 |
| 16 | RC1 | 61 | 0 | MIN N | ▷ -57.70 | -0.21 | 216.63 | 0.83 | 0.00 | 0.00 | BC 146 |
| 186 | RC1 | 148 | 0 | MAX $V_y$ | -48.38 | ▷ 1.36 | 146.18 | -0.65 | 584.42 | -0.68 | BC 139 |
| 199 | RC1 | 161 | 0 | MIN $V_y$ | -54.73 | ▷ -1.46 | 145.09 | 0.46 | 592.60 | 0.68 | BC 149 |
| 15 | RC1 | 51 | 0 | MAX $V_z$ | -50.13 | 0.21 | ▷ 217.72 | -0.99 | 0.00 | 0.00 | BC 140 |
| 192 | RC1 | 82 | 3256 | MIN $V_z$ | 2.61 | -0.74 | ▷ -74.15 | -0.07 | 927.03 | 4.99 | BC 140 |
| 16 | RC1 | 61 | 0 | MAX $M_T$ | -57.64 | -0.21 | 216.63 | ▷ 0.83 | 0.00 | 0.00 | BC 134 |
| 15 | RC1 | 51 | 0 | MIN $M_T$ | -50.13 | 0.21 | 217.72 | ▷ -0.99 | 0.00 | 0.00 | BC 140 |
| 192 | RC1 | 154 | 0 | MAX $M_y$ | 3.87 | -0.74 | -3.04 | -0.07 | ▷ 1052.68 | 2.57 | BC 155 |
| 15 | RC1 | 51 | 0 | MIN $M_y$ | -12.51 | 0.01 | 54.39 | -0.03 | ▷ 0.00 | 0.00 | BC 381 |
| 199 | RC1 | 86 | 3267 | MAX $M_z$ | -52.13 | -1.46 | 75.19 | 0.46 | 952.45 | ▷ 5.44 | BC 149 |
| 199 | RC1 | 86 | 3267 | MIN $M_z$ | -14.96 | 1.35 | 19.71 | -0.16 | 243.10 | ▷ -5.35 | BC 408 |
| | **Doorgaande staven No. 14: Doorgaande staven 16** | | | | | | | | | | |
| 19 | RC1 | 53 | 0 | Max N | ▷ 16.29 | -0.03 | 31.54 | 0.22 | 0.00 | 0.00 | BC 411 |
| | | | | Min N | ▷ -18.94 | -0.02 | 69.63 | 0.05 | 0.00 | 0.00 | BC 244 |
| | | | | Max $V_y$ | -10.54 | ▷ 0.04 | 31.34 | 0.03 | -0.00 | 0.00 | BC 473 |
| | | | | Min $V_y$ | 15.34 | ▷ -0.05 | 70.11 | 0.17 | -0.00 | 0.00 | BC 175 |
| | | | | Max $V_z$ | -4.36 | -0.04 | ▷ 136.86 | 0.04 | -0.00 | 0.00 | BC 131 |
| | | | | Min $V_z$ | -17.83 | -0.01 | ▷ 31.07 | 0.04 | 0.00 | 0.00 | BC 444 |
| | | | | Max $M_T$ | 16.29 | -0.03 | 31.54 | ▷ 0.22 | 0.00 | 0.00 | BC 411 |
| | | | | Min $M_T$ | -8.25 | -0.04 | 31.29 | ▷ 0.01 | 0.00 | 0.00 | BC 450 |
| | | | | Max $M_y$ | -5.29 | -0.04 | 136.83 | 0.04 | ▷ 0.00 | 0.00 | BC 133 |
| | | | | Min $M_y$ | -10.05 | 0.04 | 31.34 | 0.03 | ▷ -0.00 | 0.00 | BC 381 |
| | | | | Max $M_z$ | -5.32 | -0.04 | 55.23 | 0.02 | 0.00 | ▷ 0.00 | BC 406 |
| | | | | Min $M_z$ | -0.99 | -0.03 | 51.78 | 0.04 | 0.00 | ▷ 0.00 | BC 1 |
| | | 147 | 3201 | Max N | ▷ 16.56 | -0.03 | 16.99 | 0.22 | 77.66 | 0.11 | BC 411 |
| | | | | Min N | ▷ -18.31 | -0.02 | 36.43 | 0.05 | 169.72 | 0.08 | BC 244 |
| | | | | Max $V_y$ | -10.26 | ▷ 0.04 | 16.80 | 0.03 | 77.03 | -0.14 | BC 473 |
| | | | | Min $V_y$ | 15.96 | ▷ -0.05 | 36.90 | 0.17 | 171.25 | 0.16 | BC 175 |
| | | | | Max $V_z$ | -3.12 | -0.04 | ▷ 70.40 | 0.04 | 331.67 | 0.14 | BC 131 |
| | | | | Min $V_z$ | -17.56 | -0.01 | ▷ 16.53 | 0.04 | 76.18 | 0.04 | BC 444 |
| | | | | Max $M_T$ | 16.56 | -0.03 | 16.99 | ▷ 0.22 | 77.66 | 0.11 | BC 411 |
| | | | | Min $M_T$ | -7.97 | -0.04 | 16.75 | ▷ 0.01 | 76.88 | 0.14 | BC 450 |
| | | | | Max $M_y$ | -3.12 | -0.04 | 70.40 | 0.04 | ▷ 331.67 | 0.14 | BC 131 |
| | | | | Min $M_y$ | -17.56 | -0.01 | 16.53 | 0.04 | ▷ 76.18 | 0.04 | BC 444 |
| | | | | Max $M_z$ | 15.96 | -0.05 | 36.90 | 0.17 | 171.25 | ▷ 0.16 | BC 175 |
| | | | | Min $M_z$ | -10.26 | 0.04 | 16.80 | 0.03 | 77.03 | ▷ -0.14 | BC 473 |
| | | 147 | 3201 | Max N | ▷ 16.56 | -0.03 | 16.99 | 0.22 | 77.66 | 0.11 | BC 411 |
| | | 53 | 0 | Min N | ▷ -18.94 | -0.02 | 69.63 | 0.05 | 0.00 | 0.00 | BC 244 |
| | | 53 | 0 | Max $V_y$ | -10.54 | ▷ 0.04 | 31.34 | 0.03 | -0.00 | 0.00 | BC 473 |
| | | 53 | 0 | Min $V_y$ | 15.34 | ▷ -0.05 | 70.11 | 0.17 | -0.00 | 0.00 | BC 175 |
| | | 53 | 0 | Max $V_z$ | -4.36 | -0.04 | ▷ 136.86 | 0.04 | -0.00 | 0.00 | BC 131 |
| | | 147 | 3201 | Min $V_z$ | -17.56 | -0.01 | ▷ 16.53 | 0.04 | 76.18 | 0.04 | BC 444 |
| | | 53 | 0 | Max $M_T$ | 16.29 | -0.03 | 31.54 | ▷ 0.22 | 0.00 | 0.00 | BC 411 |
| | | 53 | 0 | Min $M_T$ | -8.25 | -0.04 | 31.29 | ▷ 0.01 | 0.00 | 0.00 | BC 450 |
| | | 147 | 3201 | Max $M_y$ | -3.12 | -0.04 | 70.40 | 0.04 | ▷ 331.67 | 0.14 | BC 131 |
| | | 53 | 0 | Min $M_y$ | -10.05 | 0.04 | 31.34 | 0.03 | ▷ -0.00 | 0.00 | BC 381 |
| | | 147 | 3201 | Max $M_z$ | 15.96 | -0.05 | 36.90 | 0.17 | 171.25 | ▷ 0.16 | BC 175 |
| | | 147 | 3201 | Min $M_z$ | -10.26 | 0.04 | 16.80 | 0.03 | 77.03 | ▷ -0.14 | BC 473 |
| 185 | RC1 | 147 | 0 | Max N | ▷ 16.59 | -0.27 | 15.88 | 0.17 | 77.80 | 0.11 | BC 411 |
| | | | | Min N | ▷ -18.20 | -0.01 | 34.81 | 0.06 | 169.94 | 0.08 | BC 244 |
| | | | | Max $V_y$ | -18.05 | ▷ 0.01 | 27.47 | 0.04 | 133.94 | 0.05 | BC 432 |
| | | | | Min $V_y$ | 16.59 | ▷ -0.27 | 15.88 | 0.17 | 77.80 | 0.11 | BC 411 |
| | | | | Max $V_z$ | -2.93 | -0.04 | ▷ 68.77 | 0.04 | 332.04 | 0.14 | BC 131 |
| | | | | Min $V_z$ | -17.19 | -0.00 | ▷ 15.42 | 0.04 | 76.32 | 0.04 | BC 472 |
| | | | | Max $M_T$ | 16.53 | -0.27 | 15.95 | ▷ 0.17 | 78.01 | 0.14 | BC 391 |
| | | | | Min $M_T$ | -7.94 | -0.14 | 15.64 | ▷ -0.02 | 76.99 | 0.14 | BC 450 |
| | | | | Max $M_y$ | -2.93 | -0.04 | 68.77 | 0.04 | ▷ 332.04 | 0.14 | BC 131 |
| | | | | Min $M_y$ | -17.50 | 0.00 | 15.42 | 0.04 | ▷ 76.31 | 0.04 | BC 444 |
| | | | | Max $M_z$ | 16.03 | -0.19 | 35.27 | 0.14 | 171.48 | ▷ 0.16 | BC 175 |
| | | | | Min $M_z$ | -10.26 | -0.09 | 15.64 | -0.01 | 77.16 | ▷ -0.14 | BC 473 |
| | | 83 | 3201 | Max N | ▷ 16.86 | -0.27 | 1.34 | 0.17 | 105.35 | 0.97 | BC 411 |
| | | | | Min N | ▷ -17.58 | -0.01 | 1.60 | 0.06 | 228.21 | 0.11 | BC 244 |
| | | | | Max $V_y$ | -17.56 | ▷ 0.01 | 1.05 | 0.04 | 179.59 | 0.02 | BC 432 |
| | | | | Min $V_y$ | 16.86 | ▷ -0.27 | 1.34 | 0.17 | 105.35 | 0.97 | BC 411 |
| | | | | Max $V_z$ | -1.68 | -0.04 | ▷ 2.31 | 0.04 | 445.78 | 0.27 | BC 131 |
| | | | | Min $V_z$ | -16.92 | -0.00 | ▷ 0.88 | 0.04 | 102.40 | 0.04 | BC 472 |
| | | | | Max $M_T$ | 16.80 | -0.27 | 1.41 | ▷ 0.17 | 105.80 | 0.99 | BC 391 |
| | | | | Min $M_T$ | -7.67 | -0.14 | 1.10 | ▷ -0.02 | 103.78 | 0.58 | BC 450 |
| | | | | Max $M_y$ | -1.68 | -0.04 | 2.31 | 0.04 | ▷ 445.78 | 0.27 | BC 131 |
| | | | | Min $M_y$ | -17.23 | 0.00 | 0.88 | 0.04 | ▷ 102.40 | 0.03 | BC 444 |
| | | | | Max $M_z$ | 16.80 | -0.27 | 1.41 | 0.17 | 105.80 | ▷ 0.99 | BC 363 |
| | | | | Min $M_z$ | -17.56 | 0.01 | 1.05 | 0.04 | 179.59 | ▷ 0.02 | BC 432 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 185 | RC1 | 83 | 3201 | Max N | ▷ 16.86 | -0.27 | 1.34 | 0.17 | 105.35 | 0.97 | BC 411 |
| | | 147 | 0 | Min N | ▷ -18.20 | -0.01 | 34.81 | 0.06 | 169.94 | 0.08 | BC 244 |
| | | 147 | 0 | Max $V_y$ | -18.05 | ▷ 0.01 | 27.47 | 0.04 | 133.94 | 0.05 | BC 432 |
| | | 147 | 0 | Min $V_y$ | 16.59 | ▷ -0.27 | 15.88 | 0.17 | 77.80 | 0.11 | BC 411 |
| | | 147 | 0 | Max $V_z$ | -2.93 | -0.04 | ▷ 68.77 | 0.04 | 332.04 | 0.14 | BC 131 |
| | | 83 | 3201 | Min $V_z$ | -16.92 | -0.00 | ▷ 0.88 | 0.04 | 102.40 | 0.04 | BC 472 |
| | | 147 | 0 | Max $M_T$ | 16.53 | -0.27 | 15.95 | ▷ 0.17 | 78.01 | 0.14 | BC 391 |
| | | 147 | 0 | Min $M_T$ | -7.94 | -0.14 | 15.64 | ▷ -0.02 | 76.99 | 0.14 | BC 450 |
| | | 83 | 3201 | Max $M_y$ | -1.68 | -0.04 | 2.31 | 0.04 | ▷ 445.78 | 0.27 | BC 131 |
| | | 147 | 0 | Min $M_y$ | -17.50 | 0.00 | 15.42 | 0.04 | ▷ 76.31 | 0.04 | BC 444 |
| | | 83 | 3201 | Max $M_z$ | 16.80 | -0.27 | 1.41 | 0.17 | 105.80 | ▷ 0.99 | BC 363 |
| | | 147 | 0 | Min $M_z$ | -10.26 | -0.09 | 15.64 | -0.01 | 77.16 | ▷ -0.14 | BC 473 |
| 191 | RC1 | 153 | 0 | Max N | ▷ 35.96 | 0.25 | 14.82 | -0.19 | 77.76 | -0.15 | BC 391 |
| | | | | Min N | ▷ -32.77 | 0.01 | 34.34 | -0.01 | 174.90 | -0.05 | BC 240 |
| | | | | Max $V_y$ | 35.95 | ▷ 0.26 | 14.82 | -0.19 | 77.76 | -0.15 | BC 363 |
| | | | | Min $V_y$ | -32.10 | ▷ -0.01 | 27.26 | -0.01 | 138.01 | -0.05 | BC 432 |
| | | | | Max $V_z$ | -5.03 | 0.09 | ▷ 67.45 | -0.03 | 337.41 | -0.02 | BC 154 |
| | | | | Min $V_z$ | 35.95 | 0.26 | ▷ 14.82 | -0.19 | 77.76 | -0.15 | BC 363 |
| | | | | Max $M_T$ | -8.85 | 0.17 | 15.14 | ▷ 0.04 | 79.02 | -0.05 | BC 450 |
| | | | | Min $M_T$ | 35.96 | 0.25 | 14.82 | ▷ -0.19 | 77.76 | -0.15 | BC 391 |
| | | | | Max $M_y$ | -5.03 | 0.09 | 67.45 | -0.03 | ▷ 337.41 | -0.02 | BC 154 |
| | | | | Min $M_y$ | 35.96 | 0.25 | 14.82 | -0.19 | ▷ 77.75 | -0.15 | BC 419 |
| | | | | Max $M_z$ | -4.29 | 0.07 | 27.06 | -0.02 | 137.31 | ▷ 0.00 | BC 53 |
| | | | | Min $M_z$ | 32.42 | 0.25 | 14.89 | -0.19 | 77.85 | ▷ -0.16 | BC 411 |
| | | 83 | 3256 | Max N | ▷ 35.68 | 0.25 | 0.02 | -0.19 | 101.91 | -0.98 | BC 391 |
| | | | | Min N | ▷ -33.40 | 0.01 | 0.56 | -0.01 | 231.71 | -0.07 | BC 240 |
| | | | | Max $V_y$ | 35.67 | ▷ 0.26 | 0.02 | -0.19 | 101.92 | -0.98 | BC 363 |
| | | | | Min $V_y$ | -32.61 | ▷ -0.01 | 0.39 | -0.01 | 183.03 | -0.02 | BC 432 |
| | | | | Max $V_z$ | -32.37 | 0.01 | ▷ 0.74 | -0.01 | 154.29 | -0.07 | BC 252 |
| | | | | Min $V_z$ | -3.42 | 0.05 | ▷ -0.36 | -0.02 | 398.10 | -0.19 | BC 323 |
| | | | | Max $M_T$ | -9.13 | 0.17 | 0.35 | ▷ 0.04 | 104.22 | -0.58 | BC 450 |
| | | | | Min $M_T$ | 35.68 | 0.25 | 0.02 | ▷ -0.19 | 101.91 | -0.98 | BC 391 |
| | | | | Max $M_y$ | -6.31 | 0.09 | -0.15 | -0.03 | ▷ 446.96 | -0.32 | BC 154 |
| | | | | Min $M_y$ | 35.68 | 0.25 | 0.02 | -0.19 | ▷ 101.91 | -0.98 | BC 391 |
| | | | | Max $M_z$ | -32.61 | -0.01 | 0.39 | -0.01 | 183.03 | ▷ -0.02 | BC 432 |
| | | | | Min $M_z$ | 35.67 | 0.26 | 0.02 | -0.19 | 101.92 | ▷ -0.98 | BC 363 |
| | | 153 | 0 | Max N | ▷ 35.96 | 0.25 | 14.82 | -0.19 | 77.76 | -0.15 | BC 391 |
| | | 83 | 3256 | Min N | ▷ -33.40 | 0.01 | 0.56 | -0.01 | 231.71 | -0.07 | BC 240 |
| | | 153 | 0 | Max $V_y$ | 35.95 | ▷ 0.26 | 14.82 | -0.19 | 77.76 | -0.15 | BC 363 |
| | | 153 | 0 | Min $V_y$ | -32.10 | ▷ -0.01 | 27.26 | -0.01 | 138.01 | -0.05 | BC 432 |
| | | 153 | 0 | Max $V_z$ | -5.03 | 0.09 | ▷ 67.45 | -0.03 | 337.41 | -0.02 | BC 154 |
| | | 83 | 3256 | Min $V_z$ | -3.42 | 0.05 | ▷ -0.36 | -0.02 | 398.10 | -0.19 | BC 323 |
| | | 153 | 0 | Max $M_T$ | -8.85 | 0.17 | 15.14 | ▷ 0.04 | 79.02 | -0.05 | BC 450 |
| | | 153 | 0 | Min $M_T$ | 35.96 | 0.25 | 14.82 | ▷ -0.19 | 77.76 | -0.15 | BC 391 |
| | | 83 | 3256 | Max $M_y$ | -6.31 | 0.09 | -0.15 | -0.03 | ▷ 446.96 | -0.32 | BC 154 |
| | | 153 | 0 | Min $M_y$ | 35.96 | 0.25 | 14.82 | -0.19 | ▷ 77.75 | -0.15 | BC 419 |
| | | 153 | 0 | Max $M_z$ | -4.29 | 0.07 | 27.06 | -0.02 | 137.31 | ▷ 0.00 | BC 53 |
| | | 83 | 3256 | Min $M_z$ | 35.67 | 0.26 | 0.02 | -0.19 | 101.92 | ▷ -0.98 | BC 363 |
| 46 | RC1 | 68 | 0 | Max N | ▷ 36.13 | 0.05 | 31.32 | -0.25 | 0.00 | 0.00 | BC 391 |
| | | | | Min N | ▷ -32.25 | 0.01 | 70.70 | -0.01 | 0.00 | 0.00 | BC 240 |
| | | | | Max $V_y$ | 32.59 | ▷ 0.05 | 31.36 | -0.24 | 0.00 | -0.00 | BC 411 |
| | | | | Min $V_y$ | -3.89 | ▷ -0.00 | 55.69 | -0.03 | -0.00 | 0.00 | BC 53 |
| | | | | Max $V_z$ | -4.02 | 0.00 | ▷ 137.61 | -0.05 | 0.00 | 0.00 | BC 154 |
| | | | | Min $V_z$ | 36.13 | 0.05 | ▷ 31.32 | -0.25 | 0.00 | 0.00 | BC 419 |
| | | | | Max $M_T$ | -9.77 | 0.02 | 55.66 | ▷ 0.03 | 0.00 | 0.00 | BC 373 |
| | | | | Min $M_T$ | 36.13 | 0.05 | 31.32 | ▷ -0.25 | 0.00 | 0.00 | BC 391 |
| | | | | Max $M_y$ | -4.03 | 0.00 | 118.43 | -0.05 | ▷ 0.00 | 0.00 | BC 115 |
| | | | | Min $M_y$ | -9.27 | 0.01 | 31.69 | 0.03 | ▷ -0.00 | 0.00 | BC 381 |
| | | | | Max $M_z$ | -8.04 | 0.02 | 70.44 | 0.02 | -0.00 | ▷ 0.00 | BC 261 |
| | | | | Min $M_z$ | 32.16 | 0.05 | 31.37 | -0.24 | 0.00 | ▷ -0.00 | BC 387 |
| | | 153 | 3256 | Max N | ▷ 35.85 | 0.05 | 16.53 | -0.25 | 77.89 | -0.15 | BC 391 |
| | | | | Min N | ▷ -32.89 | 0.01 | 36.93 | -0.01 | 175.20 | -0.05 | BC 240 |
| | | | | Max $V_y$ | 32.31 | ▷ 0.05 | 16.57 | -0.24 | 78.01 | -0.16 | BC 411 |
| | | | | Min $V_y$ | -4.40 | ▷ -0.00 | 28.81 | -0.03 | 137.55 | 0.00 | BC 53 |
| | | | | Max $V_z$ | -5.30 | 0.00 | ▷ 70.01 | -0.05 | 337.97 | -0.02 | BC 154 |
| | | | | Min $V_z$ | 35.85 | 0.05 | ▷ 16.53 | -0.25 | 77.89 | -0.15 | BC 419 |
| | | | | Max $M_T$ | -10.28 | 0.02 | 28.79 | ▷ 0.03 | 137.47 | -0.06 | BC 373 |
| | | | | Min $M_T$ | 35.85 | 0.05 | 16.53 | ▷ -0.25 | 77.89 | -0.15 | BC 391 |
| | | | | Max $M_y$ | -5.30 | 0.00 | 70.01 | -0.05 | ▷ 337.97 | -0.02 | BC 154 |
| | | | | Min $M_y$ | 35.85 | 0.05 | 16.53 | -0.25 | ▷ 77.89 | -0.15 | BC 419 |
| | | | | Max $M_z$ | -4.40 | -0.00 | 28.81 | -0.03 | 137.55 | ▷ 0.00 | BC 53 |
| | | | | Min $M_z$ | 32.31 | 0.05 | 16.57 | -0.24 | 78.01 | ▷ -0.16 | BC 411 |
| | | 68 | 0 | Max N | ▷ 36.13 | 0.05 | 31.32 | -0.25 | 0.00 | 0.00 | BC 391 |
| | | 153 | 3256 | Min N | ▷ -32.89 | 0.01 | 36.93 | -0.01 | 175.20 | -0.05 | BC 240 |
| | | 68 | 0 | Max $V_y$ | 32.59 | ▷ 0.05 | 31.36 | -0.24 | 0.00 | -0.00 | BC 411 |
| | | 68 | 0 | Min $V_y$ | -3.89 | ▷ -0.00 | 55.69 | -0.03 | -0.00 | 0.00 | BC 53 |
| | | 68 | 0 | Max $V_z$ | -4.02 | 0.00 | ▷ 137.61 | -0.05 | 0.00 | 0.00 | BC 154 |
| | | 153 | 3256 | Min $V_z$ | 35.85 | 0.05 | ▷ 16.53 | -0.25 | 77.89 | -0.15 | BC 419 |
| | | 68 | 0 | Max $M_T$ | -9.77 | 0.02 | 55.66 | ▷ 0.03 | 0.00 | 0.00 | BC 373 |
| | | 68 | 0 | Min $M_T$ | 36.13 | 0.05 | 31.32 | ▷ -0.25 | 0.00 | 0.00 | BC 391 |
| | | 153 | 3256 | Max $M_y$ | -5.30 | 0.00 | 70.01 | -0.05 | ▷ 337.97 | -0.02 | BC 154 |
| | | 68 | 0 | Min $M_y$ | -9.27 | 0.01 | 31.69 | 0.03 | ▷ -0.00 | 0.00 | BC 381 |
| | | 153 | 3256 | Max $M_z$ | -4.40 | -0.00 | 28.81 | -0.03 | 137.55 | ▷ 0.00 | BC 53 |
| | | 153 | 3256 | Min $M_z$ | 32.31 | 0.05 | 16.57 | -0.24 | 78.01 | ▷ -0.16 | BC 411 |
| 46 | RC1 | 68 | 0 | MAX N | ▷ 36.13 | 0.05 | 31.32 | -0.25 | 0.00 | 0.00 | BC 391 |
| 191 | RC1 | 83 | 3256 | MIN N | ▷ -33.40 | 0.01 | 0.56 | -0.01 | 231.71 | -0.07 | BC 240 |
| 191 | RC1 | 153 | 0 | MAX $V_y$ | 35.95 | ▷ 0.26 | 14.82 | -0.19 | 77.76 | -0.15 | BC 363 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 185 | RC1 | 147 | 0 | MIN $V_y$ | 16.59 | ▷ -0.27 | 15.88 | 0.17 | 77.80 | 0.11 | BC 411 |
| 46 | RC1 | 68 | 0 | MAX $V_z$ | -4.02 | 0.00 | ▷ 137.61 | -0.05 | 0.00 | 0.00 | BC 154 |
| 191 | RC1 | 83 | 3256 | MIN $V_z$ | -3.42 | 0.05 | ▷ -0.36 | -0.02 | 398.10 | -0.19 | BC 323 |
| 19 | RC1 | 53 | 0 | MAX $M_T$ | 16.29 | -0.03 | 31.54 | ▷ 0.22 | 0.00 | 0.00 | BC 411 |
| 46 | RC1 | 68 | 0 | MIN $M_T$ | 36.13 | 0.05 | 31.32 | ▷ -0.25 | 0.00 | 0.00 | BC 391 |
| 191 | RC1 | 83 | 3256 | MAX $M_y$ | -6.31 | 0.09 | -0.15 | -0.03 | ▷ 446.96 | -0.32 | BC 154 |
| 19 | RC1 | 53 | 0 | MIN $M_y$ | -10.05 | 0.04 | 31.34 | 0.03 | ▷ 0.00 | 0.00 | BC 381 |
| 185 | RC1 | 83 | 3201 | MAX $M_z$ | 16.80 | -0.27 | 1.41 | 0.17 | 105.80 | ▷ 0.99 | BC 363 |
| 191 | RC1 | 83 | 3256 | MIN $M_z$ | 35.67 | 0.26 | 0.02 | -0.19 | 101.92 | ▷ -0.98 | BC 363 |
| | **Doorgaande staven No. 15: Doorgaande staven 17** | | | | | | | | | | |
| 23 | RC1 | 55 | 0 | Max N | ▷ 12.08 | -0.02 | 31.00 | -0.18 | -0.00 | 0.00 | BC 450 |
| | | | | Min N | ▷ -25.42 | -0.01 | 54.26 | 0.01 | -0.00 | 0.00 | BC 392 |
| | | | | Max $V_y$ | 6.84 | ▷ 0.06 | 44.74 | 0.08 | 0.00 | 0.00 | BC 161 |
| | | | | Min $V_y$ | 0.58 | ▷ -0.06 | 68.55 | 0.02 | -0.00 | 0.00 | BC 247 |
| | | | | Max $V_z$ | -2.43 | -0.04 | ▷ 134.13 | 0.00 | 0.00 | 0.00 | BC 134 |
| | | | | Min $V_z$ | 5.85 | 0.06 | ▷ 30.30 | 0.09 | -0.00 | 0.00 | BC 473 |
| | | | | Max $M_T$ | 5.64 | 0.06 | 68.10 | ▷ 0.11 | 0.00 | 0.00 | BC 241 |
| | | | | Min $M_T$ | 12.04 | -0.00 | 30.98 | ▷ -0.19 | 0.00 | 0.00 | BC 446 |
| | | | | Max $M_y$ | 1.52 | -0.05 | 68.50 | 0.03 | ▷ 0.00 | 0.00 | BC 271 |
| | | | | Min $M_y$ | -24.73 | -0.00 | 68.62 | -0.02 | ▷ -0.00 | 0.00 | BC 204 |
| | | | | Max $M_z$ | -0.94 | -0.02 | 50.96 | -0.03 | 0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | -24.42 | -0.00 | 68.61 | -0.02 | 0.00 | ▷ -0.00 | BC 264 |
| | | 146 | 3201 | Max N | ▷ 12.34 | -0.02 | 16.71 | -0.18 | 76.35 | 0.05 | BC 450 |
| | | | | Min N | ▷ -24.94 | -0.01 | 28.35 | 0.01 | 132.21 | 0.02 | BC 392 |
| | | | | Max $V_y$ | 7.24 | ▷ 0.06 | 23.77 | 0.08 | 109.63 | -0.20 | BC 161 |
| | | | | Min $V_y$ | 1.19 | ▷ -0.06 | 35.96 | 0.02 | 167.24 | 0.18 | BC 247 |
| | | | | Max $V_z$ | -1.21 | -0.04 | ▷ 69.03 | 0.00 | 325.11 | 0.12 | BC 134 |
| | | | | Min $V_z$ | 6.12 | 0.06 | ▷ 16.01 | 0.09 | 74.11 | -0.19 | BC 473 |
| | | | | Max $M_T$ | 6.25 | 0.06 | 35.52 | ▷ 0.11 | 165.83 | -0.18 | BC 241 |
| | | | | Min $M_T$ | 12.31 | -0.00 | 16.68 | ▷ -0.19 | 76.28 | 0.01 | BC 446 |
| | | | | Max $M_y$ | -1.21 | -0.04 | 69.03 | 0.00 | ▷ 325.11 | 0.12 | BC 134 |
| | | | | Min $M_y$ | 6.12 | 0.06 | 16.01 | 0.09 | ▷ 74.11 | -0.19 | BC 473 |
| | | | | Max $M_z$ | 1.19 | -0.06 | 35.96 | 0.02 | 167.24 | ▷ 0.18 | BC 247 |
| | | | | Min $M_z$ | 7.24 | 0.06 | 23.77 | 0.08 | 109.63 | ▷ -0.20 | BC 161 |
| | | 146 | 3201 | Max N | ▷ 12.34 | -0.02 | 16.71 | -0.18 | 76.35 | 0.05 | BC 450 |
| | | 55 | 0 | Min N | ▷ -25.42 | -0.01 | 54.26 | 0.01 | -0.00 | 0.00 | BC 392 |
| | | 55 | 0 | Max $V_y$ | 6.84 | ▷ 0.06 | 44.74 | 0.08 | 0.00 | 0.00 | BC 161 |
| | | 55 | 0 | Min $V_y$ | 0.58 | ▷ -0.06 | 68.55 | 0.02 | -0.00 | 0.00 | BC 247 |
| | | 55 | 0 | Max $V_z$ | -2.43 | -0.04 | ▷ 134.13 | 0.00 | 0.00 | 0.00 | BC 134 |
| | | 146 | 3201 | Min $V_z$ | 6.12 | 0.06 | ▷ 16.01 | 0.09 | 74.11 | -0.19 | BC 473 |
| | | 55 | 0 | Max $M_T$ | 5.64 | 0.06 | 68.10 | ▷ 0.11 | 0.00 | 0.00 | BC 241 |
| | | 55 | 0 | Min $M_T$ | 12.04 | -0.00 | 30.98 | ▷ -0.19 | 0.00 | 0.00 | BC 446 |
| | | 146 | 3201 | Max $M_y$ | -1.21 | -0.04 | 69.03 | 0.00 | ▷ 325.11 | 0.12 | BC 134 |
| | | 55 | 0 | Min $M_y$ | -24.73 | -0.00 | 68.62 | -0.02 | ▷ -0.00 | 0.00 | BC 204 |
| | | 146 | 3201 | Max $M_z$ | 1.19 | -0.06 | 35.96 | 0.02 | 167.24 | ▷ 0.18 | BC 247 |
| | | 146 | 3201 | Min $M_z$ | 7.24 | 0.06 | 23.77 | 0.08 | 109.63 | ▷ -0.20 | BC 161 |
| 184 | RC1 | 146 | 0 | Max N | ▷ 12.38 | 0.21 | 15.60 | -0.12 | 76.25 | 0.05 | BC 450 |
| | | | | Min N | ▷ -24.85 | 0.08 | 27.23 | 0.03 | 132.00 | 0.02 | BC 392 |
| | | | | Max $V_y$ | -5.49 | ▷ 0.22 | 15.32 | 0.08 | 75.34 | 0.13 | BC 359 |
| | | | | Min $V_y$ | 6.31 | ▷ -0.35 | 33.94 | 0.01 | 165.57 | -0.18 | BC 241 |
| | | | | Max $V_z$ | -1.02 | 0.02 | ▷ 67.40 | 0.02 | 324.63 | 0.12 | BC 134 |
| | | | | Min $V_z$ | 6.21 | -0.31 | ▷ 14.95 | -0.01 | 73.99 | -0.19 | BC 469 |
| | | | | Max $M_T$ | -0.26 | 0.14 | 27.09 | ▷ 0.09 | 131.48 | 0.16 | BC 435 |
| | | | | Min $M_T$ | 12.34 | 0.21 | 15.58 | ▷ -0.13 | 76.15 | 0.01 | BC 446 |
| | | | | Max $M_y$ | -1.02 | 0.02 | 67.40 | 0.02 | ▷ 324.63 | 0.12 | BC 134 |
| | | | | Min $M_y$ | 6.13 | -0.32 | 14.95 | -0.01 | ▷ 73.99 | -0.19 | BC 473 |
| | | | | Max $M_z$ | 1.26 | 0.19 | 34.34 | 0.08 | 167.00 | ▷ 0.18 | BC 247 |
| | | | | Min $M_z$ | 7.27 | -0.29 | 22.18 | -0.01 | 109.48 | ▷ -0.20 | BC 161 |
| | | 84 | 3201 | Max N | ▷ 12.64 | 0.21 | 1.31 | -0.12 | 103.30 | -0.63 | BC 450 |
| | | | | Min N | ▷ -24.36 | 0.08 | 1.32 | 0.03 | 177.70 | -0.22 | BC 392 |
| | | | | Max $V_y$ | -5.22 | ▷ 0.22 | 1.02 | 0.08 | 101.49 | -0.59 | BC 359 |
| | | | | Min $V_y$ | 6.92 | ▷ -0.35 | 1.36 | 0.01 | 222.06 | 0.93 | BC 241 |
| | | | | Max $V_z$ | 0.20 | 0.02 | ▷ 2.30 | 0.02 | 436.17 | 0.05 | BC 134 |
| | | | | Min $V_z$ | 6.48 | -0.31 | ▷ 0.65 | -0.01 | 98.95 | 0.81 | BC 469 |
| | | | | Max $M_T$ | 0.23 | 0.14 | 1.18 | ▷ 0.09 | 176.72 | -0.31 | BC 435 |
| | | | | Min $M_T$ | 12.61 | 0.21 | 1.28 | ▷ -0.13 | 103.13 | -0.68 | BC 446 |
| | | | | Max $M_y$ | 0.20 | 0.02 | 2.30 | 0.02 | ▷ 436.17 | 0.05 | BC 134 |
| | | | | Min $M_y$ | 6.39 | -0.32 | 0.65 | -0.01 | ▷ 98.95 | 0.84 | BC 473 |
| | | | | Max $M_z$ | 6.92 | -0.35 | 1.36 | 0.01 | 222.06 | ▷ 0.93 | BC 241 |
| | | | | Min $M_z$ | 12.60 | 0.21 | 1.28 | -0.13 | 103.11 | ▷ -0.68 | BC 474 |
| | | 84 | 3201 | Max N | ▷ 12.64 | 0.21 | 1.31 | -0.12 | 103.30 | -0.63 | BC 450 |
| | | 146 | 0 | Min N | ▷ -24.85 | 0.08 | 27.23 | 0.03 | 132.00 | 0.02 | BC 392 |
| | | 146 | 0 | Max $V_y$ | -5.49 | ▷ 0.22 | 15.32 | 0.08 | 75.34 | 0.13 | BC 359 |
| | | 146 | 0 | Min $V_y$ | 6.31 | ▷ -0.35 | 33.94 | 0.01 | 165.57 | -0.18 | BC 241 |
| | | 146 | 0 | Max $V_z$ | -1.02 | 0.02 | ▷ 67.40 | 0.02 | 324.63 | 0.12 | BC 134 |
| | | 84 | 3201 | Min $V_z$ | 6.48 | -0.31 | ▷ 0.65 | -0.01 | 98.95 | 0.81 | BC 469 |
| | | 146 | 0 | Max $M_T$ | -0.26 | 0.14 | 27.09 | ▷ 0.09 | 131.48 | 0.16 | BC 435 |
| | | 146 | 0 | Min $M_T$ | 12.34 | 0.21 | 15.58 | ▷ -0.13 | 76.15 | 0.01 | BC 446 |
| | | 84 | 3201 | Max $M_y$ | 0.20 | 0.02 | 2.30 | 0.02 | ▷ 436.17 | 0.05 | BC 134 |
| | | 146 | 0 | Min $M_y$ | 6.13 | -0.32 | 14.95 | -0.01 | ▷ 73.99 | -0.19 | BC 473 |
| | | 84 | 3201 | Max $M_z$ | 6.92 | -0.35 | 1.36 | 0.01 | 222.06 | ▷ 0.93 | BC 241 |
| | | 84 | 3201 | Min $M_z$ | 12.60 | 0.21 | 1.28 | -0.13 | 103.11 | ▷ -0.68 | BC 474 |
| 190 | RC1 | 152 | 0 | Max N | ▷ 24.58 | -0.15 | 14.66 | 0.15 | 76.81 | 0.12 | BC 390 |
| | | | | Min N | ▷ -25.09 | -0.09 | 21.80 | 0.03 | 113.84 | 0.07 | BC 216 |
| | | | | Max $V_y$ | -23.61 | ▷ 0.29 | 33.87 | 0.02 | 172.37 | 0.03 | BC 241 |
| | | | | Min $V_y$ | -10.79 | ▷ -0.20 | 14.95 | -0.10 | 77.76 | -0.06 | BC 359 |
| | | | | Max $V_z$ | -9.26 | 0.04 | ▷ 66.06 | -0.01 | 330.81 | 0.03 | BC 155 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 190 | RC1 | | | Min $V_z$ | 24.58 | -0.15 | ▷ 14.66 | 0.15 | 76.81 | 0.12 | BC 390 |
| | | | | Max $M_T$ | 22.66 | -0.16 | 14.68 | ▷ 0.16 | 76.93 | 0.14 | BC 446 |
| | | | | Min $M_T$ | -12.25 | -0.16 | 14.97 | ▷ -0.11 | 77.98 | -0.09 | BC 447 |
| | | | | Max $M_y$ | -9.26 | 0.04 | 66.06 | -0.01 | ▷ 330.81 | 0.03 | BC 155 |
| | | | | Min $M_y$ | 24.58 | -0.15 | 14.66 | 0.15 | ▷ 76.81 | 0.12 | BC 390 |
| | | | | Max $M_z$ | 19.27 | -0.15 | 21.66 | 0.15 | 113.32 | ▷ 0.15 | BC 254 |
| | | | | Min $M_z$ | -12.25 | -0.16 | 14.97 | -0.11 | 77.98 | ▷ -0.09 | BC 447 |
| | | 84 | 3256 | Max N | ▷ 24.31 | -0.15 | 0.12 | 0.15 | 100.85 | 0.62 | BC 390 |
| | | | | Min N | ▷ -25.49 | -0.09 | 0.47 | 0.03 | 150.09 | 0.36 | BC 216 |
| | | | | Max $V_y$ | -24.23 | ▷ 0.29 | 0.73 | 0.02 | 228.70 | -0.93 | BC 241 |
| | | | | Min $V_y$ | -11.07 | ▷ -0.20 | 0.40 | -0.10 | 102.75 | 0.59 | BC 359 |
| | | | | Max $V_z$ | -23.97 | 0.26 | ▷ 0.93 | 0.04 | 153.14 | -0.80 | BC 277 |
| | | | | Min $V_z$ | -5.46 | 0.03 | ▷ -0.37 | -0.01 | 389.85 | -0.10 | BC 326 |
| | | | | Max $M_T$ | 22.39 | -0.16 | 0.14 | ▷ 0.16 | 101.06 | 0.67 | BC 446 |
| | | | | Min $M_T$ | -12.53 | -0.16 | 0.43 | ▷ -0.11 | 103.05 | 0.42 | BC 447 |
| | | | | Max $M_y$ | -10.51 | 0.04 | -0.16 | -0.01 | ▷ 438.09 | -0.10 | BC 155 |
| | | | | Min $M_y$ | 24.31 | -0.15 | 0.12 | 0.15 | ▷ 100.85 | 0.62 | BC 390 |
| | | | | Max $M_z$ | 22.20 | -0.16 | 0.14 | 0.16 | 101.08 | ▷ 0.67 | BC 474 |
| | | | | Min $M_z$ | -24.23 | 0.29 | 0.73 | 0.02 | 228.70 | ▷ -0.93 | BC 241 |
| | | 152 | 0 | Max N | ▷ 24.58 | -0.15 | 14.66 | 0.15 | 76.81 | 0.12 | BC 390 |
| | | 84 | 3256 | Min N | ▷ -25.49 | -0.09 | 0.47 | 0.03 | 150.09 | 0.36 | BC 216 |
| | | 152 | 0 | Max $V_y$ | -23.61 | ▷ 0.29 | 33.87 | 0.02 | 172.37 | 0.03 | BC 241 |
| | | 152 | 0 | Min $V_y$ | -10.79 | ▷ -0.20 | 14.95 | -0.10 | 77.76 | -0.06 | BC 359 |
| | | 152 | 0 | Max $V_z$ | -9.26 | 0.04 | ▷ 66.06 | -0.01 | 330.81 | 0.03 | BC 155 |
| | | 84 | 3256 | Min $V_z$ | -5.46 | 0.03 | ▷ -0.37 | -0.01 | 389.85 | -0.10 | BC 326 |
| | | 152 | 0 | Max $M_T$ | 22.66 | -0.16 | 14.68 | ▷ 0.16 | 76.93 | 0.14 | BC 446 |
| | | 152 | 0 | Min $M_T$ | -12.25 | -0.16 | 14.97 | ▷ -0.11 | 77.98 | -0.09 | BC 447 |
| | | 84 | 3256 | Max $M_y$ | -10.51 | 0.04 | -0.16 | -0.01 | ▷ 438.09 | -0.10 | BC 155 |
| | | 152 | 0 | Min $M_y$ | 24.58 | -0.15 | 14.66 | 0.15 | ▷ 76.81 | 0.12 | BC 390 |
| | | 84 | 3256 | Max $M_z$ | 22.20 | -0.16 | 0.14 | 0.16 | 101.08 | ▷ 0.67 | BC 474 |
| | | 84 | 3256 | Min $M_z$ | -24.23 | 0.29 | 0.73 | 0.02 | 228.70 | ▷ -0.93 | BC 241 |
| 45 | RC1 | 67 | 0 | Max N | ▷ 24.79 | -0.04 | 30.91 | 0.18 | -0.00 | 0.00 | BC 390 |
| | | | | Min N | ▷ -24.80 | -0.02 | 45.69 | 0.05 | 0.00 | 0.00 | BC 216 |
| | | | | Max $V_y$ | -12.05 | ▷ 0.03 | 31.26 | -0.07 | 0.00 | 0.00 | BC 447 |
| | | | | Min $V_y$ | 19.57 | ▷ -0.04 | 45.53 | 0.17 | -0.00 | 0.00 | BC 254 |
| | | | | Max $V_z$ | -8.29 | -0.01 | ▷ 134.88 | -0.02 | -0.00 | 0.00 | BC 155 |
| | | | | Min $V_z$ | 24.79 | -0.04 | ▷ 30.91 | 0.18 | -0.00 | 0.00 | BC 390 |
| | | | | Max $M_T$ | 22.87 | -0.04 | 30.94 | ▷ 0.19 | 0.00 | 0.00 | BC 446 |
| | | | | Min $M_T$ | -8.16 | 0.02 | 54.70 | ▷ -0.08 | 0.00 | 0.00 | BC 435 |
| | | | | Max $M_y$ | -7.32 | -0.01 | 69.24 | 0.00 | ▷ 0.00 | 0.00 | BC 91 |
| | | | | Min $M_y$ | -22.85 | -0.01 | 69.09 | 0.03 | ▷ -0.00 | 0.00 | BC 232 |
| | | | | Max $M_z$ | -23.31 | -0.01 | 69.60 | -0.04 | 0.00 | ▷ 0.00 | BC 205 |
| | | | | Min $M_z$ | -18.94 | -0.01 | 46.11 | -0.02 | -0.00 | ▷ -0.00 | BC 197 |
| | | 152 | 3256 | Max N | ▷ 24.51 | -0.04 | 16.36 | 0.18 | 76.94 | 0.12 | BC 390 |
| | | | | Min N | ▷ -25.20 | -0.02 | 24.36 | 0.05 | 114.02 | 0.07 | BC 216 |
| | | | | Max $V_y$ | -12.33 | ▷ 0.03 | 16.72 | -0.07 | 78.09 | -0.09 | BC 447 |
| | | | | Min $V_y$ | 19.17 | ▷ -0.04 | 24.20 | 0.17 | 113.51 | 0.15 | BC 254 |
| | | | | Max $V_z$ | -9.54 | -0.01 | ▷ 68.66 | -0.02 | 331.31 | 0.03 | BC 155 |
| | | | | Min $V_z$ | 24.51 | -0.04 | ▷ 16.36 | 0.18 | 76.94 | 0.12 | BC 390 |
| | | | | Max $M_T$ | 22.59 | -0.04 | 16.40 | ▷ 0.19 | 77.06 | 0.14 | BC 446 |
| | | | | Min $M_T$ | -8.66 | 0.02 | 28.35 | ▷ -0.08 | 135.18 | -0.07 | BC 435 |
| | | | | Max $M_y$ | -9.54 | -0.01 | 68.66 | -0.02 | ▷ 331.31 | 0.03 | BC 155 |
| | | | | Min $M_y$ | 24.51 | -0.04 | 16.36 | 0.18 | ▷ 76.94 | 0.12 | BC 390 |
| | | | | Max $M_z$ | 19.17 | -0.04 | 24.20 | 0.17 | 113.51 | ▷ 0.15 | BC 254 |
| | | | | Min $M_z$ | -12.33 | 0.03 | 16.72 | -0.07 | 78.09 | ▷ -0.09 | BC 447 |
| | | 67 | 0 | Max N | ▷ 24.79 | -0.04 | 30.91 | 0.18 | -0.00 | 0.00 | BC 390 |
| | | 152 | 3256 | Min N | ▷ -25.20 | -0.02 | 24.36 | 0.05 | 114.02 | 0.07 | BC 216 |
| | | 67 | 0 | Max $V_y$ | -12.05 | ▷ 0.03 | 31.26 | -0.07 | 0.00 | 0.00 | BC 447 |
| | | 67 | 0 | Min $V_y$ | 19.57 | ▷ -0.04 | 45.53 | 0.17 | -0.00 | 0.00 | BC 254 |
| | | 67 | 0 | Max $V_z$ | -8.29 | -0.01 | ▷ 134.88 | -0.02 | -0.00 | 0.00 | BC 155 |
| | | 152 | 3256 | Min $V_z$ | 24.51 | -0.04 | ▷ 16.36 | 0.18 | 76.94 | 0.12 | BC 390 |
| | | 67 | 0 | Max $M_T$ | 22.87 | -0.04 | 30.94 | ▷ 0.19 | 0.00 | 0.00 | BC 446 |
| | | 67 | 0 | Min $M_T$ | -8.16 | 0.02 | 54.70 | ▷ -0.08 | 0.00 | 0.00 | BC 435 |
| | | 152 | 3256 | Max $M_y$ | -9.54 | -0.01 | 68.66 | -0.02 | ▷ 331.31 | 0.03 | BC 155 |
| | | 67 | 0 | Min $M_y$ | -22.85 | -0.01 | 69.09 | 0.03 | ▷ -0.00 | 0.00 | BC 232 |
| | | 152 | 3256 | Max $M_z$ | 19.17 | -0.04 | 24.20 | 0.17 | 113.51 | ▷ 0.15 | BC 254 |
| | | 152 | 3256 | Min $M_z$ | -12.33 | 0.03 | 16.72 | -0.07 | 78.09 | ▷ -0.09 | BC 447 |
| 45 | RC1 | 67 | 0 | MAX N | ▷ 24.79 | -0.04 | 30.91 | 0.18 | 0.00 | 0.00 | BC 390 |
| 190 | RC1 | 84 | 3256 | MIN N | ▷ -25.49 | -0.09 | 0.47 | 0.03 | 150.09 | 0.36 | BC 216 |
| 190 | RC1 | 152 | 0 | MAX $V_y$ | -23.61 | ▷ 0.29 | 33.87 | 0.02 | 172.37 | 0.03 | BC 241 |
| 184 | RC1 | 146 | 0 | MIN $V_y$ | 6.31 | ▷ -0.35 | 33.94 | 0.01 | 165.57 | -0.18 | BC 241 |
| 45 | RC1 | 67 | 0 | MAX $V_z$ | -8.29 | -0.01 | ▷ 134.88 | -0.02 | 0.00 | 0.00 | BC 155 |
| 190 | RC1 | 84 | 3256 | MIN $V_z$ | -5.46 | 0.03 | ▷ -0.37 | -0.01 | 389.85 | -0.10 | BC 326 |
| 45 | RC1 | 67 | 0 | MAX $M_T$ | 22.87 | -0.04 | 30.94 | ▷ 0.19 | 0.00 | 0.00 | BC 446 |
| 23 | RC1 | 55 | 0 | MIN $M_T$ | 12.04 | 0.00 | 30.98 | ▷ -0.19 | 0.00 | 0.00 | BC 446 |
| 190 | RC1 | 84 | 3256 | MAX $M_y$ | -10.51 | 0.04 | -0.16 | -0.01 | ▷ 438.09 | -0.10 | BC 155 |
| 45 | RC1 | 67 | 0 | MIN $M_y$ | -22.85 | -0.01 | 69.09 | 0.03 | ▷ 0.00 | 0.00 | BC 232 |
| 184 | RC1 | 84 | 3201 | MAX $M_z$ | 6.92 | -0.35 | 1.36 | 0.01 | 222.06 | ▷ 0.93 | BC 241 |
| 190 | RC1 | 84 | 3256 | MIN $M_z$ | -24.23 | 0.29 | 0.73 | 0.02 | 228.70 | ▷ -0.93 | BC 241 |
| | **Doorgaande staven No. 16: Doorgaande staven 19** | | | | | | | | | | |
| 29 | RC1 | 44 | 0 | Max N | ▷ -10.36 | 0.17 | -23.79 | 0.00 | 0.00 | 0.00 | BC 356 |
| | | | Links | Min N | ▷ -123.30 | 0.27 | -21.77 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Max $V_y$ | -107.29 | ▷ 0.27 | -21.77 | 0.00 | 0.00 | 0.00 | BC 437 |
| | | | | Min $V_y$ | -62.37 | ▷ -0.01 | 22.36 | -0.00 | -0.00 | 0.00 | BC 182 |
| | | | | Max $V_z$ | -34.52 | -0.01 | ▷ 22.36 | -0.00 | -0.00 | 0.00 | BC 358 |
| | | | | Min $V_z$ | -23.07 | 0.17 | ▷ -23.80 | 0.00 | -0.00 | 0.00 | BC 432 |
| | | | | Max $M_T$ | -11.04 | 0.17 | -23.80 | ▷ 0.00 | 0.00 | 0.00 | BC 412 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 29 | RC1 | | | Min $M_T$ | -62.27 | -0.01 | 22.36 | ▷ -0.00 | 0.00 | 0.00 | BC 234 |
| | | | | Max $M_y$ | -94.16 | 0.25 | -21.77 | 0.00 | ▷ 0.00 | 0.00 | BC 381 |
| | | | | Min $M_y$ | -38.87 | 0.18 | -23.80 | 0.00 | ▷ -0.00 | 0.00 | BC 268 |
| | | | | Max $M_z$ | -50.40 | 0.01 | -13.98 | 0.00 | 0.00 | ▷ 0.00 | BC 163 |
| | | | | Min $M_z$ | -95.27 | 0.03 | -0.00 | -0.00 | 0.00 | ▷ -0.00 | BC 155 |
| | | | 0 | Max N | ▷ -10.36 | 0.17 | -23.79 | 0.00 | -0.00 | -0.00 | BC 356 |
| | | | Rechts | Min N | ▷ -123.30 | 0.27 | -21.77 | 0.00 | -0.00 | -0.00 | BC 241 |
| | | | | Max $V_y$ | -107.29 | ▷ 0.27 | -21.77 | 0.00 | -0.00 | -0.00 | BC 437 |
| | | | | Min $V_y$ | -62.37 | ▷ -0.01 | 22.36 | -0.00 | 0.00 | 0.00 | BC 182 |
| | | | | Max $V_z$ | -34.52 | -0.01 | ▷ 22.36 | -0.00 | 0.00 | 0.00 | BC 358 |
| | | | | Min $V_z$ | -23.07 | 0.17 | ▷ -23.80 | 0.00 | -0.00 | -0.00 | BC 432 |
| | | | | Max $M_T$ | -11.04 | 0.17 | -23.80 | ▷ 0.00 | -0.00 | -0.00 | BC 412 |
| | | | | Min $M_T$ | -62.27 | -0.01 | 22.36 | ▷ -0.00 | 0.00 | 0.00 | BC 234 |
| | | | | Max $M_y$ | -50.64 | -0.01 | 22.36 | -0.00 | ▷ 0.00 | 0.00 | BC 162 |
| | | | | Min $M_y$ | -38.87 | 0.18 | -23.80 | 0.00 | ▷ -0.00 | -0.00 | BC 268 |
| | | | | Max $M_z$ | -62.37 | -0.01 | 22.36 | -0.00 | 0.00 | ▷ 0.00 | BC 182 |
| | | | | Min $M_z$ | -107.43 | 0.27 | -21.77 | 0.00 | -0.00 | ▷ -0.00 | BC 433 |
| | | | 2500 | Max N | ▷ -8.36 | 0.17 | -8.70 | 0.00 | -40.61 | -0.43 | BC 356 |
| | | | Links | Min N | ▷ -120.38 | 0.27 | -8.02 | 0.00 | -37.24 | -0.66 | BC 241 |
| | | | | Max $V_y$ | -105.30 | ▷ 0.27 | -8.02 | 0.00 | -37.24 | -0.67 | BC 437 |
| | | | | Min $V_y$ | -59.44 | ▷ -0.01 | 8.24 | -0.00 | 38.25 | 0.03 | BC 182 |
| | | | | Max $V_z$ | -32.52 | -0.01 | ▷ 8.24 | -0.00 | 38.25 | 0.03 | BC 358 |
| | | | | Min $V_z$ | -21.07 | 0.17 | ▷ -8.70 | 0.00 | -40.63 | -0.43 | BC 432 |
| | | | | Max $M_T$ | -9.04 | 0.17 | -8.70 | ▷ 0.00 | -40.62 | -0.42 | BC 412 |
| | | | | Min $M_T$ | -59.34 | -0.01 | 8.24 | ▷ -0.00 | 38.25 | 0.02 | BC 234 |
| | | | | Max $M_y$ | -32.52 | -0.01 | 8.24 | -0.00 | ▷ 38.25 | 0.03 | BC 358 |
| | | | | Min $M_y$ | -21.07 | 0.17 | -8.70 | 0.00 | ▷ -40.63 | -0.43 | BC 432 |
| | | | | Max $M_z$ | -59.44 | -0.01 | 8.24 | -0.00 | 38.25 | ▷ 0.03 | BC 182 |
| | | | | Min $M_z$ | -105.30 | 0.27 | -8.02 | 0.00 | -37.24 | ▷ -0.67 | BC 437 |
| | | | 2500 | Max N | ▷ -8.36 | 0.17 | -8.70 | 0.00 | -40.61 | -0.43 | BC 356 |
| | | | Rechts | Min N | ▷ -120.38 | 0.27 | -8.02 | 0.00 | -37.24 | -0.66 | BC 241 |
| | | | | Max $V_y$ | -105.30 | ▷ 0.27 | -8.02 | 0.00 | -37.24 | -0.67 | BC 437 |
| | | | | Min $V_y$ | -59.44 | ▷ -0.01 | 8.24 | -0.00 | 38.25 | 0.03 | BC 182 |
| | | | | Max $V_z$ | -32.52 | -0.01 | ▷ 8.24 | -0.00 | 38.25 | 0.03 | BC 358 |
| | | | | Min $V_z$ | -21.07 | 0.17 | ▷ -8.70 | 0.00 | -40.63 | -0.43 | BC 432 |
| | | | | Max $M_T$ | -9.04 | 0.17 | -8.70 | ▷ 0.00 | -40.62 | -0.42 | BC 412 |
| | | | | Min $M_T$ | -59.34 | -0.01 | 8.24 | ▷ -0.00 | 38.25 | 0.02 | BC 234 |
| | | | | Max $M_y$ | -32.52 | -0.01 | 8.24 | -0.00 | ▷ 38.25 | 0.03 | BC 358 |
| | | | | Min $M_y$ | -21.07 | 0.17 | -8.70 | 0.00 | ▷ -40.63 | -0.43 | BC 432 |
| | | | | Max $M_z$ | -59.44 | -0.01 | 8.24 | -0.00 | 38.25 | ▷ 0.03 | BC 182 |
| | | | | Min $M_z$ | -105.30 | 0.27 | -8.02 | 0.00 | -37.24 | ▷ -0.67 | BC 437 |
| | | | 4345 | Max N | ▷ -3.68 | 0.17 | 2.45 | 0.00 | -46.38 | -0.74 | BC 356 |
| | | | Links | Min N | ▷ -113.51 | 0.27 | 2.12 | 0.00 | -42.69 | -1.15 | BC 241 |
| | | | | Max $V_y$ | -100.62 | ▷ 0.27 | 2.12 | 0.00 | -42.69 | -1.16 | BC 437 |
| | | | | Min $V_y$ | -52.57 | ▷ -0.01 | -2.18 | -0.00 | 43.84 | 0.06 | BC 182 |
| | | | | Max $V_z$ | -16.48 | 0.18 | ▷ 2.45 | 0.00 | -46.37 | -0.76 | BC 164 |
| | | | | Min $V_z$ | -52.60 | -0.01 | ▷ -2.18 | -0.00 | 43.84 | 0.06 | BC 242 |
| | | | | Max $M_T$ | -4.36 | 0.17 | 2.44 | ▷ 0.00 | -46.39 | -0.73 | BC 412 |
| | | | | Min $M_T$ | -52.48 | -0.01 | -2.18 | ▷ -0.00 | 43.84 | 0.03 | BC 234 |
| | | | | Max $M_y$ | -27.84 | -0.01 | -2.18 | -0.00 | ▷ 43.85 | 0.05 | BC 358 |
| | | | | Min $M_y$ | -16.39 | 0.17 | 2.44 | 0.00 | ▷ -46.41 | -0.75 | BC 432 |
| | | | | Max $M_z$ | -52.57 | -0.01 | -2.18 | -0.00 | 43.84 | ▷ 0.06 | BC 182 |
| | | | | Min $M_z$ | -100.62 | 0.27 | 2.12 | 0.00 | -42.69 | ▷ -1.16 | BC 437 |
| | | 69 | 4345 | Max N | ▷ -3.68 | 0.17 | 2.45 | 0.00 | -46.38 | -0.74 | BC 356 |
| | | | Rechts | Min N | ▷ -113.51 | 0.27 | 2.12 | 0.00 | -42.69 | -1.15 | BC 241 |
| | | | | Max $V_y$ | -100.62 | ▷ 0.27 | 2.12 | 0.00 | -42.69 | -1.16 | BC 437 |
| | | | | Min $V_y$ | -52.57 | ▷ -0.01 | -2.18 | -0.00 | 43.84 | 0.06 | BC 182 |
| | | | | Max $V_z$ | -16.48 | 0.18 | ▷ 2.45 | 0.00 | -46.37 | -0.76 | BC 164 |
| | | | | Min $V_z$ | -52.60 | -0.01 | ▷ -2.18 | -0.00 | 43.84 | 0.06 | BC 242 |
| | | | | Max $M_T$ | -4.36 | 0.17 | 2.44 | ▷ 0.00 | -46.39 | -0.73 | BC 412 |
| | | | | Min $M_T$ | -52.48 | -0.01 | -2.18 | ▷ -0.00 | 43.84 | 0.03 | BC 234 |
| | | | | Max $M_y$ | -27.84 | -0.01 | -2.18 | -0.00 | ▷ 43.85 | 0.05 | BC 358 |
| | | | | Min $M_y$ | -16.39 | 0.17 | 2.44 | 0.00 | ▷ -46.41 | -0.75 | BC 432 |
| | | | | Max $M_z$ | -52.57 | -0.01 | -2.18 | -0.00 | 43.84 | ▷ 0.06 | BC 182 |
| | | | | Min $M_z$ | -100.62 | 0.27 | 2.12 | 0.00 | -42.69 | ▷ -1.16 | BC 437 |
| | | 69 | 4345 | Max N | ▷ -3.68 | 0.17 | 2.45 | 0.00 | -46.38 | -0.74 | BC 356 |
| | | 44 | 0 | Min N | ▷ -123.30 | 0.27 | -21.77 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | 44 | 0 | Max $V_y$ | -107.29 | ▷ 0.27 | -21.77 | 0.00 | 0.00 | 0.00 | BC 437 |
| | | 44 | 0 | Min $V_y$ | -62.37 | ▷ -0.01 | 22.36 | -0.00 | -0.00 | 0.00 | BC 182 |
| | | 44 | 0 | Max $V_z$ | -34.52 | -0.01 | ▷ 22.36 | -0.00 | -0.00 | 0.00 | BC 358 |
| | | 44 | 0 | Min $V_z$ | -23.07 | 0.17 | ▷ -23.80 | 0.00 | -0.00 | 0.00 | BC 432 |
| | | 44 | 0 | Max $M_T$ | -11.04 | 0.17 | -23.80 | ▷ 0.00 | 0.00 | 0.00 | BC 412 |
| | | 44 | 0 | Min $M_T$ | -62.27 | -0.01 | 22.36 | ▷ -0.00 | 0.00 | 0.00 | BC 234 |
| | | | 3950 | Max $M_y$ | -28.84 | -0.01 | 0.05 | -0.00 | ▷ 44.27 | 0.04 | BC 358 |
| | | | 3950 | Min $M_y$ | -17.39 | 0.17 | 0.05 | 0.00 | ▷ -46.90 | -0.68 | BC 432 |
| | | 69 | 4345 | Max $M_z$ | -52.57 | -0.01 | -2.18 | -0.00 | 43.84 | ▷ 0.06 | BC 182 |
| | | 69 | 4345 | Min $M_z$ | -100.62 | 0.27 | 2.12 | 0.00 | -42.69 | ▷ -1.16 | BC 437 |
| 151 | RC1 | 69 | 0 | Max N | ▷ -24.58 | -0.53 | 2.45 | 0.00 | -46.38 | -0.74 | BC 356 |
| | | | Links | Min N | ▷ -80.57 | -0.23 | -0.00 | -0.00 | -0.01 | -0.13 | BC 148 |
| | | | | Max $V_y$ | -24.94 | ▷ -0.05 | -0.00 | -0.00 | -0.00 | -0.01 | BC 63 |
| | | | | Min $V_y$ | -71.41 | ▷ -1.75 | 2.12 | 0.00 | -42.69 | -1.15 | BC 241 |
| | | | | Max $V_z$ | -36.21 | -0.56 | ▷ 2.45 | 0.00 | -46.38 | -0.76 | BC 164 |
| | | | | Min $V_z$ | -48.31 | -0.09 | ▷ -2.18 | -0.00 | 43.84 | 0.06 | BC 242 |
| | | | | Max $M_T$ | -24.59 | -0.52 | 2.44 | ▷ 0.00 | -46.40 | -0.73 | BC 412 |
| | | | | Min $M_T$ | -48.27 | -0.09 | -2.18 | ▷ -0.00 | 43.84 | 0.03 | BC 234 |
| | | | | Max $M_y$ | -25.43 | -0.05 | -2.18 | -0.00 | ▷ 43.85 | 0.05 | BC 358 |
| | | | | Min $M_y$ | -36.06 | -0.54 | 2.44 | 0.00 | ▷ -46.41 | -0.75 | BC 432 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 151 | RC1 | | | Max $M_z$ | -48.31 | -0.09 | -2.18 | -0.00 | 43.84 | 0.06 | BC 182 |
| | | | | Min $M_z$ | -59.85 | -1.74 | 2.12 | 0.00 | -42.69 | -1.16 | BC 437 |
| | | | 0 | Max N | -24.58 | -0.53 | 2.45 | 0.00 | -46.38 | -0.74 | BC 356 |
| | | | Rechts | Min N | -80.57 | -0.23 | -0.00 | -0.00 | -0.01 | -0.12 | BC 148 |
| | | | | Max $V_y$ | -24.94 | -0.05 | -0.00 | -0.00 | -0.00 | -0.01 | BC 63 |
| | | | | Min $V_y$ | -71.41 | -1.75 | 2.12 | 0.00 | -42.69 | -1.15 | BC 241 |
| | | | | Max $V_z$ | -36.21 | -0.56 | 2.45 | 0.00 | -46.38 | -0.76 | BC 164 |
| | | | | Min $V_z$ | -48.31 | -0.09 | -2.18 | -0.00 | 43.84 | 0.06 | BC 242 |
| | | | | Max $M_T$ | -24.59 | -0.52 | 2.44 | 0.00 | -46.40 | -0.73 | BC 412 |
| | | | | Min $M_T$ | -48.27 | -0.09 | -2.18 | -0.00 | 43.84 | 0.03 | BC 234 |
| | | | | Max $M_y$ | -25.43 | -0.05 | -2.18 | -0.00 | 43.85 | 0.05 | BC 358 |
| | | | | Min $M_y$ | -36.06 | -0.54 | 2.44 | 0.00 | -46.41 | -0.75 | BC 432 |
| | | | | Max $M_z$ | -48.31 | -0.09 | -2.18 | -0.00 | 43.84 | 0.06 | BC 182 |
| | | | | Min $M_z$ | -59.85 | -1.74 | 2.12 | 0.00 | -42.69 | -1.16 | BC 437 |
| | | | 3565 | Max N | -15.48 | -0.53 | 23.97 | 0.00 | 0.71 | 1.14 | BC 356 |
| | | | Links | Min N | -67.23 | -0.23 | -0.00 | -0.00 | -0.03 | 0.69 | BC 148 |
| | | | | Max $V_y$ | -15.85 | -0.05 | -0.00 | -0.00 | -0.00 | 0.15 | BC 63 |
| | | | | Min $V_y$ | -58.08 | -1.75 | 21.71 | 0.00 | -0.22 | 5.09 | BC 241 |
| | | | | Max $V_z$ | -22.87 | -0.56 | 23.97 | 0.00 | 0.72 | 1.22 | BC 164 |
| | | | | Min $V_z$ | -27.74 | -0.08 | -22.31 | -0.00 | 0.19 | 0.33 | BC 434 |
| | | | | Max $M_T$ | -15.49 | -0.52 | 23.97 | 0.00 | 0.68 | 1.11 | BC 412 |
| | | | | Min $M_T$ | -34.93 | -0.09 | -22.31 | -0.00 | 0.19 | 0.36 | BC 234 |
| | | | | Max $M_y$ | -22.87 | -0.56 | 23.97 | 0.00 | 0.72 | 1.22 | BC 164 |
| | | | | Min $M_y$ | -58.08 | -1.75 | 21.71 | 0.00 | -0.22 | 5.09 | BC 241 |
| | | | | Max $M_z$ | -58.08 | -1.75 | 21.71 | 0.00 | -0.22 | 5.09 | BC 241 |
| | | | | Min $M_z$ | -15.84 | -0.05 | -0.00 | -0.00 | -0.00 | 0.15 | BC 64 |
| | | | 3565 | Max N | -15.48 | -0.53 | 23.97 | 0.00 | 0.71 | 1.14 | BC 356 |
| | | | Rechts | Min N | -67.23 | -0.23 | -0.00 | -0.00 | -0.03 | 0.69 | BC 148 |
| | | | | Max $V_y$ | -15.85 | -0.05 | -0.00 | -0.00 | -0.00 | 0.15 | BC 63 |
| | | | | Min $V_y$ | -58.08 | -1.75 | 21.71 | 0.00 | -0.21 | 5.09 | BC 241 |
| | | | | Max $V_z$ | -22.87 | -0.56 | 23.97 | 0.00 | 0.72 | 1.22 | BC 164 |
| | | | | Min $V_z$ | -27.74 | -0.08 | -22.31 | -0.00 | 0.19 | 0.33 | BC 434 |
| | | | | Max $M_T$ | -15.49 | -0.52 | 23.97 | 0.00 | 0.68 | 1.11 | BC 412 |
| | | | | Min $M_T$ | -34.93 | -0.09 | -22.31 | -0.00 | 0.19 | 0.36 | BC 234 |
| | | | | Max $M_y$ | -22.87 | -0.56 | 23.97 | 0.00 | 0.72 | 1.22 | BC 164 |
| | | | | Min $M_y$ | -58.08 | -1.75 | 21.71 | 0.00 | -0.21 | 5.09 | BC 241 |
| | | | | Max $M_z$ | -58.08 | -1.75 | 21.71 | 0.00 | -0.21 | 5.09 | BC 241 |
| | | | | Min $M_z$ | -15.84 | -0.05 | -0.00 | -0.00 | -0.00 | 0.15 | BC 64 |
| | | | 3625 | Max N | -15.35 | -0.53 | 24.34 | 0.00 | 2.16 | 1.18 | BC 356 |
| | | | Links | Min N | -67.05 | -0.23 | -0.00 | -0.00 | -0.03 | 0.71 | BC 148 |
| | | | | Max $V_y$ | -15.72 | -0.05 | -0.00 | -0.00 | -0.00 | 0.16 | BC 63 |
| | | | | Min $V_y$ | -57.89 | -1.75 | 22.04 | 0.00 | 1.10 | 5.19 | BC 241 |
| | | | | Max $V_z$ | -22.68 | -0.56 | 24.34 | 0.00 | 2.17 | 1.26 | BC 164 |
| | | | | Min $V_z$ | -27.61 | -0.08 | -22.65 | -0.00 | -1.16 | 0.33 | BC 434 |
| | | | | Max $M_T$ | -15.37 | -0.52 | 24.33 | 0.00 | 2.13 | 1.15 | BC 412 |
| | | | | Min $M_T$ | -34.74 | -0.09 | -22.65 | -0.00 | -1.16 | 0.37 | BC 234 |
| | | | | Max $M_y$ | -22.68 | -0.56 | 24.34 | 0.00 | 2.17 | 1.26 | BC 164 |
| | | | | Min $M_y$ | -34.79 | -0.09 | -22.65 | -0.00 | -1.16 | 0.38 | BC 242 |
| | | | | Max $M_z$ | -57.89 | -1.75 | 22.04 | 0.00 | 1.10 | 5.19 | BC 241 |
| | | | | Min $M_z$ | -15.72 | -0.05 | -0.00 | -0.00 | -0.00 | 0.16 | BC 64 |
| | | 35 | 3625 | Max N | -15.35 | -0.53 | 24.34 | 0.00 | 2.16 | 1.18 | BC 356 |
| | | | Rechts | Min N | -67.05 | -0.23 | -0.00 | -0.00 | -0.03 | 0.71 | BC 148 |
| | | | | Max $V_y$ | -15.72 | -0.05 | -0.00 | -0.00 | -0.00 | 0.16 | BC 63 |
| | | | | Min $V_y$ | -57.89 | -1.75 | 22.04 | 0.00 | 1.10 | 5.19 | BC 241 |
| | | | | Max $V_z$ | -22.68 | -0.56 | 24.34 | 0.00 | 2.17 | 1.26 | BC 164 |
| | | | | Min $V_z$ | -27.61 | -0.08 | -22.65 | -0.00 | -1.16 | 0.33 | BC 434 |
| | | | | Max $M_T$ | -15.37 | -0.52 | 24.33 | 0.00 | 2.13 | 1.15 | BC 412 |
| | | | | Min $M_T$ | -34.74 | -0.09 | -22.65 | -0.00 | -1.16 | 0.37 | BC 234 |
| | | | | Max $M_y$ | -22.68 | -0.56 | 24.34 | 0.00 | 2.17 | 1.26 | BC 164 |
| | | | | Min $M_y$ | -34.79 | -0.09 | -22.65 | -0.00 | -1.16 | 0.38 | BC 242 |
| | | | | Max $M_z$ | -57.89 | -1.75 | 22.04 | 0.00 | 1.10 | 5.19 | BC 241 |
| | | | | Min $M_z$ | -15.72 | -0.05 | -0.00 | -0.00 | -0.00 | 0.16 | BC 64 |
| | | 35 | 3625 | Max N | -15.35 | -0.53 | 24.34 | 0.00 | 2.16 | 1.18 | BC 356 |
| | | 69 | 0 | Min N | -80.57 | -0.23 | -0.00 | -0.00 | -0.01 | -0.13 | BC 148 |
| | | 69 | 0 | Max $V_y$ | -24.94 | -0.05 | -0.00 | -0.00 | -0.00 | -0.01 | BC 63 |
| | | 69 | 0 | Min $V_y$ | -71.41 | -1.75 | 2.12 | 0.00 | -42.69 | -1.15 | BC 241 |
| | | 35 | 3625 | Max $V_z$ | -22.68 | -0.56 | 24.34 | 0.00 | 2.17 | 1.26 | BC 164 |
| | | 35 | 3625 | Min $V_z$ | -27.61 | -0.08 | -22.65 | -0.00 | -1.16 | 0.33 | BC 434 |
| | | 69 | 0 | Max $M_T$ | -24.59 | -0.52 | 2.44 | 0.00 | -46.40 | -0.73 | BC 412 |
| | | 69 | 0 | Min $M_T$ | -48.27 | -0.09 | -2.18 | -0.00 | 43.84 | 0.03 | BC 234 |
| | | 69 | 0 | Max $M_y$ | -25.43 | -0.05 | -2.18 | -0.00 | 43.85 | 0.05 | BC 358 |
| | | 69 | 0 | Min $M_y$ | -36.06 | -0.54 | 2.44 | 0.00 | -46.41 | -0.75 | BC 432 |
| | | 35 | 3625 | Max $M_z$ | -57.89 | -1.75 | 22.04 | 0.00 | 1.10 | 5.19 | BC 241 |
| | | 69 | 0 | Min $M_z$ | -59.85 | -1.74 | 2.12 | 0.00 | -42.69 | -1.16 | BC 437 |
| 29 | RC1 | 69 | 4345 | MAX N | -3.68 | 0.17 | 2.45 | 0.00 | -46.38 | -0.74 | BC 356 |
| 29 | RC1 | 44 | 0 | MIN N | -123.30 | 0.27 | -21.77 | 0.00 | 0.00 | 0.00 | BC 241 |
| 29 | RC1 | 44 | 0 | MAX $V_y$ | -107.29 | 0.27 | -21.77 | 0.00 | 0.00 | 0.00 | BC 437 |
| 151 | RC1 | 69 | 0 | MIN $V_y$ | -71.41 | -1.75 | 2.12 | 0.00 | -42.69 | -1.15 | BC 241 |
| 151 | RC1 | 35 | 3625 | MAX $V_z$ | -22.68 | -0.56 | 24.34 | 0.00 | 2.17 | 1.26 | BC 164 |
| 29 | RC1 | 44 | 0 | MIN $V_z$ | -23.07 | 0.17 | -23.80 | 0.00 | 0.00 | 0.00 | BC 432 |
| 29 | RC1 | 44 | 0 | MAX $M_T$ | -11.04 | 0.17 | -23.80 | 0.00 | 0.00 | 0.00 | BC 412 |
| 29 | RC1 | 44 | 0 | MIN $M_T$ | -62.27 | -0.01 | 22.36 | 0.00 | 0.00 | 0.00 | BC 234 |
| 29 | RC1 | | 3950 | MAX $M_y$ | -28.84 | -0.01 | 0.05 | 0.00 | 44.27 | 0.04 | BC 358 |
| 29 | RC1 | | 3950 | MIN $M_y$ | -17.39 | 0.17 | 0.05 | 0.00 | -46.90 | -0.68 | BC 432 |
| 151 | RC1 | 35 | 3625 | MAX $M_z$ | -57.89 | -1.75 | 22.04 | 0.00 | 1.10 | 5.19 | BC 241 |
| 29 | RC1 | 69 | 4345 | MIN $M_z$ | -100.62 | 0.27 | 2.12 | 0.00 | -42.69 | -1.16 | BC 437 |

**Doorgaande staven No. 17: Doorgaande staven 20**

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 30 | RC1 | 47 | 0 | Max N | ▷ -11.92 | -0.19 | -24.18 | -0.00 | 0.00 | 0.00 | BC 445 |
| | | | Links | Min N | ▷ -122.90 | -0.26 | -22.18 | -0.00 | -0.00 | 0.00 | BC 200 |
| | | | | Max $V_y$ | -52.00 | ▷ 0.01 | 22.76 | 0.00 | -0.00 | 0.00 | BC 218 |
| | | | | Min $V_y$ | -112.52 | ▷ -0.26 | -22.18 | -0.00 | 0.00 | 0.00 | BC 164 |
| | | | | Max $V_z$ | -35.44 | 0.01 | ▷ 22.76 | 0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Min $V_z$ | -28.94 | -0.19 | ▷ -24.18 | -0.00 | 0.00 | 0.00 | BC 165 |
| | | | | Max $M_T$ | -63.30 | 0.00 | 22.76 | ▷ 0.00 | 0.00 | 0.00 | BC 214 |
| | | | | Min $M_T$ | -122.21 | -0.25 | -22.18 | ▷ -0.00 | -0.00 | 0.00 | BC 264 |
| | | | | Max $M_y$ | -121.64 | -0.25 | -22.18 | -0.00 | ▷ 0.00 | 0.00 | BC 268 |
| | | | | Min $M_y$ | -95.64 | -0.26 | -22.18 | -0.00 | ▷ -0.00 | 0.00 | BC 356 |
| | | | | Max $M_z$ | -52.37 | -0.00 | -14.23 | -0.00 | -0.00 | ▷ 0.00 | BC 163 |
| | | | | Min $M_z$ | -62.98 | -0.02 | -0.00 | -0.00 | 0.00 | ▷ -0.00 | BC 85 |
| | | | 0 | Max N | ▷ -11.92 | -0.19 | -24.18 | -0.00 | -0.00 | 0.00 | BC 445 |
| | | | Rechts | Min N | ▷ -122.90 | -0.26 | -22.18 | -0.00 | -0.00 | 0.00 | BC 200 |
| | | | | Max $V_y$ | -52.00 | ▷ 0.01 | 22.76 | 0.00 | 0.00 | -0.00 | BC 218 |
| | | | | Min $V_y$ | -112.52 | ▷ -0.26 | -22.18 | -0.00 | -0.00 | 0.00 | BC 164 |
| | | | | Max $V_z$ | -35.44 | 0.01 | ▷ 22.76 | 0.00 | 0.00 | -0.00 | BC 446 |
| | | | | Min $V_z$ | -28.94 | -0.19 | ▷ -24.18 | -0.00 | -0.00 | 0.00 | BC 165 |
| | | | | Max $M_T$ | -63.30 | 0.00 | 22.76 | ▷ 0.00 | 0.00 | -0.00 | BC 214 |
| | | | | Min $M_T$ | -122.21 | -0.25 | -22.18 | ▷ -0.00 | -0.00 | 0.00 | BC 264 |
| | | | | Max $M_y$ | -52.05 | 0.01 | 22.76 | 0.00 | ▷ 0.00 | -0.00 | BC 166 |
| | | | | Min $M_y$ | -12.22 | -0.19 | -24.18 | -0.00 | ▷ -0.00 | 0.00 | BC 381 |
| | | | | Max $M_z$ | -112.52 | -0.26 | -22.18 | -0.00 | -0.00 | ▷ 0.00 | BC 164 |
| | | | | Min $M_z$ | -51.96 | 0.01 | 22.76 | 0.00 | 0.00 | ▷ -0.00 | BC 190 |
| | | | 2500 | Max N | ▷ -9.93 | -0.19 | -9.07 | -0.00 | -41.56 | 0.48 | BC 445 |
| | | | Links | Min N | ▷ -119.98 | -0.26 | -8.39 | -0.00 | -38.21 | 0.65 | BC 200 |
| | | | | Max $V_y$ | -49.07 | ▷ 0.01 | 8.61 | 0.00 | 39.21 | -0.03 | BC 218 |
| | | | | Min $V_y$ | -109.59 | ▷ -0.26 | -8.39 | -0.00 | -38.20 | 0.66 | BC 164 |
| | | | | Max $V_z$ | -44.85 | 0.00 | ▷ 8.61 | 0.00 | 39.21 | -0.01 | BC 434 |
| | | | | Min $V_z$ | -26.01 | -0.19 | ▷ -9.08 | -0.00 | -41.57 | 0.48 | BC 165 |
| | | | | Max $M_T$ | -60.37 | 0.00 | 8.61 | ▷ 0.00 | 39.21 | -0.01 | BC 214 |
| | | | | Min $M_T$ | -119.29 | -0.25 | -8.39 | ▷ -0.00 | -38.21 | 0.64 | BC 264 |
| | | | | Max $M_y$ | -33.44 | 0.01 | 8.61 | 0.00 | ▷ 39.21 | -0.02 | BC 446 |
| | | | | Min $M_y$ | -26.01 | -0.19 | -9.08 | -0.00 | ▷ -41.57 | 0.48 | BC 165 |
| | | | | Max $M_z$ | -109.59 | -0.26 | -8.39 | -0.00 | -38.20 | ▷ 0.66 | BC 164 |
| | | | | Min $M_z$ | -49.07 | 0.01 | 8.61 | 0.00 | 39.21 | ▷ -0.03 | BC 218 |
| | | | 2500 | Max N | ▷ -9.93 | -0.19 | -9.07 | -0.00 | -41.56 | 0.48 | BC 445 |
| | | | Rechts | Min N | ▷ -119.98 | -0.26 | -8.39 | -0.00 | -38.21 | 0.65 | BC 200 |
| | | | | Max $V_y$ | -49.07 | ▷ 0.01 | 8.61 | 0.00 | 39.21 | -0.03 | BC 218 |
| | | | | Min $V_y$ | -109.59 | ▷ -0.26 | -8.39 | -0.00 | -38.20 | 0.66 | BC 164 |
| | | | | Max $V_z$ | -44.85 | 0.00 | ▷ 8.61 | 0.00 | 39.21 | -0.01 | BC 434 |
| | | | | Min $V_z$ | -26.01 | -0.19 | ▷ -9.08 | -0.00 | -41.57 | 0.48 | BC 165 |
| | | | | Max $M_T$ | -60.37 | 0.00 | 8.61 | ▷ 0.00 | 39.21 | -0.01 | BC 214 |
| | | | | Min $M_T$ | -119.29 | -0.25 | -8.39 | ▷ -0.00 | -38.21 | 0.64 | BC 264 |
| | | | | Max $M_y$ | -33.44 | 0.01 | 8.61 | 0.00 | ▷ 39.21 | -0.02 | BC 446 |
| | | | | Min $M_y$ | -26.01 | -0.19 | -9.08 | -0.00 | ▷ -41.57 | 0.48 | BC 165 |
| | | | | Max $M_z$ | -109.59 | -0.26 | -8.39 | -0.00 | -38.20 | ▷ 0.66 | BC 164 |
| | | | | Min $M_z$ | -49.07 | 0.01 | 8.61 | 0.00 | 39.21 | ▷ -0.03 | BC 218 |
| | | | 4345 | Max N | ▷ -5.24 | -0.19 | 2.07 | -0.00 | -48.02 | 0.83 | BC 445 |
| | | | Links | Min N | ▷ -113.11 | -0.26 | 1.78 | -0.00 | -44.30 | 1.13 | BC 200 |
| | | | | Max $V_y$ | -42.20 | ▷ 0.01 | -1.84 | 0.00 | 45.46 | -0.06 | BC 218 |
| | | | | Min $V_y$ | -102.72 | ▷ -0.26 | 1.79 | -0.00 | -44.30 | 1.14 | BC 164 |
| | | | | Max $V_z$ | -16.33 | -0.20 | ▷ 2.07 | -0.00 | -48.01 | 0.85 | BC 433 |
| | | | | Min $V_z$ | -42.25 | 0.01 | ▷ -1.84 | 0.00 | 45.46 | -0.05 | BC 166 |
| | | | | Max $M_T$ | -53.50 | 0.00 | -1.84 | ▷ 0.00 | 45.46 | -0.02 | BC 214 |
| | | | | Min $M_T$ | -112.42 | -0.25 | 1.78 | ▷ -0.00 | -44.30 | 1.11 | BC 264 |
| | | | | Max $M_y$ | -28.76 | 0.01 | -1.84 | 0.00 | ▷ 45.46 | -0.04 | BC 446 |
| | | | | Min $M_y$ | -19.14 | -0.19 | 2.07 | -0.00 | ▷ -48.04 | 0.84 | BC 165 |
| | | | | Max $M_z$ | -102.72 | -0.26 | 1.79 | -0.00 | -44.30 | ▷ 1.14 | BC 164 |
| | | | | Min $M_z$ | -42.20 | 0.01 | -1.84 | 0.00 | 45.46 | ▷ -0.06 | BC 218 |
| | | 70 | 4345 | Max N | ▷ -5.24 | -0.19 | 2.07 | -0.00 | -48.02 | 0.83 | BC 445 |
| | | | Rechts | Min N | ▷ -113.11 | -0.26 | 1.78 | -0.00 | -44.30 | 1.13 | BC 200 |
| | | | | Max $V_y$ | -42.20 | ▷ 0.01 | -1.84 | 0.00 | 45.46 | -0.06 | BC 218 |
| | | | | Min $V_y$ | -102.72 | ▷ -0.26 | 1.79 | -0.00 | -44.30 | 1.14 | BC 164 |
| | | | | Max $V_z$ | -16.33 | -0.20 | ▷ 2.07 | -0.00 | -48.01 | 0.85 | BC 433 |
| | | | | Min $V_z$ | -42.25 | 0.01 | ▷ -1.84 | 0.00 | 45.46 | -0.05 | BC 166 |
| | | | | Max $M_T$ | -53.50 | 0.00 | -1.84 | ▷ 0.00 | 45.46 | -0.02 | BC 214 |
| | | | | Min $M_T$ | -112.42 | -0.25 | 1.78 | ▷ -0.00 | -44.30 | 1.11 | BC 264 |
| | | | | Max $M_y$ | -28.76 | 0.01 | -1.84 | 0.00 | ▷ 45.46 | -0.04 | BC 446 |
| | | | | Min $M_y$ | -19.14 | -0.19 | 2.07 | -0.00 | ▷ -48.04 | 0.84 | BC 165 |
| | | | | Max $M_z$ | -102.72 | -0.26 | 1.79 | -0.00 | -44.30 | ▷ 1.14 | BC 164 |
| | | | | Min $M_z$ | -42.20 | 0.01 | -1.84 | 0.00 | 45.46 | ▷ -0.06 | BC 218 |
| | | 70 | 4345 | Max N | ▷ -5.24 | -0.19 | 2.07 | -0.00 | -48.02 | 0.83 | BC 445 |
| | | 47 | 0 | Min N | ▷ -122.90 | -0.26 | -22.18 | -0.00 | -0.00 | 0.00 | BC 200 |
| | | 47 | 0 | Max $V_y$ | -52.00 | ▷ 0.01 | 22.76 | 0.00 | -0.00 | 0.00 | BC 218 |
| | | 47 | 0 | Min $V_y$ | -112.52 | ▷ -0.26 | -22.18 | -0.00 | 0.00 | 0.00 | BC 164 |
| | | 47 | 0 | Max $V_z$ | -35.44 | 0.01 | ▷ 22.76 | 0.00 | 0.00 | 0.00 | BC 446 |
| | | 47 | 0 | Min $V_z$ | -28.94 | -0.19 | ▷ -24.18 | -0.00 | 0.00 | 0.00 | BC 165 |
| | | 47 | 0 | Max $M_T$ | -63.30 | 0.00 | 22.76 | ▷ 0.00 | 0.00 | 0.00 | BC 214 |
| | | 47 | 0 | Min $M_T$ | -122.21 | -0.25 | -22.18 | ▷ -0.00 | -0.00 | 0.00 | BC 264 |
| | | | 3950 | Max $M_y$ | -29.76 | 0.01 | 0.40 | 0.00 | ▷ 45.74 | -0.04 | BC 446 |
| | | | 3950 | Min $M_y$ | -20.62 | -0.19 | -0.32 | -0.00 | ▷ -48.39 | 0.76 | BC 165 |
| | | 70 | 4345 | Max $M_z$ | -102.72 | -0.26 | 1.79 | -0.00 | -44.30 | ▷ 1.14 | BC 164 |
| | | 70 | 4345 | Min $M_z$ | -42.20 | 0.01 | -1.84 | 0.00 | 45.46 | ▷ -0.06 | BC 218 |
| 152 | RC1 | 70 | 0 | Max N | ▷ -24.87 | 0.52 | 2.07 | -0.00 | -48.03 | 0.83 | BC 445 |
| | | | Links | Min N | ▷ -81.22 | 0.19 | -0.00 | -0.00 | -0.01 | 0.15 | BC 138 |
| | | | | Max $V_y$ | -60.18 | ▷ 1.67 | 1.79 | -0.00 | -44.30 | 1.14 | BC 164 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 152 | RC1 | | | Min $V_y$ | -25.44 | ▷ 0.04 | -0.00 | -0.00 | -0.00 | 0.02 | BC 35 |
| | | | | Max $V_z$ | -36.44 | 0.56 | ▷ 2.07 | -0.00 | -48.02 | 0.85 | BC 433 |
| | | | | Min $V_z$ | -37.93 | 0.06 | ▷ -1.84 | 0.00 | 45.46 | -0.05 | BC 166 |
| | | | | Max $M_T$ | -49.24 | 0.08 | -1.84 | ▷ 0.00 | 45.46 | -0.02 | BC 214 |
| | | | | Min $M_T$ | -70.95 | 1.64 | 1.78 | ▷ -0.00 | -44.30 | 1.11 | BC 264 |
| | | | | Max $M_y$ | -37.51 | 0.07 | -1.84 | 0.00 | ▷ 45.46 | -0.02 | BC 434 |
| | | | | Min $M_y$ | -36.72 | 0.53 | 2.07 | -0.00 | ▷ -48.04 | 0.84 | BC 165 |
| | | | | Max $M_z$ | -60.18 | 1.67 | 1.79 | -0.00 | -44.30 | ▷ 1.14 | BC 164 |
| | | | | Min $M_z$ | -37.93 | 0.06 | -1.84 | 0.00 | 45.46 | ▷ -0.06 | BC 218 |
| | | | 0 | Max N | ▷ -24.87 | 0.52 | 2.07 | -0.00 | -48.03 | 0.83 | BC 445 |
| | | | Rechts | Min N | ▷ -81.22 | 0.19 | -0.00 | -0.00 | -0.01 | 0.15 | BC 138 |
| | | | | Max $V_y$ | -60.18 | ▷ 1.67 | 1.79 | -0.00 | -44.30 | 1.14 | BC 164 |
| | | | | Min $V_y$ | -25.44 | ▷ 0.04 | -0.00 | -0.00 | -0.00 | 0.02 | BC 35 |
| | | | | Max $V_z$ | -36.44 | 0.56 | ▷ 2.07 | -0.00 | -48.02 | 0.85 | BC 433 |
| | | | | Min $V_z$ | -37.93 | 0.06 | ▷ -1.84 | 0.00 | 45.46 | -0.05 | BC 166 |
| | | | | Max $M_T$ | -49.24 | 0.08 | -1.84 | ▷ 0.00 | 45.46 | -0.02 | BC 214 |
| | | | | Min $M_T$ | -70.95 | 1.64 | 1.78 | ▷ -0.00 | -44.30 | 1.11 | BC 264 |
| | | | | Max $M_y$ | -37.51 | 0.07 | -1.84 | 0.00 | ▷ 45.46 | -0.02 | BC 434 |
| | | | | Min $M_y$ | -36.72 | 0.53 | 2.07 | -0.00 | ▷ -48.04 | 0.84 | BC 165 |
| | | | | Max $M_z$ | -60.18 | 1.67 | 1.79 | -0.00 | -44.30 | ▷ 1.14 | BC 164 |
| | | | | Min $M_z$ | -37.93 | 0.06 | -1.84 | 0.00 | 45.46 | ▷ -0.06 | BC 218 |
| | | | 3627 | Max N | ▷ -15.58 | 0.52 | 23.98 | -0.00 | -0.80 | -1.07 | BC 445 |
| | | | Links | Min N | ▷ -67.60 | 0.19 | -0.00 | -0.00 | -0.01 | -0.52 | BC 138 |
| | | | | Max $V_y$ | -46.56 | ▷ 1.67 | 21.78 | -0.00 | -1.56 | -4.93 | BC 164 |
| | | | | Min $V_y$ | -16.15 | ▷ 0.04 | -0.00 | -0.00 | -0.00 | -0.14 | BC 35 |
| | | | | Max $V_z$ | -27.16 | 0.56 | ▷ 23.98 | -0.00 | -0.78 | -1.17 | BC 433 |
| | | | | Min $V_z$ | -24.31 | 0.06 | ▷ -22.37 | 0.00 | 1.57 | -0.28 | BC 166 |
| | | | | Max $M_T$ | -35.62 | 0.08 | -22.37 | ▷ 0.00 | 1.58 | -0.32 | BC 214 |
| | | | | Min $M_T$ | -57.33 | 1.64 | 21.78 | ▷ -0.00 | -1.56 | -4.84 | BC 264 |
| | | | | Max $M_y$ | -28.23 | 0.07 | -22.37 | 0.00 | ▷ 1.58 | -0.28 | BC 434 |
| | | | | Min $M_y$ | -57.30 | 1.64 | 21.78 | -0.00 | ▷ -1.56 | -4.83 | BC 236 |
| | | | | Max $M_z$ | -16.09 | 0.05 | -0.00 | -0.00 | -0.00 | ▷ -0.13 | BC 56 |
| | | | | Min $M_z$ | -46.56 | 1.67 | 21.78 | -0.00 | -1.56 | ▷ -4.93 | BC 164 |
| | | | 3627 | Max N | ▷ -15.58 | 0.52 | 23.98 | -0.00 | -0.80 | -1.07 | BC 445 |
| | | | Rechts | Min N | ▷ -67.60 | 0.19 | -0.00 | -0.00 | -0.01 | -0.52 | BC 138 |
| | | | | Max $V_y$ | -46.56 | ▷ 1.67 | 21.78 | -0.00 | -1.56 | -4.93 | BC 164 |
| | | | | Min $V_y$ | -16.15 | ▷ 0.04 | -0.00 | -0.00 | -0.00 | -0.14 | BC 35 |
| | | | | Max $V_z$ | -27.16 | 0.56 | ▷ 23.98 | -0.00 | -0.78 | -1.17 | BC 433 |
| | | | | Min $V_z$ | -24.31 | 0.06 | ▷ -22.37 | 0.00 | 1.57 | -0.28 | BC 166 |
| | | | | Max $M_T$ | -35.62 | 0.08 | -22.37 | ▷ 0.00 | 1.58 | -0.32 | BC 214 |
| | | | | Min $M_T$ | -57.33 | 1.64 | 21.78 | ▷ -0.00 | -1.56 | -4.84 | BC 264 |
| | | | | Max $M_y$ | -28.23 | 0.07 | -22.37 | 0.00 | ▷ 1.58 | -0.28 | BC 434 |
| | | | | Min $M_y$ | -57.30 | 1.64 | 21.78 | -0.00 | ▷ -1.56 | -4.83 | BC 236 |
| | | | | Max $M_z$ | -16.09 | 0.05 | -0.00 | -0.00 | -0.00 | ▷ -0.13 | BC 56 |
| | | | | Min $M_z$ | -46.56 | 1.67 | 21.78 | -0.00 | -1.56 | ▷ -4.93 | BC 164 |
| | | | 3686 | Max N | ▷ -15.44 | 0.52 | 24.34 | -0.00 | 0.65 | -1.10 | BC 445 |
| | | | Links | Min N | ▷ -67.39 | 0.19 | -0.00 | -0.00 | -0.01 | -0.53 | BC 138 |
| | | | | Max $V_y$ | -46.35 | ▷ 1.67 | 22.12 | -0.00 | -0.24 | -5.03 | BC 164 |
| | | | | Min $V_y$ | -16.01 | ▷ 0.04 | -0.00 | -0.00 | -0.00 | -0.14 | BC 35 |
| | | | | Max $V_z$ | -27.02 | 0.56 | ▷ 24.34 | -0.00 | 0.67 | -1.21 | BC 433 |
| | | | | Min $V_z$ | -24.10 | 0.06 | ▷ -22.71 | 0.00 | 0.22 | -0.28 | BC 166 |
| | | | | Max $M_T$ | -35.41 | 0.08 | -22.71 | ▷ 0.00 | 0.22 | -0.32 | BC 214 |
| | | | | Min $M_T$ | -57.13 | 1.64 | 22.11 | ▷ -0.00 | -0.25 | -4.94 | BC 264 |
| | | | | Max $M_y$ | -27.02 | 0.56 | 24.34 | -0.00 | ▷ 0.67 | -1.21 | BC 433 |
| | | | | Min $M_y$ | -57.09 | 1.64 | 22.11 | -0.00 | ▷ -0.25 | -4.93 | BC 236 |
| | | | | Max $M_z$ | -15.95 | 0.05 | -0.00 | -0.00 | -0.00 | ▷ -0.13 | BC 56 |
| | | | | Min $M_z$ | -46.35 | 1.67 | 22.12 | -0.00 | -0.24 | ▷ -5.03 | BC 164 |
| | | | 3686 | Max N | ▷ -15.44 | 0.52 | 24.34 | -0.00 | 0.65 | -1.10 | BC 445 |
| | | | Rechts | Min N | ▷ -67.39 | 0.19 | -0.00 | -0.00 | -0.01 | -0.53 | BC 138 |
| | | | | Max $V_y$ | -46.35 | ▷ 1.67 | 22.12 | -0.00 | -0.24 | -5.03 | BC 164 |
| | | | | Min $V_y$ | -16.01 | ▷ 0.04 | -0.00 | -0.00 | -0.00 | -0.14 | BC 35 |
| | | | | Max $V_z$ | -27.02 | 0.56 | ▷ 24.34 | -0.00 | 0.67 | -1.21 | BC 433 |
| | | | | Min $V_z$ | -24.10 | 0.06 | ▷ -22.71 | 0.00 | 0.22 | -0.28 | BC 166 |
| | | | | Max $M_T$ | -35.41 | 0.08 | -22.71 | ▷ 0.00 | 0.22 | -0.32 | BC 214 |
| | | | | Min $M_T$ | -57.13 | 1.64 | 22.11 | ▷ -0.00 | -0.25 | -4.94 | BC 264 |
| | | | | Max $M_y$ | -27.02 | 0.56 | 24.34 | -0.00 | ▷ 0.67 | -1.21 | BC 433 |
| | | | | Min $M_y$ | -57.09 | 1.64 | 22.11 | -0.00 | ▷ -0.25 | -4.93 | BC 236 |
| | | | | Max $M_z$ | -15.95 | 0.05 | -0.00 | -0.00 | -0.00 | ▷ -0.13 | BC 56 |
| | | | | Min $M_z$ | -46.35 | 1.67 | 22.12 | -0.00 | -0.24 | ▷ -5.03 | BC 164 |
| | | | 3748 | Max N | ▷ -15.35 | 0.52 | 24.71 | -0.00 | 2.16 | -1.13 | BC 445 |
| | | | Links | Min N | ▷ -67.26 | 0.19 | -0.00 | -0.00 | -0.01 | -0.54 | BC 138 |
| | | | | Max $V_y$ | -46.22 | ▷ 1.67 | 22.45 | -0.00 | 1.13 | -5.13 | BC 164 |
| | | | | Min $V_y$ | -15.92 | ▷ 0.04 | -0.00 | -0.00 | -0.00 | -0.15 | BC 35 |
| | | | | Max $V_z$ | -26.93 | 0.56 | ▷ 24.71 | -0.00 | 2.18 | -1.24 | BC 433 |
| | | | | Min $V_z$ | -23.97 | 0.06 | ▷ -23.05 | 0.00 | -1.18 | -0.29 | BC 166 |
| | | | | Max $M_T$ | -35.28 | 0.08 | -23.05 | ▷ 0.00 | -1.18 | -0.33 | BC 214 |
| | | | | Min $M_T$ | -56.99 | 1.64 | 22.45 | ▷ -0.00 | 1.12 | -5.04 | BC 264 |
| | | | | Max $M_y$ | -26.93 | 0.56 | 24.71 | -0.00 | ▷ 2.18 | -1.24 | BC 433 |
| | | | | Min $M_y$ | -23.97 | 0.06 | -23.05 | 0.00 | ▷ -1.18 | -0.29 | BC 166 |
| | | | | Max $M_z$ | -15.85 | 0.05 | -0.00 | -0.00 | -0.00 | ▷ -0.13 | BC 56 |
| | | | | Min $M_z$ | -46.22 | 1.67 | 22.45 | -0.00 | 1.13 | ▷ -5.13 | BC 164 |
| | | 39 | 3748 | Max N | ▷ -15.35 | 0.52 | 24.71 | -0.00 | 2.16 | -1.13 | BC 445 |
| | | | Rechts | Min N | ▷ -67.26 | 0.19 | -0.00 | -0.00 | -0.01 | -0.54 | BC 138 |
| | | | | Max $V_y$ | -46.22 | ▷ 1.67 | 22.45 | -0.00 | 1.13 | -5.13 | BC 164 |
| | | | | Min $V_y$ | -15.92 | ▷ 0.04 | -0.00 | -0.00 | -0.00 | -0.15 | BC 35 |
| | | | | Max $V_z$ | -26.93 | 0.56 | ▷ 24.71 | -0.00 | 2.18 | -1.24 | BC 433 |
| | | | | Min $V_z$ | -23.97 | 0.06 | ▷ -23.05 | 0.00 | -1.19 | -0.29 | BC 166 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 152 | RC1 | | | Max $M_T$ | -35.28 | 0.08 | -23.05 | ▷ 0.00 | -1.18 | -0.33 | BC 214 |
| | | | | Min $M_T$ | -56.99 | 1.64 | 22.45 | ▷ -0.00 | 1.12 | -5.04 | BC 264 |
| | | | | Max $M_y$ | -26.93 | 0.56 | 24.71 | -0.00 | ▷ 2.18 | -1.24 | BC 433 |
| | | | | Min $M_y$ | -23.97 | 0.06 | -23.05 | 0.00 | ▷ -1.19 | -0.29 | BC 166 |
| | | | | Max $M_z$ | -15.85 | 0.05 | -0.00 | -0.00 | -0.00 | ▷ -0.13 | BC 56 |
| | | | | Min $M_z$ | -46.22 | 1.67 | 22.45 | -0.00 | 1.13 | ▷ -5.13 | BC 164 |
| | | | 3748 | Max N | ▷ -15.35 | 0.52 | 24.71 | -0.00 | 2.16 | -1.13 | BC 445 |
| | | 70 | 0 | Min N | ▷ -81.22 | 0.19 | -0.00 | -0.00 | -0.01 | 0.15 | BC 138 |
| | | 70 | 0 | Max $V_y$ | -60.18 | ▷ 1.67 | 1.79 | -0.00 | -44.30 | 1.14 | BC 164 |
| | | 70 | 0 | Min $V_y$ | -25.44 | ▷ 0.04 | -0.00 | -0.00 | -0.00 | 0.02 | BC 35 |
| | | 39 | 3748 | Max $V_z$ | -26.93 | 0.56 | ▷ 24.71 | -0.00 | 2.18 | -1.24 | BC 433 |
| | | 39 | 3748 | Min $V_z$ | -23.97 | 0.06 | ▷ -23.05 | 0.00 | -1.19 | -0.29 | BC 166 |
| | | 70 | 0 | Max $M_T$ | -49.24 | 0.08 | -1.84 | ▷ 0.00 | 45.46 | -0.02 | BC 214 |
| | | 70 | 0 | Min $M_T$ | -70.95 | 1.64 | 1.78 | ▷ -0.00 | -44.30 | 1.11 | BC 264 |
| | | 70 | 0 | Max $M_y$ | -37.51 | 0.07 | -1.84 | 0.00 | ▷ 45.46 | -0.02 | BC 434 |
| | | 70 | 0 | Min $M_y$ | -36.72 | 0.53 | 2.07 | -0.00 | ▷ -48.04 | 0.84 | BC 165 |
| | | 70 | 0 | Max $M_z$ | -60.18 | 1.67 | 1.79 | -0.00 | -44.30 | ▷ 1.14 | BC 164 |
| | | 39 | 3748 | Min $M_z$ | -46.22 | 1.67 | 22.45 | -0.00 | 1.13 | ▷ -5.13 | BC 164 |
| 30 | RC1 | 70 | 4345 | MAX N | ▷ -5.24 | -0.19 | 2.07 | 0.00 | -48.02 | 0.83 | BC 445 |
| 30 | RC1 | 47 | 0 | MIN N | ▷ -122.90 | -0.26 | -22.18 | 0.00 | 0.00 | 0.00 | BC 200 |
| 152 | RC1 | 70 | 0 | MAX $V_y$ | -60.18 | ▷ 1.67 | 1.79 | 0.00 | -44.30 | 1.14 | BC 164 |
| 30 | RC1 | 47 | 0 | MIN $V_y$ | -112.52 | ▷ -0.26 | -22.18 | 0.00 | 0.00 | 0.00 | BC 164 |
| 152 | RC1 | 39 | 3748 | MAX $V_z$ | -26.93 | 0.56 | ▷ 24.71 | 0.00 | 2.18 | -1.24 | BC 433 |
| 30 | RC1 | 47 | 0 | MIN $V_z$ | -28.94 | -0.19 | ▷ -24.18 | 0.00 | 0.00 | 0.00 | BC 165 |
| 30 | RC1 | 47 | 0 | MAX $M_T$ | -63.30 | 0.00 | 22.76 | ▷ 0.00 | 0.00 | 0.00 | BC 214 |
| 30 | RC1 | 47 | 0 | MIN $M_T$ | -122.21 | -0.25 | -22.18 | ▷ 0.00 | 0.00 | 0.00 | BC 264 |
| 30 | RC1 | | 3950 | MAX $M_y$ | -29.76 | 0.01 | 0.40 | 0.00 | ▷ 45.74 | -0.04 | BC 446 |
| 30 | RC1 | | 3950 | MIN $M_y$ | -20.62 | -0.19 | -0.32 | 0.00 | ▷ -48.39 | 0.76 | BC 165 |
| 30 | RC1 | 70 | 4345 | MAX $M_z$ | -102.72 | -0.26 | 1.79 | 0.00 | -44.30 | ▷ 1.14 | BC 164 |
| 152 | RC1 | 39 | 3748 | MIN $M_z$ | -46.22 | 1.67 | 22.45 | 0.00 | 1.13 | ▷ -5.13 | BC 164 |
| | **Doorgaande staven No. 18: Doorgaande staven 21** | | | | | | | | | | |
| 31 | RC1 | 58 | 0 | Max N | ▷ -15.77 | 0.35 | 23.81 | -0.00 | 0.00 | 0.00 | BC 468 |
| | | | Links | Min N | ▷ -91.79 | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | BC 134 |
| | | | | Max $V_y$ | -19.09 | ▷ 0.39 | 23.79 | -0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Min $V_y$ | -70.73 | ▷ -0.37 | 21.76 | -0.00 | 0.00 | 0.00 | BC 269 |
| | | | | Max $V_z$ | -42.05 | 0.32 | ▷ 23.81 | -0.00 | -0.00 | 0.00 | BC 240 |
| | | | | Min $V_z$ | -46.61 | -0.07 | ▷ -22.36 | 0.00 | -0.00 | 0.00 | BC 167 |
| | | | | Max $M_T$ | -32.04 | -0.06 | -22.36 | ▷ 0.00 | -0.00 | 0.00 | BC 363 |
| | | | | Min $M_T$ | -59.01 | -0.36 | 21.76 | ▷ -0.00 | 0.00 | 0.00 | BC 281 |
| | | | | Max $M_y$ | -40.98 | -0.08 | 13.95 | -0.00 | ▷ 0.00 | 0.00 | BC 278 |
| | | | | Min $M_y$ | -42.03 | 0.32 | 23.81 | -0.00 | ▷ -0.00 | 0.00 | BC 268 |
| | | | | Max $M_z$ | -52.25 | -0.04 | -0.00 | 0.00 | 0.00 | ▷ 0.00 | BC 2 |
| | | | | Min $M_z$ | -77.20 | -0.08 | 0.00 | 0.00 | 0.00 | ▷ -0.00 | BC 326 |
| | | | 0 | Max N | ▷ -15.77 | 0.35 | 23.81 | -0.00 | 0.00 | -0.00 | BC 468 |
| | | | Rechts | Min N | ▷ -91.79 | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | BC 134 |
| | | | | Max $V_y$ | -19.09 | ▷ 0.39 | 23.79 | -0.00 | 0.00 | -0.00 | BC 360 |
| | | | | Min $V_y$ | -70.73 | ▷ -0.37 | 21.76 | -0.00 | 0.00 | 0.00 | BC 269 |
| | | | | Max $V_z$ | -42.05 | 0.32 | ▷ 23.81 | -0.00 | 0.00 | -0.00 | BC 240 |
| | | | | Min $V_z$ | -46.61 | -0.07 | ▷ -22.36 | 0.00 | -0.00 | 0.00 | BC 167 |
| | | | | Max $M_T$ | -32.04 | -0.06 | -22.36 | ▷ 0.00 | -0.00 | 0.00 | BC 363 |
| | | | | Min $M_T$ | -59.01 | -0.36 | 21.76 | ▷ -0.00 | 0.00 | 0.00 | BC 281 |
| | | | | Max $M_y$ | -41.83 | 0.33 | 23.81 | -0.00 | ▷ 0.00 | -0.00 | BC 264 |
| | | | | Min $M_y$ | -46.61 | -0.07 | -22.36 | 0.00 | ▷ -0.00 | 0.00 | BC 167 |
| | | | | Max $M_z$ | -70.67 | -0.37 | 21.76 | -0.00 | 0.00 | ▷ 0.00 | BC 241 |
| | | | | Min $M_z$ | -19.13 | 0.39 | 23.79 | -0.00 | 0.00 | ▷ -0.00 | BC 356 |
| | | | 2500 | Max N | ▷ -13.78 | 0.35 | 8.71 | -0.00 | 40.64 | -0.87 | BC 468 |
| | | | Links | Min N | ▷ -88.86 | -0.09 | 0.00 | 0.00 | 0.00 | 0.24 | BC 134 |
| | | | | Max $V_y$ | -17.09 | ▷ 0.39 | 8.70 | -0.00 | 40.61 | -0.97 | BC 360 |
| | | | | Min $V_y$ | -67.80 | ▷ -0.37 | 8.02 | -0.00 | 37.23 | 0.92 | BC 269 |
| | | | | Max $V_z$ | -39.12 | 0.32 | ▷ 8.72 | -0.00 | 40.66 | -0.81 | BC 240 |
| | | | | Min $V_z$ | -43.69 | -0.07 | ▷ -8.24 | 0.00 | -38.25 | 0.18 | BC 167 |
| | | | | Max $M_T$ | -30.04 | -0.06 | -8.24 | ▷ 0.00 | -38.25 | 0.15 | BC 363 |
| | | | | Min $M_T$ | -56.09 | -0.36 | 8.02 | ▷ -0.00 | 37.23 | 0.89 | BC 281 |
| | | | | Max $M_y$ | -39.12 | 0.32 | 8.72 | -0.00 | ▷ 40.66 | -0.81 | BC 240 |
| | | | | Min $M_y$ | -43.69 | -0.07 | -8.24 | 0.00 | ▷ -38.25 | 0.18 | BC 167 |
| | | | | Max $M_z$ | -67.80 | -0.37 | 8.02 | -0.00 | 37.23 | ▷ 0.92 | BC 269 |
| | | | | Min $M_z$ | -17.09 | 0.39 | 8.70 | -0.00 | 40.61 | ▷ -0.97 | BC 360 |
| | | | 2500 | Max N | ▷ -13.78 | 0.35 | 8.71 | -0.00 | 40.64 | -0.87 | BC 468 |
| | | | Rechts | Min N | ▷ -88.86 | -0.09 | 0.00 | 0.00 | 0.00 | 0.24 | BC 134 |
| | | | | Max $V_y$ | -17.09 | ▷ 0.39 | 8.70 | -0.00 | 40.61 | -0.97 | BC 360 |
| | | | | Min $V_y$ | -67.80 | ▷ -0.37 | 8.02 | -0.00 | 37.23 | 0.92 | BC 269 |
| | | | | Max $V_z$ | -39.12 | 0.32 | ▷ 8.72 | -0.00 | 40.66 | -0.81 | BC 240 |
| | | | | Min $V_z$ | -43.69 | -0.07 | ▷ -8.24 | 0.00 | -38.25 | 0.18 | BC 167 |
| | | | | Max $M_T$ | -30.04 | -0.06 | -8.24 | ▷ 0.00 | -38.25 | 0.15 | BC 363 |
| | | | | Min $M_T$ | -56.09 | -0.36 | 8.02 | ▷ -0.00 | 37.23 | 0.89 | BC 281 |
| | | | | Max $M_y$ | -39.12 | 0.32 | 8.72 | -0.00 | ▷ 40.66 | -0.81 | BC 240 |
| | | | | Min $M_y$ | -43.69 | -0.07 | -8.24 | 0.00 | ▷ -38.25 | 0.18 | BC 167 |
| | | | | Max $M_z$ | -67.80 | -0.37 | 8.02 | -0.00 | 37.23 | ▷ 0.92 | BC 269 |
| | | | | Min $M_z$ | -17.09 | 0.39 | 8.70 | -0.00 | 40.61 | ▷ -0.97 | BC 360 |
| | | | 4345 | Max N | ▷ -9.10 | 0.35 | -2.43 | -0.00 | 46.43 | -1.51 | BC 468 |
| | | | Links | Min N | ▷ -81.99 | -0.09 | 0.00 | 0.00 | 0.00 | 0.41 | BC 134 |
| | | | | Max $V_y$ | -12.41 | ▷ 0.39 | -2.45 | -0.00 | 46.38 | -1.69 | BC 360 |
| | | | | Min $V_y$ | -60.94 | ▷ -0.37 | -2.12 | -0.00 | 42.67 | 1.59 | BC 269 |
| | | | | Max $V_z$ | -34.35 | -0.12 | ▷ 2.18 | 0.00 | -43.84 | 0.51 | BC 435 |
| | | | | Min $V_z$ | -23.71 | 0.38 | ▷ -2.45 | -0.00 | 46.37 | -1.65 | BC 168 |
| | | | | Max $M_T$ | -25.36 | -0.06 | 2.18 | ▷ 0.00 | -43.84 | 0.26 | BC 363 |
| | | | | Min $M_T$ | -49.22 | -0.36 | -2.12 | ▷ -0.00 | 42.67 | 1.55 | BC 281 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 31 | RC1 | | | Max $M_y$ | -32.26 | 0.32 | -2.43 | -0.00 | ▷ 46.46 | -1.40 | BC 240 |
| | | | | Min $M_y$ | -36.82 | -0.07 | 2.18 | 0.00 | ▷ -43.85 | 0.31 | BC 167 |
| | | | | Max $M_z$ | -60.94 | -0.37 | -2.12 | -0.00 | 42.67 | ▷ 1.59 | BC 269 |
| | | | | Min $M_z$ | -12.41 | 0.39 | -2.45 | -0.00 | 46.38 | ▷ -1.69 | BC 360 |
| | | 79 | 4345 | Max N | ▷ -9.10 | 0.35 | -2.43 | -0.00 | 46.43 | -1.51 | BC 468 |
| | | | Rechts | Min N | ▷ -81.99 | -0.09 | 0.00 | 0.00 | 0.00 | 0.41 | BC 134 |
| | | | | Max $V_y$ | -12.41 | ▷ 0.39 | -2.45 | -0.00 | 46.38 | -1.69 | BC 360 |
| | | | | Min $V_y$ | -60.94 | ▷ -0.37 | -2.12 | -0.00 | 42.67 | 1.59 | BC 269 |
| | | | | Max $V_z$ | -34.35 | -0.12 | ▷ 2.18 | 0.00 | -43.84 | 0.51 | BC 435 |
| | | | | Min $V_z$ | -23.71 | 0.38 | ▷ -2.45 | -0.00 | 46.37 | -1.65 | BC 168 |
| | | | | Max $M_T$ | -25.36 | -0.06 | 2.18 | ▷ 0.00 | -43.84 | 0.26 | BC 363 |
| | | | | Min $M_T$ | -49.22 | -0.36 | -2.12 | ▷ -0.00 | 42.67 | 1.55 | BC 281 |
| | | | | Max $M_y$ | -32.26 | 0.32 | -2.43 | -0.00 | ▷ 46.46 | -1.40 | BC 240 |
| | | | | Min $M_y$ | -36.82 | -0.07 | 2.18 | 0.00 | ▷ -43.85 | 0.31 | BC 167 |
| | | | | Max $M_z$ | -60.94 | -0.37 | -2.12 | -0.00 | 42.67 | ▷ 1.59 | BC 269 |
| | | | | Min $M_z$ | -12.41 | 0.39 | -2.45 | -0.00 | 46.38 | ▷ -1.69 | BC 360 |
| | | 79 | 4345 | Max N | ▷ -9.10 | 0.35 | -2.43 | -0.00 | 46.43 | -1.51 | BC 468 |
| | | 58 | 0 | Min N | ▷ -91.79 | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | BC 134 |
| | | 58 | 0 | Max $V_y$ | -19.09 | ▷ 0.39 | 23.79 | -0.00 | 0.00 | 0.00 | BC 360 |
| | | 58 | 0 | Min $V_y$ | -70.73 | ▷ -0.37 | 21.76 | -0.00 | 0.00 | 0.00 | BC 269 |
| | | 58 | 0 | Max $V_z$ | -42.05 | 0.32 | ▷ 23.81 | -0.00 | -0.00 | 0.00 | BC 240 |
| | | 58 | 0 | Min $V_z$ | -46.61 | -0.07 | ▷ -22.36 | 0.00 | -0.00 | 0.00 | BC 167 |
| | | 58 | 0 | Max $M_T$ | -32.04 | -0.06 | -22.36 | ▷ 0.00 | -0.00 | 0.00 | BC 363 |
| | | 58 | 0 | Min $M_T$ | -59.01 | -0.36 | 21.76 | ▷ -0.00 | 0.00 | 0.00 | BC 281 |
| | | | 3950 | Max $M_y$ | -33.73 | 0.32 | -0.04 | -0.00 | ▷ 46.95 | -1.27 | BC 240 |
| | | | 3950 | Min $M_y$ | -38.29 | -0.07 | -0.05 | 0.00 | ▷ -44.27 | 0.28 | BC 167 |
| | | 79 | 4345 | Max $M_z$ | -60.94 | -0.37 | -2.12 | -0.00 | 42.67 | ▷ 1.59 | BC 269 |
| | | 79 | 4345 | Min $M_z$ | -12.41 | 0.39 | -2.45 | -0.00 | 46.38 | ▷ -1.69 | BC 360 |
| 141 | RC1 | 79 | 0 | Max N | ▷ -24.67 | -0.68 | -2.43 | -0.00 | 46.44 | -1.51 | BC 468 |
| | | | Links | Min N | ▷ -80.14 | 0.09 | 0.00 | 0.00 | 0.00 | 0.41 | BC 134 |
| | | | | Max $V_y$ | -48.00 | ▷ 0.15 | 2.18 | 0.00 | -43.84 | 0.57 | BC 243 |
| | | | | Min $V_y$ | -24.71 | ▷ -0.77 | -2.44 | -0.00 | 46.38 | -1.69 | BC 360 |
| | | | | Max $V_z$ | -36.38 | 0.14 | ▷ 2.18 | 0.00 | -43.84 | 0.51 | BC 435 |
| | | | | Min $V_z$ | -36.33 | -0.76 | ▷ -2.45 | -0.00 | 46.38 | -1.65 | BC 168 |
| | | | | Max $M_T$ | -24.95 | 0.07 | 2.18 | ▷ 0.00 | -43.85 | 0.26 | BC 363 |
| | | | | Min $M_T$ | -45.82 | -0.09 | -2.12 | ▷ -0.00 | 42.68 | 1.55 | BC 281 |
| | | | | Max $M_y$ | -47.77 | -0.64 | -2.43 | -0.00 | ▷ 46.47 | -1.40 | BC 240 |
| | | | | Min $M_y$ | -36.57 | 0.08 | 2.18 | 0.00 | ▷ -43.85 | 0.31 | BC 167 |
| | | | | Max $M_z$ | -57.53 | -0.10 | -2.12 | -0.00 | 42.68 | ▷ 1.59 | BC 269 |
| | | | | Min $M_z$ | -24.71 | -0.77 | -2.44 | -0.00 | 46.38 | ▷ -1.69 | BC 360 |
| | | | 0 | Max N | ▷ -24.67 | -0.68 | -2.43 | -0.00 | 46.44 | -1.51 | BC 468 |
| | | | Rechts | Min N | ▷ -80.14 | 0.09 | 0.00 | 0.00 | 0.00 | 0.41 | BC 134 |
| | | | | Max $V_y$ | -48.00 | ▷ 0.15 | 2.18 | 0.00 | -43.84 | 0.57 | BC 243 |
| | | | | Min $V_y$ | -24.71 | ▷ -0.77 | -2.44 | -0.00 | 46.38 | -1.69 | BC 360 |
| | | | | Max $V_z$ | -36.38 | 0.14 | ▷ 2.18 | 0.00 | -43.84 | 0.51 | BC 435 |
| | | | | Min $V_z$ | -36.33 | -0.76 | ▷ -2.45 | -0.00 | 46.38 | -1.65 | BC 168 |
| | | | | Max $M_T$ | -24.95 | 0.07 | 2.18 | ▷ 0.00 | -43.85 | 0.26 | BC 363 |
| | | | | Min $M_T$ | -45.82 | -0.09 | -2.12 | ▷ -0.00 | 42.68 | 1.55 | BC 281 |
| | | | | Max $M_y$ | -47.77 | -0.64 | -2.43 | -0.00 | ▷ 46.47 | -1.40 | BC 240 |
| | | | | Min $M_y$ | -36.57 | 0.08 | 2.18 | 0.00 | ▷ -43.85 | 0.31 | BC 167 |
| | | | | Max $M_z$ | -57.53 | -0.10 | -2.12 | -0.00 | 42.68 | ▷ 1.59 | BC 269 |
| | | | | Min $M_z$ | -24.71 | -0.77 | -2.44 | -0.00 | 46.38 | ▷ -1.69 | BC 360 |
| | | | 3565 | Max N | ▷ -15.58 | -0.68 | -23.96 | -0.00 | -0.61 | 0.92 | BC 468 |
| | | | Links | Min N | ▷ -66.80 | 0.09 | 0.00 | 0.00 | 0.00 | 0.11 | BC 134 |
| | | | | Max $V_y$ | -34.66 | ▷ 0.15 | 22.31 | 0.00 | -0.19 | 0.02 | BC 243 |
| | | | | Min $V_y$ | -15.62 | ▷ -0.77 | -23.97 | -0.00 | -0.71 | 1.05 | BC 360 |
| | | | | Max $V_z$ | -15.82 | 0.13 | ▷ 22.31 | 0.00 | -0.19 | -0.01 | BC 447 |
| | | | | Min $V_z$ | -22.99 | -0.76 | ▷ -23.97 | -0.00 | -0.71 | 1.06 | BC 168 |
| | | | | Max $M_T$ | -15.86 | 0.07 | 22.31 | ▷ 0.00 | -0.20 | 0.01 | BC 363 |
| | | | | Min $M_T$ | -32.48 | -0.09 | -21.71 | ▷ -0.00 | 0.20 | 1.88 | BC 281 |
| | | | | Max $M_y$ | -38.05 | -0.21 | -21.71 | -0.00 | ▷ 0.20 | 2.20 | BC 433 |
| | | | | Min $M_y$ | -22.99 | -0.76 | -23.97 | -0.00 | ▷ -0.71 | 1.06 | BC 168 |
| | | | | Max $M_z$ | -40.82 | -0.48 | -21.71 | -0.00 | 0.20 | ▷ 2.76 | BC 377 |
| | | | | Min $M_z$ | -15.81 | 0.12 | 22.31 | 0.00 | -0.19 | ▷ -0.01 | BC 443 |
| | | | 3565 | Max N | ▷ -15.58 | -0.68 | -23.96 | -0.00 | -0.61 | 0.92 | BC 468 |
| | | | Rechts | Min N | ▷ -66.80 | 0.09 | 0.00 | 0.00 | 0.00 | 0.11 | BC 134 |
| | | | | Max $V_y$ | -34.66 | ▷ 0.15 | 22.31 | 0.00 | -0.19 | 0.02 | BC 243 |
| | | | | Min $V_y$ | -15.62 | ▷ -0.77 | -23.97 | -0.00 | -0.71 | 1.05 | BC 360 |
| | | | | Max $V_z$ | -15.82 | 0.13 | ▷ 22.31 | 0.00 | -0.19 | -0.01 | BC 447 |
| | | | | Min $V_z$ | -22.99 | -0.76 | ▷ -23.97 | -0.00 | -0.71 | 1.06 | BC 168 |
| | | | | Max $M_T$ | -15.86 | 0.07 | 22.31 | ▷ 0.00 | -0.20 | 0.01 | BC 363 |
| | | | | Min $M_T$ | -32.48 | -0.09 | -21.71 | ▷ -0.00 | 0.19 | 1.88 | BC 281 |
| | | | | Max $M_y$ | -38.05 | -0.21 | -21.71 | -0.00 | ▷ 0.20 | 2.20 | BC 433 |
| | | | | Min $M_y$ | -22.99 | -0.76 | -23.97 | -0.00 | ▷ -0.71 | 1.06 | BC 168 |
| | | | | Max $M_z$ | -40.82 | -0.48 | -21.71 | -0.00 | 0.20 | ▷ 2.76 | BC 377 |
| | | | | Min $M_z$ | -15.81 | 0.12 | 22.31 | 0.00 | -0.19 | ▷ -0.01 | BC 443 |
| | | | 3625 | Max N | ▷ -15.45 | -0.68 | -24.32 | -0.00 | -2.06 | 0.96 | BC 468 |
| | | | Links | Min N | ▷ -66.61 | 0.09 | 0.00 | 0.00 | 0.00 | 0.10 | BC 134 |
| | | | | Max $V_y$ | -34.48 | ▷ 0.15 | 22.65 | 0.00 | 1.16 | 0.01 | BC 243 |
| | | | | Min $V_y$ | -15.49 | ▷ -0.77 | -24.34 | -0.00 | -2.16 | 1.09 | BC 360 |
| | | | | Max $V_z$ | -15.69 | 0.13 | ▷ 22.65 | 0.00 | 1.16 | -0.02 | BC 447 |
| | | | | Min $V_z$ | -22.80 | -0.76 | ▷ -24.34 | -0.00 | -2.16 | 1.10 | BC 168 |
| | | | | Max $M_T$ | -15.73 | 0.07 | 22.65 | ▷ 0.00 | 1.15 | 0.01 | BC 363 |
| | | | | Min $M_T$ | -32.29 | -0.09 | -22.04 | ▷ -0.00 | -1.12 | 1.88 | BC 281 |
| | | | | Max $M_y$ | -27.16 | 0.14 | 22.65 | 0.00 | ▷ 1.16 | 0.01 | BC 435 |
| | | | | Min $M_y$ | -22.80 | -0.76 | -24.34 | -0.00 | ▷ -2.16 | 1.10 | BC 168 |
| | | | | Max $M_z$ | -40.70 | -0.48 | -22.04 | -0.00 | -1.12 | ▷ 2.79 | BC 377 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 141 | RC1 | | | Min $M_z$ | -15.69 | 0.13 | 22.65 | 0.00 | 1.16 | ▷ -0.02 | BC 447 |
| | | 41 | 3625 | Max N | ▷ -15.45 | -0.68 | -24.32 | -0.00 | -2.06 | 0.96 | BC 468 |
| | | | Rechts | Min N | ▷ -66.61 | 0.09 | 0.00 | 0.00 | 0.00 | 0.10 | BC 134 |
| | | | | Max $V_y$ | -34.48 | ▷ 0.15 | 22.65 | 0.00 | 1.16 | 0.01 | BC 243 |
| | | | | Min $V_y$ | -15.49 | ▷ -0.77 | -24.34 | -0.00 | -2.16 | 1.09 | BC 360 |
| | | | | Max $V_z$ | -15.69 | 0.13 | ▷ 22.65 | 0.00 | 1.16 | -0.02 | BC 447 |
| | | | | Min $V_z$ | -22.80 | -0.76 | ▷ -24.34 | -0.00 | -2.16 | 1.10 | BC 168 |
| | | | | Max $M_T$ | -15.73 | 0.07 | 22.65 | ▷ 0.00 | 1.15 | 0.01 | BC 363 |
| | | | | Min $M_T$ | -32.29 | -0.09 | -22.04 | ▷ -0.00 | -1.12 | 1.88 | BC 281 |
| | | | | Max $M_y$ | -27.16 | 0.14 | 22.65 | 0.00 | ▷ 1.16 | 0.01 | BC 435 |
| | | | | Min $M_y$ | -22.80 | -0.76 | -24.34 | -0.00 | ▷ -2.16 | 1.10 | BC 168 |
| | | | | Max $M_z$ | -40.70 | -0.48 | -22.04 | -0.00 | -1.12 | ▷ 2.79 | BC 377 |
| | | | | Min $M_z$ | -15.69 | 0.13 | 22.65 | 0.00 | 1.16 | ▷ -0.02 | BC 447 |
| | | 41 | 3625 | Max N | ▷ -15.45 | -0.68 | -24.32 | -0.00 | -2.06 | 0.96 | BC 468 |
| | | 79 | 0 | Min N | ▷ -80.14 | 0.09 | 0.00 | 0.00 | 0.00 | 0.41 | BC 134 |
| | | 79 | 0 | Max $V_y$ | -48.00 | ▷ 0.15 | 2.18 | 0.00 | -43.84 | 0.57 | BC 243 |
| | | 79 | 0 | Min $V_y$ | -24.71 | ▷ -0.77 | -2.44 | -0.00 | 46.38 | -1.69 | BC 360 |
| | | 41 | 3625 | Max $V_z$ | -15.69 | 0.13 | ▷ 22.65 | 0.00 | 1.16 | -0.02 | BC 447 |
| | | 41 | 3625 | Min $V_z$ | -22.80 | -0.76 | ▷ -24.34 | -0.00 | -2.16 | 1.10 | BC 168 |
| | | 79 | 0 | Max $M_T$ | -24.95 | 0.07 | 2.18 | ▷ 0.00 | -43.85 | 0.26 | BC 363 |
| | | 79 | 0 | Min $M_T$ | -45.82 | -0.09 | -2.12 | ▷ -0.00 | 42.68 | 1.55 | BC 281 |
| | | 79 | 0 | Max $M_y$ | -47.77 | -0.64 | -2.43 | -0.00 | ▷ 46.47 | -1.40 | BC 240 |
| | | 79 | 0 | Min $M_y$ | -36.57 | 0.08 | 2.18 | 0.00 | ▷ -43.85 | 0.31 | BC 167 |
| | | 41 | 3625 | Max $M_z$ | -40.70 | -0.48 | -22.04 | -0.00 | -1.12 | ▷ 2.79 | BC 377 |
| | | 79 | 0 | Min $M_z$ | -24.71 | -0.77 | -2.44 | -0.00 | 46.38 | ▷ -1.69 | BC 360 |
| 31 | RC1 | 79 | 4345 | MAX N | ▷ -9.10 | 0.35 | -2.43 | 0.00 | 46.43 | -1.51 | BC 468 |
| 31 | RC1 | 58 | 0 | MIN N | ▷ -91.79 | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | BC 134 |
| 31 | RC1 | 58 | 0 | MAX $V_y$ | -19.09 | ▷ 0.39 | 23.79 | 0.00 | 0.00 | 0.00 | BC 360 |
| 141 | RC1 | 79 | 0 | MIN $V_y$ | -24.71 | ▷ -0.77 | -2.44 | 0.00 | 46.38 | -1.69 | BC 360 |
| 31 | RC1 | 58 | 0 | MAX $V_z$ | -42.05 | 0.32 | ▷ 23.81 | 0.00 | 0.00 | 0.00 | BC 240 |
| 141 | RC1 | 41 | 3625 | MIN $V_z$ | -22.80 | -0.76 | ▷ -24.34 | 0.00 | -2.16 | 1.10 | BC 168 |
| 31 | RC1 | 58 | 0 | MAX $M_T$ | -32.04 | -0.06 | -22.36 | ▷ 0.00 | 0.00 | 0.00 | BC 363 |
| 31 | RC1 | 58 | 0 | MIN $M_T$ | -59.01 | -0.36 | 21.76 | ▷ 0.00 | 0.00 | 0.00 | BC 281 |
| 31 | RC1 | | 3950 | MAX $M_y$ | -33.73 | 0.32 | -0.04 | 0.00 | ▷ 46.95 | -1.27 | BC 240 |
| 31 | RC1 | | 3950 | MIN $M_y$ | -38.29 | -0.07 | -0.05 | 0.00 | ▷ -44.27 | 0.28 | BC 167 |
| 141 | RC1 | 41 | 3625 | MAX $M_z$ | -40.70 | -0.48 | -22.04 | 0.00 | -1.12 | ▷ 2.79 | BC 377 |
| 31 | RC1 | 79 | 4345 | MIN $M_z$ | -12.41 | 0.39 | -2.45 | 0.00 | 46.38 | ▷ -1.69 | BC 360 |
| | **Doorgaande staven No. 19: Doorgaande staven 22** | | | | | | | | | | |
| 32 | RC1 | 59 | 0 | Max N | ▷ -33.75 | 0.02 | -17.34 | -0.00 | 0.00 | 0.00 | BC 419 |
| | | | Links | Min N | ▷ -99.63 | -0.27 | 16.81 | 0.00 | -0.00 | 0.00 | BC 172 |
| | | | | Max $V_y$ | -78.50 | ▷ 0.42 | 18.55 | 0.00 | -0.00 | 0.00 | BC 433 |
| | | | | Min $V_y$ | -75.53 | ▷ -0.30 | 16.83 | 0.00 | -0.00 | 0.00 | BC 360 |
| | | | | Max $V_z$ | -78.08 | 0.42 | ▷ 18.55 | 0.00 | -0.00 | 0.00 | BC 461 |
| | | | | Min $V_z$ | -60.98 | 0.03 | ▷ -17.36 | -0.00 | 0.00 | 0.00 | BC 187 |
| | | | | Max $M_T$ | -91.33 | -0.28 | 16.81 | ▷ 0.00 | -0.00 | 0.00 | BC 164 |
| | | | | Min $M_T$ | -61.66 | 0.03 | -17.36 | ▷ -0.00 | 0.00 | 0.00 | BC 235 |
| | | | | Max $M_y$ | -67.63 | 0.41 | 18.55 | 0.00 | ▷ 0.00 | -0.00 | BC 381 |
| | | | | Min $M_y$ | -43.69 | 0.02 | -17.34 | -0.00 | ▷ -0.00 | 0.00 | BC 379 |
| | | | | Max $M_z$ | -61.18 | 0.07 | -0.05 | -0.00 | 0.00 | ▷ 0.00 | BC 3 |
| | | | | Min $M_z$ | -67.63 | 0.41 | 18.55 | 0.00 | 0.00 | ▷ -0.00 | BC 381 |
| | | | 0 | Max N | ▷ -33.75 | 0.02 | -17.34 | -0.00 | -0.00 | -0.00 | BC 419 |
| | | | Rechts | Min N | ▷ -99.63 | -0.27 | 16.81 | 0.00 | 0.00 | 0.00 | BC 172 |
| | | | | Max $V_y$ | -78.50 | ▷ 0.42 | 18.55 | 0.00 | 0.00 | -0.00 | BC 433 |
| | | | | Min $V_y$ | -75.53 | ▷ -0.30 | 16.83 | 0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Max $V_z$ | -78.08 | 0.42 | ▷ 18.55 | 0.00 | 0.00 | -0.00 | BC 461 |
| | | | | Min $V_z$ | -60.98 | 0.03 | ▷ -17.36 | -0.00 | -0.00 | -0.00 | BC 187 |
| | | | | Max $M_T$ | -91.33 | -0.28 | 16.81 | ▷ 0.00 | 0.00 | 0.00 | BC 164 |
| | | | | Min $M_T$ | -61.66 | 0.03 | -17.36 | ▷ -0.00 | -0.00 | -0.00 | BC 235 |
| | | | | Max $M_y$ | -67.63 | 0.41 | 18.55 | 0.00 | ▷ 0.00 | -0.00 | BC 381 |
| | | | | Min $M_y$ | -43.69 | 0.02 | -17.34 | -0.00 | ▷ -0.00 | -0.00 | BC 379 |
| | | | | Max $M_z$ | -75.53 | -0.30 | 16.83 | 0.00 | 0.00 | ▷ 0.00 | BC 360 |
| | | | | Min $M_z$ | -78.50 | 0.42 | 18.55 | 0.00 | 0.00 | ▷ -0.00 | BC 433 |
| | | | 2173 | Max N | ▷ -32.01 | 0.02 | -5.04 | -0.00 | -24.31 | -0.04 | BC 419 |
| | | | Links | Min N | ▷ -97.09 | -0.27 | 4.83 | 0.00 | 23.50 | 0.59 | BC 172 |
| | | | | Max $V_y$ | -76.76 | ▷ 0.42 | 5.43 | 0.00 | 26.05 | -0.92 | BC 433 |
| | | | | Min $V_y$ | -73.79 | ▷ -0.30 | 4.84 | 0.00 | 23.54 | 0.66 | BC 360 |
| | | | | Max $V_z$ | -76.34 | 0.42 | ▷ 5.43 | 0.00 | 26.05 | -0.92 | BC 461 |
| | | | | Min $V_z$ | -58.44 | 0.03 | ▷ -5.06 | -0.00 | -24.35 | -0.06 | BC 187 |
| | | | | Max $M_T$ | -88.79 | -0.28 | 4.83 | ▷ 0.00 | 23.50 | 0.61 | BC 164 |
| | | | | Min $M_T$ | -59.11 | 0.03 | -5.06 | ▷ -0.00 | -24.34 | -0.07 | BC 235 |
| | | | | Max $M_y$ | -76.34 | 0.42 | 5.43 | 0.00 | ▷ 26.05 | -0.92 | BC 461 |
| | | | | Min $M_y$ | -58.44 | 0.03 | -5.06 | -0.00 | ▷ -24.35 | -0.06 | BC 187 |
| | | | | Max $M_z$ | -73.79 | -0.30 | 4.84 | 0.00 | 23.54 | ▷ 0.66 | BC 360 |
| | | | | Min $M_z$ | -76.76 | 0.42 | 5.43 | 0.00 | 26.05 | ▷ -0.92 | BC 433 |
| | | 92 | 2173 | Max N | ▷ -32.01 | 0.02 | -5.04 | -0.00 | -24.31 | -0.04 | BC 419 |
| | | | Rechts | Min N | ▷ -97.09 | -0.27 | 4.83 | 0.00 | 23.50 | 0.59 | BC 172 |
| | | | | Max $V_y$ | -76.76 | ▷ 0.42 | 5.43 | 0.00 | 26.05 | -0.92 | BC 433 |
| | | | | Min $V_y$ | -73.79 | ▷ -0.30 | 4.84 | 0.00 | 23.54 | 0.66 | BC 360 |
| | | | | Max $V_z$ | -76.34 | 0.42 | ▷ 5.43 | 0.00 | 26.05 | -0.92 | BC 461 |
| | | | | Min $V_z$ | -58.44 | 0.03 | ▷ -5.06 | -0.00 | -24.35 | -0.06 | BC 187 |
| | | | | Max $M_T$ | -88.79 | -0.28 | 4.83 | ▷ 0.00 | 23.50 | 0.61 | BC 164 |
| | | | | Min $M_T$ | -59.11 | 0.03 | -5.06 | ▷ -0.00 | -24.34 | -0.07 | BC 235 |
| | | | | Max $M_y$ | -76.34 | 0.42 | 5.43 | 0.00 | ▷ 26.05 | -0.92 | BC 461 |
| | | | | Min $M_y$ | -58.44 | 0.03 | -5.06 | -0.00 | ▷ -24.35 | -0.06 | BC 187 |
| | | | | Max $M_z$ | -73.79 | -0.30 | 4.84 | 0.00 | 23.54 | ▷ 0.66 | BC 360 |
| | | | | Min $M_z$ | -76.76 | 0.42 | 5.43 | 0.00 | 26.05 | ▷ -0.92 | BC 433 |
| | | 92 | 2173 | Max N | ▷ -32.01 | 0.02 | -5.04 | -0.00 | -24.31 | -0.04 | BC 419 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 32 | RC1 | 59 | 0 | Min N | ▷ -99.63 | -0.27 | 16.81 | 0.00 | -0.00 | 0.00 | BC 172 |
| | | 59 | 0 | Max $V_y$ | -78.50 | ▷ 0.42 | 18.55 | 0.00 | -0.00 | 0.00 | BC 433 |
| | | 59 | 0 | Min $V_y$ | -75.53 | ▷ -0.30 | 16.83 | 0.00 | -0.00 | 0.00 | BC 360 |
| | | 59 | 0 | Max $V_z$ | -78.08 | 0.42 | ▷ 18.55 | 0.00 | -0.00 | 0.00 | BC 461 |
| | | 59 | 0 | Min $V_z$ | -60.98 | 0.03 | ▷ -17.36 | -0.00 | 0.00 | 0.00 | BC 187 |
| | | 59 | 0 | Max $M_T$ | -91.33 | -0.28 | 16.81 | ▷ 0.00 | -0.00 | 0.00 | BC 164 |
| | | 59 | 0 | Min $M_T$ | -61.66 | 0.03 | -17.36 | ▷ -0.00 | 0.00 | 0.00 | BC 235 |
| | | 92 | 2173 | Max $M_y$ | -76.34 | 0.42 | 5.43 | 0.00 | ▷ 26.05 | -0.92 | BC 461 |
| | | 92 | 2173 | Min $M_y$ | -58.44 | 0.03 | -5.06 | -0.00 | ▷ -24.35 | -0.06 | BC 187 |
| | | 92 | 2173 | Max $M_z$ | -73.79 | -0.30 | 4.84 | 0.00 | 23.54 | ▷ 0.66 | BC 360 |
| | | 92 | 2173 | Min $M_z$ | -76.76 | 0.42 | 5.43 | 0.00 | 26.05 | ▷ -0.92 | BC 433 |
| 178 | RC1 | 92 | 0 | Max N | ▷ -36.37 | -0.15 | -0.03 | -0.00 | -0.07 | -0.08 | BC 49 |
| | | | Links | Min N | ▷ -105.67 | -0.45 | -0.00 | -0.00 | -0.00 | -0.18 | BC 154 |
| | | | | Max $V_y$ | -67.76 | ▷ 0.73 | 4.84 | 0.00 | 23.54 | 0.66 | BC 360 |
| | | | | Min $V_y$ | -97.84 | ▷ -1.40 | 5.42 | 0.00 | 26.02 | -0.92 | BC 269 |
| | | | | Max $V_z$ | -81.27 | -1.37 | ▷ 5.43 | 0.00 | 26.05 | -0.92 | BC 461 |
| | | | | Min $V_z$ | -65.51 | -0.17 | ▷ -5.06 | -0.00 | -24.35 | -0.06 | BC 187 |
| | | | | Max $M_T$ | -84.45 | 0.61 | 4.83 | ▷ 0.00 | 23.50 | 0.61 | BC 164 |
| | | | | Min $M_T$ | -66.65 | -0.19 | -5.06 | ▷ -0.00 | -24.34 | -0.07 | BC 235 |
| | | | | Max $M_y$ | -81.27 | -1.37 | 5.43 | 0.00 | ▷ 26.05 | -0.92 | BC 461 |
| | | | | Min $M_y$ | -65.51 | -0.17 | -5.06 | -0.00 | ▷ -24.35 | -0.06 | BC 187 |
| | | | | Max $M_z$ | -67.76 | 0.73 | 4.84 | 0.00 | 23.54 | ▷ 0.66 | BC 360 |
| | | | | Min $M_z$ | -81.58 | -1.37 | 5.43 | 0.00 | 26.05 | ▷ -0.92 | BC 433 |
| | | | 0 | Max N | ▷ -36.37 | -0.15 | -0.03 | -0.00 | -0.07 | -0.08 | BC 49 |
| | | | Rechts | Min N | ▷ -105.67 | -0.45 | -0.00 | -0.00 | -0.00 | -0.18 | BC 154 |
| | | | | Max $V_y$ | -67.76 | ▷ 0.73 | 4.84 | 0.00 | 23.54 | 0.66 | BC 360 |
| | | | | Min $V_y$ | -97.84 | ▷ -1.40 | 5.42 | 0.00 | 26.02 | -0.92 | BC 269 |
| | | | | Max $V_z$ | -81.27 | -1.37 | ▷ 5.43 | 0.00 | 26.05 | -0.92 | BC 461 |
| | | | | Min $V_z$ | -65.51 | -0.17 | ▷ -5.06 | -0.00 | -24.35 | -0.06 | BC 187 |
| | | | | Max $M_T$ | -84.45 | 0.61 | 4.83 | ▷ 0.00 | 23.50 | 0.61 | BC 164 |
| | | | | Min $M_T$ | -66.65 | -0.19 | -5.06 | ▷ -0.00 | -24.34 | -0.07 | BC 235 |
| | | | | Max $M_y$ | -81.27 | -1.37 | 5.43 | 0.00 | ▷ 26.05 | -0.92 | BC 461 |
| | | | | Min $M_y$ | -65.51 | -0.17 | -5.06 | -0.00 | ▷ -24.35 | -0.06 | BC 187 |
| | | | | Max $M_z$ | -67.76 | 0.73 | 4.84 | 0.00 | 23.54 | ▷ 0.66 | BC 360 |
| | | | | Min $M_z$ | -81.58 | -1.37 | 5.43 | 0.00 | 26.05 | ▷ -0.92 | BC 433 |
| | | | 328 | Max N | ▷ -36.11 | -0.15 | -0.03 | -0.00 | -0.08 | -0.03 | BC 49 |
| | | | Links | Min N | ▷ -105.29 | -0.45 | -0.00 | -0.00 | -0.01 | -0.04 | BC 154 |
| | | | | Max $V_y$ | -67.50 | ▷ 0.73 | 3.04 | 0.00 | 24.83 | 0.42 | BC 360 |
| | | | | Min $V_y$ | -97.46 | ▷ -1.40 | 3.44 | 0.00 | 27.47 | -0.46 | BC 269 |
| | | | | Max $V_z$ | -81.01 | -1.37 | ▷ 3.45 | 0.00 | 27.51 | -0.47 | BC 461 |
| | | | | Min $V_z$ | -65.13 | -0.17 | ▷ -3.20 | -0.00 | -25.70 | -0.01 | BC 187 |
| | | | | Max $M_T$ | -84.07 | 0.61 | 3.02 | ▷ 0.00 | 24.79 | 0.40 | BC 164 |
| | | | | Min $M_T$ | -66.27 | -0.19 | -3.20 | ▷ -0.00 | -25.69 | -0.01 | BC 235 |
| | | | | Max $M_y$ | -81.01 | -1.37 | 3.45 | 0.00 | ▷ 27.51 | -0.47 | BC 461 |
| | | | | Min $M_y$ | -65.13 | -0.17 | -3.20 | -0.00 | ▷ -25.70 | -0.01 | BC 187 |
| | | | | Max $M_z$ | -67.50 | 0.73 | 3.04 | 0.00 | 24.83 | ▷ 0.42 | BC 360 |
| | | | | Min $M_z$ | -81.32 | -1.37 | 3.45 | 0.00 | 27.51 | ▷ -0.47 | BC 433 |
| | | | 328 | Max N | ▷ -36.11 | -0.15 | -0.03 | -0.00 | -0.08 | -0.03 | BC 49 |
| | | | Rechts | Min N | ▷ -105.29 | -0.45 | -0.00 | -0.00 | -0.01 | -0.04 | BC 154 |
| | | | | Max $V_y$ | -67.50 | ▷ 0.73 | 3.04 | 0.00 | 24.83 | 0.42 | BC 360 |
| | | | | Min $V_y$ | -97.46 | ▷ -1.40 | 3.44 | 0.00 | 27.47 | -0.46 | BC 269 |
| | | | | Max $V_z$ | -81.01 | -1.37 | ▷ 3.45 | 0.00 | 27.51 | -0.47 | BC 461 |
| | | | | Min $V_z$ | -65.13 | -0.17 | ▷ -3.20 | -0.00 | -25.70 | -0.01 | BC 187 |
| | | | | Max $M_T$ | -84.07 | 0.61 | 3.02 | ▷ 0.00 | 24.79 | 0.40 | BC 164 |
| | | | | Min $M_T$ | -66.27 | -0.19 | -3.20 | ▷ -0.00 | -25.69 | -0.01 | BC 235 |
| | | | | Max $M_y$ | -81.01 | -1.37 | 3.45 | 0.00 | ▷ 27.51 | -0.47 | BC 461 |
| | | | | Min $M_y$ | -65.13 | -0.17 | -3.20 | -0.00 | ▷ -25.70 | -0.01 | BC 187 |
| | | | | Max $M_z$ | -67.50 | 0.73 | 3.04 | 0.00 | 24.83 | ▷ 0.42 | BC 360 |
| | | | | Min $M_z$ | -81.32 | -1.37 | 3.45 | 0.00 | 27.51 | ▷ -0.47 | BC 433 |
| | | | 2172 | Max N | ▷ -31.43 | -0.15 | -0.03 | -0.00 | -0.14 | 0.24 | BC 49 |
| | | | Links | Min N | ▷ -98.42 | -0.45 | -0.00 | -0.00 | -0.01 | 0.78 | BC 154 |
| | | | | Max $V_y$ | -62.81 | ▷ 0.73 | -7.14 | 0.00 | 21.05 | -0.92 | BC 360 |
| | | | | Min $V_y$ | -90.59 | ▷ -1.40 | -7.71 | 0.00 | 23.53 | 2.12 | BC 269 |
| | | | | Max $V_z$ | -50.71 | -0.27 | ▷ 7.30 | -0.00 | -21.73 | 0.47 | BC 463 |
| | | | | Min $V_z$ | -71.78 | -1.27 | ▷ -7.75 | 0.00 | 23.34 | 1.91 | BC 169 |
| | | | | Max $M_T$ | -77.20 | 0.61 | -7.15 | ▷ 0.00 | 20.98 | -0.73 | BC 164 |
| | | | | Min $M_T$ | -59.40 | -0.19 | 7.24 | ▷ -0.00 | -21.97 | 0.34 | BC 235 |
| | | | | Max $M_y$ | -76.32 | -1.37 | -7.69 | 0.00 | ▷ 23.60 | 2.06 | BC 461 |
| | | | | Min $M_y$ | -58.26 | -0.17 | 7.24 | -0.00 | ▷ -21.97 | 0.30 | BC 187 |
| | | | | Max $M_z$ | -90.59 | -1.40 | -7.71 | 0.00 | 23.53 | ▷ 2.12 | BC 269 |
| | | | | Min $M_z$ | -62.81 | 0.73 | -7.14 | 0.00 | 21.05 | ▷ -0.92 | BC 360 |
| | | 80 | 2172 | Max N | ▷ -31.43 | -0.15 | -0.03 | -0.00 | -0.14 | 0.24 | BC 49 |
| | | | Rechts | Min N | ▷ -98.42 | -0.45 | -0.00 | -0.00 | -0.01 | 0.78 | BC 154 |
| | | | | Max $V_y$ | -62.81 | ▷ 0.73 | -7.14 | 0.00 | 21.05 | -0.92 | BC 360 |
| | | | | Min $V_y$ | -90.59 | ▷ -1.40 | -7.71 | 0.00 | 23.53 | 2.12 | BC 269 |
| | | | | Max $V_z$ | -50.71 | -0.27 | ▷ 7.30 | -0.00 | -21.73 | 0.47 | BC 463 |
| | | | | Min $V_z$ | -71.78 | -1.27 | ▷ -7.75 | 0.00 | 23.34 | 1.91 | BC 169 |
| | | | | Max $M_T$ | -77.20 | 0.61 | -7.15 | ▷ 0.00 | 20.98 | -0.73 | BC 164 |
| | | | | Min $M_T$ | -59.40 | -0.19 | 7.24 | ▷ -0.00 | -21.97 | 0.34 | BC 235 |
| | | | | Max $M_y$ | -76.32 | -1.37 | -7.69 | 0.00 | ▷ 23.60 | 2.06 | BC 461 |
| | | | | Min $M_y$ | -58.26 | -0.17 | 7.24 | -0.00 | ▷ -21.97 | 0.30 | BC 187 |
| | | | | Max $M_z$ | -90.59 | -1.40 | -7.71 | 0.00 | 23.53 | ▷ 2.12 | BC 269 |
| | | | | Min $M_z$ | -62.81 | 0.73 | -7.14 | 0.00 | 21.05 | ▷ -0.92 | BC 360 |
| | | 80 | 2172 | Max N | ▷ -31.43 | -0.15 | -0.03 | -0.00 | -0.14 | 0.24 | BC 49 |
| | | 92 | 0 | Min N | ▷ -105.67 | -0.45 | -0.00 | -0.00 | -0.00 | -0.18 | BC 154 |
| | | 92 | 0 | Max $V_y$ | -67.76 | ▷ 0.73 | 4.84 | 0.00 | 23.54 | 0.66 | BC 360 |
| | | 92 | 0 | Min $V_y$ | -97.84 | ▷ -1.40 | 5.42 | 0.00 | 26.02 | -0.92 | BC 269 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 178 | RC1 | 80 | 2172 | Max $V_z$ | -50.71 | -0.27 | ▷ 7.30 | -0.00 | -21.73 | 0.47 | BC 463 |
| | | 80 | 2172 | Min $V_z$ | -71.78 | -1.27 | ▷ -7.75 | 0.00 | 23.34 | 1.91 | BC 169 |
| | | 92 | 0 | Max $M_T$ | -84.45 | 0.61 | 4.83 | ▷ 0.00 | 23.50 | 0.61 | BC 164 |
| | | 92 | 0 | Min $M_T$ | -66.65 | -0.19 | -5.06 | ▷ -0.00 | -24.34 | -0.07 | BC 235 |
| | | | 988 | Max $M_y$ | -79.34 | -1.37 | -0.53 | 0.00 | ▷ 28.47 | 0.44 | BC 461 |
| | | | 988 | Min $M_y$ | -62.67 | -0.17 | 0.53 | -0.00 | ▷ -26.58 | 0.10 | BC 187 |
| | | 80 | 2172 | Max $M_z$ | -90.59 | -1.40 | -7.71 | 0.00 | 23.53 | ▷ 2.12 | BC 269 |
| | | 92 | 0 | Min $M_z$ | -81.58 | -1.37 | 5.43 | 0.00 | 26.05 | ▷ -0.92 | BC 433 |
| 103 | RC1 | 80 | 0 | Max N | ▷ -29.96 | 0.07 | 0.04 | -0.00 | -0.14 | 0.24 | BC 49 |
| | | | Links | Min N | ▷ -97.09 | 0.00 | 0.01 | -0.00 | -0.01 | 0.78 | BC 154 |
| | | | | Max $V_y$ | -68.01 | ▷ 1.02 | 4.28 | 0.00 | 21.13 | -0.03 | BC 236 |
| | | | | Min $V_y$ | -70.07 | ▷ -0.16 | 4.64 | 0.00 | 23.55 | 2.10 | BC 237 |
| | | | | Max $V_z$ | -52.04 | 0.09 | ▷ 4.68 | 0.00 | 23.36 | 1.93 | BC 197 |
| | | | | Min $V_z$ | -38.22 | 0.03 | ▷ -4.38 | -0.00 | -21.75 | 0.43 | BC 471 |
| | | | | Max $M_T$ | -52.72 | 0.66 | 4.32 | ▷ 0.00 | 21.00 | -0.73 | BC 164 |
| | | | | Min $M_T$ | -57.41 | 0.07 | -4.31 | ▷ -0.00 | -21.99 | 0.34 | BC 235 |
| | | | | Max $M_y$ | -56.35 | -0.10 | 4.62 | 0.00 | ▷ 23.62 | 2.06 | BC 461 |
| | | | | Min $M_y$ | -56.23 | 0.06 | -4.31 | -0.00 | ▷ -21.99 | 0.30 | BC 187 |
| | | | | Max $M_z$ | -70.16 | -0.15 | 4.64 | 0.00 | 23.55 | ▷ 2.12 | BC 269 |
| | | | | Min $M_z$ | -39.07 | 0.54 | 4.30 | 0.00 | 21.06 | ▷ -0.92 | BC 360 |
| | | | 0 | Max N | ▷ -29.96 | 0.07 | 0.04 | -0.00 | -0.14 | 0.24 | BC 49 |
| | | | Rechts | Min N | ▷ -97.09 | 0.00 | 0.01 | -0.00 | -0.01 | 0.78 | BC 154 |
| | | | | Max $V_y$ | -68.01 | ▷ 1.02 | 4.28 | 0.00 | 21.13 | -0.03 | BC 236 |
| | | | | Min $V_y$ | -70.07 | ▷ -0.16 | 4.64 | 0.00 | 23.55 | 2.10 | BC 237 |
| | | | | Max $V_z$ | -52.04 | 0.09 | ▷ 4.68 | 0.00 | 23.36 | 1.93 | BC 197 |
| | | | | Min $V_z$ | -38.22 | 0.03 | ▷ -4.38 | -0.00 | -21.75 | 0.43 | BC 471 |
| | | | | Max $M_T$ | -52.72 | 0.66 | 4.32 | ▷ 0.00 | 21.00 | -0.73 | BC 164 |
| | | | | Min $M_T$ | -57.41 | 0.07 | -4.31 | ▷ -0.00 | -21.99 | 0.34 | BC 235 |
| | | | | Max $M_y$ | -56.35 | -0.10 | 4.62 | 0.00 | ▷ 23.62 | 2.06 | BC 461 |
| | | | | Min $M_y$ | -56.23 | 0.06 | -4.31 | -0.00 | ▷ -21.99 | 0.30 | BC 187 |
| | | | | Max $M_z$ | -70.16 | -0.15 | 4.64 | 0.00 | 23.55 | ▷ 2.12 | BC 269 |
| | | | | Min $M_z$ | -39.07 | 0.54 | 4.30 | 0.00 | 21.06 | ▷ -0.92 | BC 360 |
| | | | 3627 | Max N | ▷ -20.67 | 0.07 | 0.04 | -0.00 | 0.00 | -0.00 | BC 49 |
| | | | Links | Min N | ▷ -83.47 | 0.00 | 0.01 | -0.00 | 0.04 | 0.78 | BC 154 |
| | | | | Max $V_y$ | -54.39 | ▷ 1.02 | -15.72 | 0.00 | 0.39 | -3.73 | BC 236 |
| | | | | Min $V_y$ | -56.44 | ▷ -0.16 | -17.26 | 0.00 | 0.66 | 2.69 | BC 237 |
| | | | | Max $V_z$ | -42.61 | 0.06 | ▷ 16.22 | -0.00 | -0.41 | 0.09 | BC 187 |
| | | | | Min $V_z$ | -46.89 | -0.10 | ▷ -17.28 | 0.00 | 0.66 | 2.40 | BC 457 |
| | | | | Max $M_T$ | -39.10 | 0.66 | -15.68 | ▷ 0.00 | 0.39 | -3.11 | BC 164 |
| | | | | Min $M_T$ | -43.79 | 0.07 | 16.22 | ▷ -0.00 | -0.41 | 0.08 | BC 235 |
| | | | | Max $M_y$ | -47.21 | -0.10 | -17.28 | 0.00 | ▷ 0.66 | 2.43 | BC 433 |
| | | | | Min $M_y$ | -20.68 | 0.04 | 16.20 | -0.00 | ▷ -0.41 | 0.00 | BC 359 |
| | | | | Max $M_z$ | -56.62 | -0.16 | -17.26 | 0.00 | 0.66 | ▷ 2.70 | BC 241 |
| | | | | Min $M_z$ | -42.94 | 1.01 | -15.72 | 0.00 | 0.39 | ▷ -3.75 | BC 248 |
| | | | 3627 | Max N | ▷ -20.67 | 0.07 | 0.04 | -0.00 | 0.00 | -0.00 | BC 49 |
| | | | Rechts | Min N | ▷ -83.47 | 0.00 | 0.01 | -0.00 | 0.04 | 0.78 | BC 154 |
| | | | | Max $V_y$ | -54.39 | ▷ 1.02 | -15.72 | 0.00 | 0.39 | -3.73 | BC 236 |
| | | | | Min $V_y$ | -56.44 | ▷ -0.16 | -17.26 | 0.00 | 0.66 | 2.69 | BC 237 |
| | | | | Max $V_z$ | -42.61 | 0.06 | ▷ 16.22 | -0.00 | -0.41 | 0.09 | BC 187 |
| | | | | Min $V_z$ | -46.89 | -0.10 | ▷ -17.28 | 0.00 | 0.66 | 2.40 | BC 457 |
| | | | | Max $M_T$ | -39.10 | 0.66 | -15.68 | ▷ 0.00 | 0.39 | -3.11 | BC 164 |
| | | | | Min $M_T$ | -43.79 | 0.07 | 16.22 | ▷ -0.00 | -0.41 | 0.08 | BC 235 |
| | | | | Max $M_y$ | -47.21 | -0.10 | -17.28 | 0.00 | ▷ 0.66 | 2.43 | BC 433 |
| | | | | Min $M_y$ | -20.68 | 0.04 | 16.20 | -0.00 | ▷ -0.41 | 0.00 | BC 359 |
| | | | | Max $M_z$ | -56.62 | -0.16 | -17.26 | 0.00 | 0.66 | ▷ 2.70 | BC 241 |
| | | | | Min $M_z$ | -42.94 | 1.01 | -15.72 | 0.00 | 0.39 | ▷ -3.75 | BC 248 |
| | | | 3686 | Max N | ▷ -20.53 | 0.07 | 0.04 | -0.00 | 0.00 | -0.01 | BC 49 |
| | | | Links | Min N | ▷ -83.26 | 0.00 | 0.01 | -0.00 | 0.04 | 0.78 | BC 154 |
| | | | | Max $V_y$ | -54.18 | ▷ 1.02 | -16.05 | 0.00 | -0.56 | -3.79 | BC 236 |
| | | | | Min $V_y$ | -56.24 | ▷ -0.16 | -17.63 | 0.00 | -0.39 | 2.70 | BC 237 |
| | | | | Max $V_z$ | -42.40 | 0.06 | ▷ 16.56 | -0.00 | 0.57 | 0.08 | BC 187 |
| | | | | Min $V_z$ | -46.75 | -0.10 | ▷ -17.64 | 0.00 | -0.39 | 2.40 | BC 457 |
| | | | | Max $M_T$ | -38.89 | 0.66 | -16.01 | ▷ 0.00 | -0.56 | -3.15 | BC 164 |
| | | | | Min $M_T$ | -43.58 | 0.07 | 16.55 | ▷ -0.00 | 0.57 | 0.07 | BC 235 |
| | | | | Max $M_y$ | -50.57 | 0.02 | 16.51 | -0.00 | ▷ 0.59 | 0.52 | BC 243 |
| | | | | Min $M_y$ | -32.89 | 0.84 | -16.07 | 0.00 | ▷ -0.56 | -3.46 | BC 408 |
| | | | | Max $M_z$ | -56.41 | -0.16 | -17.63 | 0.00 | -0.38 | ▷ 2.71 | BC 241 |
| | | | | Min $M_z$ | -42.74 | 1.01 | -16.05 | 0.00 | -0.56 | ▷ -3.82 | BC 248 |
| | | | 3686 | Max N | ▷ -20.53 | 0.07 | 0.04 | -0.00 | 0.00 | -0.01 | BC 49 |
| | | | Rechts | Min N | ▷ -83.26 | 0.00 | 0.01 | -0.00 | 0.04 | 0.78 | BC 154 |
| | | | | Max $V_y$ | -54.18 | ▷ 1.02 | -16.05 | 0.00 | -0.56 | -3.79 | BC 236 |
| | | | | Min $V_y$ | -56.24 | ▷ -0.16 | -17.63 | 0.00 | -0.39 | 2.70 | BC 237 |
| | | | | Max $V_z$ | -42.40 | 0.06 | ▷ 16.56 | -0.00 | 0.58 | 0.08 | BC 187 |
| | | | | Min $V_z$ | -46.75 | -0.10 | ▷ -17.64 | 0.00 | -0.39 | 2.40 | BC 457 |
| | | | | Max $M_T$ | -38.89 | 0.66 | -16.01 | ▷ 0.00 | -0.56 | -3.15 | BC 164 |
| | | | | Min $M_T$ | -43.58 | 0.07 | 16.56 | ▷ -0.00 | 0.57 | 0.07 | BC 235 |
| | | | | Max $M_y$ | -50.57 | 0.02 | 16.51 | -0.00 | ▷ 0.60 | 0.52 | BC 243 |
| | | | | Min $M_y$ | -32.89 | 0.84 | -16.07 | 0.00 | ▷ -0.56 | -3.46 | BC 408 |
| | | | | Max $M_z$ | -56.41 | -0.16 | -17.63 | 0.00 | -0.38 | ▷ 2.71 | BC 241 |
| | | | | Min $M_z$ | -42.74 | 1.01 | -16.05 | 0.00 | -0.56 | ▷ -3.82 | BC 248 |
| | | | 3748 | Max N | ▷ -20.44 | 0.07 | 0.04 | -0.00 | 0.01 | -0.01 | BC 49 |
| | | | Links | Min N | ▷ -83.12 | 0.00 | 0.01 | -0.00 | 0.04 | 0.78 | BC 154 |
| | | | | Max $V_y$ | -54.05 | ▷ 1.02 | -16.39 | 0.00 | -1.56 | -3.85 | BC 236 |
| | | | | Min $V_y$ | -56.10 | ▷ -0.16 | -18.00 | 0.00 | -1.48 | 2.70 | BC 237 |
| | | | | Max $V_z$ | -42.27 | 0.06 | ▷ 16.90 | -0.00 | 1.60 | 0.08 | BC 187 |
| | | | | Min $V_z$ | -46.66 | -0.10 | ▷ -18.02 | 0.00 | -1.48 | 2.41 | BC 457 |
| | | | | Max $M_T$ | -38.76 | 0.66 | -16.35 | ▷ 0.00 | -1.56 | -3.19 | BC 164 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 103 | RC1 | | | Min $M_T$ | -43.45 | 0.07 | 16.90 | ▷ -0.00 | 1.60 | 0.07 | BC 235 |
| | | | | Max $M_y$ | -50.44 | 0.02 | 16.86 | -0.00 | ▷ 1.62 | 0.52 | BC 243 |
| | | | | Min $M_y$ | -32.80 | 0.84 | -16.41 | 0.00 | ▷ -1.56 | -3.51 | BC 408 |
| | | | | Max $M_z$ | -56.28 | -0.16 | -18.00 | 0.00 | -1.48 | ▷ 2.72 | BC 241 |
| | | | | Min $M_z$ | -42.60 | 1.01 | -16.39 | 0.00 | -1.56 | ▷ -3.88 | BC 248 |
| | | 42 | 3748 | Max N | ▷ -20.44 | 0.07 | 0.04 | -0.00 | 0.01 | -0.01 | BC 49 |
| | | | Rechts | Min N | ▷ -83.12 | 0.00 | 0.01 | -0.00 | 0.04 | 0.78 | BC 154 |
| | | | | Max $V_y$ | -54.05 | ▷ 1.02 | -16.39 | 0.00 | -1.56 | -3.85 | BC 236 |
| | | | | Min $V_y$ | -56.10 | ▷ -0.16 | -18.00 | 0.00 | -1.48 | 2.70 | BC 237 |
| | | | | Max $V_z$ | -42.27 | 0.06 | ▷ 16.90 | -0.00 | 1.60 | 0.08 | BC 187 |
| | | | | Min $V_z$ | -46.66 | -0.10 | ▷ -18.02 | 0.00 | -1.48 | 2.41 | BC 457 |
| | | | | Max $M_T$ | -38.76 | 0.66 | -16.35 | ▷ 0.00 | -1.56 | -3.19 | BC 164 |
| | | | | Min $M_T$ | -43.45 | 0.07 | 16.90 | ▷ -0.00 | 1.60 | 0.07 | BC 235 |
| | | | | Max $M_y$ | -50.44 | 0.02 | 16.86 | -0.00 | ▷ 1.62 | 0.52 | BC 243 |
| | | | | Min $M_y$ | -32.80 | 0.84 | -16.41 | 0.00 | ▷ -1.56 | -3.51 | BC 408 |
| | | | | Max $M_z$ | -56.28 | -0.16 | -18.00 | 0.00 | -1.48 | ▷ 2.72 | BC 241 |
| | | | | Min $M_z$ | -42.60 | 1.01 | -16.39 | 0.00 | -1.56 | ▷ -3.88 | BC 248 |
| | | 42 | 3748 | Max N | ▷ -20.44 | 0.07 | 0.04 | -0.00 | 0.01 | -0.01 | BC 49 |
| | | 80 | 0 | Min N | ▷ -97.09 | 0.00 | 0.01 | -0.00 | -0.01 | 0.78 | BC 154 |
| | | 80 | 0 | Max $V_y$ | -68.01 | ▷ 1.02 | 4.28 | 0.00 | 21.13 | -0.03 | BC 236 |
| | | 80 | 0 | Min $V_y$ | -70.07 | ▷ -0.16 | 4.64 | 0.00 | 23.55 | 2.10 | BC 237 |
| | | 42 | 3748 | Max $V_z$ | -42.27 | 0.06 | ▷ 16.90 | -0.00 | 1.60 | 0.08 | BC 187 |
| | | 42 | 3748 | Min $V_z$ | -46.66 | -0.10 | ▷ -18.02 | 0.00 | -1.48 | 2.41 | BC 457 |
| | | 80 | 0 | Max $M_T$ | -52.72 | 0.66 | 4.32 | ▷ 0.00 | 21.00 | -0.73 | BC 164 |
| | | 80 | 0 | Min $M_T$ | -57.41 | 0.07 | -4.31 | ▷ -0.00 | -21.99 | 0.34 | BC 235 |
| | | | 789 | Max $M_y$ | -54.34 | -0.10 | -0.14 | 0.00 | ▷ 25.38 | 2.14 | BC 461 |
| | | | 789 | Min $M_y$ | -53.28 | 0.06 | 0.15 | -0.00 | ▷ -23.63 | 0.25 | BC 187 |
| | | 42 | 3748 | Max $M_z$ | -56.28 | -0.16 | -18.00 | 0.00 | -1.48 | ▷ 2.72 | BC 241 |
| | | 42 | 3748 | Min $M_z$ | -42.60 | 1.01 | -16.39 | 0.00 | -1.56 | ▷ -3.88 | BC 248 |
| 103 | RC1 | 42 | 3748 | MAX N | ▷ -20.44 | 0.07 | 0.04 | 0.00 | 0.01 | -0.01 | BC 49 |
| 178 | RC1 | 92 | 0 | MIN N | ▷ -105.67 | -0.45 | 0.00 | 0.00 | 0.00 | -0.18 | BC 154 |
| 103 | RC1 | 80 | 0 | MAX $V_y$ | -68.01 | ▷ 1.02 | 4.28 | 0.00 | 21.13 | -0.03 | BC 236 |
| 178 | RC1 | 92 | 0 | MIN $V_y$ | -97.84 | ▷ -1.40 | 5.42 | 0.00 | 26.02 | -0.92 | BC 269 |
| 32 | RC1 | 59 | 0 | MAX $V_z$ | -78.08 | 0.42 | ▷ 18.55 | 0.00 | 0.00 | 0.00 | BC 461 |
| 103 | RC1 | 42 | 3748 | MIN $V_z$ | -46.66 | -0.10 | ▷ -18.02 | 0.00 | -1.48 | 2.41 | BC 457 |
| 32 | RC1 | 59 | 0 | MAX $M_T$ | -91.33 | -0.28 | 16.81 | ▷ 0.00 | 0.00 | 0.00 | BC 164 |
| 32 | RC1 | 59 | 0 | MIN $M_T$ | -61.66 | 0.03 | -17.36 | ▷ 0.00 | 0.00 | 0.00 | BC 235 |
| 178 | RC1 | | 988 | MAX $M_y$ | -79.34 | -1.37 | -0.53 | 0.00 | ▷ 28.47 | 0.44 | BC 461 |
| 178 | RC1 | | 988 | MIN $M_y$ | -62.67 | -0.17 | 0.53 | 0.00 | ▷ -26.58 | 0.10 | BC 187 |
| 103 | RC1 | 42 | 3748 | MAX $M_z$ | -56.28 | -0.16 | -18.00 | 0.00 | -1.48 | ▷ 2.72 | BC 241 |
| 103 | RC1 | 42 | 3748 | MIN $M_z$ | -42.60 | 1.01 | -16.39 | 0.00 | -1.56 | ▷ -3.88 | BC 248 |
| | **Doorgaande staven No. 20: Doorgaande staven 23** | | | | | | | | | | |
| 43 | RC1 | 43 | 0 | Max N | ▷ -54.57 | -2.83 | 0.47 | 0.00 | 0.00 | 0.00 | BC 473 |
| | | | | Min N | ▷ -215.27 | -0.03 | 0.11 | 0.00 | 0.00 | 0.00 | BC 131 |
| | | | | Max $V_y$ | -90.46 | ▷ 2.63 | 0.18 | 0.00 | 0.00 | 0.00 | BC 403 |
| | | | | Min $V_y$ | -115.89 | ▷ -2.85 | 0.39 | 0.00 | 0.00 | 0.00 | BC 233 |
| | | | | Max $V_z$ | -82.36 | -2.60 | ▷ 0.72 | -0.00 | 0.00 | 0.00 | BC 216 |
| | | | | Min $V_z$ | -57.38 | -1.67 | ▷ -0.60 | -0.00 | 0.00 | 0.00 | BC 390 |
| | | | | Max $M_T$ | -115.71 | -2.84 | 0.47 | ▷ 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min $M_T$ | -57.18 | -1.67 | -0.55 | ▷ -0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Max $M_y$ | -115.71 | -2.84 | 0.47 | 0.00 | ▷ 0.00 | 0.00 | BC 177 |
| | | | | Min $M_y$ | -117.56 | -2.60 | 0.70 | -0.00 | ▷ -0.00 | 0.00 | BC 268 |
| | | | | Max $M_z$ | -92.46 | -1.67 | -0.52 | -0.00 | -0.00 | ▷ 0.00 | BC 378 |
| | | | | Min $M_z$ | -54.59 | -2.83 | 0.46 | 0.00 | -0.00 | ▷ -0.00 | BC 381 |
| | | 87 | 4345 | Max N | ▷ -51.10 | -2.83 | 0.47 | 0.00 | 2.04 | 12.31 | BC 473 |
| | | | | Min N | ▷ -210.18 | -0.03 | 0.11 | 0.00 | 0.49 | 0.11 | BC 131 |
| | | | | Max $V_y$ | -86.99 | ▷ 2.63 | 0.18 | 0.00 | 0.78 | -11.44 | BC 403 |
| | | | | Min $V_y$ | -110.80 | ▷ -2.85 | 0.39 | 0.00 | 1.68 | 12.37 | BC 233 |
| | | | | Max $V_z$ | -77.28 | -2.60 | ▷ 0.72 | -0.00 | 3.13 | 11.29 | BC 216 |
| | | | | Min $V_z$ | -53.91 | -1.67 | ▷ -0.60 | -0.00 | -2.60 | 7.27 | BC 390 |
| | | | | Max $M_T$ | -110.62 | -2.84 | 0.47 | ▷ 0.00 | 2.05 | 12.35 | BC 241 |
| | | | | Min $M_T$ | -53.71 | -1.67 | -0.55 | ▷ -0.00 | -2.38 | 7.27 | BC 446 |
| | | | | Max $M_y$ | -77.28 | -2.60 | 0.72 | -0.00 | ▷ 3.13 | 11.29 | BC 216 |
| | | | | Min $M_y$ | -53.91 | -1.67 | -0.60 | -0.00 | ▷ -2.60 | 7.27 | BC 390 |
| | | | | Max $M_z$ | -110.80 | -2.85 | 0.39 | 0.00 | 1.68 | ▷ 12.37 | BC 233 |
| | | | | Min $M_z$ | -86.99 | 2.63 | 0.18 | 0.00 | 0.78 | ▷ -11.44 | BC 403 |
| | | 87 | 4345 | Max N | ▷ -51.10 | -2.83 | 0.47 | 0.00 | 2.04 | 12.31 | BC 473 |
| | | 43 | 0 | Min N | ▷ -215.27 | -0.03 | 0.11 | 0.00 | 0.00 | 0.00 | BC 131 |
| | | 43 | 0 | Max $V_y$ | -90.46 | ▷ 2.63 | 0.18 | 0.00 | 0.00 | 0.00 | BC 403 |
| | | 43 | 0 | Min $V_y$ | -115.89 | ▷ -2.85 | 0.39 | 0.00 | 0.00 | 0.00 | BC 233 |
| | | 43 | 0 | Max $V_z$ | -82.36 | -2.60 | ▷ 0.72 | -0.00 | 0.00 | 0.00 | BC 216 |
| | | 43 | 0 | Min $V_z$ | -57.38 | -1.67 | ▷ -0.60 | -0.00 | 0.00 | 0.00 | BC 390 |
| | | 43 | 0 | Max $M_T$ | -115.71 | -2.84 | 0.47 | ▷ 0.00 | 0.00 | 0.00 | BC 241 |
| | | 43 | 0 | Min $M_T$ | -57.18 | -1.67 | -0.55 | ▷ -0.00 | 0.00 | 0.00 | BC 446 |
| | | 87 | 4345 | Max $M_y$ | -77.28 | -2.60 | 0.72 | -0.00 | ▷ 3.13 | 11.29 | BC 216 |
| | | 87 | 4345 | Min $M_y$ | -53.91 | -1.67 | -0.60 | -0.00 | ▷ -2.60 | 7.27 | BC 390 |
| | | 87 | 4345 | Max $M_z$ | -110.80 | -2.85 | 0.39 | 0.00 | 1.68 | ▷ 12.37 | BC 233 |
| | | 87 | 4345 | Min $M_z$ | -86.99 | 2.63 | 0.18 | 0.00 | 0.78 | ▷ -11.44 | BC 403 |
| 100 | RC1 | 87 | 0 | Max N | ▷ -49.69 | 3.36 | 0.47 | 0.00 | 2.04 | 12.31 | BC 473 |
| | | | | Min N | ▷ -208.12 | 0.03 | 0.11 | 0.00 | 0.49 | 0.11 | BC 131 |
| | | | | Max $V_y$ | -73.47 | ▷ 3.38 | 0.39 | 0.00 | 1.68 | 12.36 | BC 229 |
| | | | | Min $V_y$ | -85.58 | ▷ -3.15 | 0.18 | 0.00 | 0.77 | -11.44 | BC 375 |
| | | | | Max $V_z$ | -75.21 | 3.13 | ▷ 0.72 | -0.00 | 3.13 | 11.29 | BC 216 |
| | | | | Min $V_z$ | -52.50 | 2.02 | ▷ -0.60 | -0.00 | -2.60 | 7.27 | BC 390 |
| | | | | Max $M_T$ | -108.55 | 3.37 | 0.47 | ▷ 0.00 | 2.05 | 12.35 | BC 241 |
| | | | | Min $M_T$ | -52.30 | 2.02 | -0.55 | ▷ -0.00 | -2.38 | 7.27 | BC 446 |
| | | | | Max $M_y$ | -75.21 | 3.13 | 0.72 | -0.00 | ▷ 3.13 | 11.29 | BC 216 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 100 | RC1 | | | Min $M_y$ | -52.50 | 2.02 | -0.60 | -0.00 | ▷ -2.60 | 7.27 | BC 390 |
| | | | | Max $M_z$ | -108.74 | 3.38 | 0.39 | 0.00 | 1.68 | ▷ 12.37 | BC 233 |
| | | | | Min $M_z$ | -85.58 | -3.15 | 0.18 | 0.00 | 0.78 | ▷ -11.44 | BC 403 |
| | | 67 | 3748 | Max N | ▷ -46.70 | 3.36 | 0.47 | 0.00 | 3.80 | -0.30 | BC 473 |
| | | | | Min N | ▷ -203.73 | 0.03 | 0.11 | 0.00 | 0.91 | 0.01 | BC 131 |
| | | | | Max $V_y$ | -69.09 | ▷ 3.38 | 0.39 | 0.00 | 3.13 | -0.31 | BC 229 |
| | | | | Min $V_y$ | -82.59 | ▷ -3.15 | 0.18 | 0.00 | 1.44 | 0.37 | BC 375 |
| | | | | Max $V_z$ | -70.82 | 3.13 | ▷ 0.72 | -0.00 | 5.84 | -0.44 | BC 216 |
| | | | | Min $V_z$ | -49.51 | 2.02 | ▷ -0.60 | -0.00 | -4.83 | -0.28 | BC 390 |
| | | | | Max $M_T$ | -104.17 | 3.37 | 0.47 | ▷ 0.00 | 3.81 | -0.28 | BC 241 |
| | | | | Min $M_T$ | -49.31 | 2.02 | -0.55 | ▷ -0.00 | -4.43 | -0.30 | BC 446 |
| | | | | Max $M_y$ | -70.82 | 3.13 | 0.72 | -0.00 | ▷ 5.84 | -0.44 | BC 216 |
| | | | | Min $M_y$ | -49.51 | 2.02 | -0.60 | -0.00 | ▷ -4.83 | -0.28 | BC 390 |
| | | | | Max $M_z$ | -82.59 | -3.15 | 0.18 | 0.00 | 1.46 | ▷ 0.38 | BC 435 |
| | | | | Min $M_z$ | -70.81 | 3.13 | 0.72 | -0.00 | 5.81 | ▷ -0.44 | BC 276 |
| | | 67 | 3748 | Max N | ▷ -46.70 | 3.36 | 0.47 | 0.00 | 3.80 | -0.30 | BC 473 |
| | | 87 | 0 | Min N | ▷ -208.12 | 0.03 | 0.11 | 0.00 | 0.49 | 0.11 | BC 131 |
| | | 87 | 0 | Max $V_y$ | -73.47 | ▷ 3.38 | 0.39 | 0.00 | 1.68 | 12.36 | BC 229 |
| | | 87 | 0 | Min $V_y$ | -85.58 | ▷ -3.15 | 0.18 | 0.00 | 0.77 | -11.44 | BC 375 |
| | | 87 | 0 | Max $V_z$ | -75.21 | 3.13 | ▷ 0.72 | -0.00 | 3.13 | 11.29 | BC 216 |
| | | 87 | 0 | Min $V_z$ | -52.50 | 2.02 | ▷ -0.60 | -0.00 | -2.60 | 7.27 | BC 390 |
| | | 87 | 0 | Max $M_T$ | -108.55 | 3.37 | 0.47 | ▷ 0.00 | 2.05 | 12.35 | BC 241 |
| | | 87 | 0 | Min $M_T$ | -52.30 | 2.02 | -0.55 | ▷ -0.00 | -2.38 | 7.27 | BC 446 |
| | | 67 | 3748 | Max $M_y$ | -70.82 | 3.13 | 0.72 | -0.00 | ▷ 5.84 | -0.44 | BC 216 |
| | | 67 | 3748 | Min $M_y$ | -49.51 | 2.02 | -0.60 | -0.00 | ▷ -4.83 | -0.28 | BC 390 |
| | | 87 | 0 | Max $M_z$ | -108.74 | 3.38 | 0.39 | 0.00 | 1.68 | ▷ 12.37 | BC 233 |
| | | 87 | 0 | Min $M_z$ | -85.58 | -3.15 | 0.18 | 0.00 | 0.78 | ▷ -11.44 | BC 403 |
| 100 | RC1 | 67 | 3748 | MAX N | ▷ -46.70 | 3.36 | 0.47 | 0.00 | 3.80 | -0.30 | BC 473 |
| 43 | RC1 | 43 | 0 | MIN N | ▷ -215.27 | -0.03 | 0.11 | 0.00 | 0.00 | 0.00 | BC 131 |
| 100 | RC1 | 87 | 0 | MAX $V_y$ | -73.47 | ▷ 3.38 | 0.39 | 0.00 | 1.68 | 12.36 | BC 229 |
| 100 | RC1 | 87 | 0 | MIN $V_y$ | -85.58 | ▷ -3.15 | 0.18 | 0.00 | 0.77 | -11.44 | BC 375 |
| 43 | RC1 | 43 | 0 | MAX $V_z$ | -82.36 | -2.60 | ▷ 0.72 | 0.00 | 0.00 | 0.00 | BC 216 |
| 100 | RC1 | 87 | 0 | MIN $V_z$ | -52.50 | 2.02 | ▷ -0.60 | 0.00 | -2.60 | 7.27 | BC 390 |
| 43 | RC1 | 43 | 0 | MAX $M_T$ | -115.71 | -2.84 | 0.47 | ▷ 0.00 | 0.00 | 0.00 | BC 241 |
| 43 | RC1 | 43 | 0 | MIN $M_T$ | -57.18 | -1.67 | -0.55 | ▷ 0.00 | 0.00 | 0.00 | BC 446 |
| 100 | RC1 | 67 | 3748 | MAX $M_y$ | -70.82 | 3.13 | 0.72 | 0.00 | ▷ 5.84 | -0.44 | BC 216 |
| 100 | RC1 | 67 | 3748 | MIN $M_y$ | -49.51 | 2.02 | -0.60 | 0.00 | ▷ -4.83 | -0.28 | BC 390 |
| 43 | RC1 | 87 | 4345 | MAX $M_z$ | -110.80 | -2.85 | 0.39 | 0.00 | 1.68 | ▷ 12.37 | BC 233 |
| 43 | RC1 | 87 | 4345 | MIN $M_z$ | -86.99 | 2.63 | 0.18 | 0.00 | 0.78 | ▷ -11.44 | BC 403 |
| | **Doorgaande staven No. 21: Doorgaande staven 24** | | | | | | | | | | |
| 44 | RC1 | 66 | 0 | Max N | ▷ 8.59 | -2.58 | -0.38 | 0.00 | 0.00 | 0.00 | BC 444 |
| | | | | Min N | ▷ -203.38 | -0.02 | 1.55 | 0.00 | 0.00 | 0.00 | BC 138 |
| | | | | Max $V_y$ | -75.10 | ▷ 2.68 | 0.63 | 0.00 | 0.00 | -0.00 | BC 431 |
| | | | | Min $V_y$ | -171.72 | ▷ -2.83 | 2.08 | 0.00 | 0.00 | 0.00 | BC 225 |
| | | | | Max $V_z$ | -199.19 | -2.83 | ▷ 2.20 | 0.00 | 0.00 | 0.00 | BC 213 |
| | | | | Min $V_z$ | -6.39 | -2.61 | ▷ -0.50 | 0.00 | 0.00 | 0.00 | BC 388 |
| | | | | Max $M_T$ | -54.44 | 2.64 | 0.26 | ▷ 0.00 | 0.00 | 0.00 | BC 419 |
| | | | | Min $M_T$ | -146.84 | -2.82 | 1.81 | ▷ 0.00 | -0.00 | -0.00 | BC 421 |
| | | | | Max $M_y$ | -72.89 | 0.02 | 0.83 | 0.00 | ▷ 0.00 | 0.00 | BC 38 |
| | | | | Min $M_y$ | -91.29 | -0.03 | 0.71 | 0.00 | ▷ -0.00 | 0.00 | BC 2 |
| | | | | Max $M_z$ | -80.10 | -1.67 | 0.54 | 0.00 | 0.00 | ▷ 0.00 | BC 226 |
| | | | | Min $M_z$ | -69.91 | 2.66 | 0.66 | 0.00 | 0.00 | ▷ -0.00 | BC 191 |
| | | 99 | 2173 | Max N | ▷ 10.32 | -2.58 | -0.38 | 0.00 | -0.82 | 5.60 | BC 444 |
| | | | | Min N | ▷ -200.84 | -0.02 | 1.55 | 0.00 | 3.37 | 0.05 | BC 138 |
| | | | | Max $V_y$ | -73.36 | ▷ 2.68 | 0.63 | 0.00 | 1.37 | -5.81 | BC 431 |
| | | | | Min $V_y$ | -169.18 | ▷ -2.83 | 2.08 | 0.00 | 4.51 | 6.15 | BC 225 |
| | | | | Max $V_z$ | -196.64 | -2.83 | ▷ 2.20 | 0.00 | 4.77 | 6.14 | BC 213 |
| | | | | Min $V_z$ | -4.66 | -2.61 | ▷ -0.50 | 0.00 | -1.10 | 5.68 | BC 388 |
| | | | | Max $M_T$ | -52.71 | 2.64 | 0.26 | ▷ 0.00 | 0.57 | -5.73 | BC 419 |
| | | | | Min $M_T$ | -145.10 | -2.82 | 1.81 | ▷ 0.00 | 3.92 | 6.12 | BC 421 |
| | | | | Max $M_y$ | -196.64 | -2.83 | 2.20 | 0.00 | ▷ 4.77 | 6.14 | BC 213 |
| | | | | Min $M_y$ | -4.66 | -2.61 | -0.50 | 0.00 | ▷ -1.10 | 5.68 | BC 388 |
| | | | | Max $M_z$ | -169.18 | -2.83 | 2.08 | 0.00 | 4.51 | ▷ 6.15 | BC 225 |
| | | | | Min $M_z$ | -73.36 | 2.68 | 0.63 | 0.00 | 1.37 | ▷ -5.81 | BC 431 |
| | | 99 | 2173 | Max N | ▷ 10.32 | -2.58 | -0.38 | 0.00 | -0.82 | 5.60 | BC 444 |
| | | 66 | 0 | Min N | ▷ -203.38 | -0.02 | 1.55 | 0.00 | 0.00 | 0.00 | BC 138 |
| | | 66 | 0 | Max $V_y$ | -75.10 | ▷ 2.68 | 0.63 | 0.00 | 0.00 | -0.00 | BC 431 |
| | | 66 | 0 | Min $V_y$ | -171.72 | ▷ -2.83 | 2.08 | 0.00 | 0.00 | 0.00 | BC 225 |
| | | 66 | 0 | Max $V_z$ | -199.19 | -2.83 | ▷ 2.20 | 0.00 | 0.00 | 0.00 | BC 213 |
| | | 66 | 0 | Min $V_z$ | -6.39 | -2.61 | ▷ -0.50 | 0.00 | 0.00 | 0.00 | BC 388 |
| | | 66 | 0 | Max $M_T$ | -54.44 | 2.64 | 0.26 | ▷ 0.00 | 0.00 | 0.00 | BC 419 |
| | | 66 | 0 | Min $M_T$ | -146.84 | -2.82 | 1.81 | ▷ 0.00 | -0.00 | -0.00 | BC 421 |
| | | 99 | 2173 | Max $M_y$ | -196.64 | -2.83 | 2.20 | 0.00 | ▷ 4.77 | 6.14 | BC 213 |
| | | 99 | 2173 | Min $M_y$ | -4.66 | -2.61 | -0.50 | 0.00 | ▷ -1.10 | 5.68 | BC 388 |
| | | 99 | 2173 | Max $M_z$ | -169.18 | -2.83 | 2.08 | 0.00 | 4.51 | ▷ 6.15 | BC 225 |
| | | 99 | 2173 | Min $M_z$ | -73.36 | 2.68 | 0.63 | 0.00 | 1.37 | ▷ -5.81 | BC 431 |
| 181 | RC1 | 99 | 0 | Max N | ▷ -42.60 | -2.58 | -2.25 | 0.00 | -0.82 | 5.60 | BC 444 |
| | | | | Min N | ▷ -221.45 | -0.02 | -9.55 | 0.00 | 3.37 | 0.05 | BC 138 |
| | | | | Max $V_y$ | -99.11 | ▷ 2.68 | -5.96 | 0.00 | 1.37 | -5.81 | BC 431 |
| | | | | Min $V_y$ | -123.11 | ▷ -2.83 | -12.90 | 0.00 | 4.51 | 6.14 | BC 225 |
| | | | | Max $V_z$ | -44.65 | -2.61 | ▷ 1.62 | 0.00 | -1.06 | 5.67 | BC 360 |
| | | | | Min $V_z$ | -139.28 | -2.79 | ▷ -17.33 | 0.00 | 4.30 | 6.06 | BC 269 |
| | | | | Max $M_T$ | -64.14 | 2.64 | -1.36 | ▷ 0.00 | 0.57 | -5.72 | BC 419 |
| | | | | Min $M_T$ | -99.11 | -2.82 | -10.64 | ▷ 0.00 | 3.92 | 6.12 | BC 421 |
| | | | | Max $M_y$ | -153.76 | -2.83 | -13.81 | 0.00 | ▷ 4.77 | 6.14 | BC 213 |
| | | | | Min $M_y$ | -44.05 | -2.61 | 1.50 | 0.00 | ▷ -1.10 | 5.67 | BC 388 |
| | | | | Max $M_z$ | -123.11 | -2.83 | -12.90 | 0.00 | 4.51 | ▷ 6.14 | BC 225 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 181 | RC1 | | | Min $M_z$ | -99.11 | 2.68 | -5.96 | 0.00 | 1.37 | -5.81 | BC 431 |
| | | 88 | 2173 | Max N | -40.86 | -2.58 | -2.25 | 0.00 | -5.71 | 11.20 | BC 444 |
| | | | | Min N | -218.91 | -0.02 | -9.55 | 0.00 | -17.36 | 0.09 | BC 138 |
| | | | | Max $V_y$ | -97.38 | 2.68 | -5.96 | 0.00 | -11.57 | -11.62 | BC 431 |
| | | | | Min $V_y$ | -120.57 | -2.83 | -12.90 | 0.00 | -23.51 | 12.29 | BC 225 |
| | | | | Max $V_z$ | -42.91 | -2.61 | 1.62 | 0.00 | 2.46 | 11.35 | BC 360 |
| | | | | Min $V_z$ | -136.74 | -2.79 | -17.33 | 0.00 | -33.36 | 12.12 | BC 269 |
| | | | | Max $M_T$ | -62.40 | 2.64 | -1.36 | 0.00 | -2.39 | -11.45 | BC 419 |
| | | | | Min $M_T$ | -97.38 | -2.82 | -10.64 | 0.00 | -19.19 | 12.24 | BC 421 |
| | | | | Max $M_y$ | -42.91 | -2.61 | 1.62 | 0.00 | 2.46 | 11.35 | BC 360 |
| | | | | Min $M_y$ | -136.74 | -2.79 | -17.33 | 0.00 | -33.36 | 12.12 | BC 269 |
| | | | | Max $M_z$ | -120.57 | -2.83 | -12.90 | 0.00 | -23.51 | 12.29 | BC 225 |
| | | | | Min $M_z$ | -97.38 | 2.68 | -5.96 | 0.00 | -11.57 | -11.62 | BC 431 |
| | | 88 | 2173 | Max N | -40.86 | -2.58 | -2.25 | 0.00 | -5.71 | 11.20 | BC 444 |
| | | 99 | 0 | Min N | -221.45 | -0.02 | -9.55 | 0.00 | 3.37 | 0.05 | BC 138 |
| | | 99 | 0 | Max $V_y$ | -99.11 | 2.68 | -5.96 | 0.00 | 1.37 | -5.81 | BC 431 |
| | | 99 | 0 | Min $V_y$ | -123.11 | -2.83 | -12.90 | 0.00 | 4.51 | 6.14 | BC 225 |
| | | 99 | 0 | Max $V_z$ | -44.65 | -2.61 | 1.62 | 0.00 | -1.06 | 5.67 | BC 360 |
| | | 99 | 0 | Min $V_z$ | -139.28 | -2.79 | -17.33 | 0.00 | 4.30 | 6.06 | BC 269 |
| | | 99 | 0 | Max $M_T$ | -64.14 | 2.64 | -1.36 | 0.00 | 0.57 | -5.72 | BC 419 |
| | | 99 | 0 | Min $M_T$ | -99.11 | -2.82 | -10.64 | 0.00 | 3.92 | 6.12 | BC 421 |
| | | 99 | 0 | Max $M_y$ | -153.76 | -2.83 | -13.81 | 0.00 | 4.77 | 6.14 | BC 213 |
| | | 88 | 2173 | Min $M_y$ | -136.74 | -2.79 | -17.33 | 0.00 | -33.36 | 12.12 | BC 269 |
| | | 88 | 2173 | Max $M_z$ | -120.57 | -2.83 | -12.90 | 0.00 | -23.51 | 12.29 | BC 225 |
| | | 88 | 2173 | Min $M_z$ | -97.38 | 2.68 | -5.96 | 0.00 | -11.57 | -11.62 | BC 431 |
| 101 | RC1 | 88 | 0 | Max N | -52.45 | 3.10 | 0.96 | 0.00 | 1.55 | 11.35 | BC 448 |
| | | | | Min N | -219.66 | 0.03 | 4.69 | 0.00 | -17.36 | 0.09 | BC 138 |
| | | | | Max $V_y$ | -131.80 | 3.38 | 6.56 | 0.00 | -25.23 | 12.29 | BC 213 |
| | | | | Min $V_y$ | -63.18 | -3.22 | 0.74 | 0.00 | -10.52 | -11.62 | BC 471 |
| | | | | Max $V_z$ | -131.48 | 3.34 | 8.92 | 0.00 | -33.36 | 12.12 | BC 269 |
| | | | | Min $V_z$ | -62.18 | -3.18 | -1.89 | 0.00 | -1.52 | -11.46 | BC 363 |
| | | | | Max $M_T$ | -62.12 | -3.18 | -1.65 | 0.00 | -2.39 | -11.46 | BC 419 |
| | | | | Min $M_T$ | -69.78 | 3.36 | 4.97 | 0.00 | -19.19 | 12.25 | BC 421 |
| | | | | Max $M_y$ | -52.50 | 3.10 | 0.65 | 0.00 | 2.46 | 11.35 | BC 360 |
| | | | | Min $M_y$ | -131.48 | 3.34 | 8.92 | 0.00 | -33.36 | 12.12 | BC 269 |
| | | | | Max $M_z$ | -96.45 | 3.38 | 6.04 | 0.00 | -23.51 | 12.29 | BC 225 |
| | | | | Min $M_z$ | -98.35 | -3.21 | 1.12 | 0.00 | -11.57 | -11.63 | BC 431 |
| | | 68 | 3748 | Max N | -49.46 | 3.10 | 0.96 | 0.00 | 5.14 | -0.29 | BC 448 |
| | | | | Min N | -215.27 | 0.03 | 4.69 | 0.00 | 0.21 | -0.01 | BC 138 |
| | | | | Max $V_y$ | -127.41 | 3.38 | 6.56 | 0.00 | -0.63 | -0.37 | BC 213 |
| | | | | Min $V_y$ | -60.19 | -3.22 | 0.74 | 0.00 | -7.73 | 0.43 | BC 471 |
| | | | | Max $V_z$ | -127.10 | 3.34 | 8.92 | 0.00 | 0.06 | -0.39 | BC 269 |
| | | | | Min $V_z$ | -59.19 | -3.18 | -1.89 | 0.00 | -8.60 | 0.46 | BC 363 |
| | | | | Max $M_T$ | -59.13 | -3.18 | -1.65 | 0.00 | -8.58 | 0.46 | BC 419 |
| | | | | Min $M_T$ | -66.78 | 3.36 | 4.97 | 0.00 | -0.58 | -0.36 | BC 421 |
| | | | | Max $M_y$ | -109.57 | 3.08 | 4.64 | 0.00 | 6.10 | -0.31 | BC 240 |
| | | | | Min $M_y$ | -59.51 | -3.18 | -1.77 | 0.00 | -8.64 | 0.46 | BC 359 |
| | | | | Max $M_z$ | -58.81 | -3.18 | -1.76 | 0.00 | -8.54 | 0.46 | BC 391 |
| | | | | Min $M_z$ | -101.85 | 3.33 | 7.85 | 0.00 | 0.10 | -0.39 | BC 461 |
| | | 68 | 3748 | Max N | -49.46 | 3.10 | 0.96 | 0.00 | 5.14 | -0.29 | BC 448 |
| | | 88 | 0 | Min N | -219.66 | 0.03 | 4.69 | 0.00 | -17.36 | 0.09 | BC 138 |
| | | 88 | 0 | Max $V_y$ | -131.80 | 3.38 | 6.56 | 0.00 | -25.23 | 12.29 | BC 213 |
| | | 88 | 0 | Min $V_y$ | -63.18 | -3.22 | 0.74 | 0.00 | -10.52 | -11.62 | BC 471 |
| | | 88 | 0 | Max $V_z$ | -131.48 | 3.34 | 8.92 | 0.00 | -33.36 | 12.12 | BC 269 |
| | | 88 | 0 | Min $V_z$ | -62.18 | -3.18 | -1.89 | 0.00 | -1.52 | -11.46 | BC 363 |
| | | 88 | 0 | Max $M_T$ | -62.12 | -3.18 | -1.65 | 0.00 | -2.39 | -11.46 | BC 419 |
| | | 88 | 0 | Min $M_T$ | -69.78 | 3.36 | 4.97 | 0.00 | -19.19 | 12.25 | BC 421 |
| | | 68 | 3748 | Max $M_y$ | -109.57 | 3.08 | 4.64 | 0.00 | 6.10 | -0.31 | BC 240 |
| | | 88 | 0 | Min $M_y$ | -131.48 | 3.34 | 8.92 | 0.00 | -33.36 | 12.12 | BC 269 |
| | | 88 | 0 | Max $M_z$ | -96.45 | 3.38 | 6.04 | 0.00 | -23.51 | 12.29 | BC 225 |
| | | 88 | 0 | Min $M_z$ | -98.35 | -3.21 | 1.12 | 0.00 | -11.57 | -11.63 | BC 431 |
| 44 | RC1 | 99 | 2173 | MAX N | 10.32 | -2.58 | -0.38 | 0.00 | -0.82 | 5.60 | BC 444 |
| 181 | RC1 | 99 | 0 | MIN N | -221.45 | -0.02 | -9.55 | 0.00 | 3.37 | 0.05 | BC 138 |
| 101 | RC1 | 88 | 0 | MAX $V_y$ | -131.80 | 3.38 | 6.56 | 0.00 | -25.23 | 12.29 | BC 213 |
| 101 | RC1 | 88 | 0 | MIN $V_y$ | -63.18 | -3.22 | 0.74 | 0.00 | -10.52 | -11.62 | BC 471 |
| 101 | RC1 | 88 | 0 | MAX $V_z$ | -131.48 | 3.34 | 8.92 | 0.00 | -33.36 | 12.12 | BC 269 |
| 181 | RC1 | 99 | 0 | MIN $V_z$ | -139.28 | -2.79 | -17.33 | 0.00 | 4.30 | 6.06 | BC 269 |
| 44 | RC1 | 66 | 0 | MAX $M_T$ | -54.44 | 2.64 | 0.26 | 0.00 | 0.00 | 0.00 | BC 419 |
| 44 | RC1 | 66 | 0 | MIN $M_T$ | -146.84 | -2.82 | 1.81 | 0.00 | 0.00 | 0.00 | BC 421 |
| 101 | RC1 | 68 | 3748 | MAX $M_y$ | -109.57 | 3.08 | 4.64 | 0.00 | 6.10 | -0.31 | BC 240 |
| 181 | RC1 | 88 | 2173 | MIN $M_y$ | -136.74 | -2.79 | -17.33 | 0.00 | -33.36 | 12.12 | BC 269 |
| 101 | RC1 | 88 | 0 | MAX $M_z$ | -96.45 | 3.38 | 6.04 | 0.00 | -23.51 | 12.29 | BC 225 |
| 101 | RC1 | 88 | 0 | MIN $M_z$ | -98.35 | -3.21 | 1.12 | 0.00 | -11.57 | -11.63 | BC 431 |
| | **Doorgaande staven No. 24: Doorgaande staven 27** | | | | | | | | | | |
| 11 | RC1 | 49 | 0 | Max N | 11.37 | 0.02 | 54.72 | 0.68 | -0.00 | 0.00 | BC 451 |
| | | | | Min N | -53.56 | -0.16 | 115.11 | 0.48 | -0.00 | 0.00 | BC 204 |
| | | | | Max $V_y$ | -3.70 | 0.04 | 53.24 | -0.01 | 0.00 | 0.00 | BC 449 |
| | | | | Min $V_y$ | -52.26 | -0.20 | 213.05 | 0.94 | -0.00 | 0.00 | BC 148 |
| | | | | Max $V_z$ | -50.92 | -0.19 | 213.08 | 0.95 | -0.00 | 0.00 | BC 149 |
| | | | | Min $V_z$ | -5.09 | 0.03 | 53.21 | -0.02 | -0.00 | 0.00 | BC 413 |
| | | | | Max $M_T$ | -50.92 | -0.19 | 213.08 | 0.95 | -0.00 | 0.00 | BC 149 |
| | | | | Min $M_T$ | -12.41 | -0.03 | 53.76 | -0.06 | 0.00 | 0.00 | BC 474 |
| | | | | Max $M_y$ | -15.69 | 0.02 | 88.97 | -0.04 | 0.00 | 0.00 | BC 426 |
| | | | | Min $M_y$ | -52.43 | -0.20 | 213.04 | 0.94 | -0.00 | 0.00 | BC 140 |
| | | | | Max $M_z$ | -20.63 | -0.08 | 89.33 | 0.40 | -0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -45.46 | -0.17 | 184.85 | 0.81 | -0.00 | -0.00 | BC 115 |
| | | 149 | 3201 | Max N | 11.68 | 0.02 | 38.07 | 0.68 | 148.49 | -0.05 | BC 451 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 11 | RC1 | | | Min N | ▷ -52.88 | -0.16 | 79.08 | 0.48 | 310.75 | 0.53 | BC 204 |
| | | | | Max $V_y$ | -3.39 | ▷ 0.04 | 36.59 | -0.01 | 143.76 | -0.12 | BC 449 |
| | | | | Min $V_y$ | -50.98 | ▷ -0.20 | 144.50 | 0.94 | 572.17 | 0.63 | BC 148 |
| | | | | Max $V_z$ | -49.63 | -0.19 | ▷ 144.53 | 0.95 | 572.26 | 0.62 | BC 149 |
| | | | | Min $V_z$ | -4.78 | 0.03 | ▷ 36.56 | -0.02 | 143.66 | -0.11 | BC 413 |
| | | | | Max $M_T$ | -49.63 | -0.19 | 144.53 | ▷ 0.95 | 572.26 | 0.62 | BC 149 |
| | | | | Min $M_T$ | -12.10 | -0.03 | 37.11 | ▷ -0.06 | 145.41 | 0.11 | BC 474 |
| | | | | Max $M_y$ | -49.63 | -0.19 | 144.53 | 0.95 | ▷ 572.26 | 0.62 | BC 149 |
| | | | | Min $M_y$ | -4.78 | 0.03 | 36.56 | -0.02 | ▷ 143.66 | -0.11 | BC 413 |
| | | | | Max $M_z$ | -50.98 | -0.20 | 144.50 | 0.94 | 572.17 | ▷ 0.63 | BC 148 |
| | | | | Min $M_z$ | -3.39 | 0.04 | 36.59 | -0.01 | 143.76 | ▷ -0.12 | BC 449 |
| | | 149 | 3201 | Max N | ▷ 11.68 | 0.02 | 38.07 | 0.68 | 148.49 | -0.05 | BC 451 |
| | | 49 | 0 | Min N | ▷ -53.56 | -0.16 | 115.11 | 0.48 | -0.00 | 0.00 | BC 204 |
| | | 49 | 0 | Max $V_y$ | -3.70 | ▷ 0.04 | 53.24 | -0.01 | 0.00 | 0.00 | BC 449 |
| | | 49 | 0 | Min $V_y$ | -52.26 | ▷ -0.20 | 213.05 | 0.94 | -0.00 | 0.00 | BC 148 |
| | | 49 | 0 | Max $V_z$ | -50.92 | -0.19 | ▷ 213.08 | 0.95 | -0.00 | 0.00 | BC 149 |
| | | 149 | 3201 | Min $V_z$ | -4.78 | 0.03 | ▷ 36.56 | -0.02 | 143.66 | -0.11 | BC 413 |
| | | 49 | 0 | Max $M_T$ | -50.92 | -0.19 | 213.08 | ▷ 0.95 | -0.00 | 0.00 | BC 149 |
| | | 49 | 0 | Min $M_T$ | -12.41 | -0.03 | 53.76 | ▷ -0.06 | 0.00 | 0.00 | BC 474 |
| | | 149 | 3201 | Max $M_y$ | -49.63 | -0.19 | 144.53 | 0.95 | ▷ 572.26 | 0.62 | BC 149 |
| | | 49 | 0 | Min $M_y$ | -52.43 | -0.20 | 213.04 | 0.94 | ▷ -0.00 | 0.00 | BC 140 |
| | | 149 | 3201 | Max $M_z$ | -50.98 | -0.20 | 144.50 | 0.94 | 572.17 | ▷ 0.63 | BC 148 |
| | | 149 | 3201 | Min $M_z$ | -3.39 | 0.04 | 36.59 | -0.01 | 143.76 | ▷ -0.12 | BC 449 |
| 187 | RC1 | 149 | 0 | Max N | ▷ 11.74 | -0.42 | 36.96 | 0.55 | 148.23 | -0.05 | BC 451 |
| | | | | Min N | ▷ -52.70 | -0.81 | 77.45 | 0.29 | 310.21 | 0.53 | BC 204 |
| | | | | Max $V_y$ | -4.61 | ▷ 0.59 | 35.50 | 0.14 | 143.41 | -0.11 | BC 473 |
| | | | | Min $V_y$ | -49.32 | ▷ -1.24 | 142.90 | 0.64 | 571.31 | 0.62 | BC 149 |
| | | | | Max $V_z$ | -49.32 | -1.24 | ▷ 142.90 | 0.64 | 571.31 | 0.62 | BC 149 |
| | | | | Min $V_z$ | -4.72 | 0.59 | ▷ 35.50 | 0.14 | 143.41 | -0.11 | BC 413 |
| | | | | Max $M_T$ | -49.64 | -1.23 | 142.89 | ▷ 0.64 | 571.29 | 0.62 | BC 141 |
| | | | | Min $M_T$ | -10.58 | -0.60 | 36.03 | ▷ -0.23 | 145.26 | 0.04 | BC 450 |
| | | | | Max $M_y$ | -49.32 | -1.24 | 142.90 | 0.64 | ▷ 571.31 | 0.62 | BC 149 |
| | | | | Min $M_y$ | -4.72 | 0.59 | 35.50 | 0.14 | ▷ 143.41 | -0.11 | BC 413 |
| | | | | Max $M_z$ | -50.67 | -1.23 | 142.88 | 0.64 | 571.21 | ▷ 0.63 | BC 148 |
| | | | | Min $M_z$ | -3.33 | 0.58 | 35.53 | 0.15 | 143.52 | ▷ -0.12 | BC 449 |
| | | 81 | 3201 | Max N | ▷ 12.06 | -0.42 | 20.32 | 0.55 | 239.90 | 1.31 | BC 451 |
| | | | | Min N | ▷ -52.03 | -0.81 | 41.42 | 0.29 | 500.43 | 3.11 | BC 204 |
| | | | | Max $V_y$ | -4.30 | ▷ 0.59 | 18.86 | 0.14 | 230.40 | -2.01 | BC 473 |
| | | | | Min $V_y$ | -48.03 | ▷ -1.24 | 74.35 | 0.64 | 918.97 | 4.58 | BC 149 |
| | | | | Max $V_z$ | -48.03 | -1.24 | ▷ 74.35 | 0.64 | 918.97 | 4.58 | BC 149 |
| | | | | Min $V_z$ | -4.40 | 0.59 | ▷ 18.86 | 0.14 | 230.40 | -2.01 | BC 413 |
| | | | | Max $M_T$ | -48.36 | -1.23 | 74.34 | ▷ 0.64 | 918.91 | 4.55 | BC 141 |
| | | | | Min $M_T$ | -10.27 | -0.60 | 19.39 | ▷ -0.23 | 233.95 | 1.95 | BC 450 |
| | | | | Max $M_y$ | -48.03 | -1.24 | 74.35 | 0.64 | ▷ 918.97 | 4.58 | BC 149 |
| | | | | Min $M_y$ | -4.40 | 0.59 | 18.86 | 0.14 | ▷ 230.40 | -2.01 | BC 413 |
| | | | | Max $M_z$ | -48.03 | -1.24 | 74.35 | 0.64 | 918.97 | ▷ 4.58 | BC 149 |
| | | | | Min $M_z$ | -4.13 | 0.59 | 18.86 | 0.14 | 230.42 | ▷ -2.01 | BC 445 |
| | | 81 | 3201 | Max N | ▷ 12.06 | -0.42 | 20.32 | 0.55 | 239.90 | 1.31 | BC 451 |
| | | 149 | 0 | Min N | ▷ -52.70 | -0.81 | 77.45 | 0.29 | 310.21 | 0.53 | BC 204 |
| | | 149 | 0 | Max $V_y$ | -4.61 | ▷ 0.59 | 35.50 | 0.14 | 143.41 | -0.11 | BC 473 |
| | | 149 | 0 | Min $V_y$ | -49.32 | ▷ -1.24 | 142.90 | 0.64 | 571.31 | 0.62 | BC 149 |
| | | 149 | 0 | Max $V_z$ | -49.32 | -1.24 | ▷ 142.90 | 0.64 | 571.31 | 0.62 | BC 149 |
| | | 81 | 3201 | Min $V_z$ | -4.40 | 0.59 | ▷ 18.86 | 0.14 | 230.40 | -2.01 | BC 413 |
| | | 149 | 0 | Max $M_T$ | -49.64 | -1.23 | 142.89 | ▷ 0.64 | 571.29 | 0.62 | BC 141 |
| | | 149 | 0 | Min $M_T$ | -10.58 | -0.60 | 36.03 | ▷ -0.23 | 145.26 | 0.04 | BC 450 |
| | | 81 | 3201 | Max $M_y$ | -48.03 | -1.24 | 74.35 | 0.64 | ▷ 918.97 | 4.58 | BC 149 |
| | | 149 | 0 | Min $M_y$ | -4.72 | 0.59 | 35.50 | 0.14 | ▷ 143.41 | -0.11 | BC 413 |
| | | 81 | 3201 | Max $M_z$ | -48.03 | -1.24 | 74.35 | 0.64 | 918.97 | ▷ 4.58 | BC 149 |
| | | 81 | 3201 | Min $M_z$ | -4.13 | 0.59 | 18.86 | 0.14 | 230.42 | ▷ -2.01 | BC 445 |
| 193 | RC1 | 155 | 0 | Max N | ▷ 48.66 | 0.49 | -2.88 | 0.08 | 560.97 | -0.82 | BC 235 |
| | | | | Min N | ▷ -20.31 | 0.32 | -1.93 | -0.13 | 268.70 | -0.83 | BC 408 |
| | | | | Max $V_y$ | -0.39 | ▷ 1.14 | -2.53 | 0.24 | 1028.26 | -0.84 | BC 149 |
| | | | | Min $V_y$ | -15.07 | ▷ -0.76 | -0.50 | -0.01 | 262.31 | -0.46 | BC 473 |
| | | | | Max $V_z$ | -15.12 | -0.76 | ▷ -0.50 | -0.01 | 262.29 | -0.46 | BC 413 |
| | | | | Min $V_z$ | 48.66 | 0.49 | ▷ -2.88 | 0.08 | 560.97 | -0.82 | BC 235 |
| | | | | Max $M_T$ | -0.39 | 1.14 | -2.53 | ▷ 0.24 | 1028.26 | -0.84 | BC 149 |
| | | | | Min $M_T$ | -20.10 | 0.32 | -1.92 | ▷ -0.13 | 268.61 | -0.84 | BC 412 |
| | | | | Max $M_y$ | -0.39 | 1.14 | -2.53 | 0.24 | ▷ 1028.26 | -0.84 | BC 149 |
| | | | | Min $M_y$ | -15.07 | -0.75 | -0.50 | -0.01 | ▷ 262.27 | -0.47 | BC 409 |
| | | | | Max $M_z$ | -16.94 | 0.71 | -1.66 | 0.19 | 558.44 | ▷ 0.74 | BC 242 |
| | | | | Min $M_z$ | -17.87 | 0.60 | -2.70 | -0.06 | 560.60 | ▷ -1.13 | BC 184 |
| | | 81 | 3256 | Max N | ▷ 47.96 | 0.49 | -39.53 | 0.08 | 491.95 | -2.40 | BC 235 |
| | | | | Min N | ▷ -20.70 | 0.48 | -30.86 | -0.09 | 383.83 | -2.57 | BC 396 |
| | | | | Max $V_y$ | -1.71 | ▷ 1.14 | -72.26 | 0.24 | 906.53 | -4.56 | BC 149 |
| | | | | Min $V_y$ | -15.39 | ▷ -0.76 | -17.43 | -0.01 | 233.12 | 2.00 | BC 473 |
| | | | | Max $V_z$ | -15.44 | -0.76 | ▷ -17.43 | -0.01 | 233.11 | 2.00 | BC 413 |
| | | | | Min $V_z$ | -1.71 | 1.14 | ▷ -72.26 | 0.24 | 906.53 | -4.56 | BC 149 |
| | | | | Max $M_T$ | -1.71 | 1.14 | -72.26 | ▷ 0.24 | 906.53 | -4.56 | BC 149 |
| | | | | Min $M_T$ | -20.42 | 0.32 | -18.86 | ▷ -0.13 | 234.78 | -1.89 | BC 412 |
| | | | | Max $M_y$ | -1.80 | 1.14 | -72.25 | 0.24 | ▷ 906.54 | -4.54 | BC 146 |
| | | | | Min $M_y$ | -1.71 | 0.30 | -18.10 | 0.06 | ▷ 231.80 | -1.15 | BC 41 |
| | | | | Max $M_z$ | -15.23 | -0.76 | -17.43 | -0.01 | 233.15 | ▷ 2.00 | BC 445 |
| | | | | Min $M_z$ | -1.71 | 1.14 | -72.26 | 0.24 | 906.53 | ▷ -4.56 | BC 149 |
| | | 155 | 0 | Max N | ▷ 48.66 | 0.49 | -2.88 | 0.08 | 560.97 | -0.82 | BC 235 |
| | | 81 | 3256 | Min N | ▷ -20.70 | 0.48 | -30.86 | -0.09 | 383.83 | -2.57 | BC 396 |
| | | 155 | 0 | Max $V_y$ | -0.39 | ▷ 1.14 | -2.53 | 0.24 | 1028.26 | -0.84 | BC 149 |
| | | 155 | 0 | Min $V_y$ | -15.07 | ▷ -0.76 | -0.50 | -0.01 | 262.31 | -0.46 | BC 473 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 193 | RC1 | 155 | 0 | Max $V_z$ | -15.12 | -0.76 | ▷ -0.50 | -0.01 | 262.29 | -0.46 | BC 413 |
| | | 81 | 3256 | Min $V_z$ | -1.71 | 1.14 | ▷ -72.26 | 0.24 | 906.53 | -4.56 | BC 149 |
| | | 155 | 0 | Max $M_T$ | -0.39 | 1.14 | -2.53 | ▷ 0.24 | 1028.26 | -0.84 | BC 149 |
| | | 155 | 0 | Min $M_T$ | -20.10 | 0.32 | -1.92 | ▷ -0.13 | 268.61 | -0.84 | BC 412 |
| | | 155 | 0 | Max $M_y$ | -0.39 | 1.14 | -2.53 | 0.24 | ▷ 1028.26 | -0.84 | BC 149 |
| | | 81 | 3256 | Min $M_y$ | -1.71 | 0.30 | -18.10 | 0.06 | ▷ 231.80 | -1.15 | BC 41 |
| | | 81 | 3256 | Max $M_z$ | -15.23 | -0.76 | -17.43 | -0.01 | 233.15 | ▷ 2.00 | BC 445 |
| | | 81 | 3256 | Min $M_z$ | -1.71 | 1.14 | -72.26 | 0.24 | 906.53 | ▷ -4.56 | BC 149 |
| 83 | RC1 | 85 | 0 | Max N | ▷ 49.36 | -1.13 | 36.35 | -0.40 | 502.29 | -4.51 | BC 235 |
| | | | | Min N | ▷ -19.96 | 0.71 | 16.77 | -0.01 | 241.68 | 1.48 | BC 408 |
| | | | | Max $V_y$ | -19.96 | ▷ 0.71 | 16.77 | -0.01 | 241.68 | 1.48 | BC 408 |
| | | | | Min $V_y$ | 0.41 | ▷ -1.83 | 69.78 | -0.64 | 914.51 | -6.81 | BC 138 |
| | | | | Max $V_z$ | -0.97 | -1.81 | ▷ 69.80 | -0.63 | 914.26 | -6.73 | BC 139 |
| | | | | Min $V_z$ | 41.10 | -0.72 | ▷ 16.73 | -0.25 | 239.54 | -3.17 | BC 363 |
| | | | | Max $M_T$ | -14.70 | -0.54 | 18.19 | ▷ 0.05 | 230.60 | -2.22 | BC 469 |
| | | | | Min $M_T$ | 0.41 | -1.83 | 69.78 | ▷ -0.64 | 914.51 | -6.81 | BC 138 |
| | | | | Max $M_y$ | 0.94 | -1.82 | 69.77 | -0.64 | ▷ 914.61 | -6.78 | BC 149 |
| | | | | Min $M_y$ | -14.76 | -0.54 | 18.19 | 0.05 | ▷ 230.58 | -2.22 | BC 409 |
| | | | | Max $M_z$ | -19.96 | 0.71 | 16.77 | -0.01 | 241.68 | ▷ 1.48 | BC 408 |
| | | | | Min $M_z$ | 0.41 | -1.83 | 69.78 | -0.64 | 914.51 | ▷ -6.81 | BC 138 |
| | | 155 | 3256 | Max N | ▷ 48.66 | -1.13 | -0.30 | -0.40 | 560.96 | -0.82 | BC 235 |
| | | | | Min N | ▷ -20.28 | 0.71 | -0.17 | -0.01 | 268.70 | -0.83 | BC 408 |
| | | | | Max $V_y$ | -20.28 | ▷ 0.71 | -0.17 | -0.01 | 268.70 | -0.83 | BC 408 |
| | | | | Min $V_y$ | -0.91 | ▷ -1.83 | 0.06 | -0.64 | 1028.19 | -0.84 | BC 138 |
| | | | | Max $V_z$ | -14.87 | -0.75 | ▷ 1.52 | -0.03 | 385.12 | -0.60 | BC 221 |
| | | | | Min $V_z$ | 45.40 | -0.95 | ▷ -0.50 | -0.34 | 436.89 | -0.84 | BC 427 |
| | | | | Max $M_T$ | -15.02 | -0.54 | 1.26 | ▷ 0.05 | 262.27 | -0.47 | BC 469 |
| | | | | Min $M_T$ | -0.91 | -1.83 | 0.06 | ▷ -0.64 | 1028.19 | -0.84 | BC 138 |
| | | | | Max $M_y$ | -0.38 | -1.82 | 0.04 | -0.64 | ▷ 1028.25 | -0.84 | BC 149 |
| | | | | Min $M_y$ | -15.08 | -0.54 | 1.26 | 0.05 | ▷ 262.25 | -0.47 | BC 409 |
| | | | | Max $M_z$ | -16.93 | -0.57 | 0.90 | -0.19 | 558.43 | ▷ 0.74 | BC 242 |
| | | | | Min $M_z$ | -17.84 | 0.13 | -0.12 | -0.20 | 560.60 | ▷ -1.13 | BC 184 |
| | | 85 | 0 | Max N | ▷ 49.36 | -1.13 | 36.35 | -0.40 | 502.29 | -4.51 | BC 235 |
| | | 155 | 3256 | Min N | ▷ -20.28 | 0.71 | -0.17 | -0.01 | 268.70 | -0.83 | BC 408 |
| | | 85 | 0 | Max $V_y$ | -19.96 | ▷ 0.71 | 16.77 | -0.01 | 241.68 | 1.48 | BC 408 |
| | | 85 | 0 | Min $V_y$ | 0.41 | ▷ -1.83 | 69.78 | -0.64 | 914.51 | -6.81 | BC 138 |
| | | 85 | 0 | Max $V_z$ | -0.97 | -1.81 | ▷ 69.80 | -0.63 | 914.26 | -6.73 | BC 139 |
| | | 155 | 3256 | Min $V_z$ | 45.40 | -0.95 | ▷ -0.50 | -0.34 | 436.89 | -0.84 | BC 427 |
| | | 85 | 0 | Max $M_T$ | -14.70 | -0.54 | 18.19 | ▷ 0.05 | 230.60 | -2.22 | BC 469 |
| | | 85 | 0 | Min $M_T$ | 0.41 | -1.83 | 69.78 | ▷ -0.64 | 914.51 | -6.81 | BC 138 |
| | | 155 | 3256 | Max $M_y$ | -0.38 | -1.82 | 0.04 | -0.64 | ▷ 1028.25 | -0.84 | BC 149 |
| | | 85 | 0 | Min $M_y$ | -14.76 | -0.54 | 18.19 | 0.05 | ▷ 230.58 | -2.22 | BC 409 |
| | | 85 | 0 | Max $M_z$ | -19.96 | 0.71 | 16.77 | -0.01 | 241.68 | ▷ 1.48 | BC 408 |
| | | 85 | 0 | Min $M_z$ | 0.41 | -1.83 | 69.78 | -0.64 | 914.51 | ▷ -6.81 | BC 138 |
| 200 | RC1 | 162 | 0 | Max N | ▷ 8.78 | 0.85 | 37.41 | -0.36 | 153.35 | -0.47 | BC 451 |
| | | | | Min N | ▷ -56.80 | 1.75 | 141.47 | -0.35 | 580.81 | -1.06 | BC 139 |
| | | | | Max $V_y$ | -56.04 | ▷ 1.77 | 141.53 | -0.35 | 581.02 | -1.07 | BC 138 |
| | | | | Min $V_y$ | -9.27 | ▷ -0.48 | 36.06 | -0.16 | 148.91 | -0.08 | BC 408 |
| | | | | Max $V_z$ | -55.53 | 1.76 | ▷ 141.54 | -0.35 | 581.07 | -1.05 | BC 149 |
| | | | | Min $V_z$ | -12.65 | 0.46 | ▷ 35.42 | 0.21 | 146.86 | 0.24 | BC 410 |
| | | | | Max $M_T$ | -12.65 | 0.46 | 35.42 | ▷ 0.21 | 146.86 | 0.24 | BC 410 |
| | | | | Min $M_T$ | 6.90 | 1.17 | 77.82 | ▷ -0.39 | 319.10 | -0.70 | BC 247 |
| | | | | Max $M_y$ | -55.53 | 1.76 | 141.54 | -0.35 | ▷ 581.07 | -1.05 | BC 149 |
| | | | | Min $M_y$ | -12.65 | 0.46 | 35.42 | 0.21 | ▷ 146.86 | 0.24 | BC 410 |
| | | | | Max $M_z$ | -21.05 | 0.45 | 75.34 | 0.20 | 311.02 | ▷ 0.37 | BC 242 |
| | | | | Min $M_z$ | -56.04 | 1.77 | 141.53 | -0.35 | 581.02 | ▷ -1.07 | BC 138 |
| | | 85 | 3267 | Max N | ▷ 9.42 | 0.85 | 20.43 | -0.36 | 247.86 | -3.27 | BC 451 |
| | | | | Min N | ▷ -54.20 | 1.75 | 71.56 | -0.35 | 928.81 | -6.77 | BC 139 |
| | | | | Max $V_y$ | -53.44 | ▷ 1.77 | 71.62 | -0.35 | 929.22 | -6.85 | BC 138 |
| | | | | Min $V_y$ | -8.64 | ▷ -0.48 | 19.08 | -0.16 | 238.98 | 1.47 | BC 408 |
| | | | | Max $V_z$ | -52.93 | 1.76 | ▷ 71.63 | -0.35 | 929.32 | -6.82 | BC 149 |
| | | | | Min $V_z$ | -12.02 | 0.46 | ▷ 18.44 | 0.21 | 234.85 | -1.25 | BC 410 |
| | | | | Max $M_T$ | -12.02 | 0.46 | 18.44 | ▷ 0.21 | 234.85 | -1.25 | BC 410 |
| | | | | Min $M_T$ | 8.27 | 1.17 | 41.07 | ▷ -0.39 | 513.33 | -4.53 | BC 247 |
| | | | | Max $M_y$ | -52.93 | 1.76 | 71.63 | -0.35 | ▷ 929.32 | -6.82 | BC 149 |
| | | | | Min $M_y$ | -12.02 | 0.46 | 18.44 | 0.21 | ▷ 234.85 | -1.25 | BC 410 |
| | | | | Max $M_z$ | -8.64 | -0.48 | 19.08 | -0.16 | 238.98 | ▷ 1.47 | BC 408 |
| | | | | Min $M_z$ | -53.44 | 1.77 | 71.62 | -0.35 | 929.22 | ▷ -6.85 | BC 138 |
| | | 85 | 3267 | Max N | ▷ 9.42 | 0.85 | 20.43 | -0.36 | 247.86 | -3.27 | BC 451 |
| | | 162 | 0 | Min N | ▷ -56.80 | 1.75 | 141.47 | -0.35 | 580.81 | -1.06 | BC 139 |
| | | 162 | 0 | Max $V_y$ | -56.04 | ▷ 1.77 | 141.53 | -0.35 | 581.02 | -1.07 | BC 138 |
| | | 162 | 0 | Min $V_y$ | -9.27 | ▷ -0.48 | 36.06 | -0.16 | 148.91 | -0.08 | BC 408 |
| | | 162 | 0 | Max $V_z$ | -55.53 | 1.76 | ▷ 141.54 | -0.35 | 581.07 | -1.05 | BC 149 |
| | | 85 | 3267 | Min $V_z$ | -12.02 | 0.46 | ▷ 18.44 | 0.21 | 234.85 | -1.25 | BC 410 |
| | | 162 | 0 | Max $M_T$ | -12.65 | 0.46 | 35.42 | ▷ 0.21 | 146.86 | 0.24 | BC 410 |
| | | 162 | 0 | Min $M_T$ | 6.90 | 1.17 | 77.82 | ▷ -0.39 | 319.10 | -0.70 | BC 247 |
| | | 85 | 3267 | Max $M_y$ | -52.93 | 1.76 | 71.63 | -0.35 | ▷ 929.32 | -6.82 | BC 149 |
| | | 162 | 0 | Min $M_y$ | -12.65 | 0.46 | 35.42 | 0.21 | ▷ 146.86 | 0.24 | BC 410 |
| | | 85 | 3267 | Max $M_z$ | -8.64 | -0.48 | 19.08 | -0.16 | 238.98 | ▷ 1.47 | BC 408 |
| | | 85 | 3267 | Min $M_z$ | -53.44 | 1.77 | 71.62 | -0.35 | 929.22 | ▷ -6.85 | BC 138 |
| 12 | RC1 | 37 | 0 | Max N | ▷ 8.09 | 0.14 | 55.51 | -0.57 | 0.00 | 0.00 | BC 451 |
| | | | | Min N | ▷ -59.73 | 0.32 | 213.01 | -0.77 | -0.00 | 0.00 | BC 139 |
| | | | | Max $V_y$ | -58.96 | ▷ 0.33 | 213.08 | -0.77 | -0.00 | 0.00 | BC 138 |
| | | | | Min $V_y$ | -22.56 | ▷ -0.11 | 113.72 | 0.03 | 0.00 | 0.00 | BC 242 |
| | | | | Max $V_z$ | -58.46 | 0.32 | ▷ 213.09 | -0.78 | -0.00 | 0.00 | BC 149 |
| | | | | Min $V_z$ | -13.34 | -0.07 | ▷ 53.51 | 0.05 | -0.00 | 0.00 | BC 410 |
| | | | | Max $M_T$ | -13.34 | -0.07 | 53.51 | ▷ 0.05 | -0.00 | 0.00 | BC 410 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 12 | RC1 | | | Min $M_T$ | -58.46 | 0.32 | 213.09 | ▷ -0.78 | -0.00 | 0.00 | BC 149 |
| | | | | Max $M_y$ | -15.93 | -0.09 | 78.64 | 0.04 | ▷ 0.00 | 0.00 | BC 162 |
| | | | | Min $M_y$ | -59.44 | 0.33 | 213.02 | -0.77 | ▷ -0.00 | 0.00 | BC 133 |
| | | | | Max $M_z$ | -15.93 | -0.09 | 78.64 | 0.04 | 0.00 | ▷ 0.00 | BC 162 |
| | | | | Min $M_z$ | -37.93 | 0.09 | 53.76 | -0.15 | 0.00 | ▷ -0.00 | BC 381 |
| | | 162 | 3267 | Max N | ▷ 8.72 | 0.14 | 38.53 | -0.57 | 153.61 | -0.47 | BC 451 |
| | | | | Min N | ▷ -57.13 | 0.32 | 143.10 | -0.77 | 581.76 | -1.06 | BC 139 |
| | | | | Max $V_y$ | -56.36 | ▷ 0.33 | 143.17 | -0.77 | 581.96 | -1.07 | BC 138 |
| | | | | Min $V_y$ | -21.19 | ▷ -0.11 | 76.98 | 0.03 | 311.53 | 0.37 | BC 242 |
| | | | | Max $V_z$ | -55.86 | 0.32 | ▷ 143.18 | -0.78 | 582.02 | -1.05 | BC 149 |
| | | | | Min $V_z$ | -12.71 | -0.07 | ▷ 36.53 | 0.05 | 147.10 | 0.24 | BC 410 |
| | | | | Max $M_T$ | -12.71 | -0.07 | 36.53 | ▷ 0.05 | 147.10 | 0.24 | BC 410 |
| | | | | Min $M_T$ | -55.86 | 0.32 | 143.18 | ▷ -0.78 | 582.02 | -1.05 | BC 149 |
| | | | | Max $M_y$ | -55.86 | 0.32 | 143.18 | -0.78 | ▷ 582.02 | -1.05 | BC 149 |
| | | | | Min $M_y$ | -12.71 | -0.07 | 36.53 | 0.05 | ▷ 147.10 | 0.24 | BC 410 |
| | | | | Max $M_z$ | -21.19 | -0.11 | 76.98 | 0.03 | 311.53 | ▷ 0.37 | BC 242 |
| | | | | Min $M_z$ | -56.36 | 0.33 | 143.17 | -0.77 | 581.96 | ▷ -1.07 | BC 138 |
| | | 162 | 3267 | Max N | ▷ 8.72 | 0.14 | 38.53 | -0.57 | 153.61 | -0.47 | BC 451 |
| | | 37 | 0 | Min N | ▷ -59.73 | 0.32 | 213.01 | -0.77 | -0.00 | 0.00 | BC 139 |
| | | 37 | 0 | Max $V_y$ | -58.96 | ▷ 0.33 | 213.08 | -0.77 | -0.00 | 0.00 | BC 138 |
| | | 37 | 0 | Min $V_y$ | -22.56 | ▷ -0.11 | 113.72 | 0.03 | 0.00 | 0.00 | BC 242 |
| | | 37 | 0 | Max $V_z$ | -58.46 | 0.32 | ▷ 213.09 | -0.78 | -0.00 | 0.00 | BC 149 |
| | | 162 | 3267 | Min $V_z$ | -12.71 | -0.07 | ▷ 36.53 | 0.05 | 147.10 | 0.24 | BC 410 |
| | | 37 | 0 | Max $M_T$ | -13.34 | -0.07 | 53.51 | ▷ 0.05 | -0.00 | 0.00 | BC 410 |
| | | 37 | 0 | Min $M_T$ | -58.46 | 0.32 | 213.09 | ▷ -0.78 | -0.00 | 0.00 | BC 149 |
| | | 162 | 3267 | Max $M_y$ | -55.86 | 0.32 | 143.18 | -0.78 | ▷ 582.02 | -1.05 | BC 149 |
| | | 37 | 0 | Min $M_y$ | -59.44 | 0.33 | 213.02 | -0.77 | ▷ -0.00 | 0.00 | BC 133 |
| | | 162 | 3267 | Max $M_z$ | -21.19 | -0.11 | 76.98 | 0.03 | 311.53 | ▷ 0.37 | BC 242 |
| | | 162 | 3267 | Min $M_z$ | -56.36 | 0.33 | 143.17 | -0.77 | 581.96 | ▷ -1.07 | BC 138 |
| 83 | RC1 | 85 | 0 | MAX N | ▷ 49.36 | -1.13 | 36.35 | -0.40 | 502.29 | -4.51 | BC 235 |
| 12 | RC1 | 37 | 0 | MIN N | ▷ -59.73 | 0.32 | 213.01 | -0.77 | 0.00 | 0.00 | BC 139 |
| 200 | RC1 | 162 | 0 | MAX $V_y$ | -56.04 | ▷ 1.77 | 141.53 | -0.35 | 581.02 | -1.07 | BC 138 |
| 83 | RC1 | 85 | 0 | MIN $V_y$ | 0.41 | ▷ -1.83 | 69.78 | -0.64 | 914.51 | -6.81 | BC 138 |
| 12 | RC1 | 37 | 0 | MAX $V_z$ | -58.46 | 0.32 | ▷ 213.09 | -0.78 | 0.00 | 0.00 | BC 149 |
| 193 | RC1 | 81 | 3256 | MIN $V_z$ | -1.71 | 1.14 | ▷ -72.26 | 0.24 | 906.53 | -4.56 | BC 149 |
| 11 | RC1 | 49 | 0 | MAX $M_T$ | -50.92 | -0.19 | 213.08 | ▷ 0.95 | 0.00 | 0.00 | BC 149 |
| 12 | RC1 | 37 | 0 | MIN $M_T$ | -58.46 | 0.32 | 213.09 | ▷ -0.78 | 0.00 | 0.00 | BC 149 |
| 193 | RC1 | 155 | 0 | MAX $M_y$ | -0.39 | 1.14 | -2.53 | 0.24 | ▷ 1028.26 | -0.84 | BC 149 |
| 11 | RC1 | 49 | 0 | MIN $M_y$ | -52.43 | -0.20 | 213.04 | 0.94 | ▷ 0.00 | 0.00 | BC 140 |
| 187 | RC1 | 81 | 3201 | MAX $M_z$ | -48.03 | -1.24 | 74.35 | 0.64 | 918.97 | ▷ 4.58 | BC 149 |
| 200 | RC1 | 85 | 3267 | MIN $M_z$ | -53.44 | 1.77 | 71.62 | -0.35 | 929.22 | ▷ -6.85 | BC 138 |
| | **Doorgaande staven No. 25: Doorgaande staven 25** | | | | | | | | | | |
| 52 | RC1 | 80 | 0 | Max N | ▷ 8.19 | -0.00 | -0.25 | 0.01 | 0.00 | 0.00 | BC 359 |
| | | | | Min N | ▷ -38.02 | 0.00 | -0.72 | -0.01 | -0.00 | 0.00 | BC 241 |
| | | | | Max $V_y$ | -26.72 | ▷ 0.00 | -0.31 | -0.01 | 0.00 | 0.00 | BC 377 |
| | | | | Min $V_y$ | -4.16 | ▷ -0.00 | -0.72 | 0.01 | 0.00 | 0.00 | BC 267 |
| | | | | Max $V_z$ | 8.19 | -0.00 | ▷ -0.25 | 0.01 | 0.00 | 0.00 | BC 359 |
| | | | | Min $V_z$ | -18.35 | -0.00 | ▷ -0.91 | 0.00 | 0.00 | 0.00 | BC 155 |
| | | | | Max $M_T$ | -4.16 | -0.00 | -0.72 | ▷ 0.01 | 0.00 | 0.00 | BC 267 |
| | | | | Min $M_T$ | -25.98 | 0.00 | -0.27 | ▷ -0.01 | 0.00 | 0.00 | BC 389 |
| | | | | Max $M_y$ | -5.34 | 0.00 | -0.52 | -0.00 | ▷ 0.00 | 0.00 | BC 258 |
| | | | | Min $M_y$ | -9.34 | -0.00 | -0.62 | 0.00 | ▷ -0.00 | 0.00 | BC 114 |
| | | | | Max $M_z$ | -8.59 | -0.00 | -0.54 | 0.00 | -0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | -8.59 | -0.00 | -0.54 | 0.00 | -0.00 | ▷ 0.00 | BC 1 |
| | | 89 | 1665 | Max N | ▷ 8.19 | -0.00 | -0.78 | 0.01 | -0.86 | 0.00 | BC 359 |
| | | | | Min N | ▷ -38.02 | 0.00 | -1.50 | -0.01 | -1.85 | -0.00 | BC 241 |
| | | | | Max $V_y$ | -26.72 | ▷ 0.00 | -0.85 | -0.01 | -0.97 | -0.00 | BC 377 |
| | | | | Min $V_y$ | -4.16 | ▷ -0.00 | -1.50 | 0.01 | -1.85 | 0.00 | BC 267 |
| | | | | Max $V_z$ | 8.19 | -0.00 | ▷ -0.78 | 0.01 | -0.86 | 0.00 | BC 359 |
| | | | | Min $V_z$ | -17.66 | -0.00 | ▷ -1.72 | 0.00 | -2.13 | 0.00 | BC 21 |
| | | | | Max $M_T$ | -4.16 | -0.00 | -1.50 | ▷ 0.01 | -1.85 | 0.00 | BC 267 |
| | | | | Min $M_T$ | -25.98 | 0.00 | -0.81 | ▷ -0.01 | -0.90 | -0.00 | BC 389 |
| | | | | Max $M_y$ | 8.19 | -0.00 | -0.78 | 0.01 | ▷ -0.86 | 0.00 | BC 359 |
| | | | | Min $M_y$ | -18.35 | -0.00 | -1.69 | 0.00 | ▷ -2.16 | 0.00 | BC 155 |
| | | | | Max $M_z$ | -4.16 | -0.00 | -1.50 | 0.01 | -1.85 | ▷ 0.00 | BC 267 |
| | | | | Min $M_z$ | -26.72 | 0.00 | -0.85 | -0.01 | -0.97 | ▷ -0.00 | BC 377 |
| | | 80 | 0 | Max N | ▷ 8.19 | -0.00 | -0.25 | 0.01 | 0.00 | 0.00 | BC 359 |
| | | 80 | 0 | Min N | ▷ -38.02 | 0.00 | -0.72 | -0.01 | -0.00 | 0.00 | BC 241 |
| | | 80 | 0 | Max $V_y$ | -26.72 | ▷ 0.00 | -0.31 | -0.01 | 0.00 | 0.00 | BC 377 |
| | | 80 | 0 | Min $V_y$ | -4.16 | ▷ -0.00 | -0.72 | 0.01 | 0.00 | 0.00 | BC 267 |
| | | 80 | 0 | Max $V_z$ | 8.19 | -0.00 | ▷ -0.25 | 0.01 | 0.00 | 0.00 | BC 359 |
| | | 89 | 1665 | Min $V_z$ | -17.66 | -0.00 | ▷ -1.72 | 0.00 | -2.13 | 0.00 | BC 21 |
| | | 80 | 0 | Max $M_T$ | -4.16 | -0.00 | -0.72 | ▷ 0.01 | 0.00 | 0.00 | BC 267 |
| | | 80 | 0 | Min $M_T$ | -25.98 | 0.00 | -0.27 | ▷ -0.01 | 0.00 | 0.00 | BC 389 |
| | | 80 | 0 | Max $M_y$ | -5.34 | 0.00 | -0.52 | -0.00 | ▷ 0.00 | 0.00 | BC 258 |
| | | 89 | 1665 | Min $M_y$ | -18.35 | -0.00 | -1.69 | 0.00 | ▷ -2.16 | 0.00 | BC 155 |
| | | 89 | 1665 | Max $M_z$ | -4.16 | -0.00 | -1.50 | 0.01 | -1.85 | ▷ 0.00 | BC 267 |
| | | 89 | 1665 | Min $M_z$ | -26.72 | 0.00 | -0.85 | -0.01 | -0.97 | ▷ -0.00 | BC 377 |
| 74 | RC1 | 89 | 0 | Max N | ▷ 10.64 | 0.00 | 0.98 | -0.00 | -0.97 | 0.00 | BC 359 |
| | | | | Min N | ▷ -39.11 | -0.00 | 1.78 | 0.00 | -3.13 | -0.00 | BC 241 |
| | | | | Max $V_y$ | 8.73 | ▷ 0.00 | 1.47 | -0.00 | -1.59 | 0.00 | BC 203 |
| | | | | Min $V_y$ | -36.71 | ▷ -0.00 | 1.31 | 0.00 | -2.57 | -0.00 | BC 429 |
| | | | | Max $V_z$ | -15.02 | 0.00 | ▷ 1.81 | -0.00 | -2.56 | 0.00 | BC 21 |
| | | | | Min $V_z$ | 5.07 | -0.00 | ▷ 0.83 | 0.00 | -0.25 | -0.00 | BC 360 |
| | | | | Max $M_T$ | -27.15 | -0.00 | 1.18 | ▷ 0.00 | -1.97 | -0.00 | BC 393 |
| | | | | Min $M_T$ | 2.36 | 0.00 | 1.09 | ▷ -0.00 | -1.53 | 0.00 | BC 475 |
| | | | | Max $M_y$ | 5.07 | -0.00 | 0.83 | 0.00 | ▷ -0.25 | -0.00 | BC 360 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 74 | RC1 | | | Min $M_y$ | -39.11 | -0.00 | 1.78 | 0.00 | ▷ -3.13 | -0.00 | BC 241 |
| | | | | Max $M_z$ | 8.73 | 0.00 | 1.47 | -0.00 | -1.59 | ▷ 0.00 | BC 203 |
| | | | | Min $M_z$ | -36.71 | -0.00 | 1.31 | 0.00 | -2.57 | ▷ -0.00 | BC 429 |
| | | 17 | 4865 | Max N | ▷ 10.64 | 0.00 | -0.58 | -0.00 | 0.00 | 0.00 | BC 359 |
| | | | | Min N | ▷ -39.11 | -0.00 | -0.50 | 0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Max $V_y$ | 8.73 | ▷ 0.00 | -0.82 | -0.00 | 0.00 | 0.00 | BC 203 |
| | | | | Min $V_y$ | -36.71 | ▷ -0.00 | -0.25 | 0.00 | 0.00 | 0.00 | BC 429 |
| | | | | Max $V_z$ | -36.99 | -0.00 | ▷ -0.25 | 0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min $V_z$ | 5.14 | -0.00 | ▷ -0.98 | 0.00 | 0.00 | 0.00 | BC 168 |
| | | | | Max $M_T$ | -27.15 | -0.00 | -0.37 | ▷ 0.00 | 0.00 | 0.00 | BC 393 |
| | | | | Min $M_T$ | 2.36 | 0.00 | -0.46 | ▷ -0.00 | 0.00 | 0.00 | BC 475 |
| | | | | Max $M_y$ | -8.07 | -0.00 | -0.69 | 0.00 | ▷ 0.00 | 0.00 | BC 190 |
| | | | | Min $M_y$ | -12.54 | -0.00 | -0.41 | -0.00 | ▷ -0.00 | 0.00 | BC 53 |
| | | | | Max $M_z$ | -5.93 | 0.00 | -0.89 | -0.00 | -0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | -5.93 | 0.00 | -0.89 | -0.00 | -0.00 | ▷ 0.00 | BC 1 |
| | | 89 | 0 | Max N | ▷ 10.64 | 0.00 | 0.98 | -0.00 | -0.97 | 0.00 | BC 359 |
| | | 89 | 0 | Min N | ▷ -39.11 | -0.00 | 1.78 | 0.00 | -3.13 | -0.00 | BC 241 |
| | | 89 | 0 | Max $V_y$ | 8.73 | ▷ 0.00 | 1.47 | -0.00 | -1.59 | 0.00 | BC 203 |
| | | 89 | 0 | Min $V_y$ | -36.71 | ▷ -0.00 | 1.31 | 0.00 | -2.57 | -0.00 | BC 429 |
| | | 89 | 0 | Max $V_z$ | -15.02 | 0.00 | ▷ 1.81 | -0.00 | -2.56 | 0.00 | BC 21 |
| | | 17 | 4865 | Min $V_z$ | 5.14 | -0.00 | ▷ -0.98 | 0.00 | 0.00 | 0.00 | BC 168 |
| | | 89 | 0 | Max $M_T$ | -27.15 | -0.00 | 1.18 | ▷ 0.00 | -1.97 | -0.00 | BC 393 |
| | | 89 | 0 | Min $M_T$ | 2.36 | 0.00 | 1.09 | ▷ -0.00 | -1.53 | 0.00 | BC 475 |
| | | | 2724 | Max $M_y$ | 5.14 | -0.00 | 0.02 | 0.00 | ▷ 1.03 | -0.00 | BC 168 |
| | | 89 | 0 | Min $M_y$ | -39.11 | -0.00 | 1.78 | 0.00 | ▷ -3.13 | -0.00 | BC 241 |
| | | 89 | 0 | Max $M_z$ | 8.73 | 0.00 | 1.47 | -0.00 | -1.59 | ▷ 0.00 | BC 203 |
| | | 89 | 0 | Min $M_z$ | -36.71 | -0.00 | 1.31 | 0.00 | -2.57 | ▷ -0.00 | BC 429 |
| 74 | RC1 | 89 | 0 | MAX N | ▷ 10.64 | 0.00 | 0.98 | 0.00 | -0.97 | 0.00 | BC 359 |
| 74 | RC1 | 89 | 0 | MIN N | ▷ -39.11 | 0.00 | 1.78 | 0.00 | -3.13 | 0.00 | BC 241 |
| 52 | RC1 | 80 | 0 | MAX $V_y$ | -26.72 | ▷ 0.00 | -0.31 | -0.01 | 0.00 | 0.00 | BC 377 |
| 52 | RC1 | 80 | 0 | MIN $V_y$ | -4.16 | ▷ 0.00 | -0.72 | 0.01 | 0.00 | 0.00 | BC 267 |
| 74 | RC1 | 89 | 0 | MAX $V_z$ | -15.02 | 0.00 | ▷ 1.81 | 0.00 | -2.56 | 0.00 | BC 21 |
| 52 | RC1 | 89 | 1665 | MIN $V_z$ | -17.66 | 0.00 | ▷ -1.72 | 0.00 | -2.13 | 0.00 | BC 21 |
| 52 | RC1 | 80 | 0 | MAX $M_T$ | -4.16 | 0.00 | -0.72 | ▷ 0.01 | 0.00 | 0.00 | BC 267 |
| 52 | RC1 | 80 | 0 | MIN $M_T$ | -25.98 | 0.00 | -0.27 | ▷ -0.01 | 0.00 | 0.00 | BC 389 |
| 74 | RC1 | | 2724 | MAX $M_y$ | 5.14 | 0.00 | 0.02 | 0.00 | ▷ 1.03 | 0.00 | BC 168 |
| 74 | RC1 | 89 | 0 | MIN $M_y$ | -39.11 | 0.00 | 1.78 | 0.00 | ▷ -3.13 | 0.00 | BC 241 |
| 52 | RC1 | 89 | 1665 | MAX $M_z$ | -4.16 | 0.00 | -1.50 | 0.01 | -1.85 | ▷ 0.00 | BC 267 |
| 52 | RC1 | 89 | 1665 | MIN $M_z$ | -26.72 | 0.00 | -0.85 | -0.01 | -0.97 | ▷ 0.00 | BC 377 |
| | **Doorgaande staven No. 28: Doorgaande staven 28** | | | | | | | | | | |
| 144 | RC1 | 90 | 0 | Max N | ▷ 28.01 | 0.13 | 0.00 | -0.00 | 0.00 | 0.00 | BC 389 |
| | | | | Min N | ▷ -80.69 | -0.08 | 0.00 | -0.00 | 0.00 | 0.00 | BC 264 |
| | | | | Max $V_y$ | 22.54 | ▷ 0.17 | 0.00 | -0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min $V_y$ | -70.53 | ▷ -0.11 | 0.00 | -0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Max $V_z$ | 27.55 | 0.13 | ▷ 0.00 | -0.00 | 0.00 | 0.00 | BC 377 |
| | | | | Min $V_z$ | -15.83 | 0.04 | ▷ -0.00 | 0.00 | 0.00 | 0.00 | BC 267 |
| | | | | Max $M_T$ | -12.58 | 0.03 | -0.00 | ▷ 0.00 | 0.00 | 0.00 | BC 443 |
| | | | | Min $M_T$ | 24.15 | 0.14 | 0.00 | ▷ -0.00 | 0.00 | 0.00 | BC 185 |
| | | | | Max $M_y$ | -12.06 | 0.04 | -0.00 | -0.00 | ▷ 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -12.06 | 0.04 | -0.00 | -0.00 | ▷ 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -11.56 | 0.06 | -0.00 | 0.00 | 0.00 | ▷ 0.00 | BC 91 |
| | | | | Min $M_z$ | -7.89 | 0.05 | -0.00 | 0.00 | 0.00 | ▷ -0.00 | BC 53 |
| | | 91 | 2173 | Max N | ▷ 28.70 | 0.13 | 0.00 | -0.00 | 0.00 | -0.27 | BC 389 |
| | | | | Min N | ▷ -79.67 | -0.08 | 0.00 | -0.00 | 0.00 | 0.18 | BC 264 |
| | | | | Max $V_y$ | 23.56 | ▷ 0.17 | 0.00 | -0.00 | 0.00 | -0.37 | BC 241 |
| | | | | Min $V_y$ | -69.84 | ▷ -0.11 | 0.00 | -0.00 | 0.00 | 0.24 | BC 360 |
| | | | | Max $V_z$ | 28.25 | 0.13 | ▷ 0.00 | -0.00 | 0.00 | -0.28 | BC 377 |
| | | | | Min $V_z$ | -14.81 | 0.04 | ▷ -0.00 | 0.00 | -0.00 | -0.09 | BC 267 |
| | | | | Max $M_T$ | -11.88 | 0.03 | -0.00 | ▷ 0.00 | -0.00 | -0.06 | BC 443 |
| | | | | Min $M_T$ | 25.17 | 0.14 | 0.00 | ▷ -0.00 | 0.00 | -0.31 | BC 185 |
| | | | | Max $M_y$ | 28.25 | 0.13 | 0.00 | -0.00 | ▷ 0.00 | -0.28 | BC 377 |
| | | | | Min $M_y$ | -14.81 | 0.04 | -0.00 | 0.00 | ▷ -0.00 | -0.09 | BC 267 |
| | | | | Max $M_z$ | -69.84 | -0.11 | 0.00 | -0.00 | 0.00 | ▷ 0.24 | BC 360 |
| | | | | Min $M_z$ | 23.56 | 0.17 | 0.00 | -0.00 | 0.00 | ▷ -0.37 | BC 241 |
| | | 91 | 2173 | Max N | ▷ 28.70 | 0.13 | 0.00 | -0.00 | 0.00 | -0.27 | BC 389 |
| | | 90 | 0 | Min N | ▷ -80.69 | -0.08 | 0.00 | -0.00 | 0.00 | 0.00 | BC 264 |
| | | 90 | 0 | Max $V_y$ | 22.54 | ▷ 0.17 | 0.00 | -0.00 | 0.00 | 0.00 | BC 241 |
| | | 90 | 0 | Min $V_y$ | -70.53 | ▷ -0.11 | 0.00 | -0.00 | 0.00 | 0.00 | BC 360 |
| | | 90 | 0 | Max $V_z$ | 27.55 | 0.13 | ▷ 0.00 | -0.00 | 0.00 | 0.00 | BC 377 |
| | | 90 | 0 | Min $V_z$ | -15.83 | 0.04 | ▷ -0.00 | 0.00 | 0.00 | 0.00 | BC 267 |
| | | 90 | 0 | Max $M_T$ | -12.58 | 0.03 | -0.00 | ▷ 0.00 | 0.00 | 0.00 | BC 443 |
| | | 90 | 0 | Min $M_T$ | 24.15 | 0.14 | 0.00 | ▷ -0.00 | 0.00 | 0.00 | BC 185 |
| | | 91 | 2173 | Max $M_y$ | 28.25 | 0.13 | 0.00 | -0.00 | ▷ 0.00 | -0.28 | BC 377 |
| | | 91 | 2173 | Min $M_y$ | -14.81 | 0.04 | -0.00 | 0.00 | ▷ -0.00 | -0.09 | BC 267 |
| | | 91 | 2173 | Max $M_z$ | -69.84 | -0.11 | 0.00 | -0.00 | 0.00 | ▷ 0.24 | BC 360 |
| | | 91 | 2173 | Min $M_z$ | 23.56 | 0.17 | 0.00 | -0.00 | 0.00 | ▷ -0.37 | BC 241 |
| 180 | RC1 | 91 | 0 | Max N | ▷ -2.42 | -0.59 | 0.00 | -0.00 | 0.01 | -0.27 | BC 389 |
| | | | | Min N | ▷ -43.41 | 0.32 | 0.00 | -0.00 | 0.01 | 0.18 | BC 264 |
| | | | | Max $V_y$ | -38.82 | ▷ 0.43 | 0.00 | -0.00 | 0.01 | 0.24 | BC 392 |
| | | | | Min $V_y$ | -4.12 | ▷ -0.76 | 0.00 | -0.00 | 0.01 | -0.37 | BC 241 |
| | | | | Max $V_z$ | -2.47 | -0.60 | ▷ 0.00 | -0.00 | 0.01 | -0.28 | BC 377 |
| | | | | Min $V_z$ | -10.55 | -0.18 | ▷ -0.00 | 0.00 | -0.01 | -0.09 | BC 267 |
| | | | | Max $M_T$ | -7.90 | -0.13 | -0.00 | ▷ 0.00 | -0.01 | -0.06 | BC 443 |
| | | | | Min $M_T$ | -3.74 | -0.66 | 0.00 | ▷ -0.00 | 0.01 | -0.31 | BC 185 |
| | | | | Max $M_y$ | -2.85 | -0.70 | 0.00 | -0.00 | ▷ 0.01 | -0.34 | BC 433 |
| | | | | Min $M_y$ | -8.29 | -0.12 | -0.00 | 0.00 | ▷ -0.01 | -0.05 | BC 287 |
| | | | | Max $M_z$ | -38.21 | 0.43 | 0.00 | -0.00 | 0.01 | ▷ 0.24 | BC 360 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 180 | RC1 | | | Min $M_z$ | -4.12 | -0.76 | 0.00 | -0.00 | 0.01 | ▷ -0.37 | BC 241 |
| | | 89 | 2173 | Max N | ▷ -1.73 | -0.59 | 0.00 | -0.00 | 0.01 | 1.00 | BC 389 |
| | | | | Min N | ▷ -42.39 | 0.32 | 0.00 | -0.00 | 0.01 | -0.52 | BC 264 |
| | | | | Max $V_y$ | -38.12 | ▷ 0.43 | 0.00 | -0.00 | 0.01 | -0.70 | BC 392 |
| | | | | Min $V_y$ | -3.10 | ▷ -0.76 | 0.00 | -0.00 | 0.01 | 1.28 | BC 241 |
| | | | | Max $V_z$ | -1.78 | -0.60 | ▷ 0.00 | -0.00 | 0.01 | 1.02 | BC 377 |
| | | | | Min $V_z$ | -9.53 | -0.18 | ▷ -0.00 | 0.00 | -0.01 | 0.30 | BC 267 |
| | | | | Max $M_T$ | -7.21 | -0.13 | -0.00 | ▷ 0.00 | -0.01 | 0.21 | BC 443 |
| | | | | Min $M_T$ | -2.72 | -0.66 | 0.00 | ▷ -0.00 | 0.01 | 1.13 | BC 185 |
| | | | | Max $M_y$ | -1.78 | -0.60 | 0.00 | -0.00 | ▷ 0.01 | 1.02 | BC 377 |
| | | | | Min $M_y$ | -9.53 | -0.18 | -0.00 | 0.00 | ▷ -0.01 | 0.30 | BC 267 |
| | | | | Max $M_z$ | -3.10 | -0.76 | 0.00 | -0.00 | 0.01 | ▷ 1.28 | BC 241 |
| | | | | Min $M_z$ | -38.12 | 0.43 | 0.00 | -0.00 | 0.01 | ▷ -0.70 | BC 392 |
| | | 89 | 2173 | Max N | ▷ -1.73 | -0.59 | 0.00 | -0.00 | 0.01 | 1.00 | BC 389 |
| | | 91 | 0 | Min N | ▷ -43.41 | 0.32 | 0.00 | -0.00 | 0.01 | 0.18 | BC 264 |
| | | 91 | 0 | Max $V_y$ | -38.82 | ▷ 0.43 | 0.00 | -0.00 | 0.01 | 0.24 | BC 392 |
| | | 91 | 0 | Min $V_y$ | -4.12 | ▷ -0.76 | 0.00 | -0.00 | 0.01 | -0.37 | BC 241 |
| | | 91 | 0 | Max $V_z$ | -2.47 | -0.60 | ▷ 0.00 | -0.00 | 0.01 | -0.28 | BC 377 |
| | | 91 | 0 | Min $V_z$ | -10.55 | -0.18 | ▷ -0.00 | 0.00 | -0.01 | -0.09 | BC 267 |
| | | 91 | 0 | Max $M_T$ | -7.90 | -0.13 | -0.00 | ▷ 0.00 | -0.01 | -0.06 | BC 443 |
| | | 91 | 0 | Min $M_T$ | -3.74 | -0.66 | 0.00 | ▷ -0.00 | 0.01 | -0.31 | BC 185 |
| | | 89 | 2173 | Max $M_y$ | -1.78 | -0.60 | 0.00 | -0.00 | ▷ 0.01 | 1.02 | BC 377 |
| | | 89 | 2173 | Min $M_y$ | -9.53 | -0.18 | -0.00 | 0.00 | ▷ -0.01 | 0.30 | BC 267 |
| | | 89 | 2173 | Max $M_z$ | -3.10 | -0.76 | 0.00 | -0.00 | 0.01 | ▷ 1.28 | BC 241 |
| | | 89 | 2173 | Min $M_z$ | -38.12 | 0.43 | 0.00 | -0.00 | 0.01 | ▷ -0.70 | BC 392 |
| 144 | RC1 | 91 | 2173 | MAX N | ▷ 28.70 | 0.13 | 0.00 | 0.00 | 0.00 | -0.27 | BC 389 |
| 144 | RC1 | 90 | 0 | MIN N | ▷ -80.69 | -0.08 | 0.00 | 0.00 | 0.00 | 0.00 | BC 264 |
| 180 | RC1 | 91 | 0 | MAX $V_y$ | -38.82 | ▷ 0.43 | 0.00 | 0.00 | 0.01 | 0.24 | BC 392 |
| 180 | RC1 | 91 | 0 | MIN $V_y$ | -4.12 | ▷ -0.76 | 0.00 | 0.00 | 0.01 | -0.37 | BC 241 |
| 180 | RC1 | 91 | 0 | MAX $V_z$ | -2.47 | -0.60 | ▷ 0.00 | 0.00 | 0.01 | -0.28 | BC 377 |
| 144 | RC1 | 90 | 0 | MIN $V_z$ | -15.83 | 0.04 | ▷ 0.00 | 0.00 | 0.00 | 0.00 | BC 267 |
| 144 | RC1 | 90 | 0 | MAX $M_T$ | -12.58 | 0.03 | 0.00 | ▷ 0.00 | 0.00 | 0.00 | BC 443 |
| 144 | RC1 | 90 | 0 | MIN $M_T$ | 24.15 | 0.14 | 0.00 | ▷ 0.00 | 0.00 | 0.00 | BC 185 |
| 180 | RC1 | 89 | 2173 | MAX $M_y$ | -1.78 | -0.60 | 0.00 | 0.00 | ▷ 0.01 | 1.02 | BC 377 |
| 180 | RC1 | 89 | 2173 | MIN $M_y$ | -9.53 | -0.18 | 0.00 | 0.00 | ▷ -0.01 | 0.30 | BC 267 |
| 180 | RC1 | 89 | 2173 | MAX $M_z$ | -3.10 | -0.76 | 0.00 | 0.00 | 0.01 | ▷ 1.28 | BC 241 |
| 180 | RC1 | 89 | 2173 | MIN $M_z$ | -38.12 | 0.43 | 0.00 | 0.00 | 0.01 | ▷ -0.70 | BC 392 |
| | **Doorgaande staven No. 29: Doorgaande staven 29** | | | | | | | | | | |
| 160 | RC1 | 94 | 0 | Max N | ▷ 29.20 | -0.13 | 0.00 | -0.00 | 0.00 | 0.00 | BC 360 |
| | | | | Min N | ▷ -90.94 | 0.12 | 0.00 | -0.00 | 0.00 | 0.00 | BC 269 |
| | | | | Max $V_y$ | -87.48 | ▷ 0.13 | 0.00 | -0.00 | 0.00 | 0.00 | BC 433 |
| | | | | Min $V_y$ | 19.98 | ▷ -0.15 | 0.00 | -0.00 | 0.00 | 0.00 | BC 276 |
| | | | | Max $V_z$ | -73.30 | 0.12 | ▷ 0.00 | -0.00 | 0.00 | 0.00 | BC 377 |
| | | | | Min $V_z$ | -18.50 | -0.02 | ▷ -0.00 | 0.00 | 0.00 | 0.00 | BC 279 |
| | | | | Max $M_T$ | -8.23 | -0.02 | -0.00 | ▷ 0.00 | 0.00 | 0.00 | BC 167 |
| | | | | Min $M_T$ | -90.92 | 0.12 | 0.00 | ▷ -0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Max $M_y$ | -8.11 | -0.03 | -0.00 | -0.00 | ▷ 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -8.11 | -0.03 | -0.00 | -0.00 | ▷ 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -13.60 | -0.04 | 0.00 | -0.00 | 0.00 | ▷ 0.00 | BC 190 |
| | | | | Min $M_z$ | -82.00 | 0.12 | 0.00 | -0.00 | 0.00 | ▷ -0.00 | BC 381 |
| | | 95 | 2173 | Max N | ▷ 29.90 | -0.13 | 0.00 | -0.00 | 0.01 | 0.28 | BC 360 |
| | | | | Min N | ▷ -89.92 | 0.12 | 0.00 | -0.00 | 0.01 | -0.26 | BC 269 |
| | | | | Max $V_y$ | -86.78 | ▷ 0.13 | 0.00 | -0.00 | 0.01 | -0.28 | BC 433 |
| | | | | Min $V_y$ | 21.00 | ▷ -0.15 | 0.00 | -0.00 | 0.01 | 0.32 | BC 276 |
| | | | | Max $V_z$ | -72.61 | 0.12 | ▷ 0.00 | -0.00 | 0.01 | -0.26 | BC 377 |
| | | | | Min $V_z$ | -17.48 | -0.02 | ▷ -0.00 | 0.00 | -0.01 | 0.05 | BC 279 |
| | | | | Max $M_T$ | -7.21 | -0.02 | -0.00 | ▷ 0.00 | -0.01 | 0.04 | BC 167 |
| | | | | Min $M_T$ | -89.90 | 0.12 | 0.00 | ▷ -0.00 | 0.01 | -0.26 | BC 241 |
| | | | | Max $M_y$ | -72.61 | 0.12 | 0.00 | -0.00 | ▷ 0.01 | -0.26 | BC 377 |
| | | | | Min $M_y$ | -17.48 | -0.02 | -0.00 | 0.00 | ▷ -0.01 | 0.05 | BC 279 |
| | | | | Max $M_z$ | 21.00 | -0.15 | 0.00 | -0.00 | 0.01 | ▷ 0.32 | BC 276 |
| | | | | Min $M_z$ | -86.78 | 0.13 | 0.00 | -0.00 | 0.01 | ▷ -0.28 | BC 433 |
| | | 95 | 2173 | Max N | ▷ 29.90 | -0.13 | 0.00 | -0.00 | 0.01 | 0.28 | BC 360 |
| | | 94 | 0 | Min N | ▷ -90.94 | 0.12 | 0.00 | -0.00 | 0.00 | 0.00 | BC 269 |
| | | 94 | 0 | Max $V_y$ | -87.48 | ▷ 0.13 | 0.00 | -0.00 | 0.00 | 0.00 | BC 433 |
| | | 94 | 0 | Min $V_y$ | 19.98 | ▷ -0.15 | 0.00 | -0.00 | 0.00 | 0.00 | BC 276 |
| | | 94 | 0 | Max $V_z$ | -73.30 | 0.12 | ▷ 0.00 | -0.00 | 0.00 | 0.00 | BC 377 |
| | | 94 | 0 | Min $V_z$ | -18.50 | -0.02 | ▷ -0.00 | 0.00 | 0.00 | 0.00 | BC 279 |
| | | 94 | 0 | Max $M_T$ | -8.23 | -0.02 | -0.00 | ▷ 0.00 | 0.00 | 0.00 | BC 167 |
| | | 94 | 0 | Min $M_T$ | -90.92 | 0.12 | 0.00 | ▷ -0.00 | 0.00 | 0.00 | BC 241 |
| | | 95 | 2173 | Max $M_y$ | -72.61 | 0.12 | 0.00 | -0.00 | ▷ 0.01 | -0.26 | BC 377 |
| | | 95 | 2173 | Min $M_y$ | -17.48 | -0.02 | -0.00 | 0.00 | ▷ -0.01 | 0.05 | BC 279 |
| | | 95 | 2173 | Max $M_z$ | 21.00 | -0.15 | 0.00 | -0.00 | 0.01 | ▷ 0.32 | BC 276 |
| | | 95 | 2173 | Min $M_z$ | -86.78 | 0.13 | 0.00 | -0.00 | 0.01 | ▷ -0.28 | BC 433 |
| 179 | RC1 | 95 | 0 | Max N | ▷ -2.31 | 0.59 | 0.00 | -0.00 | 0.01 | 0.28 | BC 356 |
| | | | | Min N | ▷ -47.93 | -0.52 | 0.00 | -0.00 | 0.01 | -0.26 | BC 241 |
| | | | | Max $V_y$ | -3.48 | ▷ 0.64 | 0.00 | -0.00 | 0.01 | 0.31 | BC 168 |
| | | | | Min $V_y$ | -45.69 | ▷ -0.55 | 0.00 | -0.00 | 0.01 | -0.28 | BC 433 |
| | | | | Max $V_z$ | -39.28 | -0.50 | ▷ 0.00 | -0.00 | 0.01 | -0.26 | BC 377 |
| | | | | Min $V_z$ | -11.01 | 0.07 | ▷ -0.00 | 0.00 | -0.01 | 0.05 | BC 279 |
| | | | | Max $M_T$ | -6.25 | 0.09 | -0.00 | ▷ 0.00 | -0.01 | 0.04 | BC 167 |
| | | | | Min $M_T$ | -47.93 | -0.52 | 0.00 | ▷ -0.00 | 0.01 | -0.26 | BC 241 |
| | | | | Max $M_y$ | -44.51 | -0.54 | 0.00 | -0.00 | ▷ 0.01 | -0.27 | BC 397 |
| | | | | Min $M_y$ | -8.34 | 0.07 | -0.00 | 0.00 | ▷ -0.01 | 0.03 | BC 247 |
| | | | | Max $M_z$ | -3.66 | 0.63 | 0.00 | -0.00 | 0.01 | ▷ 0.32 | BC 276 |
| | | | | Min $M_z$ | -45.69 | -0.55 | 0.00 | -0.00 | 0.01 | ▷ -0.28 | BC 433 |
| | | 93 | 2173 | Max N | ▷ -1.61 | 0.59 | 0.00 | -0.00 | 0.01 | -1.00 | BC 356 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 179 | RC1 | | | Min N | ▷ -46.91 | -0.52 | 0.00 | -0.00 | 0.02 | 0.87 | BC 241 |
| | | | | Max $V_y$ | -2.46 | ▷ 0.64 | 0.00 | -0.00 | 0.01 | -1.08 | BC 168 |
| | | | | Min $V_y$ | -44.99 | ▷ -0.55 | 0.00 | -0.00 | 0.02 | 0.92 | BC 433 |
| | | | | Max $V_z$ | -38.59 | -0.50 | ▷ 0.00 | -0.00 | 0.02 | 0.82 | BC 377 |
| | | | | Min $V_z$ | -9.99 | 0.07 | ▷ -0.00 | 0.00 | -0.01 | -0.10 | BC 279 |
| | | | | Max $M_T$ | -5.23 | 0.09 | -0.00 | ▷ 0.00 | -0.01 | -0.15 | BC 167 |
| | | | | Min $M_T$ | -46.91 | -0.52 | 0.00 | ▷ -0.00 | 0.02 | 0.87 | BC 241 |
| | | | | Max $M_y$ | -44.23 | -0.54 | 0.00 | -0.00 | ▷ 0.02 | 0.91 | BC 401 |
| | | | | Min $M_y$ | -11.80 | 0.04 | -0.00 | 0.00 | ▷ -0.01 | -0.05 | BC 239 |
| | | | | Max $M_z$ | -44.99 | -0.55 | 0.00 | -0.00 | 0.02 | ▷ 0.92 | BC 433 |
| | | | | Min $M_z$ | -2.46 | 0.64 | 0.00 | -0.00 | 0.01 | ▷ -1.08 | BC 168 |
| | | 93 | 2173 | Max N | ▷ -1.61 | 0.59 | 0.00 | -0.00 | 0.01 | -1.00 | BC 356 |
| | | 95 | 0 | Min N | ▷ -47.93 | -0.52 | 0.00 | -0.00 | 0.01 | -0.26 | BC 241 |
| | | 95 | 0 | Max $V_y$ | -3.48 | ▷ 0.64 | 0.00 | -0.00 | 0.01 | 0.31 | BC 168 |
| | | 95 | 0 | Min $V_y$ | -45.69 | ▷ -0.55 | 0.00 | -0.00 | 0.01 | -0.28 | BC 433 |
| | | 95 | 0 | Max $V_z$ | -39.28 | -0.50 | ▷ 0.00 | -0.00 | 0.01 | -0.26 | BC 377 |
| | | 95 | 0 | Min $V_z$ | -11.01 | 0.07 | ▷ -0.00 | 0.00 | -0.01 | 0.05 | BC 279 |
| | | 95 | 0 | Max $M_T$ | -6.25 | 0.09 | -0.00 | ▷ 0.00 | -0.01 | 0.04 | BC 167 |
| | | 95 | 0 | Min $M_T$ | -47.93 | -0.52 | 0.00 | ▷ -0.00 | 0.01 | -0.26 | BC 241 |
| | | 93 | 2173 | Max $M_y$ | -44.23 | -0.54 | 0.00 | -0.00 | ▷ 0.02 | 0.91 | BC 401 |
| | | 93 | 2173 | Min $M_y$ | -11.80 | 0.04 | -0.00 | 0.00 | ▷ -0.01 | -0.05 | BC 239 |
| | | 93 | 2173 | Max $M_z$ | -44.99 | -0.55 | 0.00 | -0.00 | 0.02 | ▷ 0.92 | BC 433 |
| | | 93 | 2173 | Min $M_z$ | -2.46 | 0.64 | 0.00 | -0.00 | 0.01 | ▷ -1.08 | BC 168 |
| 160 | RC1 | 95 | 2173 | MAX N | ▷ 29.90 | -0.13 | 0.00 | 0.00 | 0.01 | 0.28 | BC 360 |
| 160 | RC1 | 94 | 0 | MIN N | ▷ -90.94 | 0.12 | 0.00 | 0.00 | 0.00 | 0.00 | BC 269 |
| 179 | RC1 | 95 | 0 | MAX $V_y$ | -3.48 | ▷ 0.64 | 0.00 | 0.00 | 0.01 | 0.31 | BC 168 |
| 179 | RC1 | 95 | 0 | MIN $V_y$ | -45.69 | ▷ -0.55 | 0.00 | 0.00 | 0.01 | -0.28 | BC 433 |
| 179 | RC1 | 95 | 0 | MAX $V_z$ | -39.28 | -0.50 | ▷ 0.00 | 0.00 | 0.01 | -0.26 | BC 377 |
| 179 | RC1 | 95 | 0 | MIN $V_z$ | -11.01 | 0.07 | ▷ 0.00 | 0.00 | -0.01 | 0.05 | BC 279 |
| 160 | RC1 | 94 | 0 | MAX $M_T$ | -8.23 | -0.02 | 0.00 | ▷ 0.00 | 0.00 | 0.00 | BC 167 |
| 160 | RC1 | 94 | 0 | MIN $M_T$ | -90.92 | 0.12 | 0.00 | ▷ 0.00 | 0.00 | 0.00 | BC 241 |
| 179 | RC1 | 93 | 2173 | MAX $M_y$ | -44.23 | -0.54 | 0.00 | 0.00 | ▷ 0.02 | 0.91 | BC 401 |
| 179 | RC1 | 93 | 2173 | MIN $M_y$ | -11.80 | 0.04 | 0.00 | 0.00 | ▷ -0.01 | -0.05 | BC 239 |
| 179 | RC1 | 93 | 2173 | MAX $M_z$ | -44.99 | -0.55 | 0.00 | 0.00 | 0.02 | ▷ 0.92 | BC 433 |
| 179 | RC1 | 93 | 2173 | MIN $M_z$ | -2.46 | 0.64 | 0.00 | 0.00 | 0.01 | ▷ -1.08 | BC 168 |
| | **Doorgaande staven No. 30: Doorgaande staven 30** | | | | | | | | | | |
| 51 | RC1 | 79 | 0 | Max N | ▷ 10.24 | -0.00 | 0.61 | 0.00 | 0.00 | 0.00 | BC 407 |
| | | | | Min N | ▷ -38.42 | 0.00 | 0.66 | -0.00 | -0.00 | 0.00 | BC 248 |
| | | | | Max $V_y$ | 2.99 | ▷ 0.00 | 1.08 | -0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min $V_y$ | 7.85 | ▷ -0.00 | 0.89 | 0.00 | -0.00 | 0.00 | BC 167 |
| | | | | Max $V_z$ | 3.68 | 0.00 | ▷ 1.09 | -0.00 | 0.00 | 0.00 | BC 185 |
| | | | | Min $V_z$ | -35.94 | 0.00 | ▷ 0.38 | -0.00 | 0.00 | 0.00 | BC 456 |
| | | | | Max $M_T$ | 3.36 | -0.00 | 0.87 | ▷ 0.00 | 0.00 | 0.00 | BC 243 |
| | | | | Min $M_T$ | -30.26 | 0.00 | 0.41 | ▷ -0.00 | -0.00 | 0.00 | BC 356 |
| | | | | Max $M_y$ | -4.30 | 0.00 | 0.87 | 0.00 | ▷ 0.00 | 0.00 | BC 114 |
| | | | | Min $M_y$ | -9.55 | 0.00 | 0.86 | 0.00 | ▷ -0.00 | 0.00 | BC 91 |
| | | | | Max $M_z$ | -7.06 | 0.00 | 0.98 | 0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | -7.06 | 0.00 | 0.98 | 0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | 93 | 4845 | Max N | ▷ 10.24 | -0.00 | -0.94 | 0.00 | -0.82 | 0.01 | BC 407 |
| | | | | Min N | ▷ -38.42 | 0.00 | -1.62 | -0.00 | -2.32 | -0.01 | BC 248 |
| | | | | Max $V_y$ | 2.99 | ▷ 0.00 | -1.20 | -0.00 | -0.29 | -0.01 | BC 241 |
| | | | | Min $V_y$ | 7.85 | ▷ -0.00 | -1.39 | 0.00 | -1.21 | 0.01 | BC 167 |
| | | | | Max $V_z$ | 3.93 | 0.00 | ▷ -0.74 | -0.00 | 0.17 | -0.01 | BC 377 |
| | | | | Min $V_z$ | -38.19 | 0.00 | ▷ -1.62 | -0.00 | -2.34 | -0.01 | BC 264 |
| | | | | Max $M_T$ | 3.36 | -0.00 | -1.41 | ▷ 0.00 | -1.31 | 0.01 | BC 243 |
| | | | | Min $M_T$ | -30.26 | 0.00 | -1.14 | ▷ -0.00 | -1.79 | -0.01 | BC 356 |
| | | | | Max $M_y$ | 3.93 | 0.00 | -0.74 | -0.00 | ▷ 0.17 | -0.01 | BC 377 |
| | | | | Min $M_y$ | -38.19 | 0.00 | -1.62 | -0.00 | ▷ -2.34 | -0.01 | BC 264 |
| | | | | Max $M_z$ | 7.85 | -0.00 | -1.39 | 0.00 | -1.21 | ▷ 0.01 | BC 167 |
| | | | | Min $M_z$ | 2.99 | 0.00 | -1.20 | -0.00 | -0.29 | ▷ -0.01 | BC 241 |
| | | 79 | 0 | Max N | ▷ 10.24 | -0.00 | 0.61 | 0.00 | 0.00 | 0.00 | BC 407 |
| | | 79 | 0 | Min N | ▷ -38.42 | 0.00 | 0.66 | -0.00 | -0.00 | 0.00 | BC 248 |
| | | 79 | 0 | Max $V_y$ | 2.99 | ▷ 0.00 | 1.08 | -0.00 | 0.00 | 0.00 | BC 241 |
| | | 79 | 0 | Min $V_y$ | 7.85 | ▷ -0.00 | 0.89 | 0.00 | -0.00 | 0.00 | BC 167 |
| | | 79 | 0 | Max $V_z$ | 3.68 | 0.00 | ▷ 1.09 | -0.00 | 0.00 | 0.00 | BC 185 |
| | | 93 | 4845 | Min $V_z$ | -38.19 | 0.00 | ▷ -1.62 | -0.00 | -2.34 | -0.01 | BC 264 |
| | | 79 | 0 | Max $M_T$ | 3.36 | -0.00 | 0.87 | ▷ 0.00 | 0.00 | 0.00 | BC 243 |
| | | 79 | 0 | Min $M_T$ | -30.26 | 0.00 | 0.41 | ▷ -0.00 | -0.00 | 0.00 | BC 356 |
| | | | 2326 | Max $M_y$ | 3.68 | 0.00 | -0.00 | -0.00 | ▷ 1.27 | -0.00 | BC 185 |
| | | 93 | 4845 | Min $M_y$ | -38.19 | 0.00 | -1.62 | -0.00 | ▷ -2.34 | -0.01 | BC 264 |
| | | 93 | 4845 | Max $M_z$ | 7.85 | -0.00 | -1.39 | 0.00 | -1.21 | ▷ 0.01 | BC 167 |
| | | 93 | 4845 | Min $M_z$ | 2.99 | 0.00 | -1.20 | -0.00 | -0.29 | ▷ -0.01 | BC 241 |
| 76 | RC1 | 93 | 0 | Max N | ▷ 8.32 | 0.00 | 0.69 | -0.01 | -0.71 | 0.00 | BC 359 |
| | | | | Min N | ▷ -37.50 | -0.00 | 1.16 | 0.01 | -1.29 | -0.00 | BC 248 |
| | | | | Max $V_y$ | -3.79 | ▷ 0.00 | 1.16 | -0.01 | -1.27 | 0.00 | BC 271 |
| | | | | Min $V_y$ | -23.01 | ▷ -0.00 | 0.63 | 0.01 | -0.61 | -0.00 | BC 357 |
| | | | | Max $V_z$ | -17.27 | 0.00 | ▷ 1.31 | 0.00 | -1.44 | 0.00 | BC 20 |
| | | | | Min $V_z$ | -23.34 | -0.00 | ▷ 0.63 | 0.01 | -0.61 | -0.00 | BC 417 |
| | | | | Max $M_T$ | -30.49 | -0.00 | 0.76 | ▷ 0.01 | -0.81 | -0.00 | BC 433 |
| | | | | Min $M_T$ | 5.97 | 0.00 | 1.03 | ▷ -0.01 | -1.06 | 0.00 | BC 167 |
| | | | | Max $M_y$ | -23.34 | -0.00 | 0.63 | 0.01 | ▷ -0.61 | -0.00 | BC 417 |
| | | | | Min $M_y$ | -17.27 | 0.00 | 1.31 | 0.00 | ▷ -1.44 | 0.00 | BC 20 |
| | | | | Max $M_z$ | -3.79 | 0.00 | 1.16 | -0.01 | -1.27 | ▷ 0.00 | BC 271 |
| | | | | Min $M_z$ | -23.01 | -0.00 | 0.63 | 0.01 | -0.61 | ▷ -0.00 | BC 357 |
| | | 80 | 1665 | Max N | ▷ 8.32 | 0.00 | 0.16 | -0.01 | 0.00 | 0.00 | BC 359 |
| | | | | Min N | ▷ -37.50 | -0.00 | 0.38 | 0.01 | 0.00 | 0.00 | BC 248 |
| | | | | Max $V_y$ | -3.79 | ▷ 0.00 | 0.37 | -0.01 | 0.00 | 0.00 | BC 271 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 76 | RC1 | | | Min $V_y$ | -23.01 | ▷ -0.00 | 0.10 | 0.01 | 0.00 | 0.00 | BC 357 |
| | | | | Max $V_z$ | -17.95 | 0.00 | ▷ 0.47 | 0.00 | -0.00 | 0.00 | BC 147 |
| | | | | Min $V_z$ | -23.34 | -0.00 | ▷ 0.10 | 0.01 | -0.00 | 0.00 | BC 417 |
| | | | | Max $M_T$ | -30.49 | -0.00 | 0.22 | ▷ 0.01 | 0.00 | 0.00 | BC 433 |
| | | | | Min $M_T$ | 5.97 | 0.00 | 0.25 | ▷ -0.01 | 0.00 | 0.00 | BC 167 |
| | | | | Max $M_y$ | -37.29 | -0.00 | 0.41 | 0.01 | ▷ 0.00 | 0.00 | BC 264 |
| | | | | Min $M_y$ | -3.79 | -0.00 | 0.28 | 0.01 | ▷ -0.00 | 0.00 | BC 198 |
| | | | | Max $M_z$ | -8.20 | 0.00 | 0.31 | -0.00 | -0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | -8.20 | 0.00 | 0.31 | -0.00 | -0.00 | ▷ 0.00 | BC 1 |
| | | 93 | 0 | Max N | ▷ 8.32 | 0.00 | 0.69 | -0.01 | -0.71 | 0.00 | BC 359 |
| | | 93 | 0 | Min N | ▷ -37.50 | -0.00 | 1.16 | 0.01 | -1.29 | -0.00 | BC 248 |
| | | 93 | 0 | Max $V_y$ | -3.79 | ▷ 0.00 | 1.16 | -0.01 | -1.27 | 0.00 | BC 271 |
| | | 93 | 0 | Min $V_y$ | -23.01 | ▷ -0.00 | 0.63 | 0.01 | -0.61 | -0.00 | BC 357 |
| | | 93 | 0 | Max $V_z$ | -17.27 | 0.00 | ▷ 1.31 | 0.00 | -1.44 | 0.00 | BC 20 |
| | | 80 | 1665 | Min $V_z$ | -23.34 | -0.00 | ▷ 0.10 | 0.01 | -0.00 | 0.00 | BC 417 |
| | | 93 | 0 | Max $M_T$ | -30.49 | -0.00 | 0.76 | ▷ 0.01 | -0.81 | -0.00 | BC 433 |
| | | 93 | 0 | Min $M_T$ | 5.97 | 0.00 | 1.03 | ▷ -0.01 | -1.06 | 0.00 | BC 167 |
| | | 80 | 1665 | Max $M_y$ | -37.29 | -0.00 | 0.41 | 0.01 | ▷ 0.00 | 0.00 | BC 264 |
| | | 93 | 0 | Min $M_y$ | -17.27 | 0.00 | 1.31 | 0.00 | ▷ -1.44 | 0.00 | BC 20 |
| | | 93 | 0 | Max $M_z$ | -3.79 | 0.00 | 1.16 | -0.01 | -1.27 | ▷ 0.00 | BC 271 |
| | | 93 | 0 | Min $M_z$ | -23.01 | -0.00 | 0.63 | 0.01 | -0.61 | ▷ -0.00 | BC 357 |
| 51 | RC1 | 79 | 0 | MAX N | ▷ 10.24 | 0.00 | 0.61 | 0.00 | 0.00 | 0.00 | BC 407 |
| 51 | RC1 | 79 | 0 | MIN N | ▷ -38.42 | 0.00 | 0.66 | 0.00 | 0.00 | 0.00 | BC 248 |
| 76 | RC1 | 93 | 0 | MAX $V_y$ | -3.79 | ▷ 0.00 | 1.16 | -0.01 | -1.27 | 0.00 | BC 271 |
| 76 | RC1 | 93 | 0 | MIN $V_y$ | -23.01 | ▷ 0.00 | 0.63 | 0.01 | -0.61 | 0.00 | BC 357 |
| 76 | RC1 | 93 | 0 | MAX $V_z$ | -17.27 | 0.00 | ▷ 1.31 | 0.00 | -1.44 | 0.00 | BC 20 |
| 51 | RC1 | 93 | 4845 | MIN $V_z$ | -38.19 | 0.00 | ▷ -1.62 | 0.00 | -2.34 | -0.01 | BC 264 |
| 76 | RC1 | 93 | 0 | MAX $M_T$ | -30.49 | 0.00 | 0.76 | ▷ 0.01 | -0.81 | 0.00 | BC 433 |
| 76 | RC1 | 93 | 0 | MIN $M_T$ | 5.97 | 0.00 | 1.03 | ▷ -0.01 | -1.06 | 0.00 | BC 167 |
| 51 | RC1 | | 2326 | MAX $M_y$ | 3.68 | 0.00 | 0.00 | 0.00 | ▷ 1.27 | 0.00 | BC 185 |
| 51 | RC1 | 93 | 4845 | MIN $M_y$ | -38.19 | 0.00 | -1.62 | 0.00 | ▷ -2.34 | -0.01 | BC 264 |
| 51 | RC1 | 93 | 4845 | MAX $M_z$ | 7.85 | 0.00 | -1.39 | 0.00 | -1.21 | ▷ 0.01 | BC 167 |
| 51 | RC1 | 93 | 4845 | MIN $M_z$ | 2.99 | 0.00 | -1.20 | 0.00 | -0.29 | ▷ -0.01 | BC 241 |
| | **Doorgaande staven No. 31: Doorgaande staven 31** | | | | | | | | | | |
| 106 | RC1 | 88 | 0 | Max N | ▷ 1.23 | -0.00 | -0.86 | 0.01 | -0.00 | 0.00 | BC 363 |
| | | | | Min N | ▷ -37.77 | 0.00 | -1.93 | -0.01 | 0.00 | 0.00 | BC 165 |
| | | | | Max $V_y$ | -34.15 | ▷ 0.00 | -2.76 | -0.01 | 0.00 | 0.00 | BC 217 |
| | | | | Min $V_y$ | -4.06 | ▷ -0.00 | -1.71 | 0.01 | 0.00 | 0.00 | BC 247 |
| | | | | Max $V_z$ | -17.31 | 0.00 | ▷ -0.37 | -0.01 | 0.00 | 0.00 | BC 360 |
| | | | | Min $V_z$ | -19.93 | -0.00 | ▷ -3.29 | 0.00 | 0.00 | 0.00 | BC 155 |
| | | | | Max $M_T$ | -9.96 | -0.00 | -2.54 | ▷ 0.01 | -0.00 | 0.00 | BC 243 |
| | | | | Min $M_T$ | -35.76 | 0.00 | -2.14 | ▷ -0.01 | 0.00 | 0.00 | BC 201 |
| | | | | Max $M_y$ | -10.84 | 0.00 | -2.24 | -0.00 | ▷ 0.00 | 0.00 | BC 278 |
| | | | | Min $M_y$ | -13.07 | -0.00 | -2.10 | 0.00 | ▷ -0.00 | 0.00 | BC 53 |
| | | | | Max $M_z$ | -10.40 | 0.00 | -1.75 | -0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | -10.40 | 0.00 | -1.75 | -0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | 96 | 1665 | Max N | ▷ 1.23 | -0.00 | -1.39 | 0.01 | -1.87 | 0.00 | BC 363 |
| | | | | Min N | ▷ -37.77 | 0.00 | -2.71 | -0.01 | -3.86 | -0.00 | BC 165 |
| | | | | Max $V_y$ | -34.15 | ▷ 0.00 | -3.54 | -0.01 | -5.25 | -0.00 | BC 217 |
| | | | | Min $V_y$ | -4.06 | ▷ -0.00 | -2.49 | 0.01 | -3.50 | 0.00 | BC 247 |
| | | | | Max $V_z$ | -17.31 | 0.00 | ▷ -0.90 | -0.01 | -1.06 | -0.00 | BC 360 |
| | | | | Min $V_z$ | -19.93 | -0.00 | ▷ -4.08 | 0.00 | -6.13 | 0.00 | BC 155 |
| | | | | Max $M_T$ | -9.96 | -0.00 | -3.33 | ▷ 0.01 | -4.89 | 0.00 | BC 243 |
| | | | | Min $M_T$ | -35.76 | 0.00 | -2.92 | ▷ -0.01 | -4.21 | -0.00 | BC 201 |
| | | | | Max $M_y$ | -17.31 | 0.00 | -0.90 | -0.01 | ▷ -1.06 | -0.00 | BC 360 |
| | | | | Min $M_y$ | -19.93 | -0.00 | -4.08 | 0.00 | ▷ -6.13 | 0.00 | BC 155 |
| | | | | Max $M_z$ | -4.06 | -0.00 | -2.49 | 0.01 | -3.50 | ▷ 0.00 | BC 247 |
| | | | | Min $M_z$ | -34.15 | 0.00 | -3.54 | -0.01 | -5.25 | ▷ -0.00 | BC 217 |
| | | 88 | 0 | Max N | ▷ 1.23 | -0.00 | -0.86 | 0.01 | -0.00 | 0.00 | BC 363 |
| | | 88 | 0 | Min N | ▷ -37.77 | 0.00 | -1.93 | -0.01 | 0.00 | 0.00 | BC 165 |
| | | 88 | 0 | Max $V_y$ | -34.15 | ▷ 0.00 | -2.76 | -0.01 | 0.00 | 0.00 | BC 217 |
| | | 88 | 0 | Min $V_y$ | -4.06 | ▷ -0.00 | -1.71 | 0.01 | 0.00 | 0.00 | BC 247 |
| | | 88 | 0 | Max $V_z$ | -17.31 | 0.00 | ▷ -0.37 | -0.01 | 0.00 | 0.00 | BC 360 |
| | | 96 | 1665 | Min $V_z$ | -19.93 | -0.00 | ▷ -4.08 | 0.00 | -6.13 | 0.00 | BC 155 |
| | | 88 | 0 | Max $M_T$ | -9.96 | -0.00 | -2.54 | ▷ 0.01 | -0.00 | 0.00 | BC 243 |
| | | 88 | 0 | Min $M_T$ | -35.76 | 0.00 | -2.14 | ▷ -0.01 | 0.00 | 0.00 | BC 201 |
| | | 88 | 0 | Max $M_y$ | -10.84 | 0.00 | -2.24 | -0.00 | ▷ 0.00 | 0.00 | BC 278 |
| | | 96 | 1665 | Min $M_y$ | -19.93 | -0.00 | -4.08 | 0.00 | ▷ -6.13 | 0.00 | BC 155 |
| | | 96 | 1665 | Max $M_z$ | -4.06 | -0.00 | -2.49 | 0.01 | -3.50 | ▷ 0.00 | BC 247 |
| | | 96 | 1665 | Min $M_z$ | -34.15 | 0.00 | -3.54 | -0.01 | -5.25 | ▷ -0.00 | BC 217 |
| 78 | RC1 | 96 | 0 | Max N | ▷ 18.02 | -0.00 | 1.91 | 0.00 | -3.72 | -0.00 | BC 268 |
| | | | | Min N | ▷ -39.13 | -0.00 | 2.31 | 0.00 | -5.68 | -0.00 | BC 165 |
| | | | | Max $V_y$ | 10.91 | ▷ 0.00 | 1.54 | 0.00 | -3.71 | 0.00 | BC 446 |
| | | | | Min $V_y$ | -33.35 | ▷ -0.00 | 2.70 | 0.00 | -7.58 | -0.00 | BC 205 |
| | | | | Max $V_z$ | -31.72 | -0.00 | ▷ 2.74 | 0.00 | -7.77 | -0.00 | BC 269 |
| | | | | Min $V_z$ | 11.95 | -0.00 | ▷ 0.86 | 0.00 | -0.39 | -0.00 | BC 360 |
| | | | | Max $M_T$ | -33.78 | -0.00 | 2.03 | ▷ 0.00 | -6.08 | -0.00 | BC 413 |
| | | | | Min $M_T$ | 10.06 | -0.00 | 1.25 | ▷ -0.00 | -2.31 | -0.00 | BC 451 |
| | | | | Max $M_y$ | 11.95 | -0.00 | 0.86 | 0.00 | ▷ -0.39 | -0.00 | BC 360 |
| | | | | Min $M_y$ | -31.72 | -0.00 | 2.74 | 0.00 | ▷ -7.77 | -0.00 | BC 269 |
| | | | | Max $M_z$ | 10.91 | 0.00 | 1.54 | 0.00 | -3.71 | ▷ 0.00 | BC 446 |
| | | | | Min $M_z$ | -33.35 | -0.00 | 2.70 | 0.00 | -7.58 | ▷ -0.00 | BC 205 |
| | | 77 | 4865 | Max N | ▷ 18.02 | -0.00 | -0.38 | 0.00 | 0.00 | 0.00 | BC 268 |
| | | | | Min N | ▷ -39.13 | -0.00 | 0.03 | 0.00 | 0.00 | 0.00 | BC 165 |
| | | | | Max $V_y$ | 10.91 | ▷ 0.00 | -0.02 | 0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Min $V_y$ | -33.35 | ▷ -0.00 | 0.42 | 0.00 | 0.00 | 0.00 | BC 205 |
| | | | | Max $V_z$ | -31.08 | -0.00 | ▷ 0.57 | 0.00 | 0.00 | 0.00 | BC 461 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 78 | RC1 | | | Min $V_z$ | 13.56 | -0.00 | ▷ -0.81 | 0.00 | 0.00 | 0.00 | BC 168 |
| | | | | Max $M_T$ | -33.78 | -0.00 | 0.47 | ▷ 0.00 | 0.00 | 0.00 | BC 413 |
| | | | | Min $M_T$ | 10.06 | -0.00 | -0.30 | ▷ -0.00 | 0.00 | 0.00 | BC 451 |
| | | | | Max $M_y$ | 2.79 | -0.00 | 0.12 | 0.00 | ▷ 0.00 | 0.00 | BC 44 |
| | | | | Min $M_y$ | 6.03 | 0.00 | -0.44 | 0.00 | ▷ -0.00 | 0.00 | BC 162 |
| | | | | Max $M_z$ | -2.19 | -0.00 | -0.40 | 0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | -2.19 | -0.00 | -0.40 | 0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | 96 | 0 | Max N | ▷ 18.02 | -0.00 | 1.91 | 0.00 | -3.72 | -0.00 | BC 268 |
| | | 96 | 0 | Min N | ▷ -39.13 | -0.00 | 2.31 | 0.00 | -5.68 | -0.00 | BC 165 |
| | | 96 | 0 | Max $V_y$ | 10.91 | ▷ 0.00 | 1.54 | 0.00 | -3.71 | 0.00 | BC 446 |
| | | 96 | 0 | Min $V_y$ | -33.35 | ▷ -0.00 | 2.70 | 0.00 | -7.58 | -0.00 | BC 205 |
| | | 96 | 0 | Max $V_z$ | -31.72 | -0.00 | ▷ 2.74 | 0.00 | -7.77 | -0.00 | BC 269 |
| | | 77 | 4865 | Min $V_z$ | 13.56 | -0.00 | ▷ -0.81 | 0.00 | 0.00 | 0.00 | BC 168 |
| | | 96 | 0 | Max $M_T$ | -33.78 | -0.00 | 2.03 | ▷ 0.00 | -6.08 | -0.00 | BC 413 |
| | | 96 | 0 | Min $M_T$ | 10.06 | -0.00 | 1.25 | ▷ -0.00 | -2.31 | -0.00 | BC 451 |
| | | | 2724 | Max $M_y$ | 11.95 | -0.00 | -0.01 | 0.00 | ▷ 0.76 | -0.00 | BC 360 |
| | | 96 | 0 | Min $M_y$ | -31.72 | -0.00 | 2.74 | 0.00 | ▷ -7.77 | -0.00 | BC 269 |
| | | 96 | 0 | Max $M_z$ | 10.91 | 0.00 | 1.54 | 0.00 | -3.71 | ▷ 0.00 | BC 446 |
| | | 96 | 0 | Min $M_z$ | -33.35 | -0.00 | 2.70 | 0.00 | -7.58 | ▷ -0.00 | BC 205 |
| 78 | RC1 | 96 | 0 | MAX N | ▷ 18.02 | 0.00 | 1.91 | 0.00 | -3.72 | 0.00 | BC 268 |
| 78 | RC1 | 96 | 0 | MIN N | ▷ -39.13 | 0.00 | 2.31 | 0.00 | -5.68 | 0.00 | BC 165 |
| 106 | RC1 | 88 | 0 | MAX $V_y$ | -34.15 | ▷ 0.00 | -2.76 | -0.01 | 0.00 | 0.00 | BC 217 |
| 106 | RC1 | 88 | 0 | MIN $V_y$ | -4.06 | ▷ 0.00 | -1.71 | 0.01 | 0.00 | 0.00 | BC 247 |
| 78 | RC1 | 96 | 0 | MAX $V_z$ | -31.72 | 0.00 | ▷ 2.74 | 0.00 | -7.77 | 0.00 | BC 269 |
| 106 | RC1 | 96 | 1665 | MIN $V_z$ | -19.93 | 0.00 | ▷ -4.08 | 0.00 | -6.13 | 0.00 | BC 155 |
| 106 | RC1 | 88 | 0 | MAX $M_T$ | -9.96 | 0.00 | -2.54 | ▷ 0.01 | 0.00 | 0.00 | BC 243 |
| 106 | RC1 | 88 | 0 | MIN $M_T$ | -35.76 | 0.00 | -2.14 | ▷ -0.01 | 0.00 | 0.00 | BC 201 |
| 78 | RC1 | | 2724 | MAX $M_y$ | 11.95 | 0.00 | -0.01 | 0.00 | ▷ 0.76 | 0.00 | BC 360 |
| 78 | RC1 | 96 | 0 | MIN $M_y$ | -31.72 | 0.00 | 2.74 | 0.00 | ▷ -7.77 | 0.00 | BC 269 |
| 106 | RC1 | 96 | 1665 | MAX $M_z$ | -4.06 | 0.00 | -2.49 | 0.01 | -3.50 | ▷ 0.00 | BC 247 |
| 106 | RC1 | 96 | 1665 | MIN $M_z$ | -34.15 | 0.00 | -3.54 | -0.01 | -5.25 | ▷ 0.00 | BC 217 |
| | **Doorgaande staven No. 32: Doorgaande staven 32** | | | | | | | | | | |
| 161 | RC1 | 97 | 0 | Max N | ▷ 24.10 | 0.17 | 0.00 | -0.00 | 0.00 | 0.00 | BC 357 |
| | | | | Min N | ▷ -121.56 | -0.10 | 0.00 | -0.00 | 0.00 | -0.00 | BC 240 |
| | | | | Max $V_y$ | 13.68 | ▷ 0.19 | 0.00 | -0.00 | 0.00 | 0.00 | BC 201 |
| | | | | Min $V_y$ | -109.52 | ▷ -0.12 | 0.00 | -0.00 | 0.00 | 0.00 | BC 444 |
| | | | | Max $V_z$ | 5.27 | 0.18 | ▷ 0.00 | -0.00 | 0.00 | 0.00 | BC 217 |
| | | | | Min $V_z$ | -39.31 | 0.04 | ▷ -0.00 | 0.00 | 0.00 | 0.00 | BC 247 |
| | | | | Max $M_T$ | -44.29 | 0.02 | -0.00 | ▷ 0.00 | 0.00 | 0.00 | BC 415 |
| | | | | Min $M_T$ | 22.19 | 0.16 | 0.00 | ▷ -0.00 | 0.00 | 0.00 | BC 417 |
| | | | | Max $M_y$ | -20.20 | 0.06 | 0.00 | 0.00 | ▷ 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -20.20 | 0.06 | 0.00 | 0.00 | ▷ 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -18.48 | 0.05 | 0.00 | 0.00 | 0.00 | ▷ 0.00 | BC 2 |
| | | | | Min $M_z$ | -46.07 | 0.04 | 0.00 | 0.00 | 0.00 | ▷ -0.00 | BC 91 |
| | | 98 | 2173 | Max N | ▷ 24.80 | 0.17 | 0.00 | -0.00 | 0.00 | -0.37 | BC 357 |
| | | | | Min N | ▷ -120.54 | -0.10 | 0.00 | -0.00 | 0.00 | 0.22 | BC 240 |
| | | | | Max $V_y$ | 14.70 | ▷ 0.19 | 0.00 | -0.00 | 0.00 | -0.42 | BC 201 |
| | | | | Min $V_y$ | -108.83 | ▷ -0.12 | 0.00 | -0.00 | 0.00 | 0.26 | BC 444 |
| | | | | Max $V_z$ | 6.29 | 0.18 | ▷ 0.00 | -0.00 | 0.00 | -0.38 | BC 217 |
| | | | | Min $V_z$ | -38.29 | 0.04 | ▷ -0.00 | 0.00 | -0.00 | -0.09 | BC 247 |
| | | | | Max $M_T$ | -43.60 | 0.02 | -0.00 | ▷ 0.00 | -0.00 | -0.05 | BC 415 |
| | | | | Min $M_T$ | 22.88 | 0.16 | 0.00 | ▷ -0.00 | 0.00 | -0.36 | BC 417 |
| | | | | Max $M_y$ | 6.29 | 0.18 | 0.00 | -0.00 | ▷ 0.00 | -0.38 | BC 217 |
| | | | | Min $M_y$ | -38.29 | 0.04 | -0.00 | 0.00 | ▷ -0.00 | -0.09 | BC 247 |
| | | | | Max $M_z$ | -108.83 | -0.12 | 0.00 | -0.00 | 0.00 | ▷ 0.26 | BC 444 |
| | | | | Min $M_z$ | 14.70 | 0.19 | 0.00 | -0.00 | 0.00 | ▷ -0.42 | BC 201 |
| | | 98 | 2173 | Max N | ▷ 24.80 | 0.17 | 0.00 | -0.00 | 0.00 | -0.37 | BC 357 |
| | | 97 | 0 | Min N | ▷ -121.56 | -0.10 | 0.00 | -0.00 | 0.00 | -0.00 | BC 240 |
| | | 97 | 0 | Max $V_y$ | 13.68 | ▷ 0.19 | 0.00 | -0.00 | 0.00 | 0.00 | BC 201 |
| | | 97 | 0 | Min $V_y$ | -109.52 | ▷ -0.12 | 0.00 | -0.00 | 0.00 | 0.00 | BC 444 |
| | | 97 | 0 | Max $V_z$ | 5.27 | 0.18 | ▷ 0.00 | -0.00 | 0.00 | 0.00 | BC 217 |
| | | 97 | 0 | Min $V_z$ | -39.31 | 0.04 | ▷ -0.00 | 0.00 | 0.00 | 0.00 | BC 247 |
| | | 97 | 0 | Max $M_T$ | -44.29 | 0.02 | -0.00 | ▷ 0.00 | 0.00 | 0.00 | BC 415 |
| | | 97 | 0 | Min $M_T$ | 22.19 | 0.16 | 0.00 | ▷ -0.00 | 0.00 | 0.00 | BC 417 |
| | | 98 | 2173 | Max $M_y$ | 6.29 | 0.18 | 0.00 | -0.00 | ▷ 0.00 | -0.38 | BC 217 |
| | | 98 | 2173 | Min $M_y$ | -38.29 | 0.04 | -0.00 | 0.00 | ▷ -0.00 | -0.09 | BC 247 |
| | | 98 | 2173 | Max $M_z$ | -108.83 | -0.12 | 0.00 | -0.00 | 0.00 | ▷ 0.26 | BC 444 |
| | | 98 | 2173 | Min $M_z$ | 14.70 | 0.19 | 0.00 | -0.00 | 0.00 | ▷ -0.42 | BC 201 |
| 182 | RC1 | 98 | 0 | Max N | ▷ -4.03 | -0.89 | 0.00 | -0.00 | 0.01 | -0.37 | BC 361 |
| | | | | Min N | ▷ -65.63 | 0.26 | 0.00 | -0.00 | 0.01 | 0.22 | BC 268 |
| | | | | Max $V_y$ | -46.20 | ▷ 0.44 | 0.00 | -0.00 | 0.01 | 0.24 | BC 376 |
| | | | | Min $V_y$ | -7.57 | ▷ -1.10 | 0.00 | -0.00 | 0.01 | -0.39 | BC 265 |
| | | | | Max $V_z$ | -7.16 | -1.09 | ▷ 0.00 | -0.00 | 0.01 | -0.38 | BC 217 |
| | | | | Min $V_z$ | -24.90 | -0.24 | ▷ -0.00 | 0.00 | -0.01 | -0.09 | BC 247 |
| | | | | Max $M_T$ | -27.50 | -0.22 | -0.00 | ▷ 0.00 | -0.01 | -0.05 | BC 415 |
| | | | | Min $M_T$ | -4.18 | -0.89 | 0.00 | ▷ -0.00 | 0.01 | -0.36 | BC 417 |
| | | | | Max $M_y$ | -5.95 | -1.02 | 0.00 | -0.00 | ▷ 0.01 | -0.40 | BC 225 |
| | | | | Min $M_y$ | -27.19 | -0.22 | -0.00 | 0.00 | ▷ -0.01 | -0.06 | BC 443 |
| | | | | Max $M_z$ | -56.62 | 0.37 | 0.00 | -0.00 | 0.01 | ▷ 0.26 | BC 444 |
| | | | | Min $M_z$ | -6.17 | -1.04 | 0.00 | -0.00 | 0.01 | ▷ -0.42 | BC 201 |
| | | 96 | 2173 | Max N | ▷ -3.33 | -0.89 | 0.00 | -0.00 | 0.01 | 1.56 | BC 361 |
| | | | | Min N | ▷ -64.61 | 0.26 | 0.00 | -0.00 | 0.01 | -0.35 | BC 268 |
| | | | | Max $V_y$ | -45.50 | ▷ 0.44 | 0.00 | -0.00 | 0.01 | -0.71 | BC 376 |
| | | | | Min $V_y$ | -6.55 | ▷ -1.10 | 0.00 | -0.00 | 0.01 | 2.00 | BC 265 |
| | | | | Max $V_z$ | -6.14 | -1.09 | ▷ 0.00 | -0.00 | 0.01 | 1.98 | BC 217 |
| | | | | Min $V_z$ | -23.88 | -0.24 | ▷ -0.00 | 0.00 | -0.01 | 0.43 | BC 247 |
| | | | | Max $M_T$ | -26.81 | -0.22 | -0.00 | ▷ 0.00 | -0.01 | 0.43 | BC 415 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 182 | RC1 | | | Min $M_T$ | -3.49 | -0.89 | 0.00 | ▷ -0.00 | 0.01 | 1.57 | BC 417 |
| | | | | Max $M_y$ | -4.84 | -1.03 | 0.00 | -0.00 | ▷ 0.01 | 1.82 | BC 165 |
| | | | | Min $M_y$ | -31.85 | -0.21 | -0.00 | 0.00 | ▷ -0.01 | 0.40 | BC 435 |
| | | | | Max $M_z$ | -6.55 | -1.10 | 0.00 | -0.00 | 0.01 | ▷ 2.00 | BC 265 |
| | | | | Min $M_z$ | -45.50 | 0.44 | 0.00 | -0.00 | 0.01 | ▷ -0.71 | BC 376 |
| | | 96 | 2173 | Max N | ▷ -3.33 | -0.89 | 0.00 | -0.00 | 0.01 | 1.56 | BC 361 |
| | | 98 | 0 | Min N | ▷ -65.63 | 0.26 | 0.00 | -0.00 | 0.01 | 0.22 | BC 268 |
| | | 98 | 0 | Max $V_y$ | -46.20 | ▷ 0.44 | 0.00 | -0.00 | 0.01 | 0.24 | BC 376 |
| | | 98 | 0 | Min $V_y$ | -7.57 | ▷ -1.10 | 0.00 | -0.00 | 0.01 | -0.39 | BC 265 |
| | | 98 | 0 | Max $V_z$ | -7.16 | -1.09 | ▷ 0.00 | -0.00 | 0.01 | -0.38 | BC 217 |
| | | 98 | 0 | Min $V_z$ | -24.90 | -0.24 | ▷ -0.00 | 0.00 | -0.01 | -0.09 | BC 247 |
| | | 98 | 0 | Max $M_T$ | -27.50 | -0.22 | -0.00 | ▷ 0.00 | -0.01 | -0.05 | BC 415 |
| | | 98 | 0 | Min $M_T$ | -4.18 | -0.89 | 0.00 | ▷ -0.00 | 0.01 | -0.36 | BC 417 |
| | | 96 | 2173 | Max $M_y$ | -4.84 | -1.03 | 0.00 | -0.00 | ▷ 0.01 | 1.82 | BC 165 |
| | | 96 | 2173 | Min $M_y$ | -31.85 | -0.21 | -0.00 | 0.00 | ▷ -0.01 | 0.40 | BC 435 |
| | | 96 | 2173 | Max $M_z$ | -6.55 | -1.10 | 0.00 | -0.00 | 0.01 | ▷ 2.00 | BC 265 |
| | | 96 | 2173 | Min $M_z$ | -45.50 | 0.44 | 0.00 | -0.00 | 0.01 | ▷ -0.71 | BC 376 |
| 161 | RC1 | 98 | 2173 | MAX N | ▷ 24.80 | 0.17 | 0.00 | 0.00 | 0.00 | -0.37 | BC 357 |
| 161 | RC1 | 97 | 0 | MIN N | ▷ -121.56 | -0.10 | 0.00 | 0.00 | 0.00 | 0.00 | BC 240 |
| 182 | RC1 | 98 | 0 | MAX $V_y$ | -46.20 | ▷ 0.44 | 0.00 | 0.00 | 0.01 | 0.24 | BC 376 |
| 182 | RC1 | 98 | 0 | MIN $V_y$ | -7.57 | ▷ -1.10 | 0.00 | 0.00 | 0.01 | -0.39 | BC 265 |
| 182 | RC1 | 98 | 0 | MAX $V_z$ | -7.16 | -1.09 | ▷ 0.00 | 0.00 | 0.01 | -0.38 | BC 217 |
| 161 | RC1 | 97 | 0 | MIN $V_z$ | -39.31 | 0.04 | ▷ 0.00 | 0.00 | 0.00 | 0.00 | BC 247 |
| 161 | RC1 | 97 | 0 | MAX $M_T$ | -44.29 | 0.02 | 0.00 | ▷ 0.00 | 0.00 | 0.00 | BC 415 |
| 161 | RC1 | 97 | 0 | MIN $M_T$ | 22.19 | 0.16 | 0.00 | ▷ 0.00 | 0.00 | 0.00 | BC 417 |
| 182 | RC1 | 96 | 2173 | MAX $M_y$ | -4.84 | -1.03 | 0.00 | 0.00 | ▷ 0.01 | 1.82 | BC 165 |
| 182 | RC1 | 96 | 2173 | MIN $M_y$ | -31.85 | -0.21 | 0.00 | 0.00 | ▷ -0.01 | 0.40 | BC 435 |
| 182 | RC1 | 96 | 2173 | MAX $M_z$ | -6.55 | -1.10 | 0.00 | 0.00 | 0.01 | ▷ 2.00 | BC 265 |
| 182 | RC1 | 96 | 2173 | MIN $M_z$ | -45.50 | 0.44 | 0.00 | 0.00 | 0.01 | ▷ -0.71 | BC 376 |
| | **Doorgaande staven No. 33: Doorgaande staven 33** | | | | | | | | | | |
| 70 | RC1 | 61 | 0 | Max N | ▷ 20.67 | 0.04 | 1.22 | 0.00 | 0.00 | 0.00 | BC 408 |
| | | | | Min N | ▷ -12.22 | 0.02 | 2.06 | 0.00 | -0.00 | 0.00 | BC 246 |
| | | | | Max $V_y$ | 7.73 | ▷ 0.05 | 1.22 | 0.00 | 0.00 | 0.00 | BC 448 |
| | | | | Min $V_y$ | -7.13 | ▷ -0.03 | 2.82 | -0.00 | 0.00 | 0.00 | BC 131 |
| | | | | Max $V_z$ | -1.59 | -0.02 | ▷ 2.82 | -0.00 | -0.00 | 0.00 | BC 154 |
| | | | | Min $V_z$ | -1.84 | -0.01 | ▷ 1.22 | 0.00 | 0.00 | 0.00 | BC 42 |
| | | | | Max $M_T$ | 10.78 | 0.01 | 1.22 | ▷ 0.01 | 0.00 | 0.00 | BC 471 |
| | | | | Min $M_T$ | 2.45 | -0.01 | 1.49 | ▷ -0.00 | 0.00 | 0.00 | BC 365 |
| | | | | Max $M_y$ | -7.92 | -0.03 | 2.82 | -0.00 | ▷ 0.00 | 0.00 | BC 146 |
| | | | | Min $M_y$ | -6.82 | 0.03 | 1.49 | 0.00 | ▷ -0.00 | 0.00 | BC 406 |
| | | | | Max $M_z$ | -6.08 | -0.02 | 2.60 | -0.00 | 0.00 | ▷ 0.00 | BC 99 |
| | | | | Min $M_z$ | 9.60 | 0.05 | 1.22 | 0.00 | 0.00 | ▷ -0.00 | BC 356 |
| | | 101 | 4300 | Max N | ▷ 20.67 | 0.04 | -0.41 | 0.00 | 1.73 | -0.18 | BC 408 |
| | | | | Min N | ▷ -12.22 | 0.02 | -0.34 | 0.00 | 3.69 | -0.10 | BC 246 |
| | | | | Max $V_y$ | 7.73 | ▷ 0.05 | -0.42 | 0.00 | 1.73 | -0.21 | BC 448 |
| | | | | Min $V_y$ | -7.13 | ▷ -0.03 | 0.42 | -0.00 | 6.96 | 0.11 | BC 131 |
| | | | | Max $V_z$ | -0.51 | -0.02 | ▷ 0.62 | -0.00 | 6.17 | 0.09 | BC 346 |
| | | | | Min $V_z$ | -2.05 | -0.01 | ▷ -0.69 | 0.00 | 2.83 | 0.04 | BC 10 |
| | | | | Max $M_T$ | 10.78 | 0.01 | -0.42 | ▷ 0.01 | 1.72 | -0.02 | BC 471 |
| | | | | Min $M_T$ | 2.45 | -0.01 | -0.15 | ▷ -0.00 | 2.88 | 0.03 | BC 365 |
| | | | | Max $M_y$ | -1.59 | -0.02 | 0.42 | -0.00 | ▷ 6.96 | 0.10 | BC 154 |
| | | | | Min $M_y$ | -1.84 | -0.01 | -0.42 | 0.00 | ▷ 1.71 | 0.02 | BC 42 |
| | | | | Max $M_z$ | -7.13 | -0.03 | 0.42 | -0.00 | 6.96 | ▷ 0.11 | BC 131 |
| | | | | Min $M_z$ | 7.73 | 0.05 | -0.42 | 0.00 | 1.73 | ▷ -0.21 | BC 448 |
| | | 61 | 0 | Max N | ▷ 20.67 | 0.04 | 1.22 | 0.00 | 0.00 | 0.00 | BC 408 |
| | | 61 | 0 | Min N | ▷ -12.22 | 0.02 | 2.06 | 0.00 | -0.00 | 0.00 | BC 246 |
| | | 61 | 0 | Max $V_y$ | 7.73 | ▷ 0.05 | 1.22 | 0.00 | 0.00 | 0.00 | BC 448 |
| | | 61 | 0 | Min $V_y$ | -7.13 | ▷ -0.03 | 2.82 | -0.00 | 0.00 | 0.00 | BC 131 |
| | | 61 | 0 | Max $V_z$ | -1.59 | -0.02 | ▷ 2.82 | -0.00 | -0.00 | 0.00 | BC 154 |
| | | 101 | 4300 | Min $V_z$ | -2.05 | -0.01 | ▷ -0.69 | 0.00 | 2.83 | 0.04 | BC 10 |
| | | 61 | 0 | Max $M_T$ | 10.78 | 0.01 | 1.22 | ▷ 0.01 | 0.00 | 0.00 | BC 471 |
| | | 61 | 0 | Min $M_T$ | 2.45 | -0.01 | 1.49 | ▷ -0.00 | 0.00 | 0.00 | BC 365 |
| | | 101 | 4300 | Max $M_y$ | -1.59 | -0.02 | 0.42 | -0.00 | ▷ 6.96 | 0.10 | BC 154 |
| | | 61 | 0 | Min $M_y$ | -6.82 | 0.03 | 1.49 | 0.00 | ▷ -0.00 | 0.00 | BC 406 |
| | | 101 | 4300 | Max $M_z$ | -7.13 | -0.03 | 0.42 | -0.00 | 6.96 | ▷ 0.11 | BC 131 |
| | | 101 | 4300 | Min $M_z$ | 7.73 | 0.05 | -0.42 | 0.00 | 1.73 | ▷ -0.21 | BC 448 |
| 33 | RC1 | 101 | 0 | Max N | ▷ 20.74 | -0.81 | -8.39 | 0.08 | 1.68 | -0.18 | BC 408 |
| | | | Links | Min N | ▷ -12.52 | -0.32 | -18.04 | 0.11 | 3.62 | -0.10 | BC 246 |
| | | | | Max $V_y$ | -7.66 | ▷ 0.53 | -34.16 | 0.15 | 6.84 | 0.11 | BC 131 |
| | | | | Min $V_y$ | 7.78 | ▷ -0.92 | -8.39 | 0.08 | 1.69 | -0.21 | BC 448 |
| | | | | Max $V_z$ | 11.52 | 0.07 | ▷ -8.36 | 0.05 | 1.68 | -0.02 | BC 411 |
| | | | | Min $V_z$ | -8.58 | 0.52 | ▷ -34.16 | 0.15 | 6.84 | 0.10 | BC 149 |
| | | | | Max $M_T$ | -2.07 | 0.45 | -34.16 | ▷ 0.15 | 6.84 | 0.09 | BC 155 |
| | | | | Min $M_T$ | -1.98 | 0.11 | -8.36 | ▷ 0.04 | 1.68 | 0.02 | BC 42 |
| | | | | Max $M_y$ | -2.12 | 0.45 | -34.16 | 0.15 | ▷ 6.84 | 0.09 | BC 148 |
| | | | | Min $M_y$ | 11.52 | 0.07 | -8.36 | 0.05 | ▷ 1.68 | -0.02 | BC 411 |
| | | | | Max $M_z$ | -7.66 | 0.53 | -34.16 | 0.15 | 6.84 | ▷ 0.11 | BC 131 |
| | | | | Min $M_z$ | 7.78 | -0.92 | -8.39 | 0.08 | 1.69 | ▷ -0.21 | BC 448 |
| | | | 0 | Max N | ▷ 20.74 | -0.81 | -8.39 | 0.08 | 1.68 | -0.18 | BC 408 |
| | | | Rechts | Min N | ▷ -12.52 | -0.32 | -18.04 | 0.11 | 3.62 | -0.10 | BC 246 |
| | | | | Max $V_y$ | -7.66 | ▷ 0.53 | -34.16 | 0.15 | 6.84 | 0.11 | BC 131 |
| | | | | Min $V_y$ | 7.78 | ▷ -0.92 | -8.39 | 0.08 | 1.69 | -0.21 | BC 448 |
| | | | | Max $V_z$ | 11.52 | 0.07 | ▷ -8.36 | 0.05 | 1.68 | -0.02 | BC 411 |
| | | | | Min $V_z$ | -8.58 | 0.52 | ▷ -34.16 | 0.15 | 6.84 | 0.10 | BC 149 |
| | | | | Max $M_T$ | -2.07 | 0.45 | -34.16 | ▷ 0.15 | 6.84 | 0.09 | BC 155 |
| | | | | Min $M_T$ | -1.98 | 0.11 | -8.36 | ▷ 0.04 | 1.68 | 0.02 | BC 42 |
| | | | | Max $M_y$ | -2.12 | 0.45 | -34.16 | 0.15 | ▷ 6.84 | 0.09 | BC 148 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 33 | RC1 | | | Min $M_y$ | 11.52 | 0.07 | -8.36 | 0.05 | ▷ 1.68 | -0.02 | BC 411 |
| | | | | Max $M_z$ | -7.66 | 0.53 | -34.16 | 0.15 | 6.84 | ▷ 0.11 | BC 131 |
| | | | | Min $M_z$ | 7.78 | -0.92 | -8.39 | 0.08 | 1.69 | ▷ -0.21 | BC 448 |
| | | | 200 | Max N | ▷ 20.74 | -1.04 | -8.46 | 0.08 | 0.00 | -0.00 | BC 408 |
| | | | Links | Min N | ▷ -12.52 | -0.69 | -18.15 | 0.11 | 0.00 | -0.00 | BC 246 |
| | | | | Max $V_y$ | -7.66 | ▷ 0.53 | -34.27 | 0.15 | 0.00 | 0.00 | BC 131 |
| | | | | Min $V_y$ | 7.78 | ▷ -1.16 | -8.47 | 0.08 | 0.00 | -0.00 | BC 448 |
| | | | | Max $V_z$ | 11.52 | -0.30 | ▷ -8.43 | 0.05 | 0.00 | -0.00 | BC 411 |
| | | | | Min $V_z$ | -8.58 | 0.52 | ▷ -34.27 | 0.15 | 0.00 | 0.00 | BC 149 |
| | | | | Max $M_T$ | -2.07 | 0.45 | -34.27 | ▷ 0.15 | 0.00 | 0.00 | BC 155 |
| | | | | Min $M_T$ | -1.98 | 0.11 | -8.43 | ▷ 0.04 | 0.00 | 0.00 | BC 42 |
| | | | | Max $M_y$ | -8.45 | 0.52 | -34.27 | 0.15 | ▷ 0.00 | 0.00 | BC 146 |
| | | | | Min $M_y$ | 6.43 | 0.04 | -8.43 | 0.04 | ▷ 0.00 | 0.00 | BC 56 |
| | | | | Max $M_z$ | -7.66 | 0.53 | -34.27 | 0.15 | 0.00 | ▷ 0.00 | BC 131 |
| | | | | Min $M_z$ | -2.34 | -1.15 | -8.47 | 0.08 | 0.00 | ▷ -0.00 | BC 358 |
| | | 63 | 200 | Max N | ▷ 20.74 | -1.04 | -8.46 | 0.08 | 0.00 | 0.00 | BC 408 |
| | | | Rechts | Min N | ▷ -12.52 | -0.69 | -18.15 | 0.11 | -0.00 | 0.00 | BC 246 |
| | | | | Max $V_y$ | -7.66 | ▷ 0.53 | -34.27 | 0.15 | 0.00 | 0.00 | BC 131 |
| | | | | Min $V_y$ | 7.78 | ▷ -1.16 | -8.47 | 0.08 | 0.00 | 0.00 | BC 448 |
| | | | | Max $V_z$ | 11.52 | -0.30 | ▷ -8.43 | 0.05 | 0.00 | 0.00 | BC 411 |
| | | | | Min $V_z$ | -8.58 | 0.52 | ▷ -34.27 | 0.15 | 0.00 | 0.00 | BC 149 |
| | | | | Max $M_T$ | -2.07 | 0.45 | -34.27 | ▷ 0.15 | 0.00 | 0.00 | BC 155 |
| | | | | Min $M_T$ | -1.98 | 0.11 | -8.43 | ▷ 0.04 | 0.00 | 0.00 | BC 42 |
| | | | | Max $M_y$ | -8.45 | 0.52 | -34.27 | 0.15 | ▷ 0.00 | 0.00 | BC 146 |
| | | | | Min $M_y$ | -7.07 | -0.86 | -14.22 | 0.09 | ▷ -0.00 | 0.00 | BC 406 |
| | | | | Max $M_z$ | -9.11 | -0.85 | -14.22 | 0.09 | -0.00 | ▷ 0.00 | BC 378 |
| | | | | Min $M_z$ | 9.66 | -1.09 | -8.47 | 0.08 | 0.00 | ▷ -0.00 | BC 356 |
| | | 101 | 0 | Max N | ▷ 20.74 | -0.81 | -8.39 | 0.08 | 1.68 | -0.18 | BC 408 |
| | | 101 | 0 | Min N | ▷ -12.52 | -0.32 | -18.04 | 0.11 | 3.62 | -0.10 | BC 246 |
| | | 101 | 0 | Max $V_y$ | -7.66 | ▷ 0.53 | -34.16 | 0.15 | 6.84 | 0.11 | BC 131 |
| | | 63 | 200 | Min $V_y$ | 7.78 | ▷ -1.16 | -8.47 | 0.08 | 0.00 | 0.00 | BC 448 |
| | | 101 | 0 | Max $V_z$ | 11.52 | 0.07 | ▷ -8.36 | 0.05 | 1.68 | -0.02 | BC 411 |
| | | 63 | 200 | Min $V_z$ | -8.58 | 0.52 | ▷ -34.27 | 0.15 | 0.00 | 0.00 | BC 149 |
| | | 101 | 0 | Max $M_T$ | -2.07 | 0.45 | -34.16 | ▷ 0.15 | 6.84 | 0.09 | BC 155 |
| | | 101 | 0 | Min $M_T$ | -1.98 | 0.11 | -8.36 | ▷ 0.04 | 1.68 | 0.02 | BC 42 |
| | | 101 | 0 | Max $M_y$ | -2.12 | 0.45 | -34.16 | 0.15 | ▷ 6.84 | 0.09 | BC 148 |
| | | 63 | 200 | Min $M_y$ | -7.07 | -0.86 | -14.22 | 0.09 | ▷ -0.00 | 0.00 | BC 406 |
| | | 101 | 0 | Max $M_z$ | -7.66 | 0.53 | -34.16 | 0.15 | 6.84 | ▷ 0.11 | BC 131 |
| | | 101 | 0 | Min $M_z$ | 7.78 | -0.92 | -8.39 | 0.08 | 1.69 | ▷ -0.21 | BC 448 |
| 33 | RC1 | 101 | 0 | MAX N | ▷ 20.74 | -0.81 | -8.39 | 0.08 | 1.68 | -0.18 | BC 408 |
| 33 | RC1 | 101 | 0 | MIN N | ▷ -12.52 | -0.32 | -18.04 | 0.11 | 3.62 | -0.10 | BC 246 |
| 33 | RC1 | 101 | 0 | MAX $V_y$ | -7.66 | ▷ 0.53 | -34.16 | 0.15 | 6.84 | 0.11 | BC 131 |
| 33 | RC1 | 63 | 200 | MIN $V_y$ | 7.78 | ▷ -1.16 | -8.47 | 0.08 | 0.00 | 0.00 | BC 448 |
| 70 | RC1 | 61 | 0 | MAX $V_z$ | -1.59 | -0.02 | ▷ 2.82 | 0.00 | 0.00 | 0.00 | BC 154 |
| 33 | RC1 | 63 | 200 | MIN $V_z$ | -8.58 | 0.52 | ▷ -34.27 | 0.15 | 0.00 | 0.00 | BC 149 |
| 33 | RC1 | 101 | 0 | MAX $M_T$ | -2.07 | 0.45 | -34.16 | ▷ 0.15 | 6.84 | 0.09 | BC 155 |
| 70 | RC1 | 61 | 0 | MIN $M_T$ | 2.45 | -0.01 | 1.49 | ▷ 0.00 | 0.00 | 0.00 | BC 365 |
| 70 | RC1 | 101 | 4300 | MAX $M_y$ | -1.59 | -0.02 | 0.42 | 0.00 | ▷ 6.96 | 0.10 | BC 154 |
| 33 | RC1 | 63 | 200 | MIN $M_y$ | -7.07 | -0.86 | -14.22 | 0.09 | ▷ 0.00 | 0.00 | BC 406 |
| 70 | RC1 | 101 | 4300 | MAX $M_z$ | -7.13 | -0.03 | 0.42 | 0.00 | 6.96 | ▷ 0.11 | BC 131 |
| 33 | RC1 | 101 | 0 | MIN $M_z$ | 7.78 | -0.92 | -8.39 | 0.08 | 1.69 | ▷ -0.21 | BC 448 |
| | **Doorgaande staven No. 34: Doorgaande staven 34** | | | | | | | | | | |
| 86 | RC1 | 86 | 0 | Max N | ▷ 34.49 | -0.03 | 2.03 | 0.02 | -0.00 | 0.00 | BC 204 |
| | | | | Min N | ▷ -9.19 | 0.01 | 2.03 | 0.01 | 0.00 | 0.00 | BC 247 |
| | | | | Max $V_y$ | 3.93 | ▷ 0.03 | 2.77 | 0.02 | 0.00 | 0.00 | BC 131 |
| | | | | Min $V_y$ | 32.02 | ▷ -0.04 | 1.20 | 0.01 | 0.00 | 0.00 | BC 448 |
| | | | | Max $V_z$ | 3.79 | 0.03 | ▷ 2.77 | 0.02 | 0.00 | 0.00 | BC 134 |
| | | | | Min $V_z$ | -1.89 | -0.03 | ▷ 1.20 | 0.01 | 0.00 | 0.00 | BC 470 |
| | | | | Max $M_T$ | 4.93 | 0.02 | 2.77 | ▷ 0.02 | 0.00 | 0.00 | BC 154 |
| | | | | Min $M_T$ | -0.48 | -0.01 | 1.20 | ▷ 0.01 | -0.00 | 0.00 | BC 361 |
| | | | | Max $M_y$ | -0.49 | -0.02 | 1.46 | 0.01 | ▷ 0.00 | 0.00 | BC 378 |
| | | | | Min $M_y$ | 0.34 | -0.01 | 1.20 | 0.01 | ▷ -0.00 | 0.00 | BC 381 |
| | | | | Max $M_z$ | -0.49 | -0.02 | 1.46 | 0.01 | 0.00 | ▷ 0.00 | BC 378 |
| | | | | Min $M_z$ | 1.54 | 0.01 | 1.99 | 0.01 | 0.00 | ▷ 0.00 | BC 1 |
| | | 102 | 4300 | Max N | ▷ 34.49 | -0.03 | -0.37 | 0.02 | 3.56 | 0.11 | BC 204 |
| | | | | Min N | ▷ -9.19 | 0.01 | -0.37 | 0.01 | 3.57 | -0.06 | BC 247 |
| | | | | Max $V_y$ | 3.93 | ▷ 0.03 | 0.37 | 0.02 | 6.75 | -0.11 | BC 131 |
| | | | | Min $V_y$ | 32.02 | ▷ -0.04 | -0.43 | 0.01 | 1.65 | 0.18 | BC 448 |
| | | | | Max $V_z$ | 3.18 | 0.02 | ▷ 0.57 | 0.02 | 5.98 | -0.10 | BC 326 |
| | | | | Min $V_z$ | 2.97 | 0.01 | ▷ -0.72 | 0.01 | 2.73 | -0.02 | BC 30 |
| | | | | Max $M_T$ | 4.93 | 0.02 | 0.37 | ▷ 0.02 | 6.75 | -0.10 | BC 154 |
| | | | | Min $M_T$ | -0.48 | -0.01 | -0.43 | ▷ 0.01 | 1.65 | 0.03 | BC 361 |
| | | | | Max $M_y$ | 3.79 | 0.03 | 0.37 | 0.02 | ▷ 6.75 | -0.11 | BC 134 |
| | | | | Min $M_y$ | -1.89 | -0.03 | -0.44 | 0.01 | ▷ 1.64 | 0.14 | BC 470 |
| | | | | Max $M_z$ | 32.02 | -0.04 | -0.43 | 0.01 | 1.65 | ▷ 0.18 | BC 448 |
| | | | | Min $M_z$ | 3.93 | 0.03 | 0.37 | 0.02 | 6.75 | ▷ -0.11 | BC 131 |
| | | 86 | 0 | Max N | ▷ 34.49 | -0.03 | 2.03 | 0.02 | -0.00 | 0.00 | BC 204 |
| | | 86 | 0 | Min N | ▷ -9.19 | 0.01 | 2.03 | 0.01 | 0.00 | 0.00 | BC 247 |
| | | 86 | 0 | Max $V_y$ | 3.93 | ▷ 0.03 | 2.77 | 0.02 | 0.00 | 0.00 | BC 131 |
| | | 86 | 0 | Min $V_y$ | 32.02 | ▷ -0.04 | 1.20 | 0.01 | 0.00 | 0.00 | BC 448 |
| | | 86 | 0 | Max $V_z$ | 3.79 | 0.03 | ▷ 2.77 | 0.02 | 0.00 | 0.00 | BC 134 |
| | | 102 | 4300 | Min $V_z$ | 2.97 | 0.01 | ▷ -0.72 | 0.01 | 2.73 | -0.02 | BC 30 |
| | | 86 | 0 | Max $M_T$ | 4.93 | 0.02 | 2.77 | ▷ 0.02 | 0.00 | 0.00 | BC 154 |
| | | 86 | 0 | Min $M_T$ | -0.48 | -0.01 | 1.20 | ▷ 0.01 | -0.00 | 0.00 | BC 361 |
| | | 102 | 4300 | Max $M_y$ | 3.79 | 0.03 | 0.37 | 0.02 | ▷ 6.75 | -0.11 | BC 134 |
| | | 86 | 0 | Min $M_y$ | 0.34 | -0.01 | 1.20 | 0.01 | ▷ -0.00 | 0.00 | BC 381 |
| | | 102 | 4300 | Max $M_z$ | 32.02 | -0.04 | -0.43 | 0.01 | 1.65 | ▷ 0.18 | BC 448 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 86 | RC1 | 102 | 4300 | Min $M_z$ | 3.93 | 0.03 | 0.37 | 0.02 | 6.75 | -0.11 | BC 131 |
| 37 | RC1 | 102 | 0 | Max N | 34.41 | 0.57 | -18.19 | 0.08 | 3.65 | 0.11 | BC 204 |
| | | | | Min N | -9.40 | -0.29 | -18.22 | 0.11 | 3.65 | -0.06 | BC 247 |
| | | | | Max $V_y$ | 32.07 | 0.93 | -8.41 | 0.01 | 1.69 | 0.19 | BC 448 |
| | | | | Min $V_y$ | 3.40 | -0.53 | -34.52 | 0.22 | 6.91 | -0.11 | BC 131 |
| | | | | Max $V_z$ | 32.07 | 0.93 | -8.41 | 0.01 | 1.69 | 0.19 | BC 448 |
| | | | | Min $V_z$ | 3.65 | -0.52 | -34.52 | 0.22 | 6.91 | -0.10 | BC 138 |
| | | | | Max $M_T$ | 3.40 | -0.53 | -34.52 | 0.22 | 6.91 | -0.11 | BC 131 |
| | | | | Min $M_T$ | 32.07 | 0.93 | -8.41 | 0.01 | 1.69 | 0.19 | BC 448 |
| | | | | Max $M_y$ | 3.65 | -0.52 | -34.52 | 0.22 | 6.91 | -0.10 | BC 138 |
| | | | | Min $M_y$ | 32.07 | 0.93 | -8.41 | 0.01 | 1.69 | 0.19 | BC 448 |
| | | | | Max $M_z$ | 32.07 | 0.93 | -8.41 | 0.01 | 1.69 | 0.19 | BC 448 |
| | | | | Min $M_z$ | 3.40 | -0.53 | -34.52 | 0.22 | 6.91 | -0.11 | BC 131 |
| | | 68 | 200 | Max N | 34.41 | 0.57 | -18.30 | 0.08 | -0.00 | 0.00 | BC 204 |
| | | | | Min N | -9.40 | -0.29 | -18.33 | 0.11 | 0.00 | 0.00 | BC 247 |
| | | | | Max $V_y$ | 32.07 | 0.93 | -8.49 | 0.01 | 0.00 | 0.00 | BC 448 |
| | | | | Min $V_y$ | 3.40 | -0.53 | -34.63 | 0.22 | 0.00 | 0.00 | BC 131 |
| | | | | Max $V_z$ | 32.07 | 0.93 | -8.49 | 0.01 | 0.00 | 0.00 | BC 448 |
| | | | | Min $V_z$ | 3.65 | -0.52 | -34.63 | 0.22 | 0.00 | 0.00 | BC 138 |
| | | | | Max $M_T$ | 3.40 | -0.53 | -34.63 | 0.22 | 0.00 | 0.00 | BC 131 |
| | | | | Min $M_T$ | 32.07 | 0.93 | -8.49 | 0.01 | 0.00 | 0.00 | BC 448 |
| | | | | Max $M_y$ | 4.35 | -0.46 | -34.63 | 0.22 | 0.00 | -0.00 | BC 140 |
| | | | | Min $M_y$ | 2.99 | -0.18 | -18.33 | 0.11 | -0.00 | 0.00 | BC 91 |
| | | | | Max $M_z$ | -0.59 | 0.50 | -14.32 | 0.06 | 0.00 | 0.00 | BC 406 |
| | | | | Min $M_z$ | 33.34 | 0.74 | -14.32 | 0.05 | -0.00 | -0.00 | BC 368 |
| | | 102 | 0 | Max N | 34.41 | 0.57 | -18.19 | 0.08 | 3.65 | 0.11 | BC 204 |
| | | 102 | 0 | Min N | -9.40 | -0.29 | -18.22 | 0.11 | 3.65 | -0.06 | BC 247 |
| | | 102 | 0 | Max $V_y$ | 32.07 | 0.93 | -8.41 | 0.01 | 1.69 | 0.19 | BC 448 |
| | | 102 | 0 | Min $V_y$ | 3.40 | -0.53 | -34.52 | 0.22 | 6.91 | -0.11 | BC 131 |
| | | 102 | 0 | Max $V_z$ | 32.07 | 0.93 | -8.41 | 0.01 | 1.69 | 0.19 | BC 448 |
| | | 68 | 200 | Min $V_z$ | 3.65 | -0.52 | -34.63 | 0.22 | 0.00 | 0.00 | BC 138 |
| | | 102 | 0 | Max $M_T$ | 3.40 | -0.53 | -34.52 | 0.22 | 6.91 | -0.11 | BC 131 |
| | | 102 | 0 | Min $M_T$ | 32.07 | 0.93 | -8.41 | 0.01 | 1.69 | 0.19 | BC 448 |
| | | 102 | 0 | Max $M_y$ | 3.65 | -0.52 | -34.52 | 0.22 | 6.91 | -0.10 | BC 138 |
| | | 68 | 200 | Min $M_y$ | 2.99 | -0.18 | -18.33 | 0.11 | -0.00 | 0.00 | BC 91 |
| | | 102 | 0 | Max $M_z$ | 32.07 | 0.93 | -8.41 | 0.01 | 1.69 | 0.19 | BC 448 |
| | | 102 | 0 | Min $M_z$ | 3.40 | -0.53 | -34.52 | 0.22 | 6.91 | -0.11 | BC 131 |
| 86 | RC1 | 86 | 0 | MAX N | 34.49 | -0.03 | 2.03 | 0.02 | 0.00 | 0.00 | BC 204 |
| 37 | RC1 | 102 | 0 | MIN N | -9.40 | -0.29 | -18.22 | 0.11 | 3.65 | -0.06 | BC 247 |
| 37 | RC1 | 102 | 0 | MAX $V_y$ | 32.07 | 0.93 | -8.41 | 0.01 | 1.69 | 0.19 | BC 448 |
| 37 | RC1 | 102 | 0 | MIN $V_y$ | 3.40 | -0.53 | -34.52 | 0.22 | 6.91 | -0.11 | BC 131 |
| 86 | RC1 | 86 | 0 | MAX $V_z$ | 3.79 | 0.03 | 2.77 | 0.02 | 0.00 | 0.00 | BC 134 |
| 37 | RC1 | 68 | 200 | MIN $V_z$ | 3.65 | -0.52 | -34.63 | 0.22 | 0.00 | 0.00 | BC 138 |
| 37 | RC1 | 102 | 0 | MAX $M_T$ | 3.40 | -0.53 | -34.52 | 0.22 | 6.91 | -0.11 | BC 131 |
| 86 | RC1 | 86 | 0 | MIN $M_T$ | -0.48 | -0.01 | 1.20 | 0.01 | 0.00 | 0.00 | BC 361 |
| 37 | RC1 | 102 | 0 | MAX $M_y$ | 3.65 | -0.52 | -34.52 | 0.22 | 6.91 | -0.10 | BC 138 |
| 37 | RC1 | 68 | 200 | MIN $M_y$ | 2.99 | -0.18 | -18.33 | 0.11 | 0.00 | 0.00 | BC 91 |
| 37 | RC1 | 102 | 0 | MAX $M_z$ | 32.07 | 0.93 | -8.41 | 0.01 | 1.69 | 0.19 | BC 448 |
| 86 | RC1 | 102 | 4300 | MIN $M_z$ | 3.93 | 0.03 | 0.37 | 0.02 | 6.75 | -0.11 | BC 131 |
| | **Doorgaande staven No. 35: Doorgaande staven 35** | | | | | | | | | | |
| 28 | RC1 | 57 | 0 | Max N | 3.19 | 0.01 | 7.25 | 0.01 | 0.00 | 0.00 | BC 359 |
| | | | | Min N | -16.97 | -0.00 | 7.25 | -0.01 | -0.00 | 0.00 | BC 356 |
| | | | | Max $V_y$ | -4.89 | 0.03 | 16.42 | -0.01 | 0.00 | 0.00 | BC 269 |
| | | | | Min $V_y$ | -16.97 | -0.00 | 7.25 | -0.01 | -0.00 | 0.00 | BC 356 |
| | | | | Max $V_z$ | -1.73 | 0.01 | 32.63 | 0.00 | -0.00 | 0.00 | BC 141 |
| | | | | Min $V_z$ | -6.52 | -0.00 | 7.25 | -0.01 | 0.00 | 0.00 | BC 440 |
| | | | | Max $M_T$ | 2.33 | 0.02 | 16.42 | 0.01 | 0.00 | 0.00 | BC 243 |
| | | | | Min $M_T$ | -16.97 | -0.00 | 7.25 | -0.01 | -0.00 | 0.00 | BC 356 |
| | | | | Max $M_y$ | -3.34 | 0.00 | 16.42 | -0.01 | 0.00 | 0.00 | BC 268 |
| | | | | Min $M_y$ | -12.94 | 0.00 | 16.42 | -0.01 | -0.00 | 0.00 | BC 232 |
| | | | | Max $M_z$ | -0.80 | 0.01 | 12.01 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.80 | 0.01 | 12.01 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 157 | 3267 | Max N | 3.45 | 0.01 | 0.12 | 0.01 | 12.04 | -0.04 | BC 359 |
| | | | | Min N | -16.71 | -0.00 | 0.11 | -0.01 | 12.04 | 0.02 | BC 356 |
| | | | | Max $V_y$ | -4.29 | 0.03 | 0.17 | -0.01 | 27.10 | -0.09 | BC 269 |
| | | | | Min $V_y$ | -16.71 | -0.00 | 0.11 | -0.01 | 12.04 | 0.02 | BC 356 |
| | | | | Max $V_z$ | -0.33 | 0.01 | 0.19 | 0.00 | 19.93 | -0.03 | BC 17 |
| | | | | Min $V_z$ | -5.23 | -0.00 | 0.11 | -0.01 | 21.48 | 0.00 | BC 428 |
| | | | | Max $M_T$ | 2.93 | 0.02 | 0.17 | 0.01 | 27.10 | -0.06 | BC 243 |
| | | | | Min $M_T$ | -16.71 | -0.00 | 0.11 | -0.01 | 12.04 | 0.02 | BC 356 |
| | | | | Max $M_y$ | -0.52 | 0.01 | 0.17 | 0.00 | 53.58 | -0.05 | BC 141 |
| | | | | Min $M_y$ | -6.25 | -0.00 | 0.11 | -0.01 | 12.03 | 0.01 | BC 440 |
| | | | | Max $M_z$ | -16.71 | -0.00 | 0.11 | -0.01 | 12.04 | 0.02 | BC 356 |
| | | | | Min $M_z$ | -4.29 | 0.03 | 0.17 | -0.01 | 27.10 | -0.09 | BC 269 |
| | | 157 | 3267 | Max N | 3.45 | 0.01 | 0.12 | 0.01 | 12.04 | -0.04 | BC 359 |
| | | 57 | 0 | Min N | -16.97 | -0.00 | 7.25 | -0.01 | -0.00 | 0.00 | BC 356 |
| | | 57 | 0 | Max $V_y$ | -4.89 | 0.03 | 16.42 | -0.01 | 0.00 | 0.00 | BC 269 |
| | | 57 | 0 | Min $V_y$ | -16.97 | -0.00 | 7.25 | -0.01 | -0.00 | 0.00 | BC 356 |
| | | 57 | 0 | Max $V_z$ | -1.73 | 0.01 | 32.63 | 0.00 | -0.00 | 0.00 | BC 141 |
| | | 157 | 3267 | Min $V_z$ | -5.23 | -0.00 | 0.11 | -0.01 | 21.48 | 0.00 | BC 428 |
| | | 57 | 0 | Max $M_T$ | 2.33 | 0.02 | 16.42 | 0.01 | 0.00 | 0.00 | BC 243 |
| | | 57 | 0 | Min $M_T$ | -16.97 | -0.00 | 7.25 | -0.01 | -0.00 | 0.00 | BC 356 |
| | | 157 | 3267 | Max $M_y$ | -0.52 | 0.01 | 0.17 | 0.00 | 53.58 | -0.05 | BC 141 |
| | | 57 | 0 | Min $M_y$ | -12.94 | 0.00 | 16.42 | -0.01 | -0.00 | 0.00 | BC 232 |
| | | 157 | 3267 | Max $M_z$ | -16.71 | -0.00 | 0.11 | -0.01 | 12.04 | 0.02 | BC 356 |
| | | 157 | 3267 | Min $M_z$ | -4.29 | 0.03 | 0.17 | -0.01 | 27.10 | -0.09 | BC 269 |
| 195 | RC1 | 157 | 0 | Max N | 3.46 | -0.01 | -0.11 | 0.01 | 12.02 | -0.04 | BC 359 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 195 | RC1 | | | Min N | ▷ -16.70 | 0.00 | -0.11 | -0.01 | 12.02 | 0.02 | BC 356 |
| | | | | Max $V_y$ | -16.70 | ▷ 0.00 | -0.11 | -0.01 | 12.02 | 0.02 | BC 356 |
| | | | | Min $V_y$ | -4.28 | ▷ -0.03 | -0.16 | -0.01 | 27.09 | -0.09 | BC 269 |
| | | | | Max $V_z$ | -3.72 | -0.02 | ▷ -0.11 | -0.01 | 12.02 | -0.06 | BC 417 |
| | | | | Min $V_z$ | -0.75 | -0.01 | ▷ -0.19 | -0.00 | 29.37 | -0.03 | BC 20 |
| | | | | Max $M_T$ | 3.36 | -0.01 | -0.16 | ▷ 0.01 | 17.63 | -0.04 | BC 171 |
| | | | | Min $M_T$ | -4.28 | -0.03 | -0.16 | ▷ -0.01 | 27.09 | -0.09 | BC 269 |
| | | | | Max $M_y$ | -0.84 | -0.02 | -0.17 | -0.00 | ▷ 53.57 | -0.06 | BC 147 |
| | | | | Min $M_y$ | -3.72 | -0.02 | -0.11 | -0.01 | ▷ 12.02 | -0.06 | BC 417 |
| | | | | Max $M_z$ | -16.70 | 0.00 | -0.11 | -0.01 | 12.02 | ▷ 0.02 | BC 356 |
| | | | | Min $M_z$ | -4.28 | -0.03 | -0.16 | -0.01 | 27.09 | ▷ -0.09 | BC 269 |
| | | 42 | 3267 | Max N | ▷ 3.92 | -0.01 | -16.42 | 0.01 | 0.00 | 0.00 | BC 203 |
| | | | | Min N | ▷ -16.43 | 0.00 | -7.25 | -0.01 | -0.00 | 0.00 | BC 356 |
| | | | | Max $V_y$ | -16.43 | ▷ 0.00 | -7.25 | -0.01 | -0.00 | 0.00 | BC 356 |
| | | | | Min $V_y$ | -3.67 | ▷ -0.03 | -16.42 | -0.01 | 0.00 | 0.00 | BC 269 |
| | | | | Max $V_z$ | -3.45 | -0.02 | ▷ -7.25 | -0.01 | 0.00 | 0.00 | BC 417 |
| | | | | Min $V_z$ | 0.37 | -0.02 | ▷ -32.63 | -0.00 | 0.00 | 0.00 | BC 147 |
| | | | | Max $M_T$ | 3.75 | -0.01 | -10.63 | ▷ 0.01 | 0.00 | 0.00 | BC 171 |
| | | | | Min $M_T$ | -3.67 | -0.03 | -16.42 | ▷ -0.01 | 0.00 | 0.00 | BC 269 |
| | | | | Max $M_y$ | -2.12 | -0.00 | -16.42 | -0.01 | ▷ 0.00 | 0.00 | BC 268 |
| | | | | Min $M_y$ | -11.72 | -0.00 | -16.42 | -0.01 | ▷ -0.00 | 0.00 | BC 232 |
| | | | | Max $M_z$ | 0.09 | -0.01 | -12.00 | -0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.09 | -0.01 | -12.00 | -0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | 42 | 3267 | Max N | ▷ 3.92 | -0.01 | -16.42 | 0.01 | 0.00 | 0.00 | BC 203 |
| | | 157 | 0 | Min N | ▷ -16.70 | 0.00 | -0.11 | -0.01 | 12.02 | 0.02 | BC 356 |
| | | 157 | 0 | Max $V_y$ | -16.70 | ▷ 0.00 | -0.11 | -0.01 | 12.02 | 0.02 | BC 356 |
| | | 157 | 0 | Min $V_y$ | -4.28 | ▷ -0.03 | -0.16 | -0.01 | 27.09 | -0.09 | BC 269 |
| | | 157 | 0 | Max $V_z$ | -3.72 | -0.02 | ▷ -0.11 | -0.01 | 12.02 | -0.06 | BC 417 |
| | | 42 | 3267 | Min $V_z$ | 0.37 | -0.02 | ▷ -32.63 | -0.00 | 0.00 | 0.00 | BC 147 |
| | | 157 | 0 | Max $M_T$ | 3.36 | -0.01 | -0.16 | ▷ 0.01 | 17.63 | -0.04 | BC 171 |
| | | 157 | 0 | Min $M_T$ | -4.28 | -0.03 | -0.16 | ▷ -0.01 | 27.09 | -0.09 | BC 269 |
| | | 157 | 0 | Max $M_y$ | -0.84 | -0.02 | -0.17 | -0.00 | ▷ 53.57 | -0.06 | BC 147 |
| | | 42 | 3267 | Min $M_y$ | -11.72 | -0.00 | -16.42 | -0.01 | ▷ -0.00 | 0.00 | BC 232 |
| | | 157 | 0 | Max $M_z$ | -16.70 | 0.00 | -0.11 | -0.01 | 12.02 | ▷ 0.02 | BC 356 |
| | | 157 | 0 | Min $M_z$ | -4.28 | -0.03 | -0.16 | -0.01 | 27.09 | ▷ -0.09 | BC 269 |
| 195 | RC1 | 42 | 3267 | MAX N | ▷ 3.92 | -0.01 | -16.42 | 0.01 | 0.00 | 0.00 | BC 203 |
| 28 | RC1 | 57 | 0 | MIN N | ▷ -16.97 | 0.00 | 7.25 | -0.01 | 0.00 | 0.00 | BC 356 |
| 28 | RC1 | 57 | 0 | MAX $V_y$ | -4.89 | ▷ 0.03 | 16.42 | -0.01 | 0.00 | 0.00 | BC 269 |
| 195 | RC1 | 157 | 0 | MIN $V_y$ | -4.28 | ▷ -0.03 | -0.16 | -0.01 | 27.09 | -0.09 | BC 269 |
| 28 | RC1 | 57 | 0 | MAX $V_z$ | -1.73 | 0.01 | ▷ 32.63 | 0.00 | 0.00 | 0.00 | BC 141 |
| 195 | RC1 | 42 | 3267 | MIN $V_z$ | 0.37 | -0.02 | ▷ -32.63 | 0.00 | 0.00 | 0.00 | BC 147 |
| 28 | RC1 | 57 | 0 | MAX $M_T$ | 2.33 | 0.02 | 16.42 | ▷ 0.01 | 0.00 | 0.00 | BC 243 |
| 195 | RC1 | 157 | 0 | MIN $M_T$ | -4.28 | -0.03 | -0.16 | ▷ -0.01 | 27.09 | -0.09 | BC 269 |
| 28 | RC1 | 157 | 3267 | MAX $M_y$ | -0.52 | 0.01 | 0.17 | 0.00 | ▷ 53.58 | -0.05 | BC 141 |
| 28 | RC1 | 57 | 0 | MIN $M_y$ | -12.94 | 0.00 | 16.42 | -0.01 | ▷ 0.00 | 0.00 | BC 232 |
| 28 | RC1 | 157 | 3267 | MAX $M_z$ | -16.71 | 0.00 | 0.11 | -0.01 | 12.04 | ▷ 0.02 | BC 356 |
| 28 | RC1 | 157 | 3267 | MIN $M_z$ | -4.29 | 0.03 | 0.17 | -0.01 | 27.10 | ▷ -0.09 | BC 269 |
| | **Doorgaande staven No. 36: Doorgaande staven 36** | | | | | | | | | | |
| 34 | RC1 | 42 | 0 | Max N | ▷ 4.87 | 0.09 | 16.82 | 0.01 | 0.00 | 0.00 | BC 243 |
| | | | | Min N | ▷ -41.63 | -0.01 | 11.05 | -0.01 | 0.00 | 0.00 | BC 168 |
| | | | | Max $V_y$ | 4.65 | ▷ 0.12 | 7.55 | 0.01 | -0.00 | 0.00 | BC 447 |
| | | | | Min $V_y$ | -20.08 | ▷ -0.11 | 7.53 | -0.01 | 0.00 | 0.00 | BC 357 |
| | | | | Max $V_z$ | 0.94 | -0.02 | ▷ 32.95 | -0.00 | 0.00 | 0.00 | BC 131 |
| | | | | Min $V_z$ | -19.74 | -0.11 | ▷ 7.53 | -0.01 | 0.00 | 0.00 | BC 477 |
| | | | | Max $M_T$ | 4.65 | 0.12 | 7.55 | ▷ 0.01 | -0.00 | 0.00 | BC 447 |
| | | | | Min $M_T$ | -20.08 | -0.11 | 7.53 | ▷ -0.01 | 0.00 | 0.00 | BC 357 |
| | | | | Max $M_y$ | -40.46 | -0.01 | 16.81 | -0.01 | ▷ 0.00 | 0.00 | BC 172 |
| | | | | Min $M_y$ | -5.95 | -0.07 | 11.06 | -0.01 | ▷ -0.00 | -0.00 | BC 278 |
| | | | | Max $M_z$ | -36.24 | -0.03 | 13.29 | -0.01 | 0.00 | ▷ 0.00 | BC 368 |
| | | | | Min $M_z$ | -41.52 | -0.02 | 7.53 | -0.01 | -0.00 | ▷ -0.00 | BC 356 |
| | | 151 | 3256 | Max N | ▷ 4.56 | 0.09 | 0.61 | 0.01 | 28.38 | -0.31 | BC 243 |
| | | | | Min N | ▷ -41.83 | -0.01 | 0.61 | -0.01 | 18.97 | 0.03 | BC 168 |
| | | | | Max $V_y$ | 4.52 | ▷ 0.12 | 0.43 | 0.01 | 12.99 | -0.40 | BC 447 |
| | | | | Min $V_y$ | -20.21 | ▷ -0.11 | 0.41 | -0.01 | 12.93 | 0.35 | BC 357 |
| | | | | Max $V_z$ | -1.07 | -0.02 | ▷ 0.69 | -0.00 | 21.44 | 0.05 | BC 3 |
| | | | | Min $V_z$ | 0.59 | -0.01 | ▷ 0.37 | -0.00 | 48.50 | 0.03 | BC 347 |
| | | | | Max $M_T$ | 4.52 | 0.12 | 0.43 | ▷ 0.01 | 12.99 | -0.40 | BC 447 |
| | | | | Min $M_T$ | -20.21 | -0.11 | 0.41 | ▷ -0.01 | 12.93 | 0.35 | BC 357 |
| | | | | Max $M_y$ | 0.33 | -0.02 | 0.57 | -0.00 | ▷ 54.55 | 0.06 | BC 131 |
| | | | | Min $M_y$ | -19.88 | -0.11 | 0.41 | -0.01 | ▷ 12.93 | 0.35 | BC 477 |
| | | | | Max $M_z$ | -20.21 | -0.11 | 0.41 | -0.01 | 12.93 | ▷ 0.35 | BC 357 |
| | | | | Min $M_z$ | 4.52 | 0.12 | 0.43 | 0.01 | 12.99 | ▷ -0.40 | BC 447 |
| | | 42 | 0 | Max N | ▷ 4.87 | 0.09 | 16.82 | 0.01 | 0.00 | 0.00 | BC 243 |
| | | 151 | 3256 | Min N | ▷ -41.83 | -0.01 | 0.61 | -0.01 | 18.97 | 0.03 | BC 168 |
| | | 42 | 0 | Max $V_y$ | 4.65 | ▷ 0.12 | 7.55 | 0.01 | -0.00 | 0.00 | BC 447 |
| | | 42 | 0 | Min $V_y$ | -20.08 | ▷ -0.11 | 7.53 | -0.01 | 0.00 | 0.00 | BC 357 |
| | | 42 | 0 | Max $V_z$ | 0.94 | -0.02 | ▷ 32.95 | -0.00 | 0.00 | 0.00 | BC 131 |
| | | 151 | 3256 | Min $V_z$ | 0.59 | -0.01 | ▷ 0.37 | -0.00 | 48.50 | 0.03 | BC 347 |
| | | 42 | 0 | Max $M_T$ | 4.65 | 0.12 | 7.55 | ▷ 0.01 | -0.00 | 0.00 | BC 447 |
| | | 42 | 0 | Min $M_T$ | -20.08 | -0.11 | 7.53 | ▷ -0.01 | 0.00 | 0.00 | BC 357 |
| | | 151 | 3256 | Max $M_y$ | 0.33 | -0.02 | 0.57 | -0.00 | ▷ 54.55 | 0.06 | BC 131 |
| | | 42 | 0 | Min $M_y$ | -5.95 | -0.07 | 11.06 | -0.01 | ▷ -0.00 | -0.00 | BC 278 |
| | | 151 | 3256 | Max $M_z$ | -20.21 | -0.11 | 0.41 | -0.01 | 12.93 | ▷ 0.35 | BC 357 |
| | | 151 | 3256 | Min $M_z$ | 4.52 | 0.12 | 0.43 | 0.01 | 12.99 | ▷ -0.40 | BC 447 |
| 189 | RC1 | 151 | 0 | Max N | ▷ 4.61 | -0.09 | -0.69 | -0.00 | 28.62 | -0.31 | BC 243 |
| | | | | Min N | ▷ -41.79 | 0.01 | -0.66 | -0.01 | 19.15 | 0.03 | BC 168 |
| | | | | Max $V_y$ | -20.18 | ▷ 0.11 | -0.45 | 0.00 | 13.04 | 0.35 | BC 357 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 189 | RC1 | | | Min $V_y$ | 4.53 | ▷ -0.12 | -0.47 | -0.00 | 13.11 | -0.40 | BC 447 |
| | | | | Max $V_z$ | -16.18 | 0.11 | ▷ -0.45 | 0.00 | 13.04 | 0.35 | BC 413 |
| | | | | Min $V_z$ | -0.17 | 0.02 | ▷ -0.77 | 0.00 | 31.07 | 0.07 | BC 4 |
| | | | | Max $M_T$ | -20.18 | 0.11 | -0.45 | ▷ 0.00 | 13.04 | 0.35 | BC 357 |
| | | | | Min $M_T$ | -41.66 | 0.01 | -0.66 | ▷ -0.01 | 19.15 | 0.03 | BC 164 |
| | | | | Max $M_y$ | 0.43 | 0.02 | -0.71 | 0.00 | ▷ 55.02 | 0.06 | BC 131 |
| | | | | Min $M_y$ | -16.18 | 0.11 | -0.45 | 0.00 | ▷ 13.04 | 0.35 | BC 413 |
| | | | | Max $M_z$ | -20.18 | 0.11 | -0.45 | 0.00 | 13.04 | ▷ 0.35 | BC 357 |
| | | | | Min $M_z$ | 4.53 | -0.12 | -0.47 | -0.00 | 13.11 | ▷ -0.40 | BC 447 |
| | | 41 | 3256 | Max N | ▷ 4.40 | -0.12 | -7.59 | -0.00 | -0.00 | 0.00 | BC 447 |
| | | | | Min N | ▷ -41.99 | 0.01 | -11.10 | -0.01 | 0.00 | 0.00 | BC 168 |
| | | | | Max $V_y$ | -20.31 | ▷ 0.11 | -7.57 | 0.00 | 0.00 | 0.00 | BC 357 |
| | | | | Min $V_y$ | 4.40 | ▷ -0.12 | -7.59 | -0.00 | -0.00 | 0.00 | BC 447 |
| | | | | Max $V_z$ | -16.31 | 0.11 | ▷ -7.56 | 0.00 | -0.00 | 0.00 | BC 413 |
| | | | | Min $V_z$ | -0.19 | 0.02 | ▷ -33.09 | 0.00 | 0.00 | 0.00 | BC 131 |
| | | | | Max $M_T$ | -20.31 | 0.11 | -7.57 | ▷ 0.00 | 0.00 | 0.00 | BC 357 |
| | | | | Min $M_T$ | -41.85 | 0.01 | -11.10 | ▷ -0.01 | 0.00 | 0.00 | BC 164 |
| | | | | Max $M_y$ | -41.02 | 0.01 | -16.89 | -0.01 | ▷ 0.00 | 0.00 | BC 172 |
| | | | | Min $M_y$ | -6.32 | 0.07 | -11.12 | 0.00 | ▷ -0.00 | -0.00 | BC 278 |
| | | | | Max $M_z$ | -36.68 | 0.03 | -13.36 | -0.01 | 0.00 | ▷ 0.00 | BC 368 |
| | | | | Min $M_z$ | -41.76 | 0.02 | -7.57 | -0.01 | -0.00 | ▷ -0.00 | BC 356 |
| | | 151 | 0 | Max N | ▷ 4.61 | -0.09 | -0.69 | -0.00 | 28.62 | -0.31 | BC 243 |
| | | 41 | 3256 | Min N | ▷ -41.99 | 0.01 | -11.10 | -0.01 | 0.00 | 0.00 | BC 168 |
| | | 151 | 0 | Max $V_y$ | -20.18 | ▷ 0.11 | -0.45 | 0.00 | 13.04 | 0.35 | BC 357 |
| | | 151 | 0 | Min $V_y$ | 4.53 | ▷ -0.12 | -0.47 | -0.00 | 13.11 | -0.40 | BC 447 |
| | | 151 | 0 | Max $V_z$ | -16.18 | 0.11 | ▷ -0.45 | 0.00 | 13.04 | 0.35 | BC 413 |
| | | 41 | 3256 | Min $V_z$ | -0.19 | 0.02 | ▷ -33.09 | 0.00 | 0.00 | 0.00 | BC 131 |
| | | 151 | 0 | Max $M_T$ | -20.18 | 0.11 | -0.45 | ▷ 0.00 | 13.04 | 0.35 | BC 357 |
| | | 151 | 0 | Min $M_T$ | -41.66 | 0.01 | -0.66 | ▷ -0.01 | 19.15 | 0.03 | BC 164 |
| | | 151 | 0 | Max $M_y$ | 0.43 | 0.02 | -0.71 | 0.00 | ▷ 55.02 | 0.06 | BC 131 |
| | | 41 | 3256 | Min $M_y$ | -6.32 | 0.07 | -11.12 | 0.00 | ▷ -0.00 | -0.00 | BC 278 |
| | | 151 | 0 | Max $M_z$ | -20.18 | 0.11 | -0.45 | 0.00 | 13.04 | ▷ 0.35 | BC 357 |
| | | 151 | 0 | Min $M_z$ | 4.53 | -0.12 | -0.47 | -0.00 | 13.11 | ▷ -0.40 | BC 447 |
| 34 | RC1 | 42 | 0 | MAX N | ▷ 4.87 | 0.09 | 16.82 | 0.01 | 0.00 | 0.00 | BC 243 |
| 189 | RC1 | 41 | 3256 | MIN N | ▷ -41.99 | 0.01 | -11.10 | -0.01 | 0.00 | 0.00 | BC 168 |
| 34 | RC1 | 42 | 0 | MAX $V_y$ | 4.65 | ▷ 0.12 | 7.55 | 0.01 | 0.00 | 0.00 | BC 447 |
| 189 | RC1 | 151 | 0 | MIN $V_y$ | 4.53 | ▷ -0.12 | -0.47 | 0.00 | 13.11 | -0.40 | BC 447 |
| 34 | RC1 | 42 | 0 | MAX $V_z$ | 0.94 | -0.02 | ▷ 32.95 | 0.00 | 0.00 | 0.00 | BC 131 |
| 189 | RC1 | 41 | 3256 | MIN $V_z$ | -0.19 | 0.02 | ▷ -33.09 | 0.00 | 0.00 | 0.00 | BC 131 |
| 34 | RC1 | 42 | 0 | MAX $M_T$ | 4.65 | 0.12 | 7.55 | ▷ 0.01 | 0.00 | 0.00 | BC 447 |
| 34 | RC1 | 42 | 0 | MIN $M_T$ | -20.08 | -0.11 | 7.53 | ▷ -0.01 | 0.00 | 0.00 | BC 357 |
| 189 | RC1 | 151 | 0 | MAX $M_y$ | 0.43 | 0.02 | -0.71 | 0.00 | ▷ 55.02 | 0.06 | BC 131 |
| 189 | RC1 | 41 | 3256 | MIN $M_y$ | -6.32 | 0.07 | -11.12 | 0.00 | ▷ 0.00 | 0.00 | BC 278 |
| 189 | RC1 | 151 | 0 | MAX $M_z$ | -20.18 | 0.11 | -0.45 | 0.00 | 13.04 | ▷ 0.35 | BC 357 |
| 189 | RC1 | 151 | 0 | MIN $M_z$ | 4.53 | -0.12 | -0.47 | 0.00 | 13.11 | ▷ -0.40 | BC 447 |
| | **Doorgaande staven No. 37: Doorgaande staven 37** | | | | | | | | | | |
| 27 | RC1 | 56 | 0 | Max N | ▷ 3.74 | -0.14 | 7.09 | -0.02 | 0.00 | 0.00 | BC 447 |
| | | | | Min N | ▷ -3.97 | -0.02 | 16.07 | 0.01 | -0.00 | 0.00 | BC 172 |
| | | | | Max $V_y$ | 2.76 | ▷ 0.19 | 10.41 | 0.03 | 0.00 | 0.00 | BC 253 |
| | | | | Min $V_y$ | 3.52 | ▷ -0.16 | 16.07 | -0.02 | 0.00 | 0.00 | BC 175 |
| | | | | Max $V_z$ | -0.40 | -0.04 | ▷ 31.92 | -0.00 | 0.00 | 0.00 | BC 141 |
| | | | | Min $V_z$ | -3.77 | -0.00 | ▷ 7.09 | 0.02 | 0.00 | 0.00 | BC 440 |
| | | | | Max $M_T$ | 2.76 | 0.19 | 10.41 | ▷ 0.03 | 0.00 | 0.00 | BC 253 |
| | | | | Min $M_T$ | 3.52 | -0.16 | 16.07 | ▷ -0.02 | 0.00 | 0.00 | BC 175 |
| | | | | Max $M_y$ | -0.20 | -0.03 | 16.07 | -0.00 | ▷ 0.00 | 0.00 | BC 70 |
| | | | | Min $M_y$ | 1.39 | -0.02 | 10.41 | 0.01 | ▷ -0.00 | 0.00 | BC 226 |
| | | | | Max $M_z$ | -0.15 | -0.03 | 11.75 | -0.00 | -0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.15 | -0.03 | 11.75 | -0.00 | -0.00 | ▷ 0.00 | BC 1 |
| | | 145 | 3201 | Max N | ▷ 3.92 | -0.15 | 0.13 | -0.02 | 25.92 | 0.49 | BC 243 |
| | | | | Min N | ▷ -3.68 | -0.02 | 0.10 | 0.01 | 11.51 | 0.06 | BC 360 |
| | | | | Max $V_y$ | 2.95 | ▷ 0.19 | 0.14 | 0.03 | 16.88 | -0.60 | BC 253 |
| | | | | Min $V_y$ | 3.82 | ▷ -0.16 | 0.13 | -0.02 | 25.92 | 0.53 | BC 175 |
| | | | | Max $V_z$ | 0.07 | -0.03 | ▷ 0.16 | -0.00 | 19.06 | 0.10 | BC 17 |
| | | | | Min $V_z$ | 0.22 | -0.03 | ▷ 0.05 | -0.00 | 45.86 | 0.09 | BC 339 |
| | | | | Max $M_T$ | 2.95 | 0.19 | 0.14 | ▷ 0.03 | 16.88 | -0.60 | BC 253 |
| | | | | Min $M_T$ | 3.82 | -0.16 | 0.13 | ▷ -0.02 | 25.92 | 0.53 | BC 175 |
| | | | | Max $M_y$ | 0.19 | -0.04 | 0.10 | -0.00 | ▷ 51.24 | 0.14 | BC 141 |
| | | | | Min $M_y$ | -3.64 | -0.00 | 0.09 | 0.02 | ▷ 11.50 | 0.01 | BC 440 |
| | | | | Max $M_z$ | 3.82 | -0.16 | 0.13 | -0.02 | 25.92 | ▷ 0.53 | BC 175 |
| | | | | Min $M_z$ | 2.95 | 0.19 | 0.14 | 0.03 | 16.88 | ▷ -0.60 | BC 253 |
| | | 145 | 3201 | Max N | ▷ 3.92 | -0.15 | 0.13 | -0.02 | 25.92 | 0.49 | BC 243 |
| | | 56 | 0 | Min N | ▷ -3.97 | -0.02 | 16.07 | 0.01 | -0.00 | 0.00 | BC 172 |
| | | 56 | 0 | Max $V_y$ | 2.76 | ▷ 0.19 | 10.41 | 0.03 | 0.00 | 0.00 | BC 253 |
| | | 56 | 0 | Min $V_y$ | 3.52 | ▷ -0.16 | 16.07 | -0.02 | 0.00 | 0.00 | BC 175 |
| | | 56 | 0 | Max $V_z$ | -0.40 | -0.04 | ▷ 31.92 | -0.00 | 0.00 | 0.00 | BC 141 |
| | | 145 | 3201 | Min $V_z$ | 0.22 | -0.03 | ▷ 0.05 | -0.00 | 45.86 | 0.09 | BC 339 |
| | | 56 | 0 | Max $M_T$ | 2.76 | 0.19 | 10.41 | ▷ 0.03 | 0.00 | 0.00 | BC 253 |
| | | 56 | 0 | Min $M_T$ | 3.52 | -0.16 | 16.07 | ▷ -0.02 | 0.00 | 0.00 | BC 175 |
| | | 145 | 3201 | Max $M_y$ | 0.19 | -0.04 | 0.10 | -0.00 | ▷ 51.24 | 0.14 | BC 141 |
| | | 56 | 0 | Min $M_y$ | 1.39 | -0.02 | 10.41 | 0.01 | ▷ -0.00 | 0.00 | BC 226 |
| | | 145 | 3201 | Max $M_z$ | 3.82 | -0.16 | 0.13 | -0.02 | 25.92 | ▷ 0.53 | BC 175 |
| | | 145 | 3201 | Min $M_z$ | 2.95 | 0.19 | 0.14 | 0.03 | 16.88 | ▷ -0.60 | BC 253 |
| 183 | RC1 | 145 | 0 | Max N | ▷ 3.92 | 0.15 | -0.20 | -0.00 | 26.16 | 0.49 | BC 243 |
| | | | | Min N | ▷ -3.67 | 0.02 | -0.13 | 0.02 | 11.62 | 0.06 | BC 360 |
| | | | | Max $V_y$ | 3.83 | ▷ 0.16 | -0.20 | -0.00 | 26.15 | 0.53 | BC 175 |
| | | | | Min $V_y$ | 2.96 | ▷ -0.19 | -0.19 | 0.00 | 17.04 | -0.60 | BC 253 |
| | | | | Max $V_z$ | 2.76 | -0.18 | ▷ -0.13 | 0.00 | 11.61 | -0.58 | BC 417 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 183 | RC1 | | | Min $V_z$ | 0.24 | 0.04 | ▷ -0.24 | 0.00 | 51.70 | 0.12 | BC 147 |
| | | | | Max $M_T$ | -3.67 | 0.02 | -0.19 | ▷ 0.02 | 17.03 | 0.08 | BC 168 |
| | | | | Min $M_T$ | 3.87 | 0.14 | -0.13 | ▷ -0.00 | 11.62 | 0.44 | BC 475 |
| | | | | Max $M_y$ | 0.24 | 0.04 | -0.24 | 0.00 | ▷ 51.70 | 0.12 | BC 147 |
| | | | | Min $M_y$ | 2.76 | -0.18 | -0.13 | 0.00 | ▷ 11.61 | -0.58 | BC 417 |
| | | | | Max $M_z$ | 3.83 | 0.16 | -0.20 | -0.00 | 26.15 | ▷ 0.53 | BC 175 |
| | | | | Min $M_z$ | 2.96 | -0.19 | -0.19 | 0.00 | 17.04 | ▷ -0.60 | BC 253 |
| | | 41 | 3201 | Max N | ▷ 4.22 | 0.15 | -16.14 | -0.00 | 0.00 | 0.00 | BC 243 |
| | | | | Min N | ▷ -3.54 | 0.02 | -7.13 | 0.02 | 0.00 | 0.00 | BC 360 |
| | | | | Max $V_y$ | 4.13 | ▷ 0.16 | -16.14 | -0.00 | 0.00 | 0.00 | BC 175 |
| | | | | Min $V_y$ | 3.15 | ▷ -0.19 | -10.46 | 0.00 | 0.00 | 0.00 | BC 253 |
| | | | | Max $V_z$ | 2.89 | -0.18 | ▷ -7.13 | 0.00 | -0.00 | 0.00 | BC 417 |
| | | | | Min $V_z$ | 0.84 | 0.04 | ▷ -32.07 | 0.00 | -0.00 | 0.00 | BC 147 |
| | | | | Max $M_T$ | -3.48 | 0.02 | -10.45 | ▷ 0.02 | -0.00 | 0.00 | BC 168 |
| | | | | Min $M_T$ | 4.00 | 0.14 | -7.13 | ▷ -0.00 | 0.00 | 0.00 | BC 475 |
| | | | | Max $M_y$ | 0.40 | 0.03 | -16.14 | 0.00 | ▷ 0.00 | 0.00 | BC 70 |
| | | | | Min $M_y$ | 1.78 | 0.02 | -10.45 | 0.01 | ▷ -0.00 | 0.00 | BC 226 |
| | | | | Max $M_z$ | 0.29 | 0.03 | -11.80 | 0.00 | -0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.29 | 0.03 | -11.80 | 0.00 | -0.00 | ▷ 0.00 | BC 1 |
| | | 41 | 3201 | Max N | ▷ 4.22 | 0.15 | -16.14 | -0.00 | 0.00 | 0.00 | BC 243 |
| | | 145 | 0 | Min N | ▷ -3.67 | 0.02 | -0.13 | 0.02 | 11.62 | 0.06 | BC 360 |
| | | 145 | 0 | Max $V_y$ | 3.83 | ▷ 0.16 | -0.20 | -0.00 | 26.15 | 0.53 | BC 175 |
| | | 145 | 0 | Min $V_y$ | 2.96 | ▷ -0.19 | -0.19 | 0.00 | 17.04 | -0.60 | BC 253 |
| | | 145 | 0 | Max $V_z$ | 2.76 | -0.18 | ▷ -0.13 | 0.00 | 11.61 | -0.58 | BC 417 |
| | | 41 | 3201 | Min $V_z$ | 0.84 | 0.04 | ▷ -32.07 | 0.00 | -0.00 | 0.00 | BC 147 |
| | | 145 | 0 | Max $M_T$ | -3.67 | 0.02 | -0.19 | ▷ 0.02 | 17.03 | 0.08 | BC 168 |
| | | 145 | 0 | Min $M_T$ | 3.87 | 0.14 | -0.13 | ▷ -0.00 | 11.62 | 0.44 | BC 475 |
| | | 145 | 0 | Max $M_y$ | 0.24 | 0.04 | -0.24 | 0.00 | ▷ 51.70 | 0.12 | BC 147 |
| | | 41 | 3201 | Min $M_y$ | 1.78 | 0.02 | -10.45 | 0.01 | ▷ -0.00 | 0.00 | BC 226 |
| | | 145 | 0 | Max $M_z$ | 3.83 | 0.16 | -0.20 | -0.00 | 26.15 | ▷ 0.53 | BC 175 |
| | | 145 | 0 | Min $M_z$ | 2.96 | -0.19 | -0.19 | 0.00 | 17.04 | ▷ -0.60 | BC 253 |
| 183 | RC1 | 41 | 3201 | MAX N | ▷ 4.22 | 0.15 | -16.14 | 0.00 | 0.00 | 0.00 | BC 243 |
| 27 | RC1 | 56 | 0 | MIN N | ▷ -3.97 | -0.02 | 16.07 | 0.01 | 0.00 | 0.00 | BC 172 |
| 27 | RC1 | 56 | 0 | MAX $V_y$ | 2.76 | ▷ 0.19 | 10.41 | 0.03 | 0.00 | 0.00 | BC 253 |
| 183 | RC1 | 145 | 0 | MIN $V_y$ | 2.96 | ▷ -0.19 | -0.19 | 0.00 | 17.04 | -0.60 | BC 253 |
| 27 | RC1 | 56 | 0 | MAX $V_z$ | -0.40 | -0.04 | ▷ 31.92 | 0.00 | 0.00 | 0.00 | BC 141 |
| 183 | RC1 | 41 | 3201 | MIN $V_z$ | 0.84 | 0.04 | ▷ -32.07 | 0.00 | 0.00 | 0.00 | BC 147 |
| 27 | RC1 | 56 | 0 | MAX $M_T$ | 2.76 | 0.19 | 10.41 | ▷ 0.03 | 0.00 | 0.00 | BC 253 |
| 27 | RC1 | 56 | 0 | MIN $M_T$ | 3.52 | -0.16 | 16.07 | ▷ -0.02 | 0.00 | 0.00 | BC 175 |
| 183 | RC1 | 145 | 0 | MAX $M_y$ | 0.24 | 0.04 | -0.24 | 0.00 | ▷ 51.70 | 0.12 | BC 147 |
| 27 | RC1 | 56 | 0 | MIN $M_y$ | 1.39 | -0.02 | 10.41 | 0.01 | ▷ 0.00 | 0.00 | BC 226 |
| 27 | RC1 | 145 | 3201 | MAX $M_z$ | 3.82 | -0.16 | 0.13 | -0.02 | 25.92 | ▷ 0.53 | BC 175 |
| 27 | RC1 | 145 | 3201 | MIN $M_z$ | 2.95 | 0.19 | 0.14 | 0.03 | 16.88 | ▷ -0.60 | BC 253 |
| | **Doorgaande staven No. 38: Doorgaande staven 38** | | | | | | | | | | |
| 8 | RC1 | 46 | 0 | Max N | ▷ 3.39 | -0.13 | 7.22 | -0.02 | 0.00 | 0.00 | BC 358 |
| | | | | Min N | ▷ -3.62 | -0.03 | 16.35 | 0.01 | 0.00 | 0.00 | BC 265 |
| | | | | Max $V_y$ | 0.98 | ▷ 0.12 | 7.21 | 0.02 | 0.00 | 0.00 | BC 472 |
| | | | | Min $V_y$ | 2.90 | ▷ -0.15 | 16.35 | -0.02 | -0.00 | 0.00 | BC 242 |
| | | | | Max $V_z$ | -1.41 | -0.04 | ▷ 32.49 | -0.00 | 0.00 | 0.00 | BC 138 |
| | | | | Min $V_z$ | 1.18 | 0.02 | ▷ 7.21 | 0.01 | 0.00 | 0.00 | BC 443 |
| | | | | Max $M_T$ | 0.99 | 0.12 | 7.21 | ▷ 0.02 | 0.00 | 0.00 | BC 412 |
| | | | | Min $M_T$ | 2.90 | -0.15 | 16.35 | ▷ -0.02 | -0.00 | 0.00 | BC 242 |
| | | | | Max $M_y$ | 3.07 | -0.14 | 12.98 | -0.02 | ▷ 0.00 | 0.00 | BC 434 |
| | | | | Min $M_y$ | -0.82 | -0.02 | 18.75 | -0.00 | ▷ -0.00 | 0.00 | BC 304 |
| | | | | Max $M_z$ | -0.53 | -0.02 | 11.95 | -0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.53 | -0.02 | 11.95 | -0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | 163 | 3267 | Max N | ▷ 3.66 | -0.13 | 0.08 | -0.02 | 11.92 | 0.44 | BC 358 |
| | | | | Min N | ▷ -3.02 | -0.03 | 0.09 | 0.01 | 26.85 | 0.09 | BC 265 |
| | | | | Max $V_y$ | 1.24 | ▷ 0.12 | 0.08 | 0.02 | 11.91 | -0.39 | BC 472 |
| | | | | Min $V_y$ | 3.51 | ▷ -0.15 | 0.09 | -0.02 | 26.86 | 0.49 | BC 242 |
| | | | | Max $V_z$ | -0.09 | -0.02 | ▷ 0.13 | -0.00 | 19.73 | 0.06 | BC 17 |
| | | | | Min $V_z$ | -0.24 | -0.04 | ▷ -0.01 | -0.00 | 47.56 | 0.12 | BC 339 |
| | | | | Max $M_T$ | 1.25 | 0.12 | 0.08 | ▷ 0.02 | 11.91 | -0.39 | BC 412 |
| | | | | Min $M_T$ | 3.51 | -0.15 | 0.09 | ▷ -0.02 | 26.86 | 0.49 | BC 242 |
| | | | | Max $M_y$ | -0.21 | -0.04 | 0.03 | -0.00 | ▷ 53.13 | 0.13 | BC 138 |
| | | | | Min $M_y$ | 1.45 | 0.02 | 0.08 | 0.01 | ▷ 11.91 | -0.07 | BC 443 |
| | | | | Max $M_z$ | 3.51 | -0.15 | 0.09 | -0.02 | 26.86 | ▷ 0.49 | BC 242 |
| | | | | Min $M_z$ | 1.24 | 0.12 | 0.08 | 0.02 | 11.91 | ▷ -0.39 | BC 472 |
| | | 163 | 3267 | Max N | ▷ 3.66 | -0.13 | 0.08 | -0.02 | 11.92 | 0.44 | BC 358 |
| | | 46 | 0 | Min N | ▷ -3.62 | -0.03 | 16.35 | 0.01 | 0.00 | 0.00 | BC 265 |
| | | 46 | 0 | Max $V_y$ | 0.98 | ▷ 0.12 | 7.21 | 0.02 | 0.00 | 0.00 | BC 472 |
| | | 46 | 0 | Min $V_y$ | 2.90 | ▷ -0.15 | 16.35 | -0.02 | -0.00 | 0.00 | BC 242 |
| | | 46 | 0 | Max $V_z$ | -1.41 | -0.04 | ▷ 32.49 | -0.00 | 0.00 | 0.00 | BC 138 |
| | | 163 | 3267 | Min $V_z$ | -0.24 | -0.04 | ▷ -0.01 | -0.00 | 47.56 | 0.12 | BC 339 |
| | | 46 | 0 | Max $M_T$ | 0.99 | 0.12 | 7.21 | ▷ 0.02 | 0.00 | 0.00 | BC 412 |
| | | 46 | 0 | Min $M_T$ | 2.90 | -0.15 | 16.35 | ▷ -0.02 | -0.00 | 0.00 | BC 242 |
| | | 163 | 3267 | Max $M_y$ | -0.21 | -0.04 | 0.03 | -0.00 | ▷ 53.13 | 0.13 | BC 138 |
| | | 46 | 0 | Min $M_y$ | -0.82 | -0.02 | 18.75 | -0.00 | ▷ -0.00 | 0.00 | BC 304 |
| | | 163 | 3267 | Max $M_z$ | 3.51 | -0.15 | 0.09 | -0.02 | 26.86 | ▷ 0.49 | BC 242 |
| | | 163 | 3267 | Min $M_z$ | 1.24 | 0.12 | 0.08 | 0.02 | 11.91 | ▷ -0.39 | BC 472 |
| 201 | RC1 | 163 | 0 | Max N | ▷ 3.66 | 0.13 | -0.15 | -0.01 | 12.14 | 0.44 | BC 358 |
| | | | | Min N | ▷ -3.00 | 0.03 | -0.24 | 0.02 | 27.34 | 0.09 | BC 265 |
| | | | | Max $V_y$ | 3.52 | ▷ 0.15 | -0.24 | -0.00 | 27.34 | 0.49 | BC 242 |
| | | | | Min $V_y$ | 1.25 | ▷ -0.12 | -0.15 | 0.01 | 12.15 | -0.39 | BC 472 |
| | | | | Max $V_z$ | 3.66 | 0.13 | ▷ -0.15 | -0.01 | 12.14 | 0.44 | BC 358 |
| | | | | Min $V_z$ | -0.26 | 0.04 | ▷ -0.30 | 0.00 | 54.02 | 0.13 | BC 154 |
| | | | | Max $M_T$ | -2.94 | 0.03 | -0.24 | ▷ 0.02 | 27.34 | 0.10 | BC 245 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 201 | RC1 | | | Min $M_T$ | 3.66 | 0.13 | -0.15 | ▷ -0.01 | 12.14 | 0.44 | BC 362 |
| | | | | Max $M_y$ | -0.26 | 0.04 | -0.30 | 0.00 | ▷ 54.02 | 0.13 | BC 154 |
| | | | | Min $M_y$ | 3.66 | 0.13 | -0.15 | -0.01 | ▷ 12.14 | 0.44 | BC 358 |
| | | | | Max $M_z$ | 3.52 | 0.15 | -0.24 | -0.00 | 27.34 | ▷ 0.49 | BC 242 |
| | | | | Min $M_z$ | 1.25 | -0.12 | -0.15 | 0.01 | 12.15 | ▷ -0.39 | BC 472 |
| | | 39 | 3267 | Max N | ▷ 4.23 | 0.14 | -16.50 | -0.00 | 0.00 | 0.00 | BC 202 |
| | | | | Min N | ▷ -2.68 | 0.02 | -7.29 | 0.02 | 0.00 | 0.00 | BC 469 |
| | | | | Max $V_y$ | 4.13 | ▷ 0.15 | -16.50 | -0.00 | -0.00 | 0.00 | BC 242 |
| | | | | Min $V_y$ | 1.52 | ▷ -0.12 | -7.29 | 0.01 | 0.00 | 0.00 | BC 472 |
| | | | | Max $V_z$ | 3.93 | 0.13 | ▷ -7.29 | -0.01 | 0.00 | 0.00 | BC 358 |
| | | | | Min $V_z$ | 0.94 | 0.04 | ▷ -32.76 | 0.00 | 0.00 | 0.00 | BC 147 |
| | | | | Max $M_T$ | -2.34 | 0.03 | -16.50 | ▷ 0.02 | 0.00 | 0.00 | BC 245 |
| | | | | Min $M_T$ | 3.93 | 0.13 | -7.29 | ▷ -0.01 | 0.00 | 0.00 | BC 362 |
| | | | | Max $M_y$ | 0.45 | 0.02 | -17.87 | 0.00 | ▷ 0.00 | 0.00 | BC 21 |
| | | | | Min $M_y$ | 0.58 | 0.02 | -18.90 | 0.00 | ▷ -0.00 | 0.00 | BC 304 |
| | | | | Max $M_z$ | 0.37 | 0.02 | -12.06 | 0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.37 | 0.02 | -12.06 | 0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | 39 | 3267 | Max N | ▷ 4.23 | 0.14 | -16.50 | -0.00 | 0.00 | 0.00 | BC 202 |
| | | 163 | 0 | Min N | ▷ -3.00 | 0.03 | -0.24 | 0.02 | 27.34 | 0.09 | BC 265 |
| | | 163 | 0 | Max $V_y$ | 3.52 | ▷ 0.15 | -0.24 | -0.00 | 27.34 | 0.49 | BC 242 |
| | | 163 | 0 | Min $V_y$ | 1.25 | ▷ -0.12 | -0.15 | 0.01 | 12.15 | -0.39 | BC 472 |
| | | 163 | 0 | Max $V_z$ | 3.66 | 0.13 | ▷ -0.15 | -0.01 | 12.14 | 0.44 | BC 358 |
| | | 39 | 3267 | Min $V_z$ | 0.94 | 0.04 | ▷ -32.76 | 0.00 | 0.00 | 0.00 | BC 147 |
| | | 163 | 0 | Max $M_T$ | -2.94 | 0.03 | -0.24 | ▷ 0.02 | 27.34 | 0.10 | BC 245 |
| | | 163 | 0 | Min $M_T$ | 3.66 | 0.13 | -0.15 | ▷ -0.01 | 12.14 | 0.44 | BC 362 |
| | | 163 | 0 | Max $M_y$ | -0.26 | 0.04 | -0.30 | 0.00 | ▷ 54.02 | 0.13 | BC 154 |
| | | 39 | 3267 | Min $M_y$ | 0.58 | 0.02 | -18.90 | 0.00 | ▷ -0.00 | 0.00 | BC 304 |
| | | 163 | 0 | Max $M_z$ | 3.52 | 0.15 | -0.24 | -0.00 | 27.34 | ▷ 0.49 | BC 242 |
| | | 163 | 0 | Min $M_z$ | 1.25 | -0.12 | -0.15 | 0.01 | 12.15 | ▷ -0.39 | BC 472 |
| 201 | RC1 | 39 | 3267 | MAX N | ▷ 4.23 | 0.14 | -16.50 | 0.00 | 0.00 | 0.00 | BC 202 |
| 8 | RC1 | 46 | 0 | MIN N | ▷ -3.62 | -0.03 | 16.35 | 0.01 | 0.00 | 0.00 | BC 265 |
| 201 | RC1 | 163 | 0 | MAX $V_y$ | 3.52 | ▷ 0.15 | -0.24 | 0.00 | 27.34 | 0.49 | BC 242 |
| 8 | RC1 | 46 | 0 | MIN $V_y$ | 2.90 | ▷ -0.15 | 16.35 | -0.02 | 0.00 | 0.00 | BC 242 |
| 8 | RC1 | 46 | 0 | MAX $V_z$ | -1.41 | -0.04 | ▷ 32.49 | 0.00 | 0.00 | 0.00 | BC 138 |
| 201 | RC1 | 39 | 3267 | MIN $V_z$ | 0.94 | 0.04 | ▷ -32.76 | 0.00 | 0.00 | 0.00 | BC 147 |
| 8 | RC1 | 46 | 0 | MAX $M_T$ | 0.99 | 0.12 | 7.21 | ▷ 0.02 | 0.00 | 0.00 | BC 412 |
| 8 | RC1 | 46 | 0 | MIN $M_T$ | 2.90 | -0.15 | 16.35 | ▷ -0.02 | 0.00 | 0.00 | BC 242 |
| 201 | RC1 | 163 | 0 | MAX $M_y$ | -0.26 | 0.04 | -0.30 | 0.00 | ▷ 54.02 | 0.13 | BC 154 |
| 201 | RC1 | 39 | 3267 | MIN $M_y$ | 0.58 | 0.02 | -18.90 | 0.00 | ▷ 0.00 | 0.00 | BC 304 |
| 8 | RC1 | 163 | 3267 | MAX $M_z$ | 3.51 | -0.15 | 0.09 | -0.02 | 26.86 | ▷ 0.49 | BC 242 |
| 8 | RC1 | 163 | 3267 | MIN $M_z$ | 1.24 | 0.12 | 0.08 | 0.02 | 11.91 | ▷ -0.39 | BC 472 |
| | **Doorgaande staven No. 39: Doorgaande staven 39** | | | | | | | | | | |
| 38 | RC1 | 39 | 0 | Max N | ▷ 4.10 | -0.30 | 16.85 | -0.02 | 0.00 | 0.00 | BC 202 |
| | | | | Min N | ▷ -41.03 | 0.14 | 11.07 | 0.01 | -0.00 | 0.00 | BC 164 |
| | | | | Max $V_y$ | -39.50 | ▷ 0.17 | 7.54 | 0.01 | 0.00 | 0.00 | BC 384 |
| | | | | Min $V_y$ | 3.25 | ▷ -0.31 | 7.55 | -0.02 | 0.00 | 0.00 | BC 446 |
| | | | | Max $V_z$ | 0.50 | -0.20 | ▷ 33.01 | -0.01 | 0.00 | 0.00 | BC 148 |
| | | | | Min $V_z$ | -40.77 | 0.16 | ▷ 7.54 | 0.01 | 0.00 | -0.00 | BC 356 |
| | | | | Max $M_T$ | -39.50 | 0.17 | 7.54 | ▷ 0.01 | 0.00 | 0.00 | BC 384 |
| | | | | Min $M_T$ | 3.25 | -0.31 | 7.55 | ▷ -0.02 | 0.00 | 0.00 | BC 446 |
| | | | | Max $M_y$ | 0.53 | -0.20 | 33.01 | -0.01 | ▷ 0.00 | 0.00 | BC 155 |
| | | | | Min $M_y$ | -38.84 | 0.11 | 16.84 | 0.01 | ▷ -0.00 | 0.00 | BC 268 |
| | | | | Max $M_z$ | -39.26 | 0.07 | 16.85 | 0.00 | 0.00 | ▷ 0.00 | BC 205 |
| | | | | Min $M_z$ | -40.77 | 0.16 | 7.54 | 0.01 | 0.00 | ▷ -0.00 | BC 356 |
| | | 156 | 3256 | Max N | ▷ 3.80 | -0.30 | 0.64 | -0.02 | 28.46 | 0.99 | BC 202 |
| | | | | Min N | ▷ -41.22 | 0.14 | 0.63 | 0.01 | 19.04 | -0.45 | BC 164 |
| | | | | Max $V_y$ | -39.64 | ▷ 0.17 | 0.43 | 0.01 | 12.97 | -0.54 | BC 384 |
| | | | | Min $V_y$ | 3.11 | ▷ -0.31 | 0.44 | -0.02 | 13.01 | 1.02 | BC 446 |
| | | | | Max $V_z$ | 0.07 | -0.13 | ▷ 0.72 | -0.01 | 30.92 | 0.41 | BC 21 |
| | | | | Min $V_z$ | -39.89 | 0.13 | ▷ 0.43 | 0.01 | 22.37 | -0.42 | BC 392 |
| | | | | Max $M_T$ | -39.64 | 0.17 | 0.43 | ▷ 0.01 | 12.97 | -0.54 | BC 384 |
| | | | | Min $M_T$ | 3.11 | -0.31 | 0.44 | ▷ -0.02 | 13.01 | 1.02 | BC 446 |
| | | | | Max $M_y$ | -0.11 | -0.20 | 0.64 | -0.01 | ▷ 54.77 | 0.67 | BC 148 |
| | | | | Min $M_y$ | -40.90 | 0.16 | 0.43 | 0.01 | ▷ 12.97 | -0.51 | BC 356 |
| | | | | Max $M_z$ | 3.11 | -0.31 | 0.44 | -0.02 | 13.01 | ▷ 1.02 | BC 446 |
| | | | | Min $M_z$ | -39.64 | 0.17 | 0.43 | 0.01 | 12.97 | ▷ -0.54 | BC 384 |
| | | 39 | 0 | Max N | ▷ 4.10 | -0.30 | 16.85 | -0.02 | 0.00 | 0.00 | BC 202 |
| | | 156 | 3256 | Min N | ▷ -41.22 | 0.14 | 0.63 | 0.01 | 19.04 | -0.45 | BC 164 |
| | | 39 | 0 | Max $V_y$ | -39.50 | ▷ 0.17 | 7.54 | 0.01 | 0.00 | 0.00 | BC 384 |
| | | 39 | 0 | Min $V_y$ | 3.25 | ▷ -0.31 | 7.55 | -0.02 | 0.00 | 0.00 | BC 446 |
| | | 39 | 0 | Max $V_z$ | 0.50 | -0.20 | ▷ 33.01 | -0.01 | 0.00 | 0.00 | BC 148 |
| | | 156 | 3256 | Min $V_z$ | -39.89 | 0.13 | ▷ 0.43 | 0.01 | 22.37 | -0.42 | BC 392 |
| | | 39 | 0 | Max $M_T$ | -39.50 | 0.17 | 7.54 | ▷ 0.01 | 0.00 | 0.00 | BC 384 |
| | | 39 | 0 | Min $M_T$ | 3.25 | -0.31 | 7.55 | ▷ -0.02 | 0.00 | 0.00 | BC 446 |
| | | 156 | 3256 | Max $M_y$ | -0.11 | -0.20 | 0.64 | -0.01 | ▷ 54.77 | 0.67 | BC 148 |
| | | 39 | 0 | Min $M_y$ | -38.84 | 0.11 | 16.84 | 0.01 | ▷ -0.00 | 0.00 | BC 268 |
| | | 156 | 3256 | Max $M_z$ | 3.11 | -0.31 | 0.44 | -0.02 | 13.01 | ▷ 1.02 | BC 446 |
| | | 156 | 3256 | Min $M_z$ | -39.64 | 0.17 | 0.43 | 0.01 | 12.97 | ▷ -0.54 | BC 384 |
| 194 | RC1 | 156 | 0 | Max N | ▷ 3.79 | 0.30 | -0.64 | 0.02 | 28.46 | 0.99 | BC 202 |
| | | | | Min N | ▷ -41.26 | -0.14 | -0.63 | -0.01 | 19.05 | -0.45 | BC 164 |
| | | | | Max $V_y$ | 3.11 | ▷ 0.31 | -0.44 | 0.02 | 13.00 | 1.02 | BC 446 |
| | | | | Min $V_y$ | -39.68 | ▷ -0.17 | -0.43 | -0.01 | 12.98 | -0.54 | BC 384 |
| | | | | Max $V_z$ | -40.08 | -0.10 | ▷ -0.42 | -0.01 | 22.37 | -0.32 | BC 397 |
| | | | | Min $V_z$ | 0.01 | 0.10 | ▷ -0.72 | 0.01 | 21.52 | 0.32 | BC 1 |
| | | | | Max $M_T$ | 3.11 | 0.31 | -0.44 | ▷ 0.02 | 13.00 | 1.02 | BC 446 |
| | | | | Min $M_T$ | -39.31 | -0.12 | -0.43 | ▷ -0.01 | 12.97 | -0.39 | BC 409 |
| | | | | Max $M_y$ | 0.07 | 0.20 | -0.63 | 0.01 | ▷ 54.76 | 0.67 | BC 146 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 194 | RC1 | | | Min $M_y$ | -39.31 | -0.12 | -0.43 | -0.01 | ▷ 12.97 | -0.39 | BC 409 |
| | | | | Max $M_z$ | 3.11 | 0.31 | -0.44 | 0.02 | 13.00 | ▷ 1.02 | BC 446 |
| | | | | Min $M_z$ | -39.68 | -0.17 | -0.43 | -0.01 | 12.98 | ▷ -0.54 | BC 384 |
| | | 35 | 3256 | Max N | ▷ 3.49 | 0.30 | -16.85 | 0.02 | 0.00 | 0.00 | BC 202 |
| | | | | Min N | ▷ -41.46 | -0.14 | -11.07 | -0.01 | -0.00 | 0.00 | BC 164 |
| | | | | Max $V_y$ | 2.98 | ▷ 0.31 | -7.55 | 0.02 | 0.00 | 0.00 | BC 446 |
| | | | | Min $V_y$ | -39.81 | ▷ -0.17 | -7.55 | -0.01 | -0.00 | 0.00 | BC 384 |
| | | | | Max $V_z$ | -39.45 | -0.12 | ▷ -7.54 | -0.01 | 0.00 | 0.00 | BC 409 |
| | | | | Min $V_z$ | -0.54 | 0.20 | ▷ -33.01 | 0.01 | 0.00 | 0.00 | BC 146 |
| | | | | Max $M_T$ | 2.98 | 0.31 | -7.55 | ▷ 0.02 | 0.00 | 0.00 | BC 446 |
| | | | | Min $M_T$ | -39.45 | -0.12 | -7.54 | ▷ -0.01 | 0.00 | 0.00 | BC 409 |
| | | | | Max $M_y$ | -0.70 | 0.20 | -33.01 | 0.01 | ▷ 0.00 | 0.00 | BC 155 |
| | | | | Min $M_y$ | -39.49 | -0.11 | -16.84 | -0.01 | ▷ -0.00 | 0.00 | BC 268 |
| | | | | Max $M_z$ | -39.84 | -0.07 | -16.84 | -0.01 | 0.00 | ▷ 0.00 | BC 205 |
| | | | | Min $M_z$ | -41.07 | -0.16 | -7.55 | -0.01 | 0.00 | ▷ -0.00 | BC 356 |
| | | 156 | 0 | Max N | ▷ 3.79 | 0.30 | -0.64 | 0.02 | 28.46 | 0.99 | BC 202 |
| | | 35 | 3256 | Min N | ▷ -41.46 | -0.14 | -11.07 | -0.01 | -0.00 | 0.00 | BC 164 |
| | | 156 | 0 | Max $V_y$ | 3.11 | ▷ 0.31 | -0.44 | 0.02 | 13.00 | 1.02 | BC 446 |
| | | 156 | 0 | Min $V_y$ | -39.68 | ▷ -0.17 | -0.43 | -0.01 | 12.98 | -0.54 | BC 384 |
| | | 156 | 0 | Max $V_z$ | -40.08 | -0.10 | ▷ -0.42 | -0.01 | 22.37 | -0.32 | BC 397 |
| | | 35 | 3256 | Min $V_z$ | -0.54 | 0.20 | ▷ -33.01 | 0.01 | 0.00 | 0.00 | BC 146 |
| | | 156 | 0 | Max $M_T$ | 3.11 | 0.31 | -0.44 | ▷ 0.02 | 13.00 | 1.02 | BC 446 |
| | | 156 | 0 | Min $M_T$ | -39.31 | -0.12 | -0.43 | ▷ -0.01 | 12.97 | -0.39 | BC 409 |
| | | 156 | 0 | Max $M_y$ | 0.07 | 0.20 | -0.63 | 0.01 | ▷ 54.76 | 0.67 | BC 146 |
| | | 35 | 3256 | Min $M_y$ | -39.49 | -0.11 | -16.84 | -0.01 | ▷ -0.00 | 0.00 | BC 268 |
| | | 156 | 0 | Max $M_z$ | 3.11 | 0.31 | -0.44 | 0.02 | 13.00 | ▷ 1.02 | BC 446 |
| | | 156 | 0 | Min $M_z$ | -39.68 | -0.17 | -0.43 | -0.01 | 12.98 | ▷ -0.54 | BC 384 |
| 38 | RC1 | 39 | 0 | MAX N | ▷ 4.10 | -0.30 | 16.85 | -0.02 | 0.00 | 0.00 | BC 202 |
| 194 | RC1 | 35 | 3256 | MIN N | ▷ -41.46 | -0.14 | -11.07 | -0.01 | 0.00 | 0.00 | BC 164 |
| 194 | RC1 | 156 | 0 | MAX $V_y$ | 3.11 | ▷ 0.31 | -0.44 | 0.02 | 13.00 | 1.02 | BC 446 |
| 38 | RC1 | 39 | 0 | MIN $V_y$ | 3.25 | ▷ -0.31 | 7.55 | -0.02 | 0.00 | 0.00 | BC 446 |
| 38 | RC1 | 39 | 0 | MAX $V_z$ | 0.50 | -0.20 | ▷ 33.01 | -0.01 | 0.00 | 0.00 | BC 148 |
| 194 | RC1 | 35 | 3256 | MIN $V_z$ | -0.54 | 0.20 | ▷ -33.01 | 0.01 | 0.00 | 0.00 | BC 146 |
| 194 | RC1 | 156 | 0 | MAX $M_T$ | 3.11 | 0.31 | -0.44 | ▷ 0.02 | 13.00 | 1.02 | BC 446 |
| 38 | RC1 | 39 | 0 | MIN $M_T$ | 3.25 | -0.31 | 7.55 | ▷ -0.02 | 0.00 | 0.00 | BC 446 |
| 38 | RC1 | 156 | 3256 | MAX $M_y$ | -0.11 | -0.20 | 0.64 | -0.01 | ▷ 54.77 | 0.67 | BC 148 |
| 38 | RC1 | 39 | 0 | MIN $M_y$ | -38.84 | 0.11 | 16.84 | 0.01 | ▷ 0.00 | 0.00 | BC 268 |
| 194 | RC1 | 156 | 0 | MAX $M_z$ | 3.11 | 0.31 | -0.44 | 0.02 | 13.00 | ▷ 1.02 | BC 446 |
| 194 | RC1 | 156 | 0 | MIN $M_z$ | -39.68 | -0.17 | -0.43 | -0.01 | 12.98 | ▷ -0.54 | BC 384 |
| | **Doorgaande staven No. 40: Doorgaande staven 40** | | | | | | | | | | |
| 7 | RC1 | 45 | 0 | Max N | ▷ 3.51 | 0.12 | 7.08 | 0.02 | 0.00 | 0.00 | BC 390 |
| | | | | Min N | ▷ -3.36 | 0.02 | 16.03 | -0.01 | 0.00 | 0.00 | BC 240 |
| | | | | Max $V_y$ | 3.27 | ▷ 0.13 | 16.03 | 0.02 | 0.00 | 0.00 | BC 234 |
| | | | | Min $V_y$ | 1.16 | ▷ -0.11 | 7.08 | -0.02 | 0.00 | 0.00 | BC 409 |
| | | | | Max $V_z$ | -0.79 | 0.05 | ▷ 31.86 | 0.00 | 0.00 | 0.00 | BC 138 |
| | | | | Min $V_z$ | -3.12 | 0.00 | ▷ 7.07 | -0.02 | 0.00 | 0.00 | BC 440 |
| | | | | Max $M_T$ | 3.27 | 0.13 | 16.03 | ▷ 0.02 | 0.00 | 0.00 | BC 234 |
| | | | | Min $M_T$ | 1.16 | -0.11 | 7.08 | ▷ -0.02 | 0.00 | 0.00 | BC 409 |
| | | | | Max $M_y$ | -0.46 | 0.03 | 18.38 | 0.00 | ▷ 0.00 | 0.00 | BC 304 |
| | | | | Min $M_y$ | -0.55 | 0.03 | 17.37 | 0.00 | ▷ -0.00 | 0.00 | BC 21 |
| | | | | Max $M_z$ | -0.37 | 0.02 | 11.71 | 0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.37 | 0.02 | 11.71 | 0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | 150 | 3201 | Max N | ▷ 3.64 | 0.12 | 0.08 | 0.02 | 11.45 | -0.39 | BC 390 |
| | | | | Min N | ▷ -3.06 | 0.02 | 0.09 | -0.01 | 25.79 | -0.05 | BC 240 |
| | | | | Max $V_y$ | 3.57 | ▷ 0.13 | 0.09 | 0.02 | 25.80 | -0.42 | BC 234 |
| | | | | Min $V_y$ | 1.29 | ▷ -0.11 | 0.08 | -0.02 | 11.45 | 0.36 | BC 409 |
| | | | | Max $V_z$ | -0.13 | 0.02 | ▷ 0.13 | 0.00 | 18.95 | -0.06 | BC 17 |
| | | | | Min $V_z$ | -0.26 | 0.04 | ▷ -0.01 | 0.00 | 45.68 | -0.13 | BC 340 |
| | | | | Max $M_T$ | 3.57 | 0.13 | 0.09 | ▷ 0.02 | 25.80 | -0.42 | BC 234 |
| | | | | Min $M_T$ | 1.29 | -0.11 | 0.08 | ▷ -0.02 | 11.45 | 0.36 | BC 409 |
| | | | | Max $M_y$ | -0.19 | 0.05 | 0.03 | 0.00 | ▷ 51.03 | -0.15 | BC 138 |
| | | | | Min $M_y$ | -2.99 | 0.00 | 0.07 | -0.02 | ▷ 11.44 | -0.01 | BC 440 |
| | | | | Max $M_z$ | 1.29 | -0.11 | 0.08 | -0.02 | 11.45 | ▷ 0.36 | BC 409 |
| | | | | Min $M_z$ | 3.57 | 0.13 | 0.09 | 0.02 | 25.80 | ▷ -0.42 | BC 234 |
| | | 150 | 3201 | Max N | ▷ 3.64 | 0.12 | 0.08 | 0.02 | 11.45 | -0.39 | BC 390 |
| | | 45 | 0 | Min N | ▷ -3.36 | 0.02 | 16.03 | -0.01 | 0.00 | 0.00 | BC 240 |
| | | 45 | 0 | Max $V_y$ | 3.27 | ▷ 0.13 | 16.03 | 0.02 | 0.00 | 0.00 | BC 234 |
| | | 45 | 0 | Min $V_y$ | 1.16 | ▷ -0.11 | 7.08 | -0.02 | 0.00 | 0.00 | BC 409 |
| | | 45 | 0 | Max $V_z$ | -0.79 | 0.05 | ▷ 31.86 | 0.00 | 0.00 | 0.00 | BC 138 |
| | | 150 | 3201 | Min $V_z$ | -0.26 | 0.04 | ▷ -0.01 | 0.00 | 45.68 | -0.13 | BC 340 |
| | | 45 | 0 | Max $M_T$ | 3.27 | 0.13 | 16.03 | ▷ 0.02 | 0.00 | 0.00 | BC 234 |
| | | 45 | 0 | Min $M_T$ | 1.16 | -0.11 | 7.08 | ▷ -0.02 | 0.00 | 0.00 | BC 409 |
| | | 150 | 3201 | Max $M_y$ | -0.19 | 0.05 | 0.03 | 0.00 | ▷ 51.03 | -0.15 | BC 138 |
| | | 45 | 0 | Min $M_y$ | -0.55 | 0.03 | 17.37 | 0.00 | ▷ -0.00 | 0.00 | BC 21 |
| | | 150 | 3201 | Max $M_z$ | 1.29 | -0.11 | 0.08 | -0.02 | 11.45 | ▷ 0.36 | BC 409 |
| | | 150 | 3201 | Min $M_z$ | 3.57 | 0.13 | 0.09 | 0.02 | 25.80 | ▷ -0.42 | BC 234 |
| 188 | RC1 | 150 | 0 | Max N | ▷ 3.65 | -0.12 | -0.15 | 0.01 | 11.68 | -0.39 | BC 390 |
| | | | | Min N | ▷ -3.05 | -0.02 | -0.24 | -0.02 | 26.29 | -0.05 | BC 240 |
| | | | | Max $V_y$ | 1.29 | ▷ 0.11 | -0.15 | -0.01 | 11.68 | 0.36 | BC 409 |
| | | | | Min $V_y$ | 3.58 | ▷ -0.13 | -0.24 | 0.01 | 26.28 | -0.42 | BC 234 |
| | | | | Max $V_z$ | 1.37 | 0.11 | ▷ -0.15 | -0.01 | 11.67 | 0.35 | BC 417 |
| | | | | Min $V_z$ | -0.28 | -0.05 | ▷ -0.31 | -0.00 | 51.91 | -0.14 | BC 148 |
| | | | | Max $M_T$ | 3.56 | -0.11 | -0.15 | ▷ 0.01 | 11.68 | -0.36 | BC 474 |
| | | | | Min $M_T$ | -2.96 | -0.02 | -0.24 | ▷ -0.02 | 26.28 | -0.06 | BC 200 |
| | | | | Max $M_y$ | -0.28 | -0.05 | -0.31 | -0.00 | ▷ 51.91 | -0.14 | BC 148 |
| | | | | Min $M_y$ | 1.37 | 0.11 | -0.15 | -0.01 | ▷ 11.67 | 0.35 | BC 417 |
| | | | | Max $M_z$ | 1.29 | 0.11 | -0.15 | -0.01 | 11.68 | ▷ 0.36 | BC 409 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 188 | RC1 | | | Min $M_z$ | 3.58 | -0.13 | -0.24 | 0.01 | 26.28 | -0.42 | BC 234 |
| | | 35 | 3201 | Max N | 3.90 | -0.13 | -16.18 | 0.01 | 0.00 | 0.00 | BC 186 |
| | | | | Min N | -2.85 | -0.00 | -7.15 | -0.02 | 0.00 | 0.00 | BC 444 |
| | | | | Max $V_y$ | 1.42 | 0.11 | -7.15 | -0.01 | 0.00 | 0.00 | BC 409 |
| | | | | Min $V_y$ | 3.87 | -0.13 | -16.18 | 0.01 | 0.00 | 0.00 | BC 234 |
| | | | | Max $V_z$ | 1.50 | 0.11 | -7.15 | -0.01 | 0.00 | 0.00 | BC 417 |
| | | | | Min $V_z$ | 0.31 | -0.05 | -32.14 | -0.00 | 0.00 | 0.00 | BC 148 |
| | | | | Max $M_T$ | 3.69 | -0.11 | -7.15 | 0.01 | 0.00 | 0.00 | BC 474 |
| | | | | Min $M_T$ | -2.66 | -0.02 | -16.18 | -0.02 | 0.00 | 0.00 | BC 200 |
| | | | | Max $M_y$ | 0.24 | -0.03 | -18.54 | -0.00 | 0.00 | 0.00 | BC 304 |
| | | | | Min $M_y$ | 0.11 | -0.03 | -17.53 | -0.00 | -0.00 | 0.00 | BC 21 |
| | | | | Max $M_z$ | 0.07 | -0.02 | -11.83 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.07 | -0.02 | -11.83 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | 35 | 3201 | Max N | 3.90 | -0.13 | -16.18 | 0.01 | 0.00 | 0.00 | BC 186 |
| | | 150 | 0 | Min N | -3.05 | -0.02 | -0.24 | -0.02 | 26.29 | -0.05 | BC 240 |
| | | 150 | 0 | Max $V_y$ | 1.29 | 0.11 | -0.15 | -0.01 | 11.68 | 0.36 | BC 409 |
| | | 150 | 0 | Min $V_y$ | 3.58 | -0.13 | -0.24 | 0.01 | 26.28 | -0.42 | BC 234 |
| | | 150 | 0 | Max $V_z$ | 1.37 | 0.11 | -0.15 | -0.01 | 11.67 | 0.35 | BC 417 |
| | | 35 | 3201 | Min $V_z$ | 0.31 | -0.05 | -32.14 | -0.00 | 0.00 | 0.00 | BC 148 |
| | | 150 | 0 | Max $M_T$ | 3.56 | -0.11 | -0.15 | 0.01 | 11.68 | -0.36 | BC 474 |
| | | 150 | 0 | Min $M_T$ | -2.96 | -0.02 | -0.24 | -0.02 | 26.28 | -0.06 | BC 200 |
| | | 150 | 0 | Max $M_y$ | -0.28 | -0.05 | -0.31 | -0.00 | 51.91 | -0.14 | BC 148 |
| | | 35 | 3201 | Min $M_y$ | 0.11 | -0.03 | -17.53 | -0.00 | -0.00 | 0.00 | BC 21 |
| | | 150 | 0 | Max $M_z$ | 1.29 | 0.11 | -0.15 | -0.01 | 11.68 | 0.36 | BC 409 |
| | | 150 | 0 | Min $M_z$ | 3.58 | -0.13 | -0.24 | 0.01 | 26.28 | -0.42 | BC 234 |
| 188 | RC1 | 35 | 3201 | MAX N | 3.90 | -0.13 | -16.18 | 0.01 | 0.00 | 0.00 | BC 186 |
| 7 | RC1 | 45 | 0 | MIN N | -3.36 | 0.02 | 16.03 | -0.01 | 0.00 | 0.00 | BC 240 |
| 7 | RC1 | 45 | 0 | MAX $V_y$ | 3.27 | 0.13 | 16.03 | 0.02 | 0.00 | 0.00 | BC 234 |
| 188 | RC1 | 150 | 0 | MIN $V_y$ | 3.58 | -0.13 | -0.24 | 0.01 | 26.28 | -0.42 | BC 234 |
| 7 | RC1 | 45 | 0 | MAX $V_z$ | -0.79 | 0.05 | 31.86 | 0.00 | 0.00 | 0.00 | BC 138 |
| 188 | RC1 | 35 | 3201 | MIN $V_z$ | 0.31 | -0.05 | -32.14 | 0.00 | 0.00 | 0.00 | BC 148 |
| 7 | RC1 | 45 | 0 | MAX $M_T$ | 3.27 | 0.13 | 16.03 | 0.02 | 0.00 | 0.00 | BC 234 |
| 7 | RC1 | 45 | 0 | MIN $M_T$ | 1.16 | -0.11 | 7.08 | -0.02 | 0.00 | 0.00 | BC 409 |
| 188 | RC1 | 150 | 0 | MAX $M_y$ | -0.28 | -0.05 | -0.31 | 0.00 | 51.91 | -0.14 | BC 148 |
| 7 | RC1 | 45 | 0 | MIN $M_y$ | -0.55 | 0.03 | 17.37 | 0.00 | 0.00 | 0.00 | BC 21 |
| 7 | RC1 | 150 | 3201 | MAX $M_z$ | 1.29 | -0.11 | 0.08 | -0.02 | 11.45 | 0.36 | BC 409 |
| 7 | RC1 | 150 | 3201 | MIN $M_z$ | 3.57 | 0.13 | 0.09 | 0.02 | 25.80 | -0.42 | BC 234 |
| | **Doorgaande staven No. 41: Doorgaande staven 41** | | | | | | | | | | |
| 24 | RC1 | 65 | 0 | Max N | 9.46 | 0.03 | 13.78 | -0.00 | 0.00 | 0.00 | BC 362 |
| | | | | Min N | -26.33 | 0.03 | 32.06 | -0.01 | 0.00 | 0.00 | BC 269 |
| | | | | Max $V_y$ | 8.68 | 0.04 | 32.06 | -0.00 | 0.00 | 0.00 | BC 234 |
| | | | | Min $V_y$ | -4.16 | -0.00 | 20.21 | 0.01 | 0.00 | 0.00 | BC 171 |
| | | | | Max $V_z$ | -10.87 | 0.02 | 65.23 | 0.00 | -0.00 | 0.00 | BC 154 |
| | | | | Min $V_z$ | -20.28 | 0.02 | 13.78 | -0.01 | -0.00 | 0.00 | BC 389 |
| | | | | Max $M_T$ | -5.08 | 0.01 | 32.06 | 0.01 | 0.00 | 0.00 | BC 243 |
| | | | | Min $M_T$ | -20.41 | 0.02 | 13.78 | -0.01 | 0.00 | 0.00 | BC 449 |
| | | | | Max $M_y$ | -7.27 | 0.01 | 32.06 | 0.00 | 0.00 | 0.00 | BC 91 |
| | | | | Min $M_y$ | -9.48 | 0.02 | 53.38 | 0.00 | -0.00 | 0.00 | BC 136 |
| | | | | Max $M_z$ | -0.85 | 0.01 | 22.82 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -20.43 | 0.02 | 13.78 | -0.01 | 0.00 | -0.00 | BC 353 |
| | | 158 | 3267 | Max N | 9.95 | 0.03 | 0.55 | -0.00 | 23.41 | -0.10 | BC 362 |
| | | | | Min N | -25.17 | 0.03 | 0.82 | -0.01 | 53.71 | -0.09 | BC 269 |
| | | | | Max $V_y$ | 9.84 | 0.04 | 0.81 | -0.00 | 53.69 | -0.12 | BC 234 |
| | | | | Min $V_y$ | -3.43 | -0.00 | 0.81 | 0.01 | 34.35 | 0.01 | BC 171 |
| | | | | Max $V_z$ | -5.82 | 0.01 | 0.92 | 0.00 | 58.14 | -0.04 | BC 27 |
| | | | | Min $V_z$ | -19.79 | 0.02 | 0.55 | -0.01 | 23.41 | -0.06 | BC 389 |
| | | | | Max $M_T$ | -3.92 | 0.01 | 0.82 | 0.01 | 53.72 | -0.02 | BC 243 |
| | | | | Min $M_T$ | -19.92 | 0.02 | 0.55 | -0.01 | 23.41 | -0.06 | BC 449 |
| | | | | Max $M_y$ | -8.47 | 0.02 | 0.82 | 0.00 | 107.89 | -0.07 | BC 154 |
| | | | | Min $M_y$ | -19.79 | 0.02 | 0.55 | -0.01 | 23.41 | -0.06 | BC 389 |
| | | | | Max $M_z$ | -3.43 | -0.00 | 0.81 | 0.01 | 34.35 | 0.01 | BC 171 |
| | | | | Min $M_z$ | 9.84 | 0.04 | 0.81 | -0.00 | 53.69 | -0.12 | BC 234 |
| | | 158 | 3267 | Max N | 9.95 | 0.03 | 0.55 | -0.00 | 23.41 | -0.10 | BC 362 |
| | | 65 | 0 | Min N | -26.33 | 0.03 | 32.06 | -0.01 | 0.00 | 0.00 | BC 269 |
| | | 65 | 0 | Max $V_y$ | 8.68 | 0.04 | 32.06 | -0.00 | 0.00 | 0.00 | BC 234 |
| | | 65 | 0 | Min $V_y$ | -4.16 | -0.00 | 20.21 | 0.01 | 0.00 | 0.00 | BC 171 |
| | | 65 | 0 | Max $V_z$ | -10.87 | 0.02 | 65.23 | 0.00 | -0.00 | 0.00 | BC 154 |
| | | 158 | 3267 | Min $V_z$ | -19.79 | 0.02 | 0.55 | -0.01 | 23.41 | -0.06 | BC 389 |
| | | 65 | 0 | Max $M_T$ | -5.08 | 0.01 | 32.06 | 0.01 | 0.00 | 0.00 | BC 243 |
| | | 65 | 0 | Min $M_T$ | -20.41 | 0.02 | 13.78 | -0.01 | 0.00 | 0.00 | BC 449 |
| | | 158 | 3267 | Max $M_y$ | -8.47 | 0.02 | 0.82 | 0.00 | 107.89 | -0.07 | BC 154 |
| | | 65 | 0 | Min $M_y$ | -9.48 | 0.02 | 53.38 | 0.00 | -0.00 | 0.00 | BC 136 |
| | | 158 | 3267 | Max $M_z$ | -3.43 | -0.00 | 0.81 | 0.01 | 34.35 | 0.01 | BC 171 |
| | | 158 | 3267 | Min $M_z$ | 9.84 | 0.04 | 0.81 | -0.00 | 53.69 | -0.12 | BC 234 |
| 196 | RC1 | 158 | 0 | Max N | 9.96 | -0.03 | -0.56 | -0.01 | 23.44 | -0.10 | BC 362 |
| | | | | Min N | -25.14 | -0.03 | -0.81 | -0.02 | 53.70 | -0.09 | BC 269 |
| | | | | Max $V_y$ | -3.42 | 0.00 | -0.82 | 0.01 | 34.36 | 0.01 | BC 171 |
| | | | | Min $V_y$ | 9.85 | -0.04 | -0.82 | -0.01 | 53.72 | -0.12 | BC 234 |
| | | | | Max $V_z$ | 9.63 | -0.02 | -0.55 | -0.01 | 42.75 | -0.06 | BC 456 |
| | | | | Min $V_z$ | -0.02 | -0.01 | -0.92 | -0.00 | 38.79 | -0.04 | BC 10 |
| | | | | Max $M_T$ | -3.42 | 0.00 | -0.82 | 0.01 | 34.36 | 0.01 | BC 171 |
| | | | | Min $M_T$ | -25.14 | -0.03 | -0.81 | -0.02 | 53.70 | -0.09 | BC 269 |
| | | | | Max $M_y$ | -4.70 | -0.02 | -0.82 | -0.00 | 107.88 | -0.06 | BC 134 |
| | | | | Min $M_y$ | 9.65 | -0.01 | -0.55 | -0.01 | 23.41 | -0.05 | BC 468 |
| | | | | Max $M_z$ | -3.42 | 0.00 | -0.82 | 0.01 | 34.36 | 0.01 | BC 171 |
| | | | | Min $M_z$ | 9.85 | -0.04 | -0.82 | -0.01 | 53.72 | -0.12 | BC 234 |
| | | 67 | 3267 | Max N | 11.02 | -0.04 | -32.06 | -0.01 | 0.00 | 0.00 | BC 174 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 196 | RC1 | | | Min N | ▷ -23.98 | -0.03 | -32.06 | -0.02 | 0.00 | 0.00 | BC 269 |
| | | | | Max $V_y$ | -2.70 | ▷ 0.00 | -20.22 | 0.01 | 0.00 | 0.00 | BC 171 |
| | | | | Min $V_y$ | 11.02 | ▷ -0.04 | -32.06 | -0.01 | 0.00 | 0.00 | BC 234 |
| | | | | Max $V_z$ | 10.14 | -0.01 | ▷ -13.78 | -0.01 | 0.00 | 0.00 | BC 468 |
| | | | | Min $V_z$ | -2.30 | -0.02 | ▷ -65.22 | -0.00 | -0.00 | 0.00 | BC 134 |
| | | | | Max $M_T$ | -2.70 | 0.00 | -20.22 | ▷ 0.01 | 0.00 | 0.00 | BC 171 |
| | | | | Min $M_T$ | -23.98 | -0.03 | -32.06 | ▷ -0.02 | 0.00 | 0.00 | BC 269 |
| | | | | Max $M_y$ | -4.92 | -0.01 | -32.06 | -0.00 | ▷ 0.00 | 0.00 | BC 91 |
| | | | | Min $M_y$ | -5.54 | -0.02 | -53.37 | -0.00 | ▷ -0.00 | 0.00 | BC 136 |
| | | | | Max $M_z$ | 0.80 | -0.01 | -22.82 | -0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | -19.43 | -0.02 | -13.79 | -0.02 | 0.00 | ▷ -0.00 | BC 353 |
| | | 67 | 3267 | Max N | ▷ 11.02 | -0.04 | -32.06 | -0.01 | 0.00 | 0.00 | BC 174 |
| | | 158 | 0 | Min N | ▷ -25.14 | -0.03 | -0.81 | -0.02 | 53.70 | -0.09 | BC 269 |
| | | 158 | 0 | Max $V_y$ | -3.42 | ▷ 0.00 | -0.82 | 0.01 | 34.36 | 0.01 | BC 171 |
| | | 158 | 0 | Min $V_y$ | 9.85 | ▷ -0.04 | -0.82 | -0.01 | 53.72 | -0.12 | BC 234 |
| | | 158 | 0 | Max $V_z$ | 9.63 | -0.02 | ▷ -0.55 | -0.01 | 42.75 | -0.06 | BC 456 |
| | | 67 | 3267 | Min $V_z$ | -2.30 | -0.02 | ▷ -65.22 | -0.00 | -0.00 | 0.00 | BC 134 |
| | | 158 | 0 | Max $M_T$ | -3.42 | 0.00 | -0.82 | ▷ 0.01 | 34.36 | 0.01 | BC 171 |
| | | 158 | 0 | Min $M_T$ | -25.14 | -0.03 | -0.81 | ▷ -0.02 | 53.70 | -0.09 | BC 269 |
| | | 158 | 0 | Max $M_y$ | -4.70 | -0.02 | -0.82 | -0.00 | ▷ 107.88 | -0.06 | BC 134 |
| | | 67 | 3267 | Min $M_y$ | -5.54 | -0.02 | -53.37 | -0.00 | ▷ -0.00 | 0.00 | BC 136 |
| | | 158 | 0 | Max $M_z$ | -3.42 | 0.00 | -0.82 | 0.01 | 34.36 | ▷ 0.01 | BC 171 |
| | | 158 | 0 | Min $M_z$ | 9.85 | -0.04 | -0.82 | -0.01 | 53.72 | ▷ -0.12 | BC 234 |
| 196 | RC1 | 67 | 3267 | MAX N | ▷ 11.02 | -0.04 | -32.06 | -0.01 | 0.00 | 0.00 | BC 174 |
| 24 | RC1 | 65 | 0 | MIN N | ▷ -26.33 | 0.03 | 32.06 | -0.01 | 0.00 | 0.00 | BC 269 |
| 24 | RC1 | 65 | 0 | MAX $V_y$ | 8.68 | ▷ 0.04 | 32.06 | 0.00 | 0.00 | 0.00 | BC 234 |
| 196 | RC1 | 158 | 0 | MIN $V_y$ | 9.85 | ▷ -0.04 | -0.82 | -0.01 | 53.72 | -0.12 | BC 234 |
| 24 | RC1 | 65 | 0 | MAX $V_z$ | -10.87 | 0.02 | ▷ 65.23 | 0.00 | 0.00 | 0.00 | BC 154 |
| 196 | RC1 | 67 | 3267 | MIN $V_z$ | -2.30 | -0.02 | ▷ -65.22 | 0.00 | 0.00 | 0.00 | BC 134 |
| 24 | RC1 | 65 | 0 | MAX $M_T$ | -5.08 | 0.01 | 32.06 | ▷ 0.01 | 0.00 | 0.00 | BC 243 |
| 196 | RC1 | 158 | 0 | MIN $M_T$ | -25.14 | -0.03 | -0.81 | ▷ -0.02 | 53.70 | -0.09 | BC 269 |
| 24 | RC1 | 158 | 3267 | MAX $M_y$ | -8.47 | 0.02 | 0.82 | 0.00 | ▷ 107.89 | -0.07 | BC 154 |
| 24 | RC1 | 65 | 0 | MIN $M_y$ | -9.48 | 0.02 | 53.38 | 0.00 | ▷ 0.00 | 0.00 | BC 136 |
| 24 | RC1 | 158 | 3267 | MAX $M_z$ | -3.43 | 0.00 | 0.81 | 0.01 | 34.35 | ▷ 0.01 | BC 171 |
| 24 | RC1 | 158 | 3267 | MIN $M_z$ | 9.84 | 0.04 | 0.81 | 0.00 | 53.69 | ▷ -0.12 | BC 234 |
| | **Doorgaande staven No. 42: Doorgaande staven 42** | | | | | | | | | | |
| 20 | RC1 | 63 | 0 | Max N | ▷ 4.24 | -0.05 | 8.55 | 0.01 | -0.00 | 0.00 | BC 363 |
| | | | | Min N | ▷ -29.91 | 0.05 | 14.88 | -0.01 | 0.00 | 0.00 | BC 436 |
| | | | | Max $V_y$ | -25.20 | ▷ 0.06 | 18.87 | -0.01 | -0.00 | 0.00 | BC 204 |
| | | | | Min $V_y$ | 2.21 | ▷ -0.05 | 8.55 | 0.01 | 0.00 | 0.00 | BC 447 |
| | | | | Max $V_z$ | -5.82 | 0.00 | ▷ 36.58 | 0.00 | -0.00 | 0.00 | BC 134 |
| | | | | Min $V_z$ | 2.18 | -0.05 | ▷ 8.55 | 0.01 | 0.00 | 0.00 | BC 471 |
| | | | | Max $M_T$ | 2.22 | -0.04 | 18.87 | ▷ 0.01 | 0.00 | 0.00 | BC 235 |
| | | | | Min $M_T$ | -11.53 | 0.01 | 8.55 | ▷ -0.01 | 0.00 | 0.00 | BC 413 |
| | | | | Max $M_y$ | -3.64 | 0.00 | 21.20 | 0.00 | ▷ 0.00 | 0.00 | BC 304 |
| | | | | Min $M_y$ | -20.17 | 0.01 | 12.54 | -0.01 | ▷ -0.00 | 0.00 | BC 278 |
| | | | | Max $M_z$ | -4.30 | 0.01 | 14.16 | 0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | -4.30 | 0.01 | 14.16 | 0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | 159 | 3267 | Max N | ▷ 4.54 | -0.05 | 0.44 | 0.01 | 14.69 | 0.16 | BC 363 |
| | | | | Min N | ▷ -29.37 | 0.05 | 0.44 | -0.01 | 25.03 | -0.17 | BC 436 |
| | | | | Max $V_y$ | -24.52 | ▷ 0.06 | 0.65 | -0.01 | 31.88 | -0.20 | BC 204 |
| | | | | Min $V_y$ | 2.51 | ▷ -0.05 | 0.44 | 0.01 | 14.68 | 0.17 | BC 447 |
| | | | | Max $V_z$ | -3.29 | 0.01 | ▷ 0.73 | 0.00 | 24.33 | -0.03 | BC 10 |
| | | | | Min $V_z$ | 2.02 | -0.04 | ▷ 0.44 | 0.01 | 25.02 | 0.15 | BC 459 |
| | | | | Max $M_T$ | 2.90 | -0.04 | 0.65 | ▷ 0.01 | 31.89 | 0.14 | BC 235 |
| | | | | Min $M_T$ | -11.23 | 0.01 | 0.44 | ▷ -0.01 | 14.69 | -0.04 | BC 413 |
| | | | | Max $M_y$ | -4.48 | 0.00 | 0.65 | 0.00 | ▷ 60.82 | -0.02 | BC 134 |
| | | | | Min $M_y$ | 2.48 | -0.05 | 0.44 | 0.01 | ▷ 14.68 | 0.16 | BC 471 |
| | | | | Max $M_z$ | 2.51 | -0.05 | 0.44 | 0.01 | 14.68 | ▷ 0.17 | BC 447 |
| | | | | Min $M_z$ | -24.52 | 0.06 | 0.65 | -0.01 | 31.88 | ▷ -0.20 | BC 204 |
| | | 159 | 3267 | Max N | ▷ 4.54 | -0.05 | 0.44 | 0.01 | 14.69 | 0.16 | BC 363 |
| | | 63 | 0 | Min N | ▷ -29.91 | 0.05 | 14.88 | -0.01 | 0.00 | 0.00 | BC 436 |
| | | 63 | 0 | Max $V_y$ | -25.20 | ▷ 0.06 | 18.87 | -0.01 | -0.00 | 0.00 | BC 204 |
| | | 63 | 0 | Min $V_y$ | 2.21 | ▷ -0.05 | 8.55 | 0.01 | 0.00 | 0.00 | BC 447 |
| | | 63 | 0 | Max $V_z$ | -5.82 | 0.00 | ▷ 36.58 | 0.00 | -0.00 | 0.00 | BC 134 |
| | | 159 | 3267 | Min $V_z$ | 2.02 | -0.04 | ▷ 0.44 | 0.01 | 25.02 | 0.15 | BC 459 |
| | | 63 | 0 | Max $M_T$ | 2.22 | -0.04 | 18.87 | ▷ 0.01 | 0.00 | 0.00 | BC 235 |
| | | 63 | 0 | Min $M_T$ | -11.53 | 0.01 | 8.55 | ▷ -0.01 | 0.00 | 0.00 | BC 413 |
| | | 159 | 3267 | Max $M_y$ | -4.48 | 0.00 | 0.65 | 0.00 | ▷ 60.82 | -0.02 | BC 134 |
| | | 63 | 0 | Min $M_y$ | -20.17 | 0.01 | 12.54 | -0.01 | ▷ -0.00 | 0.00 | BC 278 |
| | | 159 | 3267 | Max $M_z$ | 2.51 | -0.05 | 0.44 | 0.01 | 14.68 | ▷ 0.17 | BC 447 |
| | | 159 | 3267 | Min $M_z$ | -24.52 | 0.06 | 0.65 | -0.01 | 31.88 | ▷ -0.20 | BC 204 |
| 197 | RC1 | 159 | 0 | Max N | ▷ 4.54 | 0.05 | -0.44 | 0.02 | 14.70 | 0.16 | BC 363 |
| | | | | Min N | ▷ -29.37 | -0.05 | -0.44 | -0.02 | 25.03 | -0.17 | BC 436 |
| | | | | Max $V_y$ | 2.51 | ▷ 0.05 | -0.45 | 0.01 | 14.71 | 0.17 | BC 447 |
| | | | | Min $V_y$ | -24.52 | ▷ -0.06 | -0.65 | -0.02 | 31.90 | -0.20 | BC 204 |
| | | | | Max $V_z$ | -22.73 | 0.01 | ▷ -0.44 | -0.01 | 14.69 | 0.02 | BC 390 |
| | | | | Min $V_z$ | -5.50 | 0.00 | ▷ -0.74 | -0.00 | 34.68 | 0.00 | BC 27 |
| | | | | Max $M_T$ | 4.28 | 0.05 | -0.44 | ▷ 0.02 | 14.70 | 0.16 | BC 451 |
| | | | | Min $M_T$ | -24.52 | -0.06 | -0.65 | ▷ -0.02 | 31.90 | -0.20 | BC 204 |
| | | | | Max $M_y$ | -6.28 | -0.01 | -0.65 | -0.00 | ▷ 60.84 | -0.02 | BC 154 |
| | | | | Min $M_y$ | -22.73 | 0.01 | -0.44 | -0.01 | ▷ 14.69 | 0.02 | BC 390 |
| | | | | Max $M_z$ | 2.51 | 0.05 | -0.45 | 0.01 | 14.71 | ▷ 0.17 | BC 447 |
| | | | | Min $M_z$ | -24.52 | -0.06 | -0.65 | -0.02 | 31.90 | ▷ -0.20 | BC 204 |
| | | 68 | 3267 | Max N | ▷ 4.84 | 0.05 | -8.55 | 0.02 | -0.00 | 0.00 | BC 363 |
| | | | | Min N | ▷ -28.83 | -0.05 | -14.88 | -0.02 | -0.00 | 0.00 | BC 436 |
| | | | | Max $V_y$ | 2.81 | ▷ 0.05 | -8.56 | 0.01 | 0.00 | 0.00 | BC 447 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 197 | RC1 | | | Min $V_y$ | -23.84 | ▷ -0.06 | -18.87 | -0.02 | -0.00 | 0.00 | BC 204 |
| | | | | Max $V_z$ | -22.42 | 0.01 | ▷ -8.55 | -0.01 | 0.00 | 0.00 | BC 390 |
| | | | | Min $V_z$ | -4.94 | -0.01 | ▷ -36.59 | -0.00 | -0.00 | 0.00 | BC 154 |
| | | | | Max $M_T$ | 4.58 | 0.05 | -8.55 | ▷ 0.02 | 0.00 | 0.00 | BC 451 |
| | | | | Min $M_T$ | -23.84 | -0.06 | -18.87 | ▷ -0.02 | -0.00 | 0.00 | BC 204 |
| | | | | Max $M_y$ | -2.09 | -0.00 | -21.20 | -0.00 | ▷ 0.00 | 0.00 | BC 304 |
| | | | | Min $M_y$ | -19.28 | -0.01 | -12.55 | -0.01 | ▷ -0.00 | 0.00 | BC 278 |
| | | | | Max $M_z$ | -9.26 | -0.01 | -8.55 | -0.02 | 0.00 | ▷ 0.00 | BC 477 |
| | | | | Min $M_z$ | -12.05 | -0.01 | -18.87 | -0.02 | 0.00 | ▷ -0.00 | BC 241 |
| | | 68 | 3267 | Max N | ▷ 4.84 | 0.05 | -8.55 | 0.02 | -0.00 | 0.00 | BC 363 |
| | | 159 | 0 | Min N | ▷ -29.37 | -0.05 | -0.44 | -0.02 | 25.03 | -0.17 | BC 436 |
| | | 159 | 0 | Max $V_y$ | 2.51 | ▷ 0.05 | -0.45 | 0.01 | 14.71 | 0.17 | BC 447 |
| | | 159 | 0 | Min $V_y$ | -24.52 | ▷ -0.06 | -0.65 | -0.02 | 31.90 | -0.20 | BC 204 |
| | | 159 | 0 | Max $V_z$ | -22.73 | 0.01 | ▷ -0.44 | -0.01 | 14.69 | 0.02 | BC 390 |
| | | 68 | 3267 | Min $V_z$ | -4.94 | -0.01 | ▷ -36.59 | -0.00 | -0.00 | 0.00 | BC 154 |
| | | 159 | 0 | Max $M_T$ | 4.28 | 0.05 | -0.44 | ▷ 0.02 | 14.70 | 0.16 | BC 451 |
| | | 159 | 0 | Min $M_T$ | -24.52 | -0.06 | -0.65 | ▷ -0.02 | 31.90 | -0.20 | BC 204 |
| | | 159 | 0 | Max $M_y$ | -6.28 | -0.01 | -0.65 | -0.00 | ▷ 60.84 | -0.02 | BC 154 |
| | | 68 | 3267 | Min $M_y$ | -19.28 | -0.01 | -12.55 | -0.01 | ▷ -0.00 | 0.00 | BC 278 |
| | | 159 | 0 | Max $M_z$ | 2.51 | 0.05 | -0.45 | 0.01 | 14.71 | ▷ 0.17 | BC 447 |
| | | 159 | 0 | Min $M_z$ | -24.52 | -0.06 | -0.65 | -0.02 | 31.90 | ▷ -0.20 | BC 204 |
| 197 | RC1 | 68 | 3267 | MAX N | ▷ 4.84 | 0.05 | -8.55 | 0.02 | 0.00 | 0.00 | BC 363 |
| 20 | RC1 | 63 | 0 | MIN N | ▷ -29.91 | 0.05 | 14.88 | -0.01 | 0.00 | 0.00 | BC 436 |
| 20 | RC1 | 63 | 0 | MAX $V_y$ | -25.20 | ▷ 0.06 | 18.87 | -0.01 | 0.00 | 0.00 | BC 204 |
| 197 | RC1 | 159 | 0 | MIN $V_y$ | -24.52 | ▷ -0.06 | -0.65 | -0.02 | 31.90 | -0.20 | BC 204 |
| 20 | RC1 | 63 | 0 | MAX $V_z$ | -5.82 | 0.00 | ▷ 36.58 | 0.00 | 0.00 | 0.00 | BC 134 |
| 197 | RC1 | 68 | 3267 | MIN $V_z$ | -4.94 | -0.01 | ▷ -36.59 | 0.00 | 0.00 | 0.00 | BC 154 |
| 197 | RC1 | 159 | 0 | MAX $M_T$ | 4.28 | 0.05 | -0.44 | ▷ 0.02 | 14.70 | 0.16 | BC 451 |
| 197 | RC1 | 159 | 0 | MIN $M_T$ | -24.52 | -0.06 | -0.65 | ▷ -0.02 | 31.90 | -0.20 | BC 204 |
| 197 | RC1 | 159 | 0 | MAX $M_y$ | -6.28 | -0.01 | -0.65 | 0.00 | ▷ 60.84 | -0.02 | BC 154 |
| 20 | RC1 | 63 | 0 | MIN $M_y$ | -20.17 | 0.01 | 12.54 | -0.01 | ▷ 0.00 | 0.00 | BC 278 |
| 20 | RC1 | 159 | 3267 | MAX $M_z$ | 2.51 | -0.05 | 0.44 | 0.01 | 14.68 | ▷ 0.17 | BC 447 |
| 20 | RC1 | 159 | 3267 | MIN $M_z$ | -24.52 | 0.06 | 0.65 | -0.01 | 31.88 | ▷ -0.20 | BC 204 |
| | **Doorgaande staven No. 43: Doorgaande staven 43** | | | | | | | | | | |
| 174 | RC1 | 101 | 0 | Max N | ▷ -0.16 | 0.09 | 7.94 | -0.03 | 0.00 | 0.00 | BC 363 |
| | | | | Min N | ▷ -1.39 | 0.04 | 13.97 | -0.06 | 0.00 | 0.00 | BC 436 |
| | | | | Max $V_y$ | -0.74 | ▷ 0.53 | 34.58 | -0.10 | 0.00 | -0.00 | BC 149 |
| | | | | Min $V_y$ | -1.15 | ▷ -0.07 | 7.93 | -0.05 | 0.00 | 0.00 | BC 408 |
| | | | | Max $V_z$ | -0.74 | 0.53 | ▷ 34.58 | -0.10 | 0.00 | 0.00 | BC 134 |
| | | | | Min $V_z$ | -1.15 | -0.07 | ▷ 7.93 | -0.05 | -0.00 | 0.00 | BC 468 |
| | | | | Max $M_T$ | -1.11 | 0.21 | 7.94 | ▷ -0.02 | 0.00 | 0.00 | BC 390 |
| | | | | Min $M_T$ | -0.81 | 0.52 | 34.57 | ▷ -0.10 | -0.00 | 0.00 | BC 154 |
| | | | | Max $M_y$ | -0.43 | 0.31 | 20.01 | -0.06 | ▷ 0.00 | -0.00 | BC 304 |
| | | | | Min $M_y$ | -1.29 | 0.02 | 13.97 | -0.06 | ▷ -0.00 | 0.00 | BC 368 |
| | | | | Max $M_z$ | -0.71 | 0.45 | 29.75 | -0.09 | 0.00 | ▷ 0.00 | BC 122 |
| | | | | Min $M_z$ | -0.68 | 0.44 | 28.54 | -0.09 | -0.00 | ▷ -0.00 | BC 136 |
| | | 160 | 3267 | Max N | ▷ 0.55 | 0.53 | 0.03 | -0.10 | 56.54 | -1.73 | BC 131 |
| | | | | Min N | ▷ -0.98 | -0.05 | 0.08 | -0.04 | 13.09 | 0.17 | BC 448 |
| | | | | Max $V_y$ | 0.54 | ▷ 0.53 | 0.03 | -0.10 | 56.54 | -1.74 | BC 149 |
| | | | | Min $V_y$ | -0.85 | ▷ -0.07 | 0.07 | -0.05 | 13.08 | 0.22 | BC 408 |
| | | | | Max $V_z$ | 0.18 | 0.23 | ▷ 0.13 | -0.04 | 21.68 | -0.76 | BC 10 |
| | | | | Min $V_z$ | 0.43 | 0.46 | ▷ -0.01 | -0.09 | 50.42 | -1.49 | BC 346 |
| | | | | Max $M_T$ | -0.81 | 0.21 | 0.08 | ▷ -0.02 | 13.09 | -0.70 | BC 390 |
| | | | | Min $M_T$ | 0.48 | 0.52 | 0.03 | ▷ -0.10 | 56.53 | -1.70 | BC 154 |
| | | | | Max $M_y$ | 0.55 | 0.53 | 0.03 | -0.10 | ▷ 56.54 | -1.73 | BC 134 |
| | | | | Min $M_y$ | -0.86 | -0.07 | 0.07 | -0.05 | ▷ 13.08 | 0.22 | BC 468 |
| | | | | Max $M_z$ | -0.85 | -0.07 | 0.07 | -0.05 | 13.08 | ▷ 0.22 | BC 408 |
| | | | | Min $M_z$ | 0.54 | 0.53 | 0.03 | -0.10 | 56.54 | ▷ -1.74 | BC 149 |
| | | 160 | 3267 | Max N | ▷ 0.55 | 0.53 | 0.03 | -0.10 | 56.54 | -1.73 | BC 131 |
| | | 101 | 0 | Min N | ▷ -1.39 | 0.04 | 13.97 | -0.06 | 0.00 | 0.00 | BC 436 |
| | | 101 | 0 | Max $V_y$ | -0.74 | ▷ 0.53 | 34.58 | -0.10 | 0.00 | -0.00 | BC 149 |
| | | 101 | 0 | Min $V_y$ | -1.15 | ▷ -0.07 | 7.93 | -0.05 | 0.00 | 0.00 | BC 408 |
| | | 101 | 0 | Max $V_z$ | -0.74 | 0.53 | ▷ 34.58 | -0.10 | 0.00 | 0.00 | BC 134 |
| | | 160 | 3267 | Min $V_z$ | 0.43 | 0.46 | ▷ -0.01 | -0.09 | 50.42 | -1.49 | BC 346 |
| | | 101 | 0 | Max $M_T$ | -1.11 | 0.21 | 7.94 | ▷ -0.02 | 0.00 | 0.00 | BC 390 |
| | | 101 | 0 | Min $M_T$ | -0.81 | 0.52 | 34.57 | ▷ -0.10 | -0.00 | 0.00 | BC 154 |
| | | 160 | 3267 | Max $M_y$ | 0.55 | 0.53 | 0.03 | -0.10 | ▷ 56.54 | -1.73 | BC 134 |
| | | 101 | 0 | Min $M_y$ | -1.29 | 0.02 | 13.97 | -0.06 | ▷ -0.00 | 0.00 | BC 368 |
| | | 160 | 3267 | Max $M_z$ | -0.85 | -0.07 | 0.07 | -0.05 | 13.08 | ▷ 0.22 | BC 408 |
| | | 160 | 3267 | Min $M_z$ | 0.54 | 0.53 | 0.03 | -0.10 | 56.54 | ▷ -1.74 | BC 149 |
| 198 | RC1 | 160 | 0 | Max N | ▷ 0.57 | -0.53 | -0.30 | -0.19 | 57.41 | -1.73 | BC 131 |
| | | | | Min N | ▷ -0.97 | 0.05 | -0.15 | -0.04 | 13.33 | 0.17 | BC 448 |
| | | | | Max $V_y$ | -0.84 | ▷ 0.07 | -0.15 | -0.04 | 13.34 | 0.22 | BC 408 |
| | | | | Min $V_y$ | 0.56 | ▷ -0.53 | -0.30 | -0.19 | 57.41 | -1.73 | BC 149 |
| | | | | Max $V_z$ | -0.14 | -0.13 | ▷ -0.15 | -0.05 | 13.32 | -0.44 | BC 389 |
| | | | | Min $V_z$ | 0.49 | -0.52 | ▷ -0.30 | -0.19 | 57.41 | -1.70 | BC 154 |
| | | | | Max $M_T$ | -0.90 | 0.06 | -0.15 | ▷ -0.03 | 13.33 | 0.19 | BC 356 |
| | | | | Min $M_T$ | 0.49 | -0.52 | -0.30 | ▷ -0.19 | 57.41 | -1.70 | BC 154 |
| | | | | Max $M_y$ | 0.49 | -0.52 | -0.30 | -0.19 | ▷ 57.41 | -1.70 | BC 154 |
| | | | | Min $M_y$ | -0.14 | -0.13 | -0.15 | -0.05 | ▷ 13.32 | -0.44 | BC 389 |
| | | | | Max $M_z$ | -0.84 | 0.07 | -0.15 | -0.04 | 13.34 | ▷ 0.22 | BC 408 |
| | | | | Min $M_z$ | 0.56 | -0.53 | -0.30 | -0.19 | 57.41 | ▷ -1.73 | BC 149 |
| | | 102 | 3267 | Max N | ▷ 1.85 | -0.53 | -34.84 | -0.19 | -0.00 | 0.00 | BC 131 |
| | | | | Min N | ▷ -0.67 | 0.05 | -8.01 | -0.04 | -0.00 | 0.00 | BC 448 |
| | | | | Max $V_y$ | -0.55 | ▷ 0.07 | -8.01 | -0.04 | 0.00 | 0.00 | BC 408 |
| | | | | Min $V_y$ | 1.84 | ▷ -0.53 | -34.84 | -0.19 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_z$ | 0.15 | -0.13 | ▷ -8.01 | -0.05 | -0.00 | -0.00 | BC 389 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 198 | RC1 | | | Min $V_z$ | 1.78 | -0.52 | ▷ -34.84 | -0.19 | -0.00 | 0.00 | BC 154 |
| | | | | Max $M_T$ | -0.61 | 0.06 | -8.01 | ▷ -0.03 | 0.00 | 0.00 | BC 356 |
| | | | | Min $M_T$ | 1.78 | -0.52 | -34.84 | ▷ -0.19 | -0.00 | 0.00 | BC 154 |
| | | | | Max $M_y$ | 1.06 | -0.31 | -20.16 | -0.11 | ▷ 0.00 | -0.00 | BC 304 |
| | | | | Min $M_y$ | -0.33 | -0.01 | -11.75 | -0.06 | ▷ -0.00 | 0.00 | BC 160 |
| | | | | Max $M_z$ | 1.65 | -0.46 | -31.10 | -0.16 | -0.00 | ▷ 0.00 | BC 345 |
| | | | | Min $M_z$ | 1.52 | -0.44 | -28.76 | -0.16 | -0.00 | ▷ -0.00 | BC 129 |
| | | 102 | 3267 | Max N | ▷ 1.85 | -0.53 | -34.84 | -0.19 | -0.00 | 0.00 | BC 131 |
| | | 160 | 0 | Min N | ▷ -0.97 | 0.05 | -0.15 | -0.04 | 13.33 | 0.17 | BC 448 |
| | | 160 | 0 | Max $V_y$ | -0.84 | ▷ 0.07 | -0.15 | -0.04 | 13.34 | 0.22 | BC 408 |
| | | 160 | 0 | Min $V_y$ | 0.56 | ▷ -0.53 | -0.30 | -0.19 | 57.41 | -1.73 | BC 149 |
| | | 160 | 0 | Max $V_z$ | -0.14 | -0.13 | ▷ -0.15 | -0.05 | 13.32 | -0.44 | BC 389 |
| | | 102 | 3267 | Min $V_z$ | 1.78 | -0.52 | ▷ -34.84 | -0.19 | -0.00 | 0.00 | BC 154 |
| | | 160 | 0 | Max $M_T$ | -0.90 | 0.06 | -0.15 | ▷ -0.03 | 13.33 | 0.19 | BC 356 |
| | | 160 | 0 | Min $M_T$ | 0.49 | -0.52 | -0.30 | ▷ -0.19 | 57.41 | -1.70 | BC 154 |
| | | 160 | 0 | Max $M_y$ | 0.49 | -0.52 | -0.30 | -0.19 | ▷ 57.41 | -1.70 | BC 154 |
| | | 102 | 3267 | Min $M_y$ | -0.33 | -0.01 | -11.75 | -0.06 | ▷ -0.00 | 0.00 | BC 160 |
| | | 160 | 0 | Max $M_z$ | -0.84 | 0.07 | -0.15 | -0.04 | 13.34 | ▷ 0.22 | BC 408 |
| | | 160 | 0 | Min $M_z$ | 0.56 | -0.53 | -0.30 | -0.19 | 57.41 | ▷ -1.73 | BC 149 |
| 198 | RC1 | 102 | 3267 | MAX N | ▷ 1.85 | -0.53 | -34.84 | -0.19 | 0.00 | 0.00 | BC 131 |
| 174 | RC1 | 101 | 0 | MIN N | ▷ -1.39 | 0.04 | 13.97 | -0.06 | 0.00 | 0.00 | BC 436 |
| 174 | RC1 | 101 | 0 | MAX $V_y$ | -0.74 | ▷ 0.53 | 34.58 | -0.10 | 0.00 | 0.00 | BC 149 |
| 198 | RC1 | 160 | 0 | MIN $V_y$ | 0.56 | ▷ -0.53 | -0.30 | -0.19 | 57.41 | -1.73 | BC 149 |
| 174 | RC1 | 101 | 0 | MAX $V_z$ | -0.74 | 0.53 | ▷ 34.58 | -0.10 | 0.00 | 0.00 | BC 134 |
| 198 | RC1 | 102 | 3267 | MIN $V_z$ | 1.78 | -0.52 | ▷ -34.84 | -0.19 | 0.00 | 0.00 | BC 154 |
| 174 | RC1 | 101 | 0 | MAX $M_T$ | -1.11 | 0.21 | 7.94 | ▷ -0.02 | 0.00 | 0.00 | BC 390 |
| 198 | RC1 | 160 | 0 | MIN $M_T$ | 0.49 | -0.52 | -0.30 | ▷ -0.19 | 57.41 | -1.70 | BC 154 |
| 198 | RC1 | 160 | 0 | MAX $M_y$ | 0.49 | -0.52 | -0.30 | -0.19 | ▷ 57.41 | -1.70 | BC 154 |
| 198 | RC1 | 102 | 3267 | MIN $M_y$ | -0.33 | -0.01 | -11.75 | -0.06 | ▷ 0.00 | 0.00 | BC 160 |
| 174 | RC1 | 160 | 3267 | MAX $M_z$ | -0.85 | -0.07 | 0.07 | -0.05 | 13.08 | ▷ 0.22 | BC 408 |
| 174 | RC1 | 160 | 3267 | MIN $M_z$ | 0.54 | 0.53 | 0.03 | -0.10 | 56.54 | ▷ -1.74 | BC 149 |
| | **Doorgaande staven No. 44: Doorgaande staven 44** | | | | | | | | | | |
| 203 | RC1 | 149 | 0 | Max N | ▷ 0.78 | -0.04 | 0.83 | 0.01 | 0.00 | 0.00 | BC 413 |
| | | | | Min N | ▷ -1.14 | -0.28 | 1.30 | 0.03 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_y$ | -0.83 | ▷ -0.03 | 0.88 | 0.01 | 0.00 | 0.00 | BC 362 |
| | | | | Min $V_y$ | -1.12 | ▷ -0.28 | 1.30 | 0.03 | -0.00 | 0.00 | BC 148 |
| | | | | Max $V_z$ | -0.67 | -0.15 | ▷ 1.46 | 0.02 | 0.00 | 0.00 | BC 22 |
| | | | | Min $V_z$ | 0.78 | -0.04 | ▷ 0.83 | 0.01 | 0.00 | 0.00 | BC 413 |
| | | | | Max $M_T$ | -1.12 | -0.28 | 1.30 | ▷ 0.03 | -0.00 | 0.00 | BC 148 |
| | | | | Min $M_T$ | -0.44 | -0.04 | 0.88 | ▷ 0.00 | 0.00 | 0.00 | BC 359 |
| | | | | Max $M_y$ | -0.82 | -0.08 | 0.88 | 0.02 | ▷ 0.00 | 0.00 | BC 378 |
| | | | | Min $M_y$ | -0.60 | -0.14 | 1.29 | 0.02 | ▷ -0.00 | 0.00 | BC 91 |
| | | | | Max $M_z$ | -0.76 | -0.11 | 1.29 | 0.02 | 0.00 | ▷ 0.00 | BC 182 |
| | | | | Min $M_z$ | -0.46 | -0.10 | 1.46 | 0.01 | 0.00 | ▷ 0.00 | BC 1 |
| | | 23 | 2250 | Max N | ▷ 0.78 | -0.04 | 0.60 | 0.01 | 1.61 | 0.09 | BC 413 |
| | | | | Min N | ▷ -1.14 | -0.28 | 0.96 | 0.03 | 2.54 | 0.63 | BC 149 |
| | | | | Max $V_y$ | -0.83 | ▷ -0.03 | 0.64 | 0.01 | 1.71 | 0.08 | BC 362 |
| | | | | Min $V_y$ | -1.12 | ▷ -0.28 | 0.95 | 0.03 | 2.53 | 0.64 | BC 148 |
| | | | | Max $V_z$ | -0.67 | -0.15 | ▷ 1.07 | 0.02 | 2.84 | 0.34 | BC 22 |
| | | | | Min $V_z$ | 0.78 | -0.04 | ▷ 0.60 | 0.01 | 1.61 | 0.09 | BC 413 |
| | | | | Max $M_T$ | -1.12 | -0.28 | 0.95 | ▷ 0.03 | 2.53 | 0.64 | BC 148 |
| | | | | Min $M_T$ | -0.44 | -0.04 | 0.64 | ▷ 0.00 | 1.72 | 0.10 | BC 359 |
| | | | | Max $M_y$ | -0.67 | -0.15 | 1.07 | 0.02 | ▷ 2.84 | 0.34 | BC 22 |
| | | | | Min $M_y$ | 0.78 | -0.04 | 0.60 | 0.01 | ▷ 1.61 | 0.09 | BC 413 |
| | | | | Max $M_z$ | -1.12 | -0.28 | 0.95 | 0.03 | 2.53 | ▷ 0.64 | BC 148 |
| | | | | Min $M_z$ | -0.83 | -0.03 | 0.64 | 0.01 | 1.71 | ▷ 0.08 | BC 362 |
| | | 149 | 0 | Max N | ▷ 0.78 | -0.04 | 0.83 | 0.01 | 0.00 | 0.00 | BC 413 |
| | | 149 | 0 | Min N | ▷ -1.14 | -0.28 | 1.30 | 0.03 | 0.00 | 0.00 | BC 149 |
| | | 149 | 0 | Max $V_y$ | -0.83 | ▷ -0.03 | 0.88 | 0.01 | 0.00 | 0.00 | BC 362 |
| | | 149 | 0 | Min $V_y$ | -1.12 | ▷ -0.28 | 1.30 | 0.03 | -0.00 | 0.00 | BC 148 |
| | | 149 | 0 | Max $V_z$ | -0.67 | -0.15 | ▷ 1.46 | 0.02 | 0.00 | 0.00 | BC 22 |
| | | 23 | 2250 | Min $V_z$ | 0.78 | -0.04 | ▷ 0.60 | 0.01 | 1.61 | 0.09 | BC 413 |
| | | 149 | 0 | Max $M_T$ | -1.12 | -0.28 | 1.30 | ▷ 0.03 | -0.00 | 0.00 | BC 148 |
| | | 149 | 0 | Min $M_T$ | -0.44 | -0.04 | 0.88 | ▷ 0.00 | 0.00 | 0.00 | BC 359 |
| | | 23 | 2250 | Max $M_y$ | -0.67 | -0.15 | 1.07 | 0.02 | ▷ 2.84 | 0.34 | BC 22 |
| | | 149 | 0 | Min $M_y$ | -0.60 | -0.14 | 1.29 | 0.02 | ▷ -0.00 | 0.00 | BC 91 |
| | | 23 | 2250 | Max $M_z$ | -1.12 | -0.28 | 0.95 | 0.03 | 2.53 | ▷ 0.64 | BC 148 |
| | | 149 | 0 | Min $M_z$ | -0.46 | -0.10 | 1.46 | 0.01 | 0.00 | ▷ 0.00 | BC 1 |
| 219 | RC1 | 23 | 0 | Max N | ▷ 6.37 | 0.04 | -0.69 | 0.00 | 1.81 | 0.09 | BC 413 |
| | | | | Min N | ▷ -2.98 | 0.15 | -0.92 | -0.00 | 2.47 | 0.34 | BC 244 |
| | | | | Max $V_y$ | -1.61 | ▷ 0.28 | -0.94 | 0.01 | 2.51 | 0.64 | BC 148 |
| | | | | Min $V_y$ | -0.83 | ▷ 0.03 | -0.64 | 0.01 | 1.71 | 0.08 | BC 362 |
| | | | | Max $V_z$ | -2.75 | 0.12 | ▷ -0.63 | -0.00 | 1.67 | 0.27 | BC 436 |
| | | | | Min $V_z$ | -0.51 | 0.10 | ▷ -1.06 | 0.00 | 2.83 | 0.23 | BC 31 |
| | | | | Max $M_T$ | -0.80 | 0.11 | -0.94 | ▷ 0.01 | 2.51 | 0.24 | BC 202 |
| | | | | Min $M_T$ | -1.97 | 0.07 | -0.63 | ▷ -0.00 | 1.68 | 0.16 | BC 356 |
| | | | | Max $M_y$ | -0.51 | 0.10 | -1.06 | 0.00 | ▷ 2.83 | 0.23 | BC 31 |
| | | | | Min $M_y$ | -2.75 | 0.12 | -0.63 | -0.00 | ▷ 1.67 | 0.27 | BC 436 |
| | | | | Max $M_z$ | -1.61 | 0.28 | -0.94 | 0.01 | 2.51 | ▷ 0.64 | BC 148 |
| | | | | Min $M_z$ | -0.83 | 0.03 | -0.64 | 0.01 | 1.71 | ▷ 0.08 | BC 362 |
| | | 148 | 2250 | Max N | ▷ 6.37 | 0.04 | -0.92 | 0.00 | 0.00 | 0.00 | BC 413 |
| | | | | Min N | ▷ -2.98 | 0.15 | -1.27 | -0.00 | 0.00 | 0.00 | BC 244 |
| | | | | Max $V_y$ | -1.61 | ▷ 0.28 | -1.29 | 0.01 | 0.00 | 0.00 | BC 148 |
| | | | | Min $V_y$ | -0.83 | ▷ 0.03 | -0.88 | 0.01 | 0.00 | 0.00 | BC 362 |
| | | | | Max $V_z$ | -2.75 | 0.12 | ▷ -0.86 | -0.00 | 0.00 | 0.00 | BC 436 |
| | | | | Min $V_z$ | -0.51 | 0.10 | ▷ -1.46 | 0.00 | 0.00 | 0.00 | BC 31 |
| | | | | Max $M_T$ | -0.80 | 0.11 | -1.29 | ▷ 0.01 | 0.00 | 0.00 | BC 202 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 219 | RC1 | | | Min $M_T$ | -1.97 | 0.07 | -0.87 | ▷ -0.00 | -0.00 | 0.00 | BC 356 |
| | | | | Max $M_y$ | -2.98 | 0.15 | -1.27 | -0.00 | ▷ 0.00 | 0.00 | BC 244 |
| | | | | Min $M_y$ | -1.88 | 0.15 | -1.28 | -0.00 | ▷ -0.00 | -0.00 | BC 264 |
| | | | | Max $M_z$ | -2.92 | 0.15 | -1.27 | -0.00 | 0.00 | ▷ 0.00 | BC 232 |
| | | | | Min $M_z$ | -1.88 | 0.15 | -1.28 | -0.00 | -0.00 | ▷ -0.00 | BC 264 |
| | | 23 | 0 | Max N | ▷ 6.37 | 0.04 | -0.69 | 0.00 | 1.81 | 0.09 | BC 413 |
| | | 23 | 0 | Min N | ▷ -2.98 | 0.15 | -0.92 | -0.00 | 2.47 | 0.34 | BC 244 |
| | | 23 | 0 | Max $V_y$ | -1.61 | ▷ 0.28 | -0.94 | 0.01 | 2.51 | 0.64 | BC 148 |
| | | 23 | 0 | Min $V_y$ | -0.83 | ▷ 0.03 | -0.64 | 0.01 | 1.71 | 0.08 | BC 362 |
| | | 23 | 0 | Max $V_z$ | -2.75 | 0.12 | ▷ -0.63 | -0.00 | 1.67 | 0.27 | BC 436 |
| | | 148 | 2250 | Min $V_z$ | -0.51 | 0.10 | ▷ -1.46 | 0.00 | 0.00 | 0.00 | BC 31 |
| | | 23 | 0 | Max $M_T$ | -0.80 | 0.11 | -0.94 | ▷ 0.01 | 2.51 | 0.24 | BC 202 |
| | | 23 | 0 | Min $M_T$ | -1.97 | 0.07 | -0.63 | ▷ -0.00 | 1.68 | 0.16 | BC 356 |
| | | 23 | 0 | Max $M_y$ | -0.51 | 0.10 | -1.06 | 0.00 | ▷ 2.83 | 0.23 | BC 31 |
| | | 148 | 2250 | Min $M_y$ | -1.88 | 0.15 | -1.28 | -0.00 | ▷ -0.00 | -0.00 | BC 264 |
| | | 23 | 0 | Max $M_z$ | -1.61 | 0.28 | -0.94 | 0.01 | 2.51 | ▷ 0.64 | BC 148 |
| | | 148 | 2250 | Min $M_z$ | -1.88 | 0.15 | -1.28 | -0.00 | -0.00 | ▷ -0.00 | BC 264 |
| 219 | RC1 | 23 | 0 | MAX N | ▷ 6.37 | 0.04 | -0.69 | 0.00 | 1.81 | 0.09 | BC 413 |
| 219 | RC1 | 23 | 0 | MIN N | ▷ -2.98 | 0.15 | -0.92 | 0.00 | 2.47 | 0.34 | BC 244 |
| 219 | RC1 | 23 | 0 | MAX $V_y$ | -1.61 | ▷ 0.28 | -0.94 | 0.01 | 2.51 | 0.64 | BC 148 |
| 203 | RC1 | 149 | 0 | MIN $V_y$ | -1.12 | ▷ -0.28 | 1.30 | 0.03 | 0.00 | 0.00 | BC 148 |
| 203 | RC1 | 149 | 0 | MAX $V_z$ | -0.67 | -0.15 | ▷ 1.46 | 0.02 | 0.00 | 0.00 | BC 22 |
| 219 | RC1 | 148 | 2250 | MIN $V_z$ | -0.51 | 0.10 | ▷ -1.46 | 0.00 | 0.00 | 0.00 | BC 31 |
| 203 | RC1 | 149 | 0 | MAX $M_T$ | -1.12 | -0.28 | 1.30 | ▷ 0.03 | 0.00 | 0.00 | BC 148 |
| 219 | RC1 | 23 | 0 | MIN $M_T$ | -1.97 | 0.07 | -0.63 | ▷ 0.00 | 1.68 | 0.16 | BC 356 |
| 203 | RC1 | 23 | 2250 | MAX $M_y$ | -0.67 | -0.15 | 1.07 | 0.02 | ▷ 2.84 | 0.34 | BC 22 |
| 219 | RC1 | 148 | 2250 | MIN $M_y$ | -1.88 | 0.15 | -1.28 | 0.00 | ▷ 0.00 | 0.00 | BC 264 |
| 203 | RC1 | 23 | 2250 | MAX $M_z$ | -1.12 | -0.28 | 0.95 | 0.03 | 2.53 | ▷ 0.64 | BC 148 |
| 219 | RC1 | 148 | 2250 | MIN $M_z$ | -1.88 | 0.15 | -1.28 | 0.00 | 0.00 | ▷ 0.00 | BC 264 |
| | **Doorgaande staven No. 45: Doorgaande staven 45** | | | | | | | | | | |
| 205 | RC1 | 147 | 0 | Max N | ▷ 6.16 | 0.01 | 0.92 | 0.00 | 0.00 | 0.00 | BC 413 |
| | | | | Min N | ▷ -2.12 | -0.08 | 1.27 | 0.00 | 0.00 | 0.00 | BC 244 |
| | | | | Max $V_y$ | 6.04 | ▷ 0.01 | 0.92 | 0.00 | 0.00 | 0.00 | BC 445 |
| | | | | Min $V_y$ | -1.13 | ▷ -0.16 | 1.28 | -0.00 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_z$ | -0.09 | -0.04 | ▷ 1.45 | 0.01 | 0.00 | 0.00 | BC 15 |
| | | | | Min $V_z$ | -2.03 | -0.07 | ▷ 0.86 | 0.00 | 0.00 | 0.00 | BC 436 |
| | | | | Max $M_T$ | -0.52 | -0.04 | 0.88 | ▷ 0.01 | 0.00 | 0.00 | BC 468 |
| | | | | Min $M_T$ | 4.39 | 0.00 | 1.32 | ▷ -0.01 | -0.00 | 0.00 | BC 197 |
| | | | | Max $M_y$ | -2.12 | -0.08 | 1.27 | 0.00 | ▷ 0.00 | 0.00 | BC 244 |
| | | | | Min $M_y$ | -0.99 | -0.08 | 1.28 | 0.01 | ▷ -0.00 | -0.00 | BC 264 |
| | | | | Max $M_z$ | -2.06 | -0.08 | 1.27 | 0.00 | 0.00 | ▷ 0.00 | BC 232 |
| | | | | Min $M_z$ | -0.99 | -0.08 | 1.28 | 0.01 | -0.00 | ▷ -0.00 | BC 264 |
| | | 26 | 2250 | Max N | ▷ 6.16 | 0.01 | 0.69 | 0.00 | 1.81 | -0.03 | BC 413 |
| | | | | Min N | ▷ -2.12 | -0.08 | 0.93 | 0.00 | 2.47 | 0.18 | BC 244 |
| | | | | Max $V_y$ | 6.04 | ▷ 0.01 | 0.68 | 0.00 | 1.81 | -0.03 | BC 445 |
| | | | | Min $V_y$ | -1.13 | ▷ -0.16 | 0.94 | -0.00 | 2.50 | 0.36 | BC 149 |
| | | | | Max $V_z$ | -0.09 | -0.04 | ▷ 1.06 | 0.01 | 2.83 | 0.08 | BC 15 |
| | | | | Min $V_z$ | -2.03 | -0.07 | ▷ 0.63 | 0.00 | 1.68 | 0.16 | BC 436 |
| | | | | Max $M_T$ | -0.52 | -0.04 | 0.64 | ▷ 0.01 | 1.70 | 0.08 | BC 468 |
| | | | | Min $M_T$ | 4.39 | 0.00 | 0.97 | ▷ -0.01 | 2.57 | -0.00 | BC 197 |
| | | | | Max $M_y$ | -0.09 | -0.04 | 1.06 | 0.01 | ▷ 2.83 | 0.08 | BC 15 |
| | | | | Min $M_y$ | -2.03 | -0.07 | 0.63 | 0.00 | ▷ 1.68 | 0.16 | BC 436 |
| | | | | Max $M_z$ | -1.13 | -0.16 | 0.94 | -0.00 | 2.50 | ▷ 0.36 | BC 149 |
| | | | | Min $M_z$ | 6.04 | 0.01 | 0.68 | 0.00 | 1.81 | ▷ -0.03 | BC 445 |
| | | 147 | 0 | Max N | ▷ 6.16 | 0.01 | 0.92 | 0.00 | 0.00 | 0.00 | BC 413 |
| | | 147 | 0 | Min N | ▷ -2.12 | -0.08 | 1.27 | 0.00 | 0.00 | 0.00 | BC 244 |
| | | 147 | 0 | Max $V_y$ | 6.04 | ▷ 0.01 | 0.92 | 0.00 | 0.00 | 0.00 | BC 445 |
| | | 147 | 0 | Min $V_y$ | -1.13 | ▷ -0.16 | 1.28 | -0.00 | 0.00 | 0.00 | BC 149 |
| | | 147 | 0 | Max $V_z$ | -0.09 | -0.04 | ▷ 1.45 | 0.01 | 0.00 | 0.00 | BC 15 |
| | | 26 | 2250 | Min $V_z$ | -2.03 | -0.07 | ▷ 0.63 | 0.00 | 1.68 | 0.16 | BC 436 |
| | | 147 | 0 | Max $M_T$ | -0.52 | -0.04 | 0.88 | ▷ 0.01 | 0.00 | 0.00 | BC 468 |
| | | 147 | 0 | Min $M_T$ | 4.39 | 0.00 | 1.32 | ▷ -0.01 | -0.00 | 0.00 | BC 197 |
| | | 26 | 2250 | Max $M_y$ | -0.09 | -0.04 | 1.06 | 0.01 | ▷ 2.83 | 0.08 | BC 15 |
| | | 147 | 0 | Min $M_y$ | -0.99 | -0.08 | 1.28 | 0.01 | ▷ -0.00 | -0.00 | BC 264 |
| | | 26 | 2250 | Max $M_z$ | -1.13 | -0.16 | 0.94 | -0.00 | 2.50 | ▷ 0.36 | BC 149 |
| | | 26 | 2250 | Min $M_z$ | 6.04 | 0.01 | 0.68 | 0.00 | 1.81 | ▷ -0.03 | BC 445 |
| 222 | RC1 | 26 | 0 | Max N | ▷ 0.77 | 0.03 | -0.90 | -0.00 | 2.42 | 0.06 | BC 241 |
| | | | | Min N | ▷ -0.59 | 0.04 | -0.94 | -0.00 | 2.51 | 0.09 | BC 175 |
| | | | | Max $V_y$ | -0.16 | ▷ 0.16 | -0.95 | -0.01 | 2.53 | 0.36 | BC 149 |
| | | | | Min $V_y$ | 0.76 | ▷ -0.01 | -0.60 | 0.00 | 1.61 | -0.03 | BC 445 |
| | | | | Max $V_z$ | 0.75 | -0.01 | ▷ -0.60 | 0.00 | 1.61 | -0.03 | BC 413 |
| | | | | Min $V_z$ | -0.15 | 0.08 | ▷ -1.07 | -0.01 | 2.84 | 0.17 | BC 22 |
| | | | | Max $M_T$ | -0.50 | 0.00 | -0.64 | ▷ 0.01 | 1.71 | 0.01 | BC 471 |
| | | | | Min $M_T$ | -0.15 | 0.16 | -0.95 | ▷ -0.01 | 2.53 | 0.36 | BC 134 |
| | | | | Max $M_y$ | -0.15 | 0.08 | -1.07 | -0.01 | ▷ 2.84 | 0.17 | BC 22 |
| | | | | Min $M_y$ | 0.75 | -0.01 | -0.60 | 0.00 | ▷ 1.61 | -0.03 | BC 413 |
| | | | | Max $M_z$ | -0.16 | 0.16 | -0.95 | -0.01 | 2.53 | ▷ 0.36 | BC 149 |
| | | | | Min $M_z$ | 0.76 | -0.01 | -0.60 | 0.00 | 1.61 | ▷ -0.03 | BC 445 |
| | | 146 | 2250 | Max N | ▷ 0.77 | 0.03 | -1.25 | -0.00 | 0.00 | 0.00 | BC 241 |
| | | | | Min N | ▷ -0.59 | 0.04 | -1.29 | -0.00 | 0.00 | 0.00 | BC 175 |
| | | | | Max $V_y$ | -0.16 | ▷ 0.16 | -1.30 | -0.01 | 0.00 | 0.00 | BC 149 |
| | | | | Min $V_y$ | 0.76 | ▷ -0.01 | -0.83 | 0.00 | 0.00 | 0.00 | BC 445 |
| | | | | Max $V_z$ | 0.75 | -0.01 | ▷ -0.83 | 0.00 | 0.00 | 0.00 | BC 413 |
| | | | | Min $V_z$ | -0.15 | 0.08 | ▷ -1.46 | -0.01 | 0.00 | 0.00 | BC 22 |
| | | | | Max $M_T$ | -0.50 | 0.00 | -0.88 | ▷ 0.01 | -0.00 | 0.00 | BC 471 |
| | | | | Min $M_T$ | -0.15 | 0.16 | -1.30 | ▷ -0.01 | 0.00 | 0.00 | BC 134 |
| | | | | Max $M_y$ | -0.13 | 0.08 | -1.30 | 0.01 | ▷ 0.00 | 0.00 | BC 264 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 222 | RC1 | | | Min $M_y$ | -0.14 | 0.08 | -1.30 | -0.01 | ▷ -0.00 | 0.00 | BC 172 |
| | | | | Max $M_z$ | -0.17 | 0.04 | -1.46 | -0.01 | 0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.17 | 0.04 | -1.46 | -0.01 | 0.00 | ▷ 0.00 | BC 1 |
| | | 26 | 0 | Max N | ▷ 0.77 | 0.03 | -0.90 | -0.00 | 2.42 | 0.06 | BC 241 |
| | | 26 | 0 | Min N | ▷ -0.59 | 0.04 | -0.94 | -0.00 | 2.51 | 0.09 | BC 175 |
| | | 26 | 0 | Max $V_y$ | -0.16 | ▷ 0.16 | -0.95 | -0.01 | 2.53 | 0.36 | BC 149 |
| | | 26 | 0 | Min $V_y$ | 0.76 | ▷ -0.01 | -0.60 | 0.00 | 1.61 | -0.03 | BC 445 |
| | | 26 | 0 | Max $V_z$ | 0.75 | -0.01 | ▷ -0.60 | 0.00 | 1.61 | -0.03 | BC 413 |
| | | 146 | 2250 | Min $V_z$ | -0.15 | 0.08 | ▷ -1.46 | -0.01 | 0.00 | 0.00 | BC 22 |
| | | 26 | 0 | Max $M_T$ | -0.50 | 0.00 | -0.64 | ▷ 0.01 | 1.71 | 0.01 | BC 471 |
| | | 26 | 0 | Min $M_T$ | -0.15 | 0.16 | -0.95 | ▷ -0.01 | 2.53 | 0.36 | BC 134 |
| | | 26 | 0 | Max $M_y$ | -0.15 | 0.08 | -1.07 | -0.01 | ▷ 2.84 | 0.17 | BC 22 |
| | | 146 | 2250 | Min $M_y$ | -0.14 | 0.08 | -1.30 | -0.01 | ▷ -0.00 | 0.00 | BC 172 |
| | | 26 | 0 | Max $M_z$ | -0.16 | 0.16 | -0.95 | -0.01 | 2.53 | ▷ 0.36 | BC 149 |
| | | 26 | 0 | Min $M_z$ | 0.76 | -0.01 | -0.60 | 0.00 | 1.61 | ▷ -0.03 | BC 445 |
| 205 | RC1 | 147 | 0 | MAX N | ▷ 6.16 | 0.01 | 0.92 | 0.00 | 0.00 | 0.00 | BC 413 |
| 205 | RC1 | 147 | 0 | MIN N | ▷ -2.12 | -0.08 | 1.27 | 0.00 | 0.00 | 0.00 | BC 244 |
| 222 | RC1 | 26 | 0 | MAX $V_y$ | -0.16 | ▷ 0.16 | -0.95 | -0.01 | 2.53 | 0.36 | BC 149 |
| 205 | RC1 | 147 | 0 | MIN $V_y$ | -1.13 | ▷ -0.16 | 1.28 | 0.00 | 0.00 | 0.00 | BC 149 |
| 205 | RC1 | 147 | 0 | MAX $V_z$ | -0.09 | -0.04 | ▷ 1.45 | 0.01 | 0.00 | 0.00 | BC 15 |
| 222 | RC1 | 146 | 2250 | MIN $V_z$ | -0.15 | 0.08 | ▷ -1.46 | -0.01 | 0.00 | 0.00 | BC 22 |
| 205 | RC1 | 147 | 0 | MAX $M_T$ | -0.52 | -0.04 | 0.88 | ▷ 0.01 | 0.00 | 0.00 | BC 468 |
| 222 | RC1 | 26 | 0 | MIN $M_T$ | -0.15 | 0.16 | -0.95 | ▷ -0.01 | 2.53 | 0.36 | BC 134 |
| 222 | RC1 | 26 | 0 | MAX $M_y$ | -0.15 | 0.08 | -1.07 | -0.01 | ▷ 2.84 | 0.17 | BC 22 |
| 205 | RC1 | 147 | 0 | MIN $M_y$ | -0.99 | -0.08 | 1.28 | 0.01 | ▷ 0.00 | 0.00 | BC 264 |
| 205 | RC1 | 26 | 2250 | MAX $M_z$ | -1.13 | -0.16 | 0.94 | 0.00 | 2.50 | ▷ 0.36 | BC 149 |
| 205 | RC1 | 26 | 2250 | MIN $M_z$ | 6.04 | 0.01 | 0.68 | 0.00 | 1.81 | ▷ -0.03 | BC 445 |
| | **Doorgaande staven No. 46: Doorgaande staven 46** | | | | | | | | | | |
| 207 | RC1 | 156 | 0 | Max N | ▷ 0.33 | -0.02 | 0.85 | -0.01 | -0.00 | 0.00 | BC 384 |
| | | | | Min N | ▷ -0.62 | 0.01 | 0.87 | 0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Max $V_y$ | 0.15 | ▷ 0.05 | 1.26 | 0.02 | -0.00 | 0.00 | BC 201 |
| | | | | Min $V_y$ | 0.28 | ▷ -0.02 | 0.85 | -0.01 | 0.00 | 0.00 | BC 400 |
| | | | | Max $V_z$ | -0.20 | 0.02 | ▷ 1.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.14 | 0.01 | ▷ 0.85 | 0.01 | 0.00 | 0.00 | BC 415 |
| | | | | Max $M_T$ | 0.13 | 0.05 | 1.26 | ▷ 0.02 | -0.00 | 0.00 | BC 241 |
| | | | | Min $M_T$ | 0.31 | -0.02 | 0.85 | ▷ -0.01 | 0.00 | 0.00 | BC 356 |
| | | | | Max $M_y$ | -0.61 | 0.02 | 1.27 | 0.01 | ▷ 0.00 | 0.00 | BC 182 |
| | | | | Min $M_y$ | 0.28 | -0.01 | 1.26 | -0.01 | ▷ -0.00 | 0.00 | BC 160 |
| | | | | Max $M_z$ | -0.20 | 0.02 | 1.43 | 0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.20 | 0.02 | 1.43 | 0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | 27 | 2150 | Max N | ▷ 0.33 | -0.02 | 0.63 | -0.01 | 1.59 | 0.05 | BC 384 |
| | | | | Min N | ▷ -0.62 | 0.01 | 0.64 | 0.00 | 1.63 | -0.03 | BC 446 |
| | | | | Max $V_y$ | 0.15 | ▷ 0.05 | 0.93 | 0.02 | 2.35 | -0.11 | BC 201 |
| | | | | Min $V_y$ | 0.28 | ▷ -0.02 | 0.63 | -0.01 | 1.59 | 0.05 | BC 400 |
| | | | | Max $V_z$ | -0.20 | 0.02 | ▷ 1.06 | 0.00 | 2.68 | -0.05 | BC 1 |
| | | | | Min $V_z$ | 0.14 | 0.01 | ▷ 0.63 | 0.01 | 1.59 | -0.01 | BC 415 |
| | | | | Max $M_T$ | 0.13 | 0.05 | 0.93 | ▷ 0.02 | 2.35 | -0.10 | BC 241 |
| | | | | Min $M_T$ | 0.31 | -0.02 | 0.63 | ▷ -0.01 | 1.59 | 0.04 | BC 356 |
| | | | | Max $M_y$ | -0.20 | 0.02 | 1.06 | 0.00 | ▷ 2.68 | -0.05 | BC 1 |
| | | | | Min $M_y$ | 0.14 | 0.01 | 0.63 | 0.01 | ▷ 1.59 | -0.01 | BC 415 |
| | | | | Max $M_z$ | 0.28 | -0.02 | 0.63 | -0.01 | 1.59 | ▷ 0.05 | BC 400 |
| | | | | Min $M_z$ | 0.15 | 0.05 | 0.93 | 0.02 | 2.35 | ▷ -0.11 | BC 201 |
| | | 156 | 0 | Max N | ▷ 0.33 | -0.02 | 0.85 | -0.01 | -0.00 | 0.00 | BC 384 |
| | | 156 | 0 | Min N | ▷ -0.62 | 0.01 | 0.87 | 0.00 | 0.00 | 0.00 | BC 446 |
| | | 156 | 0 | Max $V_y$ | 0.15 | ▷ 0.05 | 1.26 | 0.02 | -0.00 | 0.00 | BC 201 |
| | | 156 | 0 | Min $V_y$ | 0.28 | ▷ -0.02 | 0.85 | -0.01 | 0.00 | 0.00 | BC 400 |
| | | 156 | 0 | Max $V_z$ | -0.20 | 0.02 | ▷ 1.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 27 | 2150 | Min $V_z$ | 0.14 | 0.01 | ▷ 0.63 | 0.01 | 1.59 | -0.01 | BC 415 |
| | | 156 | 0 | Max $M_T$ | 0.13 | 0.05 | 1.26 | ▷ 0.02 | -0.00 | 0.00 | BC 241 |
| | | 156 | 0 | Min $M_T$ | 0.31 | -0.02 | 0.85 | ▷ -0.01 | 0.00 | 0.00 | BC 356 |
| | | 27 | 2150 | Max $M_y$ | -0.20 | 0.02 | 1.06 | 0.00 | ▷ 2.68 | -0.05 | BC 1 |
| | | 156 | 0 | Min $M_y$ | 0.28 | -0.01 | 1.26 | -0.01 | ▷ -0.00 | 0.00 | BC 160 |
| | | 27 | 2150 | Max $M_z$ | 0.28 | -0.02 | 0.63 | -0.01 | 1.59 | ▷ 0.05 | BC 400 |
| | | 27 | 2150 | Min $M_z$ | 0.15 | 0.05 | 0.93 | 0.02 | 2.35 | ▷ -0.11 | BC 201 |
| 225 | RC1 | 27 | 0 | Max N | ▷ 1.75 | 0.02 | -0.65 | -0.01 | 1.65 | 0.05 | BC 412 |
| | | | | Min N | ▷ -1.26 | -0.01 | -0.63 | 0.00 | 1.61 | -0.03 | BC 446 |
| | | | | Max $V_y$ | 1.74 | ▷ 0.02 | -0.65 | -0.01 | 1.65 | 0.05 | BC 400 |
| | | | | Min $V_y$ | 1.42 | ▷ -0.05 | -0.95 | 0.02 | 2.39 | -0.11 | BC 201 |
| | | | | Max $V_z$ | -1.26 | -0.01 | ▷ -0.63 | 0.00 | 1.61 | -0.03 | BC 446 |
| | | | | Min $V_z$ | -0.26 | -0.02 | ▷ -1.06 | 0.01 | 2.68 | -0.05 | BC 12 |
| | | | | Max $M_T$ | 1.32 | -0.05 | -0.95 | ▷ 0.02 | 2.39 | -0.10 | BC 241 |
| | | | | Min $M_T$ | 1.69 | 0.02 | -0.65 | ▷ -0.01 | 1.64 | 0.04 | BC 356 |
| | | | | Max $M_y$ | -0.26 | -0.02 | -1.06 | 0.01 | ▷ 2.68 | -0.05 | BC 12 |
| | | | | Min $M_y$ | -1.26 | -0.01 | -0.63 | 0.00 | ▷ 1.61 | -0.03 | BC 446 |
| | | | | Max $M_z$ | 1.74 | 0.02 | -0.65 | -0.01 | 1.65 | ▷ 0.05 | BC 400 |
| | | | | Min $M_z$ | 1.42 | -0.05 | -0.95 | 0.02 | 2.39 | ▷ -0.11 | BC 201 |
| | | 155 | 2150 | Max N | ▷ 1.75 | 0.02 | -0.88 | -0.01 | -0.00 | 0.00 | BC 412 |
| | | | | Min N | ▷ -1.26 | -0.01 | -0.86 | 0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Max $V_y$ | 1.74 | ▷ 0.02 | -0.88 | -0.01 | 0.00 | 0.00 | BC 400 |
| | | | | Min $V_y$ | 1.42 | ▷ -0.05 | -1.28 | 0.02 | -0.00 | 0.00 | BC 201 |
| | | | | Max $V_z$ | -1.26 | -0.01 | ▷ -0.86 | 0.00 | 0.00 | 0.00 | BC 446 |
| | | | | Min $V_z$ | -0.26 | -0.02 | ▷ -1.43 | 0.01 | 0.00 | 0.00 | BC 12 |
| | | | | Max $M_T$ | 1.32 | -0.05 | -1.28 | ▷ 0.02 | -0.00 | 0.00 | BC 241 |
| | | | | Min $M_T$ | 1.69 | 0.02 | -0.88 | ▷ -0.01 | 0.00 | 0.00 | BC 356 |
| | | | | Max $M_y$ | -1.03 | -0.01 | -0.86 | 0.00 | ▷ 0.00 | 0.00 | BC 426 |
| | | | | Min $M_y$ | 1.60 | -0.01 | -0.88 | 0.00 | ▷ -0.00 | 0.00 | BC 415 |
| | | | | Max $M_z$ | -0.24 | -0.02 | -1.43 | 0.00 | 0.00 | ▷ 0.00 | BC 1 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 225 | RC1 | | | Min $M_z$ | -0.24 | -0.02 | -1.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 27 | 0 | Max N | 1.75 | 0.02 | -0.65 | -0.01 | 1.65 | 0.05 | BC 412 |
| | | 27 | 0 | Min N | -1.26 | -0.01 | -0.63 | 0.00 | 1.61 | -0.03 | BC 446 |
| | | 27 | 0 | Max $V_y$ | 1.74 | 0.02 | -0.65 | -0.01 | 1.65 | 0.05 | BC 400 |
| | | 27 | 0 | Min $V_y$ | 1.42 | -0.05 | -0.95 | 0.02 | 2.39 | -0.11 | BC 201 |
| | | 27 | 0 | Max $V_z$ | -1.26 | -0.01 | -0.63 | 0.00 | 1.61 | -0.03 | BC 446 |
| | | 155 | 2150 | Min $V_z$ | -0.26 | -0.02 | -1.43 | 0.01 | 0.00 | 0.00 | BC 12 |
| | | 27 | 0 | Max $M_T$ | 1.32 | -0.05 | -0.95 | 0.02 | 2.39 | -0.10 | BC 241 |
| | | 27 | 0 | Min $M_T$ | 1.69 | 0.02 | -0.65 | -0.01 | 1.64 | 0.04 | BC 356 |
| | | 27 | 0 | Max $M_y$ | -0.26 | -0.02 | -1.06 | 0.01 | 2.68 | -0.05 | BC 12 |
| | | 155 | 2150 | Min $M_y$ | 1.60 | -0.01 | -0.88 | 0.00 | -0.00 | 0.00 | BC 415 |
| | | 27 | 0 | Max $M_z$ | 1.74 | 0.02 | -0.65 | -0.01 | 1.65 | 0.05 | BC 400 |
| | | 27 | 0 | Min $M_z$ | 1.42 | -0.05 | -0.95 | 0.02 | 2.39 | -0.11 | BC 201 |
| 225 | RC1 | 27 | 0 | MAX N | 1.75 | 0.02 | -0.65 | -0.01 | 1.65 | 0.05 | BC 412 |
| 225 | RC1 | 27 | 0 | MIN N | -1.26 | -0.01 | -0.63 | 0.00 | 1.61 | -0.03 | BC 446 |
| 207 | RC1 | 156 | 0 | MAX $V_y$ | 0.15 | 0.05 | 1.26 | 0.02 | 0.00 | 0.00 | BC 201 |
| 225 | RC1 | 27 | 0 | MIN $V_y$ | 1.42 | -0.05 | -0.95 | 0.02 | 2.39 | -0.11 | BC 201 |
| 207 | RC1 | 156 | 0 | MAX $V_z$ | -0.20 | 0.02 | 1.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| 225 | RC1 | 155 | 2150 | MIN $V_z$ | -0.26 | -0.02 | -1.43 | 0.01 | 0.00 | 0.00 | BC 12 |
| 225 | RC1 | 27 | 0 | MAX $M_T$ | 1.32 | -0.05 | -0.95 | 0.02 | 2.39 | -0.10 | BC 241 |
| 225 | RC1 | 27 | 0 | MIN $M_T$ | 1.69 | 0.02 | -0.65 | -0.01 | 1.64 | 0.04 | BC 356 |
| 207 | RC1 | 27 | 2150 | MAX $M_y$ | -0.20 | 0.02 | 1.06 | 0.00 | 2.68 | -0.05 | BC 1 |
| 225 | RC1 | 155 | 2150 | MIN $M_y$ | 1.60 | -0.01 | -0.88 | 0.00 | 0.00 | 0.00 | BC 415 |
| 225 | RC1 | 27 | 0 | MAX $M_z$ | 1.74 | 0.02 | -0.65 | -0.01 | 1.65 | 0.05 | BC 400 |
| 207 | RC1 | 27 | 2150 | MIN $M_z$ | 0.15 | 0.05 | 0.93 | 0.02 | 2.35 | -0.11 | BC 201 |
| | **Doorgaande staven No. 47: Doorgaande staven 47** | | | | | | | | | | |
| 208 | RC1 | 155 | 0 | Max N | 2.13 | 0.03 | 0.88 | -0.00 | -0.00 | 0.00 | BC 408 |
| | | | | Min N | -3.36 | 0.02 | 1.30 | -0.00 | -0.00 | 0.00 | BC 148 |
| | | | | Max $V_y$ | 1.19 | 0.04 | 1.30 | -0.00 | 0.00 | 0.00 | BC 204 |
| | | | | Min $V_y$ | 1.53 | 0.00 | 0.88 | 0.00 | -0.00 | 0.00 | BC 449 |
| | | | | Max $V_z$ | -2.09 | 0.03 | 1.47 | -0.00 | -0.00 | 0.00 | BC 11 |
| | | | | Min $V_z$ | 2.13 | 0.03 | 0.88 | -0.00 | -0.00 | 0.00 | BC 408 |
| | | | | Max $M_T$ | -2.41 | 0.02 | 1.30 | 0.00 | -0.00 | 0.00 | BC 166 |
| | | | | Min $M_T$ | -1.31 | 0.02 | 1.30 | -0.00 | -0.00 | 0.00 | BC 243 |
| | | | | Max $M_y$ | -2.32 | 0.01 | 0.89 | 0.00 | 0.00 | -0.00 | BC 378 |
| | | | | Min $M_y$ | 1.69 | 0.04 | 1.30 | -0.00 | -0.00 | 0.00 | BC 160 |
| | | | | Max $M_z$ | 2.12 | 0.03 | 0.88 | -0.00 | -0.00 | 0.00 | BC 384 |
| | | | | Min $M_z$ | -2.32 | 0.01 | 0.89 | 0.00 | 0.00 | -0.00 | BC 378 |
| | | 28 | 2250 | Max N | 2.13 | 0.03 | 0.65 | -0.00 | 1.72 | -0.07 | BC 408 |
| | | | | Min N | -3.36 | 0.02 | 0.95 | -0.00 | 2.54 | -0.05 | BC 148 |
| | | | | Max $V_y$ | 1.19 | 0.04 | 0.95 | -0.00 | 2.53 | -0.08 | BC 204 |
| | | | | Min $V_y$ | 1.53 | 0.00 | 0.65 | 0.00 | 1.72 | -0.00 | BC 449 |
| | | | | Max $V_z$ | -2.09 | 0.03 | 1.08 | -0.00 | 2.86 | -0.06 | BC 11 |
| | | | | Min $V_z$ | 2.13 | 0.03 | 0.65 | -0.00 | 1.72 | -0.07 | BC 408 |
| | | | | Max $M_T$ | -2.41 | 0.02 | 0.95 | 0.00 | 2.53 | -0.05 | BC 166 |
| | | | | Min $M_T$ | -1.31 | 0.02 | 0.95 | -0.00 | 2.54 | -0.05 | BC 243 |
| | | | | Max $M_y$ | -2.09 | 0.03 | 1.08 | -0.00 | 2.86 | -0.06 | BC 11 |
| | | | | Min $M_y$ | 2.13 | 0.03 | 0.65 | -0.00 | 1.72 | -0.07 | BC 408 |
| | | | | Max $M_z$ | 1.53 | 0.00 | 0.65 | 0.00 | 1.72 | -0.00 | BC 449 |
| | | | | Min $M_z$ | 1.19 | 0.04 | 0.95 | -0.00 | 2.53 | -0.08 | BC 204 |
| | | 155 | 0 | Max N | 2.13 | 0.03 | 0.88 | -0.00 | -0.00 | 0.00 | BC 408 |
| | | 155 | 0 | Min N | -3.36 | 0.02 | 1.30 | -0.00 | -0.00 | 0.00 | BC 148 |
| | | 155 | 0 | Max $V_y$ | 1.19 | 0.04 | 1.30 | -0.00 | 0.00 | 0.00 | BC 204 |
| | | 155 | 0 | Min $V_y$ | 1.53 | 0.00 | 0.88 | 0.00 | -0.00 | 0.00 | BC 449 |
| | | 155 | 0 | Max $V_z$ | -2.09 | 0.03 | 1.47 | -0.00 | -0.00 | 0.00 | BC 11 |
| | | 28 | 2250 | Min $V_z$ | 2.13 | 0.03 | 0.65 | -0.00 | 1.72 | -0.07 | BC 408 |
| | | 155 | 0 | Max $M_T$ | -2.41 | 0.02 | 1.30 | 0.00 | -0.00 | 0.00 | BC 166 |
| | | 155 | 0 | Min $M_T$ | -1.31 | 0.02 | 1.30 | -0.00 | -0.00 | 0.00 | BC 243 |
| | | 28 | 2250 | Max $M_y$ | -2.09 | 0.03 | 1.08 | -0.00 | 2.86 | -0.06 | BC 11 |
| | | 155 | 0 | Min $M_y$ | 1.69 | 0.04 | 1.30 | -0.00 | -0.00 | 0.00 | BC 160 |
| | | 155 | 0 | Max $M_z$ | 2.12 | 0.03 | 0.88 | -0.00 | -0.00 | 0.00 | BC 384 |
| | | 28 | 2250 | Min $M_z$ | 1.19 | 0.04 | 0.95 | -0.00 | 2.53 | -0.08 | BC 204 |
| 228 | RC1 | 28 | 0 | Max N | 2.33 | -0.03 | -0.65 | 0.00 | 1.73 | -0.07 | BC 408 |
| | | | | Min N | -3.85 | -0.02 | -0.95 | -0.00 | 2.52 | -0.05 | BC 149 |
| | | | | Max $V_y$ | 1.70 | -0.00 | -0.65 | -0.00 | 1.73 | -0.00 | BC 449 |
| | | | | Min $V_y$ | 1.25 | -0.04 | -0.95 | -0.00 | 2.53 | -0.08 | BC 204 |
| | | | | Max $V_z$ | -3.34 | -0.02 | -0.64 | -0.00 | 1.72 | -0.04 | BC 338 |
| | | | | Min $V_z$ | -1.69 | -0.02 | -1.07 | -0.00 | 2.85 | -0.06 | BC 16 |
| | | | | Max $M_T$ | -2.61 | -0.02 | -0.95 | 0.00 | 2.53 | -0.05 | BC 166 |
| | | | | Min $M_T$ | -1.70 | -0.02 | -0.95 | -0.00 | 2.52 | -0.05 | BC 243 |
| | | | | Max $M_y$ | -1.69 | -0.02 | -1.07 | -0.00 | 2.85 | -0.06 | BC 16 |
| | | | | Min $M_y$ | -3.34 | -0.02 | -0.64 | -0.00 | 1.72 | -0.04 | BC 338 |
| | | | | Max $M_z$ | 1.70 | -0.00 | -0.65 | -0.00 | 1.73 | -0.00 | BC 449 |
| | | | | Min $M_z$ | 1.25 | -0.04 | -0.95 | -0.00 | 2.53 | -0.08 | BC 204 |
| | | 154 | 2250 | Max N | 2.33 | -0.03 | -0.89 | 0.00 | -0.00 | 0.00 | BC 408 |
| | | | | Min N | -3.85 | -0.02 | -1.29 | -0.00 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_y$ | 1.70 | -0.00 | -0.89 | -0.00 | -0.00 | 0.00 | BC 449 |
| | | | | Min $V_y$ | 1.25 | -0.04 | -1.30 | -0.00 | 0.00 | 0.00 | BC 204 |
| | | | | Max $V_z$ | -3.34 | -0.02 | -0.88 | -0.00 | 0.00 | 0.00 | BC 338 |
| | | | | Min $V_z$ | -1.69 | -0.02 | -1.46 | -0.00 | -0.00 | 0.00 | BC 16 |
| | | | | Max $M_T$ | -2.61 | -0.02 | -1.30 | 0.00 | -0.00 | 0.00 | BC 166 |
| | | | | Min $M_T$ | -1.70 | -0.02 | -1.29 | -0.00 | -0.00 | 0.00 | BC 243 |
| | | | | Max $M_y$ | -2.51 | -0.01 | -0.88 | 0.00 | 0.00 | -0.00 | BC 378 |
| | | | | Min $M_y$ | 1.25 | -0.04 | -1.30 | -0.00 | -0.00 | 0.00 | BC 232 |
| | | | | Max $M_z$ | 2.31 | -0.03 | -0.89 | 0.00 | 0.00 | 0.00 | BC 384 |
| | | | | Min $M_z$ | 1.81 | -0.04 | -1.30 | 0.00 | 0.00 | -0.00 | BC 160 |
| | | 28 | 0 | Max N | 2.33 | -0.03 | -0.65 | 0.00 | 1.73 | -0.07 | BC 408 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 228 | RC1 | 28 | 0 | Min N | ▷ -3.85 | -0.02 | -0.95 | -0.00 | 2.52 | -0.05 | BC 149 |
| | | 28 | 0 | Max $V_y$ | 1.70 | ▷ -0.00 | -0.65 | -0.00 | 1.73 | -0.00 | BC 449 |
| | | 28 | 0 | Min $V_y$ | 1.25 | ▷ -0.04 | -0.95 | -0.00 | 2.53 | -0.08 | BC 204 |
| | | 28 | 0 | Max $V_z$ | -3.34 | -0.02 | ▷ -0.64 | -0.00 | 1.72 | -0.04 | BC 338 |
| | | 154 | 2250 | Min $V_z$ | -1.69 | -0.02 | ▷ -1.46 | -0.00 | -0.00 | 0.00 | BC 16 |
| | | 28 | 0 | Max $M_T$ | -2.61 | -0.02 | -0.95 | ▷ 0.00 | 2.53 | -0.05 | BC 166 |
| | | 28 | 0 | Min $M_T$ | -1.70 | -0.02 | -0.95 | ▷ -0.00 | 2.52 | -0.05 | BC 243 |
| | | 28 | 0 | Max $M_y$ | -1.69 | -0.02 | -1.07 | -0.00 | ▷ 2.85 | -0.06 | BC 16 |
| | | 154 | 2250 | Min $M_y$ | 1.25 | -0.04 | -1.30 | -0.00 | ▷ -0.00 | 0.00 | BC 232 |
| | | 154 | 2250 | Max $M_z$ | 2.31 | -0.03 | -0.89 | 0.00 | 0.00 | ▷ 0.00 | BC 384 |
| | | 28 | 0 | Min $M_z$ | 1.25 | -0.04 | -0.95 | -0.00 | 2.53 | ▷ -0.08 | BC 204 |
| 228 | RC1 | 28 | 0 | MAX N | ▷ 2.33 | -0.03 | -0.65 | 0.00 | 1.73 | -0.07 | BC 408 |
| 228 | RC1 | 28 | 0 | MIN N | ▷ -3.85 | -0.02 | -0.95 | 0.00 | 2.52 | -0.05 | BC 149 |
| 208 | RC1 | 155 | 0 | MAX $V_y$ | 1.19 | ▷ 0.04 | 1.30 | 0.00 | 0.00 | 0.00 | BC 204 |
| 228 | RC1 | 28 | 0 | MIN $V_y$ | 1.25 | ▷ -0.04 | -0.95 | 0.00 | 2.53 | -0.08 | BC 204 |
| 208 | RC1 | 155 | 0 | MAX $V_z$ | -2.09 | 0.03 | ▷ 1.47 | 0.00 | 0.00 | 0.00 | BC 11 |
| 228 | RC1 | 154 | 2250 | MIN $V_z$ | -1.69 | -0.02 | ▷ -1.46 | 0.00 | 0.00 | 0.00 | BC 16 |
| 208 | RC1 | 155 | 0 | MAX $M_T$ | -2.41 | 0.02 | 1.30 | ▷ 0.00 | 0.00 | 0.00 | BC 166 |
| 228 | RC1 | 28 | 0 | MIN $M_T$ | -1.70 | -0.02 | -0.95 | ▷ 0.00 | 2.52 | -0.05 | BC 243 |
| 208 | RC1 | 28 | 2250 | MAX $M_y$ | -2.09 | 0.03 | 1.08 | 0.00 | ▷ 2.86 | -0.06 | BC 11 |
| 208 | RC1 | 155 | 0 | MIN $M_y$ | 1.69 | 0.04 | 1.30 | 0.00 | ▷ 0.00 | 0.00 | BC 160 |
| 208 | RC1 | 155 | 0 | MAX $M_z$ | 2.12 | 0.03 | 0.88 | 0.00 | 0.00 | ▷ 0.00 | BC 384 |
| 208 | RC1 | 28 | 2250 | MIN $M_z$ | 1.19 | 0.04 | 0.95 | 0.00 | 2.53 | ▷ -0.08 | BC 204 |
| | **Doorgaande staven No. 48: Doorgaande staven 48** | | | | | | | | | | |
| 209 | RC1 | 154 | 0 | Max N | ▷ 2.20 | 0.05 | 0.89 | -0.12 | -0.00 | 0.00 | BC 413 |
| | | | | Min N | ▷ -2.43 | 0.04 | 0.89 | -0.12 | 0.00 | 0.00 | BC 446 |
| | | | | Max $V_y$ | -2.24 | ▷ 0.10 | 1.31 | -0.48 | -0.00 | 0.00 | BC 154 |
| | | | | Min $V_y$ | 1.86 | ▷ 0.02 | 0.89 | -0.12 | 0.00 | 0.00 | BC 360 |
| | | | | Max $V_z$ | -1.42 | 0.08 | ▷ 1.47 | -0.28 | 0.00 | 0.00 | BC 27 |
| | | | | Min $V_z$ | -2.37 | 0.03 | ▷ 0.89 | -0.12 | 0.00 | 0.00 | BC 450 |
| | | | | Max $M_T$ | 2.14 | 0.05 | 0.89 | ▷ -0.11 | 0.00 | 0.00 | BC 389 |
| | | | | Min $M_T$ | -2.24 | 0.10 | 1.31 | ▷ -0.48 | -0.00 | 0.00 | BC 154 |
| | | | | Max $M_y$ | -1.89 | 0.04 | 0.89 | -0.20 | ▷ 0.00 | -0.00 | BC 378 |
| | | | | Min $M_y$ | 1.49 | 0.04 | 1.31 | -0.25 | ▷ -0.00 | 0.00 | BC 232 |
| | | | | Max $M_z$ | -1.97 | 0.09 | 1.31 | -0.42 | -0.00 | ▷ 0.00 | BC 100 |
| | | | | Min $M_z$ | -1.67 | 0.07 | 1.30 | -0.26 | 0.00 | ▷ -0.00 | BC 182 |
| | | 31 | 2250 | Max N | ▷ 2.20 | 0.05 | 0.65 | -0.12 | 1.74 | -0.11 | BC 413 |
| | | | | Min N | ▷ -2.43 | 0.04 | 0.65 | -0.12 | 1.73 | -0.09 | BC 446 |
| | | | | Max $V_y$ | -2.24 | ▷ 0.10 | 0.96 | -0.48 | 2.55 | -0.23 | BC 154 |
| | | | | Min $V_y$ | 1.86 | ▷ 0.02 | 0.65 | -0.12 | 1.74 | -0.05 | BC 360 |
| | | | | Max $V_z$ | -1.42 | 0.08 | ▷ 1.08 | -0.28 | 2.87 | -0.19 | BC 27 |
| | | | | Min $V_z$ | -2.37 | 0.03 | ▷ 0.65 | -0.12 | 1.73 | -0.08 | BC 450 |
| | | | | Max $M_T$ | 2.14 | 0.05 | 0.65 | ▷ -0.11 | 1.74 | -0.10 | BC 389 |
| | | | | Min $M_T$ | -2.24 | 0.10 | 0.96 | ▷ -0.48 | 2.55 | -0.23 | BC 154 |
| | | | | Max $M_y$ | -1.42 | 0.08 | 1.08 | -0.28 | ▷ 2.87 | -0.19 | BC 27 |
| | | | | Min $M_y$ | -2.37 | 0.03 | 0.65 | -0.12 | ▷ 1.73 | -0.08 | BC 450 |
| | | | | Max $M_z$ | 1.86 | 0.02 | 0.65 | -0.12 | 1.74 | ▷ -0.05 | BC 360 |
| | | | | Min $M_z$ | -2.24 | 0.10 | 0.96 | -0.48 | 2.55 | ▷ -0.23 | BC 154 |
| | | 154 | 0 | Max N | ▷ 2.20 | 0.05 | 0.89 | -0.12 | -0.00 | 0.00 | BC 413 |
| | | 154 | 0 | Min N | ▷ -2.43 | 0.04 | 0.89 | -0.12 | 0.00 | 0.00 | BC 446 |
| | | 154 | 0 | Max $V_y$ | -2.24 | ▷ 0.10 | 1.31 | -0.48 | -0.00 | 0.00 | BC 154 |
| | | 154 | 0 | Min $V_y$ | 1.86 | ▷ 0.02 | 0.89 | -0.12 | 0.00 | 0.00 | BC 360 |
| | | 154 | 0 | Max $V_z$ | -1.42 | 0.08 | ▷ 1.47 | -0.28 | 0.00 | 0.00 | BC 27 |
| | | 31 | 2250 | Min $V_z$ | -2.37 | 0.03 | ▷ 0.65 | -0.12 | 1.73 | -0.08 | BC 450 |
| | | 154 | 0 | Max $M_T$ | 2.14 | 0.05 | 0.89 | ▷ -0.11 | 0.00 | 0.00 | BC 389 |
| | | 154 | 0 | Min $M_T$ | -2.24 | 0.10 | 1.31 | ▷ -0.48 | -0.00 | 0.00 | BC 154 |
| | | 31 | 2250 | Max $M_y$ | -1.42 | 0.08 | 1.08 | -0.28 | ▷ 2.87 | -0.19 | BC 27 |
| | | 154 | 0 | Min $M_y$ | 1.49 | 0.04 | 1.31 | -0.25 | ▷ -0.00 | 0.00 | BC 232 |
| | | 154 | 0 | Max $M_z$ | -1.97 | 0.09 | 1.31 | -0.42 | -0.00 | ▷ 0.00 | BC 100 |
| | | 31 | 2250 | Min $M_z$ | -2.24 | 0.10 | 0.96 | -0.48 | 2.55 | ▷ -0.23 | BC 154 |
| 231 | RC1 | 31 | 0 | Max N | ▷ 1.50 | -0.05 | -0.64 | -0.11 | 1.71 | -0.10 | BC 417 |
| | | | | Min N | ▷ -8.06 | -0.08 | -0.89 | -0.18 | 2.38 | -0.18 | BC 279 |
| | | | | Max $V_y$ | 1.19 | ▷ -0.02 | -0.64 | -0.12 | 1.71 | -0.05 | BC 360 |
| | | | | Min $V_y$ | -3.51 | ▷ -0.10 | -0.94 | -0.48 | 2.50 | -0.23 | BC 154 |
| | | | | Max $V_z$ | -7.56 | -0.06 | ▷ -0.58 | -0.12 | 1.56 | -0.13 | BC 471 |
| | | | | Min $V_z$ | -1.97 | -0.07 | ▷ -1.07 | -0.19 | 2.84 | -0.15 | BC 25 |
| | | | | Max $M_T$ | 1.50 | -0.05 | -0.64 | ▷ -0.11 | 1.71 | -0.10 | BC 389 |
| | | | | Min $M_T$ | -3.51 | -0.10 | -0.94 | ▷ -0.48 | 2.50 | -0.23 | BC 154 |
| | | | | Max $M_y$ | -1.97 | -0.07 | -1.07 | -0.19 | ▷ 2.84 | -0.15 | BC 25 |
| | | | | Min $M_y$ | -7.56 | -0.06 | -0.58 | -0.12 | ▷ 1.56 | -0.13 | BC 471 |
| | | | | Max $M_z$ | 1.19 | -0.02 | -0.64 | -0.12 | 1.71 | ▷ -0.05 | BC 360 |
| | | | | Min $M_z$ | -3.51 | -0.10 | -0.94 | -0.48 | 2.50 | ▷ -0.23 | BC 154 |
| | | 153 | 2250 | Max N | ▷ 1.50 | -0.05 | -0.88 | -0.11 | -0.00 | 0.00 | BC 417 |
| | | | | Min N | ▷ -8.06 | -0.08 | -1.23 | -0.18 | 0.00 | -0.00 | BC 279 |
| | | | | Max $V_y$ | 1.19 | ▷ -0.02 | -0.88 | -0.12 | 0.00 | 0.00 | BC 360 |
| | | | | Min $V_y$ | -3.51 | ▷ -0.10 | -1.29 | -0.48 | 0.00 | 0.00 | BC 154 |
| | | | | Max $V_z$ | -7.56 | -0.06 | ▷ -0.81 | -0.12 | 0.00 | -0.00 | BC 471 |
| | | | | Min $V_z$ | -1.97 | -0.07 | ▷ -1.46 | -0.19 | 0.00 | 0.00 | BC 25 |
| | | | | Max $M_T$ | 1.50 | -0.05 | -0.88 | ▷ -0.11 | 0.00 | 0.00 | BC 389 |
| | | | | Min $M_T$ | -3.51 | -0.10 | -1.29 | ▷ -0.48 | 0.00 | 0.00 | BC 154 |
| | | | | Max $M_y$ | -8.06 | -0.08 | -1.23 | -0.18 | ▷ 0.00 | -0.00 | BC 279 |
| | | | | Min $M_y$ | 0.26 | -0.04 | -1.29 | -0.25 | ▷ -0.00 | 0.00 | BC 232 |
| | | | | Max $M_z$ | 0.38 | -0.10 | -1.29 | -0.25 | -0.00 | ▷ 0.00 | BC 205 |
| | | | | Min $M_z$ | -7.99 | -0.08 | -1.23 | -0.18 | 0.00 | ▷ -0.00 | BC 219 |
| | | 31 | 0 | Max N | ▷ 1.50 | -0.05 | -0.64 | -0.11 | 1.71 | -0.10 | BC 417 |
| | | 31 | 0 | Min N | ▷ -8.06 | -0.08 | -0.89 | -0.18 | 2.38 | -0.18 | BC 279 |
| | | 31 | 0 | Max $V_y$ | 1.19 | ▷ -0.02 | -0.64 | -0.12 | 1.71 | -0.05 | BC 360 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 231 | RC1 | 31 | 0 | Min $V_y$ | -3.51 | ▷ -0.10 | -0.94 | -0.48 | 2.50 | -0.23 | BC 154 |
| | | 31 | 0 | Max $V_z$ | -7.56 | -0.06 | ▷ -0.58 | -0.12 | 1.56 | -0.13 | BC 471 |
| | | 153 | 2250 | Min $V_z$ | -1.97 | -0.07 | ▷ -1.46 | -0.19 | 0.00 | 0.00 | BC 25 |
| | | 31 | 0 | Max $M_T$ | 1.50 | -0.05 | -0.64 | ▷ -0.11 | 1.71 | -0.10 | BC 389 |
| | | 31 | 0 | Min $M_T$ | -3.51 | -0.10 | -0.94 | ▷ -0.48 | 2.50 | -0.23 | BC 154 |
| | | 31 | 0 | Max $M_y$ | -1.97 | -0.07 | -1.07 | -0.19 | ▷ 2.84 | -0.15 | BC 25 |
| | | 153 | 2250 | Min $M_y$ | 0.26 | -0.04 | -1.29 | -0.25 | ▷ -0.00 | 0.00 | BC 232 |
| | | 153 | 2250 | Max $M_z$ | 0.38 | -0.10 | -1.29 | -0.25 | -0.00 | ▷ 0.00 | BC 205 |
| | | 31 | 0 | Min $M_z$ | -3.51 | -0.10 | -0.94 | -0.48 | 2.50 | ▷ -0.23 | BC 154 |
| 209 | RC1 | 154 | 0 | MAX N | ▷ 2.20 | 0.05 | 0.89 | -0.12 | 0.00 | 0.00 | BC 413 |
| 231 | RC1 | 31 | 0 | MIN N | ▷ -8.06 | -0.08 | -0.89 | -0.18 | 2.38 | -0.18 | BC 279 |
| 209 | RC1 | 154 | 0 | MAX $V_y$ | -2.24 | ▷ 0.10 | 1.31 | -0.48 | 0.00 | 0.00 | BC 154 |
| 231 | RC1 | 31 | 0 | MIN $V_y$ | -3.51 | ▷ -0.10 | -0.94 | -0.48 | 2.50 | -0.23 | BC 154 |
| 209 | RC1 | 154 | 0 | MAX $V_z$ | -1.42 | 0.08 | ▷ 1.47 | -0.28 | 0.00 | 0.00 | BC 27 |
| 231 | RC1 | 153 | 2250 | MIN $V_z$ | -1.97 | -0.07 | ▷ -1.46 | -0.19 | 0.00 | 0.00 | BC 25 |
| 231 | RC1 | 31 | 0 | MAX $M_T$ | 1.50 | -0.05 | -0.64 | ▷ -0.11 | 1.71 | -0.10 | BC 389 |
| 209 | RC1 | 154 | 0 | MIN $M_T$ | -2.24 | 0.10 | 1.31 | ▷ -0.48 | 0.00 | 0.00 | BC 154 |
| 209 | RC1 | 31 | 2250 | MAX $M_y$ | -1.42 | 0.08 | 1.08 | -0.28 | ▷ 2.87 | -0.19 | BC 27 |
| 231 | RC1 | 153 | 2250 | MIN $M_y$ | 0.26 | -0.04 | -1.29 | -0.25 | ▷ 0.00 | 0.00 | BC 232 |
| 231 | RC1 | 153 | 2250 | MAX $M_z$ | 0.38 | -0.10 | -1.29 | -0.25 | 0.00 | ▷ 0.00 | BC 205 |
| 209 | RC1 | 31 | 2250 | MIN $M_z$ | -2.24 | 0.10 | 0.96 | -0.48 | 2.55 | ▷ -0.23 | BC 154 |
| | **Doorgaande staven No. 49: Doorgaande staven 49** | | | | | | | | | | |
| 210 | RC1 | 153 | 0 | Max N | ▷ 1.46 | 0.04 | 0.88 | -0.00 | -0.00 | 0.00 | BC 417 |
| | | | | Min N | ▷ -8.26 | 0.11 | 1.27 | 0.01 | 0.00 | -0.00 | BC 279 |
| | | | | Max $V_y$ | -3.60 | ▷ 0.21 | 1.27 | 0.01 | 0.00 | 0.00 | BC 154 |
| | | | | Min $V_y$ | 1.46 | ▷ 0.04 | 0.88 | -0.00 | 0.00 | 0.00 | BC 389 |
| | | | | Max $V_z$ | -2.14 | 0.11 | ▷ 1.46 | -0.00 | 0.00 | -0.00 | BC 3 |
| | | | | Min $V_z$ | -3.11 | 0.18 | ▷ 0.86 | 0.01 | 0.00 | -0.00 | BC 347 |
| | | | | Max $M_T$ | -3.11 | 0.18 | 0.86 | ▷ 0.01 | 0.00 | 0.00 | BC 346 |
| | | | | Min $M_T$ | 1.17 | 0.08 | 1.30 | ▷ -0.00 | -0.00 | 0.00 | BC 197 |
| | | | | Max $M_y$ | -8.19 | 0.11 | 1.27 | 0.01 | ▷ 0.00 | -0.00 | BC 219 |
| | | | | Min $M_y$ | 0.27 | 0.13 | 1.30 | 0.00 | ▷ -0.00 | 0.00 | BC 232 |
| | | | | Max $M_z$ | 0.29 | 0.13 | 1.30 | 0.00 | -0.00 | ▷ 0.00 | BC 172 |
| | | | | Min $M_z$ | -8.19 | 0.11 | 1.27 | 0.01 | 0.00 | ▷ -0.00 | BC 219 |
| | | 32 | 2250 | Max N | ▷ 1.46 | 0.04 | 0.65 | -0.00 | 1.72 | -0.10 | BC 417 |
| | | | | Min N | ▷ -8.26 | 0.11 | 0.92 | 0.01 | 2.46 | -0.24 | BC 279 |
| | | | | Max $V_y$ | -3.60 | ▷ 0.21 | 0.92 | 0.01 | 2.46 | -0.48 | BC 154 |
| | | | | Min $V_y$ | 1.46 | ▷ 0.04 | 0.65 | -0.00 | 1.72 | -0.10 | BC 389 |
| | | | | Max $V_z$ | -2.14 | 0.11 | ▷ 1.06 | -0.00 | 2.84 | -0.24 | BC 3 |
| | | | | Min $V_z$ | -3.11 | 0.18 | ▷ 0.62 | 0.01 | 1.66 | -0.41 | BC 347 |
| | | | | Max $M_T$ | -3.11 | 0.18 | 0.62 | ▷ 0.01 | 1.66 | -0.41 | BC 346 |
| | | | | Min $M_T$ | 1.17 | 0.08 | 0.95 | ▷ -0.00 | 2.53 | -0.17 | BC 197 |
| | | | | Max $M_y$ | -2.14 | 0.11 | 1.06 | -0.00 | ▷ 2.84 | -0.24 | BC 3 |
| | | | | Min $M_y$ | -3.11 | 0.18 | 0.62 | 0.01 | ▷ 1.66 | -0.41 | BC 347 |
| | | | | Max $M_z$ | 1.46 | 0.04 | 0.65 | -0.00 | 1.72 | ▷ -0.10 | BC 389 |
| | | | | Min $M_z$ | -3.60 | 0.21 | 0.92 | 0.01 | 2.46 | ▷ -0.48 | BC 154 |
| | | 153 | 0 | Max N | ▷ 1.46 | 0.04 | 0.88 | -0.00 | -0.00 | 0.00 | BC 417 |
| | | 153 | 0 | Min N | ▷ -8.26 | 0.11 | 1.27 | 0.01 | 0.00 | -0.00 | BC 279 |
| | | 153 | 0 | Max $V_y$ | -3.60 | ▷ 0.21 | 1.27 | 0.01 | 0.00 | 0.00 | BC 154 |
| | | 153 | 0 | Min $V_y$ | 1.46 | ▷ 0.04 | 0.88 | -0.00 | 0.00 | 0.00 | BC 389 |
| | | 153 | 0 | Max $V_z$ | -2.14 | 0.11 | ▷ 1.46 | -0.00 | 0.00 | -0.00 | BC 3 |
| | | 32 | 2250 | Min $V_z$ | -3.11 | 0.18 | ▷ 0.62 | 0.01 | 1.66 | -0.41 | BC 347 |
| | | 153 | 0 | Max $M_T$ | -3.11 | 0.18 | 0.86 | ▷ 0.01 | 0.00 | 0.00 | BC 346 |
| | | 153 | 0 | Min $M_T$ | 1.17 | 0.08 | 1.30 | ▷ -0.00 | -0.00 | 0.00 | BC 197 |
| | | 32 | 2250 | Max $M_y$ | -2.14 | 0.11 | 1.06 | -0.00 | ▷ 2.84 | -0.24 | BC 3 |
| | | 153 | 0 | Min $M_y$ | 0.27 | 0.13 | 1.30 | 0.00 | ▷ -0.00 | 0.00 | BC 232 |
| | | 153 | 0 | Max $M_z$ | 0.29 | 0.13 | 1.30 | 0.00 | -0.00 | ▷ 0.00 | BC 172 |
| | | 32 | 2250 | Min $M_z$ | -3.60 | 0.21 | 0.92 | 0.01 | 2.46 | ▷ -0.48 | BC 154 |
| 234 | RC1 | 32 | 0 | Max N | ▷ 1.48 | -0.05 | -0.65 | 0.01 | 1.73 | -0.11 | BC 413 |
| | | | | Min N | ▷ -5.77 | -0.08 | -0.65 | 0.01 | 1.73 | -0.18 | BC 355 |
| | | | | Max $V_y$ | 1.44 | ▷ -0.04 | -0.65 | -0.00 | 1.72 | -0.10 | BC 389 |
| | | | | Min $V_y$ | 0.01 | ▷ -0.21 | -0.98 | 0.03 | 2.59 | -0.48 | BC 154 |
| | | | | Max $V_z$ | -0.05 | -0.07 | ▷ -0.64 | 0.02 | 1.70 | -0.16 | BC 380 |
| | | | | Min $V_z$ | 0.05 | -0.14 | ▷ -1.09 | 0.02 | 2.90 | -0.31 | BC 27 |
| | | | | Max $M_T$ | 0.01 | -0.21 | -0.98 | ▷ 0.03 | 2.59 | -0.48 | BC 154 |
| | | | | Min $M_T$ | 1.44 | -0.04 | -0.65 | ▷ -0.00 | 1.72 | -0.10 | BC 389 |
| | | | | Max $M_y$ | 0.05 | -0.14 | -1.09 | 0.02 | ▷ 2.90 | -0.31 | BC 27 |
| | | | | Min $M_y$ | -0.05 | -0.07 | -0.64 | 0.02 | ▷ 1.70 | -0.16 | BC 380 |
| | | | | Max $M_z$ | 1.44 | -0.04 | -0.65 | -0.00 | 1.72 | ▷ -0.10 | BC 389 |
| | | | | Min $M_z$ | 0.01 | -0.21 | -0.98 | 0.03 | 2.59 | ▷ -0.48 | BC 154 |
| | | 152 | 2250 | Max N | ▷ 1.48 | -0.05 | -0.89 | 0.01 | 0.00 | 0.00 | BC 413 |
| | | | | Min N | ▷ -5.77 | -0.08 | -0.89 | 0.01 | 0.00 | -0.00 | BC 355 |
| | | | | Max $V_y$ | 1.44 | ▷ -0.04 | -0.88 | -0.00 | 0.00 | 0.00 | BC 389 |
| | | | | Min $V_y$ | 0.01 | ▷ -0.21 | -1.32 | 0.03 | 0.00 | 0.00 | BC 154 |
| | | | | Max $V_z$ | -0.05 | -0.07 | ▷ -0.87 | 0.02 | 0.00 | -0.00 | BC 380 |
| | | | | Min $V_z$ | 0.05 | -0.14 | ▷ -1.49 | 0.02 | 0.00 | 0.00 | BC 27 |
| | | | | Max $M_T$ | 0.01 | -0.21 | -1.32 | ▷ 0.03 | 0.00 | 0.00 | BC 154 |
| | | | | Min $M_T$ | 1.44 | -0.04 | -0.88 | ▷ -0.00 | 0.00 | 0.00 | BC 389 |
| | | | | Max $M_y$ | -5.38 | -0.10 | -1.30 | 0.01 | ▷ 0.00 | -0.00 | BC 259 |
| | | | | Min $M_y$ | -0.29 | -0.13 | -1.29 | 0.01 | ▷ -0.00 | 0.00 | BC 200 |
| | | | | Max $M_z$ | -0.30 | -0.13 | -1.29 | 0.01 | -0.00 | ▷ 0.00 | BC 172 |
| | | | | Min $M_z$ | -5.38 | -0.10 | -1.30 | 0.01 | 0.00 | ▷ -0.00 | BC 259 |
| | | 32 | 0 | Max N | ▷ 1.48 | -0.05 | -0.65 | 0.01 | 1.73 | -0.11 | BC 413 |
| | | 32 | 0 | Min N | ▷ -5.77 | -0.08 | -0.65 | 0.01 | 1.73 | -0.18 | BC 355 |
| | | 32 | 0 | Max $V_y$ | 1.44 | ▷ -0.04 | -0.65 | -0.00 | 1.72 | -0.10 | BC 389 |
| | | 32 | 0 | Min $V_y$ | 0.01 | ▷ -0.21 | -0.98 | 0.03 | 2.59 | -0.48 | BC 154 |
| | | 32 | 0 | Max $V_z$ | -0.05 | -0.07 | ▷ -0.64 | 0.02 | 1.70 | -0.16 | BC 380 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 234 | RC1 | 152 | 2250 | Min $V_z$ | 0.05 | -0.14 | ▷ -1.49 | 0.02 | 0.00 | 0.00 | BC 27 |
| | | 32 | 0 | Max $M_T$ | 0.01 | -0.21 | -0.98 | ▷ 0.03 | 2.59 | -0.48 | BC 154 |
| | | 32 | 0 | Min $M_T$ | 1.44 | -0.04 | -0.65 | ▷ -0.00 | 1.72 | -0.10 | BC 389 |
| | | 32 | 0 | Max $M_y$ | 0.05 | -0.14 | -1.09 | 0.02 | ▷ 2.90 | -0.31 | BC 27 |
| | | 152 | 2250 | Min $M_y$ | -0.29 | -0.13 | -1.29 | 0.01 | ▷ -0.00 | 0.00 | BC 200 |
| | | 152 | 2250 | Max $M_z$ | -0.30 | -0.13 | -1.29 | 0.01 | -0.00 | ▷ 0.00 | BC 172 |
| | | 32 | 0 | Min $M_z$ | 0.01 | -0.21 | -0.98 | 0.03 | 2.59 | ▷ -0.48 | BC 154 |
| 234 | RC1 | 32 | 0 | MAX N | ▷ 1.48 | -0.05 | -0.65 | 0.01 | 1.73 | -0.11 | BC 413 |
| 210 | RC1 | 153 | 0 | MIN N | ▷ -8.26 | 0.11 | 1.27 | 0.01 | 0.00 | 0.00 | BC 279 |
| 210 | RC1 | 153 | 0 | MAX $V_y$ | -3.60 | ▷ 0.21 | 1.27 | 0.01 | 0.00 | 0.00 | BC 154 |
| 234 | RC1 | 32 | 0 | MIN $V_y$ | 0.01 | ▷ -0.21 | -0.98 | 0.03 | 2.59 | -0.48 | BC 154 |
| 210 | RC1 | 153 | 0 | MAX $V_z$ | -2.14 | 0.11 | ▷ 1.46 | 0.00 | 0.00 | 0.00 | BC 3 |
| 234 | RC1 | 152 | 2250 | MIN $V_z$ | 0.05 | -0.14 | ▷ -1.49 | 0.02 | 0.00 | 0.00 | BC 27 |
| 234 | RC1 | 32 | 0 | MAX $M_T$ | 0.01 | -0.21 | -0.98 | ▷ 0.03 | 2.59 | -0.48 | BC 154 |
| 210 | RC1 | 153 | 0 | MIN $M_T$ | 1.17 | 0.08 | 1.30 | ▷ 0.00 | 0.00 | 0.00 | BC 197 |
| 234 | RC1 | 32 | 0 | MAX $M_y$ | 0.05 | -0.14 | -1.09 | 0.02 | ▷ 2.90 | -0.31 | BC 27 |
| 234 | RC1 | 152 | 2250 | MIN $M_y$ | -0.29 | -0.13 | -1.29 | 0.01 | ▷ 0.00 | 0.00 | BC 200 |
| 234 | RC1 | 152 | 2250 | MAX $M_z$ | -0.30 | -0.13 | -1.29 | 0.01 | 0.00 | ▷ 0.00 | BC 172 |
| 210 | RC1 | 32 | 2250 | MIN $M_z$ | -3.60 | 0.21 | 0.92 | 0.01 | 2.46 | ▷ -0.48 | BC 154 |
| | **Doorgaande staven No. 50: Doorgaande staven 50** | | | | | | | | | | |
| 211 | RC1 | 152 | 0 | Max N | ▷ 1.20 | 0.05 | 0.87 | 0.11 | 0.00 | 0.00 | BC 413 |
| | | | | Min N | ▷ -5.55 | 0.06 | 0.82 | 0.12 | 0.00 | -0.00 | BC 355 |
| | | | | Max $V_y$ | -1.33 | ▷ 0.12 | 1.26 | 0.47 | 0.00 | 0.00 | BC 138 |
| | | | | Min $V_y$ | -4.03 | ▷ 0.03 | 0.83 | 0.11 | 0.00 | -0.00 | BC 447 |
| | | | | Max $V_z$ | 0.07 | 0.06 | ▷ 1.43 | 0.19 | -0.00 | 0.00 | BC 16 |
| | | | | Min $V_z$ | -5.55 | 0.06 | ▷ 0.82 | 0.12 | 0.00 | -0.00 | BC 355 |
| | | | | Max $M_T$ | -0.99 | 0.12 | 1.26 | ▷ 0.47 | 0.00 | -0.00 | BC 156 |
| | | | | Min $M_T$ | 1.19 | 0.05 | 0.87 | ▷ 0.11 | -0.00 | 0.00 | BC 381 |
| | | | | Max $M_y$ | -5.20 | 0.07 | 1.23 | 0.17 | ▷ 0.00 | -0.00 | BC 259 |
| | | | | Min $M_y$ | -0.23 | 0.08 | 1.27 | 0.26 | ▷ -0.00 | 0.00 | BC 200 |
| | | | | Max $M_z$ | -0.24 | 0.08 | 1.27 | 0.26 | -0.00 | ▷ 0.00 | BC 172 |
| | | | | Min $M_z$ | -5.20 | 0.07 | 1.23 | 0.17 | 0.00 | ▷ -0.00 | BC 259 |
| | | 33 | 2150 | Max N | ▷ 1.20 | 0.05 | 0.65 | 0.11 | 1.63 | -0.11 | BC 413 |
| | | | | Min N | ▷ -5.55 | 0.06 | 0.59 | 0.12 | 1.52 | -0.12 | BC 355 |
| | | | | Max $V_y$ | -1.33 | ▷ 0.12 | 0.92 | 0.47 | 2.34 | -0.26 | BC 138 |
| | | | | Min $V_y$ | -4.03 | ▷ 0.03 | 0.61 | 0.11 | 1.55 | -0.07 | BC 447 |
| | | | | Max $V_z$ | 0.07 | 0.06 | ▷ 1.06 | 0.19 | 2.68 | -0.14 | BC 16 |
| | | | | Min $V_z$ | -5.55 | 0.06 | ▷ 0.59 | 0.12 | 1.52 | -0.12 | BC 355 |
| | | | | Max $M_T$ | -0.99 | 0.12 | 0.93 | ▷ 0.47 | 2.35 | -0.26 | BC 156 |
| | | | | Min $M_T$ | 1.19 | 0.05 | 0.65 | ▷ 0.11 | 1.63 | -0.11 | BC 381 |
| | | | | Max $M_y$ | 0.07 | 0.06 | 1.06 | 0.19 | ▷ 2.68 | -0.14 | BC 16 |
| | | | | Min $M_y$ | -5.55 | 0.06 | 0.59 | 0.12 | ▷ 1.52 | -0.12 | BC 355 |
| | | | | Max $M_z$ | -4.03 | 0.03 | 0.61 | 0.11 | 1.55 | ▷ -0.07 | BC 447 |
| | | | | Min $M_z$ | -1.33 | 0.12 | 0.92 | 0.47 | 2.34 | ▷ -0.26 | BC 138 |
| | | 152 | 0 | Max N | ▷ 1.20 | 0.05 | 0.87 | 0.11 | 0.00 | 0.00 | BC 413 |
| | | 152 | 0 | Min N | ▷ -5.55 | 0.06 | 0.82 | 0.12 | 0.00 | -0.00 | BC 355 |
| | | 152 | 0 | Max $V_y$ | -1.33 | ▷ 0.12 | 1.26 | 0.47 | 0.00 | 0.00 | BC 138 |
| | | 152 | 0 | Min $V_y$ | -4.03 | ▷ 0.03 | 0.83 | 0.11 | 0.00 | -0.00 | BC 447 |
| | | 152 | 0 | Max $V_z$ | 0.07 | 0.06 | ▷ 1.43 | 0.19 | -0.00 | 0.00 | BC 16 |
| | | 33 | 2150 | Min $V_z$ | -5.55 | 0.06 | ▷ 0.59 | 0.12 | 1.52 | -0.12 | BC 355 |
| | | 152 | 0 | Max $M_T$ | -0.99 | 0.12 | 1.26 | ▷ 0.47 | 0.00 | -0.00 | BC 156 |
| | | 152 | 0 | Min $M_T$ | 1.19 | 0.05 | 0.87 | ▷ 0.11 | -0.00 | 0.00 | BC 381 |
| | | 33 | 2150 | Max $M_y$ | 0.07 | 0.06 | 1.06 | 0.19 | ▷ 2.68 | -0.14 | BC 16 |
| | | 152 | 0 | Min $M_y$ | -0.23 | 0.08 | 1.27 | 0.26 | ▷ -0.00 | 0.00 | BC 200 |
| | | 152 | 0 | Max $M_z$ | -0.24 | 0.08 | 1.27 | 0.26 | -0.00 | ▷ 0.00 | BC 172 |
| | | 33 | 2150 | Min $M_z$ | -1.33 | 0.12 | 0.92 | 0.47 | 2.34 | ▷ -0.26 | BC 138 |
| 237 | RC1 | 33 | 0 | Max N | ▷ 0.22 | -0.05 | -0.63 | 0.12 | 1.60 | -0.11 | BC 357 |
| | | | | Min N | ▷ -0.24 | -0.03 | -0.67 | 0.12 | 1.69 | -0.07 | BC 447 |
| | | | | Max $V_y$ | -0.24 | ▷ -0.03 | -0.67 | 0.12 | 1.69 | -0.07 | BC 447 |
| | | | | Min $V_y$ | 0.04 | ▷ -0.12 | -0.95 | 0.48 | 2.39 | -0.26 | BC 138 |
| | | | | Max $V_z$ | 0.21 | -0.05 | ▷ -0.63 | 0.11 | 1.60 | -0.11 | BC 413 |
| | | | | Min $V_z$ | 0.04 | -0.08 | ▷ -1.07 | 0.28 | 2.71 | -0.18 | BC 4 |
| | | | | Max $M_T$ | 0.04 | -0.12 | -0.95 | ▷ 0.48 | 2.39 | -0.26 | BC 153 |
| | | | | Min $M_T$ | 0.21 | -0.05 | -0.63 | ▷ 0.11 | 1.60 | -0.11 | BC 381 |
| | | | | Max $M_y$ | 0.04 | -0.08 | -1.07 | 0.28 | ▷ 2.71 | -0.18 | BC 4 |
| | | | | Min $M_y$ | 0.21 | -0.05 | -0.63 | 0.11 | ▷ 1.60 | -0.11 | BC 413 |
| | | | | Max $M_z$ | -0.24 | -0.03 | -0.67 | 0.12 | 1.69 | ▷ -0.07 | BC 447 |
| | | | | Min $M_z$ | 0.04 | -0.12 | -0.95 | 0.48 | 2.39 | ▷ -0.26 | BC 138 |
| | | 151 | 2150 | Max N | ▷ 0.22 | -0.05 | -0.86 | 0.12 | -0.00 | 0.00 | BC 357 |
| | | | | Min N | ▷ -0.24 | -0.03 | -0.90 | 0.12 | 0.00 | 0.00 | BC 447 |
| | | | | Max $V_y$ | -0.24 | ▷ -0.03 | -0.90 | 0.12 | 0.00 | 0.00 | BC 447 |
| | | | | Min $V_y$ | 0.04 | ▷ -0.12 | -1.28 | 0.48 | 0.00 | 0.00 | BC 138 |
| | | | | Max $V_z$ | 0.21 | -0.05 | ▷ -0.86 | 0.11 | 0.00 | 0.00 | BC 413 |
| | | | | Min $V_z$ | 0.04 | -0.08 | ▷ -1.45 | 0.28 | 0.00 | 0.00 | BC 4 |
| | | | | Max $M_T$ | 0.04 | -0.12 | -1.28 | ▷ 0.48 | 0.00 | 0.00 | BC 153 |
| | | | | Min $M_T$ | 0.21 | -0.05 | -0.86 | ▷ 0.11 | 0.00 | 0.00 | BC 381 |
| | | | | Max $M_y$ | 0.02 | -0.06 | -1.27 | 0.18 | ▷ 0.00 | 0.00 | BC 160 |
| | | | | Min $M_y$ | -0.20 | -0.07 | -1.31 | 0.17 | ▷ -0.00 | 0.00 | BC 287 |
| | | | | Max $M_z$ | 0.03 | -0.07 | -1.44 | 0.20 | 0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.02 | -0.08 | -1.27 | 0.26 | 0.00 | ▷ -0.00 | BC 172 |
| | | 33 | 0 | Max N | ▷ 0.22 | -0.05 | -0.63 | 0.12 | 1.60 | -0.11 | BC 357 |
| | | 33 | 0 | Min N | ▷ -0.24 | -0.03 | -0.67 | 0.12 | 1.69 | -0.07 | BC 447 |
| | | 33 | 0 | Max $V_y$ | -0.24 | ▷ -0.03 | -0.67 | 0.12 | 1.69 | -0.07 | BC 447 |
| | | 33 | 0 | Min $V_y$ | 0.04 | ▷ -0.12 | -0.95 | 0.48 | 2.39 | -0.26 | BC 138 |
| | | 33 | 0 | Max $V_z$ | 0.21 | -0.05 | ▷ -0.63 | 0.11 | 1.60 | -0.11 | BC 413 |
| | | 151 | 2150 | Min $V_z$ | 0.04 | -0.08 | ▷ -1.45 | 0.28 | 0.00 | 0.00 | BC 4 |
| | | 33 | 0 | Max $M_T$ | 0.04 | -0.12 | -0.95 | ▷ 0.48 | 2.39 | -0.26 | BC 153 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 237 | RC1 | 33 | 0 | Min $M_T$ | 0.21 | -0.05 | -0.63 | ▷ 0.11 | 1.60 | -0.11 | BC 381 |
| | | 33 | 0 | Max $M_y$ | 0.04 | -0.08 | -1.07 | 0.28 | ▷ 2.71 | -0.18 | BC 4 |
| | | 151 | 2150 | Min $M_y$ | -0.20 | -0.07 | -1.31 | 0.17 | ▷ -0.00 | 0.00 | BC 287 |
| | | 151 | 2150 | Max $M_z$ | 0.03 | -0.07 | -1.44 | 0.20 | 0.00 | ▷ 0.00 | BC 1 |
| | | 33 | 0 | Min $M_z$ | 0.04 | -0.12 | -0.95 | 0.48 | 2.39 | ▷ -0.26 | BC 138 |
| 211 | RC1 | 152 | 0 | MAX N | ▷ 1.20 | 0.05 | 0.87 | 0.11 | 0.00 | 0.00 | BC 413 |
| 211 | RC1 | 152 | 0 | MIN N | ▷ -5.55 | 0.06 | 0.82 | 0.12 | 0.00 | 0.00 | BC 355 |
| 211 | RC1 | 152 | 0 | MAX $V_y$ | -1.33 | ▷ 0.12 | 1.26 | 0.47 | 0.00 | 0.00 | BC 138 |
| 237 | RC1 | 33 | 0 | MIN $V_y$ | 0.04 | ▷ -0.12 | -0.95 | 0.48 | 2.39 | -0.26 | BC 138 |
| 211 | RC1 | 152 | 0 | MAX $V_z$ | 0.07 | 0.06 | ▷ 1.43 | 0.19 | 0.00 | 0.00 | BC 16 |
| 237 | RC1 | 151 | 2150 | MIN $V_z$ | 0.04 | -0.08 | ▷ -1.45 | 0.28 | 0.00 | 0.00 | BC 4 |
| 237 | RC1 | 33 | 0 | MAX $M_T$ | 0.04 | -0.12 | -0.95 | ▷ 0.48 | 2.39 | -0.26 | BC 153 |
| 211 | RC1 | 152 | 0 | MIN $M_T$ | 1.19 | 0.05 | 0.87 | ▷ 0.11 | 0.00 | 0.00 | BC 381 |
| 237 | RC1 | 33 | 0 | MAX $M_y$ | 0.04 | -0.08 | -1.07 | 0.28 | ▷ 2.71 | -0.18 | BC 4 |
| 211 | RC1 | 152 | 0 | MIN $M_y$ | -0.23 | 0.08 | 1.27 | 0.26 | ▷ 0.00 | 0.00 | BC 200 |
| 211 | RC1 | 152 | 0 | MAX $M_z$ | -0.24 | 0.08 | 1.27 | 0.26 | 0.00 | ▷ 0.00 | BC 172 |
| 211 | RC1 | 33 | 2150 | MIN $M_z$ | -1.33 | 0.12 | 0.92 | 0.47 | 2.34 | ▷ -0.26 | BC 138 |
| | **Doorgaande staven No. 51: Doorgaande staven 51** | | | | | | | | | | |
| 213 | RC1 | 162 | 0 | Max N | ▷ 0.74 | 0.02 | 0.88 | -0.00 | 0.00 | 0.00 | BC 408 |
| | | | | Min N | ▷ -1.53 | 0.26 | 1.32 | -0.03 | 0.00 | 0.00 | BC 146 |
| | | | | Max $V_y$ | -1.52 | ▷ 0.26 | 1.32 | -0.03 | 0.00 | 0.00 | BC 138 |
| | | | | Min $V_y$ | -0.80 | ▷ 0.02 | 0.89 | -0.01 | 0.00 | 0.00 | BC 446 |
| | | | | Max $V_z$ | -0.90 | 0.13 | ▷ 1.48 | -0.02 | 0.00 | 0.00 | BC 22 |
| | | | | Min $V_z$ | 0.72 | 0.02 | ▷ 0.88 | -0.00 | 0.00 | 0.00 | BC 356 |
| | | | | Max $M_T$ | -0.66 | 0.02 | 0.89 | ▷ -0.00 | 0.00 | 0.00 | BC 363 |
| | | | | Min $M_T$ | -1.50 | 0.26 | 1.32 | ▷ -0.03 | 0.00 | 0.00 | BC 139 |
| | | | | Max $M_y$ | -0.82 | 0.04 | 1.30 | -0.02 | ▷ 0.00 | -0.00 | BC 162 |
| | | | | Min $M_y$ | -0.83 | 0.04 | 1.30 | -0.02 | ▷ -0.00 | 0.00 | BC 198 |
| | | | | Max $M_z$ | -0.67 | 0.08 | 1.47 | -0.01 | 0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.82 | 0.04 | 1.30 | -0.02 | 0.00 | ▷ -0.00 | BC 162 |
| | | 38 | 2250 | Max N | ▷ 0.74 | 0.02 | 0.65 | -0.00 | 1.72 | -0.05 | BC 408 |
| | | | | Min N | ▷ -1.53 | 0.26 | 0.97 | -0.03 | 2.57 | -0.59 | BC 146 |
| | | | | Max $V_y$ | -1.52 | ▷ 0.26 | 0.97 | -0.03 | 2.57 | -0.59 | BC 138 |
| | | | | Min $V_y$ | -0.80 | ▷ 0.02 | 0.65 | -0.01 | 1.73 | -0.04 | BC 446 |
| | | | | Max $V_z$ | -0.90 | 0.13 | ▷ 1.09 | -0.02 | 2.88 | -0.29 | BC 22 |
| | | | | Min $V_z$ | 0.72 | 0.02 | ▷ 0.65 | -0.00 | 1.72 | -0.06 | BC 356 |
| | | | | Max $M_T$ | -0.66 | 0.02 | 0.65 | ▷ -0.00 | 1.73 | -0.05 | BC 363 |
| | | | | Min $M_T$ | -1.50 | 0.26 | 0.97 | ▷ -0.03 | 2.57 | -0.59 | BC 139 |
| | | | | Max $M_y$ | -0.90 | 0.13 | 1.09 | -0.02 | ▷ 2.88 | -0.29 | BC 22 |
| | | | | Min $M_y$ | 0.72 | 0.02 | 0.65 | -0.00 | ▷ 1.72 | -0.06 | BC 356 |
| | | | | Max $M_z$ | -0.80 | 0.02 | 0.65 | -0.01 | 1.73 | ▷ -0.04 | BC 446 |
| | | | | Min $M_z$ | -1.52 | 0.26 | 0.97 | -0.03 | 2.57 | ▷ -0.59 | BC 138 |
| | | 162 | 0 | Max N | ▷ 0.74 | 0.02 | 0.88 | -0.00 | 0.00 | 0.00 | BC 408 |
| | | 162 | 0 | Min N | ▷ -1.53 | 0.26 | 1.32 | -0.03 | 0.00 | 0.00 | BC 146 |
| | | 162 | 0 | Max $V_y$ | -1.52 | ▷ 0.26 | 1.32 | -0.03 | 0.00 | 0.00 | BC 138 |
| | | 162 | 0 | Min $V_y$ | -0.80 | ▷ 0.02 | 0.89 | -0.01 | 0.00 | 0.00 | BC 446 |
| | | 162 | 0 | Max $V_z$ | -0.90 | 0.13 | ▷ 1.48 | -0.02 | 0.00 | 0.00 | BC 22 |
| | | 38 | 2250 | Min $V_z$ | 0.72 | 0.02 | ▷ 0.65 | -0.00 | 1.72 | -0.06 | BC 356 |
| | | 162 | 0 | Max $M_T$ | -0.66 | 0.02 | 0.89 | ▷ -0.00 | 0.00 | 0.00 | BC 363 |
| | | 162 | 0 | Min $M_T$ | -1.50 | 0.26 | 1.32 | ▷ -0.03 | 0.00 | 0.00 | BC 139 |
| | | 38 | 2250 | Max $M_y$ | -0.90 | 0.13 | 1.09 | -0.02 | ▷ 2.88 | -0.29 | BC 22 |
| | | 162 | 0 | Min $M_y$ | -0.83 | 0.04 | 1.30 | -0.02 | ▷ -0.00 | 0.00 | BC 198 |
| | | 162 | 0 | Max $M_z$ | -0.67 | 0.08 | 1.47 | -0.01 | 0.00 | ▷ 0.00 | BC 1 |
| | | 38 | 2250 | Min $M_z$ | -1.52 | 0.26 | 0.97 | -0.03 | 2.57 | ▷ -0.59 | BC 138 |
| 240 | RC1 | 38 | 0 | Max N | ▷ 1.19 | -0.02 | -0.65 | 0.00 | 1.74 | -0.05 | BC 408 |
| | | | | Min N | ▷ -2.31 | -0.26 | -0.96 | -0.01 | 2.54 | -0.59 | BC 149 |
| | | | | Max $V_y$ | -1.02 | ▷ -0.02 | -0.65 | -0.01 | 1.73 | -0.04 | BC 446 |
| | | | | Min $V_y$ | -2.29 | ▷ -0.26 | -0.96 | -0.01 | 2.54 | -0.59 | BC 138 |
| | | | | Max $V_z$ | -1.03 | -0.02 | ▷ -0.65 | -0.01 | 1.73 | -0.04 | BC 450 |
| | | | | Min $V_z$ | -1.31 | -0.13 | ▷ -1.08 | -0.01 | 2.87 | -0.29 | BC 12 |
| | | | | Max $M_T$ | -0.53 | -0.02 | -0.65 | ▷ 0.00 | 1.73 | -0.05 | BC 363 |
| | | | | Min $M_T$ | -1.16 | -0.08 | -0.95 | ▷ -0.01 | 2.54 | -0.19 | BC 270 |
| | | | | Max $M_y$ | -1.31 | -0.13 | -1.08 | -0.01 | ▷ 2.87 | -0.29 | BC 12 |
| | | | | Min $M_y$ | -1.03 | -0.02 | -0.65 | -0.01 | ▷ 1.73 | -0.04 | BC 450 |
| | | | | Max $M_z$ | -1.02 | -0.02 | -0.65 | -0.01 | 1.73 | ▷ -0.04 | BC 446 |
| | | | | Min $M_z$ | -2.29 | -0.26 | -0.96 | -0.01 | 2.54 | ▷ -0.59 | BC 138 |
| | | 161 | 2250 | Max N | ▷ 1.19 | -0.02 | -0.89 | 0.00 | 0.00 | 0.00 | BC 408 |
| | | | | Min N | ▷ -2.31 | -0.26 | -1.30 | -0.01 | 0.00 | 0.00 | BC 149 |
| | | | | Max $V_y$ | -1.02 | ▷ -0.02 | -0.89 | -0.01 | 0.00 | 0.00 | BC 446 |
| | | | | Min $V_y$ | -2.29 | ▷ -0.26 | -1.30 | -0.01 | 0.00 | 0.00 | BC 138 |
| | | | | Max $V_z$ | -1.03 | -0.02 | ▷ -0.89 | -0.01 | 0.00 | 0.00 | BC 450 |
| | | | | Min $V_z$ | -1.31 | -0.13 | ▷ -1.47 | -0.01 | 0.00 | 0.00 | BC 12 |
| | | | | Max $M_T$ | -0.53 | -0.02 | -0.89 | ▷ 0.00 | 0.00 | 0.00 | BC 363 |
| | | | | Min $M_T$ | -1.16 | -0.08 | -1.30 | ▷ -0.01 | -0.00 | 0.00 | BC 270 |
| | | | | Max $M_y$ | -1.09 | -0.04 | -1.30 | -0.01 | ▷ 0.00 | -0.00 | BC 198 |
| | | | | Min $M_y$ | -1.16 | -0.08 | -1.30 | -0.01 | ▷ -0.00 | 0.00 | BC 182 |
| | | | | Max $M_z$ | -1.16 | -0.08 | -1.30 | -0.01 | -0.00 | ▷ 0.00 | BC 182 |
| | | | | Min $M_z$ | -1.09 | -0.04 | -1.30 | -0.01 | 0.00 | ▷ -0.00 | BC 198 |
| | | 38 | 0 | Max N | ▷ 1.19 | -0.02 | -0.65 | 0.00 | 1.74 | -0.05 | BC 408 |
| | | 38 | 0 | Min N | ▷ -2.31 | -0.26 | -0.96 | -0.01 | 2.54 | -0.59 | BC 149 |
| | | 38 | 0 | Max $V_y$ | -1.02 | ▷ -0.02 | -0.65 | -0.01 | 1.73 | -0.04 | BC 446 |
| | | 38 | 0 | Min $V_y$ | -2.29 | ▷ -0.26 | -0.96 | -0.01 | 2.54 | -0.59 | BC 138 |
| | | 38 | 0 | Max $V_z$ | -1.03 | -0.02 | ▷ -0.65 | -0.01 | 1.73 | -0.04 | BC 450 |
| | | 161 | 2250 | Min $V_z$ | -1.31 | -0.13 | ▷ -1.47 | -0.01 | 0.00 | 0.00 | BC 12 |
| | | 38 | 0 | Max $M_T$ | -0.53 | -0.02 | -0.65 | ▷ 0.00 | 1.73 | -0.05 | BC 363 |
| | | 38 | 0 | Min $M_T$ | -1.16 | -0.08 | -0.95 | ▷ -0.01 | 2.54 | -0.19 | BC 270 |
| | | 38 | 0 | Max $M_y$ | -1.31 | -0.13 | -1.08 | -0.01 | ▷ 2.87 | -0.29 | BC 12 |

## ■ 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 240 | RC1 | 161 | 2250 | Min $M_y$ | -1.16 | -0.08 | -1.30 | -0.01 | ▷ -0.00 | 0.00 | BC 182 |
| | | 161 | 2250 | Max $M_z$ | -1.16 | -0.08 | -1.30 | -0.01 | -0.00 | ▷ 0.00 | BC 182 |
| | | 38 | 0 | Min $M_z$ | -2.29 | -0.26 | -0.96 | -0.01 | 2.54 | ▷ -0.59 | BC 138 |
| 240 | RC1 | 38 | 0 | MAX N | ▷ 1.19 | -0.02 | -0.65 | 0.00 | 1.74 | -0.05 | BC 408 |
| 240 | RC1 | 38 | 0 | MIN N | ▷ -2.31 | -0.26 | -0.96 | -0.01 | 2.54 | -0.59 | BC 149 |
| 213 | RC1 | 162 | 0 | MAX $V_y$ | -1.52 | ▷ 0.26 | 1.32 | -0.03 | 0.00 | 0.00 | BC 138 |
| 240 | RC1 | 38 | 0 | MIN $V_y$ | -2.29 | ▷ -0.26 | -0.96 | -0.01 | 2.54 | -0.59 | BC 138 |
| 213 | RC1 | 162 | 0 | MAX $V_z$ | -0.90 | 0.13 | ▷ 1.48 | -0.02 | 0.00 | 0.00 | BC 22 |
| 240 | RC1 | 161 | 2250 | MIN $V_z$ | -1.31 | -0.13 | ▷ -1.47 | -0.01 | 0.00 | 0.00 | BC 12 |
| 240 | RC1 | 38 | 0 | MAX $M_T$ | -0.53 | -0.02 | -0.65 | ▷ 0.00 | 1.73 | -0.05 | BC 363 |
| 213 | RC1 | 162 | 0 | MIN $M_T$ | -1.50 | 0.26 | 1.32 | ▷ -0.03 | 0.00 | 0.00 | BC 139 |
| 213 | RC1 | 38 | 2250 | MAX $M_y$ | -0.90 | 0.13 | 1.09 | -0.02 | ▷ 2.88 | -0.29 | BC 22 |
| 213 | RC1 | 162 | 0 | MIN $M_y$ | -0.83 | 0.04 | 1.30 | -0.02 | ▷ 0.00 | 0.00 | BC 198 |
| 240 | RC1 | 161 | 2250 | MAX $M_z$ | -1.16 | -0.08 | -1.30 | -0.01 | 0.00 | ▷ 0.00 | BC 182 |
| 213 | RC1 | 38 | 2250 | MIN $M_z$ | -1.52 | 0.26 | 0.97 | -0.03 | 2.57 | ▷ -0.59 | BC 138 |
| | **Doorgaande staven No. 52: Doorgaande staven 52** | | | | | | | | | | |
| 215 | RC1 | 159 | 0 | Max N | ▷ 0.12 | -0.05 | 1.30 | -0.03 | 0.00 | 0.00 | BC 204 |
| | | | | Min N | ▷ -0.10 | -0.03 | 0.89 | -0.02 | 0.00 | 0.00 | BC 447 |
| | | | | Max $V_y$ | 0.03 | ▷ -0.02 | 0.89 | -0.02 | 0.00 | 0.00 | BC 461 |
| | | | | Min $V_y$ | 0.02 | ▷ -0.05 | 1.47 | -0.00 | -0.00 | 0.00 | BC 18 |
| | | | | Max $V_z$ | 0.02 | -0.05 | ▷ 1.47 | -0.00 | 0.00 | 0.00 | BC 11 |
| | | | | Min $V_z$ | -0.10 | -0.04 | ▷ 0.89 | -0.00 | 0.00 | 0.00 | BC 391 |
| | | | | Max $M_T$ | -0.01 | -0.03 | 0.89 | ▷ 0.01 | 0.00 | 0.00 | BC 390 |
| | | | | Min $M_T$ | -0.09 | -0.05 | 1.30 | ▷ -0.03 | 0.00 | 0.00 | BC 267 |
| | | | | Max $M_y$ | 0.03 | -0.03 | 0.89 | 0.01 | ▷ 0.00 | 0.00 | BC 361 |
| | | | | Min $M_y$ | -0.00 | -0.04 | 1.30 | -0.02 | ▷ -0.00 | 0.00 | BC 91 |
| | | | | Max $M_z$ | 0.02 | -0.05 | 1.47 | -0.00 | -0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.02 | -0.05 | 1.47 | -0.00 | -0.00 | ▷ 0.00 | BC 1 |
| | | 164 | 2250 | Max N | ▷ 0.12 | -0.05 | 0.95 | -0.03 | 2.54 | 0.11 | BC 204 |
| | | | | Min N | ▷ -0.10 | -0.03 | 0.65 | -0.02 | 1.73 | 0.08 | BC 447 |
| | | | | Max $V_y$ | 0.03 | ▷ -0.02 | 0.65 | -0.02 | 1.73 | 0.05 | BC 461 |
| | | | | Min $V_y$ | 0.02 | ▷ -0.05 | 1.08 | -0.00 | 2.86 | 0.11 | BC 18 |
| | | | | Max $V_z$ | 0.02 | -0.05 | ▷ 1.08 | -0.00 | 2.86 | 0.11 | BC 11 |
| | | | | Min $V_z$ | -0.10 | -0.04 | ▷ 0.65 | -0.00 | 1.72 | 0.08 | BC 391 |
| | | | | Max $M_T$ | -0.01 | -0.03 | 0.65 | ▷ 0.01 | 1.73 | 0.08 | BC 390 |
| | | | | Min $M_T$ | -0.09 | -0.05 | 0.95 | ▷ -0.03 | 2.53 | 0.10 | BC 267 |
| | | | | Max $M_y$ | 0.02 | -0.05 | 1.08 | -0.00 | ▷ 2.86 | 0.11 | BC 11 |
| | | | | Min $M_y$ | -0.10 | -0.04 | 0.65 | -0.00 | ▷ 1.72 | 0.08 | BC 391 |
| | | | | Max $M_z$ | 0.02 | -0.05 | 1.08 | -0.00 | 2.86 | ▷ 0.11 | BC 18 |
| | | | | Min $M_z$ | 0.03 | -0.02 | 0.65 | -0.02 | 1.73 | ▷ 0.05 | BC 461 |
| | | 159 | 0 | Max N | ▷ 0.12 | -0.05 | 1.30 | -0.03 | 0.00 | 0.00 | BC 204 |
| | | 159 | 0 | Min N | ▷ -0.10 | -0.03 | 0.89 | -0.02 | 0.00 | 0.00 | BC 447 |
| | | 159 | 0 | Max $V_y$ | 0.03 | ▷ -0.02 | 0.89 | -0.02 | 0.00 | 0.00 | BC 461 |
| | | 159 | 0 | Min $V_y$ | 0.02 | ▷ -0.05 | 1.47 | -0.00 | -0.00 | 0.00 | BC 18 |
| | | 159 | 0 | Max $V_z$ | 0.02 | -0.05 | ▷ 1.47 | -0.00 | 0.00 | 0.00 | BC 11 |
| | | 164 | 2250 | Min $V_z$ | -0.10 | -0.04 | ▷ 0.65 | -0.00 | 1.72 | 0.08 | BC 391 |
| | | 159 | 0 | Max $M_T$ | -0.01 | -0.03 | 0.89 | ▷ 0.01 | 0.00 | 0.00 | BC 390 |
| | | 159 | 0 | Min $M_T$ | -0.09 | -0.05 | 1.30 | ▷ -0.03 | 0.00 | 0.00 | BC 267 |
| | | 164 | 2250 | Max $M_y$ | 0.02 | -0.05 | 1.08 | -0.00 | ▷ 2.86 | 0.11 | BC 11 |
| | | 159 | 0 | Min $M_y$ | -0.00 | -0.04 | 1.30 | -0.02 | ▷ -0.00 | 0.00 | BC 91 |
| | | 164 | 2250 | Max $M_z$ | 0.02 | -0.05 | 1.08 | -0.00 | 2.86 | ▷ 0.11 | BC 18 |
| | | 159 | 0 | Min $M_z$ | 0.02 | -0.05 | 1.47 | -0.00 | -0.00 | ▷ 0.00 | BC 1 |
| 243 | RC1 | 164 | 0 | Max N | ▷ -0.01 | 0.03 | -0.65 | 0.00 | 1.73 | 0.07 | BC 57 |
| | | | | Min N | ▷ -0.11 | 0.05 | -0.95 | 0.01 | 2.53 | 0.11 | BC 234 |
| | | | | Max $V_y$ | -0.05 | ▷ 0.05 | -1.07 | 0.00 | 2.86 | 0.11 | BC 18 |
| | | | | Min $V_y$ | -0.11 | ▷ 0.02 | -0.65 | -0.02 | 1.72 | 0.05 | BC 461 |
| | | | | Max $V_z$ | -0.04 | 0.04 | ▷ -0.65 | -0.03 | 1.72 | 0.08 | BC 460 |
| | | | | Min $V_z$ | -0.03 | 0.05 | ▷ -1.07 | -0.02 | 2.86 | 0.11 | BC 9 |
| | | | | Max $M_T$ | -0.10 | 0.05 | -0.95 | ▷ 0.01 | 2.53 | 0.11 | BC 198 |
| | | | | Min $M_T$ | -0.05 | 0.05 | -0.95 | ▷ -0.03 | 2.53 | 0.10 | BC 267 |
| | | | | Max $M_y$ | -0.03 | 0.05 | -1.07 | -0.02 | ▷ 2.86 | 0.11 | BC 9 |
| | | | | Min $M_y$ | -0.04 | 0.04 | -0.65 | -0.03 | ▷ 1.72 | 0.08 | BC 460 |
| | | | | Max $M_z$ | -0.05 | 0.05 | -1.07 | 0.00 | 2.86 | ▷ 0.11 | BC 18 |
| | | | | Min $M_z$ | -0.11 | 0.02 | -0.65 | -0.02 | 1.72 | ▷ 0.05 | BC 461 |
| | | 158 | 2250 | Max N | ▷ -0.01 | 0.03 | -0.89 | 0.00 | 0.00 | 0.00 | BC 57 |
| | | | | Min N | ▷ -0.11 | 0.05 | -1.30 | 0.01 | 0.00 | 0.00 | BC 234 |
| | | | | Max $V_y$ | -0.05 | ▷ 0.05 | -1.47 | 0.00 | 0.00 | 0.00 | BC 18 |
| | | | | Min $V_y$ | -0.11 | ▷ 0.02 | -0.89 | -0.02 | 0.00 | 0.00 | BC 461 |
| | | | | Max $V_z$ | -0.04 | 0.04 | ▷ -0.88 | -0.03 | 0.00 | 0.00 | BC 460 |
| | | | | Min $V_z$ | -0.03 | 0.05 | ▷ -1.47 | -0.02 | 0.00 | 0.00 | BC 9 |
| | | | | Max $M_T$ | -0.10 | 0.05 | -1.30 | ▷ 0.01 | 0.00 | 0.00 | BC 198 |
| | | | | Min $M_T$ | -0.05 | 0.05 | -1.30 | ▷ -0.03 | 0.00 | 0.00 | BC 267 |
| | | | | Max $M_y$ | -0.04 | 0.04 | -1.30 | -0.02 | ▷ 0.00 | 0.00 | BC 91 |
| | | | | Min $M_y$ | -0.07 | 0.03 | -0.89 | 0.01 | ▷ -0.00 | 0.00 | BC 361 |
| | | | | Max $M_z$ | -0.05 | 0.05 | -1.47 | -0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.05 | 0.05 | -1.47 | -0.00 | 0.00 | ▷ 0.00 | BC 1 |
| | | 164 | 0 | Max N | ▷ -0.01 | 0.03 | -0.65 | 0.00 | 1.73 | 0.07 | BC 57 |
| | | 164 | 0 | Min N | ▷ -0.11 | 0.05 | -0.95 | 0.01 | 2.53 | 0.11 | BC 234 |
| | | 164 | 0 | Max $V_y$ | -0.05 | ▷ 0.05 | -1.07 | 0.00 | 2.86 | 0.11 | BC 18 |
| | | 164 | 0 | Min $V_y$ | -0.11 | ▷ 0.02 | -0.65 | -0.02 | 1.72 | 0.05 | BC 461 |
| | | 164 | 0 | Max $V_z$ | -0.04 | 0.04 | ▷ -0.65 | -0.03 | 1.72 | 0.08 | BC 460 |
| | | 158 | 2250 | Min $V_z$ | -0.03 | 0.05 | ▷ -1.47 | -0.02 | 0.00 | 0.00 | BC 9 |
| | | 164 | 0 | Max $M_T$ | -0.10 | 0.05 | -0.95 | ▷ 0.01 | 2.53 | 0.11 | BC 198 |
| | | 164 | 0 | Min $M_T$ | -0.05 | 0.05 | -0.95 | ▷ -0.03 | 2.53 | 0.10 | BC 267 |
| | | 164 | 0 | Max $M_y$ | -0.03 | 0.05 | -1.07 | -0.02 | ▷ 2.86 | 0.11 | BC 9 |
| | | 158 | 2250 | Min $M_y$ | -0.07 | 0.03 | -0.89 | 0.01 | ▷ -0.00 | 0.00 | BC 361 |
| | | 164 | 0 | Max $M_z$ | -0.05 | 0.05 | -1.07 | 0.00 | 2.86 | ▷ 0.11 | BC 18 |

## 4.11 STAAFVERZAMELINGEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ / $V_u$ | $V_z$ / $V_v$ | Momenten [kNm] $M_T$ | $M_y$ / $M_u$ | $M_z$ / $M_v$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 243 | RC1 | 158 | 2250 | Min $M_z$ | -0.05 | 0.05 | -1.47 | -0.00 | 0.00 | ▷ 0.00 | BC 1 |
| 215 | RC1 | 159 | 0 | MAX N | ▷ 0.12 | -0.05 | 1.30 | -0.03 | 0.00 | 0.00 | BC 204 |
| 243 | RC1 | 164 | 0 | MIN N | ▷ -0.11 | 0.05 | -0.95 | 0.01 | 2.53 | 0.11 | BC 234 |
| 243 | RC1 | 164 | 0 | MAX $V_y$ | -0.05 | ▷ 0.05 | -1.07 | 0.00 | 2.86 | 0.11 | BC 18 |
| 215 | RC1 | 159 | 0 | MIN $V_y$ | 0.02 | ▷ -0.05 | 1.47 | 0.00 | 0.00 | 0.00 | BC 18 |
| 215 | RC1 | 159 | 0 | MAX $V_z$ | 0.02 | -0.05 | ▷ 1.47 | 0.00 | 0.00 | 0.00 | BC 11 |
| 243 | RC1 | 158 | 2250 | MIN $V_z$ | -0.03 | 0.05 | ▷ -1.47 | -0.02 | 0.00 | 0.00 | BC 9 |
| 243 | RC1 | 164 | 0 | MAX $M_T$ | -0.10 | 0.05 | -0.95 | ▷ 0.01 | 2.53 | 0.11 | BC 198 |
| 215 | RC1 | 159 | 0 | MIN $M_T$ | -0.09 | -0.05 | 1.30 | ▷ -0.03 | 0.00 | 0.00 | BC 267 |
| 215 | RC1 | 164 | 2250 | MAX $M_y$ | 0.02 | -0.05 | 1.08 | 0.00 | ▷ 2.86 | 0.11 | BC 11 |
| 215 | RC1 | 159 | 0 | MIN $M_y$ | 0.00 | -0.04 | 1.30 | -0.02 | ▷ 0.00 | 0.00 | BC 91 |
| 215 | RC1 | 164 | 2250 | MAX $M_z$ | 0.02 | -0.05 | 1.08 | 0.00 | 2.86 | ▷ 0.11 | BC 18 |
| 215 | RC1 | 159 | 0 | MIN $M_z$ | 0.02 | -0.05 | 1.47 | 0.00 | 0.00 | ▷ 0.00 | BC 1 |

**RF-STEEL EC3**
CA1
Ontwerp van stalen staven volgens Eurocode 3

## 1.1 ALGEMENE GEGEVENS

Te ontwerpen staven: 47-50,53-69,71-73,75,77,79,81,82,84,87-99,102,112-139,146-148,154-159, 162-173,202,204,206,212,214,216-218,220,221,223,224,226,227,229,230, 232,233,235,236,238,239,241,242

Te ontwerpen staafverz.: Alle

Nationale bijlagen: NEN

Ontwerp uiterste grenstoestand
Te berekenen belastingscombinaties:

| | |
|---|---|
| BC1 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 |
| BC2 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 |
| BC3 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 |
| BC4 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 |
| BC5 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 |
| BC6 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC7 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 |
| BC8 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 |
| BC9 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 |
| BC10 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 |
| BC11 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG130 |
| BC12 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 |
| BC13 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC14 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 |
| BC15 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG140 |
| BC16 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 |
| BC17 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG150 |
| BC18 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 |
| BC19 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG130 |
| BC20 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 |
| BC21 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC22 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 |
| BC23 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG140 |
| BC24 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 |
| BC25 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG150 |
| BC26 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG130 |
| BC27 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG130 + 1.65*BG140 |
| BC28 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC29 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG130 + 1.65*BG150 |
| BC30 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG140 |
| BC31 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG140 + 1.65*BG150 |
| BC32 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG150 |
| BC33 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 |
| BC34 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 |
| BC35 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| BC36 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 |
| BC37 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 |
| BC38 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC39 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 |
| BC40 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 |
| BC41 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 |
| BC42 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 |
| BC43 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 |
| BC44 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 |
| BC45 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC46 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 |
| BC47 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 |
| BC48 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 |
| BC49 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 |
| BC50 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 |
| BC51 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 |
| BC52 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 |
| BC53 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC54 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 |
| BC55 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 |
| BC56 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 |
| BC57 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 |
| BC58 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 |
| BC59 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 |
| BC60 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC61 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 |
| BC62 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 |
| BC63 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 |
| BC64 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 |
| BC65 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 |
| BC66 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 |
| BC67 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 |
| BC68 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 |
| BC69 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC70 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 |
| BC71 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 |
| BC72 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 |
| BC73 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 |
| BC74 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 |
| BC75 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 |
| BC76 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC77 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 |
| BC78 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 |
| BC79 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 |
| BC80 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 |
| BC81 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 |
| BC82 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 |
| BC83 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 |
| BC84 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC85 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| BC86 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 |
| BC87 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 |
| BC88 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 |
| BC89 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 |
| BC90 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 |
| BC91 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC92 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 |
| BC93 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 |
| BC94 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 |
| BC95 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 |
| BC96 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 |
| BC97 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 |
| BC98 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 |
| BC99 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 |
| BC100 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| BC101 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC102 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| BC103 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 |
| BC104 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| BC105 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG150 |
| BC106 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 |
| BC107 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| BC108 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC109 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| BC110 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG140 |
| BC111 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| BC112 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG150 |
| BC113 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 |
| BC114 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 |
| BC115 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| BC116 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC117 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| BC118 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 |
| BC119 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| BC120 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG150 |
| BC121 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG130 |
| BC122 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| BC123 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC124 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| BC125 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG140 |
| BC126 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| BC127 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG150 |
| BC128 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG300 |
| BC129 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG300 |
| BC130 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG300 |
| BC131 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG300 |
| BC132 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| BC133 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC134 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| BC135 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG300 |
| BC136 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC137 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG300 |
| BC138 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG300 |
| BC139 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| BC140 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC141 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| BC142 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG300 |
| BC143 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC144 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG300 |
| BC145 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG300 |
| BC146 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG300 |
| BC147 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| BC148 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC149 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| BC150 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG300 |
| BC151 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC152 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG300 |
| BC153 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG300 |
| BC154 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| BC155 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC156 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| BC157 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG300 |
| BC158 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC159 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG300 |
| BC160 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG401 |
| BC161 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG402 |
| BC162 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG403 |
| BC163 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG404 |
| BC164 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG401 |
| BC165 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG402 |
| BC166 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG403 |
| BC167 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG404 |
| BC168 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG401 |
| BC169 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG402 |
| BC170 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG403 |
| BC171 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG404 |
| BC172 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG401 |
| BC173 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG402 |
| BC174 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG403 |
| BC175 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG404 |
| BC176 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | 1.65*BG401 |
| BC177 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| BC178 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| BC179 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| BC180 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC181 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC182 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC183 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC184 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| BC185 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| BC186 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| BC187 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| BC188 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG401 |
| BC189 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG402 |
| BC190 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG403 |
| BC191 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG404 |
| BC192 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC193 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC194 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC195 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC196 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG401 |
| BC197 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG402 |
| BC198 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG403 |
| BC199 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG404 |
| BC200 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG401 |
| BC201 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG402 |
| BC202 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG403 |
| BC203 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG404 |
| BC204 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| BC205 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| BC206 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| BC207 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| BC208 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC209 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC210 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC211 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC212 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| BC213 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| BC214 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| BC215 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| BC216 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG401 |
| BC217 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG402 |
| BC218 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG403 |
| BC219 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG404 |
| BC220 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC221 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC222 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC223 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC224 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG401 |
| BC225 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG402 |
| BC226 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG403 |
| BC227 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG404 |
| BC228 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG401 |
| BC229 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG402 |
| BC230 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG403 |
| BC231 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG404 |
| BC232 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG401 |
| BC233 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG402 |
| BC234 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG403 |
| BC235 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG404 |
| BC236 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| BC237 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| BC238 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| BC239 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| BC240 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC241 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC242 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC243 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC244 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| BC245 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| BC246 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| BC247 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| BC248 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG401 |
| BC249 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG402 |
| BC250 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG403 |
| BC251 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG404 |
| BC252 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC253 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC254 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC255 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC256 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG401 |
| BC257 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG402 |
| BC258 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG403 |
| BC259 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG404 |
| BC260 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG401 |
| BC261 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG402 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| BC262 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG403 |
| BC263 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG404 |
| BC264 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| BC265 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| BC266 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| BC267 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| BC268 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC269 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC270 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC271 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC272 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| BC273 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| BC274 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| BC275 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| BC276 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG401 |
| BC277 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG402 |
| BC278 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG403 |
| BC279 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG404 |
| BC280 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC281 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC282 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC283 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC284 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG401 |
| BC285 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG402 |
| BC286 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG403 |
| BC287 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG404 |
| BC288 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 |
| BC289 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 |
| BC290 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 |
| BC291 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 |
| BC292 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| BC293 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC294 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| BC295 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 |
| BC296 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| BC297 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG150 |
| BC298 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 |
| BC299 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| BC300 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC301 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| BC302 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG140 |
| BC303 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| BC304 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG150 |
| BC305 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 |
| BC306 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 |
| BC307 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| BC308 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC309 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| BC310 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | + 1.65*BG120 + 1.65*BG140 |
| BC311 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| BC312 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG150 |
| BC313 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG130 |
| BC314 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| BC315 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC316 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| BC317 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG140 |
| BC318 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| BC319 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG150 |
| BC320 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG300 |
| BC321 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG300 |
| BC322 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG300 |
| BC323 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG300 |
| BC324 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| BC325 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC326 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| BC327 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG300 |
| BC328 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC329 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG300 |
| BC330 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG300 |
| BC331 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| BC332 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC333 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| BC334 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG300 |
| BC335 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC336 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG300 |
| BC337 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG300 |
| BC338 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG300 |
| BC339 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| BC340 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC341 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| BC342 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG300 |
| BC343 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC344 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG300 |
| BC345 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG300 |
| BC346 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| BC347 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC348 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| BC349 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG300 |
| BC350 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC351 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG300 |
| BC352 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG401 |
| BC353 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG402 |
| BC354 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG403 |
| BC355 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG404 |
| BC356 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG401 |
| BC357 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG402 |
| BC358 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG403 |
| BC359 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG404 |
| BC360 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG401 |

## 1.1 ALGEMENE GEGEVENS

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|---|---|
| BC361 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG402 |
| BC362 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG403 |
| BC363 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG404 |
| BC364 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG401 |
| BC365 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG402 |
| BC366 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG403 |
| BC367 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG404 |
| BC368 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| BC369 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| BC370 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| BC371 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| BC372 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC373 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC374 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC375 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC376 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| BC377 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| BC378 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| BC379 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| BC380 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG401 |
| BC381 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG402 |
| BC382 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG403 |
| BC383 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG404 |
| BC384 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC385 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC386 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC387 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC388 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG401 |
| BC389 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG402 |
| BC390 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG403 |
| BC391 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG404 |
| BC392 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG401 |
| BC393 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG402 |
| BC394 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG403 |
| BC395 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG404 |
| BC396 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| BC397 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| BC398 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| BC399 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| BC400 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC401 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC402 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC403 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC404 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| BC405 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| BC406 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| BC407 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + |

## 1.1 ALGEMENE GEGEVENS

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|---|---|
| | + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| BC408 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG401 |
| BC409 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG402 |
| BC410 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG403 |
| BC411 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG404 |
| BC412 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC413 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC414 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC415 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC416 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG401 |
| BC417 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG402 |
| BC418 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG403 |
| BC419 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG404 |
| BC420 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG401 |
| BC421 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG402 |
| BC422 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG403 |
| BC423 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG404 |
| BC424 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG401 |
| BC425 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG402 |
| BC426 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG403 |
| BC427 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG404 |
| BC428 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| BC429 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| BC430 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| BC431 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| BC432 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC433 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC434 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC435 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC436 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| BC437 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| BC438 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| BC439 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| BC440 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG401 |
| BC441 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG402 |
| BC442 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG403 |
| BC443 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG404 |
| BC444 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC445 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC446 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC447 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC448 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG401 |
| BC449 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG402 |
| BC450 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG403 |
| BC451 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG404 |
| BC452 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG401 |
| BC453 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG402 |
| BC454 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG403 |
| BC455 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG404 |

## 1.1 ALGEMENE GEGEVENS

| | | |
|---|---|---|
| | BC456 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| | BC457 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| | BC458 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| | BC459 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| | BC460 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | BC461 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | BC462 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | BC463 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | BC464 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| | BC465 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| | BC466 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| | BC467 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| | BC468 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG401 |
| | BC469 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG402 |
| | BC470 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG403 |
| | BC471 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG404 |
| | BC472 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | BC473 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | BC474 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | BC475 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | BC476 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG401 |
| | BC477 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG402 |
| | BC478 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG403 |
| | BC479 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG404 |
| Ontwerp bruikbaarheidsgrenstoestand<br>Te berekenen belastingscombinaties: | BC480 | BG10 + BG20 + BG30 + BG40 |
| | BC481 | BG10 + BG20 + BG30 + BG40 + BG100 |
| | BC482 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 |
| | BC483 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 |
| | BC484 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 |
| | BC485 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 |
| | BC486 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 |
| | BC487 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 |
| | BC488 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 |
| | BC489 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 |
| | BC490 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 |
| | BC491 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 |
| | BC492 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 |
| | BC493 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 |
| | BC494 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 |
| | BC495 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 |
| | BC496 | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 |
| | BC497 | BG10 + BG20 + BG30 + BG40 + BG110 |
| | BC498 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 |
| | BC499 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 |
| | BC500 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 |
| | BC501 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 |
| | BC502 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 |
| | BC503 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 |
| | BC504 | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 |
| | BC505 | BG10 + BG20 + BG30 + BG40 + BG130 |
| | BC506 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 |
| | BC507 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 |
| | BC508 | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 |
| | BC509 | BG10 + BG20 + BG30 + BG40 + BG140 |
| | BC510 | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 |
| | BC511 | BG10 + BG20 + BG30 + BG40 + BG150 |
| | BC512 | BG10 + BG20 + BG30 + BG40 + BG120 |
| | BC513 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 |
| | BC514 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 |
| | BC515 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG130 |
| | BC516 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG130 + BG140 |
| | BC517 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG130 + BG140 + BG150 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| BC518 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG130 + BG150 |
| BC519 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG140 |
| BC520 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG140 + BG150 |
| BC521 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG150 |
| BC522 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG130 |
| BC523 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG130 + BG140 |
| BC524 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG130 + BG140 + BG150 |
| BC525 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG130 + BG150 |
| BC526 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG140 |
| BC527 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG140 + BG150 |
| BC528 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG150 |
| BC529 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 |
| BC530 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG130 |
| BC531 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG130 + BG140 |
| BC532 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG130 + BG140 + BG150 |
| BC533 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG130 + BG150 |
| BC534 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG140 |
| BC535 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG140 + BG150 |
| BC536 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG150 |
| BC537 | BG10 + BG20 + BG30 + BG40 + BG120 + BG130 |
| BC538 | BG10 + BG20 + BG30 + BG40 + BG120 + BG130 + BG140 |
| BC539 | BG10 + BG20 + BG30 + BG40 + BG120 + BG130 + BG140 + BG150 |
| BC540 | BG10 + BG20 + BG30 + BG40 + BG120 + BG130 + BG150 |
| BC541 | BG10 + BG20 + BG30 + BG40 + BG120 + BG140 |
| BC542 | BG10 + BG20 + BG30 + BG40 + BG120 + BG140 + BG150 |
| BC543 | BG10 + BG20 + BG30 + BG40 + BG120 + BG150 |
| BC544 | BG10 + BG20 + BG30 + BG40 + BG300 |
| BC545 | BG10 + BG20 + BG30 + BG40 + BG100 + BG300 |
| BC546 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG300 |
| BC547 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG300 |
| BC548 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG300 |
| BC549 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 + BG300 |
| BC550 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 + BG300 |
| BC551 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG300 |
| BC552 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 + BG300 |
| BC553 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 + BG300 |
| BC554 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG300 |
| BC555 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG300 |
| BC556 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 + BG300 |
| BC557 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 + BG300 |
| BC558 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG300 |
| BC559 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 + BG300 |
| BC560 | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 + BG300 |
| BC561 | BG10 + BG20 + BG30 + BG40 + BG110 + BG300 |
| BC562 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG300 |
| BC563 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG300 |
| BC564 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 + BG300 |
| BC565 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 + BG300 |
| BC566 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG300 |
| BC567 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 + BG300 |
| BC568 | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 + BG300 |
| BC569 | BG10 + BG20 + BG30 + BG40 + BG130 + BG300 |
| BC570 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG300 |
| BC571 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 + BG300 |
| BC572 | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 + BG300 |
| BC573 | BG10 + BG20 + BG30 + BG40 + BG140 + BG300 |
| BC574 | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 + BG300 |
| BC575 | BG10 + BG20 + BG30 + BG40 + BG150 + BG300 |
| BC576 | BG10 + BG20 + BG30 + BG40 + BG401 |
| BC577 | BG10 + BG20 + BG30 + BG40 + BG402 |
| BC578 | BG10 + BG20 + BG30 + BG40 + BG403 |
| BC579 | BG10 + BG20 + BG30 + BG40 + BG404 |
| BC580 | BG10 + BG20 + BG30 + BG40 + BG100 + BG401 |
| BC581 | BG10 + BG20 + BG30 + BG40 + BG100 + BG402 |
| BC582 | BG10 + BG20 + BG30 + BG40 + BG100 + BG403 |
| BC583 | BG10 + BG20 + BG30 + BG40 + BG100 + BG404 |
| BC584 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG401 |
| BC585 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG402 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| BC586 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG403 |
| BC587 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG404 |
| BC588 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG401 |
| BC589 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG402 |
| BC590 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG403 |
| BC591 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG404 |
| BC592 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG401 |
| BC593 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG402 |
| BC594 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG403 |
| BC595 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG404 |
| BC596 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 + BG401 |
| BC597 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 + BG402 |
| BC598 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 + BG403 |
| BC599 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 + BG404 |
| BC600 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 + BG401 |
| BC601 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 + BG402 |
| BC602 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 + BG403 |
| BC603 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 + BG404 |
| BC604 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG401 |
| BC605 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG402 |
| BC606 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG403 |
| BC607 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG404 |
| BC608 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 + BG401 |
| BC609 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 + BG402 |
| BC610 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 + BG403 |
| BC611 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 + BG404 |
| BC612 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 + BG401 |
| BC613 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 + BG402 |
| BC614 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 + BG403 |
| BC615 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 + BG404 |
| BC616 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG401 |
| BC617 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG402 |
| BC618 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG403 |
| BC619 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG404 |
| BC620 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG401 |
| BC621 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG402 |
| BC622 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG403 |
| BC623 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG404 |
| BC624 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 + BG401 |
| BC625 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 + BG402 |
| BC626 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 + BG403 |
| BC627 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 + BG404 |
| BC628 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 + BG401 |
| BC629 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 + BG402 |
| BC630 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 + BG403 |
| BC631 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 + BG404 |
| BC632 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG401 |
| BC633 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG402 |
| BC634 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG403 |
| BC635 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG404 |
| BC636 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 + BG401 |
| BC637 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 + BG402 |
| BC638 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 + BG403 |
| BC639 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 + |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | + BG404 |
| BC640 | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 + BG401 |
| BC641 | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 + BG402 |
| BC642 | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 + BG403 |
| BC643 | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 + BG404 |
| BC644 | BG10 + BG20 + BG30 + BG40 + BG110 + BG401 |
| BC645 | BG10 + BG20 + BG30 + BG40 + BG110 + BG402 |
| BC646 | BG10 + BG20 + BG30 + BG40 + BG110 + BG403 |
| BC647 | BG10 + BG20 + BG30 + BG40 + BG110 + BG404 |
| BC648 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG401 |
| BC649 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG402 |
| BC650 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG403 |
| BC651 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG404 |
| BC652 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG401 |
| BC653 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG402 |
| BC654 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG403 |
| BC655 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG404 |
| BC656 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 + BG401 |
| BC657 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 + BG402 |
| BC658 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 + BG403 |
| BC659 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 + BG404 |
| BC660 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 + BG401 |
| BC661 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 + BG402 |
| BC662 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 + BG403 |
| BC663 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 + BG404 |
| BC664 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG401 |
| BC665 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG402 |
| BC666 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG403 |
| BC667 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG404 |
| BC668 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 + BG401 |
| BC669 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 + BG402 |
| BC670 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 + BG403 |
| BC671 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 + BG404 |
| BC672 | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 + BG401 |
| BC673 | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 + BG402 |
| BC674 | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 + BG403 |
| BC675 | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 + BG404 |
| BC676 | BG10 + BG20 + BG30 + BG40 + BG130 + BG401 |
| BC677 | BG10 + BG20 + BG30 + BG40 + BG130 + BG402 |
| BC678 | BG10 + BG20 + BG30 + BG40 + BG130 + BG403 |
| BC679 | BG10 + BG20 + BG30 + BG40 + BG130 + BG404 |
| BC680 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG401 |
| BC681 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG402 |
| BC682 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG403 |
| BC683 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG404 |
| BC684 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 + BG401 |
| BC685 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 + BG402 |
| BC686 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 + BG403 |
| BC687 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 + BG404 |
| BC688 | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 + BG401 |
| BC689 | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 + BG402 |
| BC690 | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 + BG403 |
| BC691 | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 + BG404 |
| BC692 | BG10 + BG20 + BG30 + BG40 + BG140 + BG401 |
| BC693 | BG10 + BG20 + BG30 + BG40 + BG140 + BG402 |
| BC694 | BG10 + BG20 + BG30 + BG40 + BG140 + BG403 |
| BC695 | BG10 + BG20 + BG30 + BG40 + BG140 + BG404 |
| BC696 | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 + BG401 |
| BC697 | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 + BG402 |
| BC698 | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 + BG403 |
| BC699 | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 + BG404 |
| BC700 | BG10 + BG20 + BG30 + BG40 + BG150 + BG401 |
| BC701 | BG10 + BG20 + BG30 + BG40 + BG150 + BG402 |
| BC702 | BG10 + BG20 + BG30 + BG40 + BG150 + BG403 |
| BC703 | BG10 + BG20 + BG30 + BG40 + BG150 + BG404 |

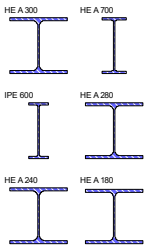
## 1.2 MATERIALEN

| Matl. No. | Materiaal Omschrijving | E-Modulus E [N/mm²] | Glijdingsmodulu G [N/mm²] | Coï¿½ff. van Poisso ν [-] | Vloeispanning $f_{yk}$ [N/mm²] | Max. Dikte t [mm] |
|---|---|---|---|---|---|---|
| 1 | Staal S 235 \| NEN EN 1993-1-1:2007-11 | 210000.0 | 80769.2 | 0.300 | 235.0 | 40.0 |
| | | | | | 215.0 | 80.0 |
| | | | | | 215.0 | 100.0 |
| | | | | | 195.0 | 150.0 |

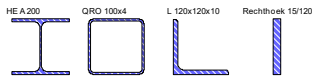
## 1.2 MATERIALEN

| Matl. No. | Materiaal Omschrijving | E-Modulus E [N/mm²] | Glijdingsmodulu G [N/mm²] | Coï¿½ff. van Poisso ν [-] | Vloeispanning $f_{yk}$ [N/mm²] | Max. Dikte t [mm] |
|---|---|---|---|---|---|---|
| | | | | | 185.0<br>175.0<br>165.0 | 200.0<br>250.0<br>400.0 |

## 1.3 DOORSNEDES




| Snede No. | Matl. No. | Doorsnede Omschrijving | Doorsnede Type | Max Ontwerp Unity check | Commentaar |
|---|---|---|---|---|---|
| 2 | 1 | HE A 300 \| Euronorm 53-62 | Gewalst I-profiel | 0.29 | Hoofddraag kolom |
| 3 | 1 | HE A 700 \| Euronorm 53-62 | Gewalst I-profiel | 0.78 | Hoofddraag ligger |
| 4 | 1 | IPE 600 \| Euronorm 19-57 | Gewalst I-profiel | 0.60 | Hoofddraag dakligger |
| 5 | 1 | HE A 280 \| Euronorm 53-62 | Gewalst I-profiel | 0.50 | Hoofddraag dakligger |
| 6 | 1 | HE A 240 \| Euronorm 53-62 | Gewalst I-profiel | 0.40 | Hoofddraag dakligger rand |
| 7 | 1 | HE A 300 \| Euronorm 53-62 | Gewalst I-profiel | 0.36 | Tussenkolom |
| 8 | 1 | HE A 180 \| Euronorm 53-62 | Gewalst I-profiel | 0.22 | Tussenliggers |
| 9 | 1 | HE A 200 \| Euronorm 53-62 | Gewalst I-profiel | 0.14 | Dakligger rand |
| 10 | 1 | QRO 100x4 \| EN 10219-2:2006 | Vierkant Gewalst | 0.40 | Dakligger midden |
| 11 | 1 | L 120x120x10 \| EN 10056-1:1998 | Hoek | 0.11 | Horizontale verbanden |
| 12 | 1 | Rechthoek 15/120 | Platte staaf | 0.18 | Verticale verbanden |
| 13 | 1 | HE A 180 \| Euronorm 53-62 | Gewalst I-profiel | 0.22 | Kolom |
| 14 | 1 | HE A 200 \| Euronorm 53-62 | Gewalst I-profiel | 0.14 | Dakligger |




## 1.5 KNIKLENGTES - STAVEN

| Staaf No. | Knik Mogelijk | Knik om y/u-as Mogelijk | $k_{cr,y/u}$ | $L_{cr,y/u}$ [mm] | Knik om z/v-as Mogelijk | $k_{cr,z/v}$ | $L_{cr,z/v}$ [mm] | Kip Mogelijk | $k_z$ | $k_w$ | $L_w$ [mm] | $L_T$ [mm] |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 47 | ☒ | ☒ | 1.00 | 6400 | ☒ | 1.00 | 6400 | ☒ | 1.0 | 1.0 | 6400 | 6400 |
| 48 | ☒ | ☒ | 1.00 | 6510 | ☒ | 1.00 | 6510 | ☒ | 1.0 | 1.0 | 6510 | 6510 |
| 49 | ☒ | ☒ | 1.00 | 6530 | ☒ | 1.00 | 6530 | ☒ | 1.0 | 1.0 | 6530 | 6530 |
| 50 | ☒ | ☒ | 1.00 | 6400 | ☒ | 1.00 | 6400 | ☒ | 1.0 | 1.0 | 6400 | 6400 |
| 53 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 54 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 55 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 56 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 57 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 58 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 59 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 60 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 61 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 62 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 63 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 64 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 65 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 66 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 67 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 68 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 69 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 71 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 72 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 73 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 75 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 77 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 79 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 81 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 82 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 84 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 87 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 88 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 89 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 90 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 91 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 92 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 93 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 94 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 95 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 96 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 97 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 98 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 99 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 102 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 112 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 113 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |

## 1.5 KNIKLENGTES - STAVEN

| Staaf | Knik | Knik om y/u-as | | | Knik om z/v-as | | | Kip | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| No. | Mogelijk | Mogelijk | $k_{cr,y/u}$ | $L_{cr,y/u}$ [mm] | Mogelijk | $k_{cr,z/v}$ | $L_{cr,z/v}$ [mm] | Mogelijk | $k_z$ | $k_w$ | $L_w$ [mm] | $L_T$ [mm] |
| 114 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 115 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 116 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 117 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 118 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 119 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 120 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 121 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 122 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 123 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 124 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 125 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 126 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 127 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 128 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 129 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 130 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 131 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 132 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 133 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 134 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 135 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 136 | ☐ | ☐ | 1.00 | 7827 | ☐ | 1.00 | 7827 | ☐ | 1.0 | 1.0 | 7827 | 7827 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 137 | ☐ | ☐ | 1.00 | 7512 | ☐ | 1.00 | 7512 | ☐ | 1.0 | 1.0 | 7512 | 7512 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 138 | ☐ | ☐ | 1.00 | 7827 | ☐ | 1.00 | 7827 | ☐ | 1.0 | 1.0 | 7827 | 7827 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 139 | ☐ | ☐ | 1.00 | 7451 | ☐ | 1.00 | 7451 | ☐ | 1.0 | 1.0 | 7451 | 7451 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 146 | ☐ | ☐ | 1.00 | 7411 | ☐ | 1.00 | 7411 | ☐ | 1.0 | 1.0 | 7411 | 7411 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 147 | ☐ | ☐ | 1.00 | 7529 | ☐ | 1.00 | 7529 | ☐ | 1.0 | 1.0 | 7529 | 7529 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 148 | ☒ | ☒ | 1.00 | 1665 | ☒ | 1.00 | 1665 | ☒ | 1.0 | 1.0 | 1665 | 1665 |
| 154 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 155 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 156 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 157 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 158 | ☐ | ☐ | 1.00 | 7512 | ☐ | 1.00 | 7512 | ☐ | 1.0 | 1.0 | 7512 | 7512 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 159 | ☐ | ☐ | 1.00 | 7451 | ☐ | 1.00 | 7451 | ☐ | 1.0 | 1.0 | 7451 | 7451 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 162 | ☒ | ☒ | 1.00 | 1665 | ☒ | 1.00 | 1665 | ☒ | 1.0 | 1.0 | 1665 | 1665 |
| 163 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 164 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 165 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 166 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 167 | ☐ | ☐ | 1.00 | 7411 | ☐ | 1.00 | 7411 | ☐ | 1.0 | 1.0 | 7411 | 7411 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 168 | ☐ | ☐ | 1.00 | 7529 | ☐ | 1.00 | 7529 | ☐ | 1.0 | 1.0 | 7529 | 7529 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 169 | ☒ | ☒ | 1.00 | 1665 | ☒ | 1.00 | 1665 | ☒ | 1.0 | 1.0 | 1665 | 1665 |
| 170 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 171 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 172 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 173 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 202 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 204 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 206 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |

## 1.5 KNIKLENGTES - STAVEN

| Staaf | Knik | Knik om y/u-as | | | Knik om z/v-as | | | Kip | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| No. | Mogelijk | Mogelijk | $k_{cr,y/u}$ | $L_{cr,y/u}$ [mm] | Mogelijk | $k_{cr,z/v}$ | $L_{cr,z/v}$ [mm] | Mogelijk | $k_z$ | $k_w$ | $L_w$ [mm] | $L_T$ [mm] |
| 212 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 214 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 216 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 217 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 218 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 220 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 221 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 223 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 224 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 226 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 227 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 229 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 230 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 232 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 233 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 235 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 236 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 238 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 239 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 241 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 242 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |

## 1.6 KNIKLENGTES - STAAFVERZAMELINGEN

| Staafver | Knik | Knik om y-as | | | Knik om z-as | | | Kip | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| No. | Mogelijk | Mogelijk | $k_{cr,y}$ | $L_{cr,y}$ [mm] | Mogelijk | $k_{cr,z}$ | $L_{cr,z}$ [mm] | Mogelijk | $k_z$ | $k_w$ | $L_w$ [mm] | $L_T$ [mm] |
| 1 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 2 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 3 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 4 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 5 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 6 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 7 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 8 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 9 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 10 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 11 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 12 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 13 | ☒ | ☒ | 1.00 | 19447 | ☒ | 0.20 | 3889 | ☒ | 1.0 | 1.0 | 3889 | 19447 |
| 14 | ☒ | ☒ | 1.00 | 12912 | ☒ | 0.25 | 3228 | ☒ | 1.0 | 1.0 | 3228 | 12912 |
| 15 | ☒ | ☒ | 1.00 | 12912 | ☒ | 0.25 | 3228 | ☒ | 1.0 | 1.0 | 3228 | 12912 |
| 16 | ☒ | ☒ | 1.00 | 7970 | ☒ | 1.00 | 7970 | ☒ | 1.0 | 1.0 | 7970 | 7970 |
| 17 | ☒ | ☒ | 1.00 | 8093 | ☒ | 1.00 | 8093 | ☒ | 1.0 | 1.0 | 8093 | 8093 |
| 18 | ☒ | ☒ | 1.00 | 7970 | ☒ | 1.00 | 7970 | ☒ | 1.0 | 1.0 | 7970 | 7970 |
| 19 | ☒ | ☒ | 1.00 | 8093 | ☒ | 1.00 | 8093 | ☒ | 1.0 | 1.0 | 8093 | 8093 |
| 20 | ☒ | ☒ | 1.00 | 8093 | ☒ | 1.00 | 8093 | ☒ | 1.0 | 1.0 | 8093 | 8093 |
| 21 | ☒ | ☒ | 1.00 | 8093 | ☒ | 1.00 | 8093 | ☒ | 1.0 | 1.0 | 8093 | 8093 |
| 24 | ☒ | ☒ | 1.00 | 19447 | ☒ | 0.20 | 3889 | ☒ | 1.0 | 1.0 | 3889 | 19447 |
| 25 | ☒ | ☒ | 1.00 | 6530 | ☒ | 1.00 | 6530 | ☒ | 1.0 | 1.0 | 6530 | 6530 |
| 28 | ☒ | ☒ | 1.00 | 4345 | ☒ | 1.00 | 4345 | ☒ | 1.0 | 1.0 | 4345 | 4345 |
| 29 | ☒ | ☒ | 1.00 | 4345 | ☒ | 1.00 | 4345 | ☒ | 1.0 | 1.0 | 4345 | 4345 |
| 30 | ☒ | ☒ | 1.00 | 6510 | ☒ | 1.00 | 6510 | ☒ | 1.0 | 1.0 | 6510 | 6510 |
| 31 | ☒ | ☒ | 1.00 | 6530 | ☒ | 1.00 | 6530 | ☒ | 1.0 | 1.0 | 6530 | 6530 |
| 32 | ☒ | ☒ | 1.00 | 4345 | ☒ | 1.00 | 4345 | ☒ | 1.0 | 1.0 | 4345 | 4345 |
| 33 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 34 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 35 | ☒ | ☒ | 1.00 | 6535 | ☒ | 1.00 | 6535 | ☒ | 1.0 | 1.0 | 6535 | 6535 |
| 36 | ☒ | ☒ | 1.00 | 6511 | ☒ | 1.00 | 6511 | ☒ | 1.0 | 1.0 | 6511 | 6511 |
| 37 | ☒ | ☒ | 1.00 | 6401 | ☒ | 1.00 | 6401 | ☒ | 1.0 | 1.0 | 6401 | 6401 |
| 38 | ☒ | ☒ | 1.00 | 6535 | ☒ | 1.00 | 6535 | ☒ | 1.0 | 1.0 | 6535 | 6535 |
| 39 | ☒ | ☒ | 1.00 | 6511 | ☒ | 1.00 | 6511 | ☒ | 1.0 | 1.0 | 6511 | 6511 |
| 40 | ☒ | ☒ | 1.00 | 6401 | ☒ | 1.00 | 6401 | ☒ | 1.0 | 1.0 | 6401 | 6401 |
| 41 | ☒ | ☒ | 1.00 | 6535 | ☒ | 1.00 | 6535 | ☒ | 1.0 | 1.0 | 6535 | 6535 |
| 42 | ☒ | ☒ | 1.00 | 6535 | ☒ | 1.00 | 6535 | ☒ | 1.0 | 1.0 | 6535 | 6535 |
| 43 | ☒ | ☒ | 1.00 | 6535 | ☒ | 1.00 | 6535 | ☒ | 1.0 | 1.0 | 6535 | 6535 |
| 44 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 45 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 46 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 47 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 48 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 49 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 50 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 51 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 52 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |

## 1.9 BRUIKBAARHEIDSGEGEVENS

| No. | Verwijzing naar | Staven/VerzamelingNo. | Referentielengte Handmatig | Referentielengte l [mm] | Richt. | Toog $e_0$ [mm] | Staaftype |
|---|---|---|---|---|---|---|---|
| 1 | Staaflijst | 1 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 2 | Staaflijst | 2 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 3 | Staaflijst | 3 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 4 | Staaflijst | 4 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 5 | Staaflijst | 5 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 6 | Staaflijst | 6 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 7 | Staaflijst | 7 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 8 | Staaflijst | 8 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 9 | Staaflijst | 9 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 10 | Staaflijst | 10 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 11 | Staaflijst | 11 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 12 | Staaflijst | 12 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 13 | Staaflijst | 13 | ☐ | 19447 | y, z | 0.0 | Ligger |
| 14 | Staaflijst | 14 | ☐ | 12912 | y, z | 0.0 | Ligger |
| 15 | Staaflijst | 15 | ☐ | 12912 | y, z | 0.0 | Ligger |
| 16 | Staaflijst | 16 | ☐ | 7970 | y, z | 0.0 | Ligger |
| 17 | Staaflijst | 17 | ☐ | 8093 | y, z | 0.0 | Ligger |
| 18 | Staaflijst | 18 | ☐ | 7970 | y, z | 0.0 | Ligger |
| 19 | Staaflijst | 19 | ☐ | 8093 | y, z | 0.0 | Ligger |
| 20 | Staaflijst | 20 | ☐ | 8093 | y, z | 0.0 | Ligger |
| 21 | Staaflijst | 21 | ☐ | 8093 | y, z | 0.0 | Ligger |
| 22 | Staaflijst | 24 | ☐ | 19447 | y, z | 0.0 | Ligger |
| 23 | Staaflijst | 25 | ☐ | 6530 | y, z | 0.0 | Ligger |
| 24 | Staaflijst | 28 | ☐ | 4345 | y, z | 0.0 | Ligger |
| 25 | Staaflijst | 29 | ☐ | 4345 | y, z | 0.0 | Ligger |
| 26 | Staaflijst | 30 | ☐ | 6510 | y, z | 0.0 | Ligger |
| 27 | Staaflijst | 31 | ☐ | 6530 | y, z | 0.0 | Ligger |
| 28 | Staaflijst | 32 | ☐ | 4345 | y, z | 0.0 | Ligger |
| 29 | Staaflijst | 33 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 30 | Staaflijst | 34 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 31 | Staaflijst | 35 | ☐ | 6535 | y, z | 0.0 | Ligger |
| 32 | Staaflijst | 36 | ☐ | 6511 | y, z | 0.0 | Ligger |
| 33 | Staaflijst | 37 | ☐ | 6401 | y, z | 0.0 | Ligger |
| 34 | Staaflijst | 38 | ☐ | 6535 | y, z | 0.0 | Ligger |
| 35 | Staaflijst | 39 | ☐ | 6511 | y, z | 0.0 | Ligger |
| 36 | Staaflijst | 40 | ☐ | 6401 | y, z | 0.0 | Ligger |
| 37 | Staaflijst | 41 | ☐ | 6535 | y, z | 0.0 | Ligger |
| 38 | Staaflijst | 42 | ☐ | 6535 | y, z | 0.0 | Ligger |
| 39 | Staaflijst | 43 | ☐ | 6535 | y, z | 0.0 | Ligger |
| 40 | Staaflijst | 44 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 41 | Staaflijst | 45 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 42 | Staaflijst | 46 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 43 | Staaflijst | 47 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 44 | Staaflijst | 48 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 45 | Staaflijst | 49 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 46 | Staaflijst | 50 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 47 | Staaflijst | 51 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 48 | Staaflijst | 52 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 49 | Staaf | 47 | ☐ | 6400 | y, z | 0.0 | Ligger |
| 50 | Staaf | 48 | ☐ | 6510 | y, z | 0.0 | Ligger |
| 51 | Staaf | 49 | ☐ | 6530 | y, z | 0.0 | Ligger |
| 52 | Staaf | 50 | ☐ | 6400 | y, z | 0.0 | Ligger |
| 53 | Staaf | 53 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 54 | Staaf | 54 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 55 | Staaf | 55 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 56 | Staaf | 56 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 57 | Staaf | 57 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 58 | Staaf | 58 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 59 | Staaf | 59 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 60 | Staaf | 60 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 61 | Staaf | 61 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 62 | Staaf | 62 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 63 | Staaf | 63 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 64 | Staaf | 64 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 65 | Staaf | 65 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 66 | Staaf | 66 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 67 | Staaf | 67 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 68 | Staaf | 68 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 69 | Staaf | 69 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 70 | Staaf | 71 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 71 | Staaf | 72 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 72 | Staaf | 73 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 73 | Staaf | 75 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 74 | Staaf | 77 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 75 | Staaf | 79 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 76 | Staaf | 81 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 77 | Staaf | 82 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 78 | Staaf | 84 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 79 | Staaf | 87 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 80 | Staaf | 88 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 81 | Staaf | 89 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 82 | Staaf | 90 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 83 | Staaf | 91 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 84 | Staaf | 92 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 85 | Staaf | 93 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 86 | Staaf | 94 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 87 | Staaf | 95 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 88 | Staaf | 96 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 89 | Staaf | 97 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 90 | Staaf | 98 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 91 | Staaf | 99 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 92 | Staaf | 102 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 93 | Staaf | 112 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 94 | Staaf | 113 | ☐ | 3957 | y, z | 0.0 | Ligger |

## 1.9 BRUIKBAARHEIDSGEGEVENS

| No. | Verwijzing naar | Staven/VerzamelingNo. | Referentielengte Handmatig | l [mm] | Richt. | Toog $e_0$ [mm] | Staaftype |
|---|---|---|---|---|---|---|---|
| 95 | Staaf | 114 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 96 | Staaf | 115 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 97 | Staaf | 116 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 98 | Staaf | 117 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 99 | Staaf | 118 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 100 | Staaf | 119 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 101 | Staaf | 120 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 102 | Staaf | 121 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 103 | Staaf | 122 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 104 | Staaf | 123 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 105 | Staaf | 124 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 106 | Staaf | 125 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 107 | Staaf | 126 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 108 | Staaf | 127 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 109 | Staaf | 128 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 110 | Staaf | 129 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 111 | Staaf | 130 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 112 | Staaf | 131 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 113 | Staaf | 132 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 114 | Staaf | 133 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 115 | Staaf | 134 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 116 | Staaf | 135 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 117 | Staaf | 136 | ☐ | 7827 | y, z | 0.0 | Ligger |
| 118 | Staaf | 137 | ☐ | 7512 | y, z | 0.0 | Ligger |
| 119 | Staaf | 138 | ☐ | 7827 | y, z | 0.0 | Ligger |
| 120 | Staaf | 139 | ☐ | 7451 | y, z | 0.0 | Ligger |
| 121 | Staaf | 146 | ☐ | 7411 | y, z | 0.0 | Ligger |
| 122 | Staaf | 147 | ☐ | 7529 | y, z | 0.0 | Ligger |
| 123 | Staaf | 148 | ☐ | 1665 | y, z | 0.0 | Ligger |
| 124 | Staaf | 154 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 125 | Staaf | 155 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 126 | Staaf | 156 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 127 | Staaf | 157 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 128 | Staaf | 158 | ☐ | 7512 | y, z | 0.0 | Ligger |
| 129 | Staaf | 159 | ☐ | 7451 | y, z | 0.0 | Ligger |
| 130 | Staaf | 162 | ☐ | 1665 | y, z | 0.0 | Ligger |
| 131 | Staaf | 163 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 132 | Staaf | 164 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 133 | Staaf | 165 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 134 | Staaf | 166 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 135 | Staaf | 167 | ☐ | 7411 | y, z | 0.0 | Ligger |
| 136 | Staaf | 168 | ☐ | 7529 | y, z | 0.0 | Ligger |
| 137 | Staaf | 169 | ☐ | 1665 | y, z | 0.0 | Ligger |
| 138 | Staaf | 170 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 139 | Staaf | 171 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 140 | Staaf | 172 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 141 | Staaf | 173 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 142 | Staaf | 202 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 143 | Staaf | 204 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 144 | Staaf | 206 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 145 | Staaf | 212 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 146 | Staaf | 214 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 147 | Staaf | 216 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 148 | Staaf | 217 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 149 | Staaf | 218 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 150 | Staaf | 220 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 151 | Staaf | 221 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 152 | Staaf | 223 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 153 | Staaf | 224 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 154 | Staaf | 226 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 155 | Staaf | 227 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 156 | Staaf | 229 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 157 | Staaf | 230 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 158 | Staaf | 232 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 159 | Staaf | 233 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 160 | Staaf | 235 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 161 | Staaf | 236 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 162 | Staaf | 238 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 163 | Staaf | 239 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 164 | Staaf | 241 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 165 | Staaf | 242 | ☐ | 3967 | y, z | 0.0 | Ligger |

## 1.10 BRANDWERENDHEID - STAVEN

| No. | Staaf No. | Ben. tijd $t_{fi,ben}$ [min] | Brand Blootstellin | Brand Beschermi | Beschermin Type | Volumieke m $\rho_p$ [kg/m³] | Thermische vo $\lambda_p$ [W/m*K] | Specifieke hitte $c_p$ [J/(kg*K)] | Dikte $d_p$ [mm] |
|---|---|---|---|---|---|---|---|---|---|
| 1 | 47-50 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 2 | 53-69 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 3 | 71-73 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 4 | 75 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 5 | 77 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 6 | 79 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 7 | 81 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 8 | 82 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 9 | 84 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 10 | 87-99 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 11 | 102 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 12 | 112-139 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 13 | 146-148 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 14 | 154-159 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 15 | 162-173 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |

## 1.10 BRANDWERENDHEID - STAVEN

| No. | Staaf No. | Ben. tijd $t_{fi,ben}$ [min] | Brand Blootstellin | Brand Beschermi | Beschermin Type | Volumieke m $\rho_p$ [kg/m³] | Thermische vo $\lambda_p$ [W/m*K] | Specifieke hitte $c_p$ [J/(kg*K)] | Dikte $d_p$ [mm] |
|---|---|---|---|---|---|---|---|---|---|
| 16 | 202 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 17 | 204 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 18 | 206 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 19 | 212 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 20 | 214 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 21 | 216-218 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 22 | 220 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 23 | 221 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 24 | 223 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 25 | 224 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 26 | 226 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 27 | 227 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 28 | 229 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 29 | 230 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 30 | 232 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 31 | 233 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 32 | 235 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 33 | 236 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 34 | 238 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 35 | 239 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 36 | 241 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 37 | 242 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |

## 2.2 BEREKENING PER DOORSNEDE

| Snede No. | Staaf No. | Positie x [mm] | BG/BC/ RC | Berekening | | vergelijki No. | Omschrijving |
|---|---|---|---|---|---|---|---|
| 2 | **HE A 300 \| Euronorm 53-62 - Hoofddraag kolom** | | | | | | |
| | 30 | 198 | BC200 | 0.29 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 3 | **HE A 700 \| Euronorm 53-62 - Hoofddraag ligger** | | | | | | |
| | 85 | 3256 | BC556 | 0.78 | ≤ 1 | SE401) | Bruikbaarheid - Belastingscombinaties 'Karakteristiek' - z-richting |
| 4 | **IPE 600 \| Euronorm 19-57 - Hoofddraag dakligger** | | | | | | |
| | 191 | 3256 | BC154 | 0.60 | ≤ 1 | ST331) | Stabiliteitsberekening - Kip volgens 6.3.2.1 en 6.3.2.3 - I-profiel |
| 5 | **HE A 280 \| Euronorm 53-62 - Hoofddraag dakligger** | | | | | | |
| | 24 | 3267 | BC154 | 0.50 | ≤ 1 | ST331) | Stabiliteitsberekening - Kip volgens 6.3.2.1 en 6.3.2.3 - I-profiel |
| 6 | **HE A 240 \| Euronorm 53-62 - Hoofddraag dakligger rand** | | | | | | |
| | 189 | 0 | BC131 | 0.40 | ≤ 1 | ST331) | Stabiliteitsberekening - Kip volgens 6.3.2.1 en 6.3.2.3 - I-profiel |
| 7 | **HE A 300 \| Euronorm 53-62 - Tussenkolom** | | | | | | |
| | 44 | 198 | BC205 | 0.36 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 8 | **HE A 180 \| Euronorm 53-62 - Tussenliggers** | | | | | | |
| | 78 | 0 | BC277 | 0.22 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 9 | **HE A 200 \| Euronorm 53-62 - Dakligger rand** | | | | | | |
| | 33 | 200 | BC149 | 0.14 | ≤ 1 | CS121) | Doorsnedecontrole - Dwarskracht in z-as volgens 6.2.6 |
| 10 | **QRO 100x4 \| EN 10219-2:2006 - Dakligger midden** | | | | | | |
| | 213 | 2250 | BC554 | 0.40 | ≤ 1 | SE401) | Bruikbaarheid - Belastingscombinaties 'Karakteristiek' - z-richting |
| 11 | **L 120x120x10 \| EN 10056-1:1998 - Horizontale verbanden** | | | | | | |
| | 119 | 0 | BC139 | 0.11 | ≤ 1 | CS101) | Doorsnedecontrole - Trek volgens 6.2.3 |
| 12 | **Rechthoek 15/120 - Verticale verbanden** | | | | | | |
| | 172 | 2737 | BC240 | 0.18 | ≤ 1 | CS101) | Doorsnedecontrole - Trek volgens 6.2.3 |
| 13 | **HE A 180 \| Euronorm 53-62 - Kolom** | | | | | | |
| | 161 | 198 | BC240 | 0.22 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 14 | **HE A 200 \| Euronorm 53-62 - Dakligger** | | | | | | |
| | 37 | 200 | BC138 | 0.14 | ≤ 1 | CS121) | Doorsnedecontrole - Dwarskracht in z-as volgens 6.2.6 |

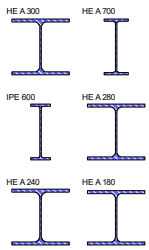
**RF-STEEL EC3**
CA2
Aardbeving

## 1.1 ALGEMENE GEGEVENS

| | | |
|---|---|---|
| Te ontwerpen staven: | 47-50,53-69,71-73,75,77,79,81,82,84,87-99,102,112-139,146-148,154-159, 162-173,202,204,206,212,214,216-218,220,221,223,224,226,227,229,230, 232,233,235,236,238,239,241,242 | |
| Te ontwerpen staafverz.: | Alle | |
| Nationale bijlagen: | NEN | |
| Ontwerp uiterste grenstoestand<br>Te berekenen RC's: | RC20 | Tabel NB.7 A1.3 |
| Ontwerp bruikbaarheidsgrenstoestand<br>Te berekenen RC's: | RC20 | Tabel NB.7 A1.3 |

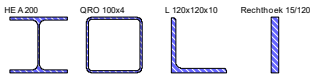
## 1.2 MATERIALEN

| Matl. No. | Materiaal Omschrijving | E-Modulus E [N/mm²] | Glijdingsmodulu G [N/mm²] | Coï¿½ff. van Poisso ν [-] | Vloeispanning $f_{yk}$ [N/mm²] | Max. Dikte t [mm] |
|---|---|---|---|---|---|---|
| 1 | Staal S 235 \| NEN EN 1993-1-1:2007-11 | 210000.0 | 80769.2 | 0.300 | 235.0 | 40.0 |
| | | | | | 215.0 | 80.0 |
| | | | | | 215.0 | 100.0 |
| | | | | | 195.0 | 150.0 |
| | | | | | 185.0 | 200.0 |
| | | | | | 175.0 | 250.0 |
| | | | | | 165.0 | 400.0 |




## 1.3 DOORSNEDES

| Snede No. | Matl. No. | Doorsnede Omschrijving | Doorsnede Type | Max Ontwerp Unity check | Commentaar |
|---|---|---|---|---|---|
| 2 | 1 | HE A 300 \| Euronorm 53-62 | Gewalst I-profiel | 0.59 | Hoofddraag kolom |
| 3 | 1 | HE A 700 \| Euronorm 53-62 | Gewalst I-profiel | 0.49 | Hoofddraag ligger |
| 4 | 1 | IPE 600 \| Euronorm 19-57 | Gewalst I-profiel | 0.53 | Hoofddraag dakligger |
| 5 | 1 | HE A 280 \| Euronorm 53-62 | Gewalst I-profiel | 0.39 | Hoofddraag dakligger |
| 6 | 1 | HE A 240 \| Euronorm 53-62 | Gewalst I-profiel | 0.56 | Hoofddraag dakligger rand |
| 7 | 1 | HE A 300 \| Euronorm 53-62 | Gewalst I-profiel | 0.77 | Tussenkolom |
| 8 | 1 | HE A 180 \| Euronorm 53-62 | Gewalst I-profiel | 0.92 | Tussenliggers |
| 9 | 1 | HE A 200 \| Euronorm 53-62 | Gewalst I-profiel | 0.29 | Dakligger rand |
| 10 | 1 | QRO 100x4 \| EN 10219-2:2006 | Vierkant Gewalst | 0.99 | Dakligger midden |
| 11 | 1 | L 120x120x10 \| EN 10056-1:1998 | Hoek | 0.47 | Horizontale verbanden |
| 12 | 1 | Rechthoek 15/120 | Platte staaf | 0.73 | Verticale verbanden |
| 13 | 1 | HE A 180 \| Euronorm 53-62 | Gewalst I-profiel | 0.74 | Kolom |
| 14 | 1 | HE A 200 \| Euronorm 53-62 | Gewalst I-profiel | 0.25 | Dakligger |




## 1.5 KNIKLENGTES - STAVEN

| Staaf No. | Knik Mogelijk | Knik om y/u-as Mogelijk | $k_{cr,y/u}$ | $L_{cr,y/u}$ [mm] | Knik om z/v-as Mogelijk | $k_{cr,z/v}$ | $L_{cr,z/v}$ [mm] | Kip Mogelijk | $k_z$ | $k_w$ | $L_w$ [mm] | $L_T$ [mm] |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 47 | ☒ | ☒ | 1.00 | 6400 | ☒ | 1.00 | 6400 | ☒ | 1.0 | 1.0 | 6400 | 6400 |
| 48 | ☒ | ☒ | 1.00 | 6510 | ☒ | 1.00 | 6510 | ☒ | 1.0 | 1.0 | 6510 | 6510 |
| 49 | ☒ | ☒ | 1.00 | 6530 | ☒ | 1.00 | 6530 | ☒ | 1.0 | 1.0 | 6530 | 6530 |
| 50 | ☒ | ☒ | 1.00 | 6400 | ☒ | 1.00 | 6400 | ☒ | 1.0 | 1.0 | 6400 | 6400 |
| 53 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 54 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 55 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 56 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 57 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 58 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 59 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 60 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 61 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 62 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 63 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 64 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 65 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 66 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 67 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 68 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 69 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 71 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 72 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 73 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 75 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 77 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 79 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 81 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 82 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 84 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 87 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 88 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 89 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 90 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 91 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 92 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 93 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 94 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 95 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 96 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 97 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 98 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 99 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |

## 1.5 KNIKLENGTES - STAVEN

| Staaf | Knik | Knik om y/u-as | | | Knik om z/v-as | | | Kip | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| No. | Mogelijk | Mogelijk | $k_{cr,y/u}$ | $L_{cr,y/u}$ [mm] | Mogelijk | $k_{cr,z/v}$ | $L_{cr,z/v}$ [mm] | Mogelijk | $k_z$ | $k_w$ | $L_w$ [mm] | $L_T$ [mm] |
| 102 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 112 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 113 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 114 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 115 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 116 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 117 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 118 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 119 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 120 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 121 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 122 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 123 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 124 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 125 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 126 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 127 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 128 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 129 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 130 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 131 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 132 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 133 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 134 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 135 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 136 | ☐ | ☐ | 1.00 | 7827 | ☐ | 1.00 | 7827 | ☐ | 1.0 | 1.0 | 7827 | 7827 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 137 | ☐ | ☐ | 1.00 | 7512 | ☐ | 1.00 | 7512 | ☐ | 1.0 | 1.0 | 7512 | 7512 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 138 | ☐ | ☐ | 1.00 | 7827 | ☐ | 1.00 | 7827 | ☐ | 1.0 | 1.0 | 7827 | 7827 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 139 | ☐ | ☐ | 1.00 | 7451 | ☐ | 1.00 | 7451 | ☐ | 1.0 | 1.0 | 7451 | 7451 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 146 | ☐ | ☐ | 1.00 | 7411 | ☐ | 1.00 | 7411 | ☐ | 1.0 | 1.0 | 7411 | 7411 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 147 | ☐ | ☐ | 1.00 | 7529 | ☐ | 1.00 | 7529 | ☐ | 1.0 | 1.0 | 7529 | 7529 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 148 | ☒ | ☒ | 1.00 | 1665 | ☒ | 1.00 | 1665 | ☒ | 1.0 | 1.0 | 1665 | 1665 |
| 154 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 155 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 156 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 157 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 158 | ☐ | ☐ | 1.00 | 7512 | ☐ | 1.00 | 7512 | ☐ | 1.0 | 1.0 | 7512 | 7512 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 159 | ☐ | ☐ | 1.00 | 7451 | ☐ | 1.00 | 7451 | ☐ | 1.0 | 1.0 | 7451 | 7451 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 162 | ☒ | ☒ | 1.00 | 1665 | ☒ | 1.00 | 1665 | ☒ | 1.0 | 1.0 | 1665 | 1665 |
| 163 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 164 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 165 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 166 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 167 | ☐ | ☐ | 1.00 | 7411 | ☐ | 1.00 | 7411 | ☐ | 1.0 | 1.0 | 7411 | 7411 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 168 | ☐ | ☐ | 1.00 | 7529 | ☐ | 1.00 | 7529 | ☐ | 1.0 | 1.0 | 7529 | 7529 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 169 | ☒ | ☒ | 1.00 | 1665 | ☒ | 1.00 | 1665 | ☒ | 1.0 | 1.0 | 1665 | 1665 |
| 170 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 171 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 172 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |

## 1.5 KNIKLENGTES - STAVEN

| Staaf | Knik | Knik om y/u-as | | | Knik om z/v-as | | | Kip | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| No. | Mogelijk | Mogelijk | $k_{cr,y/u}$ | $L_{cr,y/u}$ [mm] | Mogelijk | $k_{cr,z/v}$ | $L_{cr,z/v}$ [mm] | Mogelijk | $k_z$ | $k_w$ | $L_w$ [mm] | $L_T$ [mm] |
| 173 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 202 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 204 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 206 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 212 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 214 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 216 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 217 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 218 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 220 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 221 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 223 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 224 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 226 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 227 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 229 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 230 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 232 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 233 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 235 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 236 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 238 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 239 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 241 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 242 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |

## 1.6 KNIKLENGTES - STAAFVERZAMELINGEN

| Staafver | Knik | Knik om y-as | | | Knik om z-as | | | Kip | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| No. | Mogelijk | Mogelijk | $k_{cr,y}$ | $L_{cr,y}$ [mm] | Mogelijk | $k_{cr,z}$ | $L_{cr,z}$ [mm] | Mogelijk | $k_z$ | $k_w$ | $L_w$ [mm] | $L_T$ [mm] |
| 1 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 2 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 3 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 4 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 5 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 6 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 7 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 8 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 9 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 10 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 11 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 12 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 13 | ☒ | ☒ | 1.00 | 19447 | ☒ | 0.20 | 3889 | ☒ | 1.0 | 1.0 | 3889 | 19447 |
| 14 | ☒ | ☒ | 1.00 | 12912 | ☒ | 0.25 | 3228 | ☒ | 1.0 | 1.0 | 3228 | 12912 |
| 15 | ☒ | ☒ | 1.00 | 12912 | ☒ | 0.25 | 3228 | ☒ | 1.0 | 1.0 | 3228 | 12912 |
| 16 | ☒ | ☒ | 1.00 | 7970 | ☒ | 1.00 | 7970 | ☒ | 1.0 | 1.0 | 7970 | 7970 |
| 17 | ☒ | ☒ | 1.00 | 8093 | ☒ | 1.00 | 8093 | ☒ | 1.0 | 1.0 | 8093 | 8093 |
| 18 | ☒ | ☒ | 1.00 | 7970 | ☒ | 1.00 | 7970 | ☒ | 1.0 | 1.0 | 7970 | 7970 |
| 19 | ☒ | ☒ | 1.00 | 8093 | ☒ | 1.00 | 8093 | ☒ | 1.0 | 1.0 | 8093 | 8093 |
| 20 | ☒ | ☒ | 1.00 | 8093 | ☒ | 1.00 | 8093 | ☒ | 1.0 | 1.0 | 8093 | 8093 |
| 21 | ☒ | ☒ | 1.00 | 8093 | ☒ | 1.00 | 8093 | ☒ | 1.0 | 1.0 | 8093 | 8093 |
| 24 | ☒ | ☒ | 1.00 | 19447 | ☒ | 0.20 | 3889 | ☒ | 1.0 | 1.0 | 3889 | 19447 |
| 25 | ☒ | ☒ | 1.00 | 6530 | ☒ | 1.00 | 6530 | ☒ | 1.0 | 1.0 | 6530 | 6530 |
| 28 | ☒ | ☒ | 1.00 | 4345 | ☒ | 1.00 | 4345 | ☒ | 1.0 | 1.0 | 4345 | 4345 |
| 29 | ☒ | ☒ | 1.00 | 4345 | ☒ | 1.00 | 4345 | ☒ | 1.0 | 1.0 | 4345 | 4345 |
| 30 | ☒ | ☒ | 1.00 | 6510 | ☒ | 1.00 | 6510 | ☒ | 1.0 | 1.0 | 6510 | 6510 |
| 31 | ☒ | ☒ | 1.00 | 6530 | ☒ | 1.00 | 6530 | ☒ | 1.0 | 1.0 | 6530 | 6530 |
| 32 | ☒ | ☒ | 1.00 | 4345 | ☒ | 1.00 | 4345 | ☒ | 1.0 | 1.0 | 4345 | 4345 |
| 33 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 34 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 35 | ☒ | ☒ | 1.00 | 6535 | ☒ | 1.00 | 6535 | ☒ | 1.0 | 1.0 | 6535 | 6535 |
| 36 | ☒ | ☒ | 1.00 | 6511 | ☒ | 1.00 | 6511 | ☒ | 1.0 | 1.0 | 6511 | 6511 |
| 37 | ☒ | ☒ | 1.00 | 6401 | ☒ | 1.00 | 6401 | ☒ | 1.0 | 1.0 | 6401 | 6401 |
| 38 | ☒ | ☒ | 1.00 | 6535 | ☒ | 1.00 | 6535 | ☒ | 1.0 | 1.0 | 6535 | 6535 |
| 39 | ☒ | ☒ | 1.00 | 6511 | ☒ | 1.00 | 6511 | ☒ | 1.0 | 1.0 | 6511 | 6511 |
| 40 | ☒ | ☒ | 1.00 | 6401 | ☒ | 1.00 | 6401 | ☒ | 1.0 | 1.0 | 6401 | 6401 |
| 41 | ☒ | ☒ | 1.00 | 6535 | ☒ | 1.00 | 6535 | ☒ | 1.0 | 1.0 | 6535 | 6535 |
| 42 | ☒ | ☒ | 1.00 | 6535 | ☒ | 1.00 | 6535 | ☒ | 1.0 | 1.0 | 6535 | 6535 |
| 43 | ☒ | ☒ | 1.00 | 6535 | ☒ | 1.00 | 6535 | ☒ | 1.0 | 1.0 | 6535 | 6535 |
| 44 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 45 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 46 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 47 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |

## 1.6 KNIKLENGTES - STAAFVERZAMELINGEN

| Staafver | Knik | Knik om y-as | | | Knik om z-as | | | Kip | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| No. | Mogelijk | Mogelijk | $k_{cr,y}$ | $L_{cr,y}$ [mm] | Mogelijk | $k_{cr,z}$ | $L_{cr,z}$ [mm] | Mogelijk | $k_z$ | $k_w$ | $L_w$ [mm] | $L_T$ [mm] |
| 48 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 49 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 50 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 51 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 52 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |

## 1.9 BRUIKBAARHEIDSGEGEVENS

| No. | Verwijzing naar | Staven/VerzamelingNo. | Referentielengte Handmatig | Referentielengte l [mm] | Richt. | Toog $e_0$ [mm] | Staaftype |
|---|---|---|---|---|---|---|---|
| 1 | Staaflijst | 1 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 2 | Staaflijst | 2 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 3 | Staaflijst | 3 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 4 | Staaflijst | 4 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 5 | Staaflijst | 5 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 6 | Staaflijst | 6 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 7 | Staaflijst | 7 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 8 | Staaflijst | 8 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 9 | Staaflijst | 9 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 10 | Staaflijst | 10 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 11 | Staaflijst | 11 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 12 | Staaflijst | 12 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 13 | Staaflijst | 13 | ☐ | 19447 | y, z | 0.0 | Ligger |
| 14 | Staaflijst | 14 | ☐ | 12912 | y, z | 0.0 | Ligger |
| 15 | Staaflijst | 15 | ☐ | 12912 | y, z | 0.0 | Ligger |
| 16 | Staaflijst | 16 | ☐ | 7970 | y, z | 0.0 | Ligger |
| 17 | Staaflijst | 17 | ☐ | 8093 | y, z | 0.0 | Ligger |
| 18 | Staaflijst | 18 | ☐ | 7970 | y, z | 0.0 | Ligger |
| 19 | Staaflijst | 19 | ☐ | 8093 | y, z | 0.0 | Ligger |
| 20 | Staaflijst | 20 | ☐ | 8093 | y, z | 0.0 | Ligger |
| 21 | Staaflijst | 21 | ☐ | 8093 | y, z | 0.0 | Ligger |
| 22 | Staaflijst | 24 | ☐ | 19447 | y, z | 0.0 | Ligger |
| 23 | Staaflijst | 25 | ☐ | 6530 | y, z | 0.0 | Ligger |
| 24 | Staaflijst | 28 | ☐ | 4345 | y, z | 0.0 | Ligger |
| 25 | Staaflijst | 29 | ☐ | 4345 | y, z | 0.0 | Ligger |
| 26 | Staaflijst | 30 | ☐ | 6510 | y, z | 0.0 | Ligger |
| 27 | Staaflijst | 31 | ☐ | 6530 | y, z | 0.0 | Ligger |
| 28 | Staaflijst | 32 | ☐ | 4345 | y, z | 0.0 | Ligger |
| 29 | Staaflijst | 33 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 30 | Staaflijst | 34 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 31 | Staaflijst | 35 | ☐ | 6535 | y, z | 0.0 | Ligger |
| 32 | Staaflijst | 36 | ☐ | 6511 | y, z | 0.0 | Ligger |
| 33 | Staaflijst | 37 | ☐ | 6401 | y, z | 0.0 | Ligger |
| 34 | Staaflijst | 38 | ☐ | 6535 | y, z | 0.0 | Ligger |
| 35 | Staaflijst | 39 | ☐ | 6511 | y, z | 0.0 | Ligger |
| 36 | Staaflijst | 40 | ☐ | 6401 | y, z | 0.0 | Ligger |
| 37 | Staaflijst | 41 | ☐ | 6535 | y, z | 0.0 | Ligger |
| 38 | Staaflijst | 42 | ☐ | 6535 | y, z | 0.0 | Ligger |
| 39 | Staaflijst | 43 | ☐ | 6535 | y, z | 0.0 | Ligger |
| 40 | Staaflijst | 44 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 41 | Staaflijst | 45 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 42 | Staaflijst | 46 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 43 | Staaflijst | 47 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 44 | Staaflijst | 48 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 45 | Staaflijst | 49 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 46 | Staaflijst | 50 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 47 | Staaflijst | 51 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 48 | Staaflijst | 52 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 49 | Staaf | 47 | ☐ | 6400 | y, z | 0.0 | Ligger |
| 50 | Staaf | 48 | ☐ | 6510 | y, z | 0.0 | Ligger |
| 51 | Staaf | 49 | ☐ | 6530 | y, z | 0.0 | Ligger |
| 52 | Staaf | 50 | ☐ | 6400 | y, z | 0.0 | Ligger |
| 53 | Staaf | 53 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 54 | Staaf | 54 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 55 | Staaf | 55 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 56 | Staaf | 56 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 57 | Staaf | 57 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 58 | Staaf | 58 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 59 | Staaf | 59 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 60 | Staaf | 60 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 61 | Staaf | 61 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 62 | Staaf | 62 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 63 | Staaf | 63 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 64 | Staaf | 64 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 65 | Staaf | 65 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 66 | Staaf | 66 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 67 | Staaf | 67 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 68 | Staaf | 68 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 69 | Staaf | 69 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 70 | Staaf | 71 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 71 | Staaf | 72 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 72 | Staaf | 73 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 73 | Staaf | 75 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 74 | Staaf | 77 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 75 | Staaf | 79 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 76 | Staaf | 81 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 77 | Staaf | 82 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 78 | Staaf | 84 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 79 | Staaf | 87 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 80 | Staaf | 88 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 81 | Staaf | 89 | ☐ | 3901 | y, z | 0.0 | Ligger |

## 1.9 BRUIKBAARHEIDSGEGEVENS

| No. | Verwijzing naar | Staven/VerzamelingNo. | Referentielengte Handmatig | Referentielengte l [mm] | Richt. | Toog $e_0$ [mm] | Staaftype |
|---|---|---|---|---|---|---|---|
| 82 | Staaf | 90 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 83 | Staaf | 91 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 84 | Staaf | 92 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 85 | Staaf | 93 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 86 | Staaf | 94 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 87 | Staaf | 95 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 88 | Staaf | 96 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 89 | Staaf | 97 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 90 | Staaf | 98 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 91 | Staaf | 99 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 92 | Staaf | 102 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 93 | Staaf | 112 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 94 | Staaf | 113 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 95 | Staaf | 114 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 96 | Staaf | 115 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 97 | Staaf | 116 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 98 | Staaf | 117 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 99 | Staaf | 118 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 100 | Staaf | 119 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 101 | Staaf | 120 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 102 | Staaf | 121 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 103 | Staaf | 122 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 104 | Staaf | 123 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 105 | Staaf | 124 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 106 | Staaf | 125 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 107 | Staaf | 126 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 108 | Staaf | 127 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 109 | Staaf | 128 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 110 | Staaf | 129 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 111 | Staaf | 130 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 112 | Staaf | 131 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 113 | Staaf | 132 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 114 | Staaf | 133 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 115 | Staaf | 134 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 116 | Staaf | 135 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 117 | Staaf | 136 | ☐ | 7827 | y, z | 0.0 | Ligger |
| 118 | Staaf | 137 | ☐ | 7512 | y, z | 0.0 | Ligger |
| 119 | Staaf | 138 | ☐ | 7827 | y, z | 0.0 | Ligger |
| 120 | Staaf | 139 | ☐ | 7451 | y, z | 0.0 | Ligger |
| 121 | Staaf | 146 | ☐ | 7411 | y, z | 0.0 | Ligger |
| 122 | Staaf | 147 | ☐ | 7529 | y, z | 0.0 | Ligger |
| 123 | Staaf | 148 | ☐ | 1665 | y, z | 0.0 | Ligger |
| 124 | Staaf | 154 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 125 | Staaf | 155 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 126 | Staaf | 156 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 127 | Staaf | 157 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 128 | Staaf | 158 | ☐ | 7512 | y, z | 0.0 | Ligger |
| 129 | Staaf | 159 | ☐ | 7451 | y, z | 0.0 | Ligger |
| 130 | Staaf | 162 | ☐ | 1665 | y, z | 0.0 | Ligger |
| 131 | Staaf | 163 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 132 | Staaf | 164 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 133 | Staaf | 165 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 134 | Staaf | 166 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 135 | Staaf | 167 | ☐ | 7411 | y, z | 0.0 | Ligger |
| 136 | Staaf | 168 | ☐ | 7529 | y, z | 0.0 | Ligger |
| 137 | Staaf | 169 | ☐ | 1665 | y, z | 0.0 | Ligger |
| 138 | Staaf | 170 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 139 | Staaf | 171 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 140 | Staaf | 172 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 141 | Staaf | 173 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 142 | Staaf | 202 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 143 | Staaf | 204 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 144 | Staaf | 206 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 145 | Staaf | 212 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 146 | Staaf | 214 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 147 | Staaf | 216 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 148 | Staaf | 217 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 149 | Staaf | 218 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 150 | Staaf | 220 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 151 | Staaf | 221 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 152 | Staaf | 223 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 153 | Staaf | 224 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 154 | Staaf | 226 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 155 | Staaf | 227 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 156 | Staaf | 229 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 157 | Staaf | 230 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 158 | Staaf | 232 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 159 | Staaf | 233 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 160 | Staaf | 235 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 161 | Staaf | 236 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 162 | Staaf | 238 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 163 | Staaf | 239 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 164 | Staaf | 241 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 165 | Staaf | 242 | ☐ | 3967 | y, z | 0.0 | Ligger |

## 1.10 BRANDWERENDHEID - STAVEN

| No. | Staaf No. | Ben. tijd $t_{fi,ben}$ [min] | Brand Blootstellin | Brand Beschermi | Beschermin Type | Volumieke m $\rho_p$ [kg/m³] | Thermische vo $\lambda_p$ [W/m*K] | Specifieke hitte $c_p$ [J/(kg*K)] | Dikte $d_p$ [mm] |
|---|---|---|---|---|---|---|---|---|---|
| 1 | 47-50 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 2 | 53-69 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 3 | 71-73 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 4 | 75 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 5 | 77 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 6 | 79 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 7 | 81 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 8 | 82 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 9 | 84 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 10 | 87-99 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 11 | 102 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 12 | 112-139 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 13 | 146-148 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 14 | 154-159 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 15 | 162-173 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 16 | 202 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 17 | 204 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 18 | 206 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 19 | 212 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 20 | 214 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 21 | 216-218 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 22 | 220 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 23 | 221 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 24 | 223 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 25 | 224 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 26 | 226 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 27 | 227 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 28 | 229 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 29 | 230 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 30 | 232 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 31 | 233 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 32 | 235 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 33 | 236 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 34 | 238 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 35 | 239 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 36 | 241 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 37 | 242 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |

## 2.2 BEREKENING PER DOORSNEDE

| Snede No. | Staaf No. | Positie x [mm] | BG/BC/ RC | Berekening | | vergelijki No. | Omschrijving |
|---|---|---|---|---|---|---|---|
| 2 | **HE A 300 \| Euronorm 53-62 - Hoofddraag kolom** | | | | | | |
| | 29 | 198 | RC20 | 0.59 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 3 | **HE A 700 \| Euronorm 53-62 - Hoofddraag ligger** | | | | | | |
| | 15 | 0 | RC20 | 0.49 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 4 | **IPE 600 \| Euronorm 19-57 - Hoofddraag dakligger** | | | | | | |
| | 46 | 0 | RC20 | 0.53 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 5 | **HE A 280 \| Euronorm 53-62 - Hoofddraag dakligger** | | | | | | |
| | 196 | 3075 | RC20 | 0.39 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 6 | **HE A 240 \| Euronorm 53-62 - Hoofddraag dakligger rand** | | | | | | |
| | 194 | 3256 | RC20 | 0.56 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 7 | **HE A 300 \| Euronorm 53-62 - Tussenkolom** | | | | | | |
| | 44 | 198 | RC20 | 0.77 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 8 | **HE A 180 \| Euronorm 53-62 - Tussenliggers** | | | | | | |
| | 48 | 197 | RC20 | 0.92 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 9 | **HE A 200 \| Euronorm 53-62 - Dakligger rand** | | | | | | |
| | 64 | 0 | RC20 | 0.29 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 10 | **QRO 100x4 \| EN 10219-2:2006 - Dakligger midden** | | | | | | |
| | 84 | 196 | RC20 | 0.99 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 11 | **L 120x120x10 \| EN 10056-1:1998 - Horizontale verbanden** | | | | | | |
| | 92 | 3912 | RC20 | 0.47 | ≤ 1 | CS101) | Doorsnedecontrole - Trek volgens 6.2.3 |
| 12 | **Rechthoek 15/120 - Verticale verbanden** | | | | | | |
| | 138 | 7827 | RC20 | 0.73 | ≤ 1 | CS101) | Doorsnedecontrole - Trek volgens 6.2.3 |
| 13 | **HE A 180 \| Euronorm 53-62 - Kolom** | | | | | | |
| | 161 | 198 | RC20 | 0.74 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 14 | **HE A 200 \| Euronorm 53-62 - Dakligger** | | | | | | |
| | 37 | 160 | RC20 | 0.25 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |

**RF-STEEL EC3**
CA3
Brand 60min

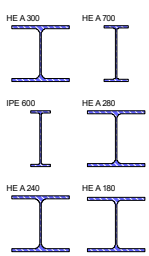
## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| Te ontwerpen staven: | 47-50,53-69,71-73,75,77,79,81,82,84,87-99,102,112-139,146-148,154-159, 162-173,202,204,206,212,214,216-218,220,221,223,224,226,227,229,230, 232,233,235,236,238,239,241,242 |
| Te ontwerpen staafverz.: | Alle |
| Nationale bijlagen: | NEN |
| Brandwerendheid ontwerp | |
| Te berekenen belastingscombinaties: | BC959 BG10 + BG20 + BG30 + BG40 |
| | BC960 BG10 + BG20 + BG30 + BG40 + 0.8*BG100 |
| | BC961 BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 |
| | BC962 BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 |
| | BC963 BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 |
| | BC964 BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | BC965 BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 |
| | BC966 BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 |
| | BC967 BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 |
| | BC968 BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG150 |
| | BC969 BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 |
| | BC970 BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 |
| | BC971 BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | BC972 BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 |
| | BC973 BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 |
| | BC974 BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 |
| | BC975 BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 |
| | BC976 BG10 + BG20 + BG30 + BG40 + 0.8*BG110 |
| | BC977 BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 |
| | BC978 BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 |
| | BC979 BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | BC980 BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 |
| | BC981 BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 |
| | BC982 BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 |
| | BC983 BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 |
| | BC984 BG10 + BG20 + BG30 + BG40 + 0.8*BG130 |
| | BC985 BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 |
| | BC986 BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | BC987 BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 |
| | BC988 BG10 + BG20 + BG30 + BG40 + 0.8*BG140 |
| | BC989 BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 |
| | BC990 BG10 + BG20 + BG30 + BG40 + 0.8*BG150 |

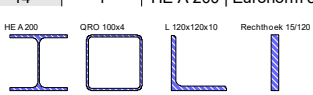
## 1.2 MATERIALEN

| Matl. No. | Materiaal Omschrijving | E-Modulus E [N/mm²] | Glijdingsmodulu G [N/mm²] | Coï¿½ff. van Poisso ν [-] | Vloeispanning $f_{yk}$ [N/mm²] | Max. Dikte t [mm] |
|---|---|---|---|---|---|---|
| 1 | Staal S 235 \| NEN EN 1993-1-1:2007-11 | 210000.0 | 80769.2 | 0.300 | 235.0 | 40.0 |
| | | | | | 215.0 | 80.0 |
| | | | | | 215.0 | 100.0 |
| | | | | | 195.0 | 150.0 |
| | | | | | 185.0 | 200.0 |
| | | | | | 175.0 | 250.0 |
| | | | | | 165.0 | 400.0 |

## 1.3 DOORSNEDES




| Snede No. | Matl. No. | Doorsnede Omschrijving | Doorsnede Type | Max Ontwerp Unity check | Commentaar |
|---|---|---|---|---|---|
| 2 | 1 | HE A 300 \| Euronorm 53-62 | Gewalst I-profiel | 0.31 | Hoofddraag kolom |
| 3 | 1 | HE A 700 \| Euronorm 53-62 | Gewalst I-profiel | 0.45 | Hoofddraag ligger |
| 4 | 1 | IPE 600 \| Euronorm 19-57 | Gewalst I-profiel | 0.59 | Hoofddraag dakligger |
| 5 | 1 | HE A 280 \| Euronorm 53-62 | Gewalst I-profiel | 0.87 | Hoofddraag dakligger |
| 6 | 1 | HE A 240 \| Euronorm 53-62 | Gewalst I-profiel | 0.82 | Hoofddraag dakligger rand |
| 7 | 1 | HE A 300 \| Euronorm 53-62 | Gewalst I-profiel | 0.49 | Tussenkolom |
| 8 | 1 | HE A 180 \| Euronorm 53-62 | Gewalst I-profiel | 0.60 | Tussenliggers |
| 9 | 1 | HE A 200 \| Euronorm 53-62 | Gewalst I-profiel | 0.23 | Dakligger rand |
| 10 | 1 | QRO 100x4 \| EN 10219-2:2006 | Vierkant Gewalst | 0.86 | Dakligger midden |
| 11 | 1 | L 120x120x10 \| EN 10056-1:1998 | Hoek | 0.15 | Horizontale verbanden |
| 12 | 1 | Rechthoek 15/120 | Platte staaf | 0.11 | Verticale verbanden |
| 13 | 1 | HE A 180 \| Euronorm 53-62 | Gewalst I-profiel | 0.36 | Kolom |
| 14 | 1 | HE A 200 \| Euronorm 53-62 | Gewalst I-profiel | 0.22 | Dakligger |



## 1.5 KNIKLENGTES - STAVEN

| Staaf | Knik | Knik om y/u-as | | | Knik om z/v-as | | | Kip | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| No. | Mogelijk | Mogelijk | $k_{cr,y/u}$ | $L_{cr,y/u}$ [mm] | Mogelijk | $k_{cr,z/v}$ | $L_{cr,z/v}$ [mm] | Mogelijk | $k_z$ | $k_w$ | $L_w$ [mm] | $L_T$ [mm] |
| 47 | ☒ | ☒ | 1.00 | 6400 | ☒ | 1.00 | 6400 | ☒ | 1.0 | 1.0 | 6400 | 6400 |
| 48 | ☒ | ☒ | 1.00 | 6510 | ☒ | 1.00 | 6510 | ☒ | 1.0 | 1.0 | 6510 | 6510 |
| 49 | ☒ | ☒ | 1.00 | 6530 | ☒ | 1.00 | 6530 | ☒ | 1.0 | 1.0 | 6530 | 6530 |
| 50 | ☒ | ☒ | 1.00 | 6400 | ☒ | 1.00 | 6400 | ☒ | 1.0 | 1.0 | 6400 | 6400 |
| 53 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 54 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 55 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 56 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 57 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 58 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 59 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 60 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 61 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 62 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 63 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 64 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 65 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 66 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 67 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 68 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 69 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 71 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 72 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 73 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 75 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 77 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 79 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 81 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 82 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 84 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 87 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 88 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 89 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 90 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 91 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 92 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 93 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 94 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 95 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 96 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 97 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 98 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 99 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 102 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 112 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 113 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 114 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 115 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 116 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 117 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 118 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 119 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 120 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 121 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 122 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 123 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 124 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 125 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 126 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 127 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 128 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 129 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 130 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 131 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |

## 1.5 KNIKLENGTES - STAVEN

| Staaf | Knik | Knik om y/u-as | | | Knik om z/v-as | | | Kip | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| No. | Mogelijk | Mogelijk | $k_{cr,y/u}$ | $L_{cr,y/u}$ [mm] | Mogelijk | $k_{cr,z/v}$ | $L_{cr,z/v}$ [mm] | Mogelijk | $k_z$ | $k_w$ | $L_w$ [mm] | $L_T$ [mm] |
| 132 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 133 | ☐ | ☐ | 1.00 | 6255 | ☐ | 1.00 | 6255 | ☐ | 1.0 | 1.0 | 6255 | 6255 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 134 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 135 | ☐ | ☐ | 1.00 | 5704 | ☐ | 1.00 | 5704 | ☐ | 1.0 | 1.0 | 5704 | 5704 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 136 | ☐ | ☐ | 1.00 | 7827 | ☐ | 1.00 | 7827 | ☐ | 1.0 | 1.0 | 7827 | 7827 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 137 | ☐ | ☐ | 1.00 | 7512 | ☐ | 1.00 | 7512 | ☐ | 1.0 | 1.0 | 7512 | 7512 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 138 | ☐ | ☐ | 1.00 | 7827 | ☐ | 1.00 | 7827 | ☐ | 1.0 | 1.0 | 7827 | 7827 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 139 | ☐ | ☐ | 1.00 | 7451 | ☐ | 1.00 | 7451 | ☐ | 1.0 | 1.0 | 7451 | 7451 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 146 | ☐ | ☐ | 1.00 | 7411 | ☐ | 1.00 | 7411 | ☐ | 1.0 | 1.0 | 7411 | 7411 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 147 | ☐ | ☐ | 1.00 | 7529 | ☐ | 1.00 | 7529 | ☐ | 1.0 | 1.0 | 7529 | 7529 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 148 | ☒ | ☒ | 1.00 | 1665 | ☒ | 1.00 | 1665 | ☒ | 1.0 | 1.0 | 1665 | 1665 |
| 154 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 155 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 156 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 157 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 158 | ☐ | ☐ | 1.00 | 7512 | ☐ | 1.00 | 7512 | ☐ | 1.0 | 1.0 | 7512 | 7512 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 159 | ☐ | ☐ | 1.00 | 7451 | ☐ | 1.00 | 7451 | ☐ | 1.0 | 1.0 | 7451 | 7451 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 162 | ☒ | ☒ | 1.00 | 1665 | ☒ | 1.00 | 1665 | ☒ | 1.0 | 1.0 | 1665 | 1665 |
| 163 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 164 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 165 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 166 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 167 | ☐ | ☐ | 1.00 | 7411 | ☐ | 1.00 | 7411 | ☐ | 1.0 | 1.0 | 7411 | 7411 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 168 | ☐ | ☐ | 1.00 | 7529 | ☐ | 1.00 | 7529 | ☐ | 1.0 | 1.0 | 7529 | 7529 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 169 | ☒ | ☒ | 1.00 | 1665 | ☒ | 1.00 | 1665 | ☒ | 1.0 | 1.0 | 1665 | 1665 |
| 170 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 171 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 172 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 173 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 202 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 204 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 206 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 212 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 214 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 216 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 217 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 218 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 220 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 221 | ☐ | ☐ | 1.00 | 3912 | ☐ | 1.00 | 3912 | ☐ | 1.0 | 1.0 | 3912 | 3912 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 223 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 224 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 226 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 227 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 229 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 230 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 232 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 233 | ☐ | ☐ | 1.00 | 3957 | ☐ | 1.00 | 3957 | ☐ | 1.0 | 1.0 | 3957 | 3957 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 235 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 236 | ☐ | ☐ | 1.00 | 3901 | ☐ | 1.00 | 3901 | ☐ | 1.0 | 1.0 | 3901 | 3901 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 238 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 239 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 241 | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |

## 1.5 KNIKLENGTES - STAVEN

| Staaf | Knik | Knik om y/u-as | | | Knik om z/v-as | | | Kip | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| No. | Mogelijk | Mogelijk | $k_{cr,y/u}$ | $L_{cr,y/u}$ [mm] | Mogelijk | $k_{cr,z/v}$ | $L_{cr,z/v}$ [mm] | Mogelijk | $k_z$ | $k_w$ | $L_w$ [mm] | $L_T$ [mm] |
| 242 | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| | ☐ | ☐ | 1.00 | 3967 | ☐ | 1.00 | 3967 | ☐ | 1.0 | 1.0 | 3967 | 3967 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |

## 1.6 KNIKLENGTES - STAAFVERZAMELINGEN

| Staafver | Knik | Knik om y-as | | | Knik om z-as | | | Kip | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| No. | Mogelijk | Mogelijk | $k_{cr,y}$ | $L_{cr,y}$ [mm] | Mogelijk | $k_{cr,z}$ | $L_{cr,z}$ [mm] | Mogelijk | $k_z$ | $k_w$ | $L_w$ [mm] | $L_T$ [mm] |
| 1 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 2 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 3 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 4 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 5 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 6 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 7 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 8 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 9 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 10 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 11 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 12 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 13 | ☒ | ☒ | 1.00 | 19447 | ☒ | 0.20 | 3889 | ☒ | 1.0 | 1.0 | 3889 | 19447 |
| 14 | ☒ | ☒ | 1.00 | 12912 | ☒ | 0.25 | 3228 | ☒ | 1.0 | 1.0 | 3228 | 12912 |
| 15 | ☒ | ☒ | 1.00 | 12912 | ☒ | 0.25 | 3228 | ☒ | 1.0 | 1.0 | 3228 | 12912 |
| 16 | ☒ | ☒ | 1.00 | 7970 | ☒ | 1.00 | 7970 | ☒ | 1.0 | 1.0 | 7970 | 7970 |
| 17 | ☒ | ☒ | 1.00 | 8093 | ☒ | 1.00 | 8093 | ☒ | 1.0 | 1.0 | 8093 | 8093 |
| 18 | ☒ | ☒ | 1.00 | 7970 | ☒ | 1.00 | 7970 | ☒ | 1.0 | 1.0 | 7970 | 7970 |
| 19 | ☒ | ☒ | 1.00 | 8093 | ☒ | 1.00 | 8093 | ☒ | 1.0 | 1.0 | 8093 | 8093 |
| 20 | ☒ | ☒ | 1.00 | 8093 | ☒ | 1.00 | 8093 | ☒ | 1.0 | 1.0 | 8093 | 8093 |
| 21 | ☒ | ☒ | 1.00 | 8093 | ☒ | 1.00 | 8093 | ☒ | 1.0 | 1.0 | 8093 | 8093 |
| 24 | ☒ | ☒ | 1.00 | 19447 | ☒ | 0.20 | 3889 | ☒ | 1.0 | 1.0 | 3889 | 19447 |
| 25 | ☒ | ☒ | 1.00 | 6530 | ☒ | 1.00 | 6530 | ☒ | 1.0 | 1.0 | 6530 | 6530 |
| 28 | ☒ | ☒ | 1.00 | 4345 | ☒ | 1.00 | 4345 | ☒ | 1.0 | 1.0 | 4345 | 4345 |
| 29 | ☒ | ☒ | 1.00 | 4345 | ☒ | 1.00 | 4345 | ☒ | 1.0 | 1.0 | 4345 | 4345 |
| 30 | ☒ | ☒ | 1.00 | 6510 | ☒ | 1.00 | 6510 | ☒ | 1.0 | 1.0 | 6510 | 6510 |
| 31 | ☒ | ☒ | 1.00 | 6530 | ☒ | 1.00 | 6530 | ☒ | 1.0 | 1.0 | 6530 | 6530 |
| 32 | ☒ | ☒ | 1.00 | 4345 | ☒ | 1.00 | 4345 | ☒ | 1.0 | 1.0 | 4345 | 4345 |
| 33 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 34 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 35 | ☒ | ☒ | 1.00 | 6535 | ☒ | 1.00 | 6535 | ☒ | 1.0 | 1.0 | 6535 | 6535 |
| 36 | ☒ | ☒ | 1.00 | 6511 | ☒ | 1.00 | 6511 | ☒ | 1.0 | 1.0 | 6511 | 6511 |
| 37 | ☒ | ☒ | 1.00 | 6401 | ☒ | 1.00 | 6401 | ☒ | 1.0 | 1.0 | 6401 | 6401 |
| 38 | ☒ | ☒ | 1.00 | 6535 | ☒ | 1.00 | 6535 | ☒ | 1.0 | 1.0 | 6535 | 6535 |
| 39 | ☒ | ☒ | 1.00 | 6511 | ☒ | 1.00 | 6511 | ☒ | 1.0 | 1.0 | 6511 | 6511 |
| 40 | ☒ | ☒ | 1.00 | 6401 | ☒ | 1.00 | 6401 | ☒ | 1.0 | 1.0 | 6401 | 6401 |
| 41 | ☒ | ☒ | 1.00 | 6535 | ☒ | 1.00 | 6535 | ☒ | 1.0 | 1.0 | 6535 | 6535 |
| 42 | ☒ | ☒ | 1.00 | 6535 | ☒ | 1.00 | 6535 | ☒ | 1.0 | 1.0 | 6535 | 6535 |
| 43 | ☒ | ☒ | 1.00 | 6535 | ☒ | 1.00 | 6535 | ☒ | 1.0 | 1.0 | 6535 | 6535 |
| 44 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 45 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 46 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 47 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 48 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 49 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 50 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☐ | 1.0 | 1.0 | 4300 | 4300 |
| 51 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |
| 52 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☐ | 1.0 | 1.0 | 4500 | 4500 |

## 1.9 BRUIKBAARHEIDSGEGEVENS

| | | | Referentielengte | | | Toog | |
|---|---|---|---|---|---|---|---|
| No. | Verwijzing naar | Staven/VerzamelingNo. | Handmatig | l [mm] | Richt. | $e_0$ [mm] | Staaftype |
| 1 | Staaflijst | 1 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 2 | Staaflijst | 2 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 3 | Staaflijst | 3 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 4 | Staaflijst | 4 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 5 | Staaflijst | 5 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 6 | Staaflijst | 6 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 7 | Staaflijst | 7 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 8 | Staaflijst | 8 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 9 | Staaflijst | 9 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 10 | Staaflijst | 10 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 11 | Staaflijst | 11 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 12 | Staaflijst | 12 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 13 | Staaflijst | 13 | ☐ | 19447 | y, z | 0.0 | Ligger |
| 14 | Staaflijst | 14 | ☐ | 12912 | y, z | 0.0 | Ligger |
| 15 | Staaflijst | 15 | ☐ | 12912 | y, z | 0.0 | Ligger |
| 16 | Staaflijst | 16 | ☐ | 7970 | y, z | 0.0 | Ligger |
| 17 | Staaflijst | 17 | ☐ | 8093 | y, z | 0.0 | Ligger |
| 18 | Staaflijst | 18 | ☐ | 7970 | y, z | 0.0 | Ligger |
| 19 | Staaflijst | 19 | ☐ | 8093 | y, z | 0.0 | Ligger |
| 20 | Staaflijst | 20 | ☐ | 8093 | y, z | 0.0 | Ligger |
| 21 | Staaflijst | 21 | ☐ | 8093 | y, z | 0.0 | Ligger |
| 22 | Staaflijst | 24 | ☐ | 19447 | y, z | 0.0 | Ligger |
| 23 | Staaflijst | 25 | ☐ | 6530 | y, z | 0.0 | Ligger |
| 24 | Staaflijst | 28 | ☐ | 4345 | y, z | 0.0 | Ligger |
| 25 | Staaflijst | 29 | ☐ | 4345 | y, z | 0.0 | Ligger |
| 26 | Staaflijst | 30 | ☐ | 6510 | y, z | 0.0 | Ligger |
| 27 | Staaflijst | 31 | ☐ | 6530 | y, z | 0.0 | Ligger |
| 28 | Staaflijst | 32 | ☐ | 4345 | y, z | 0.0 | Ligger |

## 1.9 BRUIKBAARHEIDSGEGEVENS

| No. | Verwijzing naar | Staven/VerzamelingNo. | Referentielengte Handmatig | Referentielengte l [mm] | Richt. | Toog $e_0$ [mm] | Staaftype |
|---|---|---|---|---|---|---|---|
| 29 | Staaflijst | 33 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 30 | Staaflijst | 34 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 31 | Staaflijst | 35 | ☐ | 6535 | y, z | 0.0 | Ligger |
| 32 | Staaflijst | 36 | ☐ | 6511 | y, z | 0.0 | Ligger |
| 33 | Staaflijst | 37 | ☐ | 6401 | y, z | 0.0 | Ligger |
| 34 | Staaflijst | 38 | ☐ | 6535 | y, z | 0.0 | Ligger |
| 35 | Staaflijst | 39 | ☐ | 6511 | y, z | 0.0 | Ligger |
| 36 | Staaflijst | 40 | ☐ | 6401 | y, z | 0.0 | Ligger |
| 37 | Staaflijst | 41 | ☐ | 6535 | y, z | 0.0 | Ligger |
| 38 | Staaflijst | 42 | ☐ | 6535 | y, z | 0.0 | Ligger |
| 39 | Staaflijst | 43 | ☐ | 6535 | y, z | 0.0 | Ligger |
| 40 | Staaflijst | 44 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 41 | Staaflijst | 45 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 42 | Staaflijst | 46 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 43 | Staaflijst | 47 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 44 | Staaflijst | 48 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 45 | Staaflijst | 49 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 46 | Staaflijst | 50 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 47 | Staaflijst | 51 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 48 | Staaflijst | 52 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 49 | Staaf | 47 | ☐ | 6400 | y, z | 0.0 | Ligger |
| 50 | Staaf | 48 | ☐ | 6510 | y, z | 0.0 | Ligger |
| 51 | Staaf | 49 | ☐ | 6530 | y, z | 0.0 | Ligger |
| 52 | Staaf | 50 | ☐ | 6400 | y, z | 0.0 | Ligger |
| 53 | Staaf | 53 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 54 | Staaf | 54 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 55 | Staaf | 55 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 56 | Staaf | 56 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 57 | Staaf | 57 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 58 | Staaf | 58 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 59 | Staaf | 59 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 60 | Staaf | 60 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 61 | Staaf | 61 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 62 | Staaf | 62 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 63 | Staaf | 63 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 64 | Staaf | 64 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 65 | Staaf | 65 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 66 | Staaf | 66 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 67 | Staaf | 67 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 68 | Staaf | 68 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 69 | Staaf | 69 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 70 | Staaf | 71 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 71 | Staaf | 72 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 72 | Staaf | 73 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 73 | Staaf | 75 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 74 | Staaf | 77 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 75 | Staaf | 79 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 76 | Staaf | 81 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 77 | Staaf | 82 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 78 | Staaf | 84 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 79 | Staaf | 87 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 80 | Staaf | 88 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 81 | Staaf | 89 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 82 | Staaf | 90 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 83 | Staaf | 91 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 84 | Staaf | 92 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 85 | Staaf | 93 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 86 | Staaf | 94 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 87 | Staaf | 95 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 88 | Staaf | 96 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 89 | Staaf | 97 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 90 | Staaf | 98 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 91 | Staaf | 99 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 92 | Staaf | 102 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 93 | Staaf | 112 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 94 | Staaf | 113 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 95 | Staaf | 114 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 96 | Staaf | 115 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 97 | Staaf | 116 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 98 | Staaf | 117 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 99 | Staaf | 118 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 100 | Staaf | 119 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 101 | Staaf | 120 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 102 | Staaf | 121 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 103 | Staaf | 122 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 104 | Staaf | 123 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 105 | Staaf | 124 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 106 | Staaf | 125 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 107 | Staaf | 126 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 108 | Staaf | 127 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 109 | Staaf | 128 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 110 | Staaf | 129 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 111 | Staaf | 130 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 112 | Staaf | 131 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 113 | Staaf | 132 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 114 | Staaf | 133 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 115 | Staaf | 134 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 116 | Staaf | 135 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 117 | Staaf | 136 | ☐ | 7827 | y, z | 0.0 | Ligger |
| 118 | Staaf | 137 | ☐ | 7512 | y, z | 0.0 | Ligger |
| 119 | Staaf | 138 | ☐ | 7827 | y, z | 0.0 | Ligger |
| 120 | Staaf | 139 | ☐ | 7451 | y, z | 0.0 | Ligger |
| 121 | Staaf | 146 | ☐ | 7411 | y, z | 0.0 | Ligger |
| 122 | Staaf | 147 | ☐ | 7529 | y, z | 0.0 | Ligger |

## 1.9 BRUIKBAARHEIDSGEGEVENS

| No. | Verwijzing naar | Staven/VerzamelingNo. | Referentielengte Handmatig | Referentielengte l [mm] | Richt. | Toog $e_0$ [mm] | Staaftype |
|---|---|---|---|---|---|---|---|
| 123 | Staaf | 148 | ☐ | 1665 | y, z | 0.0 | Ligger |
| 124 | Staaf | 154 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 125 | Staaf | 155 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 126 | Staaf | 156 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 127 | Staaf | 157 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 128 | Staaf | 158 | ☐ | 7512 | y, z | 0.0 | Ligger |
| 129 | Staaf | 159 | ☐ | 7451 | y, z | 0.0 | Ligger |
| 130 | Staaf | 162 | ☐ | 1665 | y, z | 0.0 | Ligger |
| 131 | Staaf | 163 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 132 | Staaf | 164 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 133 | Staaf | 165 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 134 | Staaf | 166 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 135 | Staaf | 167 | ☐ | 7411 | y, z | 0.0 | Ligger |
| 136 | Staaf | 168 | ☐ | 7529 | y, z | 0.0 | Ligger |
| 137 | Staaf | 169 | ☐ | 1665 | y, z | 0.0 | Ligger |
| 138 | Staaf | 170 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 139 | Staaf | 171 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 140 | Staaf | 172 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 141 | Staaf | 173 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 142 | Staaf | 202 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 143 | Staaf | 204 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 144 | Staaf | 206 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 145 | Staaf | 212 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 146 | Staaf | 214 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 147 | Staaf | 216 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 148 | Staaf | 217 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 149 | Staaf | 218 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 150 | Staaf | 220 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 151 | Staaf | 221 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 152 | Staaf | 223 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 153 | Staaf | 224 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 154 | Staaf | 226 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 155 | Staaf | 227 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 156 | Staaf | 229 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 157 | Staaf | 230 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 158 | Staaf | 232 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 159 | Staaf | 233 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 160 | Staaf | 235 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 161 | Staaf | 236 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 162 | Staaf | 238 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 163 | Staaf | 239 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 164 | Staaf | 241 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 165 | Staaf | 242 | ☐ | 3967 | y, z | 0.0 | Ligger |

## 1.10 BRANDWERENDHEID - STAVEN

| No. | Staaf No. | Ben. tijd $t_{fi,ben}$ [min] | Brand Blootstellin | Brand Beschermi | Beschermin Type | Volumieke m $\rho_p$ [kg/m³] | Thermische vo $\lambda_p$ [W/m*K] | Specifieke hitte $c_p$ [J/(kg*K)] | Dikte $d_p$ [mm] |
|---|---|---|---|---|---|---|---|---|---|
| 1 | 47-50 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 2 | 53-69 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 3 | 71-73 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 4 | 75 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 5 | 77 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 6 | 79 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 7 | 81 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 8 | 82 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 9 | 84 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 10 | 87-99 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 11 | 102 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 12 | 112-139 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 13 | 146-148 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 14 | 154-159 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 15 | 162-173 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 16 | 202 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 17 | 204 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 18 | 206 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 19 | 212 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 20 | 214 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 21 | 216-218 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 22 | 220 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 23 | 221 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 24 | 223 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 25 | 224 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 26 | 226 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 27 | 227 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 28 | 229 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 29 | 230 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 30 | 232 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 31 | 233 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 32 | 235 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 33 | 236 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 34 | 238 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 35 | 239 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 36 | 241 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 37 | 242 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |

## 1.11 BRANDWERENDHEID - STAAFVERZAMELINGEN

| No. | Staafverz. N | Ben. tijd $t_{fi,ben}$ [min] | Brand Blootstellin | Brand Beschermi | Beschermin Type | Volumieke m $\rho_p$ [kg/m³] | Thermische vo $\lambda_p$ [W/m*K] | Specifieke hitte $c_p$ [J/(kg*K)] | Dikte $d_p$ [mm] |
|---|---|---|---|---|---|---|---|---|---|
| 1 | 1-21 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 2 | 24 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 3 | 25 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 4 | 28-52 | 60 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |

## 2.2 BEREKENING PER DOORSNEDE

| Snede No. | Staaf No. | Positie x [mm] | BG/BC/ RC | Berekening | | vergelijki No. | Omschrijving |
|---|---|---|---|---|---|---|---|
| 2 | **HE A 300 \| Euronorm 53-62 - Hoofddraag kolom** | | | | | | |
| | 14 | 4345 | BC969 | 0.31 | ≤ 1 | FS854) | Berekening bij brand - Stabiliteitsberekening - Buiging en druk volgens EN 1993-1-2, 4.2.3.5 |
| 3 | **HE A 700 \| Euronorm 53-62 - Hoofddraag ligger** | | | | | | |
| | 192 | 0 | BC971 | 0.45 | ≤ 1 | FS831) | Berekening bij brand - Stabiliteitsberekening - Kip volgens EN 1993-1-2, 4.2.3.3 |
| 4 | **IPE 600 \| Euronorm 19-57 - Hoofddraag dakligger** | | | | | | |
| | 191 | 3256 | BC985 | 0.59 | ≤ 1 | FS831) | Berekening bij brand - Stabiliteitsberekening - Kip volgens EN 1993-1-2, 4.2.3.3 |
| 5 | **HE A 280 \| Euronorm 53-62 - Hoofddraag dakligger** | | | | | | |
| | 196 | 0 | BC965 | 0.87 | ≤ 1 | FS832) | Berekening bij brand - Stabiliteitsberekening - Kip volgens EN 1993-1-2, 4.2.3.4 |
| 6 | **HE A 240 \| Euronorm 53-62 - Hoofddraag dakligger rand** | | | | | | |
| | 189 | 0 | BC962 | 0.82 | ≤ 1 | FS831) | Berekening bij brand - Stabiliteitsberekening - Kip volgens EN 1993-1-2, 4.2.3.3 |
| 7 | **HE A 300 \| Euronorm 53-62 - Tussenkolom** | | | | | | |
| | 101 | 0 | BC986 | 0.49 | ≤ 1 | FS854) | Berekening bij brand - Stabiliteitsberekening - Buiging en druk volgens EN 1993-1-2, 4.2.3.5 |
| 8 | **HE A 180 \| Euronorm 53-62 - Tussenliggers** | | | | | | |
| | 78 | 0 | BC986 | 0.60 | ≤ 1 | FS831) | Berekening bij brand - Stabiliteitsberekening - Kip volgens EN 1993-1-2, 4.2.3.3 |
| 9 | **HE A 200 \| Euronorm 53-62 - Dakligger rand** | | | | | | |
| | 69 | 2152 | BC980 | 0.23 | ≤ 1 | FS854) | Berekening bij brand - Stabiliteitsberekening - Buiging en druk volgens EN 1993-1-2, 4.2.3.5 |
| 10 | **QRO 100x4 \| EN 10219-2:2006 - Dakligger midden** | | | | | | |
| | 84 | 2152 | BC969 | 0.86 | ≤ 1 | FS854) | Berekening bij brand - Stabiliteitsberekening - Buiging en druk volgens EN 1993-1-2, 4.2.3.5 |
| 11 | **L 120x120x10 \| EN 10056-1:1998 - Horizontale verbanden** | | | | | | |
| | 119 | 0 | BC985 | 0.15 | ≤ 1 | FC601) | Berekening bij brand - Doorsnedecontrole - Trek volgens EN 1993-1-2, 4.2.3.1 |
| 12 | **Rechthoek 15/120 - Verticale verbanden** | | | | | | |
| | 172 | 2737 | BC986 | 0.11 | ≤ 1 | FC601) | Berekening bij brand - Doorsnedecontrole - Trek volgens EN 1993-1-2, 4.2.3.1 |
| 13 | **HE A 180 \| Euronorm 53-62 - Kolom** | | | | | | |
| | 161 | 0 | BC986 | 0.36 | ≤ 1 | FS812) | Berekening bij brand - Stabiliteitsberekening - Knik om z-as volgens EN 1993-1-2, 4.2.3.2 |
| 14 | **HE A 200 \| Euronorm 53-62 - Dakligger** | | | | | | |
| | 86 | 3518 | BC965 | 0.22 | ≤ 1 | FS831) | Berekening bij brand - Stabiliteitsberekening - Kip volgens EN 1993-1-2, 4.2.3.3 |

**RF-STEEL EC3**
CA4
Brand 120min

## 1.1 ALGEMENE GEGEVENS

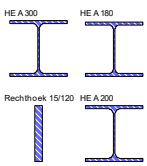
| | | |
|---|---|---|
| Te ontwerpen staven: | 87,88,99,102,167-173 | |
| Te ontwerpen staafverz.: | 8,19-21,31,32 | |
| Nationale bijlagen: | NEN | |
| Brandwerendheid ontwerp | | |
| Te berekenen belastingscombinaties: | BC959 | BG10 + BG20 + BG30 + BG40 |
| | BC960 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 |
| | BC961 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 |
| | BC962 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 |
| | BC963 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 |
| | BC964 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | BC965 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 |
| | BC966 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 |
| | BC967 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 |
| | BC968 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG150 |
| | BC969 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 |
| | BC970 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 |
| | BC971 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| BC972 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 |
| BC973 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 |
| BC974 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 |
| BC975 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 |
| BC976 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 |
| BC977 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 |
| BC978 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 |
| BC979 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| BC980 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 |
| BC981 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 |
| BC982 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 |
| BC983 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 |
| BC984 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 |
| BC985 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 |
| BC986 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| BC987 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 |
| BC988 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 |
| BC989 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 |
| BC990 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 |

## 1.2 MATERIALEN

| Matl. No. | Materiaal Omschrijving | E-Modulus E [N/mm²] | Glijdingsmodulu G [N/mm²] | Coï¿½ff. van Poisso ν [-] | Vloeispanning $f_{yk}$ [N/mm²] | Max. Dikte t [mm] |
|---|---|---|---|---|---|---|
| 1 | Staal S 235 \| NEN EN 1993-1-1:2007-11 | 210000.0 | 80769.2 | 0.300 | 235.0 | 40.0 |
| | | | | | 215.0 | 80.0 |
| | | | | | 215.0 | 100.0 |
| | | | | | 195.0 | 150.0 |
| | | | | | 185.0 | 200.0 |
| | | | | | 175.0 | 250.0 |
| | | | | | 165.0 | 400.0 |




## 1.3 DOORSNEDES

| Snede No. | Matl. No. | Doorsnede Omschrijving | Doorsnede Type | Max Ontwerp Unity check | Commentaar |
|---|---|---|---|---|---|
| 2 | 1 | HE A 300 \| Euronorm 53-62 | Gewalst I-profiel | 0.65 | Hoofddraag kolom |
| 7 | 1 | HE A 300 \| Euronorm 53-62 | Gewalst I-profiel | 0.68 | Tussenkolom |
| 8 | 1 | HE A 180 \| Euronorm 53-62 | Gewalst I-profiel | 0.69 | Tussenliggers |
| 12 | 1 | Rechthoek 15/120 | Platte staaf | 0.45 | Verticale verbanden |
| 13 | 1 | HE A 180 \| Euronorm 53-62 | Gewalst I-profiel | 0.59 | Kolom |
| 14 | 1 | HE A 200 \| Euronorm 53-62 | Gewalst I-profiel | 0.50 | Dakligger |

## 1.5 KNIKLENGTES - STAVEN

| Staaf No. | Knik Mogelijk | Knik om y-as Mogelijk | $k_{cr,y}$ | $L_{cr,y}$ [mm] | Knik om z-as Mogelijk | $k_{cr,z}$ | $L_{cr,z}$ [mm] | Kip Mogelijk | $k_z$ | $k_w$ | $L_w$ [mm] | $L_T$ [mm] |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 87 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 88 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 99 | ☒ | ☒ | 1.00 | 4500 | ☒ | 1.00 | 4500 | ☒ | 1.0 | 1.0 | 4500 | 4500 |
| 102 | ☒ | ☒ | 1.00 | 4300 | ☒ | 1.00 | 4300 | ☒ | 1.0 | 1.0 | 4300 | 4300 |
| 167 | ☐ | ☐ | 1.00 | 7411 | ☐ | 1.00 | 7411 | ☐ | 1.0 | 1.0 | 7411 | 7411 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 168 | ☐ | ☐ | 1.00 | 7529 | ☐ | 1.00 | 7529 | ☐ | 1.0 | 1.0 | 7529 | 7529 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 169 | ☒ | ☒ | 1.00 | 1665 | ☒ | 1.00 | 1665 | ☒ | 1.0 | 1.0 | 1665 | 1665 |
| 170 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 171 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 172 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 173 | ☐ | ☐ | 1.00 | 2737 | ☐ | 1.00 | 2737 | ☐ | 1.0 | 1.0 | 2737 | 2737 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |

## 1.6 KNIKLENGTES - STAAFVERZAMELINGEN

| Staafver No. | Knik Mogelijk | Knik om y-as Mogelijk | $k_{cr,y}$ | $L_{cr,y}$ [mm] | Knik om z-as Mogelijk | $k_{cr,z}$ | $L_{cr,z}$ [mm] | Kip Mogelijk | $k_z$ | $k_w$ | $L_w$ [mm] | $L_T$ [mm] |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 8 | ☒ | ☒ | 1.00 | 7850 | ☒ | 1.00 | 7850 | ☒ | 1.0 | 1.0 | 7850 | 7850 |
| 19 | ☒ | ☒ | 1.00 | 8093 | ☒ | 1.00 | 8093 | ☒ | 1.0 | 1.0 | 8093 | 8093 |
| 20 | ☒ | ☒ | 1.00 | 8093 | ☒ | 1.00 | 8093 | ☒ | 1.0 | 1.0 | 8093 | 8093 |
| 21 | ☒ | ☒ | 1.00 | 8093 | ☒ | 1.00 | 8093 | ☒ | 1.0 | 1.0 | 8093 | 8093 |
| 31 | ☒ | ☒ | 1.00 | 6530 | ☒ | 1.00 | 6530 | ☒ | 1.0 | 1.0 | 6530 | 6530 |
| 32 | ☒ | ☒ | 1.00 | 4345 | ☒ | 1.00 | 4345 | ☒ | 1.0 | 1.0 | 4345 | 4345 |

## 1.9 BRUIKBAARHEIDSGEGEVENS

| No. | Verwijzing naar | Staven/VerzamelingNo. | Referentielengte Handmatig | Referentielengte l [mm] | Richt. | Toog $e_0$ [mm] | Staaftype |
|---|---|---|---|---|---|---|---|
| 1 | Staaflijst | 1 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 2 | Staaflijst | 2 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 3 | Staaflijst | 3 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 4 | Staaflijst | 4 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 5 | Staaflijst | 5 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 6 | Staaflijst | 6 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 7 | Staaflijst | 7 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 8 | Staaflijst | 8 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 9 | Staaflijst | 9 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 10 | Staaflijst | 10 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 11 | Staaflijst | 11 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 12 | Staaflijst | 12 | ☐ | 7850 | y, z | 0.0 | Ligger |
| 13 | Staaflijst | 13 | ☐ | 19447 | y, z | 0.0 | Ligger |
| 14 | Staaflijst | 14 | ☐ | 12912 | y, z | 0.0 | Ligger |
| 15 | Staaflijst | 15 | ☐ | 12912 | y, z | 0.0 | Ligger |
| 16 | Staaflijst | 16 | ☐ | 7970 | y, z | 0.0 | Ligger |
| 17 | Staaflijst | 17 | ☐ | 8093 | y, z | 0.0 | Ligger |
| 18 | Staaflijst | 18 | ☐ | 7970 | y, z | 0.0 | Ligger |
| 19 | Staaflijst | 19 | ☐ | 8093 | y, z | 0.0 | Ligger |
| 20 | Staaflijst | 20 | ☐ | 8093 | y, z | 0.0 | Ligger |
| 21 | Staaflijst | 21 | ☐ | 8093 | y, z | 0.0 | Ligger |
| 22 | Staaflijst | 24 | ☐ | 19447 | y, z | 0.0 | Ligger |
| 23 | Staaflijst | 25 | ☐ | 6530 | y, z | 0.0 | Ligger |
| 24 | Staaflijst | 28 | ☐ | 4345 | y, z | 0.0 | Ligger |
| 25 | Staaflijst | 29 | ☐ | 4345 | y, z | 0.0 | Ligger |
| 26 | Staaflijst | 30 | ☐ | 6510 | y, z | 0.0 | Ligger |
| 27 | Staaflijst | 31 | ☐ | 6530 | y, z | 0.0 | Ligger |
| 28 | Staaflijst | 32 | ☐ | 4345 | y, z | 0.0 | Ligger |
| 29 | Staaflijst | 33 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 30 | Staaflijst | 34 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 31 | Staaflijst | 35 | ☐ | 6535 | y, z | 0.0 | Ligger |
| 32 | Staaflijst | 36 | ☐ | 6511 | y, z | 0.0 | Ligger |
| 33 | Staaflijst | 37 | ☐ | 6401 | y, z | 0.0 | Ligger |
| 34 | Staaflijst | 38 | ☐ | 6535 | y, z | 0.0 | Ligger |
| 35 | Staaflijst | 39 | ☐ | 6511 | y, z | 0.0 | Ligger |
| 36 | Staaflijst | 40 | ☐ | 6401 | y, z | 0.0 | Ligger |
| 37 | Staaflijst | 41 | ☐ | 6535 | y, z | 0.0 | Ligger |
| 38 | Staaflijst | 42 | ☐ | 6535 | y, z | 0.0 | Ligger |
| 39 | Staaflijst | 43 | ☐ | 6535 | y, z | 0.0 | Ligger |
| 40 | Staaflijst | 44 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 41 | Staaflijst | 45 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 42 | Staaflijst | 46 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 43 | Staaflijst | 47 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 44 | Staaflijst | 48 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 45 | Staaflijst | 49 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 46 | Staaflijst | 50 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 47 | Staaflijst | 51 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 48 | Staaflijst | 52 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 49 | Staaf | 47 | ☐ | 6400 | y, z | 0.0 | Ligger |
| 50 | Staaf | 48 | ☐ | 6510 | y, z | 0.0 | Ligger |
| 51 | Staaf | 49 | ☐ | 6530 | y, z | 0.0 | Ligger |
| 52 | Staaf | 50 | ☐ | 6400 | y, z | 0.0 | Ligger |
| 53 | Staaf | 53 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 54 | Staaf | 54 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 55 | Staaf | 55 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 56 | Staaf | 56 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 57 | Staaf | 57 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 58 | Staaf | 58 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 59 | Staaf | 59 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 60 | Staaf | 60 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 61 | Staaf | 61 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 62 | Staaf | 62 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 63 | Staaf | 63 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 64 | Staaf | 64 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 65 | Staaf | 65 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 66 | Staaf | 66 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 67 | Staaf | 67 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 68 | Staaf | 68 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 69 | Staaf | 69 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 70 | Staaf | 71 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 71 | Staaf | 72 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 72 | Staaf | 73 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 73 | Staaf | 75 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 74 | Staaf | 77 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 75 | Staaf | 79 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 76 | Staaf | 81 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 77 | Staaf | 82 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 78 | Staaf | 84 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 79 | Staaf | 87 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 80 | Staaf | 88 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 81 | Staaf | 89 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 82 | Staaf | 90 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 83 | Staaf | 91 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 84 | Staaf | 92 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 85 | Staaf | 93 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 86 | Staaf | 94 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 87 | Staaf | 95 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 88 | Staaf | 96 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 89 | Staaf | 97 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 90 | Staaf | 98 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 91 | Staaf | 99 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 92 | Staaf | 102 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 93 | Staaf | 112 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 94 | Staaf | 113 | ☐ | 3957 | y, z | 0.0 | Ligger |

## 1.9 BRUIKBAARHEIDSGEGEVENS

| No. | Verwijzing naar | Staven/VerzamelingNo. | Referentielengte Handmatig | l [mm] | Richt. | Toog $e_0$ [mm] | Staaftype |
|---|---|---|---|---|---|---|---|
| 95 | Staaf | 114 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 96 | Staaf | 115 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 97 | Staaf | 116 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 98 | Staaf | 117 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 99 | Staaf | 118 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 100 | Staaf | 119 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 101 | Staaf | 120 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 102 | Staaf | 121 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 103 | Staaf | 122 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 104 | Staaf | 123 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 105 | Staaf | 124 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 106 | Staaf | 125 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 107 | Staaf | 126 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 108 | Staaf | 127 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 109 | Staaf | 128 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 110 | Staaf | 129 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 111 | Staaf | 130 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 112 | Staaf | 131 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 113 | Staaf | 132 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 114 | Staaf | 133 | ☐ | 6255 | y, z | 0.0 | Ligger |
| 115 | Staaf | 134 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 116 | Staaf | 135 | ☐ | 5704 | y, z | 0.0 | Ligger |
| 117 | Staaf | 136 | ☐ | 7827 | y, z | 0.0 | Ligger |
| 118 | Staaf | 137 | ☐ | 7512 | y, z | 0.0 | Ligger |
| 119 | Staaf | 138 | ☐ | 7827 | y, z | 0.0 | Ligger |
| 120 | Staaf | 139 | ☐ | 7451 | y, z | 0.0 | Ligger |
| 121 | Staaf | 146 | ☐ | 7411 | y, z | 0.0 | Ligger |
| 122 | Staaf | 147 | ☐ | 7529 | y, z | 0.0 | Ligger |
| 123 | Staaf | 148 | ☐ | 1665 | y, z | 0.0 | Ligger |
| 124 | Staaf | 154 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 125 | Staaf | 155 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 126 | Staaf | 156 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 127 | Staaf | 157 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 128 | Staaf | 158 | ☐ | 7512 | y, z | 0.0 | Ligger |
| 129 | Staaf | 159 | ☐ | 7451 | y, z | 0.0 | Ligger |
| 130 | Staaf | 162 | ☐ | 1665 | y, z | 0.0 | Ligger |
| 131 | Staaf | 163 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 132 | Staaf | 164 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 133 | Staaf | 165 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 134 | Staaf | 166 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 135 | Staaf | 167 | ☐ | 7411 | y, z | 0.0 | Ligger |
| 136 | Staaf | 168 | ☐ | 7529 | y, z | 0.0 | Ligger |
| 137 | Staaf | 169 | ☐ | 1665 | y, z | 0.0 | Ligger |
| 138 | Staaf | 170 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 139 | Staaf | 171 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 140 | Staaf | 172 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 141 | Staaf | 173 | ☐ | 2737 | y, z | 0.0 | Ligger |
| 142 | Staaf | 202 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 143 | Staaf | 204 | ☐ | 4500 | y, z | 0.0 | Ligger |
| 144 | Staaf | 206 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 145 | Staaf | 212 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 146 | Staaf | 214 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 147 | Staaf | 216 | ☐ | 4300 | y, z | 0.0 | Ligger |
| 148 | Staaf | 217 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 149 | Staaf | 218 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 150 | Staaf | 220 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 151 | Staaf | 221 | ☐ | 3912 | y, z | 0.0 | Ligger |
| 152 | Staaf | 223 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 153 | Staaf | 224 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 154 | Staaf | 226 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 155 | Staaf | 227 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 156 | Staaf | 229 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 157 | Staaf | 230 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 158 | Staaf | 232 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 159 | Staaf | 233 | ☐ | 3957 | y, z | 0.0 | Ligger |
| 160 | Staaf | 235 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 161 | Staaf | 236 | ☐ | 3901 | y, z | 0.0 | Ligger |
| 162 | Staaf | 238 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 163 | Staaf | 239 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 164 | Staaf | 241 | ☐ | 3967 | y, z | 0.0 | Ligger |
| 165 | Staaf | 242 | ☐ | 3967 | y, z | 0.0 | Ligger |

## 1.10 BRANDWERENDHEID - STAVEN

| No. | Staaf No. | Ben. tijd $t_{fi,ben}$ [min] | Brand Blootstellin | Brand Beschermi | Beschermin Type | Volumieke m $\rho_p$ [kg/m³] | Thermische vo $\lambda_p$ [W/m*K] | Specifieke hitte $c_p$ [J/(kg*K)] | Dikte $d_p$ [mm] |
|---|---|---|---|---|---|---|---|---|---|
| 1 | 87 | 120 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 5.000 |
| 2 | 88 | 120 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 5.000 |
| 3 | 99 | 120 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 20.000 |
| 4 | 102 | 120 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 20.000 |
| 5 | 167 | 120 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 6 | 168 | 120 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 7 | 169 | 120 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 20.000 |
| 8 | 170 | 120 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 9 | 171 | 120 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 10 | 172 | 120 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |
| 11 | 173 | 120 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 10.000 |

## 1.11 BRANDWERENDHEID - STAAFVERZAMELINGEN

| No. | Staafverz. N | Ben. tijd $t_{fi,ben}$ [min] | Brand Blootstellin | Brand Beschermi | Beschermin Type | Volumieke m $\rho_p$ [kg/m³] | Thermische vo $\lambda_p$ [W/m*K] | Specifieke hitte $c_p$ [J/(kg*K)] | Dikte $d_p$ [mm] |
|---|---|---|---|---|---|---|---|---|---|
| 1 | 8 | 120 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 15.000 |
| 2 | 19 | 120 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 15.000 |
| 3 | 20 | 120 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 20.000 |
| 4 | 21 | 120 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 20.000 |
| 5 | 31 | 120 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 20.000 |
| 6 | 32 | 120 | Alle Zijdes | ☒ | Contour | 300.000 | 0.120 | 1200.000 | 15.000 |

## 2.2 BEREKENING PER DOORSNEDE

| Snede No. | Staaf No. | Positie x [mm] | BG/BC/ RC | Berekening | | vergelijki No. | Omschrijving |
|---|---|---|---|---|---|---|---|
| 2 | **HE A 300 \| Euronorm 53-62 - Hoofddraag kolom** | | | | | | |
| | 18 | 4345 | BC986 | 0.65 | ≤ 1 | FS854) | Berekening bij brand - Stabiliteitsberekening - Buiging en druk volgens EN 1993-1-2, 4.2.3.5 |
| 7 | **HE A 300 \| Euronorm 53-62 - Tussenkolom** | | | | | | |
| | 101 | 0 | BC986 | 0.68 | ≤ 1 | FS854) | Berekening bij brand - Stabiliteitsberekening - Buiging en druk volgens EN 1993-1-2, 4.2.3.5 |
| 8 | **HE A 180 \| Euronorm 53-62 - Tussenliggers** | | | | | | |
| | 78 | 0 | BC986 | 0.69 | ≤ 1 | FS831) | Berekening bij brand - Stabiliteitsberekening - Kip volgens EN 1993-1-2, 4.2.3.3 |
| 12 | **Rechthoek 15/120 - Verticale verbanden** | | | | | | |
| | 172 | 2737 | BC986 | 0.45 | ≤ 1 | FC601) | Berekening bij brand - Doorsnedecontrole - Trek volgens EN 1993-1-2, 4.2.3.1 |
| 13 | **HE A 180 \| Euronorm 53-62 - Kolom** | | | | | | |
| | 161 | 0 | BC986 | 0.59 | ≤ 1 | FS812) | Berekening bij brand - Stabiliteitsberekening - Knik om z-as volgens EN 1993-1-2, 4.2.3.2 |
| 14 | **HE A 200 \| Euronorm 53-62 - Dakligger** | | | | | | |
| | 87 | 2152 | BC959 | 0.50 | ≤ 1 | FS831) | Berekening bij brand - Stabiliteitsberekening - Kip volgens EN 1993-1-2, 4.2.3.3 |

# INHOUD

## 1.1 ALGEMENE GEGEVENS

| | | |
|---|---|---|
| Berekening volgens norm: | NEN EN 1992-1-1+C2:2011/NB:2016-11 | |
| UITERSTE GRENSTOESTAND | | |
| Te berekenen BC's: | BC1 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 |
| | | Blijvend en tijdelijk |
| | BC2 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 |
| | | Blijvend en tijdelijk |
| | BC3 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 |
| | | Blijvend en tijdelijk |
| | BC4 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 |
| | | Blijvend en tijdelijk |
| | BC5 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 |
| | | Blijvend en tijdelijk |
| | BC6 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC7 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC8 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 |
| | | Blijvend en tijdelijk |
| | BC9 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC10 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC11 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG130 |
| | | Blijvend en tijdelijk |
| | BC12 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 |
| | | Blijvend en tijdelijk |
| | BC13 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC14 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC15 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG140 |
| | | Blijvend en tijdelijk |
| | BC16 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC17 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC18 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 |
| | | Blijvend en tijdelijk |
| | BC19 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG130 |
| | | Blijvend en tijdelijk |
| | BC20 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 |
| | | Blijvend en tijdelijk |
| | BC21 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC22 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC23 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG140 |
| | | Blijvend en tijdelijk |
| | BC24 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC25 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC26 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG130 |
| | | Blijvend en tijdelijk |
| | BC27 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG130 + 1.65*BG140 |
| | | Blijvend en tijdelijk |
| | BC28 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC29 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG130 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC30 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG140 |
| | | Blijvend en tijdelijk |
| | BC31 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG140 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC32 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC33 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 |
| | | Blijvend en tijdelijk |
| | BC34 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| BC35 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 |
| BC36 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 |
| BC37 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 |
| BC38 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC39 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 |
| BC40 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 |
| BC41 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 |
| BC42 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 |
| BC43 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 |
| BC44 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 |
| BC45 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC46 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 |
| BC47 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 |
| BC48 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 |
| BC49 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 |
| BC50 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 |
| BC51 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 |
| BC52 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 |
| BC53 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC54 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 |
| BC55 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 |
| BC56 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 |
| BC57 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 |
| BC58 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 |
| BC59 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 |
| BC60 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC61 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 |
| BC62 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 |
| BC63 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 |
| BC64 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 |
| BC65 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 |
| BC66 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 |
| BC67 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 |
| BC68 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 |

## 1.1 ALGEMENE GEGEVENS

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|---|---|
| BC69 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC70 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 |
| BC71 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 |
| BC72 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 |
| BC73 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 |
| BC74 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 |
| BC75 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 |
| BC76 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC77 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 |
| BC78 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 |
| BC79 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 |
| BC80 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 |
| BC81 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 |
| BC82 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 |
| BC83 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 |
| BC84 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC85 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 |
| BC86 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 |
| BC87 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 |
| BC88 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 |
| BC89 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 |
| BC90 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 |
| BC91 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC92 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 |
| BC93 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 |
| BC94 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 |
| BC95 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 |
| BC96 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 |
| BC97 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 |
| BC98 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 |
| BC99 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 |
| BC100 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| BC101 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC102 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + |

## 1.1 ALGEMENE GEGEVENS

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|---|---|
| | + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC103 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC104 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC105 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC106 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 |
| | Blijvend en tijdelijk |
| BC107 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC108 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC109 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC110 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC111 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC112 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC113 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 |
| | Blijvend en tijdelijk |
| BC114 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 |
| | Blijvend en tijdelijk |
| BC115 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC116 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC117 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC118 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC119 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC120 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC121 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG130 |
| | Blijvend en tijdelijk |
| BC122 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC123 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC124 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC125 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC126 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC127 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC128 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC129 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC130 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC131 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC132 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC133 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC134 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |

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|---|---|
| BC135 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG300 |
| BC136 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC137 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG300 |
| BC138 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG300 |
| BC139 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| BC140 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC141 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| BC142 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG300 |
| BC143 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC144 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG300 |
| BC145 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG300 |
| BC146 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG300 |
| BC147 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| BC148 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC149 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| BC150 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG300 |
| BC151 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC152 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG300 |
| BC153 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG300 |
| BC154 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| BC155 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC156 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| BC157 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG300 |
| BC158 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC159 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG300 |
| BC160 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG401 |
| BC161 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG402 |
| BC162 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG403 |
| BC163 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG404 |
| BC164 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG401 |
| BC165 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG402 |
| BC166 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG403 |
| BC167 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG404 |
| BC168 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | + 1.65*BG110 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC169 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC170 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC171 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC172 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC173 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC174 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC175 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC176 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC177 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC178 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC179 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC180 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC181 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC182 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC183 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC184 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC185 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC186 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC187 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC188 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC189 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC190 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC191 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC192 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC193 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC194 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC195 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC196 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC197 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC198 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC199 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | + 1.65*BG110 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC200 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC201 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC202 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC203 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC204 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC205 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC206 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC207 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC208 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC209 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC210 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC211 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC212 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC213 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC214 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC215 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC216 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC217 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC218 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC219 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC220 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC221 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC222 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC223 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC224 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC225 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC226 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC227 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC228 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC229 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC230 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC231 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG404 |

## 1.1 ALGEMENE GEGEVENS

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|---|---|
| BC232 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG401 |
| BC233 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG402 |
| BC234 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG403 |
| BC235 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG404 |
| BC236 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| BC237 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| BC238 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| BC239 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| BC240 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC241 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC242 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC243 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC244 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| BC245 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| BC246 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| BC247 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| BC248 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG401 |
| BC249 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG402 |
| BC250 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG403 |
| BC251 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG404 |
| BC252 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC253 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC254 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC255 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC256 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG401 |
| BC257 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG402 |
| BC258 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG403 |
| BC259 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG404 |
| BC260 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG401 |
| BC261 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG402 |
| BC262 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG403 |
| BC263 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG404 |
| | Blijvend en tijdelijk |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| BC264 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC265 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC266 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC267 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC268 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC269 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC270 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC271 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC272 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC273 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC274 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC275 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC276 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC277 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC278 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC279 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC280 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC281 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC282 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC283 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC284 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC285 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC286 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC287 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC288 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 |
| | Blijvend en tijdelijk |
| BC289 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 |
| | Blijvend en tijdelijk |
| BC290 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 |
| | Blijvend en tijdelijk |
| BC291 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 |
| | Blijvend en tijdelijk |
| BC292 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC293 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC294 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC295 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC296 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | 1.65*BG110 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC297 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC298 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 |
| | Blijvend en tijdelijk |
| BC299 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC300 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC301 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC302 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC303 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC304 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC305 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 |
| | Blijvend en tijdelijk |
| BC306 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 |
| | Blijvend en tijdelijk |
| BC307 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC308 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC309 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC310 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC311 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC312 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC313 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG130 |
| | Blijvend en tijdelijk |
| BC314 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC315 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC316 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC317 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC318 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC319 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC320 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC321 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC322 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC323 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC324 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC325 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC326 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC327 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC328 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |

## 1.1 ALGEMENE GEGEVENS

| | | |
|---|---|---|
| BC329 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG300 |
| BC330 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG300 |
| BC331 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| BC332 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC333 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| BC334 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG300 |
| BC335 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC336 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG300 |
| BC337 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG300 |
| BC338 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG300 |
| BC339 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| BC340 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC341 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| BC342 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG300 |
| BC343 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC344 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG300 |
| BC345 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG300 |
| BC346 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| BC347 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC348 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| BC349 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG300 |
| BC350 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC351 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG300 |
| BC352 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG401 |
| BC353 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG402 |
| BC354 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG403 |
| BC355 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG404 |
| BC356 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG401 |
| BC357 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG402 |
| BC358 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG403 |
| BC359 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG404 |
| BC360 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG401 |
| BC361 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG402 |
| BC362 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | 1.65*BG110 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC363 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC364 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC365 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC366 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC367 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC368 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC369 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC370 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC371 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC372 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC373 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC374 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC375 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC376 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC377 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC378 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC379 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC380 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC381 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC382 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC383 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC384 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC385 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC386 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC387 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC388 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC389 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC390 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC391 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC392 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC393 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | 1.65*BG130 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC394 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC395 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC396 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC397 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC398 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC399 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC400 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC401 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC402 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC403 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC404 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC405 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC406 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC407 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC408 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC409 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC410 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC411 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC412 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC413 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC414 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC415 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC416 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC417 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC418 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC419 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC420 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC421 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC422 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC423 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC424 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC425 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG402 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| BC426 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG403 |
| BC427 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG404 |
| BC428 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| BC429 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| BC430 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| BC431 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| BC432 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC433 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC434 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC435 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC436 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| BC437 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| BC438 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| BC439 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| BC440 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG401 |
| BC441 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG402 |
| BC442 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG403 |
| BC443 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG404 |
| BC444 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC445 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC446 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC447 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC448 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG401 |
| BC449 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG402 |
| BC450 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG403 |
| BC451 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG404 |
| BC452 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG401 |
| BC453 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG402 |
| BC454 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG403 |
| BC455 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG404 |
| BC456 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| BC457 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |

## 1.1 ALGEMENE GEGEVENS

| | | |
|---|---|---|
| | BC458 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| | | Blijvend en tijdelijk |
| | BC459 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| | | Blijvend en tijdelijk |
| | BC460 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | | Blijvend en tijdelijk |
| | BC461 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | | Blijvend en tijdelijk |
| | BC462 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | | Blijvend en tijdelijk |
| | BC463 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | | Blijvend en tijdelijk |
| | BC464 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| | | Blijvend en tijdelijk |
| | BC465 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| | | Blijvend en tijdelijk |
| | BC466 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| | | Blijvend en tijdelijk |
| | BC467 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| | | Blijvend en tijdelijk |
| | BC468 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG401 |
| | | Blijvend en tijdelijk |
| | BC469 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG402 |
| | | Blijvend en tijdelijk |
| | BC470 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG403 |
| | | Blijvend en tijdelijk |
| | BC471 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG404 |
| | | Blijvend en tijdelijk |
| | BC472 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | | Blijvend en tijdelijk |
| | BC473 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | | Blijvend en tijdelijk |
| | BC474 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | | Blijvend en tijdelijk |
| | BC475 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | | Blijvend en tijdelijk |
| | BC476 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG401 |
| | | Blijvend en tijdelijk |
| | BC477 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG402 |
| | | Blijvend en tijdelijk |
| | BC478 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG403 |
| | | Blijvend en tijdelijk |
| | BC479 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG404 |
| | | Blijvend en tijdelijk |
| BRUIKBAARHEIDSGRENSTOESTAND | | |
| Te berekenen BC's: | BC480 | BG10 + BG20 + BG30 + BG40 |
| | | Karakteristiek met directe belasting, $k_t$ 0.600 |
| | BC481 | BG10 + BG20 + BG30 + BG40 + BG100 |
| | | Karakteristiek met directe belasting, $k_t$ 0.440 |
| | BC482 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 |
| | | Karakteristiek met directe belasting, $k_t$ 0.467 |
| | BC483 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 |
| | | Karakteristiek met directe belasting, $k_t$ 0.486 |
| | BC484 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 |
| | | Karakteristiek met directe belasting, $k_t$ 0.500 |
| | BC485 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 |
| | | Karakteristiek met directe belasting, $k_t$ 0.511 |
| | BC486 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 |
| | | Karakteristiek met directe belasting, $k_t$ 0.500 |
| | BC487 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 |
| | | Karakteristiek met directe belasting, $k_t$ 0.486 |
| | BC488 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 |
| | | Karakteristiek met directe belasting, $k_t$ 0.500 |
| | BC489 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 |
| | | Karakteristiek met directe belasting, $k_t$ 0.486 |
| | BC490 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 |
| | | Karakteristiek met directe belasting, $k_t$ 0.467 |
| | BC491 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 |
| | | Karakteristiek met directe belasting, $k_t$ 0.486 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| BC492 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC493 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC494 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC495 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC496 | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC497 | BG10 + BG20 + BG30 + BG40 + BG110 |
| | Karakteristiek met directe belasting, $k_t$ 0.440 |
| BC498 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC499 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC500 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC501 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC502 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC503 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC504 | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC505 | BG10 + BG20 + BG30 + BG40 + BG130 |
| | Karakteristiek met directe belasting, $k_t$ 0.440 |
| BC506 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC507 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC508 | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC509 | BG10 + BG20 + BG30 + BG40 + BG140 |
| | Karakteristiek met directe belasting, $k_t$ 0.440 |
| BC510 | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC511 | BG10 + BG20 + BG30 + BG40 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.440 |
| BC512 | BG10 + BG20 + BG30 + BG40 + BG120 |
| | Karakteristiek met directe belasting, $k_t$ 0.440 |
| BC513 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC514 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC515 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG130 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC516 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG130 + BG140 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC517 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG130 + BG140 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.520 |
| BC518 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG130 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC519 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG140 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC520 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG140 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC521 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC522 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG130 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC523 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG130 + BG140 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC524 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG130 + BG140 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC525 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG130 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC526 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG140 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC527 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG140 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC528 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC529 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC530 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG130 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC531 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG130 + BG140 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC532 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG130 + BG140 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC533 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG130 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC534 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG140 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC535 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG140 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC536 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC537 | BG10 + BG20 + BG30 + BG40 + BG120 + BG130 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC538 | BG10 + BG20 + BG30 + BG40 + BG120 + BG130 + BG140 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC539 | BG10 + BG20 + BG30 + BG40 + BG120 + BG130 + BG140 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC540 | BG10 + BG20 + BG30 + BG40 + BG120 + BG130 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC541 | BG10 + BG20 + BG30 + BG40 + BG120 + BG140 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC542 | BG10 + BG20 + BG30 + BG40 + BG120 + BG140 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC543 | BG10 + BG20 + BG30 + BG40 + BG120 + BG150 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC544 | BG10 + BG20 + BG30 + BG40 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.440 |
| BC545 | BG10 + BG20 + BG30 + BG40 + BG100 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC546 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC547 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC548 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC549 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.520 |
| BC550 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC551 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC552 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC553 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC554 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC555 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC556 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC557 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC558 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC559 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC560 | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC561 | BG10 + BG20 + BG30 + BG40 + BG110 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC562 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC563 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC564 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC565 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC566 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC567 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC568 | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 + BG300 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC569 | BG10 + BG20 + BG30 + BG40 + BG130 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC570 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC571 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC572 | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC573 | BG10 + BG20 + BG30 + BG40 + BG140 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC574 | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC575 | BG10 + BG20 + BG30 + BG40 + BG150 + BG300 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC576 | BG10 + BG20 + BG30 + BG40 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.440 |
| BC577 | BG10 + BG20 + BG30 + BG40 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.440 |
| BC578 | BG10 + BG20 + BG30 + BG40 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.440 |
| BC579 | BG10 + BG20 + BG30 + BG40 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.440 |
| BC580 | BG10 + BG20 + BG30 + BG40 + BG100 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC581 | BG10 + BG20 + BG30 + BG40 + BG100 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC582 | BG10 + BG20 + BG30 + BG40 + BG100 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC583 | BG10 + BG20 + BG30 + BG40 + BG100 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC584 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC585 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC586 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC587 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC588 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC589 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC590 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC591 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC592 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC593 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC594 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC595 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC596 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.520 |
| BC597 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.520 |
| BC598 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.520 |
| BC599 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.520 |
| BC600 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC601 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC602 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC603 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC604 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC605 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG402 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC606 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC607 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC608 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC609 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC610 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC611 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC612 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC613 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC614 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC615 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC616 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC617 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC618 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC619 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC620 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC621 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC622 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC623 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC624 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC625 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC626 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC627 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC628 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC629 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC630 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC631 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC632 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC633 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC634 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC635 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC636 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC637 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC638 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC639 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 + BG404 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC640 | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC641 | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC642 | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC643 | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC644 | BG10 + BG20 + BG30 + BG40 + BG110 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC645 | BG10 + BG20 + BG30 + BG40 + BG110 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC646 | BG10 + BG20 + BG30 + BG40 + BG110 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC647 | BG10 + BG20 + BG30 + BG40 + BG110 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC648 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC649 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC650 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC651 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC652 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC653 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC654 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC655 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC656 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC657 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC658 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC659 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.511 |
| BC660 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC661 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC662 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC663 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC664 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC665 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC666 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC667 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC668 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC669 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC670 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC671 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC672 | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC673 | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC674 | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC675 | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC676 | BG10 + BG20 + BG30 + BG40 + BG130 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC677 | BG10 + BG20 + BG30 + BG40 + BG130 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| BC678 | BG10 + BG20 + BG30 + BG40 + BG130 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC679 | BG10 + BG20 + BG30 + BG40 + BG130 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC680 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC681 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC682 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC683 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC684 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC685 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC686 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC687 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.500 |
| BC688 | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC689 | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC690 | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC691 | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC692 | BG10 + BG20 + BG30 + BG40 + BG140 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC693 | BG10 + BG20 + BG30 + BG40 + BG140 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC694 | BG10 + BG20 + BG30 + BG40 + BG140 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC695 | BG10 + BG20 + BG30 + BG40 + BG140 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC696 | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC697 | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC698 | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC699 | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.486 |
| BC700 | BG10 + BG20 + BG30 + BG40 + BG150 + BG401 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC701 | BG10 + BG20 + BG30 + BG40 + BG150 + BG402 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC702 | BG10 + BG20 + BG30 + BG40 + BG150 + BG403 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC703 | BG10 + BG20 + BG30 + BG40 + BG150 + BG404 |
| | Karakteristiek met directe belasting, $k_t$ 0.467 |
| BC704 | BG10 + BG20 + BG30 + BG40 |
| | Frequent, $k_t$ 0.400 |
| BC705 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 |
| | Frequent, $k_t$ 0.437 |
| BC706 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 |
| | Frequent, $k_t$ 0.462 |
| BC707 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 + 0.9*BG130 |
| | Frequent, $k_t$ 0.481 |
| BC708 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 + 0.9*BG130 + 0.9*BG140 |
| | Frequent, $k_t$ 0.495 |
| BC709 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 + 0.9*BG130 + 0.9*BG140 + 0.9*BG150 |
| | Frequent, $k_t$ 0.506 |
| BC710 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 + 0.9*BG130 + 0.9*BG150 |
| | Frequent, $k_t$ 0.495 |
| BC711 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 + 0.9*BG140 |
| | Frequent, $k_t$ 0.481 |
| BC712 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 + 0.9*BG140 + 0.9*BG150 |
| | Frequent, $k_t$ 0.495 |
| BC713 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 + 0.9*BG150 |
| | Frequent, $k_t$ 0.481 |
| BC714 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG130 |
| | Frequent, $k_t$ 0.462 |
| BC715 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG130 + 0.9*BG140 |
| | Frequent, $k_t$ 0.481 |
| BC716 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG130 + 0.9*BG140 + 0.9*BG150 |
| | Frequent, $k_t$ 0.495 |
| BC717 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG130 + 0.9*BG150 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | Frequent, $k_t$ 0.481 |
| BC718 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG140 |
| | Frequent, $k_t$ 0.462 |
| BC719 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG140 + 0.9*BG150 |
| | Frequent, $k_t$ 0.481 |
| BC720 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG150 |
| | Frequent, $k_t$ 0.462 |
| BC721 | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 |
| | Frequent, $k_t$ 0.437 |
| BC722 | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG130 |
| | Frequent, $k_t$ 0.462 |
| BC723 | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG130 + 0.9*BG140 |
| | Frequent, $k_t$ 0.481 |
| BC724 | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG130 + 0.9*BG140 + 0.9*BG150 |
| | Frequent, $k_t$ 0.495 |
| BC725 | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG130 + 0.9*BG150 |
| | Frequent, $k_t$ 0.481 |
| BC726 | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG140 |
| | Frequent, $k_t$ 0.462 |
| BC727 | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG140 + 0.9*BG150 |
| | Frequent, $k_t$ 0.481 |
| BC728 | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG150 |
| | Frequent, $k_t$ 0.462 |
| BC729 | BG10 + BG20 + BG30 + BG40 + 0.9*BG130 |
| | Frequent, $k_t$ 0.437 |
| BC730 | BG10 + BG20 + BG30 + BG40 + 0.9*BG130 + 0.9*BG140 |
| | Frequent, $k_t$ 0.462 |
| BC731 | BG10 + BG20 + BG30 + BG40 + 0.9*BG130 + 0.9*BG140 + 0.9*BG150 |
| | Frequent, $k_t$ 0.481 |
| BC732 | BG10 + BG20 + BG30 + BG40 + 0.9*BG130 + 0.9*BG150 |
| | Frequent, $k_t$ 0.462 |
| BC733 | BG10 + BG20 + BG30 + BG40 + 0.9*BG140 |
| | Frequent, $k_t$ 0.437 |
| BC734 | BG10 + BG20 + BG30 + BG40 + 0.9*BG140 + 0.9*BG150 |
| | Frequent, $k_t$ 0.462 |
| BC735 | BG10 + BG20 + BG30 + BG40 + 0.9*BG150 |
| | Frequent, $k_t$ 0.437 |
| BC736 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 |
| | Frequent, $k_t$ 0.433 |
| BC737 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 |
| | Frequent, $k_t$ 0.457 |
| BC738 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG130 |
| | Frequent, $k_t$ 0.475 |
| BC739 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG130 + 0.8*BG140 |
| | Frequent, $k_t$ 0.489 |
| BC740 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | Frequent, $k_t$ 0.500 |
| BC741 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG130 + 0.8*BG150 |
| | Frequent, $k_t$ 0.489 |
| BC742 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG140 |
| | Frequent, $k_t$ 0.475 |
| BC743 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG140 + 0.8*BG150 |
| | Frequent, $k_t$ 0.489 |
| BC744 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG150 |
| | Frequent, $k_t$ 0.475 |
| BC745 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG130 |
| | Frequent, $k_t$ 0.457 |
| BC746 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG130 + 0.8*BG140 |
| | Frequent, $k_t$ 0.475 |
| BC747 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | Frequent, $k_t$ 0.489 |
| BC748 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG130 + 0.8*BG150 |
| | Frequent, $k_t$ 0.475 |
| BC749 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG140 |
| | Frequent, $k_t$ 0.457 |
| BC750 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG140 + 0.8*BG150 |
| | Frequent, $k_t$ 0.475 |
| BC751 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG150 |
| | Frequent, $k_t$ 0.457 |
| BC752 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 |
| | Frequent, $k_t$ 0.433 |
| BC753 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0 |

## 1.1 ALGEMENE GEGEVENS

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|---|---|
| | 0.8*BG130 |
| | Frequent, $k_t$ 0.457 |
| BC754 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0.8*BG130 + 0.8*BG140 |
| | Frequent, $k_t$ 0.475 |
| BC755 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | Frequent, $k_t$ 0.489 |
| BC756 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0.8*BG130 + 0.8*BG150 |
| | Frequent, $k_t$ 0.475 |
| BC757 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0.8*BG140 |
| | Frequent, $k_t$ 0.457 |
| BC758 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0.8*BG140 + 0.8*BG150 |
| | Frequent, $k_t$ 0.475 |
| BC759 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0.8*BG150 |
| | Frequent, $k_t$ 0.457 |
| BC760 | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG130 |
| | Frequent, $k_t$ 0.433 |
| BC761 | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG130 + 0.8*BG140 |
| | Frequent, $k_t$ 0.457 |
| BC762 | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | Frequent, $k_t$ 0.475 |
| BC763 | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG130 + 0.8*BG150 |
| | Frequent, $k_t$ 0.457 |
| BC764 | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG140 |
| | Frequent, $k_t$ 0.433 |
| BC765 | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG140 + 0.8*BG150 |
| | Frequent, $k_t$ 0.457 |
| BC766 | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG150 |
| | Frequent, $k_t$ 0.433 |
| BC767 | BG10 + BG20 + BG30 + BG40 + 0.2*BG300 |
| | Frequent, $k_t$ 0.410 |
| BC768 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG300 |
| | Frequent, $k_t$ 0.440 |
| BC769 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.2*BG300 |
| | Frequent, $k_t$ 0.462 |
| BC770 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.2*BG300 |
| | Frequent, $k_t$ 0.479 |
| BC771 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG300 |
| | Frequent, $k_t$ 0.492 |
| BC772 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, $k_t$ 0.502 |
| BC773 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, $k_t$ 0.492 |
| BC774 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.2*BG300 |
| | Frequent, $k_t$ 0.479 |
| BC775 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, $k_t$ 0.492 |
| BC776 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, $k_t$ 0.479 |
| BC777 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.2*BG300 |
| | Frequent, $k_t$ 0.462 |
| BC778 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.2*BG300 |
| | Frequent, $k_t$ 0.479 |
| BC779 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, $k_t$ 0.492 |
| BC780 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, $k_t$ 0.479 |
| BC781 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.2*BG300 |
| | Frequent, $k_t$ 0.462 |
| BC782 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, $k_t$ 0.479 |
| BC783 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, $k_t$ 0.462 |
| BC784 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.2*BG300 |
| | Frequent, $k_t$ 0.440 |
| BC785 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.2*BG300 |
| | Frequent, $k_t$ 0.462 |
| BC786 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG300 |

## 1.1 ALGEMENE GEGEVENS

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|---|---|
| | Frequent, $k_t$ 0.479 |
| BC787 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, $k_t$ 0.492 |
| BC788 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, $k_t$ 0.479 |
| BC789 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.2*BG300 |
| | Frequent, $k_t$ 0.462 |
| BC790 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, $k_t$ 0.479 |
| BC791 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, $k_t$ 0.462 |
| BC792 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.2*BG300 |
| | Frequent, $k_t$ 0.440 |
| BC793 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.2*BG300 |
| | Frequent, $k_t$ 0.462 |
| BC794 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, $k_t$ 0.479 |
| BC795 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, $k_t$ 0.462 |
| BC796 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.2*BG300 |
| | Frequent, $k_t$ 0.440 |
| BC797 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, $k_t$ 0.462 |
| BC798 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, $k_t$ 0.440 |
| BC799 | BG10 + BG20 + BG30 + BG40 + 0.2*BG401 |
| | Frequent, $k_t$ 0.410 |
| BC800 | BG10 + BG20 + BG30 + BG40 + 0.2*BG402 |
| | Frequent, $k_t$ 0.410 |
| BC801 | BG10 + BG20 + BG30 + BG40 + 0.2*BG403 |
| | Frequent, $k_t$ 0.410 |
| BC802 | BG10 + BG20 + BG30 + BG40 + 0.2*BG404 |
| | Frequent, $k_t$ 0.410 |
| BC803 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG401 |
| | Frequent, $k_t$ 0.440 |
| BC804 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG402 |
| | Frequent, $k_t$ 0.440 |
| BC805 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG403 |
| | Frequent, $k_t$ 0.440 |
| BC806 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG404 |
| | Frequent, $k_t$ 0.440 |
| BC807 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.2*BG401 |
| | Frequent, $k_t$ 0.462 |
| BC808 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.2*BG402 |
| | Frequent, $k_t$ 0.462 |
| BC809 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.2*BG403 |
| | Frequent, $k_t$ 0.462 |
| BC810 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.2*BG404 |
| | Frequent, $k_t$ 0.462 |
| BC811 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.2*BG401 |
| | Frequent, $k_t$ 0.479 |
| BC812 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.2*BG402 |
| | Frequent, $k_t$ 0.479 |
| BC813 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.2*BG403 |
| | Frequent, $k_t$ 0.479 |
| BC814 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.2*BG404 |
| | Frequent, $k_t$ 0.479 |
| BC815 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG401 |
| | Frequent, $k_t$ 0.492 |
| BC816 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG402 |
| | Frequent, $k_t$ 0.492 |
| BC817 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG403 |
| | Frequent, $k_t$ 0.492 |
| BC818 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG404 |
| | Frequent, $k_t$ 0.492 |
| BC819 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, $k_t$ 0.502 |
| BC820 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, $k_t$ 0.502 |
| BC821 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 |

## 1.1 ALGEMENE GEGEVENS

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|---|---|
| | Frequent, $k_t$ 0.502 |
| BC822 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, $k_t$ 0.502 |
| BC823 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, $k_t$ 0.492 |
| BC824 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, $k_t$ 0.492 |
| BC825 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, $k_t$ 0.492 |
| BC826 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, $k_t$ 0.492 |
| BC827 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.2*BG401 |
| | Frequent, $k_t$ 0.479 |
| BC828 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.2*BG402 |
| | Frequent, $k_t$ 0.479 |
| BC829 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.2*BG403 |
| | Frequent, $k_t$ 0.479 |
| BC830 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.2*BG404 |
| | Frequent, $k_t$ 0.479 |
| BC831 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, $k_t$ 0.492 |
| BC832 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, $k_t$ 0.492 |
| BC833 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, $k_t$ 0.492 |
| BC834 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, $k_t$ 0.492 |
| BC835 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, $k_t$ 0.479 |
| BC836 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, $k_t$ 0.479 |
| BC837 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, $k_t$ 0.479 |
| BC838 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, $k_t$ 0.479 |
| BC839 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.2*BG401 |
| | Frequent, $k_t$ 0.462 |
| BC840 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.2*BG402 |
| | Frequent, $k_t$ 0.462 |
| BC841 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.2*BG403 |
| | Frequent, $k_t$ 0.462 |
| BC842 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.2*BG404 |
| | Frequent, $k_t$ 0.462 |
| BC843 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.2*BG401 |
| | Frequent, $k_t$ 0.479 |
| BC844 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.2*BG402 |
| | Frequent, $k_t$ 0.479 |
| BC845 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.2*BG403 |
| | Frequent, $k_t$ 0.479 |
| BC846 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.2*BG404 |
| | Frequent, $k_t$ 0.479 |
| BC847 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, $k_t$ 0.492 |
| BC848 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, $k_t$ 0.492 |
| BC849 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, $k_t$ 0.492 |
| BC850 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, $k_t$ 0.492 |
| BC851 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, $k_t$ 0.479 |
| BC852 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, $k_t$ 0.479 |

## 1.1 ALGEMENE GEGEVENS

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| BC853 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, $k_t$ 0.479 |
| BC854 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, $k_t$ 0.479 |
| BC855 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.2*BG401 |
| | Frequent, $k_t$ 0.462 |
| BC856 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.2*BG402 |
| | Frequent, $k_t$ 0.462 |
| BC857 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.2*BG403 |
| | Frequent, $k_t$ 0.462 |
| BC858 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.2*BG404 |
| | Frequent, $k_t$ 0.462 |
| BC859 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, $k_t$ 0.479 |
| BC860 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, $k_t$ 0.479 |
| BC861 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, $k_t$ 0.479 |
| BC862 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, $k_t$ 0.479 |
| BC863 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, $k_t$ 0.462 |
| BC864 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, $k_t$ 0.462 |
| BC865 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, $k_t$ 0.462 |
| BC866 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, $k_t$ 0.462 |
| BC867 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.2*BG401 |
| | Frequent, $k_t$ 0.440 |
| BC868 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.2*BG402 |
| | Frequent, $k_t$ 0.440 |
| BC869 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.2*BG403 |
| | Frequent, $k_t$ 0.440 |
| BC870 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.2*BG404 |
| | Frequent, $k_t$ 0.440 |
| BC871 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.2*BG401 |
| | Frequent, $k_t$ 0.462 |
| BC872 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.2*BG402 |
| | Frequent, $k_t$ 0.462 |
| BC873 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.2*BG403 |
| | Frequent, $k_t$ 0.462 |
| BC874 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.2*BG404 |
| | Frequent, $k_t$ 0.462 |
| BC875 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG401 |
| | Frequent, $k_t$ 0.479 |
| BC876 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG402 |
| | Frequent, $k_t$ 0.479 |
| BC877 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG403 |
| | Frequent, $k_t$ 0.479 |
| BC878 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG404 |
| | Frequent, $k_t$ 0.479 |
| BC879 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, $k_t$ 0.492 |
| BC880 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, $k_t$ 0.492 |
| BC881 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, $k_t$ 0.492 |
| BC882 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, $k_t$ 0.492 |
| BC883 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, $k_t$ 0.479 |
| BC884 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, $k_t$ 0.479 |
| BC885 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG403 |

## 1.1 ALGEMENE GEGEVENS

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|---|---|
| | Frequent, $k_t$ 0.479 |
| BC886 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, $k_t$ 0.479 |
| BC887 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.2*BG401 |
| | Frequent, $k_t$ 0.462 |
| BC888 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.2*BG402 |
| | Frequent, $k_t$ 0.462 |
| BC889 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.2*BG403 |
| | Frequent, $k_t$ 0.462 |
| BC890 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.2*BG404 |
| | Frequent, $k_t$ 0.462 |
| BC891 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, $k_t$ 0.479 |
| BC892 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, $k_t$ 0.479 |
| BC893 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, $k_t$ 0.479 |
| BC894 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, $k_t$ 0.479 |
| BC895 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, $k_t$ 0.462 |
| BC896 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, $k_t$ 0.462 |
| BC897 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, $k_t$ 0.462 |
| BC898 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, $k_t$ 0.462 |
| BC899 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.2*BG401 |
| | Frequent, $k_t$ 0.440 |
| BC900 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.2*BG402 |
| | Frequent, $k_t$ 0.440 |
| BC901 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.2*BG403 |
| | Frequent, $k_t$ 0.440 |
| BC902 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.2*BG404 |
| | Frequent, $k_t$ 0.440 |
| BC903 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.2*BG401 |
| | Frequent, $k_t$ 0.462 |
| BC904 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.2*BG402 |
| | Frequent, $k_t$ 0.462 |
| BC905 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.2*BG403 |
| | Frequent, $k_t$ 0.462 |
| BC906 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.2*BG404 |
| | Frequent, $k_t$ 0.462 |
| BC907 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, $k_t$ 0.479 |
| BC908 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, $k_t$ 0.479 |
| BC909 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, $k_t$ 0.479 |
| BC910 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, $k_t$ 0.479 |
| BC911 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, $k_t$ 0.462 |
| BC912 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, $k_t$ 0.462 |
| BC913 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, $k_t$ 0.462 |
| BC914 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, $k_t$ 0.462 |
| BC915 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.2*BG401 |
| | Frequent, $k_t$ 0.440 |
| BC916 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.2*BG402 |
| | Frequent, $k_t$ 0.440 |
| BC917 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.2*BG403 |
| | Frequent, $k_t$ 0.440 |
| BC918 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.2*BG404 |
| | Frequent, $k_t$ 0.440 |
| BC919 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 |

## 1.1 ALGEMENE GEGEVENS

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|---|---|
| | Frequent, $k_t$ 0.462 |
| BC920 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, $k_t$ 0.462 |
| BC921 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, $k_t$ 0.462 |
| BC922 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, $k_t$ 0.462 |
| BC923 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, $k_t$ 0.440 |
| BC924 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, $k_t$ 0.440 |
| BC925 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, $k_t$ 0.440 |
| BC926 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, $k_t$ 0.440 |
| BC927 | BG10 + BG20 + BG30 + BG40 |
| | Quasi-blijvend, $k_t$ 0.400 |
| BC928 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 |
| | Quasi-blijvend, $k_t$ 0.433 |
| BC929 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 |
| | Quasi-blijvend, $k_t$ 0.457 |
| BC930 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 |
| | Quasi-blijvend, $k_t$ 0.475 |
| BC931 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 |
| | Quasi-blijvend, $k_t$ 0.489 |
| BC932 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | Quasi-blijvend, $k_t$ 0.500 |
| BC933 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 |
| | Quasi-blijvend, $k_t$ 0.489 |
| BC934 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 |
| | Quasi-blijvend, $k_t$ 0.475 |
| BC935 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 |
| | Quasi-blijvend, $k_t$ 0.489 |
| BC936 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG150 |
| | Quasi-blijvend, $k_t$ 0.475 |
| BC937 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 |
| | Quasi-blijvend, $k_t$ 0.457 |
| BC938 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 |
| | Quasi-blijvend, $k_t$ 0.475 |
| BC939 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | Quasi-blijvend, $k_t$ 0.489 |
| BC940 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 |
| | Quasi-blijvend, $k_t$ 0.475 |
| BC941 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 |
| | Quasi-blijvend, $k_t$ 0.457 |
| BC942 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 |
| | Quasi-blijvend, $k_t$ 0.475 |
| BC943 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 |
| | Quasi-blijvend, $k_t$ 0.457 |
| BC944 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 |
| | Quasi-blijvend, $k_t$ 0.433 |
| BC945 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 |
| | Quasi-blijvend, $k_t$ 0.457 |
| BC946 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 |
| | Quasi-blijvend, $k_t$ 0.475 |
| BC947 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | Quasi-blijvend, $k_t$ 0.489 |
| BC948 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 |
| | Quasi-blijvend, $k_t$ 0.475 |
| BC949 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 |
| | Quasi-blijvend, $k_t$ 0.457 |
| BC950 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 |
| | Quasi-blijvend, $k_t$ 0.475 |
| BC951 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 |
| | Quasi-blijvend, $k_t$ 0.457 |
| BC952 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 |
| | Quasi-blijvend, $k_t$ 0.433 |
| BC953 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 |
| | Quasi-blijvend, $k_t$ 0.457 |
| BC954 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | Quasi-blijvend, $k_t$ 0.475 |
| BC955 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 |
| | Quasi-blijvend, $k_t$ 0.457 |
| BC956 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 |

## 1.1 ALGEMENE GEGEVENS

| | | |
|---|---|---|
| | | Quasi-blijvend, $k_t$ 0.433 |
| | BC957 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 |
| | | Quasi-blijvend, $k_t$ 0.457 |
| | BC958 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 |
| | | Quasi-blijvend, $k_t$ 0.433 |
| Definitie van aanwezige bijlegwapening | Automatische ordening volgens de specificaties in tabel 1.4 | |
| Controlemethode: | Berekeningsmethode: | |
| | Door het aannemen van identieke vervormingsverhouding van de langswapening | |
| Ontwerp van | | |
| Betonspanningsberekening | ☐ | |
| Scheurwijdte | ☒ | |
| Lay out van de langswapening | | |
| Benodigde langswapening is automatisch verhoogd voor ontwerp bruikbaarheidsgrenstoestand: | ☒ | |
| DETAILS | | |
| Berekeningsmethode voor wapeningsomhullende | Gemengd | |
| Pas de snedekrachten toe zonder ribcomponenten | ☐ | |
| Ontwerpsituatie instellingen voor bruikbaarheidsgrenstoestandcontrole | | |
| Belastingscombinatie: | | |
| Karakteristiek met directe belasting | Controles: $k_1*f_{ck}$, $k_3*f_{yk}$ | |
| Karakteristiek met opgelegde vervorming | Controles: $k_1*f_{ck}$, $k_4*f_{yk}$ | |
| Frequent | Controles: $w_k$ | |
| Quasi-blijvend | Controles: $k_2*f_{ck}$, $w_k$, $u_l$ | |

## 1.1.1 NATIONALE BIJLAGE PARAMETERS

| | | | |
|---|---|---|---|
| 2 Basis ontwerp | | | |
| 2.4.2.4 Partiï¿½le veiligheidsfactoren voor materialen | | | |
| Partiï¿½le factor voor beton in de uiterste grenstoestand (blijvend, tijdelijk) | $\gamma_c$ | 1.500 | - |
| Partiï¿½le factor voor staal in de uiterste grenstoestand (blijvend, tijdelijk) | $\gamma_s$ | 1.150 | - |
| Partiï¿½le factor voor beton in de uiterste grenstoestand (buitengewoon) | $\gamma_c$ | 1.200 | - |
| Partiï¿½le factor voor staal in de uiterste grenstoestand (buitengewoon) | $\gamma_s$ | 1.000 | - |
| Partiï¿½le factor voor beton in de bruikbaarheidsgrenstoestand | $\gamma_c$ | 1.000 | - |
| Partiï¿½le factor voor staal in de bruikbaarheidsgrenstoestand | $\gamma_s$ | 1.000 | - |
| 3. Materialen | | | |
| 3.1 Beton | | | |
| Max. waarde van sterkteklasse van beton | $C_{max}$ | C90/105 | |
| Factor voor beschouwing langetermijn acties op druksterkte | $\alpha_{cc}$ | 1.000 | - |
| Factor voor beschouwing langetermijn acties op treksterkte | $\alpha_{ct}$ | 1.000 | - |
| 3.2 Wapeningsstaal | | | |
| Max. waarde van vloeigrens | $f_{yk}$ | 600.00 | N/mm^2 |
| Factor voor berekening van de rekenwaarde voor rekgrens van staal | $k_{ud1}$ | 0.900 | - |
| 4. Duurzaamheid en betondekking | | | |
| 4.4.1 Min. betondekking | | | |
| Constructie-klasse | C.K. | S4 | |
| Aanpassing van de constructie-klasse | | | |
| Min. betondekking | | | |
| Extra veiligheid element voor verhogen van min. betondekking | $\Delta c_{dur,\gamma}$ | 0.000 | m |
| Reductie van de betondekking bij gebruik van roestvast staal | $\Delta c_{dur,st}$ | 0.000 | m |
| Reductiefactor voor de beton met extra bescherming | $\Delta c_{dur,add}$ | 0.000 | m |
| Verhoging van de deklaag onder slijtagebelasting | | | |
| Verhogingswaarde voor slijtageklasse XM1 | $k_1$ | 0.000 | m |
| Verhogingswaarde voor slijtageklasse XM2 | $k_2$ | 0.000 | m |
| Verhogingswaarde voor slijtageklasse XM3 | $k_3$ | 0.000 | m |
| Toelage in berekening voor afwijking | $\Delta c_{dev}$ | 0.005 | m |
| Verhogingswaarde voor betonnering van oneffen vlakken | | | |
| Verhogingswaarde voor grondverbetering | | | |
| Verhogingswaarde voor beton direct op de grond | | | |
| 6. Uiterste grenstoestand (UGT) | | | |
| 6.2.2. Staven zonder ontwerp afschuifwapening | | | |
| Factor $k_0$ voor berekening van de rekenwaarde voor afschuifweerstand | $k_0$ | 0.180 | - |
| Factor $k_1$ voor berekening van de rekenwaarde voor afschuifweerstand | $k_1$ | 0.150 | - |
| Factor $k_2$ voor berekening van de rekenwaarde voor afschuifweerstand | $k_2$ | 0.035 | - |
| 6.2.3 Staven met ontwerp afschuifwapening | | | |
| Min. hoek van drukschoor | $\Theta_{min}$ | 21.801 | ï¿½ |
| Max. hoek van drukschoor | $\Theta_{max}$ | 45.000 | ï¿½ |
| Reductiefactor voor beton gescheurd door afschuiving | | | |
| Reductiefactor $k_1$ voor beton gescheurd door afschuiving | $k_1$ | 0.600 | - |
| Reductiefactor $k_2$ voor beton gescheurd door afschuiving | $k_2$ | 250.000 | - |
| Factor voor beschouwing spanningvoorwaarde in drukregel | $\alpha_{cw}$ | 1.000 | - |
| 7. Bruikbaarheidsgrenstoestand (BGT) | | | |
| 7.2 Spanningsbegrenzing | | | |
| Factor $k_1$ voor beperking van drukspanning in beton | $k_1$ | 0.600 | - |
| Factor $k_2$ voor beperking van drukspanning in beton | $k_2$ | 0.450 | - |
| 7.3 Scheurwijdtecontrole | | | |
| Begrenzing berekende scheurwijdte van gewapend beton en voorgespannen beton met VZA-spankabels | | | |
| Max. grootte van scheurwijdte voor milieuklassen X0, XC1 | $w_{max}$ | 0.400 | mm |
| Max. grootte van scheurwijdte voor milieuklasse XD1-3, XS1-3 | $w_{max}$ | 0.200 | mm |
| Factor $k_3$ voor de berekening van de max. h.o.h.-afstand scheuren | $k_3$ | 3.400 | - |
| Factor $k_4$ voor berekening van de max. h.o.h.-afstand scheuren | $k_4$ | 0.425 | - |
| 8. Detaillering van wapening en voorgespannen spanelementen - Algemeen | | | |
| 8.8 Aanvullende richtlijnen voor grote staafdiameters | | | |
| Staafdiameter | $\varnothing_{groot}$ | 32 | mm |
| 9. Detailleren van staven en bijzondere bepalingen | | | |
| 9.6 Wanden | | | |
| 9.6.2 Verticale wapening | | | |

## 1.1.1 NATIONALE BIJLAGE PARAMETERS

| | | | |
|---|---|---|---|
| Min. gebied van verticale wapening $A_{s,vmin}$ | $k_1$ | 0.000 | - |
| Max. gebied van verticale wapening $A_{s,vmax}$ | $k_2$ | 0.040 | - |
| 9.6.3 Horizontale wapening | | | |
| Min. gebied van horizontale wapening $A_{s,hmin}$ d.m.v. $k_3$ | $k_3$ | 0.000 | - |
| Min. gebied van horizontale wapening $A_{s,hmin}$ d.m.v. $k_4$ | $k_4$ | 0.000 | - |
| 11. Lichtgewicht toeslag betonconstructies | | | |
| 11.3 Materialen | | | |
| Factor voor beschouwing langetermijn acties op druksterkte | $\alpha_{lcc}$ | 0.850 | - |
| Factor voor beschouwing langetermijn acties op treksterkte | $\alpha_{lct}$ | 0.850 | - |
| 11.6 Uiterste grenstoestand berekening (UGT) | | | |
| 11.6.1 Staven zonder ontwerp afschuifwapening | | | |
| Factor $k_0$ voor berekening van de rekenwaarde voor afschuifweerstand | $k_0$ | 0.150 | - |
| Factor $k_1$ voor berekening van de rekenwaarde voor afschuifweerstand | $k_1$ | 0.150 | - |
| Factor $k_2$ voor berekening van de rekenwaarde voor afschuifweerstand | $k_2$ | 0.028 | - |
| 11.6.2 Constructie-element met ontwerp afschuifwapening | | | |
| Reductiefactor $k_1$ voor beton gescheurd door afschuiving | $k_1$ | 0.500 | - |
| Reductiefactor $k_2$ voor beton gescheurd door afschuiving | $k_2$ | 250.000 | - |

## 1.2 MATERIALEN

| Mater. No. | Materiaal omschrijving | | Opm. |
|---|---|---|---|
| | Betonsterkteklasse | Staalomschrijving | |
| 2 | Beton C30/37 | B 500 S (A) | |

## 1.2.1 MATERIAAL PARAMETERS

| Mater. No. | Omschrijving | Naam | Grootte | Eenheid |
|---|---|---|---|---|
| **2** | **Betonsterkteklasse: Beton C30/37** | | | |
| | Karakteristieke cilinderdruksterkte | $f_{ck}$ | 30.00 | N/mm^2 |
| | 5 % Kwantiel van de zuivere treksterkte | $f_{ctk,0.05}$ | 2.00 | N/mm^2 |
| | Karakteristiek voor niet-lineaire berekening | | | |
| | Gem. secans elasticiteitsmodulus | $E_{cm}$ | 33000.00 | N/mm^2 |
| | Gem. cilinderdruksterkte | $f_{cm}$ | 38.00 | N/mm^2 |
| | Gem. zuivere treksterkte | $f_{ctm}$ | 2.90 | N/mm^2 |
| | Uiterste rek bij zuivere druk | $\varepsilon_{c1}$ | -2.200 | ï¿½ |
| | Uiterste rek bij bezwijken | $\varepsilon_{c1u}$ | -3.500 | ï¿½ |
| | Glijdingsmodulus | G | 13750.00 | N/mm^2 |
| | Coï¿½ff. van Poisson | $\nu$ | 0.200 | - |
| | Karakteristieke rekken voor parabolisch-rechthoekig verloop | | | |
| | Uiterste rek bij zuivere druk | $\varepsilon_{c2}$ | -2.000 | ï¿½ |
| | Uiterste rek bij bezwijken | $\varepsilon_{cu2}$ | -3.500 | ï¿½ |
| | Parabool exponent | n | 2.000 | - |
| | Volumiek gewicht | $\gamma$ | 25.00 | kN/m^3 |
| | **Wapeningsstaal: B 500 S (A)** | | | |
| | Elasticiteitsmodulus | $E_s$ | 200000.00 | N/mm^2 |
| | Gem. waarde van de vloeispanning | $f_{ym}$ | 550.00 | N/mm^2 |
| | Karakteristieke vloeispanning | $f_{yk}$ | 500.00 | N/mm^2 |
| | Gem. waarde van de treksterkte | $f_{tm}$ | 551.25 | N/mm^2 |
| | Karakteristieke treksterkte | $f_{tk}$ | 525.00 | N/mm^2 |
| | Rekgrens | $\varepsilon_{uk}$ | 25.000 | ï¿½ |

## 1.3 VLAKKEN

| Vlak No. | Mat. No. | $f_{ct,eff,wk}$ [N/mm²] | $f_{ct,eff,As,min}$ [N/mm²] | $w_{k,+z\ (bov)}$ [mm] / $w_{k,-z\ (ond)}$ [mm] | Gevolgen t.g.v. verhindering Pas Toe | $k_c$ [-] | Opmerkingen |
|---|---|---|---|---|---|---|---|
| 1 | Dikte Type: constant, Dikte: 200 mm | | | | | | |
| | 2 | 2.90 | 2.90 | 0.150<br>0.150 | ☒ | var. | 6) |

Opmerkingen:
6) Berekening van min. wapening voor effecten t.g.v. verhindering

## 1.4 WAPENINGSGROEPNO. 1

| | |
|---|---|
| Toegepast op vlakken: | Alle |
| | |
| WAPENINGSVERHOUDING | |
| Min. verdeelwapening | 20.0 % |
| Min. basiswapening | 0.0 % |
| Min. drukwapening | 0.0 % |
| Min. trekwapening | 0.0 % |
| Max. wapeningpercentage | 4.0 % |
| Min. afschuifwapeningpercentage | 0.0 % |
| | |
| WAPENINGSGEBIED VOOR BGT-ONTWERP | |
| Gebruik toegepaste basis wapening en benodigde bijlegwapening volgens tabellen 2.1, 2.2, 2.3 | |
| | |
| Betondekking volgens norm | ☐ |
| | |
| BASISWAPENINGLAYOUT - BOVEN (-z) | |
| Aantal wapeningsrichtingen | 2 |
| Dekking tot hart van de wapening | d-1: 40, d-2: 52 mm |
| Staaldiameter | ds-1: 12, ds-2: 12 mm |
| Wapeningsrichtingen | Phi-1: 0.000°, Phi-2: 90.000° |
| Wapeningsgebied | As-1,-z (bov): 1508.000, As-2,-z (bov): 1508.000 mm²/m |

## 1.4 WAPENINGSGROEPNO. 1

| | |
|---|---|
| BASISWAPENINGLAYOUT - ONDER (+z) | |
| Aantal wapeningsrichtingen | 2 |
| Dekking tot hart van de wapening | d-1: 40, d-2: 52 mm |
| Staaldiameter | ds-1: 12, ds-2: 12 mm |
| Wapeningsrichtingen | Phi-1: 0.000°, Phi-2: 90.000° |
| Wapeningsgebied | As-1,+z (ond): 1508.000, As-2,+z (ond): 1508.000 mm²/m |
| | |
| LAYOUT BIJLEGWAPENING - BOVEN (-z) | |
| Aantal wapeningsrichtingen | 2 |
| Dekking tot hart van de wapening | d-1: 40, d-2: 50 mm |
| Staaldiameter | ds-1: 10, ds-2: 10 mm |
| Wapeningsrichtingen | Phi-1: 0.000°, Phi-2: 90.000° |
| Wapeningsgebied | Gebruik benodigde bijlegwapeninghoeveelheid volgens tabellen 2.1, 2.2, 2.3 |
| | |
| LAYOUT BIJLEGWAPENING - ONDER (+z) | |
| Aantal wapeningsrichtingen | 2 |
| Dekking tot hart van de wapening | d-1: 40, d-2: 50 mm |
| Staaldiameter | ds-1: 10, ds-2: 10 mm |
| Wapeningsrichtingen | Phi-1: 0.000°, Phi-2: 90.000° |
| Wapeningsgebied | Gebruik benodigde bijlegwapeninghoeveelheid volgens tabellen 2.1, 2.2, 2.3 |
| | |
| LANGSWAPENING VOOR AFSCHUIFKRACHTCONTROLE | |
| Gebruik benodigde hoeveelheid langswapening | |
| | |
| INSTELLINGEN VOOR NEN EN 1992-1-1+C2:2011/NB:2016-11 | |
| Min. langswapening voor platen volgens 9.3.1 | ☒ |
| Richting van min. wapening | |
| Wapeningsrichting met de hoofd trekkracht van de boven (-z) en onder (z+) vlakken, gezamenlijk: | ☒ |
| Min. langswapening voor wanden volgens hoofdstuk 9.6 | ☐ |
| Min. afschuifwapening | ☐ |
| Neutrale lijn hoogte grens | ☒ |
| Variabele betondrukdiagonaal - min | 21.801 ° |
| Variabele hellingshoek van de betonnen schoor - max | 45.000 ° |
| Partiï¿½le veiligheidsfactor $\gamma_s$ | BT 1.15, BU 1.00, BGT 1.00 |
| Partiï¿½le veiligheidsfactor $\gamma_c$ | BT 1.50, BU 1.20, BGT 1.00 |
| Beschouwing van langetermijneffecten Alpha-cc | BT 1.00, BU 1.00, BGT 1.00 |
| Beschouwing van langetermijn effecten Alpha-ct | BGT 1.00 |

## 2.1 BENODIGDE TOTALE WAPENING

| Vlak | Punt | Puntcoï¿½rdinaten [m] | | | | Benodigde Wapening | | | Basis | Bijlegwapening | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| No. | No. | X | Y | Z | Symbool | UGT | BGT | UGT/BGT | Wap. | Benodigd | Toegepast | Eenheid | Opmerkin |
| 1 | G1801 | 0.000 | 0.000 | 0.000 | $a_{s,1,-z\ (bov)}$ | 1073.286 | 2036.082 | 2036.082 | 1508.000 | 528.082 | 528.082 | mm²/m | |
| 1 | G1801 | 0.000 | 0.000 | 0.000 | $a_{s,2,-z\ (bov)}$ | 1041.064 | 2187.146 | 2187.146 | 1508.000 | 679.147 | 679.147 | mm²/m | |
| 1 | G1804 | 1.500 | 0.000 | 0.000 | $a_{s,1,+z\ (ond)}$ | 403.600 | 1361.643 | 1361.643 | 1508.000 | 0.000 | 0.000 | mm²/m | |
| 1 | G1384 | 11.500 | 5.500 | 0.000 | $a_{s,2,+z\ (ond)}$ | 97.475 | 1510.781 | 1510.781 | 1508.000 | 2.781 | 2.781 | mm²/m | |
| 1 | G387 | 13.000 | 18.000 | 0.000 | $a_{sw}$ | 1248.779 | - | 1248.779 | - | - | - | mm²/m² | |

## 3.1 BRUIKBAARHEID TOTAAL

| Vlak | Punt | Puntcoï¿½rdinaten [m] | | | BG | Controle | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| No. | No. | X | Y | Z | geval | type | Aanw. waarde | Grenswaarde | Eenheid | Unity check | Opmerkinge |
| 1 | G1280 | 19.500 | 7.000 | 0.000 | Omhullende F | $a_{s,min}$ | 1508.053 | 1508.052 | mm²/m | 1.0 | |
| 1 | G1801 | 0.000 | 0.000 | 0.000 | Omhullende F | $w_k$ | 0.146 | 0.150 | mm | 1.0 | |

**RF-CONCRETE Members**
BG1
Ontwerp van betonnen staven

Project: 23920-21 Model: 23920-21_5000_00 Datum: 05/10/2022

## 1.1 ALGEMENE GEGEVENS

| | | |
|---|---|---|
| Ontwerp volgens norm: | NEN EN 1992-1-1+C2:2011/NB:2016-11 | |
| UITERSTE GRENSTOESTAND | | |
| Te ontwerpen belastingscombinaties: | BC1 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 |
| | | Blijvend en tijdelijk |
| | BC2 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 |
| | | Blijvend en tijdelijk |
| | BC3 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 |
| | | Blijvend en tijdelijk |
| | BC4 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 |
| | | Blijvend en tijdelijk |
| | BC5 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 |
| | | Blijvend en tijdelijk |
| | BC6 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC7 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC8 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 |
| | | Blijvend en tijdelijk |
| | BC9 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC10 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC11 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG130 |
| | | Blijvend en tijdelijk |
| | BC12 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 |
| | | Blijvend en tijdelijk |
| | BC13 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC14 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC15 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG140 |
| | | Blijvend en tijdelijk |
| | BC16 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC17 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC18 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 |
| | | Blijvend en tijdelijk |
| | BC19 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG130 |
| | | Blijvend en tijdelijk |
| | BC20 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 |
| | | Blijvend en tijdelijk |
| | BC21 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC22 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC23 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG140 |
| | | Blijvend en tijdelijk |
| | BC24 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC25 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG110 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC26 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG130 |
| | | Blijvend en tijdelijk |
| | BC27 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG130 + 1.65*BG140 |
| | | Blijvend en tijdelijk |
| | BC28 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC29 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG130 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC30 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG140 |
| | | Blijvend en tijdelijk |
| | BC31 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG140 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC32 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC33 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 |
| | | Blijvend en tijdelijk |
| | BC34 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 |

## 1.1 ALGEMENE GEGEVENS

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|---|---|
| BC35 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 |
| BC36 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 |
| BC37 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 |
| BC38 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC39 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 |
| BC40 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 |
| BC41 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 |
| BC42 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 |
| BC43 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 |
| BC44 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 |
| BC45 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC46 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 |
| BC47 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 |
| BC48 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 |
| BC49 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 |
| BC50 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 |
| BC51 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 |
| BC52 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 |
| BC53 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC54 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 |
| BC55 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 |
| BC56 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 |
| BC57 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 |
| BC58 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 |
| BC59 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 |
| BC60 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC61 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 |
| BC62 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 |
| BC63 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 |
| BC64 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 |
| BC65 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 |
| BC66 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 |
| BC67 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 |
| BC68 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 |

## 1.1 ALGEMENE GEGEVENS

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|---|---|
| BC69 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC70 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 |
| BC71 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 |
| BC72 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 |
| BC73 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 |
| BC74 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 |
| BC75 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 |
| BC76 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC77 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 |
| BC78 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 |
| BC79 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 |
| BC80 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 |
| BC81 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 |
| BC82 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 |
| BC83 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 |
| BC84 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC85 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 |
| BC86 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 |
| BC87 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 |
| BC88 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 |
| BC89 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 |
| BC90 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 |
| BC91 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC92 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 |
| BC93 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 |
| BC94 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 |
| BC95 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 |
| BC96 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 |
| BC97 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 |
| BC98 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 |
| BC99 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 |
| BC100 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| BC101 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| BC102 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + |

## 1.1 ALGEMENE GEGEVENS

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| | + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC103 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC104 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC105 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC106 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 |
| | Blijvend en tijdelijk |
| BC107 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC108 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC109 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC110 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC111 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC112 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC113 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 |
| | Blijvend en tijdelijk |
| BC114 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 |
| | Blijvend en tijdelijk |
| BC115 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC116 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC117 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC118 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC119 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC120 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC121 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG130 |
| | Blijvend en tijdelijk |
| BC122 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC123 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC124 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC125 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC126 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC127 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC128 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC129 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC130 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC131 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC132 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC133 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC134 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| BC135 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG300 |
| BC136 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC137 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG300 |
| BC138 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG300 |
| BC139 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| BC140 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC141 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| BC142 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG300 |
| BC143 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC144 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG300 |
| BC145 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG300 |
| BC146 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG300 |
| BC147 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| BC148 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC149 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| BC150 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG300 |
| BC151 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC152 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG300 |
| BC153 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG300 |
| BC154 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| BC155 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC156 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| BC157 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG300 |
| BC158 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC159 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG300 |
| BC160 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG401 |
| BC161 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG402 |
| BC162 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG403 |
| BC163 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG404 |
| BC164 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG401 |
| BC165 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG402 |
| BC166 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG403 |
| BC167 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG404 |
| BC168 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | + 1.65*BG110 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC169 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC170 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC171 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC172 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC173 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC174 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC175 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC176 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC177 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC178 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC179 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC180 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC181 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC182 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC183 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC184 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC185 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC186 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC187 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC188 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC189 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC190 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC191 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC192 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC193 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC194 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC195 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC196 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC197 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC198 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC199 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + |

## 1.1 ALGEMENE GEGEVENS

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|---|---|
| | + 1.65*BG110 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC200 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC201 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC202 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC203 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC204 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC205 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC206 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC207 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC208 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC209 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC210 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC211 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC212 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC213 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC214 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC215 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC216 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC217 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC218 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC219 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC220 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC221 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC222 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC223 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC224 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC225 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC226 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC227 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC228 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC229 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC230 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC231 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG404 |

## 1.1 ALGEMENE GEGEVENS

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|---|---|
| BC232 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG401 |
| BC233 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG402 |
| BC234 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG403 |
| BC235 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG404 |
| BC236 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| BC237 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| BC238 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| BC239 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| BC240 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC241 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC242 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC243 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC244 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| BC245 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| BC246 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| BC247 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| BC248 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG401 |
| BC249 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG402 |
| BC250 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG403 |
| BC251 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG404 |
| BC252 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC253 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC254 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC255 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC256 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG401 |
| BC257 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG402 |
| BC258 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG403 |
| BC259 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG404 |
| BC260 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG401 |
| BC261 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG402 |
| BC262 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG403 |
| BC263 | Blijvend en tijdelijk<br>1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG404<br>Blijvend en tijdelijk |

## 1.1 ALGEMENE GEGEVENS

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|---|---|
| BC264 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC265 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC266 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC267 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC268 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC269 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC270 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC271 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC272 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC273 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC274 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC275 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC276 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC277 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC278 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC279 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC280 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC281 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC282 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC283 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC284 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC285 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC286 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC287 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC288 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 |
| | Blijvend en tijdelijk |
| BC289 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 |
| | Blijvend en tijdelijk |
| BC290 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 |
| | Blijvend en tijdelijk |
| BC291 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 |
| | Blijvend en tijdelijk |
| BC292 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC293 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC294 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC295 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC296 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | 1.65*BG110 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC297 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG120 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC298 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 |
| | Blijvend en tijdelijk |
| BC299 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC300 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC301 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC302 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC303 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC304 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC305 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 |
| | Blijvend en tijdelijk |
| BC306 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 |
| | Blijvend en tijdelijk |
| BC307 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC308 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC309 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC310 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC311 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC312 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG120 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC313 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG130 |
| | Blijvend en tijdelijk |
| BC314 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC315 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC316 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG130 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC317 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG140 |
| | Blijvend en tijdelijk |
| BC318 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG140 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC319 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC320 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC321 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC322 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC323 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC324 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC325 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC326 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC327 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC328 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |

## 1.1 ALGEMENE GEGEVENS

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|---|---|---|
| BC329 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG300 |
| BC330 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG300 |
| BC331 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| BC332 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC333 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| BC334 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG300 |
| BC335 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC336 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG300 |
| BC337 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG300 |
| BC338 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG300 |
| BC339 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| BC340 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC341 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| BC342 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG300 |
| BC343 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC344 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG300 |
| BC345 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG300 |
| BC346 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG300 |
| BC347 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC348 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG300 |
| BC349 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG300 |
| BC350 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG300 |
| BC351 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG300 |
| BC352 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG401 |
| BC353 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG402 |
| BC354 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG403 |
| BC355 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG404 |
| BC356 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG401 |
| BC357 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG402 |
| BC358 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG403 |
| BC359 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG404 |
| BC360 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG401 |
| BC361 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG402 |
| BC362 | Blijvend en tijdelijk | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | 1.65*BG110 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC363 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC364 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC365 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC366 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC367 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC368 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC369 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC370 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC371 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC372 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC373 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC374 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC375 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC376 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC377 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC378 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC379 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC380 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC381 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC382 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC383 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC384 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC385 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC386 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC387 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC388 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC389 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC390 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC391 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG110 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC392 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC393 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | 1.65*BG130 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC394 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC395 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC396 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC397 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC398 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC399 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC400 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC401 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC402 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC403 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC404 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC405 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC406 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC407 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC408 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC409 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC410 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC411 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC412 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC413 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC414 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC415 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC416 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC417 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC418 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC419 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC420 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC421 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC422 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC423 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC424 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC425 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG402 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| BC426 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG403 |
| BC427 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG404 |
| BC428 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| BC429 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402 |
| BC430 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| BC431 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| BC432 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC433 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC434 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC435 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC436 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| BC437 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| BC438 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| BC439 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| BC440 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG401 |
| BC441 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG402 |
| BC442 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG403 |
| BC443 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG404 |
| BC444 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| BC445 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| BC446 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| BC447 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| BC448 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG401 |
| BC449 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG402 |
| BC450 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG403 |
| BC451 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG110 + 1.65*BG150 + 1.65*BG404 |
| BC452 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG401 |
| BC453 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG402 |
| BC454 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG403 |
| BC455 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG404 |
| BC456 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG401 |
| BC457 | Blijvend en tijdelijk<br>0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG402<br>Blijvend en tijdelijk |

## 1.1 ALGEMENE GEGEVENS

| | | |
|---|---|---|
| | BC458 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG403 |
| | | Blijvend en tijdelijk |
| | BC459 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG404 |
| | | Blijvend en tijdelijk |
| | BC460 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | | Blijvend en tijdelijk |
| | BC461 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | | Blijvend en tijdelijk |
| | BC462 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | | Blijvend en tijdelijk |
| | BC463 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | | Blijvend en tijdelijk |
| | BC464 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG401 |
| | | Blijvend en tijdelijk |
| | BC465 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG402 |
| | | Blijvend en tijdelijk |
| | BC466 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG403 |
| | | Blijvend en tijdelijk |
| | BC467 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG130 + 1.65*BG150 + 1.65*BG404 |
| | | Blijvend en tijdelijk |
| | BC468 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG401 |
| | | Blijvend en tijdelijk |
| | BC469 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG402 |
| | | Blijvend en tijdelijk |
| | BC470 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG403 |
| | | Blijvend en tijdelijk |
| | BC471 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG404 |
| | | Blijvend en tijdelijk |
| | BC472 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG401 |
| | | Blijvend en tijdelijk |
| | BC473 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG402 |
| | | Blijvend en tijdelijk |
| | BC474 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG403 |
| | | Blijvend en tijdelijk |
| | BC475 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG140 + 1.65*BG150 + 1.65*BG404 |
| | | Blijvend en tijdelijk |
| | BC476 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG401 |
| | | Blijvend en tijdelijk |
| | BC477 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG402 |
| | | Blijvend en tijdelijk |
| | BC478 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG403 |
| | | Blijvend en tijdelijk |
| | BC479 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG404 |
| | | Blijvend en tijdelijk |
| BRUIKBAARHEIDSGRENSTOESTANDEN | | |
| Te ontwerpen belastingscombinaties: | BC480 | BG10 + BG20 + BG30 + BG40 |
| | | Karakteristiek met directe belasting, k-t: 0.600 |
| | BC481 | BG10 + BG20 + BG30 + BG40 + BG100 |
| | | Karakteristiek met directe belasting, k-t: 0.440 |
| | BC482 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 |
| | | Karakteristiek met directe belasting, k-t: 0.467 |
| | BC483 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 |
| | | Karakteristiek met directe belasting, k-t: 0.486 |
| | BC484 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 |
| | | Karakteristiek met directe belasting, k-t: 0.500 |
| | BC485 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 |
| | | Karakteristiek met directe belasting, k-t: 0.511 |
| | BC486 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 |
| | | Karakteristiek met directe belasting, k-t: 0.500 |
| | BC487 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 |
| | | Karakteristiek met directe belasting, k-t: 0.486 |
| | BC488 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 |
| | | Karakteristiek met directe belasting, k-t: 0.500 |
| | BC489 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 |
| | | Karakteristiek met directe belasting, k-t: 0.486 |
| | BC490 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 |
| | | Karakteristiek met directe belasting, k-t: 0.467 |
| | BC491 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 |
| | | Karakteristiek met directe belasting, k-t: 0.486 |
| | BC492 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + B |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | BG150 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC493 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC494 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC495 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC496 | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC497 | BG10 + BG20 + BG30 + BG40 + BG110 |
| | Karakteristiek met directe belasting, k-t: 0.440 |
| BC498 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC499 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC500 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC501 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC502 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC503 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC504 | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC505 | BG10 + BG20 + BG30 + BG40 + BG130 |
| | Karakteristiek met directe belasting, k-t: 0.440 |
| BC506 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC507 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC508 | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC509 | BG10 + BG20 + BG30 + BG40 + BG140 |
| | Karakteristiek met directe belasting, k-t: 0.440 |
| BC510 | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC511 | BG10 + BG20 + BG30 + BG40 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.440 |
| BC512 | BG10 + BG20 + BG30 + BG40 + BG120 |
| | Karakteristiek met directe belasting, k-t: 0.440 |
| BC513 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC514 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC515 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG130 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC516 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG130 + BG140 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC517 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG130 + BG140 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.520 |
| BC518 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG130 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC519 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG140 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC520 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG140 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC521 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG120 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC522 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG130 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC523 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG130 + BG140 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC524 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG130 + BG140 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC525 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG130 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC526 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG140 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC527 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG140 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC528 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC529 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC530 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG130 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC531 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG130 + BG140 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC532 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG130 + BG140 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC533 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG130 + B |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | BG150 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC534 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG140 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC535 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG140 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC536 | BG10 + BG20 + BG30 + BG40 + BG110 + BG120 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC537 | BG10 + BG20 + BG30 + BG40 + BG120 + BG130 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC538 | BG10 + BG20 + BG30 + BG40 + BG120 + BG130 + BG140 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC539 | BG10 + BG20 + BG30 + BG40 + BG120 + BG130 + BG140 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC540 | BG10 + BG20 + BG30 + BG40 + BG120 + BG130 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC541 | BG10 + BG20 + BG30 + BG40 + BG120 + BG140 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC542 | BG10 + BG20 + BG30 + BG40 + BG120 + BG140 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC543 | BG10 + BG20 + BG30 + BG40 + BG120 + BG150 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC544 | BG10 + BG20 + BG30 + BG40 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.440 |
| BC545 | BG10 + BG20 + BG30 + BG40 + BG100 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC546 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC547 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC548 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC549 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.520 |
| BC550 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC551 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC552 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC553 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC554 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC555 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC556 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC557 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC558 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC559 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC560 | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC561 | BG10 + BG20 + BG30 + BG40 + BG110 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC562 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC563 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC564 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC565 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC566 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC567 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC568 | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC569 | BG10 + BG20 + BG30 + BG40 + BG130 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC570 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC571 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC572 | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 + BG300 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC573 | BG10 + BG20 + BG30 + BG40 + BG140 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC574 | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC575 | BG10 + BG20 + BG30 + BG40 + BG150 + BG300 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC576 | BG10 + BG20 + BG30 + BG40 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.440 |
| BC577 | BG10 + BG20 + BG30 + BG40 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.440 |
| BC578 | BG10 + BG20 + BG30 + BG40 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.440 |
| BC579 | BG10 + BG20 + BG30 + BG40 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.440 |
| BC580 | BG10 + BG20 + BG30 + BG40 + BG100 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC581 | BG10 + BG20 + BG30 + BG40 + BG100 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC582 | BG10 + BG20 + BG30 + BG40 + BG100 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC583 | BG10 + BG20 + BG30 + BG40 + BG100 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC584 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC585 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC586 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC587 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC588 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC589 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC590 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC591 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC592 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC593 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC594 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC595 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC596 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.520 |
| BC597 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.520 |
| BC598 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.520 |
| BC599 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG140 + BG150 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.520 |
| BC600 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC601 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC602 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC603 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG130 + BG150 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC604 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC605 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC606 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC607 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC608 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC609 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.511 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| BC610 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC611 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG140 + BG150 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC612 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC613 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC614 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC615 | BG10 + BG20 + BG30 + BG40 + BG100 + BG110 + BG150 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC616 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC617 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC618 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC619 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC620 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC621 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC622 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC623 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC624 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC625 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC626 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC627 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG140 + BG150 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC628 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC629 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC630 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC631 | BG10 + BG20 + BG30 + BG40 + BG100 + BG130 + BG150 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC632 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC633 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC634 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC635 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC636 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC637 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC638 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC639 | BG10 + BG20 + BG30 + BG40 + BG100 + BG140 + BG150 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC640 | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC641 | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC642 | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC643 | BG10 + BG20 + BG30 + BG40 + BG100 + BG150 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC644 | BG10 + BG20 + BG30 + BG40 + BG110 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC645 | BG10 + BG20 + BG30 + BG40 + BG110 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC646 | BG10 + BG20 + BG30 + BG40 + BG110 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC647 | BG10 + BG20 + BG30 + BG40 + BG110 + BG404 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC648 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC649 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC650 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC651 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC652 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC653 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC654 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC655 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC656 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC657 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC658 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC659 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG140 + BG150 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.511 |
| BC660 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC661 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC662 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC663 | BG10 + BG20 + BG30 + BG40 + BG110 + BG130 + BG150 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC664 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC665 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC666 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC667 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC668 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC669 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC670 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC671 | BG10 + BG20 + BG30 + BG40 + BG110 + BG140 + BG150 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC672 | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC673 | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC674 | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC675 | BG10 + BG20 + BG30 + BG40 + BG110 + BG150 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC676 | BG10 + BG20 + BG30 + BG40 + BG130 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC677 | BG10 + BG20 + BG30 + BG40 + BG130 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC678 | BG10 + BG20 + BG30 + BG40 + BG130 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC679 | BG10 + BG20 + BG30 + BG40 + BG130 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC680 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC681 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC682 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC683 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC684 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC685 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC686 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 + BG403 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC687 | BG10 + BG20 + BG30 + BG40 + BG130 + BG140 + BG150 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.500 |
| BC688 | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC689 | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC690 | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC691 | BG10 + BG20 + BG30 + BG40 + BG130 + BG150 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC692 | BG10 + BG20 + BG30 + BG40 + BG140 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC693 | BG10 + BG20 + BG30 + BG40 + BG140 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC694 | BG10 + BG20 + BG30 + BG40 + BG140 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC695 | BG10 + BG20 + BG30 + BG40 + BG140 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC696 | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC697 | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC698 | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC699 | BG10 + BG20 + BG30 + BG40 + BG140 + BG150 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.486 |
| BC700 | BG10 + BG20 + BG30 + BG40 + BG150 + BG401 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC701 | BG10 + BG20 + BG30 + BG40 + BG150 + BG402 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC702 | BG10 + BG20 + BG30 + BG40 + BG150 + BG403 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC703 | BG10 + BG20 + BG30 + BG40 + BG150 + BG404 |
| | Karakteristiek met directe belasting, k-t: 0.467 |
| BC704 | BG10 + BG20 + BG30 + BG40 |
| | Frequent, k-t: 0.400 |
| BC705 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 |
| | Frequent, k-t: 0.437 |
| BC706 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 |
| | Frequent, k-t: 0.462 |
| BC707 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 + 0.9*BG130 |
| | Frequent, k-t: 0.481 |
| BC708 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 + 0.9*BG130 + 0.9*BG140 |
| | Frequent, k-t: 0.495 |
| BC709 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 + 0.9*BG130 + 0.9*BG140 + 0.9*BG150 |
| | Frequent, k-t: 0.506 |
| BC710 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 + 0.9*BG130 + 0.9*BG150 |
| | Frequent, k-t: 0.495 |
| BC711 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 + 0.9*BG140 |
| | Frequent, k-t: 0.481 |
| BC712 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 + 0.9*BG140 + 0.9*BG150 |
| | Frequent, k-t: 0.495 |
| BC713 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG110 + 0.9*BG150 |
| | Frequent, k-t: 0.481 |
| BC714 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG130 |
| | Frequent, k-t: 0.462 |
| BC715 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG130 + 0.9*BG140 |
| | Frequent, k-t: 0.481 |
| BC716 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG130 + 0.9*BG140 + 0.9*BG150 |
| | Frequent, k-t: 0.495 |
| BC717 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG130 + 0.9*BG150 |
| | Frequent, k-t: 0.481 |
| BC718 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG140 |
| | Frequent, k-t: 0.462 |
| BC719 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG140 + 0.9*BG150 |
| | Frequent, k-t: 0.481 |
| BC720 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 + 0.9*BG150 |
| | Frequent, k-t: 0.462 |
| BC721 | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 |
| | Frequent, k-t: 0.437 |
| BC722 | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG130 |
| | Frequent, k-t: 0.462 |
| BC723 | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG130 + 0.9*BG140 |
| | Frequent, k-t: 0.481 |
| BC724 | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG130 + 0.9*BG140 + 0.9*BG150 |
| | Frequent, k-t: 0.495 |
| BC725 | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG130 + 0.9*BG150 |
| | Frequent, k-t: 0.481 |
| BC726 | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG140 |
| | Frequent, k-t: 0.462 |
| BC727 | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG140 + 0 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | 0.9*BG150 |
| | Frequent, k-t: 0.481 |
| BC728 | BG10 + BG20 + BG30 + BG40 + 0.9*BG110 + 0.9*BG150 |
| | Frequent, k-t: 0.462 |
| BC729 | BG10 + BG20 + BG30 + BG40 + 0.9*BG130 |
| | Frequent, k-t: 0.437 |
| BC730 | BG10 + BG20 + BG30 + BG40 + 0.9*BG130 + 0.9*BG140 |
| | Frequent, k-t: 0.462 |
| BC731 | BG10 + BG20 + BG30 + BG40 + 0.9*BG130 + 0.9*BG140 + 0.9*BG150 |
| | Frequent, k-t: 0.481 |
| BC732 | BG10 + BG20 + BG30 + BG40 + 0.9*BG130 + 0.9*BG150 |
| | Frequent, k-t: 0.462 |
| BC733 | BG10 + BG20 + BG30 + BG40 + 0.9*BG140 |
| | Frequent, k-t: 0.437 |
| BC734 | BG10 + BG20 + BG30 + BG40 + 0.9*BG140 + 0.9*BG150 |
| | Frequent, k-t: 0.462 |
| BC735 | BG10 + BG20 + BG30 + BG40 + 0.9*BG150 |
| | Frequent, k-t: 0.437 |
| BC736 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 |
| | Frequent, k-t: 0.433 |
| BC737 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 |
| | Frequent, k-t: 0.457 |
| BC738 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG130 |
| | Frequent, k-t: 0.475 |
| BC739 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG130 + 0.8*BG140 |
| | Frequent, k-t: 0.489 |
| BC740 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | Frequent, k-t: 0.500 |
| BC741 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG130 + 0.8*BG150 |
| | Frequent, k-t: 0.489 |
| BC742 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG140 |
| | Frequent, k-t: 0.475 |
| BC743 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG140 + 0.8*BG150 |
| | Frequent, k-t: 0.489 |
| BC744 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0*BG120 + 0.8*BG150 |
| | Frequent, k-t: 0.475 |
| BC745 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG130 |
| | Frequent, k-t: 0.457 |
| BC746 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG130 + 0.8*BG140 |
| | Frequent, k-t: 0.475 |
| BC747 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | Frequent, k-t: 0.489 |
| BC748 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG130 + 0.8*BG150 |
| | Frequent, k-t: 0.475 |
| BC749 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG140 |
| | Frequent, k-t: 0.457 |
| BC750 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG140 + 0.8*BG150 |
| | Frequent, k-t: 0.475 |
| BC751 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 + 0.8*BG150 |
| | Frequent, k-t: 0.457 |
| BC752 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 |
| | Frequent, k-t: 0.433 |
| BC753 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0.8*BG130 |
| | Frequent, k-t: 0.457 |
| BC754 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0.8*BG130 + 0.8*BG140 |
| | Frequent, k-t: 0.475 |
| BC755 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | Frequent, k-t: 0.489 |
| BC756 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0.8*BG130 + 0.8*BG150 |
| | Frequent, k-t: 0.475 |
| BC757 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0.8*BG140 |
| | Frequent, k-t: 0.457 |
| BC758 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0.8*BG140 + 0.8*BG150 |
| | Frequent, k-t: 0.475 |
| BC759 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0*BG120 + 0.8*BG150 |
| | Frequent, k-t: 0.457 |
| BC760 | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG130 |
| | Frequent, k-t: 0.433 |
| BC761 | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG130 + 0.8*BG140 |
| | Frequent, k-t: 0.457 |
| BC762 | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | Frequent, k-t: 0.475 |

## 1.1 ALGEMENE GEGEVENS

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|---|---|
| BC763 | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG130 + 0.8*BG150 |
| | Frequent, k-t: 0.457 |
| BC764 | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG140 |
| | Frequent, k-t: 0.433 |
| BC765 | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG140 + 0.8*BG150 |
| | Frequent, k-t: 0.457 |
| BC766 | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG150 |
| | Frequent, k-t: 0.433 |
| BC767 | BG10 + BG20 + BG30 + BG40 + 0.2*BG300 |
| | Frequent, k-t: 0.410 |
| BC768 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG300 |
| | Frequent, k-t: 0.440 |
| BC769 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.2*BG300 |
| | Frequent, k-t: 0.462 |
| BC770 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.2*BG300 |
| | Frequent, k-t: 0.479 |
| BC771 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG300 |
| | Frequent, k-t: 0.492 |
| BC772 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, k-t: 0.502 |
| BC773 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, k-t: 0.492 |
| BC774 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.2*BG300 |
| | Frequent, k-t: 0.479 |
| BC775 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, k-t: 0.492 |
| BC776 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, k-t: 0.479 |
| BC777 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.2*BG300 |
| | Frequent, k-t: 0.462 |
| BC778 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.2*BG300 |
| | Frequent, k-t: 0.479 |
| BC779 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, k-t: 0.492 |
| BC780 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, k-t: 0.479 |
| BC781 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.2*BG300 |
| | Frequent, k-t: 0.462 |
| BC782 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, k-t: 0.479 |
| BC783 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, k-t: 0.462 |
| BC784 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.2*BG300 |
| | Frequent, k-t: 0.440 |
| BC785 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.2*BG300 |
| | Frequent, k-t: 0.462 |
| BC786 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG300 |
| | Frequent, k-t: 0.479 |
| BC787 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, k-t: 0.492 |
| BC788 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, k-t: 0.479 |
| BC789 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.2*BG300 |
| | Frequent, k-t: 0.462 |
| BC790 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, k-t: 0.479 |
| BC791 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, k-t: 0.462 |
| BC792 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.2*BG300 |
| | Frequent, k-t: 0.440 |
| BC793 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.2*BG300 |
| | Frequent, k-t: 0.462 |
| BC794 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, k-t: 0.479 |
| BC795 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, k-t: 0.462 |
| BC796 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.2*BG300 |
| | Frequent, k-t: 0.440 |
| BC797 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 + 0.2*BG300 |

## 1.1 ALGEMENE GEGEVENS

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|---|---|
| | Frequent, k-t: 0.462 |
| BC798 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG300 |
| | Frequent, k-t: 0.440 |
| BC799 | BG10 + BG20 + BG30 + BG40 + 0.2*BG401 |
| | Frequent, k-t: 0.410 |
| BC800 | BG10 + BG20 + BG30 + BG40 + 0.2*BG402 |
| | Frequent, k-t: 0.410 |
| BC801 | BG10 + BG20 + BG30 + BG40 + 0.2*BG403 |
| | Frequent, k-t: 0.410 |
| BC802 | BG10 + BG20 + BG30 + BG40 + 0.2*BG404 |
| | Frequent, k-t: 0.410 |
| BC803 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG401 |
| | Frequent, k-t: 0.440 |
| BC804 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG402 |
| | Frequent, k-t: 0.440 |
| BC805 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG403 |
| | Frequent, k-t: 0.440 |
| BC806 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG404 |
| | Frequent, k-t: 0.440 |
| BC807 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.2*BG401 |
| | Frequent, k-t: 0.462 |
| BC808 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.2*BG402 |
| | Frequent, k-t: 0.462 |
| BC809 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.2*BG403 |
| | Frequent, k-t: 0.462 |
| BC810 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.2*BG404 |
| | Frequent, k-t: 0.462 |
| BC811 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.2*BG401 |
| | Frequent, k-t: 0.479 |
| BC812 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.2*BG402 |
| | Frequent, k-t: 0.479 |
| BC813 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.2*BG403 |
| | Frequent, k-t: 0.479 |
| BC814 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.2*BG404 |
| | Frequent, k-t: 0.479 |
| BC815 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG401 |
| | Frequent, k-t: 0.492 |
| BC816 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG402 |
| | Frequent, k-t: 0.492 |
| BC817 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG403 |
| | Frequent, k-t: 0.492 |
| BC818 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG404 |
| | Frequent, k-t: 0.492 |
| BC819 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, k-t: 0.502 |
| BC820 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, k-t: 0.502 |
| BC821 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, k-t: 0.502 |
| BC822 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, k-t: 0.502 |
| BC823 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, k-t: 0.492 |
| BC824 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, k-t: 0.492 |
| BC825 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, k-t: 0.492 |
| BC826 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, k-t: 0.492 |
| BC827 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.2*BG401 |
| | Frequent, k-t: 0.479 |
| BC828 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.2*BG402 |
| | Frequent, k-t: 0.479 |
| BC829 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.2*BG403 |
| | Frequent, k-t: 0.479 |
| BC830 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.2*BG404 |
| | Frequent, k-t: 0.479 |
| BC831 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, k-t: 0.492 |
| BC832 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, k-t: 0.492 |

## 1.1 ALGEMENE GEGEVENS

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|---|---|
| BC833 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, k-t: 0.492 |
| BC834 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, k-t: 0.492 |
| BC835 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, k-t: 0.479 |
| BC836 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, k-t: 0.479 |
| BC837 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, k-t: 0.479 |
| BC838 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, k-t: 0.479 |
| BC839 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.2*BG401 |
| | Frequent, k-t: 0.462 |
| BC840 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.2*BG402 |
| | Frequent, k-t: 0.462 |
| BC841 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.2*BG403 |
| | Frequent, k-t: 0.462 |
| BC842 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.2*BG404 |
| | Frequent, k-t: 0.462 |
| BC843 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.2*BG401 |
| | Frequent, k-t: 0.479 |
| BC844 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.2*BG402 |
| | Frequent, k-t: 0.479 |
| BC845 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.2*BG403 |
| | Frequent, k-t: 0.479 |
| BC846 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.2*BG404 |
| | Frequent, k-t: 0.479 |
| BC847 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, k-t: 0.492 |
| BC848 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, k-t: 0.492 |
| BC849 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, k-t: 0.492 |
| BC850 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, k-t: 0.492 |
| BC851 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, k-t: 0.479 |
| BC852 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, k-t: 0.479 |
| BC853 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, k-t: 0.479 |
| BC854 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, k-t: 0.479 |
| BC855 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.2*BG401 |
| | Frequent, k-t: 0.462 |
| BC856 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.2*BG402 |
| | Frequent, k-t: 0.462 |
| BC857 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.2*BG403 |
| | Frequent, k-t: 0.462 |
| BC858 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.2*BG404 |
| | Frequent, k-t: 0.462 |
| BC859 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, k-t: 0.479 |
| BC860 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, k-t: 0.479 |
| BC861 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, k-t: 0.479 |
| BC862 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, k-t: 0.479 |
| BC863 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, k-t: 0.462 |
| BC864 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, k-t: 0.462 |
| BC865 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 + 0 |

## 1.1 ALGEMENE GEGEVENS

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|---|---|
| | 0.2*BG403 |
| | Frequent, k-t: 0.462 |
| BC866 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, k-t: 0.462 |
| BC867 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.2*BG401 |
| | Frequent, k-t: 0.440 |
| BC868 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.2*BG402 |
| | Frequent, k-t: 0.440 |
| BC869 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.2*BG403 |
| | Frequent, k-t: 0.440 |
| BC870 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.2*BG404 |
| | Frequent, k-t: 0.440 |
| BC871 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.2*BG401 |
| | Frequent, k-t: 0.462 |
| BC872 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.2*BG402 |
| | Frequent, k-t: 0.462 |
| BC873 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.2*BG403 |
| | Frequent, k-t: 0.462 |
| BC874 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.2*BG404 |
| | Frequent, k-t: 0.462 |
| BC875 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG401 |
| | Frequent, k-t: 0.479 |
| BC876 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG402 |
| | Frequent, k-t: 0.479 |
| BC877 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG403 |
| | Frequent, k-t: 0.479 |
| BC878 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.2*BG404 |
| | Frequent, k-t: 0.479 |
| BC879 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, k-t: 0.492 |
| BC880 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, k-t: 0.492 |
| BC881 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, k-t: 0.492 |
| BC882 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, k-t: 0.492 |
| BC883 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, k-t: 0.479 |
| BC884 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, k-t: 0.479 |
| BC885 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, k-t: 0.479 |
| BC886 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, k-t: 0.479 |
| BC887 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.2*BG401 |
| | Frequent, k-t: 0.462 |
| BC888 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.2*BG402 |
| | Frequent, k-t: 0.462 |
| BC889 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.2*BG403 |
| | Frequent, k-t: 0.462 |
| BC890 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.2*BG404 |
| | Frequent, k-t: 0.462 |
| BC891 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, k-t: 0.479 |
| BC892 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, k-t: 0.479 |
| BC893 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, k-t: 0.479 |
| BC894 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, k-t: 0.479 |
| BC895 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, k-t: 0.462 |
| BC896 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, k-t: 0.462 |
| BC897 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, k-t: 0.462 |
| BC898 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, k-t: 0.462 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| BC899 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.2*BG401 |
| | Frequent, k-t: 0.440 |
| BC900 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.2*BG402 |
| | Frequent, k-t: 0.440 |
| BC901 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.2*BG403 |
| | Frequent, k-t: 0.440 |
| BC902 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.2*BG404 |
| | Frequent, k-t: 0.440 |
| BC903 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.2*BG401 |
| | Frequent, k-t: 0.462 |
| BC904 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.2*BG402 |
| | Frequent, k-t: 0.462 |
| BC905 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.2*BG403 |
| | Frequent, k-t: 0.462 |
| BC906 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.2*BG404 |
| | Frequent, k-t: 0.462 |
| BC907 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, k-t: 0.479 |
| BC908 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, k-t: 0.479 |
| BC909 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, k-t: 0.479 |
| BC910 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, k-t: 0.479 |
| BC911 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, k-t: 0.462 |
| BC912 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, k-t: 0.462 |
| BC913 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, k-t: 0.462 |
| BC914 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, k-t: 0.462 |
| BC915 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.2*BG401 |
| | Frequent, k-t: 0.440 |
| BC916 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.2*BG402 |
| | Frequent, k-t: 0.440 |
| BC917 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.2*BG403 |
| | Frequent, k-t: 0.440 |
| BC918 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.2*BG404 |
| | Frequent, k-t: 0.440 |
| BC919 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, k-t: 0.462 |
| BC920 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, k-t: 0.462 |
| BC921 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, k-t: 0.462 |
| BC922 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, k-t: 0.462 |
| BC923 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG401 |
| | Frequent, k-t: 0.440 |
| BC924 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG402 |
| | Frequent, k-t: 0.440 |
| BC925 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG403 |
| | Frequent, k-t: 0.440 |
| BC926 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG404 |
| | Frequent, k-t: 0.440 |
| BC927 | BG10 + BG20 + BG30 + BG40 |
| | Quasi-blijvend, k-t: 0.400 |
| BC928 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 |
| | Quasi-blijvend, k-t: 0.433 |
| BC929 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 |
| | Quasi-blijvend, k-t: 0.457 |
| BC930 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 |
| | Quasi-blijvend, k-t: 0.475 |
| BC931 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 |
| | Quasi-blijvend, k-t: 0.489 |
| BC932 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | Quasi-blijvend, k-t: 0.500 |
| BC933 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 |
| | Quasi-blijvend, k-t: 0.489 |
| BC934 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 |
| | Quasi-blijvend, k-t: 0.475 |
| BC935 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 |
| | Quasi-blijvend, k-t: 0.489 |
| BC936 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG110 + 0 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | 0.8*BG150 |
| | Quasi-blijvend, k-t: 0.475 |
| BC937 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 |
| | Quasi-blijvend, k-t: 0.457 |
| BC938 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 |
| | Quasi-blijvend, k-t: 0.475 |
| BC939 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | Quasi-blijvend, k-t: 0.489 |
| BC940 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG130 + 0.8*BG150 |
| | Quasi-blijvend, k-t: 0.475 |
| BC941 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 |
| | Quasi-blijvend, k-t: 0.457 |
| BC942 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG140 + 0.8*BG150 |
| | Quasi-blijvend, k-t: 0.475 |
| BC943 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.8*BG150 |
| | Quasi-blijvend, k-t: 0.457 |
| BC944 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 |
| | Quasi-blijvend, k-t: 0.433 |
| BC945 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 |
| | Quasi-blijvend, k-t: 0.457 |
| BC946 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 |
| | Quasi-blijvend, k-t: 0.475 |
| BC947 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | Quasi-blijvend, k-t: 0.489 |
| BC948 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG130 + 0.8*BG150 |
| | Quasi-blijvend, k-t: 0.475 |
| BC949 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 |
| | Quasi-blijvend, k-t: 0.457 |
| BC950 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG140 + 0.8*BG150 |
| | Quasi-blijvend, k-t: 0.475 |
| BC951 | BG10 + BG20 + BG30 + BG40 + 0.8*BG110 + 0.8*BG150 |
| | Quasi-blijvend, k-t: 0.457 |
| BC952 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 |
| | Quasi-blijvend, k-t: 0.433 |
| BC953 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 |
| | Quasi-blijvend, k-t: 0.457 |
| BC954 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG140 + 0.8*BG150 |
| | Quasi-blijvend, k-t: 0.475 |
| BC955 | BG10 + BG20 + BG30 + BG40 + 0.8*BG130 + 0.8*BG150 |
| | Quasi-blijvend, k-t: 0.457 |
| BC956 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 |
| | Quasi-blijvend, k-t: 0.433 |
| BC957 | BG10 + BG20 + BG30 + BG40 + 0.8*BG140 + 0.8*BG150 |
| | Quasi-blijvend, k-t: 0.457 |
| BC958 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 |
| | Quasi-blijvend, k-t: 0.433 |

| | |
|---|---|
| Ontwerpsituatie instellingen voor bruikbaarheidsgrenstoestandcontrole | |
| Belastingscombinatie: | |
| Karakteristiek met directe belasting | Controles: $k_1*f_{ck}$, $k_3*f_{yk}$ |
| Karakteristiek met opgelegde vervorming | Controles: $k_1*f_{ck}$, $k_4*f_{yk}$ |
| Frequent | Controles: $w_k$ |
| Quasi-blijvend | Controles: $k_2*f_{ck}$, $w_k$, $u_l$ |
| | |
| Vervormingen relatief t.o.v.: | Onvervormd systeem |

## 1.2 MATERIALEN

| Mat. No. | Materiaalomschrijving | | Opm. |
|---|---|---|---|
| | Betonkwaliteit | Wapeningskwaliteit | |
| 2 | Beton C30/37 | B 500 S (A) | |

## 1.2.1 MATERIAAL PARAMETERS

| Mat. No. | Omschrijving | Naam | Grootte | Eenheid |
|---|---|---|---|---|
| **2** | **Betonkwaliteit: Beton C30/37** | | | |
| | Karakteristieke cilinderdruksterkte | $f_{ck}$ | 30.000 | N/mm^2 |
| | Gem. cilinderdruksterkte | $f_{cm}$ | 38.000 | N/mm^2 |
| | Gem. zuivere treksterkte | $f_{ctm}$ | 2.900 | N/mm^2 |
| | 5 % Fractie van de zuivere treksterkte | $f_{ctk,005}$ | 2.000 | N/mm^2 |
| | 95 % Fractie van de zuivere treksterkte | $f_{ctk,0.95}$ | 3.800 | N/mm^2 |
| | Gem. secans elasticiteitsmodulus | $E_{cm}$ | 33000.000 | N/mm^2 |
| | Karakteristieke rekken voor niet-lineaire berekeningen | | | |
| | Uiterste betonstuik bij zuivere druk | $\varepsilon_{c1}$ | -2.200 | ‰ |
| | Uiterste rek bij bezwijken | $\varepsilon_{cu1}$ | -3.500 | ‰ |
| | Karakteristieke rekken voor parabolisch-rechthoekig verloop | | | |
| | Uiterste betonstuik bij zuivere druk | $\varepsilon_{c2}$ | -2.000 | ‰ |
| | Uiterste rek bij bezwijken | $\varepsilon_{cu2}$ | -3.500 | ‰ |
| | Exponent van Parabool | n | 2 | |
| | Vol. gewicht | $\gamma$ | 25.00 | kN/m^3 |
| | **Wapeningskwaliteit: B 500 S (A)** | | | |

## 1.2.1 MATERIAAL PARAMETERS

| Mat. No. | Omschrijving | Naam | Grootte | Eenheid |
|---|---|---|---|---|
| | Elasticiteitsmodulus | $E_s$ | 200000 | N/mm^2 |
| | Karakteristieke waarde van de vloeispanning | $f_{yk}$ | 500 | N/mm^2 |
| | Karakteristieke Waarde van de Trekvastheid | $f_{tk}$ | 525 | N/mm^2 |
| | Rekgrens | $\varepsilon_{uk}$ | 25.000 | ‰ |

Rechthoek 400/600

## 1.3 DOORSNEDES

| Snede No. | Mat. No. | Doorsnede Omschrijving | Opmerkingen | Opm. |
|---|---|---|---|---|
| 1 | 2 | Rechthoek 400/600 | | BetonRandbalk |

VLU 800/0/0/200/0...

## 1.4 RIBBEN

| Staaf No. | Doorsnede No. Begin | Doorsnede No. Eind | Effectieve breedte Vlak No. | b-1 [mm] | Vlak. No | b-2 [mm] | Opmerkingen |
|---|---|---|---|---|---|---|---|
| 1 | 1 | 1 | 1 | 200 | | | |
| 2 | 1 | 1 | 1 | 200 | | | |
| 3 | 1 | 1 | 1 | 200 | | | |
| 4 | 1 | 1 | 1 | 200 | | | |
| 35 | 1 | 1 | 1 | 200 | | | |
| 36 | 1 | 1 | 1 | 200 | | | |
| 39 | 1 | 1 | 1 | 200 | | | |
| 40 | 1 | 1 | 1 | 200 | | | |
| 41 | 1 | 1 | 1 | 200 | | | |
| 42 | 1 | 1 | 1 | 200 | | | |
| 104 | 1 | 1 | 1 | 200 | | | |
| 105 | 1 | 1 | 1 | 200 | | | |
| 108 | 1 | 1 | 1 | 200 | | | |
| 109 | 1 | 1 | 1 | 200 | | | |
| 110 | 1 | 1 | 1 | 200 | | | |
| 111 | 1 | 1 | 1 | 200 | | | |

**RF-CONCRETE Members**
BG1
Ontwerp van betonnen staven

## 1.6 WAPENINGGROEP NO. 1

| | |
|---|---|
| Toegepast op staven: | 1-4,35,36,39-42,104,105,108-111 |
| | |
| LANGSWAPENING | |
| Beschikbare diameters: | 12.0, 16.0 mm |
| Max. aantal lagen: | 1 |
| Min. h.o.h.-afstand voor 1e laag: | 20.0 mm |
| Type verankering: | Recht |
| Oppervlak: | Geribd |
| Reductie van wapening: | Geen |
| | |
| AFSCHUIFWAPENING | |
| Beschikbare diameters: | 10.0 mm |
| Aantal beugelbenen: | 2 |
| Hoek: | 90° |
| Type verankering: | Bocht |
| Beugel layout: | |
| | |
| LAY-OUT WAPENING | |
| Betondekking volgens norm | ☐ |
| Betondekking c-boven: | 30.0 mm |
| Betondekking $c_{onder}$: | 30.0 mm |
| Betondekking $c_{flank}$ | 30.0 mm |
| Lay-out wapening: | -z (bov) - +z (ond) (geoptimaliseerde verdeling) |
| Over complete breedte van de doorsnede: | ☒ |
| Wringwapening verdeeld over de omtrek: | ☒ |
| Relevante snedekrachten: | N, V-y, V-z, M-T, M-y, M-z |
| | |
| MIN. WAPENING | |
| Min. wapeningsoppervlak (min. A-s,boven): | 0.00 $mm^2$ |
| Min. wapeningsoppervlak (min. A-s,onder): | 0.00 $mm^2$ |
| Min. langswapening volgens norm: | ☒ |
| Min. afschuifwapening volgens norm: | ☒ |
| Langswapening voor dwarskrachtontwerp: | Gebruik theoretische langswapening |
| | |
| AFSCHUIF VERBINDING | |
| Afschuifverbinding beschikbaar: | ☐ |
| Ontwerp van flensverbindingen bij opgesplitste doorsnedes | ☐ |
| | |
| INSTELLINGEN VOOR EN 1992-1-1:2004/A1:2014 | |
| Max. wapeningspercentage: | 8.00 % |
| Hoogte beperking neutrale lijn | ☒ |
| Partiï¿½le veiligheidsfactor gamma-c | BT 1.50, BU 1.20, BGT 1.00 |
| Partiï¿½le veiligheidsfactor Gamma-s | BT 1.15, BU 1.00, BGT 1.00 |
| Reductiefactor Alpha-cc | BT 1.00, BU 1.00, BGT 1.00 |
| Reductiefactor Alpha-ct | BT 1.00, BU 1.00, BGT 1.00 |
| Min. hellingshoek van de betonschoor | 21.80 ° |
| Max. hellingshoek van de betonschoor | 45.00 ° |
| | |
| BRUIKBAARHEID | |
| Scheurwijdte berekening | |
| Grenswaarde van toelaatbare scheurwijdte $w_{k,max,-z\ (bov)}$: | 0.2 mm |
| Grenswaarde van toelaatbare scheurwijdte $w_{k,max,+z\ (ond)}$: | 0.2 mm |
| Ontwerp zonder directe scheurwijdte berekening: | ☐ |
| Ontwerp met directe scheurwijdteberekening: | ☒ |

## 1.6 WAPENINGGROEP NO. 1

| | |
|---|---|
| Gebruik verg. (7.14) voor $s_{r,max}$: | ☒ |
| Werkzame betontreksterkte op het tijdstip van scheuren: | 1.000 * $f_{ctm}$ |
| $A_{s,min}$ voor effecten t.g.v. verhindering : | ☒ |
| Spanningsverdeling in het profiel voor scheuren: | Afhankelijk van de gedefinieerde belasting ($k_c$ = 0.0 ... 1.0) |
| $A_{s,min}$ Lay-out: | -z (bov) /+z (ond) |
| Scheurformatie binnen de eerste 28 dagen: | ☐ |
| Spanningsberekening | |
| Begrenzing van de betondrukspanning $\sigma_c$: | ☐ |
| Doorbuigingsberekening | |
| Doorbuiging $u_{l,z}$: | ☐ |
| Bepaling van langswapening | |
| Verhoog de vereiste langswapening automatisch voor ontwerp bruikbaarheidsgrenstoestand : | ☒ |

## 2.3 BENODIGDE WAPENING PER STAAF

| Wapening | Staaf No. | Locatie x [m] | Belasting | Wapening Oppervl. | Eenheid | Foutboodschap of opmerking |
|---|---|---|---|---|---|---|
| Staaf No. 1 - Rib VLU 800/0/0/200/0/400 | | | | | | |
| $A_{s,z}$ | 1 | 6.400 | BC164 | 349.11 | mm² | 13) 25) 28) |
| $A_{s,+z}$ | 1 | 6.400 | BC433 | 394.26 | mm² | |
| $A_{s,T}$ | 1 | 0.000 | BC155 | 2187.53 | mm² | |
| $a_{sw,V,bgl}$ | 1 | 0.000 | BC154 | 350.54 | mm²/m | 58) 69) |
| $a_{sw,T,beugel}$ | 1 | 0.000 | BC155 | 187.48 | mm²/m | |
| Staaf No. 2 - Rib VLU 800/0/0/200/0/400 | | | | | | |
| $A_{s,z}$ | 2 | 4.300 | BC17 | 450.85 | mm² | 25) 28) |
| $A_{s,+z}$ | 2 | 4.300 | BC148 | 558.95 | mm² | |
| $A_{s,T}$ | 2 | 1.433 | BC155 | 2470.67 | mm² | |
| $a_{sw,V,bgl}$ | 2 | 0.000 | BC170 | 350.54 | mm²/m | 58) 69) |
| $a_{sw,T,beugel}$ | 2 | 1.433 | BC155 | 211.74 | mm²/m | |
| Staaf No. 3 - Rib VLU 800/0/0/200/0/400 | | | | | | |
| $A_{s,z}$ | 3 | 6.530 | BC260 | 394.67 | mm² | 25) 28) |
| $A_{s,+z}$ | 3 | 6.530 | BC260 | 394.67 | mm² | 25) 29) |
| $A_{s,T}$ | 3 | 0.000 | BC155 | 1654.59 | mm² | |
| $a_{sw,V,bgl}$ | 3 | 0.000 | BC154 | 350.54 | mm²/m | 58) 69) |
| $a_{sw,T,beugel}$ | 3 | 0.000 | BC155 | 141.80 | mm²/m | |
| Staaf No. 4 - Rib VLU 800/0/0/200/0/400 | | | | | | |
| $A_{s,z}$ | 4 | 4.300 | BC419 | 347.38 | mm² | 13) 25) 28) |
| $A_{s,+z}$ | 4 | 4.300 | BC419 | 347.38 | mm² | 13) 25) 29) |
| $A_{s,T}$ | 4 | 1.433 | BC155 | 2177.82 | mm² | |
| $a_{sw,V,bgl}$ | 4 | 0.000 | BC187 | 350.54 | mm²/m | 58) 69) |
| $a_{sw,T,beugel}$ | 4 | 1.433 | BC155 | 186.64 | mm²/m | |
| Staaf No. 35 - Rib VLU 800/0/0/200/0/400 | | | | | | |
| $A_{s,z}$ | 35 | 0.000 | BC168 | 350.24 | mm² | 13) 25) 28) |
| $A_{s,+z}$ | 35 | 0.000 | BC433 | 395.54 | mm² | |
| $A_{s,T}$ | 35 | 5.005 | BC473 | 661.82 | mm² | |
| $a_{sw,V,bgl}$ | 35 | 0.000 | BC185 | 350.54 | mm²/m | 58) 69) |
| $a_{sw,T,beugel}$ | 35 | 5.005 | BC473 | 56.72 | mm²/m | |
| Staaf No. 36 - Rib VLU 800/0/0/200/0/400 | | | | | | |
| $A_{s,z}$ | 36 | 0.000 | BC389 | 342.07 | mm² | 13) 25) 28) |
| $A_{s,+z}$ | 36 | 0.000 | BC468 | 350.78 | mm² | |
| $A_{s,T}$ | 36 | 6.530 | BC155 | 2117.39 | mm² | |
| $a_{sw,V,bgl}$ | 36 | 0.000 | BC236 | 350.54 | mm²/m | 58) 69) |
| $a_{sw,T,beugel}$ | 36 | 6.530 | BC155 | 181.47 | mm²/m | |
| Staaf No. 39 - Rib VLU 800/0/0/200/0/400 | | | | | | |
| $A_{s,z}$ | 39 | 4.500 | BC414 | 435.13 | mm² | 13) 25) 28) |
| $A_{s,+z}$ | 39 | 4.500 | BC414 | 435.13 | mm² | 13) 25) 29) |
| $A_{s,T}$ | 39 | 0.000 | BC140 | 1124.21 | mm² | |
| $a_{sw,V,bgl}$ | 39 | 0.000 | BC134 | 350.54 | mm²/m | 58) 69) |
| $a_{sw,T,beugel}$ | 39 | 0.000 | BC140 | 96.35 | mm²/m | |
| Staaf No. 40 - Rib VLU 800/0/0/200/0/400 | | | | | | |
| $A_{s,z}$ | 40 | 2.500 | BC155 | 931.11 | mm² | 13) 25) 28) |
| $A_{s,+z}$ | 40 | 2.500 | BC155 | 931.11 | mm² | 13) 25) 29) |
| $A_{s,T}$ | 40 | 0.000 | BC148 | 618.96 | mm² | |
| $a_{sw,V,bgl}$ | 40 | 0.000 | BC155 | 350.54 | mm²/m | 58) 69) |
| $a_{sw,T,beugel}$ | 40 | 0.000 | BC148 | 53.05 | mm²/m | |
| Staaf No. 41 - Rib VLU 800/0/0/200/0/400 | | | | | | |
| $A_{s,z}$ | 41 | 2.000 | BC227 | 729.00 | mm² | 13) 25) 28) |
| $A_{s,+z}$ | 41 | 2.000 | BC227 | 729.00 | mm² | 13) 25) 29) |
| $A_{s,T}$ | 41 | 4.500 | BC140 | 1237.95 | mm² | |
| $a_{sw,V,bgl}$ | 41 | 0.000 | BC134 | 350.54 | mm²/m | 58) 69) |
| $a_{sw,T,beugel}$ | 41 | 4.500 | BC140 | 106.10 | mm²/m | |
| Staaf No. 42 - Rib VLU 800/0/0/200/0/400 | | | | | | |
| $A_{s,z}$ | 42 | 0.000 | BC1 | 438.03 | mm² | 25) 28) |
| $A_{s,+z}$ | 42 | 0.000 | BC147 | 504.68 | mm² | |
| $A_{s,T}$ | 42 | 2.867 | BC155 | 2546.42 | mm² | |
| $a_{sw,V,bgl}$ | 42 | 0.000 | BC146 | 350.54 | mm²/m | 58) 69) |
| $a_{sw,T,beugel}$ | 42 | 2.867 | BC155 | 218.23 | mm²/m | |
| Staaf No. 104 - Rib VLU 800/0/0/200/0/400 | | | | | | |
| $A_{s,z}$ | 104 | 0.000 | BC26 | 392.67 | mm² | 25) 28) |
| $A_{s,+z}$ | 104 | 0.000 | BC26 | 392.67 | mm² | 25) 29) |
| $A_{s,T}$ | 104 | 1.505 | BC269 | 667.21 | mm² | |
| $a_{sw,V,bgl}$ | 104 | 0.000 | BC172 | 350.54 | mm²/m | 58) 69) |
| $a_{sw,T,beugel}$ | 104 | 1.505 | BC269 | 57.18 | mm²/m | |
| Staaf No. 105 - Rib VLU 800/0/0/200/0/400 | | | | | | |
| $A_{s,z}$ | 105 | 0.000 | BC155 | 320.00 | mm² | 25) |
| $A_{s,+z}$ | 105 | 0.000 | BC155 | 320.00 | mm² | 25) |
| $A_{s,T}$ | 105 | 6.400 | BC155 | 1933.60 | mm² | |

## 2.3 BENODIGDE WAPENING PER STAAF

| Wapening | Staaf No. | Locatie x [m] | Belasting | Wapening Oppervl. | Eenheid | Foutboodschap of opmerking |
|---|---|---|---|---|---|---|
| $a_{sw,V,bgl}$ | 105 | 0.000 | BC269 | 350.54 | mm²/m | 58) 69) |
| $a_{sw,T,beugel}$ | 105 | 6.400 | BC155 | 165.71 | mm²/m | |
| Staaf No. 108 - Rib VLU 800/0/0/200/0/400 | | | | | | |
| $A_{s,z}$ | 108 | 0.000 | BC398 | 320.00 | mm² | 13) 25) |
| $A_{s,+z}$ | 108 | 0.000 | BC398 | 320.00 | mm² | 13) 25) |
| $A_{s,T}$ | 108 | 4.500 | BC140 | 957.38 | mm² | |
| $a_{sw,V,bgl}$ | 108 | 0.000 | BC134 | 350.54 | mm²/m | 58) 69) |
| $a_{sw,T,beugel}$ | 108 | 4.500 | BC140 | 82.05 | mm²/m | |
| Staaf No. 109 - Rib VLU 800/0/0/200/0/400 | | | | | | |
| $A_{s,z}$ | 109 | 2.500 | BC227 | 1381.90 | mm² | 13) 25) 28) |
| $A_{s,+z}$ | 109 | 2.500 | BC340 | 1381.90 | mm² | 27) 29) |
| $A_{s,T}$ | 109 | 0.000 | BC140 | 1116.88 | mm² | |
| $a_{sw,V,bgl}$ | 109 | 0.000 | BC134 | 350.54 | mm²/m | 58) 69) |
| $a_{sw,T,beugel}$ | 109 | 0.000 | BC140 | 95.72 | mm²/m | |
| Staaf No. 110 - Rib VLU 800/0/0/200/0/400 | | | | | | |
| $A_{s,z}$ | 110 | 2.000 | BC154 | 970.92 | mm² | 13) 25) 28) |
| $A_{s,+z}$ | 110 | 2.000 | BC154 | 970.92 | mm² | 13) 25) 29) |
| $A_{s,T}$ | 110 | 4.500 | BC148 | 858.06 | mm² | |
| $a_{sw,V,bgl}$ | 110 | 0.000 | BC154 | 350.54 | mm²/m | 58) 69) |
| $a_{sw,T,beugel}$ | 110 | 4.500 | BC148 | 73.54 | mm²/m | |
| Staaf No. 111 - Rib VLU 800/0/0/200/0/400 | | | | | | |
| $A_{s,z}$ | 111 | 0.000 | BC167 | 320.00 | mm² | 13) 25) |
| $A_{s,+z}$ | 111 | 0.000 | BC167 | 320.00 | mm² | 13) 25) |
| $A_{s,T}$ | 111 | 3.344 | BC155 | 1790.89 | mm² | |
| $a_{sw,V,bgl}$ | 111 | 0.000 | BC234 | 350.54 | mm²/m | 58) 69) |
| $a_{sw,T,beugel}$ | 111 | 3.344 | BC155 | 153.48 | mm²/m | |

## 3.1 TOEGEPASTE LANGSWAPENING

| Onderde No. | Wapening Positie | Aant. Wap. st | $d_s$ [mm] | $A_s$ [cm²] | Lengte [m] | x-positie [m] van | x-positie [m] tot | Gewicht [kg] | Opm. |
|---|---|---|---|---|---|---|---|---|---|
| Staaf No.1 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | |
| 1 | Basis -z (bov) | 4 | 16.0 | 804.25 | 6.720 | -0.160 | 6.560 | 42.43 | |
| 2 | -z (bov) | 3 | 12.0 | 339.29 | 6.640 | -0.120 | 6.520 | 17.69 | |
| 3 | Basis +z (ond) | 4 | 16.0 | 804.25 | 6.720 | -0.160 | 6.560 | 42.43 | |
| 4 | +z (ond) | 3 | 12.0 | 339.29 | 6.640 | -0.120 | 6.520 | 17.69 | |
| 5 | +-y(zijde) | 14 | 12.0 | 1583.36 | 6.640 | -0.120 | 6.520 | 82.53 | 158) |
| Staaf No.2 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | |
| 1 | Basis -z (bov) | 4 | 16.0 | 804.25 | 4.620 | -0.160 | 4.460 | 29.17 | |
| 2 | -z (bov) | 4 | 12.0 | 452.39 | 4.540 | -0.120 | 4.420 | 16.12 | |
| 3 | Basis +z (ond) | 4 | 16.0 | 804.25 | 4.644 | -0.160 | 4.484 | 29.32 | |
| 4 | +z (ond) | 4 | 12.0 | 452.39 | 4.540 | -0.120 | 4.420 | 16.12 | |
| 5 | +-y(zijde) | 16 | 12.0 | 1809.56 | 4.540 | -0.120 | 4.420 | 64.49 | 158) |
| Staaf No.3 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | |
| 1 | Basis -z (bov) | 4 | 16.0 | 804.25 | 6.850 | -0.160 | 6.690 | 43.25 | |
| 2 | -z (bov) | 2 | 12.0 | 226.19 | 6.770 | -0.120 | 6.650 | 12.02 | |
| 3 | Basis +z (ond) | 4 | 16.0 | 804.25 | 6.850 | -0.160 | 6.690 | 43.25 | |
| 4 | +z (ond) | 2 | 12.0 | 226.19 | 6.770 | -0.120 | 6.650 | 12.02 | |
| 5 | +-y(zijde) | 12 | 12.0 | 1357.17 | 6.770 | -0.120 | 6.650 | 72.13 | 158) |
| Staaf No.4 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | |
| 1 | Basis -z (bov) | 4 | 16.0 | 804.25 | 4.620 | -0.160 | 4.460 | 29.17 | |
| 2 | -z (bov) | 3 | 12.0 | 339.29 | 4.540 | -0.120 | 4.420 | 12.09 | |
| 3 | Basis +z (ond) | 4 | 16.0 | 804.25 | 4.620 | -0.160 | 4.460 | 29.17 | |
| 4 | +z (ond) | 3 | 12.0 | 339.29 | 4.540 | -0.120 | 4.420 | 12.09 | |
| 5 | +-y(zijde) | 14 | 12.0 | 1583.36 | 4.540 | -0.120 | 4.420 | 56.43 | 158) |
| Staaf No.35 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | |
| 1 | Basis -z (bov) | 4 | 16.0 | 804.25 | 6.830 | -0.160 | 6.670 | 43.12 | |
| 2 | Basis +z (ond) | 4 | 16.0 | 804.25 | 6.830 | -0.160 | 6.670 | 43.12 | |
| 3 | +-y(zijde) | 6 | 12.0 | 678.58 | 6.750 | -0.120 | 6.630 | 35.96 | 158) |
| Staaf No.36 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | |
| 1 | Basis -z (bov) | 4 | 16.0 | 804.25 | 6.850 | -0.160 | 6.690 | 43.25 | |
| 2 | -z (bov) | 3 | 12.0 | 339.29 | 6.770 | -0.120 | 6.650 | 18.03 | |
| 3 | Basis +z (ond) | 4 | 16.0 | 804.25 | 6.850 | -0.160 | 6.690 | 43.25 | |
| 4 | +z (ond) | 3 | 12.0 | 339.29 | 6.770 | -0.120 | 6.650 | 18.03 | |
| 5 | +-y(zijde) | 14 | 12.0 | 1583.36 | 6.770 | -0.120 | 6.650 | 84.15 | 158) |
| Staaf No.39 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | |
| 1 | Basis -z (bov) | 4 | 16.0 | 804.25 | 4.820 | -0.160 | 4.660 | 30.43 | |
| 2 | Basis +z (ond) | 4 | 16.0 | 804.25 | 4.820 | -0.160 | 4.660 | 30.43 | |
| 3 | +-y(zijde) | 8 | 12.0 | 904.78 | 4.740 | -0.120 | 4.620 | 33.67 | 158) |
| Staaf No.40 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | |
| 1 | Basis -z (bov) | 4 | 16.0 | 804.25 | 4.820 | -0.160 | 4.660 | 30.43 | |
| 2 | -z (bov) | 2 | 12.0 | 226.19 | 4.740 | -0.120 | 4.620 | 8.42 | |
| 3 | Basis +z (ond) | 4 | 16.0 | 804.25 | 4.836 | -0.160 | 4.676 | 30.53 | |
| 4 | +z (ond) | 2 | 12.0 | 226.19 | 4.740 | -0.120 | 4.620 | 8.42 | |
| 5 | +-y(zijde) | 4 | 12.0 | 452.39 | 4.740 | -0.120 | 4.620 | 16.83 | 158) |
| Staaf No.41 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | |
| 1 | Basis -z (bov) | 4 | 16.0 | 804.25 | 4.820 | -0.160 | 4.660 | 30.43 | |
| 2 | Basis +z (ond) | 4 | 16.0 | 804.25 | 4.937 | -0.200 | 4.737 | 31.17 | |
| 3 | +-y(zijde) | 6 | 12.0 | 678.58 | 4.740 | -0.120 | 4.620 | 25.25 | 158) |
| Staaf No.42 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | |
| 1 | Basis -z (bov) | 4 | 16.0 | 804.25 | 4.620 | -0.160 | 4.460 | 29.17 | |
| 2 | -z (bov) | 5 | 12.0 | 565.49 | 4.540 | -0.120 | 4.420 | 20.15 | |
| 3 | Basis +z (ond) | 4 | 16.0 | 804.25 | 4.620 | -0.160 | 4.460 | 29.17 | |
| 4 | +z (ond) | 5 | 12.0 | 565.49 | 4.540 | -0.120 | 4.420 | 20.15 | |
| 5 | +-y(zijde) | 16 | 12.0 | 1809.56 | 4.540 | -0.120 | 4.420 | 64.49 | 158) |
| Staaf No.104 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | |
| 1 | Basis -z (bov) | 4 | 16.0 | 804.25 | 6.830 | -0.160 | 6.670 | 43.12 | |
| 2 | Basis +z (ond) | 4 | 16.0 | 804.25 | 6.830 | -0.160 | 6.670 | 43.12 | |
| 3 | +-y(zijde) | 4 | 12.0 | 452.39 | 6.750 | -0.120 | 6.630 | 23.97 | 158) |
| Staaf No.105 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | |

## 3.1 TOEGEPASTE LANGSWAPENING

| Onderde No. | Wapening Positie | Aant. Wap. st | $d_s$ [mm] | $A_s$ [cm$^2$] | Lengte [m] | x-positie [m] van | x-positie [m] tot | Gewicht [kg] | Opm. |
|---|---|---|---|---|---|---|---|---|---|
| 1 | Basis -z (bov) | 4 | 16.0 | 804.25 | 6.720 | -0.160 | 6.560 | 42.43 | |
| 2 | -z (bov) | 2 | 12.0 | 226.19 | 6.640 | -0.120 | 6.520 | 11.79 | |
| 3 | Basis +z (ond) | 4 | 16.0 | 804.25 | 6.720 | -0.160 | 6.560 | 42.43 | |
| 4 | +z (ond) | 2 | 12.0 | 226.19 | 6.640 | -0.120 | 6.520 | 11.79 | |
| 5 | +-y(zijde) | 12 | 12.0 | 1357.17 | 6.640 | -0.120 | 6.520 | 70.74 | 158) |
| Staaf No.108 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | |
| 1 | Basis -z (bov) | 4 | 16.0 | 804.25 | 4.820 | -0.160 | 4.660 | 30.43 | |
| 2 | Basis +z (ond) | 4 | 16.0 | 804.25 | 4.820 | -0.160 | 4.660 | 30.43 | |
| 3 | +-y(zijde) | 6 | 12.0 | 678.58 | 4.740 | -0.120 | 4.620 | 25.25 | 158) |
| Staaf No.109 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | |
| 1 | Basis -z (bov) | 4 | 16.0 | 804.25 | 4.820 | -0.160 | 4.660 | 30.43 | |
| 2 | -z (bov) | 6 | 12.0 | 678.58 | 4.740 | -0.120 | 4.620 | 25.25 | |
| 3 | Basis +z (ond) | 4 | 16.0 | 804.25 | 4.859 | -0.164 | 4.696 | 30.68 | |
| 4 | +z (ond) | 6 | 12.0 | 678.58 | 4.768 | -0.122 | 4.646 | 25.40 | |
| 5 | +-y(zijde) | 6 | 12.0 | 678.58 | 4.740 | -0.120 | 4.620 | 25.25 | 158) |
| Staaf No.110 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | |
| 1 | Basis -z (bov) | 4 | 16.0 | 804.25 | 4.820 | -0.160 | 4.660 | 30.43 | |
| 2 | -z (bov) | 2 | 12.0 | 226.19 | 4.740 | -0.120 | 4.620 | 8.42 | |
| 3 | Basis +z (ond) | 4 | 16.0 | 804.25 | 4.856 | -0.196 | 4.660 | 30.66 | |
| 4 | +z (ond) | 2 | 12.0 | 226.19 | 4.740 | -0.120 | 4.620 | 8.42 | |
| 5 | +-y(zijde) | 6 | 12.0 | 678.58 | 4.740 | -0.120 | 4.620 | 25.25 | 158) |
| Staaf No.111 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | |
| 1 | Basis -z (bov) | 4 | 16.0 | 804.25 | 4.620 | -0.160 | 4.460 | 29.17 | |
| 2 | -z (bov) | 2 | 12.0 | 226.19 | 4.540 | -0.120 | 4.420 | 8.06 | |
| 3 | Basis +z (ond) | 4 | 16.0 | 804.25 | 4.620 | -0.160 | 4.460 | 29.17 | |
| 4 | +z (ond) | 2 | 12.0 | 226.19 | 4.540 | -0.120 | 4.420 | 8.06 | |
| 5 | +-y(zijde) | 12 | 12.0 | 1357.17 | 4.540 | -0.120 | 4.420 | 48.37 | 158) |

## 3.2 TOEGEPASTE AFSCHUIFWAPENING

| Onderde No. | Aant. Beugel | $d_s$ [mm] | Lengte [m] | x-positie [m] van | x-positie [m] tot | h.o.h.-afst $s_{li}$ [m] | Maatvoering beugel [mm] | Aant. Benen | Gewicht [kg] | Opm. |
|---|---|---|---|---|---|---|---|---|---|---|
| Staaf No. 1 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | | |
| 1 | 10 | 10.0 | 2.000 | 0.000 | 2.000 | 0.200 | 760.0/360.0/139.3 | 2 | 17.08 | |
| 2 | 6 | 10.0 | 1.500 | 2.000 | 3.500 | 0.250 | 760.0/360.0/139.3 | 2 | 9.32 | |
| 3 | 9 | 10.0 | 2.700 | 3.500 | 6.200 | 0.300 | 760.0/360.0/139.3 | 2 | 13.97 | |
| 4 | 1 | 10.0 | 0.200 | 6.200 | 6.400 | 0.200 | 760.0/360.0/139.3 | 2 | 1.55 | |
| Staaf No. 2 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | | |
| 5 | 21 | 10.0 | 4.000 | 0.000 | 4.000 | 0.200 | 760.0/360.0/139.3 | 2 | 32.61 | |
| 6 | 1 | 10.0 | 0.250 | 4.000 | 4.250 | 0.250 | 760.0/360.0/139.3 | 2 | 1.55 | |
| 7 | 1 | 10.0 | 0.050 | 4.250 | 4.300 | 0.050 | 760.0/360.0/139.3 | 2 | 1.55 | |
| Staaf No. 3 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | | |
| 8 | 33 | 10.0 | 6.400 | 0.000 | 6.400 | 0.200 | 760.0/360.0/139.3 | 2 | 51.24 | 113) |
| 9 | 1 | 10.0 | 0.130 | 6.400 | 6.530 | 0.130 | 760.0/360.0/139.3 | 2 | 1.55 | 113) |
| Staaf No. 4 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | | |
| 10 | 22 | 10.0 | 4.200 | 0.000 | 4.200 | 0.200 | 760.0/360.0/139.3 | 2 | 34.16 | |
| 11 | 1 | 10.0 | 0.100 | 4.200 | 4.300 | 0.100 | 760.0/360.0/139.3 | 2 | 1.55 | |
| Staaf No. 35 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | | |
| 12 | 22 | 10.0 | 6.300 | 0.000 | 6.300 | 0.300 | 760.0/360.0/139.3 | 2 | 34.16 | 115) |
| 13 | 1 | 10.0 | 0.210 | 6.300 | 6.510 | 0.210 | 760.0/360.0/139.3 | 2 | 1.55 | 115) |
| Staaf No. 36 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | | |
| 14 | 12 | 10.0 | 3.300 | 0.000 | 3.300 | 0.300 | 760.0/360.0/139.3 | 2 | 18.63 | |
| 15 | 4 | 10.0 | 1.000 | 3.300 | 4.300 | 0.250 | 760.0/360.0/139.3 | 2 | 6.21 | |
| 16 | 9 | 10.0 | 1.800 | 4.300 | 6.100 | 0.200 | 760.0/360.0/139.3 | 2 | 13.97 | |
| 17 | 1 | 10.0 | 0.250 | 6.100 | 6.350 | 0.250 | 760.0/360.0/139.3 | 2 | 1.55 | |
| 18 | 1 | 10.0 | 0.180 | 6.350 | 6.530 | 0.180 | 760.0/360.0/139.3 | 2 | 1.55 | |
| Staaf No. 39 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | | |
| 19 | 23 | 10.0 | 4.400 | 0.000 | 4.400 | 0.200 | 760.0/360.0/139.3 | 2 | 35.71 | 113) |
| 20 | 1 | 10.0 | 0.100 | 4.400 | 4.500 | 0.100 | 760.0/360.0/139.3 | 2 | 1.55 | 113) |
| Staaf No. 40 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | | |
| 21 | 16 | 10.0 | 4.500 | 0.000 | 4.500 | 0.300 | 760.0/360.0/139.3 | 2 | 24.84 | 115) |
| Staaf No. 41 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | | |
| 22 | 15 | 10.0 | 4.500 | 0.000 | 4.500 | 0.300 | 760.0/360.0/139.3 | 2 | 24.84 | |
| Staaf No. 42 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | | |
| 23 | 11 | 10.0 | 2.200 | 0.000 | 2.200 | 0.200 | 760.0/360.0/139.3 | 2 | 17.08 | |
| 24 | 8 | 10.0 | 1.200 | 2.200 | 3.400 | 0.150 | 760.0/360.0/139.3 | 2 | 12.42 | |
| 25 | 4 | 10.0 | 0.800 | 3.400 | 4.200 | 0.200 | 760.0/360.0/139.3 | 2 | 6.21 | |
| 26 | 1 | 10.0 | 0.100 | 4.200 | 4.300 | 0.100 | 760.0/360.0/139.3 | 2 | 1.55 | |
| Staaf No. 104 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | | |
| 27 | 22 | 10.0 | 6.300 | 0.000 | 6.300 | 0.300 | 760.0/360.0/139.3 | 2 | 34.16 | 115) |
| 28 | 1 | 10.0 | 0.210 | 6.300 | 6.510 | 0.210 | 760.0/360.0/139.3 | 2 | 1.55 | 115) |
| Staaf No. 105 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | | |
| 29 | 33 | 10.0 | 6.400 | 0.000 | 6.400 | 0.200 | 760.0/360.0/139.3 | 2 | 51.24 | |
| Staaf No. 108 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | | |
| 30 | 23 | 10.0 | 4.400 | 0.000 | 4.400 | 0.200 | 760.0/360.0/139.3 | 2 | 35.71 | 113) |
| 31 | 1 | 10.0 | 0.100 | 4.400 | 4.500 | 0.100 | 760.0/360.0/139.3 | 2 | 1.55 | 113) |
| Staaf No. 109 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | | |
| 32 | 3 | 10.0 | 0.500 | 0.000 | 0.500 | 0.250 | 760.0/360.0/139.3 | 2 | 4.66 | |
| 33 | 13 | 10.0 | 3.900 | 0.500 | 4.400 | 0.300 | 760.0/360.0/139.3 | 2 | 20.19 | |
| 34 | 1 | 10.0 | 0.100 | 4.400 | 4.500 | 0.100 | 760.0/360.0/139.3 | 2 | 1.55 | |
| Staaf No. 110 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | | |
| 35 | 16 | 10.0 | 4.500 | 0.000 | 4.500 | 0.300 | 760.0/360.0/139.3 | 2 | 24.84 | 115) |
| Staaf No. 111 - Rib VLU 800/0/0/200/0/400 | | | | | | | | | | |
| 36 | 22 | 10.0 | 4.200 | 0.000 | 4.200 | 0.200 | 760.0/360.0/139.3 | 2 | 34.16 | |
| 37 | 1 | 10.0 | 0.100 | 4.200 | 4.300 | 0.100 | 760.0/360.0/139.3 | 2 | 1.55 | |

## 4.1 BRUIKBAARHEIDSCONTROLE PER DOORSNEDE

| Prof. No. | Locatie x [m] | Belasting | Ontwerp Type | Aanwezige waar | Grenswaarde | Eenheid | Capaciteit | Opm. |
|---|---|---|---|---|---|---|---|---|
| Doorsnede No.1 - Rechthoek 400/600 | | | | | | | | |
| 109 | 2.500 | BC800 | $A_{s,min}$ | 1709.03 | 1381.90 | $mm^2$ | 0.81 | |
| 1 | 0.000 | BC704 | $w_k$ | 0.000 | 0.200 | mm | 0.00 | |

## OPM.

| No. | Omschrijving |
|---|---|
| 13) | Symmetrische wapening voor dubbele buiging |
| 25) | Min. wapening voor drukwapening volgens 9.5.2(2) |
| 26) | Min. wapening voor liggers - Bovenin volgens 9.2.1.1(1) |
| 27) | Min. wapening voor liggers - Onderin volgens 9.2.1.1(1) |
| 28) | Bovenwapening is verhoogd t.g.v. BGT-eis |
| 29) | Onderwapening is verhoogd t.g.v. BGT-eis |
| 58) | Gebruik maken van de gemiddelde waarde van hefboom z |
| 69) | Min. afschuifwapening volgens 9.2.2.(5) |
| 113) | Min. afschuifwapening voor drukstaven volgens 9.5.3 |
| 115) | Min. afschuifwapening voor liggers volgens 9.2.2 |
| 158) | Wringwapening verdeeld over de omtrek |

## 1.1 GLOBALE GEGEVENS

| | | |
|---|---|---|
| Activiteiten | ☒ Modale berekening (eigenvectoren)<br>☒ Massa-combinaties<br>☐ Opgelegde trillingen<br>☐ Responsspectra<br>☐ Accelerogrammen<br>☐ Tijddiagrammen<br>☒ Equivalente statische kracht berekening | |
| Instelling | Zwaartekrachtversnelling | : 10.00 m/s² |

## 1.2.1 MASSA-GEVAL - ALGEMEEN

| No. | Beschrijving massa-geval | Parameters | |
|---|---|---|---|
| MG1 | PB: BG10+BG20+BG30+BG40 | Type massa-geval<br>Massa's | : Blijvend<br>☒ : Vanuit kracht componenten van Belastingscombinatie BC480 |
| MG5 | VB: BG130 | Type massa-geval<br>Massa's | : Opgelegd - categorie E<br>☒ : Vanuit kracht componenten van Belastingsgeval BG130-VB: Zonnepanelen |
| MG6 | VB: BG140 | Type massa-geval<br>Massa's | : Opgelegd - categorie E<br>☒ : Vanuit kracht componenten van Belastingsgeval BG140-VB: Stellingen - Pallet |
| MG7 | VB: BG150 | Type massa-geval<br>Massa's | : Opgelegd - categorie E<br>☒ : Vanuit kracht componenten van Belastingsgeval BG150-VB: Heftruck |

## 1.3.1 MASSA-COMBINATIES - ALGEMEEN

| No. | Beschrijving massa-combinatie | Parameters | | | |
|---|---|---|---|---|---|
| MC1 | Massa Combinatie | Massa-gevallen | : | 1.00 | MG1 - PB: BG10+BG20+BG30+BG40 |
| | | | | 0.80 | MG5 - VB: BG130 |
| | | | | 0.80 | MG6 - VB: BG140 |
| | | | | 0.80 | MG7 - VB: BG150 |
| | | Commentaar | : | | |

## 1.4.1 NATUURLIJK TRILLINGSGEVAL - ALGEMEEN

| EWG Geval | Eigentrillingsgeval beschrijving | Parameters | | |
|---|---|---|---|---|
| EWG1 | Natuurlijke trillingsgevallen | Aantal van kleinste eigenwaardes | : | 10 |
| | | Inwerkende massa's | : | MC1 - Massa Combinatie |
| | | Massa's beschouwd in | : | ☒ X-richting<br>☒ Y-richting |

## 1.4.2. NATUURLIJK TRILLINGSGEVAL - BEREKENING PARAMTERS

| EWG Geval | Eigentrillingsgeval beschrijving | Berekeningsparameters | | |
|---|---|---|---|---|
| EWG1 | Natuurlijke trillingsgevallen | Type massamatrix: | : | Diagonale matrix (translatie DOFs) |
| | | Schalen van trillingseigenvormen | : | Max $\{u_j\} = 1$ |
| | | Oplossingsmethode voor eigenwaardes | : | Lanczos |

## 1.5.1 RESPONSE SPECTRA - ALGEMEEN

| RS Geval | Responsspectra beschrijving | Definitie-type | Commentaar |
|---|---|---|---|
| RS1 | Responsspectra | Volgens norm:<br>EN 1998-1:2010 - Europese Unie<br>Nationale Bijlage:<br>NBN - Belgiï¿½ | |

## 1.5.2 RESPONSSPECTRA - NORMPARAMETERS

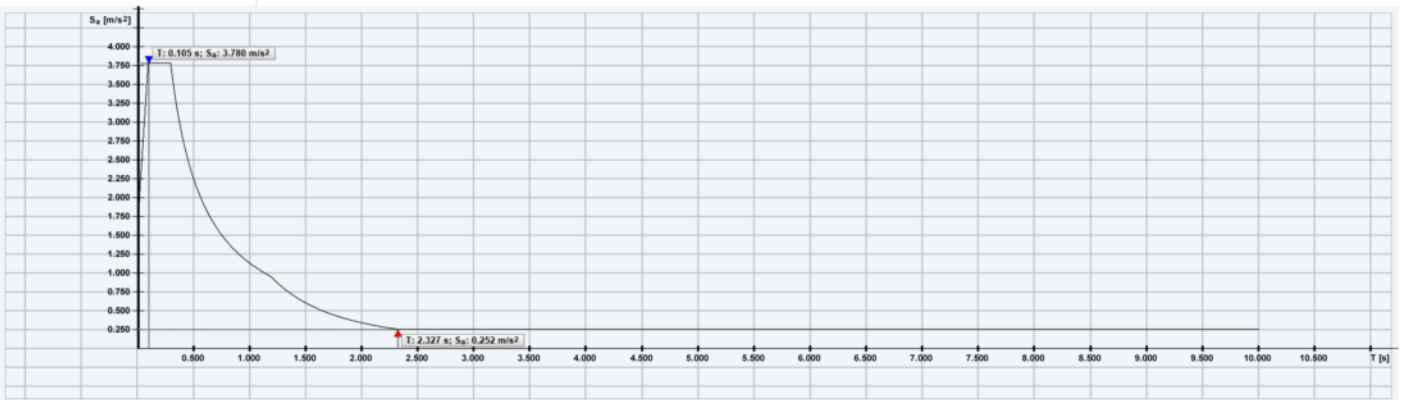
| No. | Responsspectrum beschrijving | Massa-geval parameters | | | |
|---|---|---|---|---|---|
| RS1 | Responsspectra | Type spectrum | | | |
| | | Type spectrum | | : | Ontwerp spectrum voor lineaire berekening |
| | | Type spectrum | | : | 2 |
| | | Spectrumrichting | | : | Horizontaal spectrum |
| | | Aardbevingsactie | | | |
| | | Piekwaarde grondversnelling | PGA | : | 0.150 |
| | | Referentie piek-grondversnelling | $a_{gR}$ | : | 1.0500 |
| | | Belangcategorie | | : | III |
| | | Belangfactor | $\gamma_I$ | : | 1.2000 |
| | | Ontwerp grondversnelling | $a_g$ | : | 1.2600 |
| | | Parameter voor de omschrijving van het responsspectrum | | | |
| | | Bodemtype | | : | D |
| | | Bodemfactor | S | : | 1.8000 |

## 1.5.2 RESPONSSPECTRA - NORMPARAMETERS

| No. | Responsspectrum beschrijving | Massa-geval parameters | | | |
|---|---|---|---|---|---|
| | | Ondergrens van vlak van constante spectrale versnelling (horizontaal) | $T_{B-H}$ | : | 0.1000 |
| | | Bovengrens van vlak van constante spectrale versnelling (horizontaal) | $T_{C-H}$ | : | 0.3000 |
| | | Waarde definieert het begin van het vlak van constante spectrum verplaatsingen (horizontaal) | $T_{D-H}$ | : | 1.2000 |
| | | Factoren | | | |
| | | Gedragsfactor | q | : | 1.5000 |
| | | Grenswaarde voor horizontale ontwerp spectrum | β | : | 0.2000 |

## 1.5.3.1 RESPONSSPECTRA - GRAFIEK

RS1




## 1.8.1 DYNAMISCHE BELASTINGSGEVAL - ALGEMEEN

| DBG Geval | Dynamische belastingsgevallen beschrijving | Parameters | | |
|---|---|---|---|---|
| DBG1 | Dynamische Belastingsgeval | Type methode | : | Equivalente statische kracht berekening (responsspectrum vereist) |
| | | Natuurlijke trilling toewijzen | : | Eigentrillingsgeval: Natuurlijke trillingsgevallen |

## 1.8.5.1 DYNAMISCHE BELASTINGSGEVALLEN - EQUIVALENTE STATISCHE KRACHT BEREKENING

| DBG Geval | Dynamische belastingsgevallen beschrijving | Parameters |
|---|---|---|
| DBG1 | Dynamische Belastingsgeval | Reactiespectrum toewijzen:<br><br>Responsspectrum in richting — Vergrotingsfactor<br>☒ x: RS1 - Responsspectra — 1.000<br>☒ y: RS1 - Responsspectra — 1.000<br><br>Roteer $a_X$ $a_Y$ om Z: — $\alpha$ = 0.00 [°] |
| | | Instellingen:<br><br>☐ Beschouw buitengewone torsie acties: |
| | | Te genereren:<br><br>☒ Belastingsgeval met $E_{X,i}$ / $E_{Z,i}$ vanuit alle modale vormen<br>Nummer van eerst gegenereerd belastingsgeval: 800<br>☒ Resultaatcombinaties(modale combinatie)<br>Aantal van eerst gegenereerde resultaat combinatie: 10<br>☒ Combinatie van richtingscomponenten met<br>☐ SRSS<br>☒ 100 / 30 %<br>☐ 100 / 40 % |
| | | Combinatie regels:<br><br>Combinatieregel modale respons:<br>☒ SRSS<br>☐ CQC<br><br>Opties<br>☒ Gebruik equivalente lineaire combinatie<br><br>☐ Gemerkte resultaten m.b.v. dominante modus |

## 1.8.5.2 DYNAMISCHE BELASTINGSGEVALLEN - EQUIVALENT STATISCHE KRACHT BEREKENING- TE GENEREREN EIGENVORMEN

| DBG Geval | Dynamische belastingsgevallen beschrijving | Vorm No. | Te generer | Nat. frequentie ω [rad/s] | Nat. frequentie f [Hz] | Periode T [s] | Versnelling $S_a$ [m/s²] |
|---|---|---|---|---|---|---|---|
| DBG1 | Dynamische Belastingsgeval | 1 | ☒ | 18.625 | 2.964 | 0.337 | 3.361 |
| | | 2 | ☒ | 19.360 | 3.081 | 0.325 | 3.494 |
| | | 3 | ☐ | 19.980 | 3.180 | 0.314 | 3.606 |
| | | 4 | ☒ | 26.865 | 4.276 | 0.234 | 3.780 |
| | | 5 | ☒ | 27.298 | 4.345 | 0.230 | 3.780 |
| | | 6 | ☐ | 37.050 | 5.897 | 0.170 | 3.780 |
| | | 7 | ☐ | 40.107 | 6.383 | 0.157 | 3.780 |
| | | 8 | ☐ | 40.646 | 6.469 | 0.155 | 3.780 |
| | | 9 | ☐ | 40.966 | 6.520 | 0.153 | 3.780 |
| | | 10 | ☐ | 41.398 | 6.589 | 0.152 | 3.780 |

**EWG1**
Natuurlijke trillingsgevallen

## 5.7 EFFECTIEVE MODALEMASSAFACTOREN

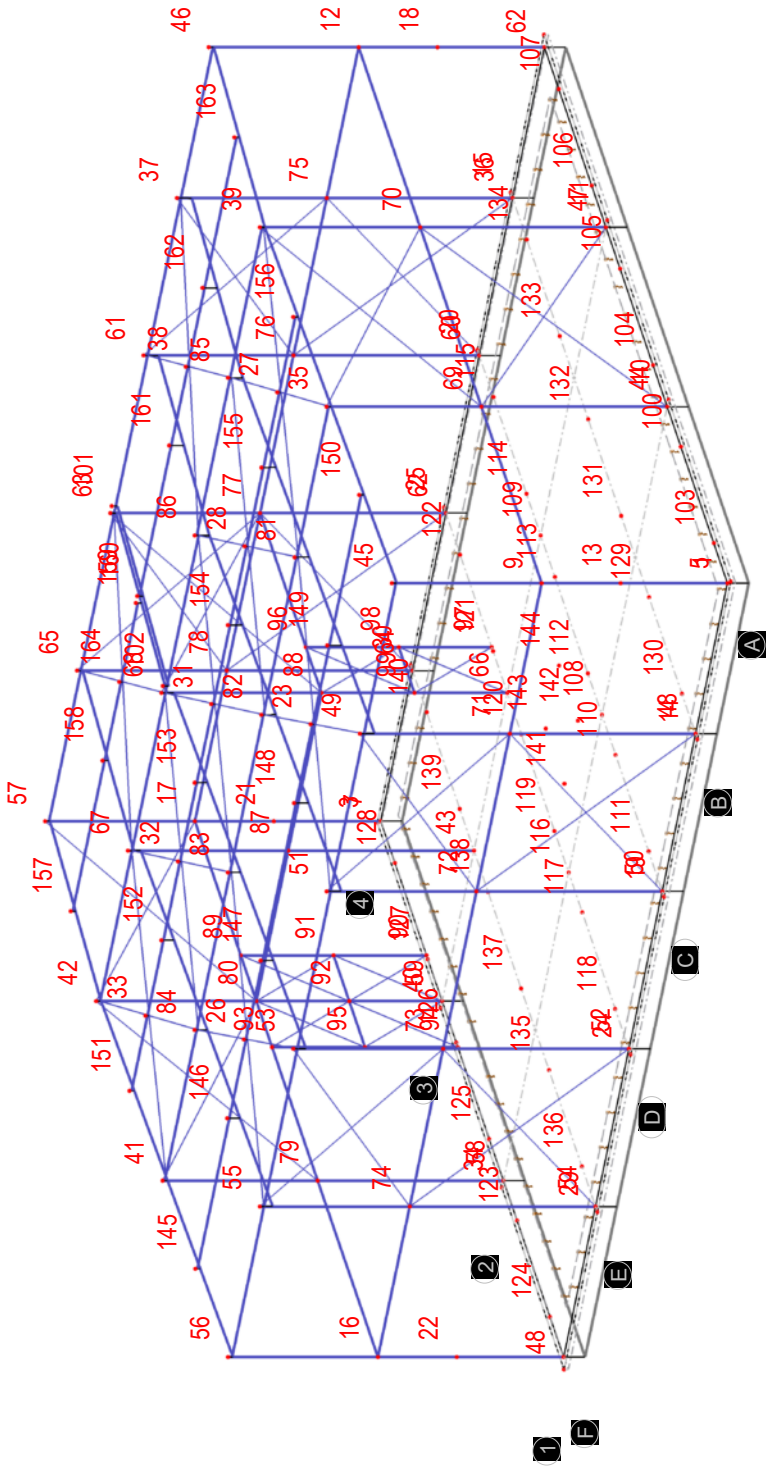
EWG1

| Vorm No. | Modale Ma $M_i$ [kg] | Effectieve modale massa $m_{eX}$ [kg] | $m_{eY}$ [kg] | $m_{eZ}$ [kg] | $m_{\varphi X}$ [kg.m²] | $m_{\varphi Y}$ [kg.m²] | $m_{\varphi Z}$ [kg.m²] | Effectieve modale massafactor $f_{meX}$ [-] | $f_{meY}$ [-] | $f_{meZ}$ [-] |
|---|---|---|---|---|---|---|---|---|---|---|
| 1 | 81689.69 | 456544.38 | 2936.21 | 0.00 | 13671.77 | 2118703.35 | 1549336.81 | 0.530 | 0.003 | 0.000 |
| 2 | 69735.79 | 2270.38 | 526173.93 | 0.00 | 1768175.17 | 7348.18 | 519395.25 | 0.003 | 0.611 | 0.000 |
| 3 | 161827.06 | 15016.04 | 3905.63 | 0.00 | 6436.53 | 31101.23 | 75950429.81 | 0.017 | 0.005 | 0.000 |
| 4 | 199594.40 | 386048.94 | 1768.47 | 0.00 | 12334.62 | 2582059.99 | 118420.09 | 0.448 | 0.002 | 0.000 |
| 5 | 78491.47 | 1245.34 | 325873.35 | 0.00 | 2823775.69 | 10297.54 | 44557.12 | 0.001 | 0.378 | 0.000 |
| 6 | 16267.97 | 508.87 | 232.86 | 0.00 | 18225.10 | 46051.17 | 1495903.01 | 0.001 | 0.000 | 0.000 |
| 7 | 745.77 | 0.04 | 390.14 | 0.00 | 2524.85 | 0.13 | 3760.56 | 0.000 | 0.000 | 0.000 |
| 8 | 3083.94 | 2.27 | 64.55 | 0.00 | 13073.68 | 525.14 | 15276.59 | 0.000 | 0.000 | 0.000 |
| 9 | 4088.05 | 4.49 | 19.08 | 0.00 | 6907.12 | 806.99 | 116.97 | 0.000 | 0.000 | 0.000 |
| 10 | 5312.75 | 3.88 | 38.94 | 0.00 | 13747.09 | 591.14 | 10804.83 | 0.000 | 0.000 | 0.000 |
| Som | 620836.89 | 861644.63 | 861403.17 | 0.00 | 4678871.63 | 4797484.87 | 79708001.04 | 1.000 | 1.000 | 0.000 |

## INHOUD

## KNOOPNUMMERING

Isometrisch

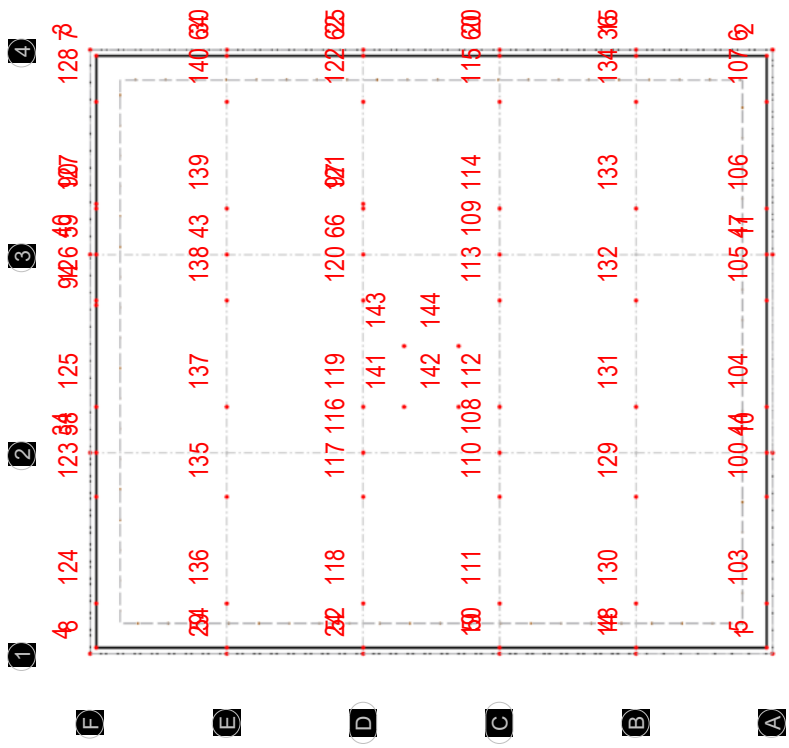


Knoopnummering

## KNOOPNUMMERING BEGANE GROND

Tegen Z-richting in

4981 mm

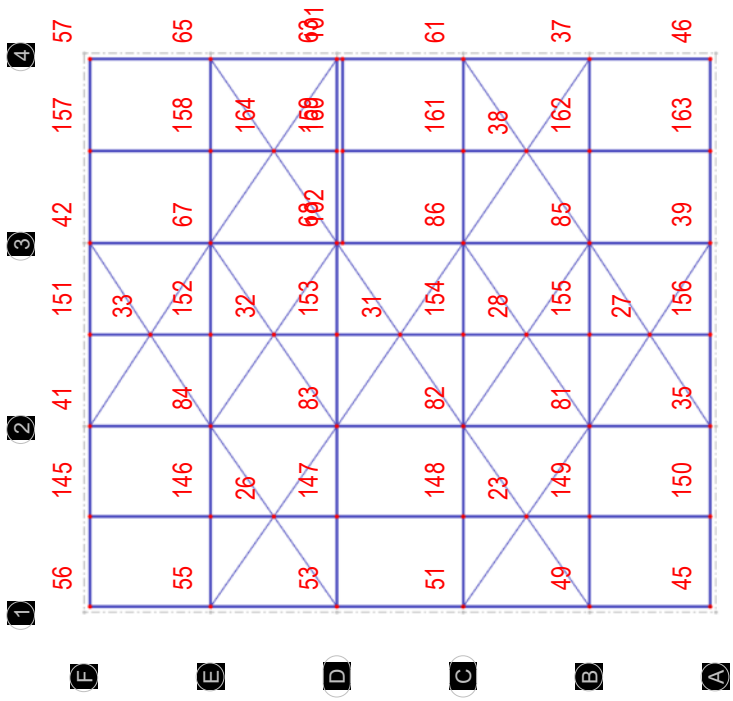



Knoopnummering

## KNOOPNUMMERING DAK

Tegen Z-richting in

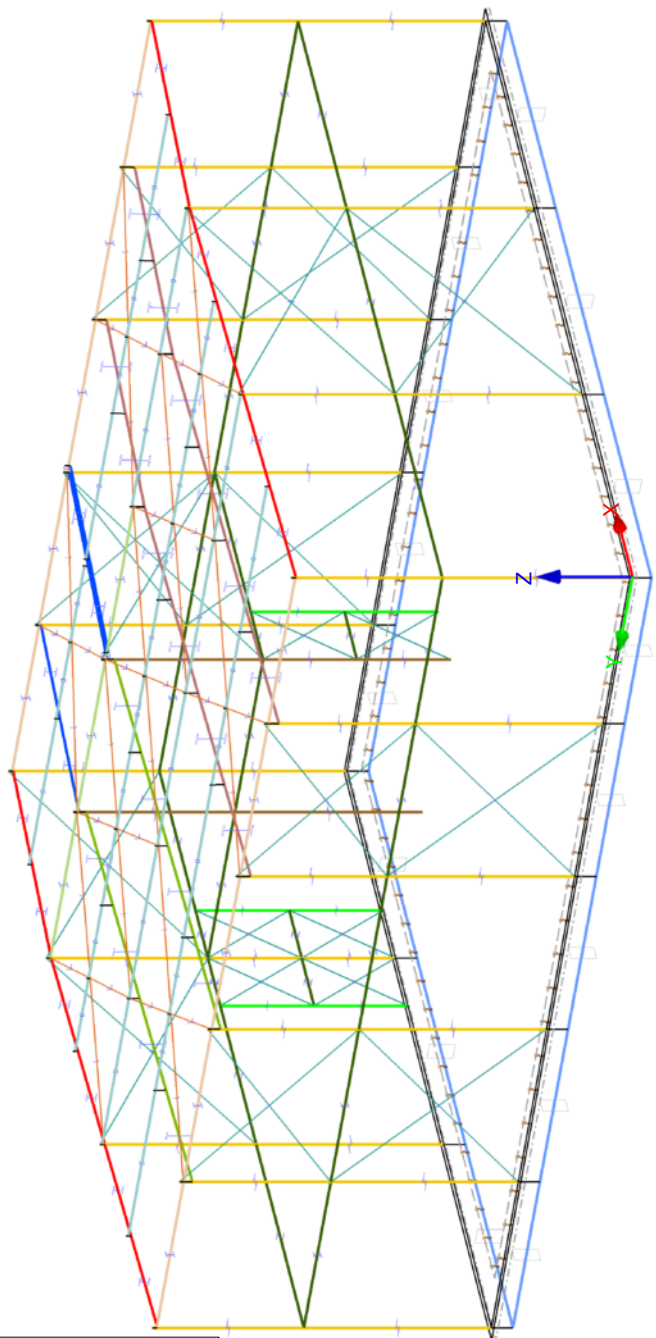
5382 mm




Knoopnummering

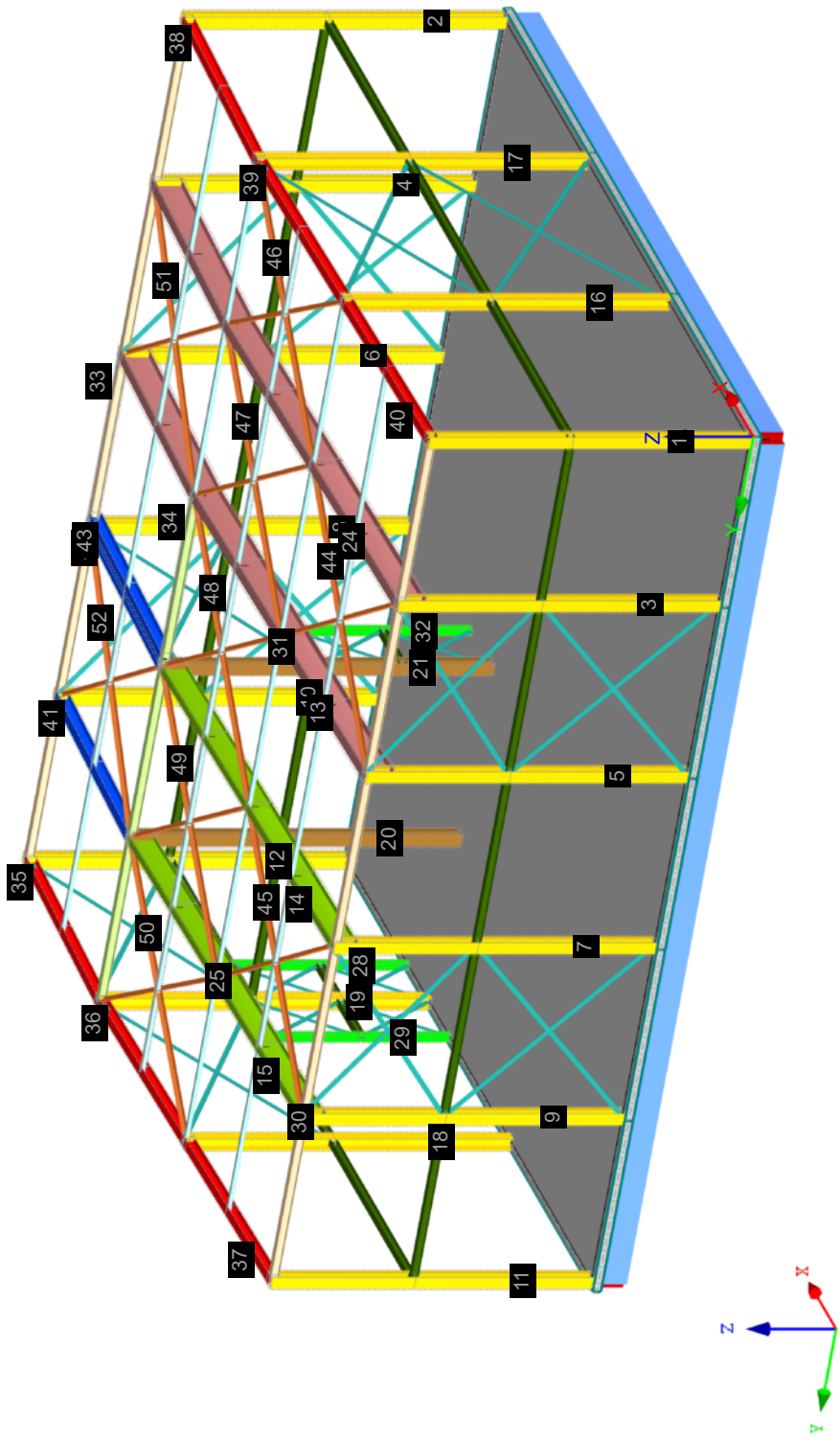
## DOORSNEDES

Isometrisch



## STAAFVERZAMELING

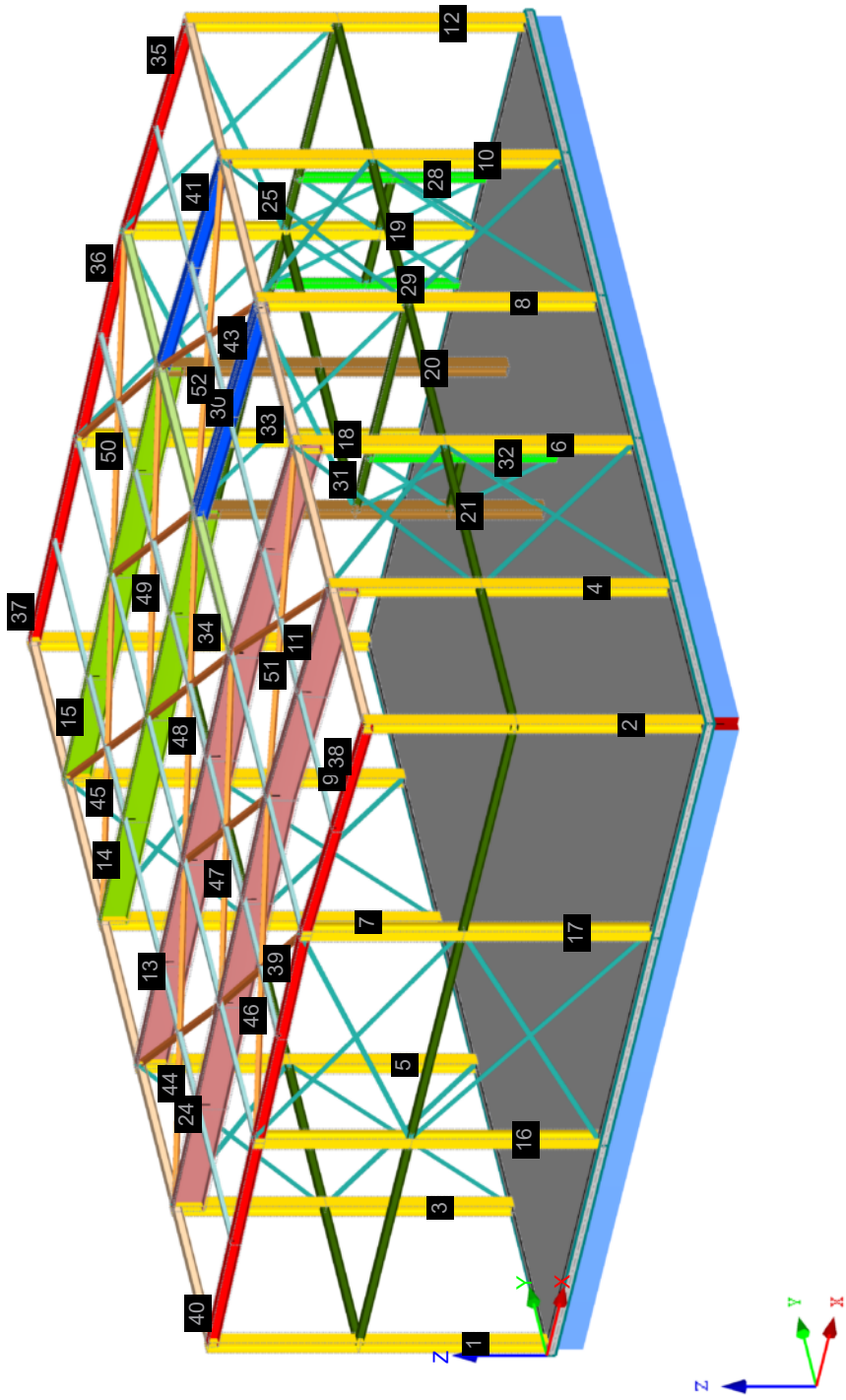
Isometrisch




Nummering staafverz.

## STAAFVERZAMELING

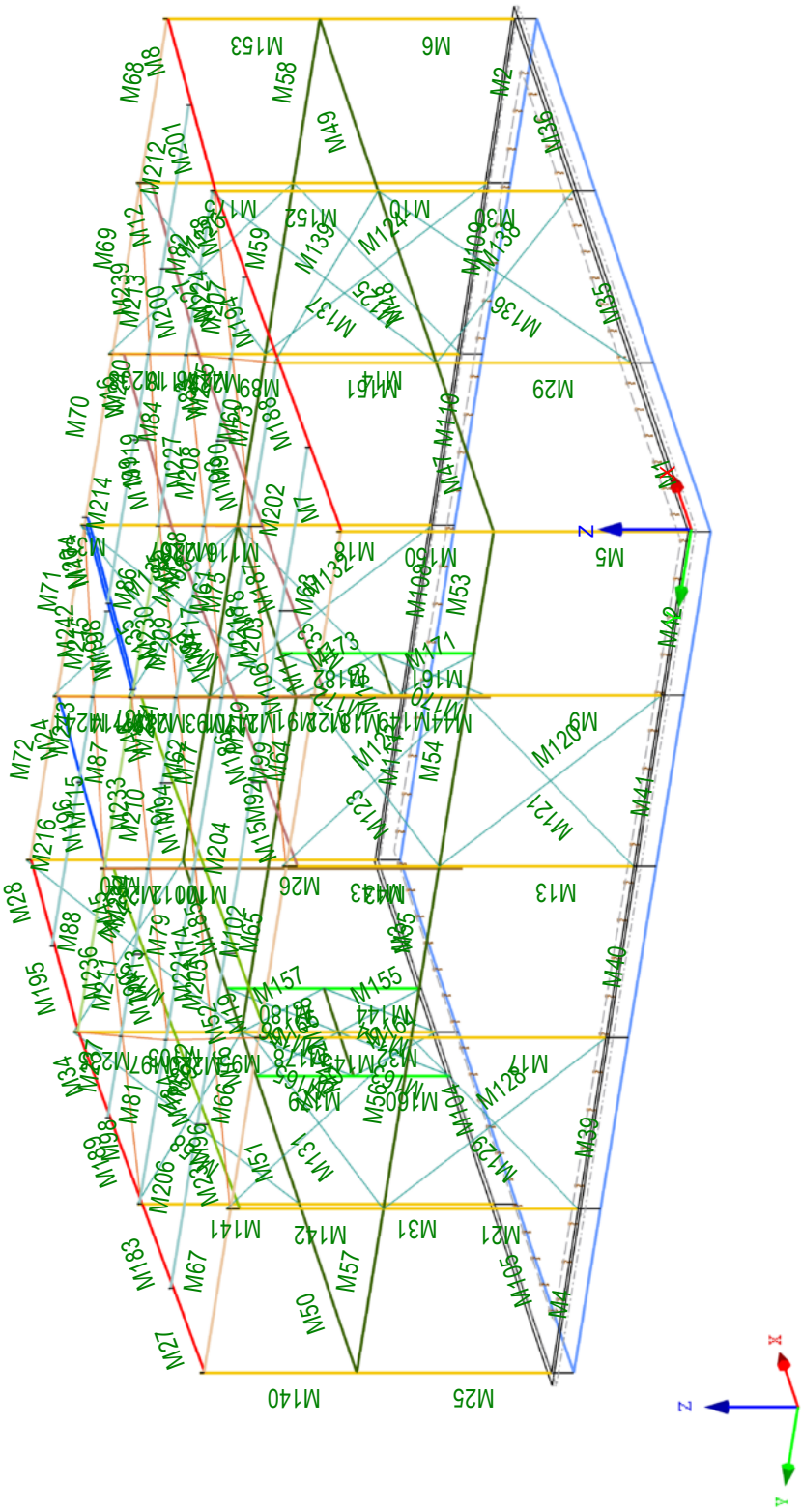
Isometrisch




Nummering staafverz.

## STAVEN

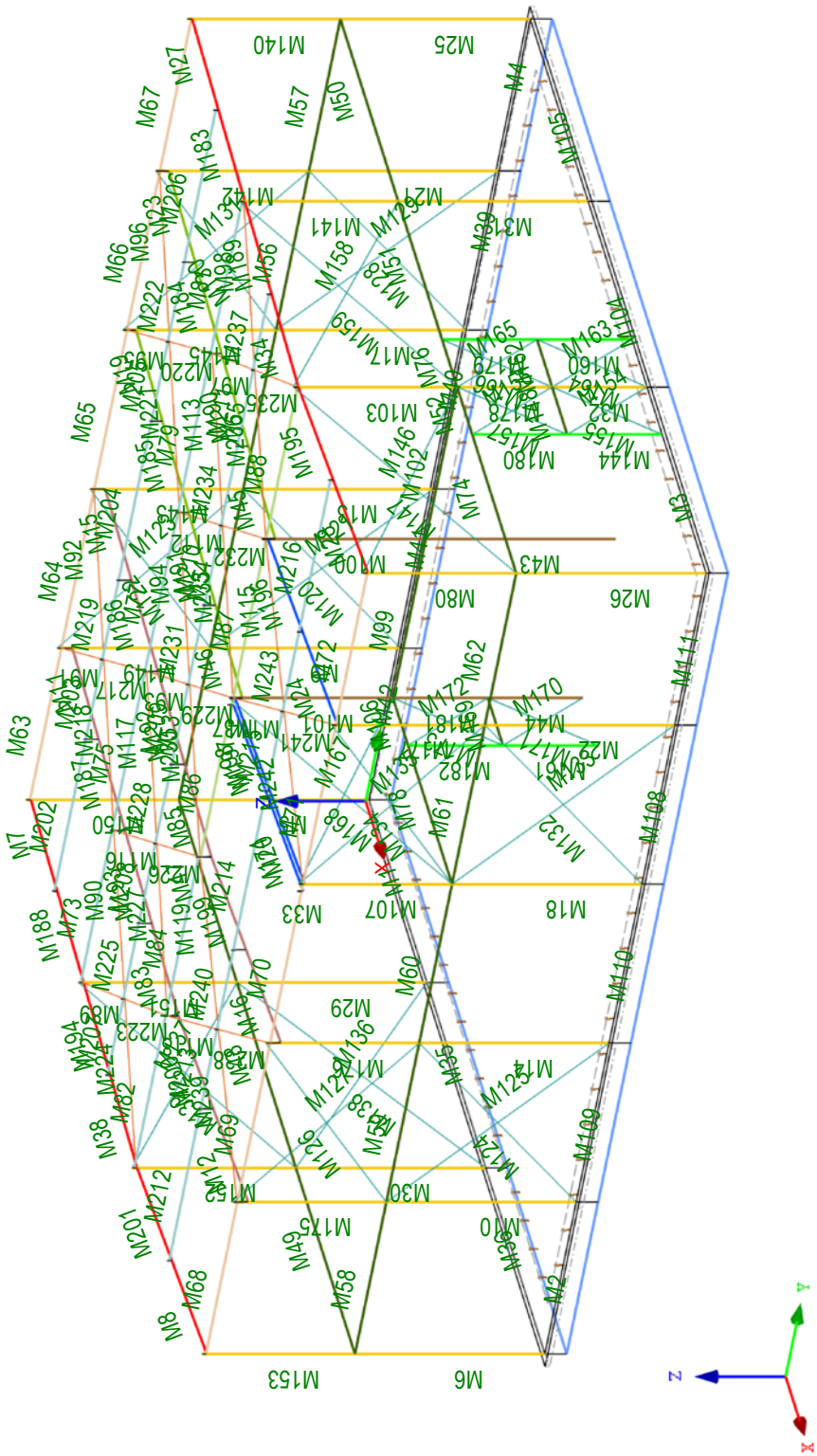
Isometrisch



Staafnummering

## STAVEN

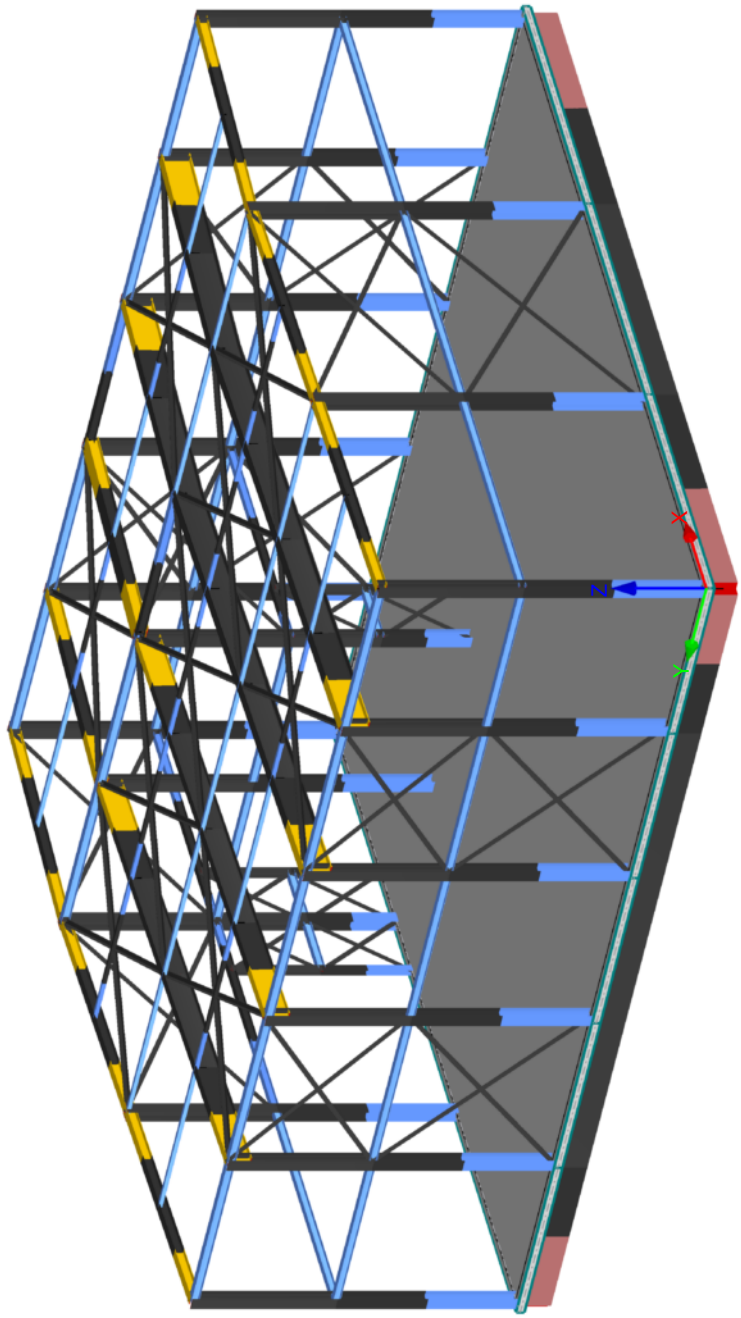
Isometrisch



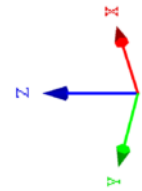
Staafnummering

## STAAFEINDSCHARNIEREN

Isometrisch

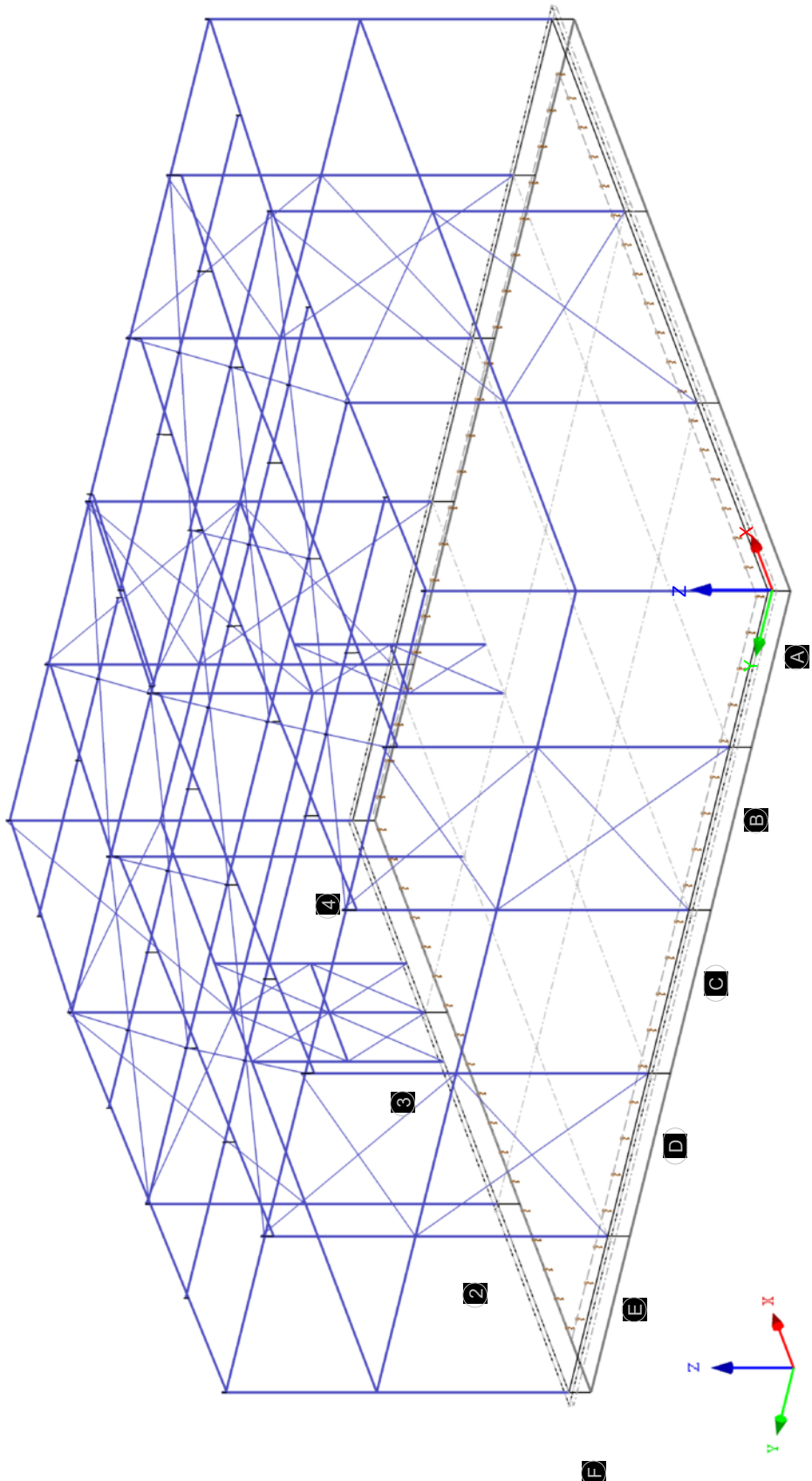


Staafeindscharnieren
1: Lokaal; NNN
2: Lokaal; NNN
3: Lokaal; NNN



## BG10: PB: EIGEN GEWICHT

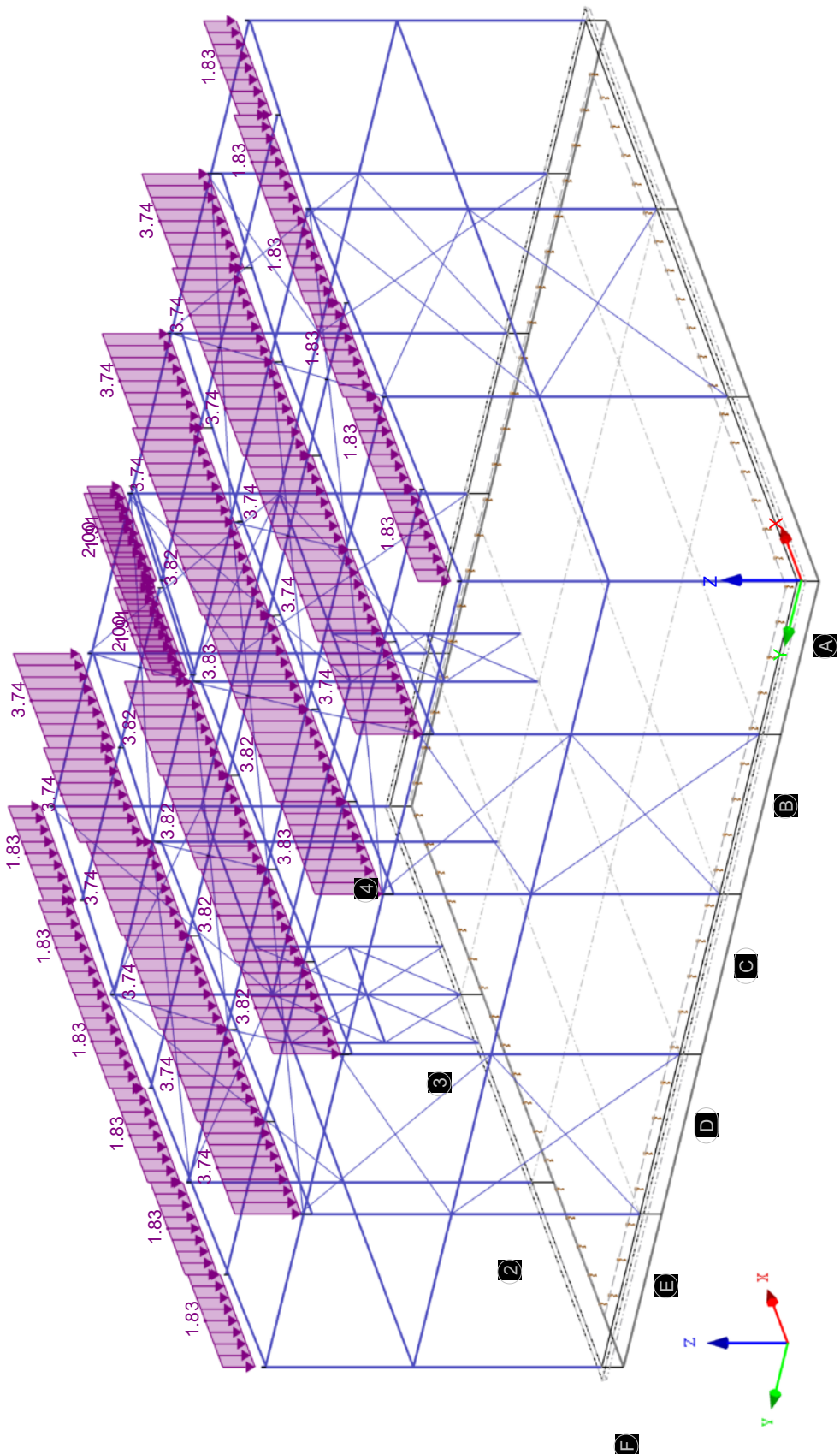
Isometrisch




BG10 : PB: Eigen Gewicht

## BG20: PB: DAKBEDEKKING

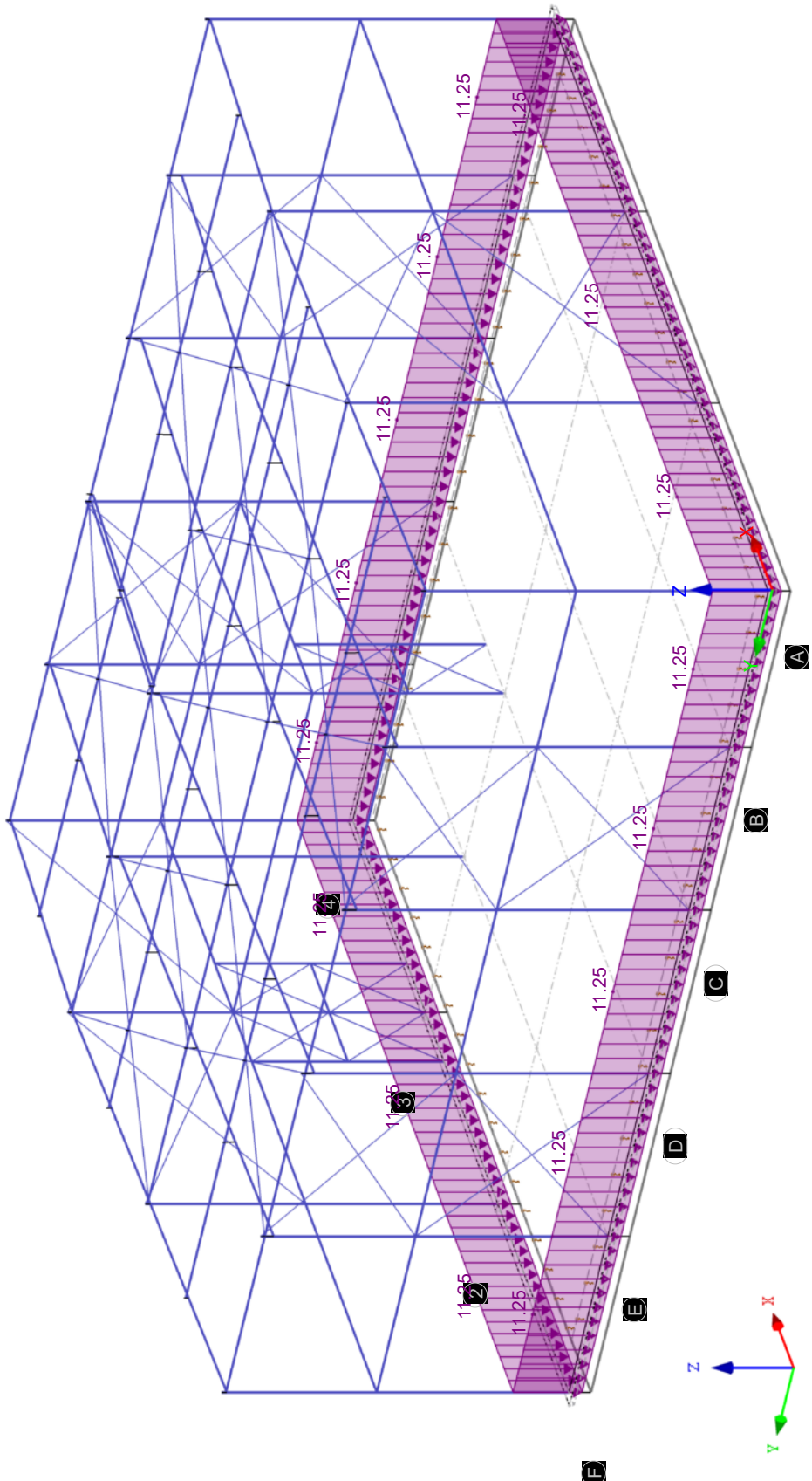
Isometrisch




BG20 : PB: Dakbedekking
Belastingen [kN/m]

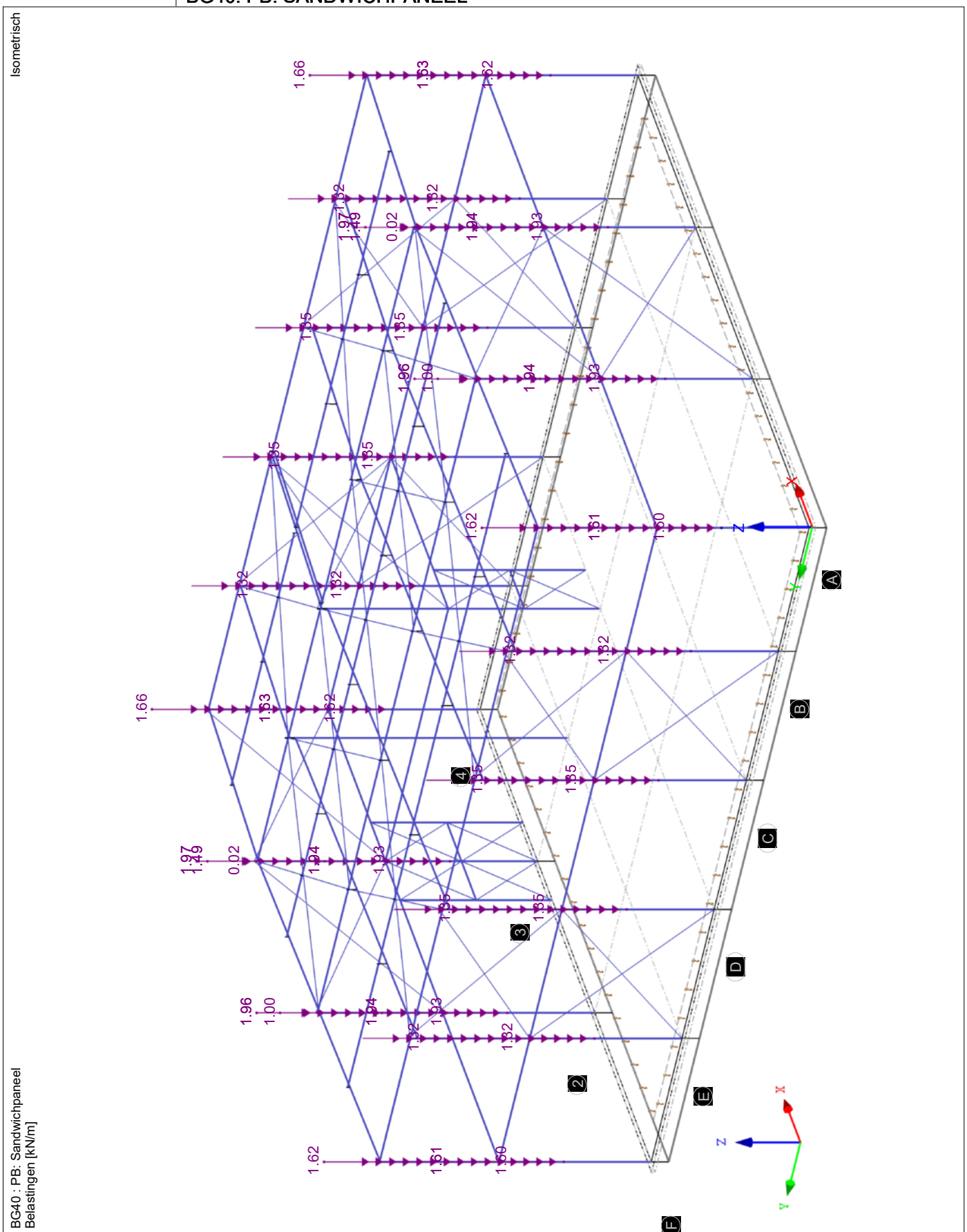
## BG30: PB: KSZ - METSELWERK

Isometrisch



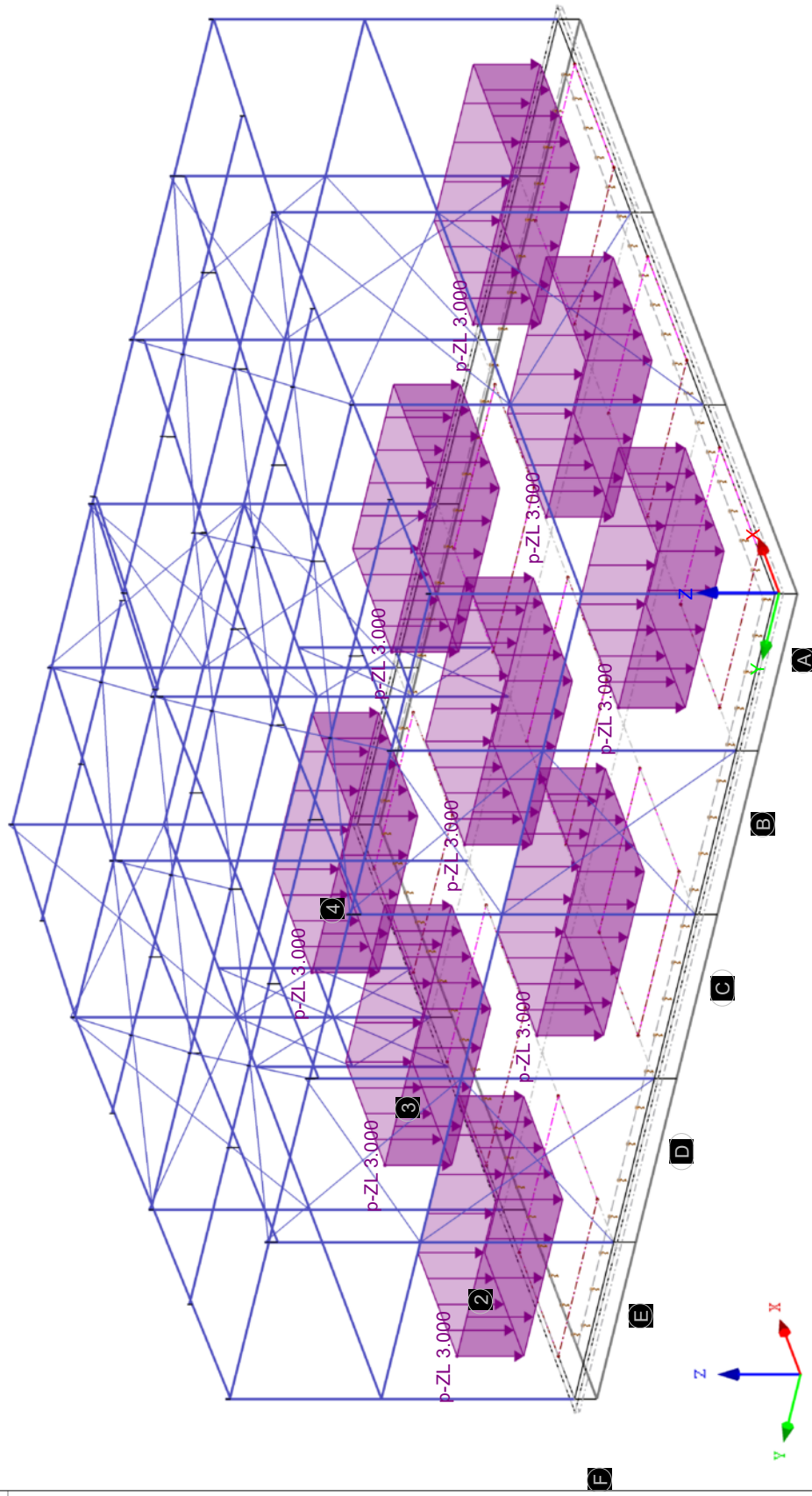

BG30 : PB: KSZ - Metselwerk
Belastingen [kN/m]

## BG40: PB: SANDWICHPANEEL



## BG100: VB: OPGELEGDE BELASTING OP VLOEREN 1

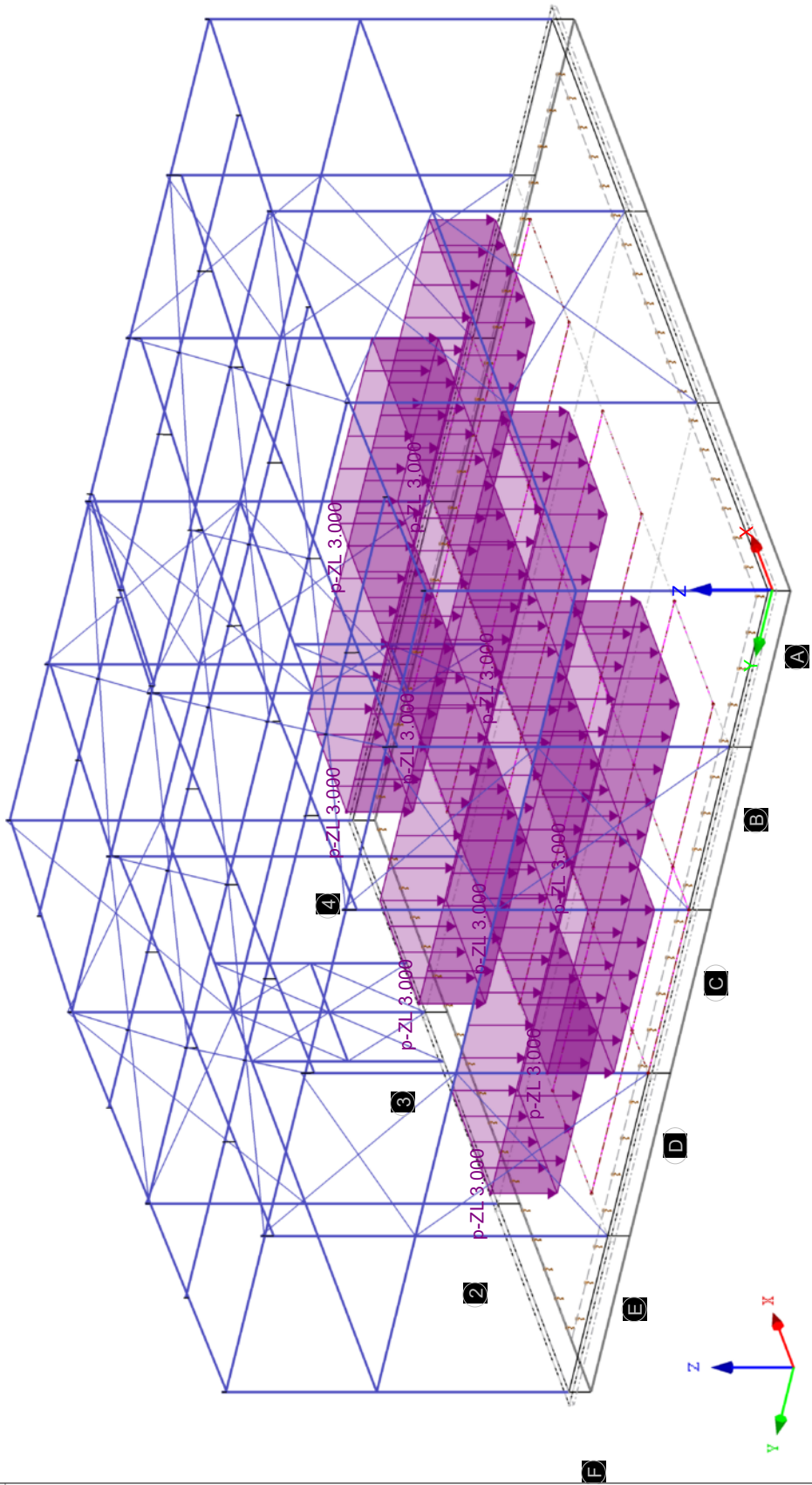
Isometrisch




BG100 : VB: Opgelegde belasting op vloeren 1
Belastingen [kN/m^2]

## BG110: VB: OPGELEGDE BELASTING OP VLOEREN 2

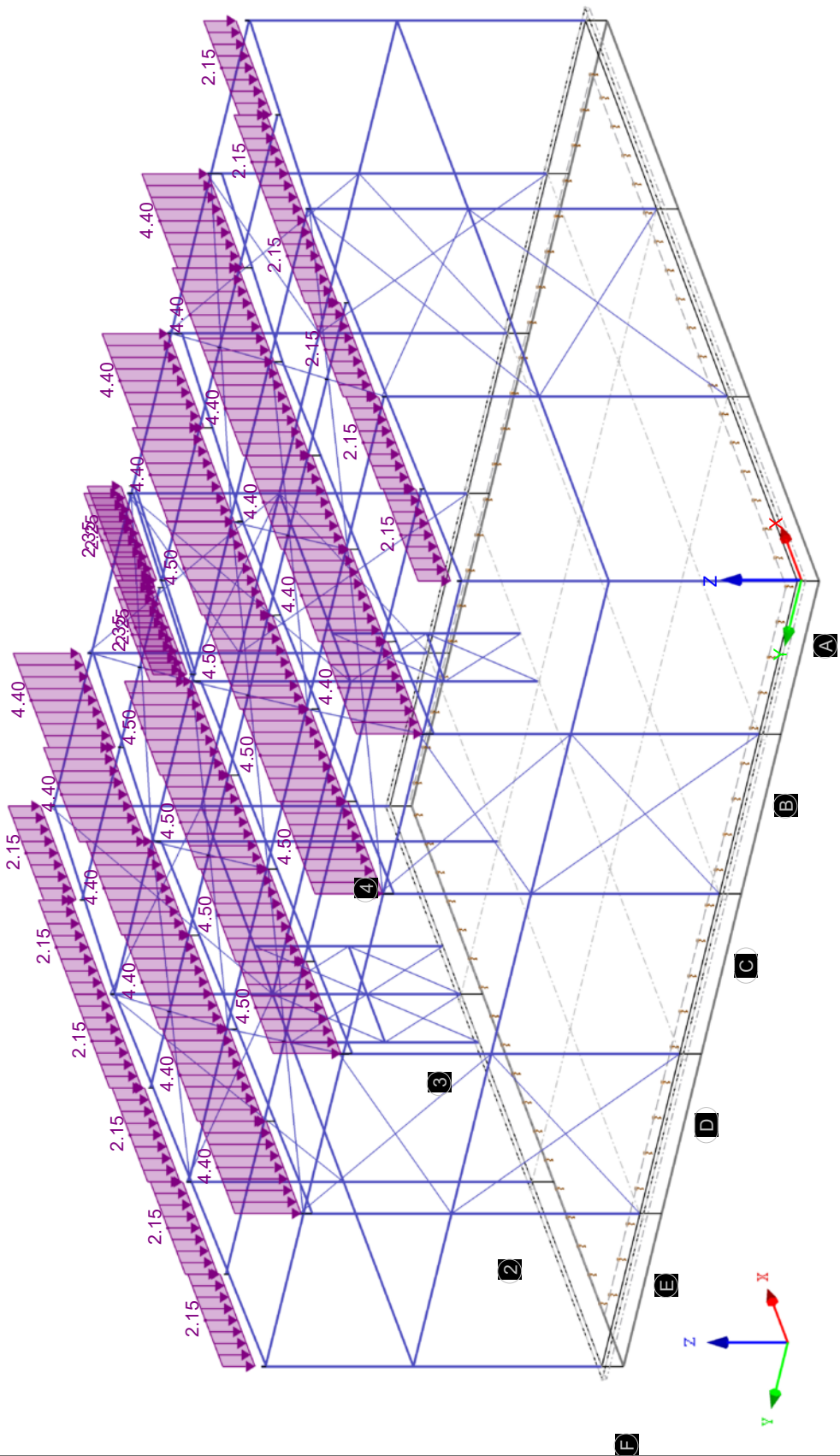
Isometrisch




BG110 : VB: Opgelegde belasting op vloeren 2
Belastingen [kN/m^2]

## BG120: VB: DAKBELASTING

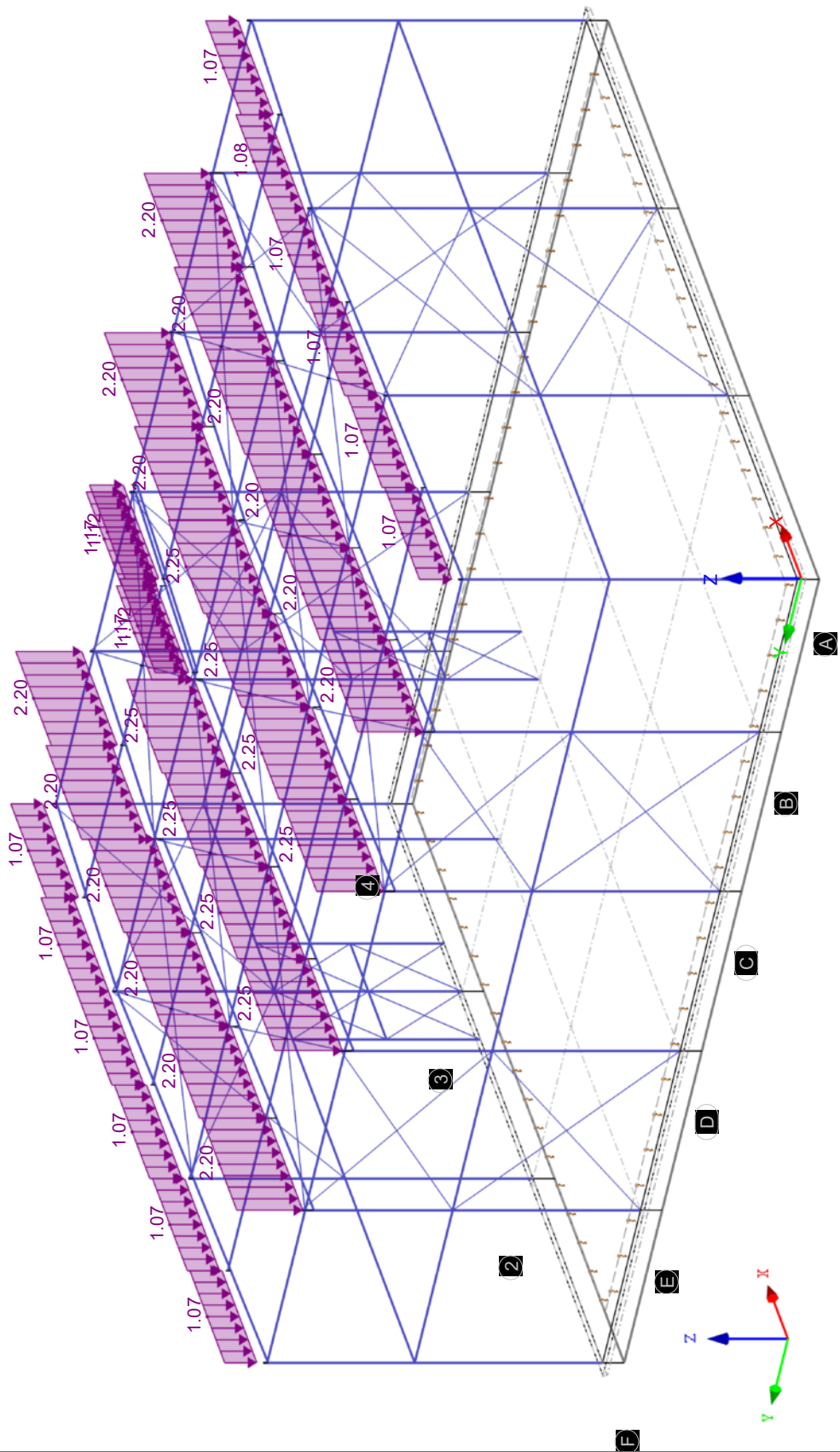
Isometrisch




BG120 : VB: Dakbelasting
Belastingen [kN/m]

## BG130: VB: ZONNEPANELEN

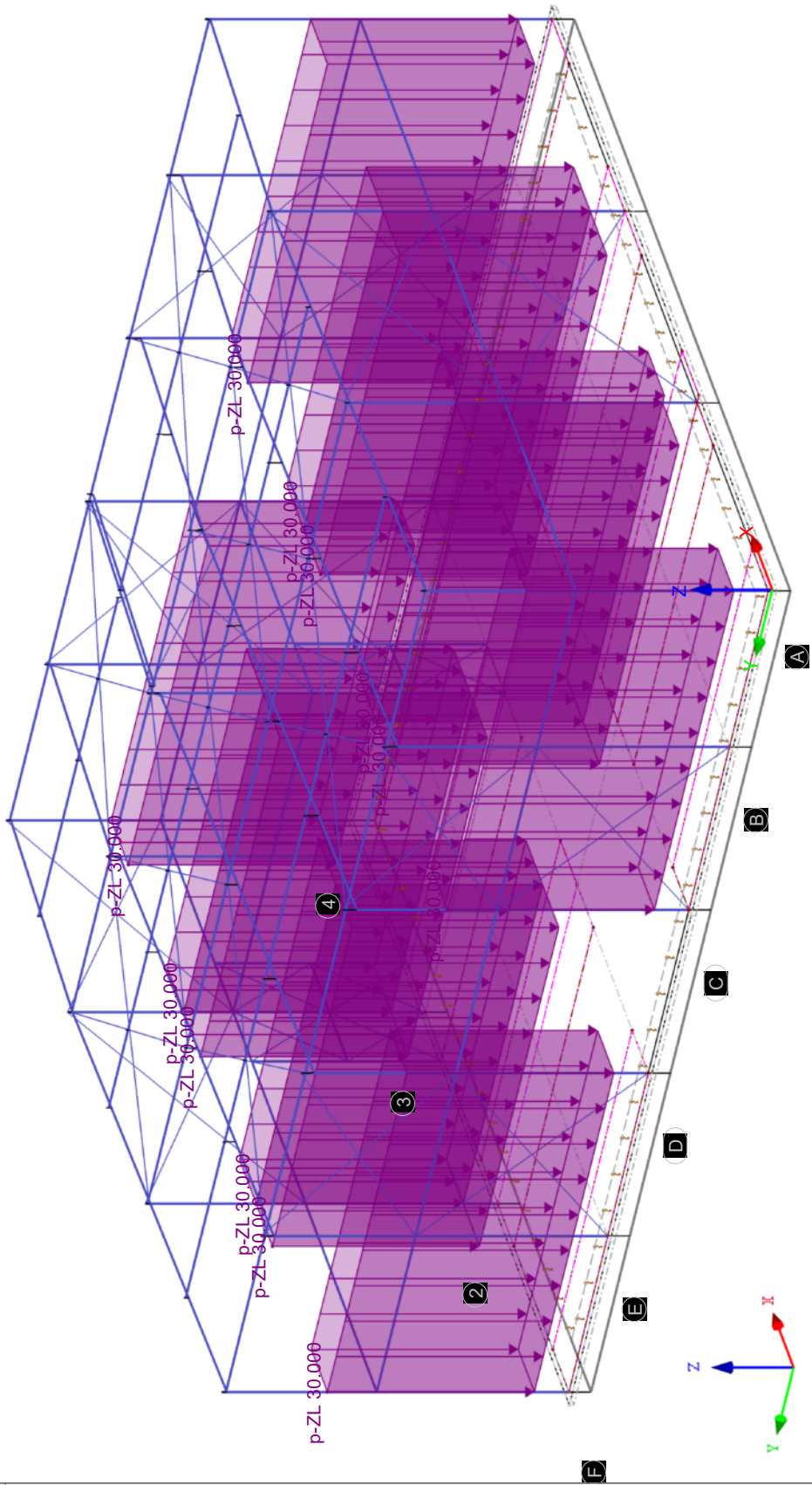
Isometrisch




BG130 : VB: Zonnepanelen
Belastingen [kN/m]

## BG140: VB: STELLINGEN - PALLET

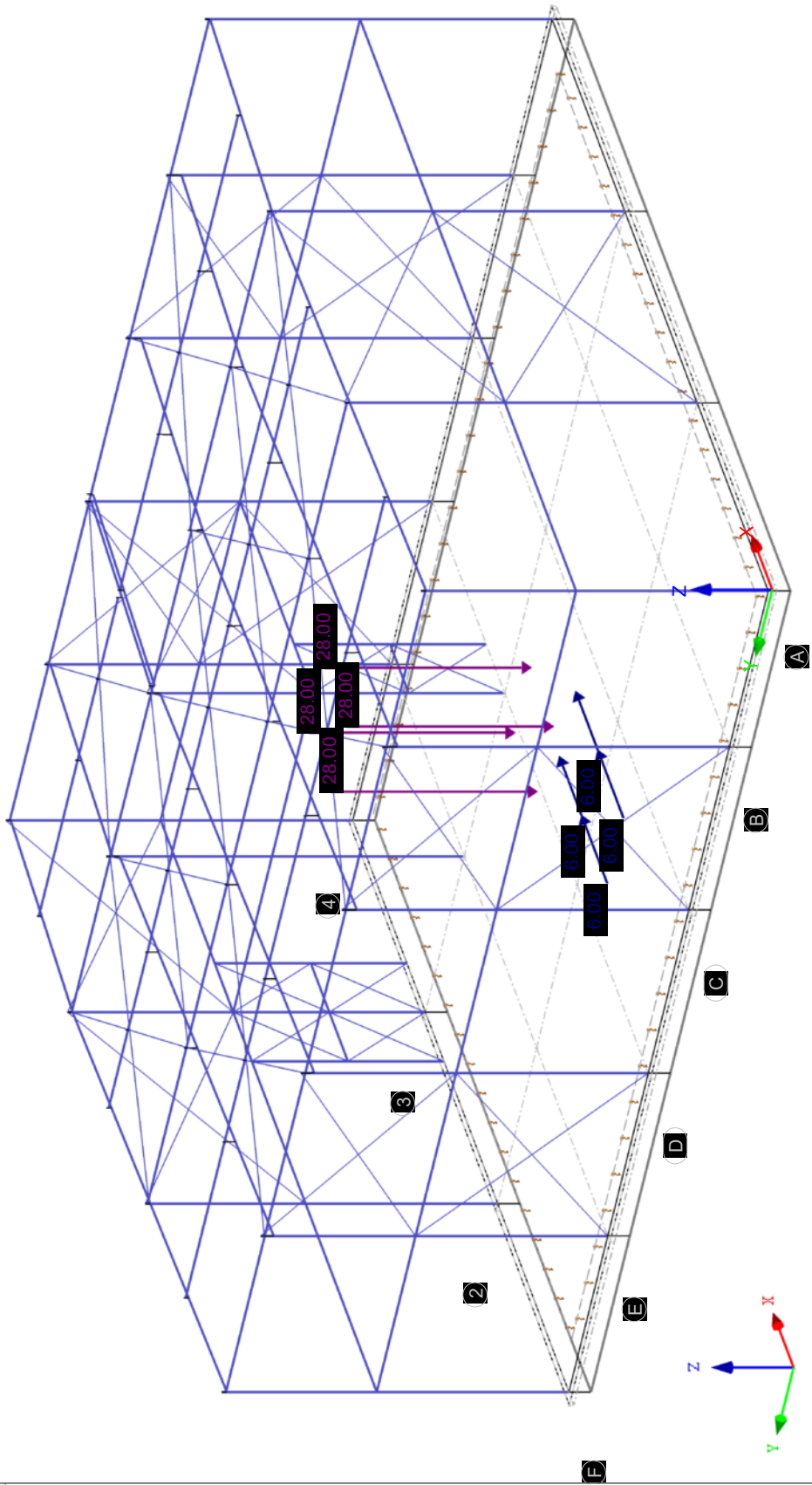
Isometrisch




BG140 : VB: Stellingen - Pallet
Belastingen [kN/m^2]

## BG150: VB: HEFTRUCK

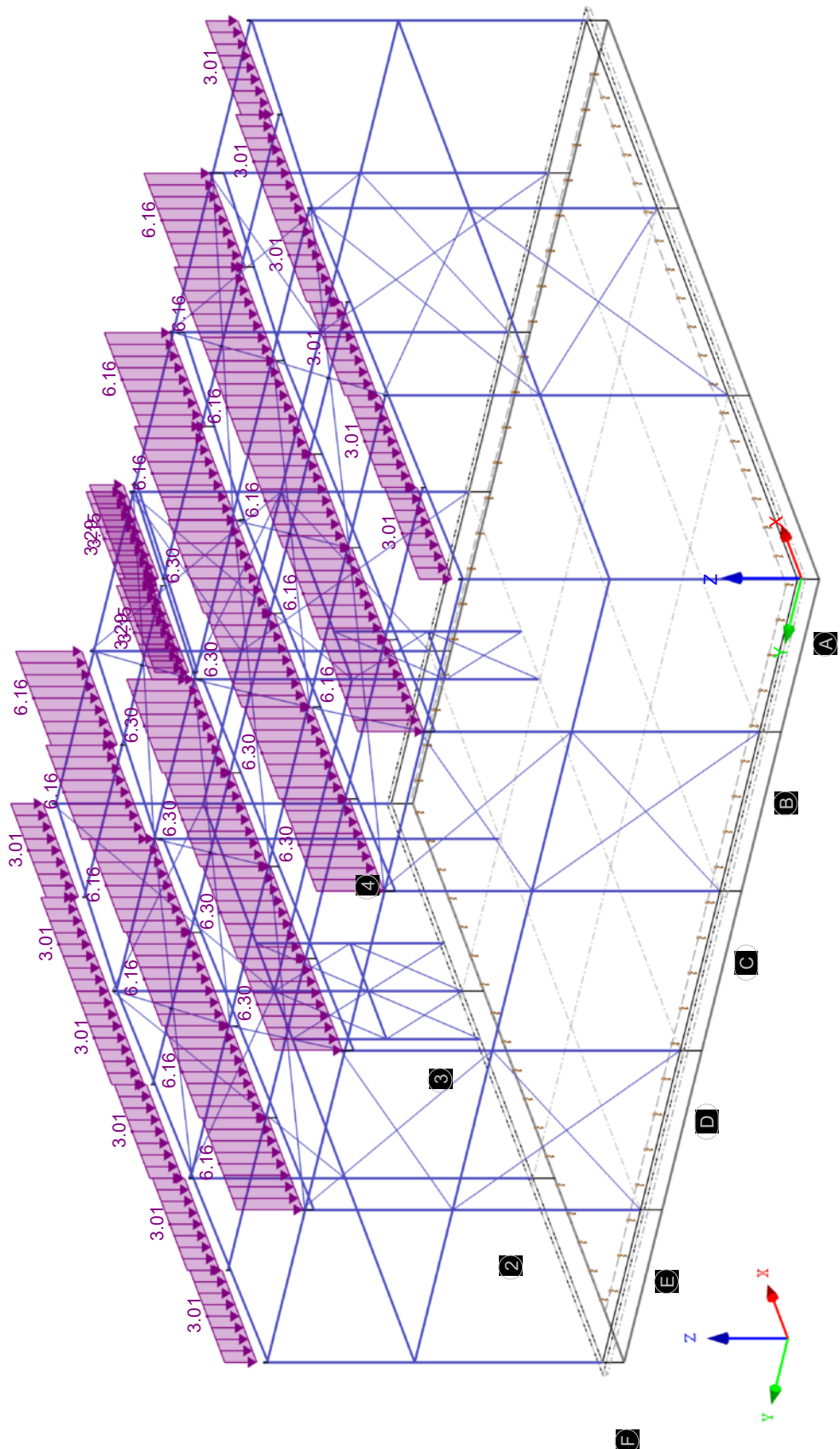
Isometrisch




BG150 : VB: Heftruck
Belastingen [kN]

## BG300: VB: SNEEUW

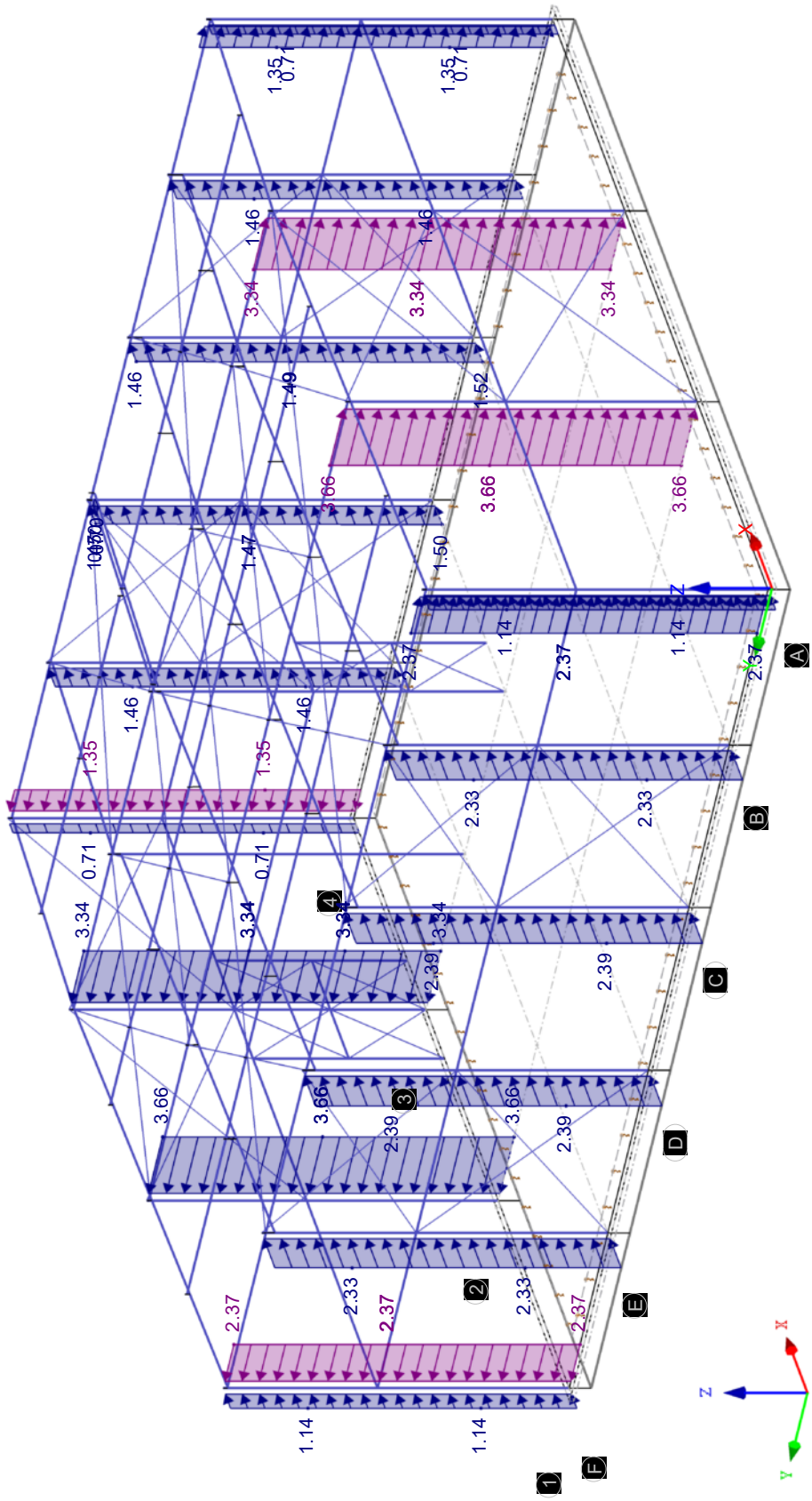
Isometrisch




BG300 : VB: Sneeuw
Belastingen [kN/m]

## BG401: VB: WIND (+X RICHTING)

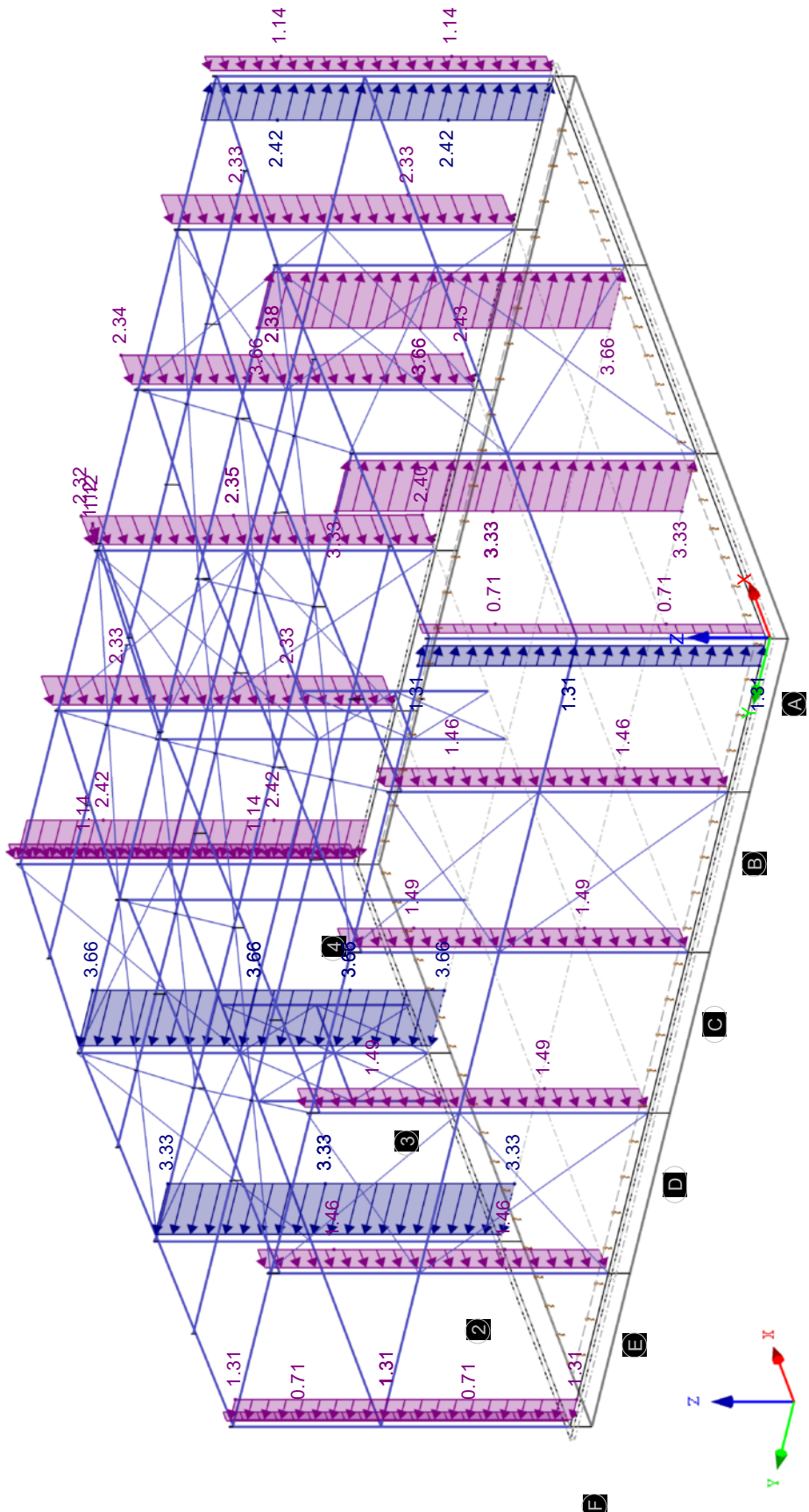
Isometrisch




BG401 : VB: Wind (+X richting)
Belastingen [kN/m]

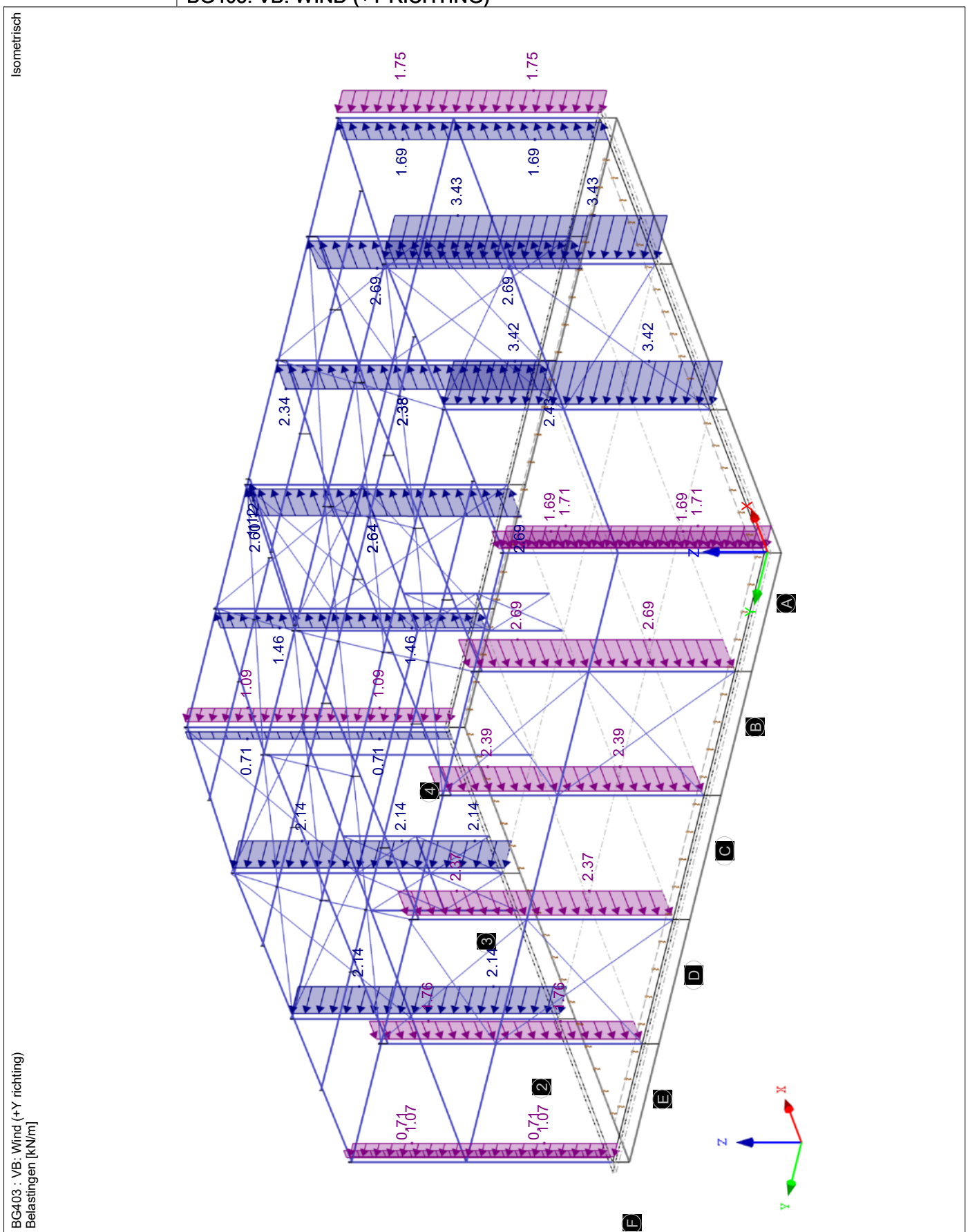
## BG402: VB: WIND (-X RICHTING)

Isometrisch



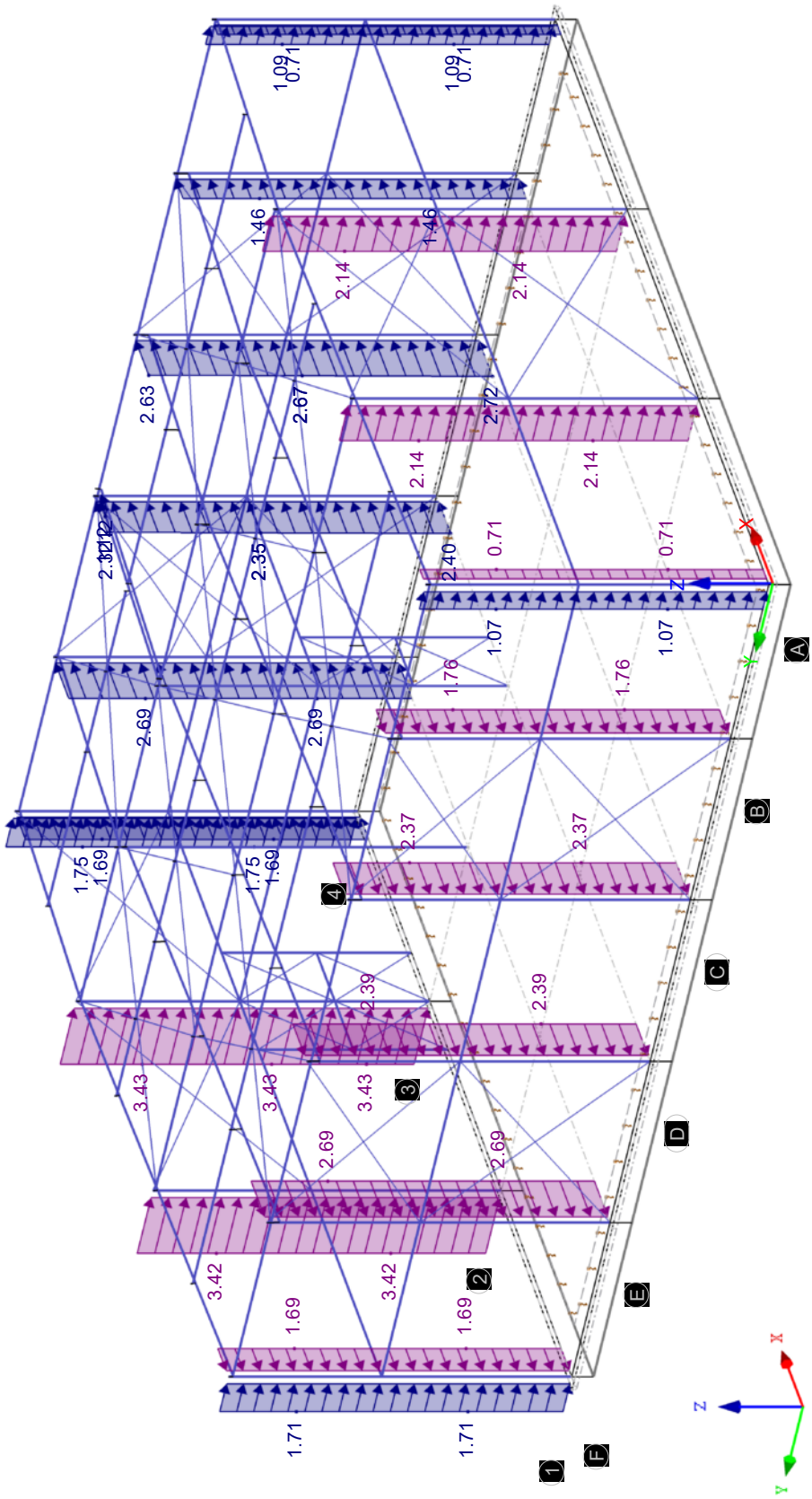

BG402 : VB: Wind (-X richting)
Belastingen [kN/m]

## BG403: VB: WIND (+Y RICHTING)



## BG404: VB: WIND (-Y RICHTING)

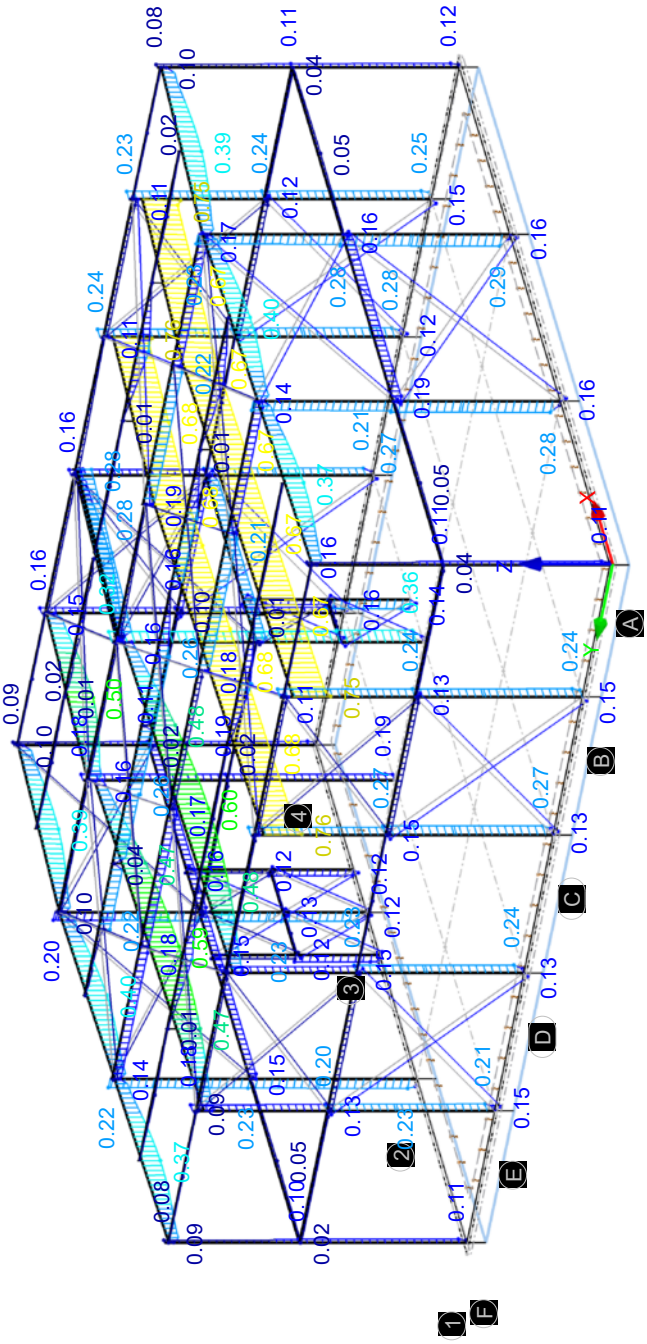
Isometrisch




BG404 : VB: Wind (-Y richting)
Belastingen [kN/m]

## CONTROLE UGT

Isometrisch




RF-STEEL EC3 BG1
Uiterste grenstoestand: Doorsnedecontrole, Stabiliteitsberekening

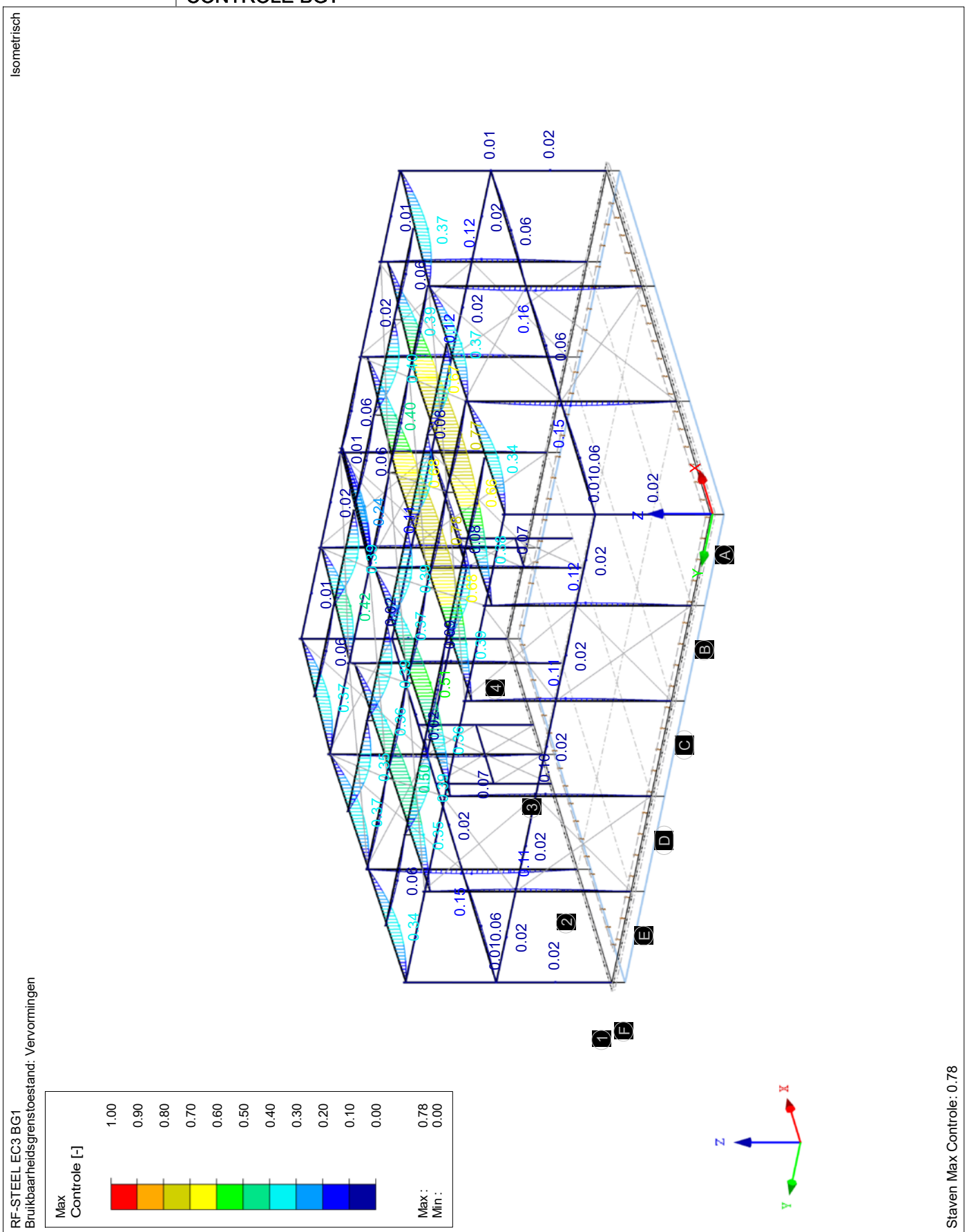
Max
Controle [-]

1.00
0.90
0.80
0.70
0.60
0.50
0.40
0.30
0.20
0.10
0.00

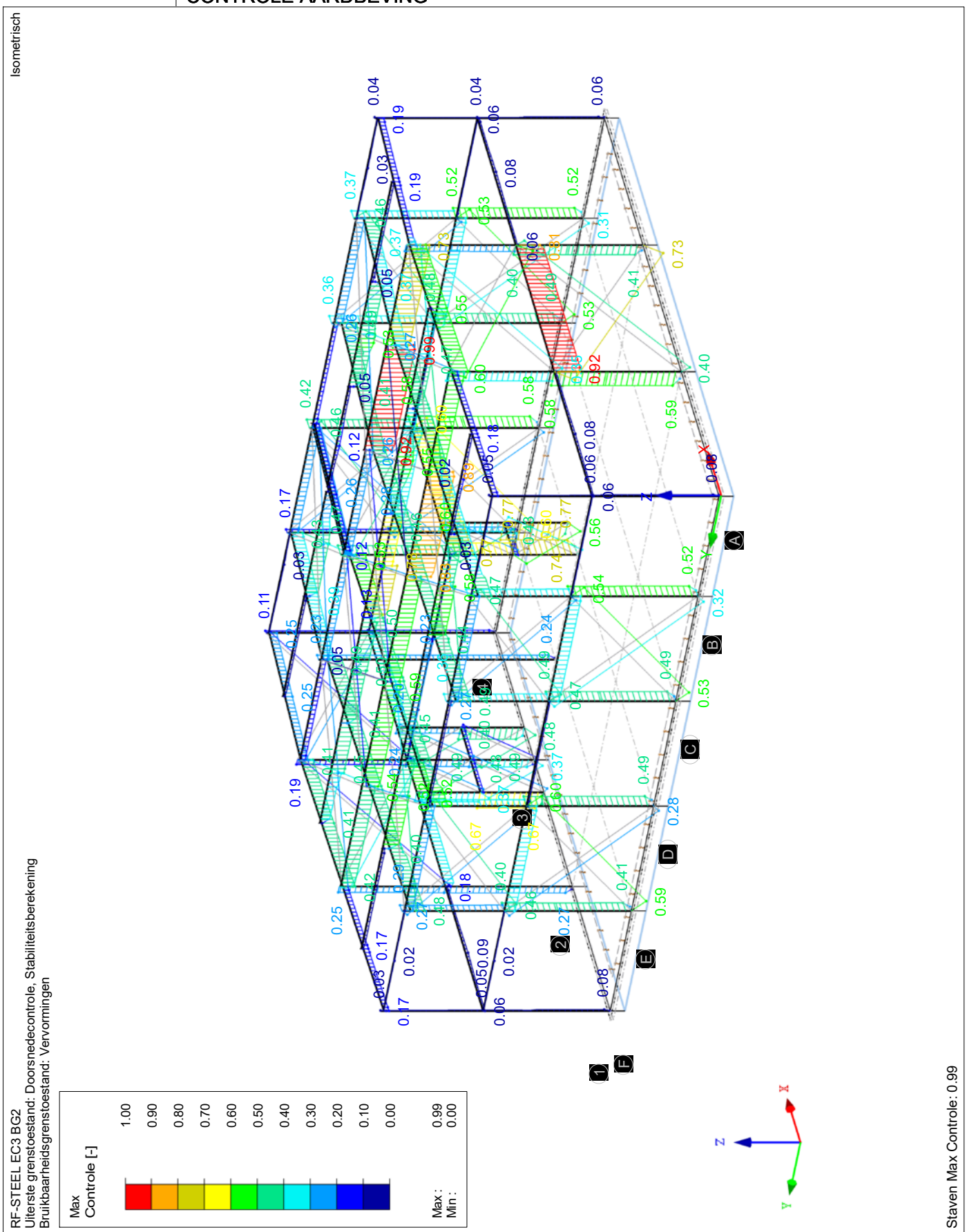
Max : 0.76
Min : 0.00

Staven Max Controle: 0.76

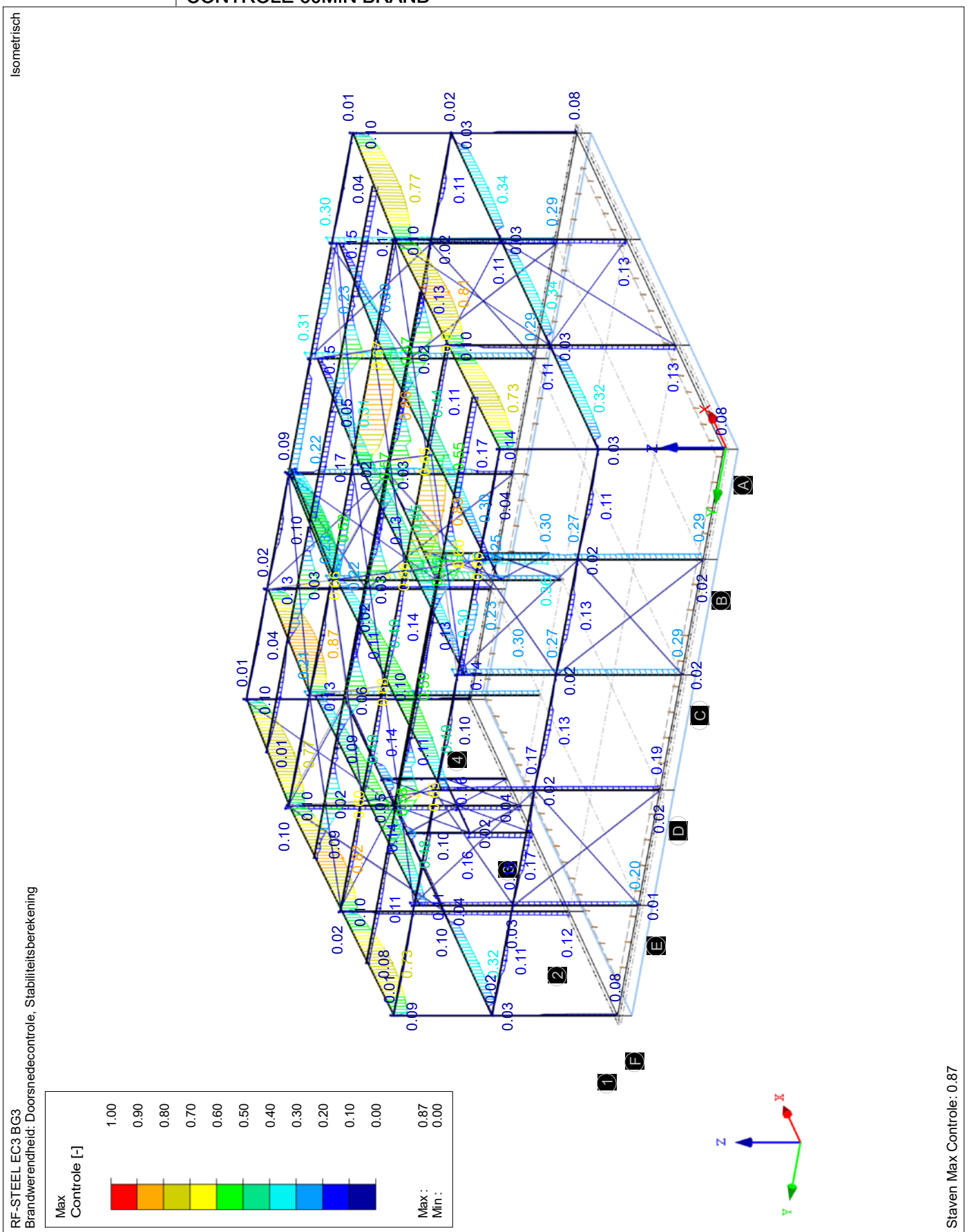
## CONTROLE BGT



## CONTROLE AARDBEVING

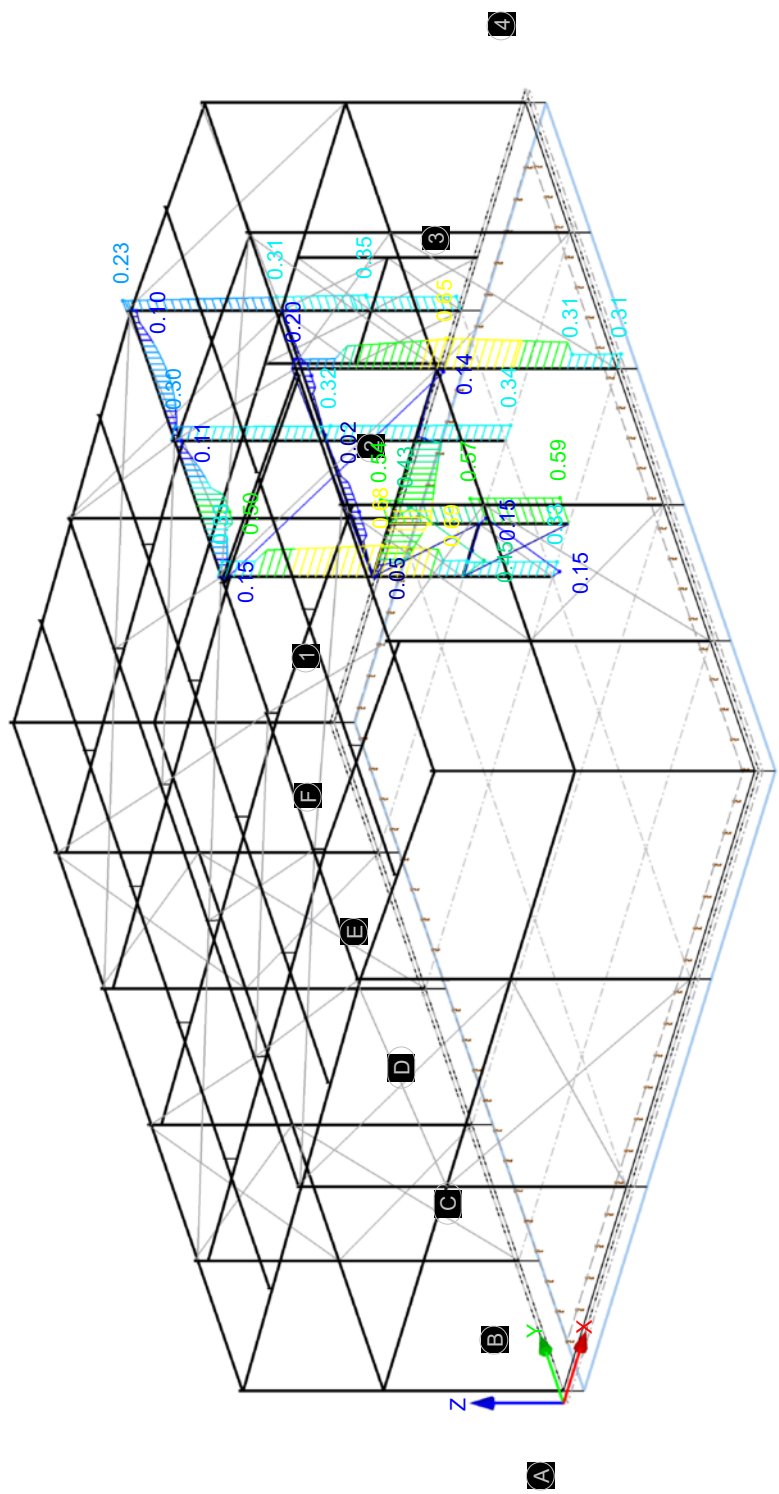


## CONTROLE 60MIN BRAND



## CONTROLE 120MIN BRAND

Isometrisch




RF-STEEL EC3 BG4
Brandwerendheid: Doorsnedecontrole, Stabiliteitsberekening

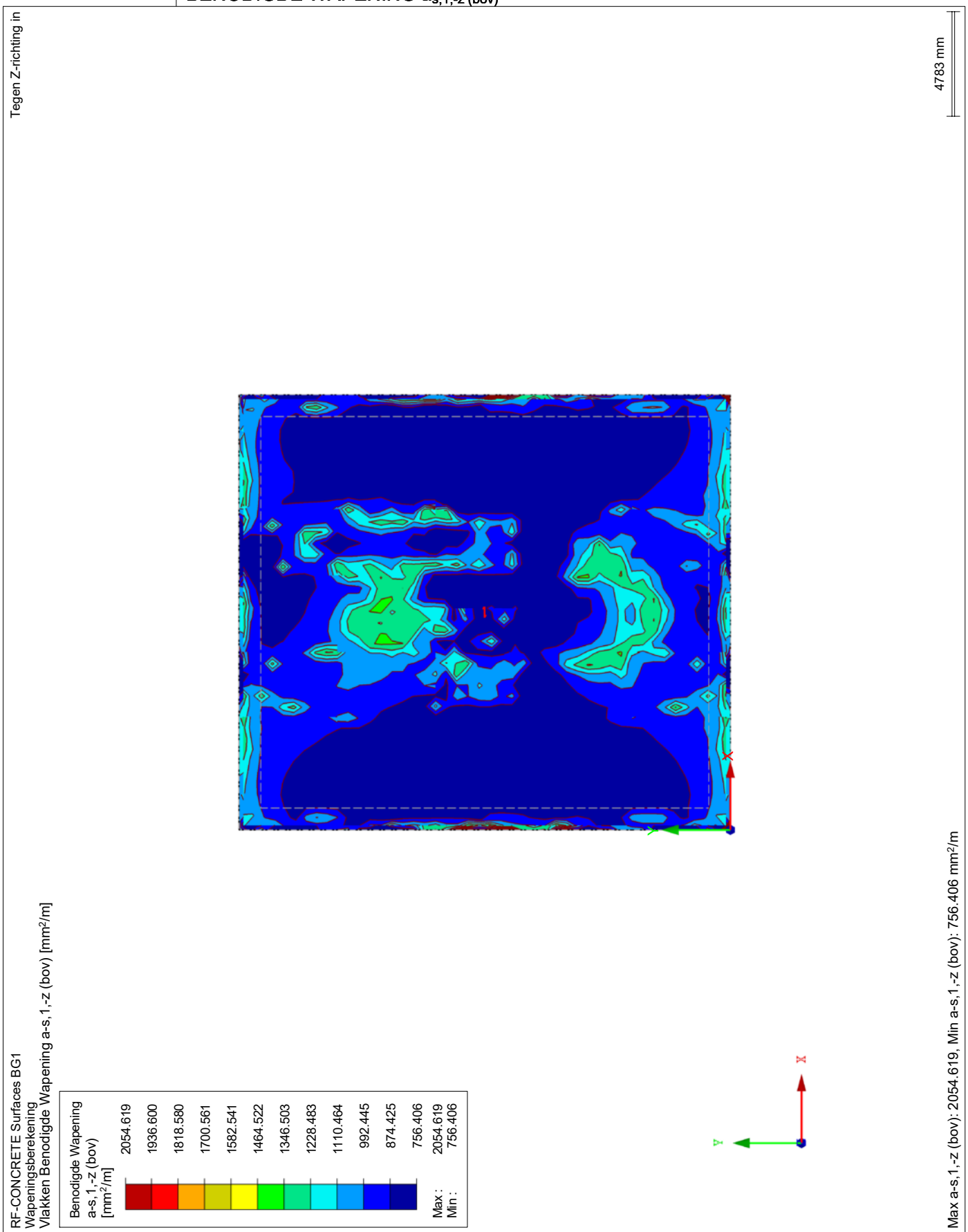
Max
Controle [-]

1.00
0.90
0.80
0.70
0.60
0.50
0.40
0.30
0.20
0.10
0.00

Max : 0.69
Min : 0.00

Staven Max Controle: 0.69

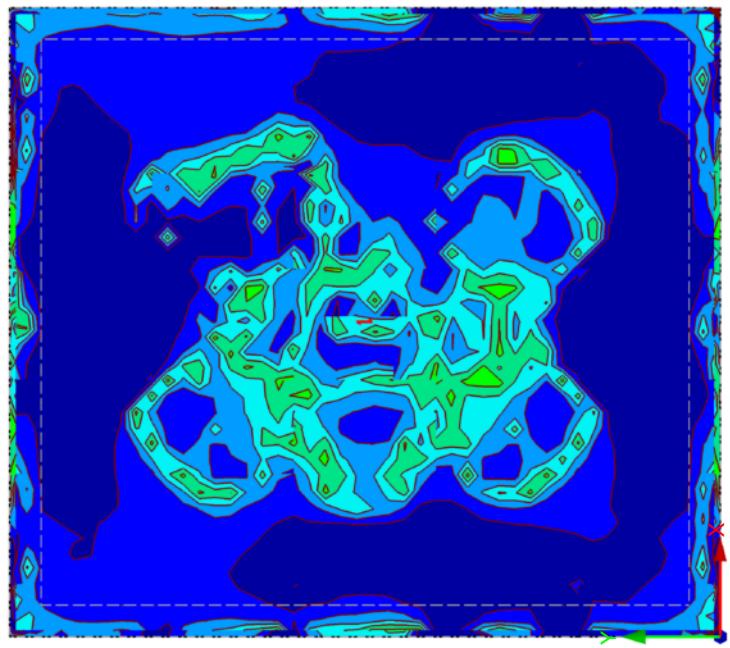
## BENODIGDE WAPENING $a_{s,1,-z\ (bov)}$



## BENODIGDE WAPENING $a_{s,2,-z\ (bov)}$

Tegen Z-richting in

4783 mm



RF-CONCRETE Surfaces BG1
Wapeningsberekening
Vlakken Benodigde Wapening a-s,2,-z (bov) [mm²/m]

Benodigde Wapening
a-s,2,-z (bov)
[mm²/m]

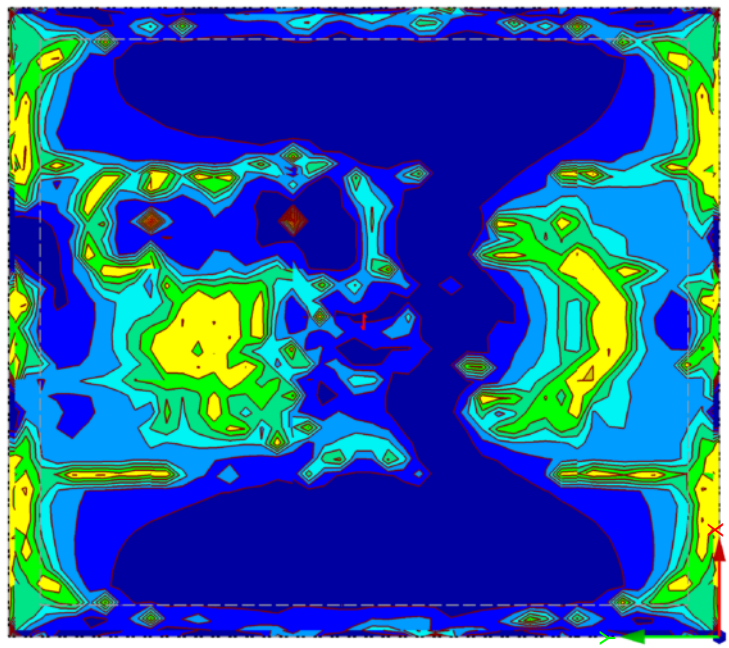
| | |
|---|---|
| | 2187.146 |
| | 2065.164 |
| | 1943.182 |
| | 1821.199 |
| | 1699.217 |
| | 1577.234 |
| | 1455.252 |
| | 1333.270 |
| | 1211.287 |
| | 1089.305 |
| | 967.322 |
| | 845.340 |
| Max : | 2187.146 |
| Min : | 845.340 |

Max a-s,2,-z (bov): 2187.146, Min a-s,2,-z (bov): 845.340 mm²/m

## BENODIGDE WAPENING $a_{s,1,+z\ (ond)}$

Tegen Z-richting in

4783 mm



RF-CONCRETE Surfaces BG1
Wapeningsberekening
Vlakken Benodigde Wapening a-s,1,+z (ond) [mm²/m]

Benodigde Wapening
a-s,1,+z (ond)
[mm²/m]

| | |
|---|---|
| 1696.606 | |
| 1611.133 | |
| 1525.660 | |
| 1440.188 | |
| 1354.715 | |
| 1269.242 | |
| 1183.769 | |
| 1098.297 | |
| 1012.824 | |
| 927.351 | |
| 841.878 | |
| 756.406 | |

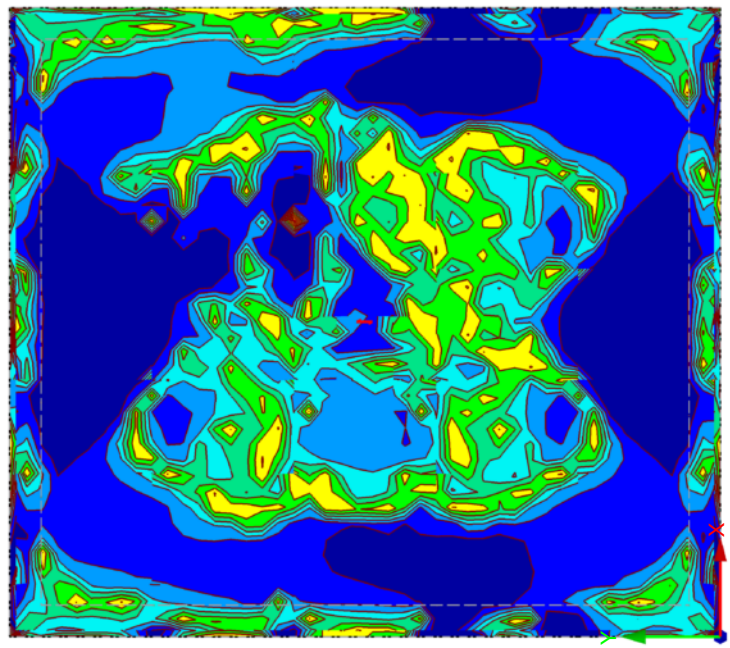
Max : 1696.606
Min : 756.406

Max a-s,1,+z (ond): 1696.606, Min a-s,1,+z (ond): 756.406 mm²/m

## BENODIGDE WAPENING $a_{s,2,+z\ (ond)}$

Tegen Z-richting in

4783 mm



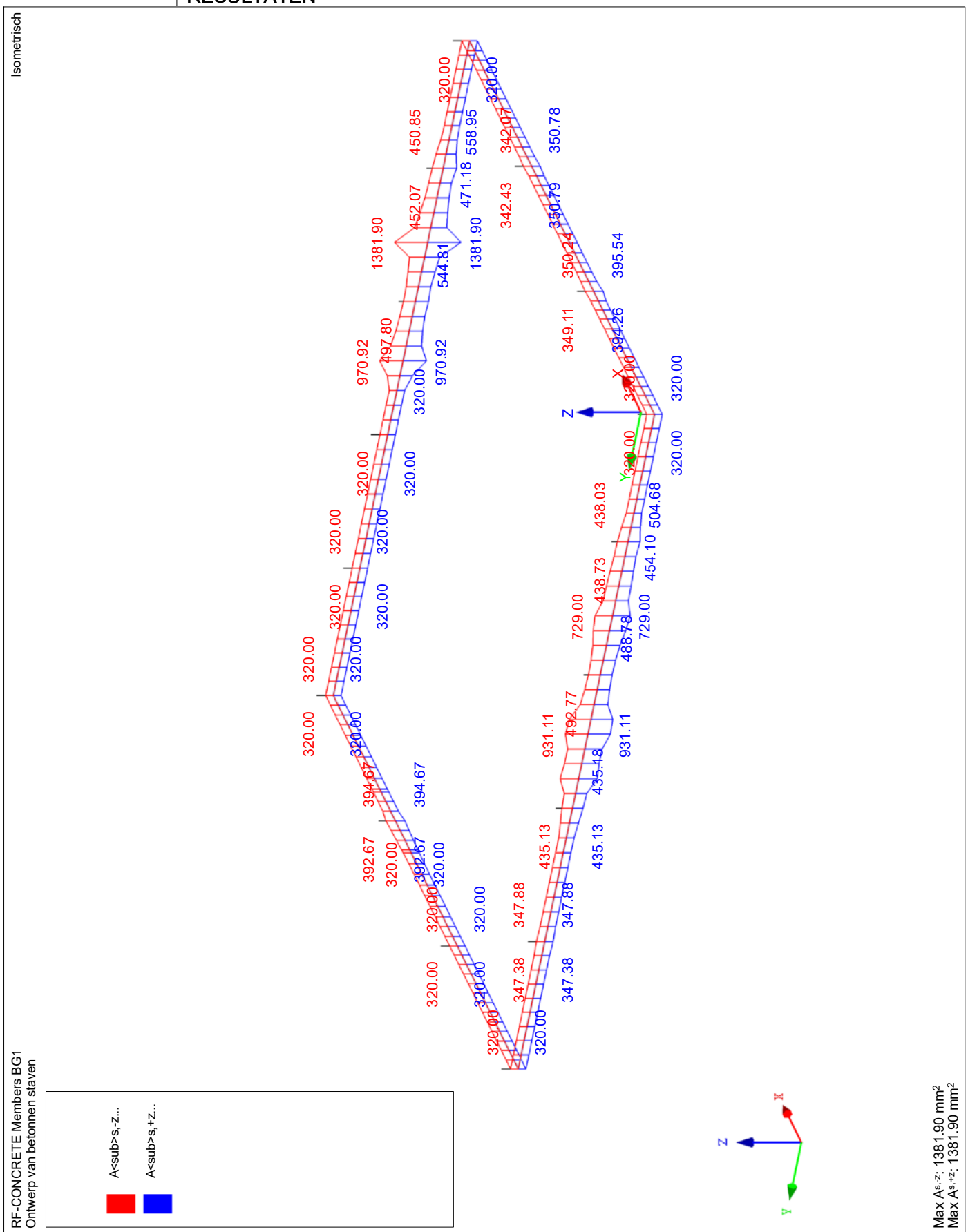
RF-CONCRETE Surfaces BG1
Wapeningsberekening
Vlakken Benodigde Wapening a-s,2,+z (ond) [mm²/m]

Benodigde Wapening a-s,2,+z (ond) [mm²/m]

| | |
|---|---|
| | 1872.405 |
| | 1779.035 |
| | 1685.666 |
| | 1592.296 |
| | 1498.927 |
| | 1405.557 |
| | 1312.188 |
| | 1218.818 |
| | 1125.449 |
| | 1032.079 |
| | 938.710 |
| | 845.340 |
| Max : | 1872.405 |
| Min : | 845.340 |

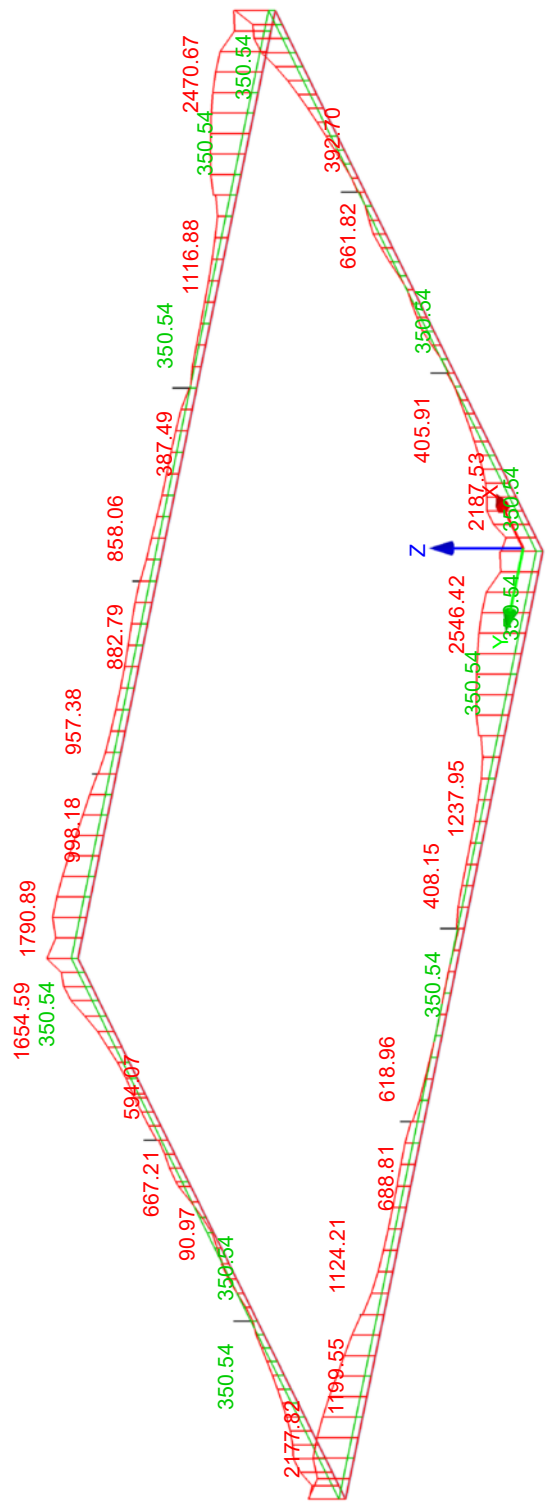
Max a-s,2,+z (ond): 1872.405, Min a-s,2,+z (ond): 845.340 mm²/m

## RESULTATEN


Isometrisch
RF-CONCRETE Members BG1
Ontwerp van betonnen staven
A<sub>s,-z...
A<sub>s,+z...
Max As,-z: 1381.90 mm²
Max As,+z: 1381.90 mm²

## RESULTATEN

Isometrisch

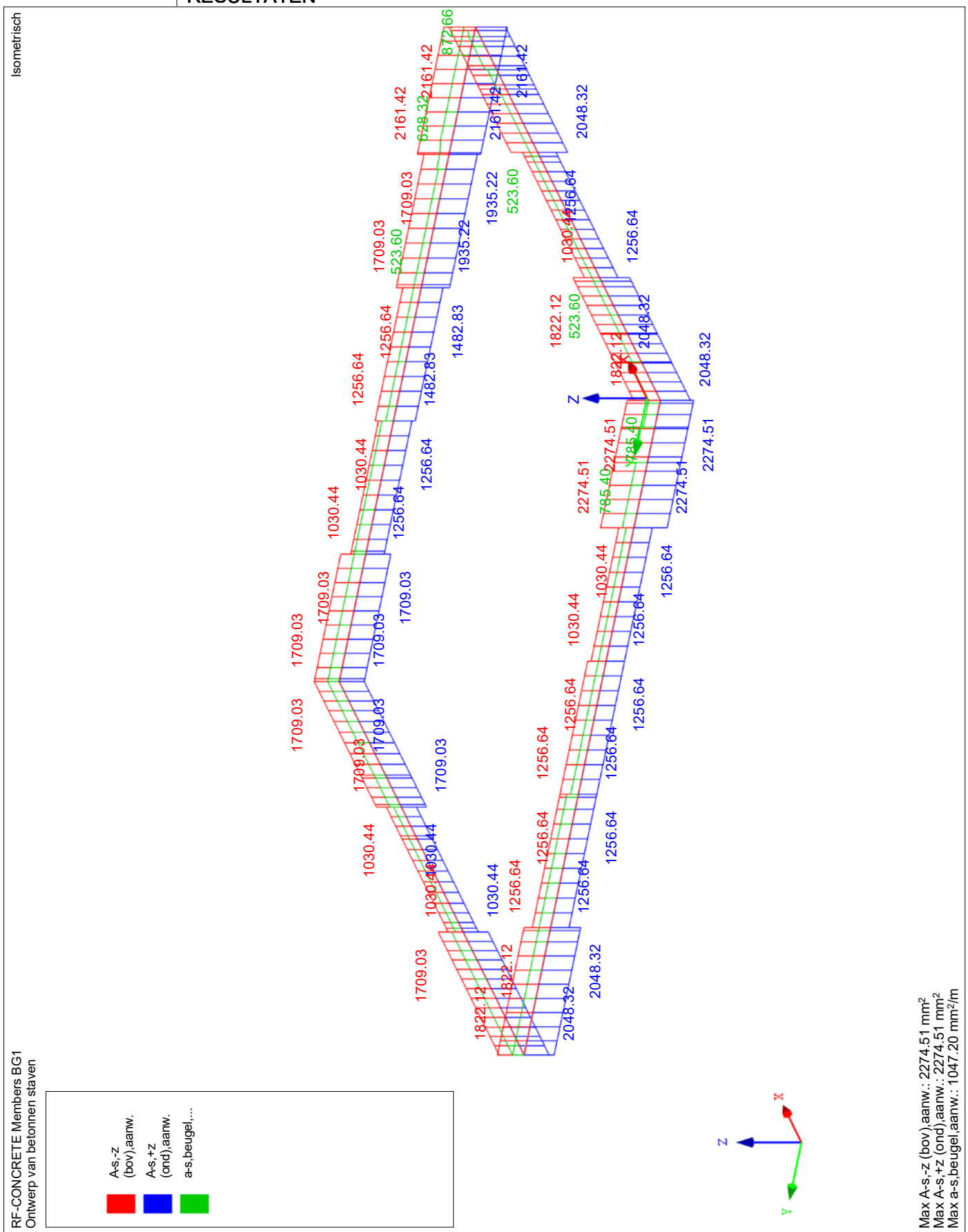



RF-CONCRETE Members BG1
Ontwerp van betonnen staven

A-s,T
a-sw,T,beu...
a-sw,V,bgl

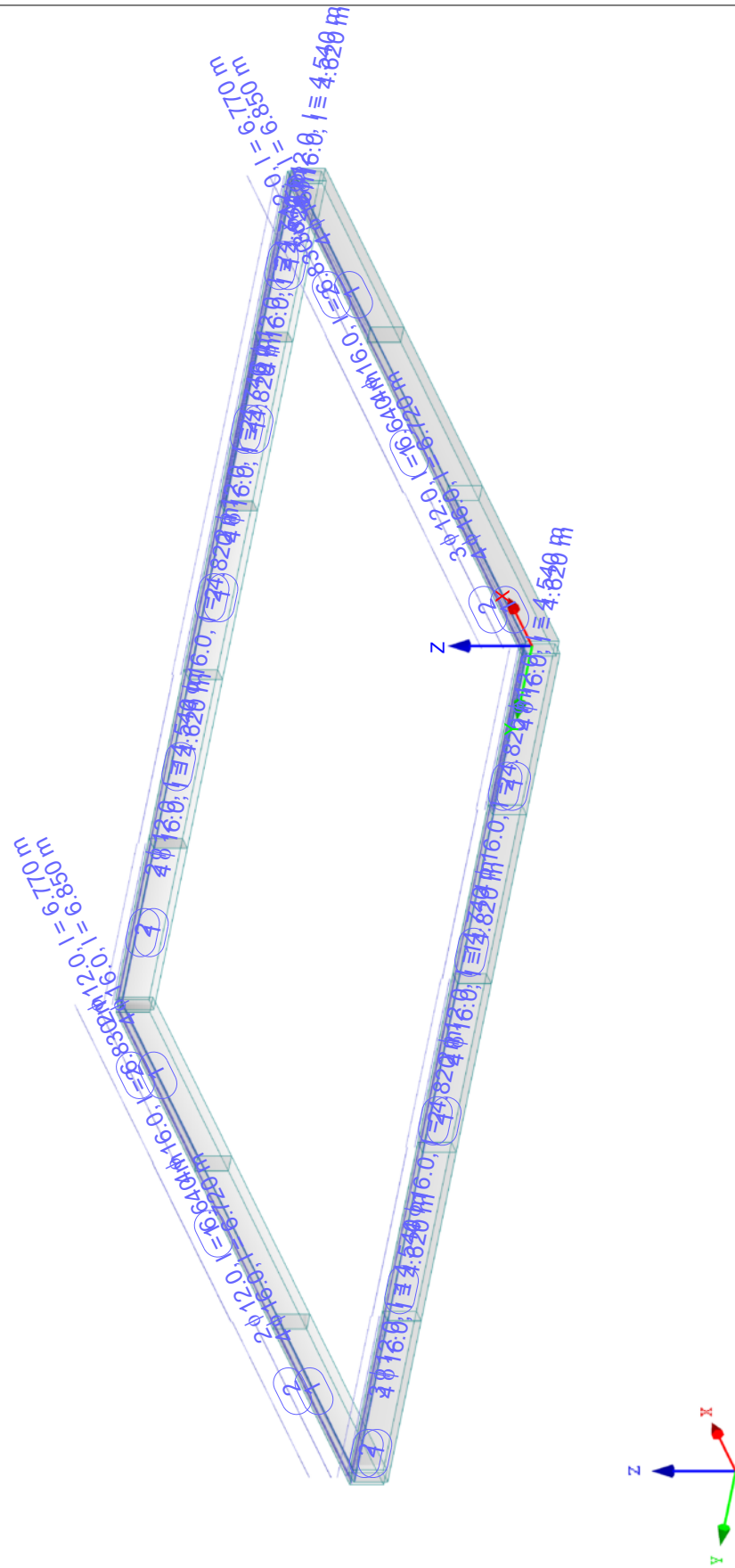
Max A-s,T: 2546.42 mm²
Max a-sw,T,beugel: 218.23 mm²/m
Max a-sw,V,bgl: 350.54 mm²/m

## RESULTATEN


Isometrisch
RF-CONCRETE Members BG1
Ontwerp van betonnen staven
A-s,-z (bov),aanw.
A-s,+z (ond),aanw.
a-s,beugel,...
Max A-s,-z (bov),aanw.: 2274.51 mm²
Max A-s,+z (ond),aanw.: 2274.51 mm²
Max a-s,beugel,aanw.: 1047.20 mm²/m

## MODEL

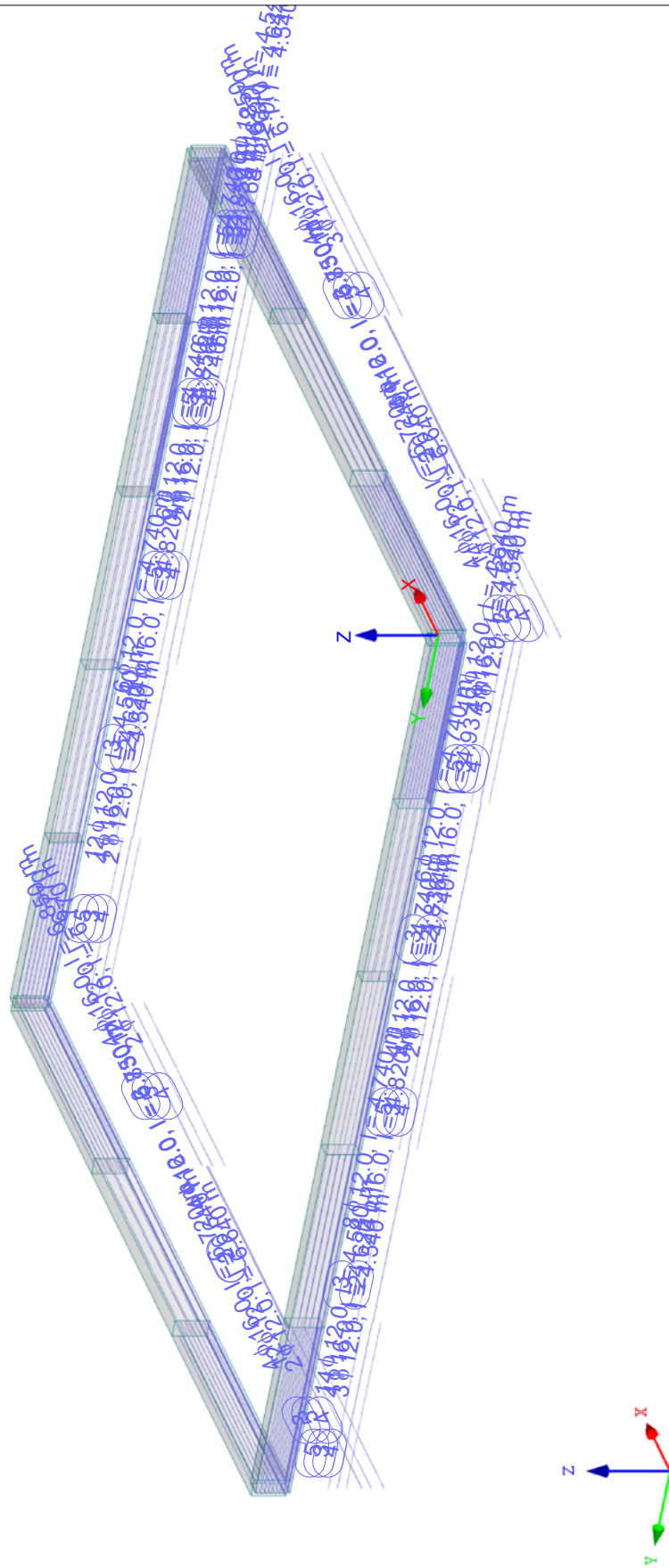
Isometrisch



RF-CONCRETE Members BG1
Ontwerp van betonnen staven

## MODEL

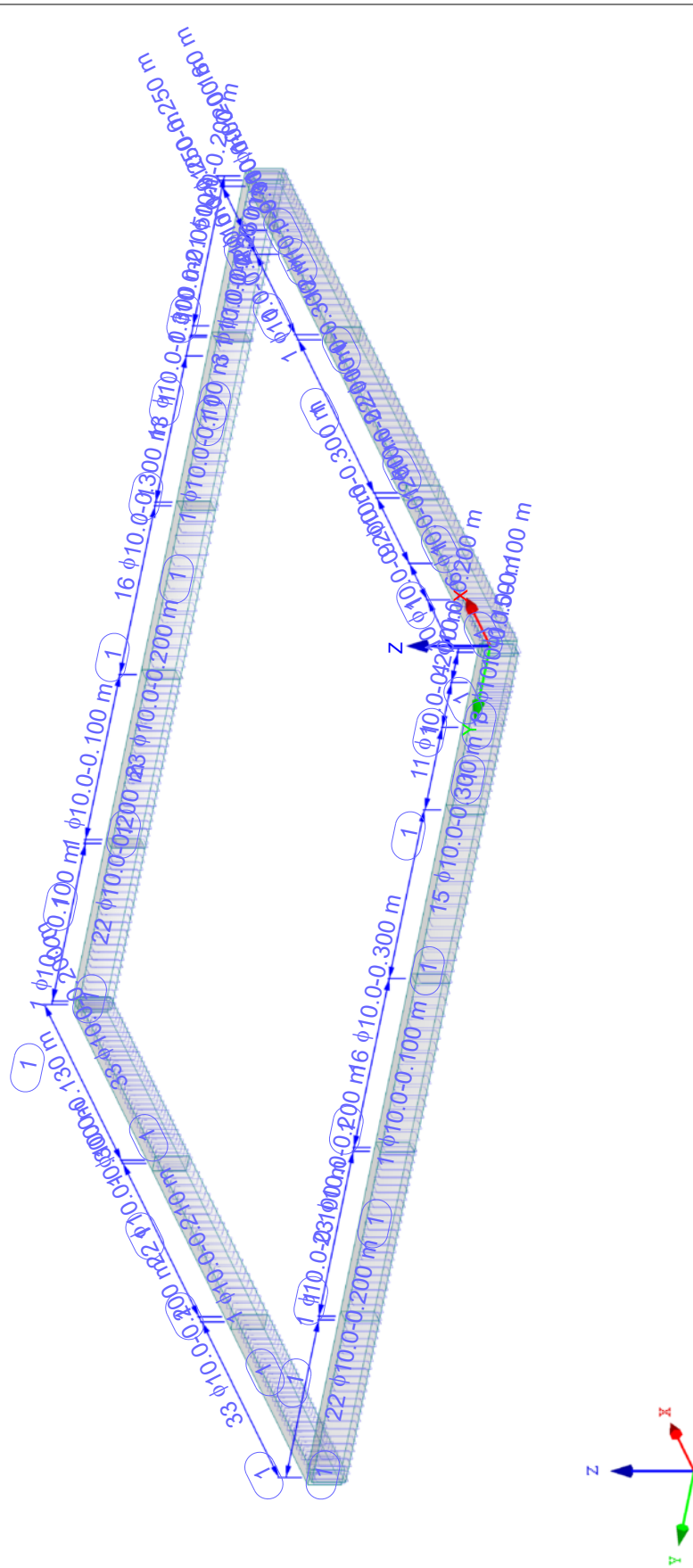
Isometrisch



RF-CONCRETE Members BG1
Ontwerp van betonnen staven

## MODEL

Isometrisch




RF-CONCRETE Members BG1
Ontwerp van betonnen staven

## INHOUD



## ALGEMENE GEGEVENS MODEL

| | | | |
|---|---|---|---|
| Algemeen | Modelnaam | : | 23920-21_5001_00_00_Sluis_21092022_1431 |
| | Modeltype | : | 3D |
| | Positieve richting van globale z-as | : | Naar Boven |
| | Classificatie van belastingsgevallen en combinaties | : | Volgens norm: EN 1990<br>Nationale Bijlage: NEN - Nederland |
| | ☒Combinaties automatisch aanmaken | : | ☒Belastingscombinaties |

| | | |
|---|---|---|
| Opties | ☐ | RF-FORM-FINDING - Vind aanvangsevenwichtsvormen van membranen en kabelconstructies |
| | ☐ | RF-CUTTING-PATTERN |
| | ☐ | Leidingwerk berekening |
| | ☐ | Gebruik CQC regel |
| | ☐ | CAD/BIM model mogelijk maken |

| | | |
|---|---|---|
| Standaard zwaartekracht | | |
| g | : | 10.00 m/s$^2$ |

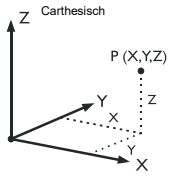
## EE-NETINSTELLINGEN

| | | | | |
|---|---|---|---|---|
| Algemeen | Doellengte van eindige elementen | $l_{FE}$ | : | 200 mm |
| | Max. afstand tussen een knoop en een lijn om in de lijn te integreren | ε | : | 1 mm |
| | Max. aantal netknopen (in duizenden) | | : | 500 |

| | | | |
|---|---|---|---|
| Staven | Aantal staafverdelingen van kabels, Elastische bedding, voutes of plastische karakteristiek | : | 10 |
| | ☒ Stel staafverdelingen in voor grote vervorming of post-kritische berekening | | |
| | ☒ Gebruik staafverdeling ook voor rechte staven, die niet zijn geï¿½ntegreerd in de vlakken, met | : | Stel Lengte $l_{FE}$ in = 0 [mm] |
| | Min. aantal staafverdelingen | : | 5 |
| | ☒ Gebruik staafverdeling door de knopen die op de staaf liggen | | |

## EE-NETINSTELLINGEN

| | | | | |
|---|---|---|---|---|
| Vlakken | Max. verh. van EE-rechthoekdiagonalen | $\Delta_D$ | : | 2 |
| | Max. uit-het-vlak hoek van twee EE uit het vlak | $\alpha$ | : | 0.50 ° |
| | ☒ Integreer ook ongebruikte objecten in de vlakken | | | |
| | Vorm van de eindige elementen | | : | Driehoeken en schalen<br>☒Gelijke Vierhoeken genereren indien mogelijk |




## 1.1 KNOPEN

| Knoop No. | Knooptype | Referentie knoop | Coï¿½rdinaten Syteem | Knoopcoï¿½rdinaten X [mm] | Y [mm] | Z [mm] | Opm. |
|---|---|---|---|---|---|---|---|
| 1 | Standaard | - | Carthesisch | -200 | -200 | 0 | |
| 2 | Standaard | - | Carthesisch | 7200 | -200 | 0 | |
| 3 | Standaard | - | Carthesisch | 7200 | 4200 | 0 | |
| 4 | Standaard | - | Carthesisch | -200 | 4200 | 0 | |
| 5 | Standaard | - | Carthesisch | 0 | 0 | 0 | |
| 6 | Standaard | - | Carthesisch | 0 | 0 | 4050 | |
| 7 | Standaard | - | Carthesisch | 3500 | 0 | 0 | |
| 8 | Standaard | - | Carthesisch | 3500 | 0 | 4050 | |
| 9 | Standaard | - | Carthesisch | 7000 | 0 | 0 | |
| 10 | Standaard | - | Carthesisch | 7000 | 0 | 4050 | |
| 11 | Standaard | - | Carthesisch | 0 | 4000 | 0 | |
| 12 | Standaard | - | Carthesisch | 0 | 4000 | 4050 | |
| 13 | Standaard | - | Carthesisch | 3500 | 4000 | 0 | |
| 14 | Standaard | - | Carthesisch | 3500 | 4000 | 4050 | |
| 15 | Standaard | - | Carthesisch | 7000 | 4000 | 0 | |
| 16 | Standaard | - | Carthesisch | 7000 | 4000 | 4050 | |
| 17 | Standaard | - | Carthesisch | 0 | 0 | 2500 | |
| 18 | Standaard | - | Carthesisch | 7000 | 0 | 2500 | |
| 19 | Standaard | - | Carthesisch | 0 | 4000 | 2500 | |
| 20 | Standaard | - | Carthesisch | 7000 | 4000 | 2500 | |
| 21 | Standaard | - | Carthesisch | 2500 | 1100 | 0 | |
| 22 | Standaard | - | Carthesisch | 2500 | 2900 | 0 | |
| 23 | Standaard | - | Carthesisch | 4500 | 1100 | 0 | |
| 24 | Standaard | - | Carthesisch | 4500 | 2900 | 0 | |

## 1.2 LIJNEN

| Lijn No. | Lijntype | Knopen No. | Lijnlengte L [mm] | | Opm. |
|---|---|---|---|---|---|
| 1 | Polylijn | 1,2 | 7400 | X | |
| 2 | Polylijn | 2,3 | 4400 | Y | |
| 3 | Polylijn | 3,4 | 7400 | X | |
| 4 | Polylijn | 4,1 | 4400 | Y | |
| 5 | Polylijn | 5,6 | 4050 | Z | |
| 6 | Polylijn | 7,8 | 4050 | Z | |
| 7 | Polylijn | 9,10 | 4050 | Z | |
| 8 | Polylijn | 11,12 | 4050 | Z | |
| 9 | Polylijn | 13,14 | 4050 | Z | |
| 10 | Polylijn | 15,16 | 4050 | Z | |
| 11 | Polylijn | 6,12 | 4000 | Y | |
| 12 | Polylijn | 8,14 | 4000 | Y | |
| 13 | Polylijn | 10,16 | 4000 | Y | |
| 14 | Polylijn | 6,8 | 3500 | X | |
| 15 | Polylijn | 8,10 | 3500 | X | |
| 16 | Polylijn | 12,14 | 3500 | X | |
| 17 | Polylijn | 14,16 | 3500 | X | |
| 18 | Polylijn | 6,14 | 5315 | XY | |
| 19 | Polylijn | 12,8 | 5315 | XY | |
| 20 | Polylijn | 5,8 | 5353 | XZ | |
| 21 | Polylijn | 7,6 | 5353 | XZ | |
| 22 | Polylijn | 11,14 | 5353 | XZ | |
| 23 | Polylijn | 13,12 | 5353 | XZ | |
| 24 | Polylijn | 5,7 | 3500 | X | |
| 25 | Polylijn | 7,9 | 3500 | X | |
| 26 | Polylijn | 11,13 | 3500 | X | |
| 27 | Polylijn | 13,15 | 3500 | X | |
| 28 | Polylijn | 8,16 | 5315 | XY | |
| 29 | Polylijn | 14,10 | 5315 | XY | |

## 1.3 MATERIALEN

| Matl. No. | Modulus E [N/mm²] | Modulus G [N/mm²] | Coï¿½ff. v. Pois $\nu$ [-] | Vol. gewicht $\gamma$ [kN/m³] | Therm. uitz. $\alpha$ [1/K] | Materiaalfactor $\gamma_M$ [-] | Materiaal Model |
|---|---|---|---|---|---|---|---|
| 1 | Staal S 235 \| NEN EN 1993-1-1:2007-11 | | | | | | |
| | 210000.0 | 80769.2 | 0.300 | 78.50 | 1.20E-05 | 1.00 | Isotroop Lineair Elastisch |
| 2 | Beton C30/37 \| EN 1992-1-1:2004/A1:2014 | | | | | | |
| | 33000.0 | 13750.0 | 0.200 | 25.00 | 1.00E-05 | 1.00 | Isotroop Lineair Elastisch |

## 1.4 VLAKKEN

| Vlak No. | Vlaktype Geometrie | Vlaktype Stijfheid | Randen No. | Matl. No. | Dikte Type | Dikte [mm] | Vlak A [mm²] | Gewicht G [kg] |
|---|---|---|---|---|---|---|---|---|
| 1 | Vlak | Standaard | 1-4 | 2 | &Blijvend | 150.0 | 32560000 | 12210.00 |

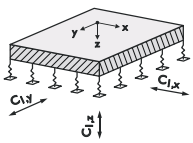
## 1.4.1 VLAKKEN - EXCENTRICITEITEN

| Vlak No. | Excentriciteit $e_z$ [mm] | Opm. |
|---|---|---|
| 1 | 75.0 | |

## 1.4.2 VLAKKEN - GEï¿½NTEGREERDE OBJECTEN

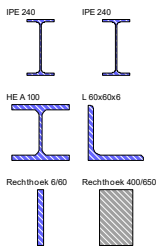
| Vlak No. | Geï¿½ntegreerde objecten No. Knopen | Lijnen | Sparingen | Opm. |
|---|---|---|---|---|
| 1 | 21-24 | 24-27 | | |

## 1.9 STEUNVLAKKEN



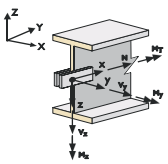
| Fund. No. | Op vlakken No. | Veerconstanten RF-SOILIN | Translationeel steunpunt of veer [kN/m³] $u_x$ | $u_y$ | $u_z$ | Dwarskrachtveer [kN/m] $v_{xz}$ | $v_{yz}$ |
|---|---|---|---|---|---|---|---|
| 1 | 1 | - | 1000.000 | 1000.000 | 7000.000 | ☐ | ☐ |

## 1.13 DOORSNEDES



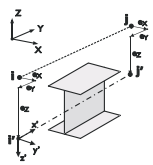

| Sneden No. | Matl. No. | J [mm⁴] / A [mm²] | $I_{y/u}$ [mm⁴] / $A_{y/u}$ [mm²] | $I_{z/v}$ [mm⁴] / $A_{z/v}$ [mm²] | Hoofdassen α [°] | Rotatie α' [°] | Globale maatvoering [mm] Breedte b | Hoogte h |
|---|---|---|---|---|---|---|---|---|
| 1 | IPE 240 \| Euronorm 19-57 | | | | | | | |
| | 1 | 129000.0 | 38900000.0 | 2840000.0 | 0.00 | 0.00 | 120.0 | 240.0 |
| | | 3910.0 | 1965.1 | 1382.2 | | | | |
| | Hoofddraag kolom | | | | | | | |
| 2 | IPE 240 \| Euronorm 19-57 | | | | | | | |
| | 1 | 129000.0 | 38900000.0 | 2840000.0 | 0.00 | 0.00 | 120.0 | 240.0 |
| | | 3910.0 | 1965.1 | 1382.2 | | | | |
| | Hoofddraag ligger | | | | | | | |
| 3 | HE A 100 \| Euronorm 53-62 | | | | | | | |
| | 1 | 52600.0 | 3490000.0 | 1340000.0 | 0.00 | 0.00 | 100.0 | 96.0 |
| | | 2120.0 | 1334.1 | 402.8 | | | | |
| | Tussenligger | | | | | | | |
| 4 | L 60x60x6 \| EN 10056-1:1998 | | | | | | | |
| | 1 | 8200.0 | 361000.0 | 94400.0 | -45.00 | 0.00 | 60.0 | 60.0 |
| | | 691.0 | 290.6 | 284.1 | | | | |
| | Horizontale verbanden | | | | | | | |
| 5 | Rechthoek 6/60 | | | | | | | |
| | 1 | 4047.8 | 108000.0 | 1080.0 | 0.00 | 0.00 | 6.0 | 60.0 |
| | | 360.0 | 300.0 | 300.0 | | | | |
| | Verticale verbanden | | | | | | | |
| 6 | Rechthoek 400/650 | | | | | | | |
| | 2 | 8554303488.0 | 9154165760.0 | 3466666752.0 | 0.00 | 0.00 | 400.0 | 650.0 |
| | | 260000.0 | 216666.7 | 216666.7 | | | | |
| | Randbalk beton | | | | | | | |

## 1.14 STAAFEINDSCHARNIEREN



| Vrijgave No. | Referentie Systeem | Normaal-/ Afschuifscharnier of Veer[k $u_x$ | $u_y$ | $u_z$ | Momentscharnier of veer[kNm/rad] $\varphi_x$ | $\varphi_y$ | $\varphi_z$ | Opm. |
|---|---|---|---|---|---|---|---|---|
| 1 | Lok. x,y,z | ☐ | ☐ | ☐ | ☐ | ☒ | ☒ | |
| 2 | Lok. x,y,z | ☐ | ☐ | ☐ | ☐ | ☒ | ☒ | |
| 3 | Lok. x,y,z | ☐ | ☐ | ☐ | ☐ | 5360.000 | ☒ | |

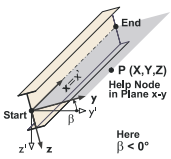
## 1.15/1 STAAFEXCENTRICITEITEN - ABSOLUUT



| Exc. No. | Referentie Systeem | Staafbegin - excentriciteit [mm] $e_{i,X}$ | $e_{i,Y}$ | $e_{i,Z}$ | Staafeind - Excentriciteit $e_{j,X}$ | $e_{j,Y}$ | $e_{j,Z}$ | Staafeindscharnier positie Staafbegin | Staafeinde |
|---|---|---|---|---|---|---|---|---|---|
| 1 | Globaal | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | op staaf | op staaf |

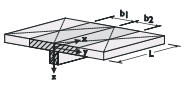
## 1.15/2 STAAFEXCENTRICITEITEN - RELATIEF

| Exc. No. | Doorsnede uitlijning y-as | Doorsnede uitlijning z-as | Dwarsoffset van doorsnede tot ander object: Object type | Object No. | y-as | z-as | Offset in langsrichting van aanlig: Staafbegin | Staafeinde |
|---|---|---|---|---|---|---|---|---|
| 1 | Midden | Boven (-z) | Geen | 0 | Midden | Midden | ☐ | ☐ |




## 1.17 STAVEN

| Stf. No. | Lijn No. | Staaf | Rotatie Type | Rotatie β[ï¿½] | Doorsnede Begin | Doorsnede Einde | Scharnier No. Begin | Scharnier No. Einde | Exc. No. | Deel No. | Lengte L [mm] | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1 | 5 | Ligger | Hoek | 90.00 | 1 | 1 | 1 | - | - | - | 4050 | Z |
| 2 | 6 | Ligger | Hoek | 90.00 | 1 | 1 | 1 | - | - | - | 4050 | Z |
| 3 | 7 | Ligger | Hoek | 90.00 | 1 | 1 | 1 | - | - | - | 4050 | Z |
| 4 | 8 | Ligger | Hoek | 90.00 | 1 | 1 | 1 | - | - | - | 4050 | Z |
| 5 | 9 | Ligger | Hoek | 90.00 | 1 | 1 | 1 | - | - | - | 4050 | Z |
| 6 | 10 | Ligger | Hoek | 90.00 | 1 | 1 | 1 | - | - | - | 4050 | Z |
| 7 | 11 | Ligger | Hoek | 0.00 | 2 | 2 | 3 | 3 | 1 | - | 4000 | Y |
| 8 | 12 | Ligger | Hoek | 0.00 | 2 | 2 | 3 | 3 | 1 | - | 4000 | Y |
| 9 | 13 | Ligger | Hoek | 0.00 | 2 | 2 | 3 | 3 | 1 | - | 4000 | Y |
| 10 | 14 | Ligger | Hoek | 0.00 | 3 | 3 | 2 | 2 | 1 | - | 3500 | X |
| 11 | 15 | Ligger | Hoek | 0.00 | 3 | 3 | 2 | 2 | 1 | - | 3500 | X |
| 12 | 16 | Ligger | Hoek | 0.00 | 3 | 3 | 2 | 2 | 1 | - | 3500 | X |
| 13 | 17 | Ligger | Hoek | 0.00 | 3 | 3 | 2 | 2 | 1 | - | 3500 | X |
| 14 | 18 | Trek | Hoek | 0.00 | 4 | 4 | - | - | 1 | - | 5315 | XY |
| 15 | 19 | Trek | Hoek | 0.00 | 4 | 4 | - | - | 1 | - | 5315 | XY |
| 16 | 20 | Trek | Hoek | 0.00 | 5 | 5 | - | - | - | - | 5353 | XZ |
| 17 | 21 | Trek | Hoek | 0.00 | 5 | 5 | - | - | - | - | 5353 | XZ |
| 18 | 22 | Trek | Hoek | 0.00 | 5 | 5 | - | - | - | - | 5353 | XZ |
| 19 | 23 | Trek | Hoek | 0.00 | 5 | 5 | - | - | - | - | 5353 | XZ |
| 20 | 28 | Trek | Hoek | 0.00 | 4 | 4 | - | - | 1 | - | 5315 | XY |
| 21 | 29 | Trek | Hoek | 0.00 | 4 | 4 | - | - | 1 | - | 5315 | XY |
| 22 | 24 | Rib | Hoek | 0.00 | 6 | 6 | - | - | | - | 3500 | X |
| 23 | 25 | Rib | Hoek | 0.00 | 6 | 6 | - | - | | - | 3500 | X |
| 24 | 26 | Rib | Hoek | 0.00 | 6 | 6 | - | - | | - | 3500 | X |
| 25 | 27 | Rib | Hoek | 0.00 | 6 | 6 | - | - | | - | 3500 | X |




## 1.18 RIBBEN

| Stf. No. | Rib Positie | Meewerkende breedte - Zijde Vlak No. | Meewerkende breedte - Zijde $b_1$ [mm] | Meewerkende breedte - Zijde Vlak No. | Meewerkende breedte - Zijde $b_2$ [mm] | Opm. |
|---|---|---|---|---|---|---|
| 22 | Op +z-rand | 1 | 200 | | 0 | |
| 23 | Op +z-rand | 1 | 200 | | 0 | |
| 24 | Op +z-rand | 1 | 200 | | 0 | |
| 25 | Op +z-rand | 1 | 200 | | 0 | |

## 2.1 BELASTINGSGEVALLEN

| Bel. Geval | BG omschrijving | EN 1990 \| NEN Actiecategorie | Eigen gewicht - Factor in richting: Actief | X | Y | Z |
|---|---|---|---|---|---|---|
| BG10 | PB: Eigen Gewicht | Blijvend | ☒ | 0.000 | 0.000 | -1.000 |
| BG20 | PB: Dakbedekking | Blijvend | ☐ | | | |
| BG30 | PB: KSZ - Metselwerk | Blijvend | ☐ | | | |
| BG40 | PB: Sandwichpaneel | Blijvend | ☐ | | | |
| BG100 | VB: Opgelegde belasting op vloeren 1 | Opgelegd - Categorie E: Industriefunctie en kantoorfunctie | ☐ | | | |
| BG120 | VB: Dakbelasting | Opgelegd - Categorie H: Daken | ☐ | | | |
| BG150 | VB: Heftruck | Opgelegd - Categorie E: Industriefunctie en kantoorfunctie | ☐ | | | |
| BG300 | VB: Sneeuw | Sneeuw (H ≤ 1000 m a.s.l.) | ☐ | | | |
| BG401 | VB: Wind (+X richting) | Wind | ☐ | | | |
| BG402 | VB: Wind (-X richting) | Wind | ☐ | | | |
| BG403 | VB: Wind (+Y richting) | Wind | ☐ | | | |
| BG404 | VB: Wind (-Y richting) | Wind | ☐ | | | |
| BG800 | DBG1 - Eigenvorm 1, richting - Y | Aardbeving | ☐ | | | |
| BG801 | DBG1 - Eigenvorm 2, richting - X | Aardbeving | ☐ | | | |
| BG802 | DBG1 - Eigenvorm 4, richting - X | Aardbeving | ☐ | | | |
| BG803 | DBG1 - Eigenvorm 5, richting - Y | Aardbeving | ☐ | | | |
| BG804 | DBG1 - Eigenvorm 7, richting - X | Aardbeving | ☐ | | | |

## 2.2 ACTIES

| Actie | Actie Omschrijving | EN 1990 \| NEN Actiecategorie | Inwerkend | Belastingsgevallen in actie | |
|---|---|---|---|---|---|
| A1 | Blijvend | Blijvend | Gelijktijdig | BG10<br>BG20<br>BG30<br>BG40 | PB: Eigen Gewicht<br>PB: Dakbedekking<br>PB: KSZ - Metselwerk<br>PB: Sandwichpaneel |
| A2 | Opgelegd | Opgelegd - Categorie E: Industriefunctie en kantoorfunctie | Alternatief | BG100<br>BG150 | VB: Opgelegde belasting op vloeren 1<br>VB: Heftruck |
| A3 | Opgelegd | Opgelegd - Categorie H: Daken | | BG120 | VB: Dakbelasting |
| A4 | Sneeuw | Sneeuw (H ≤ 1000 m a.s.l.) | | BG300 | VB: Sneeuw |
| A5 | Wind | Wind | Alternatief | BG401<br>BG402<br>BG403<br>BG404 | VB: Wind (+X richting)<br>VB: Wind (-X richting)<br>VB: Wind (+Y richting)<br>VB: Wind (-Y richting) |

## 2.3 COMBINATIEREGELS

| CE. No. | Omschrijving | EN 1990 \| NEN Ontwerpsituatie | Instellingen |
|---|---|---|---|
| CE1 | UGT | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | Beschouw : ☒Gunstige blijvende acties<br>Nummeren van gegenereerde combinaties: 1e Nummer van gegenereerde: 1 - Belastingscombinaties; 1 - Resultaatcombinaties<br>Opties: ☒Veranderlijke- en verkeersbelastingen worden samengevoegd als ï¿½ï¿½n onafhankelijke actie<br>Resultaatcombinaties: ☒Genereer aanvullende of/of resultaatcombinatie (omhullende); ☒Genereer aanvullend een verschillende of/of resultaatcombinatie voor elke combinatieregel<br>Gegenereerde belastingscombinaties<br>Berekeningsmethode : Geometrisch lineair |
| CE2 | BGT | BGT - Karakteristiek | Beschouw : ☐Gunstige blijvende acties<br>Nummeren van gegenereerde combinaties: 1e Nummer van gegenereerde: 1 - Belastingscombinaties; 1 - Resultaatcombinaties<br>Opties: ☒Veranderlijke- en verkeersbelastingen worden samengevoegd als ï¿½ï¿½n onafhankelijke actie<br>Resultaatcombinaties: ☒Genereer aanvullende of/of resultaatcombinatie (omhullende); ☒Genereer aanvullend een verschillende of/of resultaatcombinatie voor elke combinatieregel<br>Gegenereerde belastingscombinaties<br>Berekeningsmethode : Geometrisch lineair |
| CE3 | BGT | BGT - Frequent | Beschouw : ☐Gunstige blijvende acties<br>Nummeren van gegenereerde combinaties: 1e Nummer van gegenereerde: 1 - Belastingscombinaties; 1 - Resultaatcombinaties<br>Opties: ☒Veranderlijke- en verkeersbelastingen worden samengevoegd als ï¿½ï¿½n onafhankelijke actie<br>Resultaatcombinaties: ☒Genereer aanvullende of/of resultaatcombinatie (omhullende); ☒Genereer aanvullend een verschillende of/of resultaatcombinatie voor elke combinatieregel<br>Gegenereerde belastingscombinaties<br>Berekeningsmethode : Geometrisch lineair |
| CE4 | BGT | BGT - Quasi-blijvend | Beschouw : ☐Gunstige blijvende acties<br>Nummeren van gegenereerde combinaties: 1e Nummer van gegenereerde: 1 - Belastingscombinaties; 1 - Resultaatcombinaties<br>Opties: ☒Veranderlijke- en verkeersbelastingen worden samengevoegd als ï¿½ï¿½n onafhankelijke actie<br>Resultaatcombinaties: ☒Genereer aanvullende of/of resultaatcombinatie (omhullende); ☒Genereer aanvullend een verschillende of/of resultaatcombinatie voor elke combinatieregel<br>Gegenereerde belastingscombinaties<br>Berekeningsmethode : Geometrisch lineair |

## 2.4 ACTIECOMBINATIES

| Actie-Combin. | Actiecombinatie Omschrijving | EN 1990 \| NEN Ontwerpsituatie | No. | Factor | Actie | |
|---|---|---|---|---|---|---|
| AC1 | 1.49G | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.485 | A1 | Blijvend |
| AC2 | 1.49G + 1.65QiE | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.485 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| AC3 | 1.49G + 1.65QiE + 0.00QiH | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.485 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A3 | Opgelegd |
| AC4 | 1.49G + 1.65QiE + 0.00QiH + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.485 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A3 | Opgelegd |
| | | | 4 | 0.00 | A5 | Wind |

## 2.4 ACTIECOMBINATIES

| Actie-Combin. | Actiecombinatie Omschrijving | EN 1990 \| NEN Ontwerpsituatie | No. | Factor | Actie | |
|---|---|---|---|---|---|---|
| AC5 | 1.49G + 1.65QiE + 0.00Qs | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.485 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A4 | Sneeuw |
| AC6 | 1.49G + 1.65QiE + 0.00Qs + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.485 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A4 | Sneeuw |
| | | | 4 | 0.00 | A5 | Wind |
| AC7 | 1.49G + 1.65QiE + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.485 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A5 | Wind |
| AC8 | 1.49G + 0.00QiH | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.485 | A1 | Blijvend |
| | | | 2 | 0.00 | A3 | Opgelegd |
| AC9 | 1.49G + 0.00QiH + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.485 | A1 | Blijvend |
| | | | 2 | 0.00 | A3 | Opgelegd |
| | | | 3 | 0.00 | A5 | Wind |
| AC10 | 1.49G + 0.00Qs | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.485 | A1 | Blijvend |
| | | | 2 | 0.00 | A4 | Sneeuw |
| AC11 | 1.49G + 0.00Qs + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.485 | A1 | Blijvend |
| | | | 2 | 0.00 | A4 | Sneeuw |
| | | | 3 | 0.00 | A5 | Wind |
| AC12 | 1.49G + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.485 | A1 | Blijvend |
| | | | 2 | 0.00 | A5 | Wind |
| AC13 | 0.90G | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| AC14 | 0.90G + 1.65QiE | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| AC15 | 0.90G + 1.65QiE + 0.00QiH | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A3 | Opgelegd |
| AC16 | 0.90G + 1.65QiE + 0.00QiH + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A3 | Opgelegd |
| | | | 4 | 0.00 | A5 | Wind |
| AC17 | 0.90G + 1.65QiE + 0.00Qs | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A4 | Sneeuw |
| AC18 | 0.90G + 1.65QiE + 0.00Qs + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A4 | Sneeuw |
| | | | 4 | 0.00 | A5 | Wind |
| AC19 | 0.90G + 1.65QiE + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A5 | Wind |
| AC20 | 0.90G + 0.00QiH | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 0.00 | A3 | Opgelegd |
| AC21 | 0.90G + 0.00QiH + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 0.00 | A3 | Opgelegd |
| | | | 3 | 0.00 | A5 | Wind |
| AC22 | 0.90G + 0.00Qs | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 0.00 | A4 | Sneeuw |
| AC23 | 0.90G + 0.00Qs + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 0.00 | A4 | Sneeuw |
| | | | 3 | 0.00 | A5 | Wind |
| AC24 | 0.90G + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 0.00 | A5 | Wind |
| AC25 | 1.32G | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |
| AC26 | 1.32G + 1.65QiE | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| AC27 | 1.32G + 1.65QiE + 0.00QiH | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A3 | Opgelegd |
| AC28 | 1.32G + 1.65QiE + 0.00QiH + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A3 | Opgelegd |
| | | | 4 | 0.00 | A5 | Wind |
| AC29 | 1.32G + 1.65QiE + 0.00Qs | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |

## 2.4 ACTIECOMBINATIES

| Actie-Combin. | Actiecombinatie Omschrijving | EN 1990 \| NEN Ontwerpsituatie | No. | Factor | Actie | |
|---|---|---|---|---|---|---|
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A4 | Sneeuw |
| AC30 | 1.32G + 1.65QiE + 0.00Qs + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A4 | Sneeuw |
| | | | 4 | 0.00 | A5 | Wind |
| AC31 | 1.32G + 1.65QiE + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A5 | Wind |
| AC32 | 1.32G + 1.65QiH | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |
| | | | 2 | 1.65 | A3 | Opgelegd |
| AC33 | 1.32G + 1.65QiE + 1.65QiH | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 1.65 | A3 | Opgelegd |
| AC34 | 1.32G + 1.65QiE + 1.65QiH + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 1.65 | A3 | Opgelegd |
| | | | 4 | 0.00 | A5 | Wind |
| AC35 | 1.32G + 1.65QiH + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |
| | | | 2 | 1.65 | A3 | Opgelegd |
| | | | 3 | 0.00 | A5 | Wind |
| AC36 | 1.32G + 1.65Qs | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |
| | | | 2 | 1.65 | A4 | Sneeuw |
| AC37 | 1.32G + 1.65QiE + 1.65Qs | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 1.65 | A4 | Sneeuw |
| AC38 | 1.32G + 1.65QiE + 1.65Qs + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 1.65 | A4 | Sneeuw |
| | | | 4 | 0.00 | A5 | Wind |
| AC39 | 1.32G + 1.65Qs + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |
| | | | 2 | 1.65 | A4 | Sneeuw |
| | | | 3 | 0.00 | A5 | Wind |
| AC40 | 1.32G + 1.65Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |
| | | | 2 | 1.65 | A5 | Wind |
| AC41 | 1.32G + 1.65QiE + 1.65Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 1.65 | A5 | Wind |
| AC42 | 1.32G + 1.65QiE + 0.00QiH + 1.65Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A3 | Opgelegd |
| | | | 4 | 1.65 | A5 | Wind |
| AC43 | 1.32G + 1.65QiE + 0.00Qs + 1.65Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A4 | Sneeuw |
| | | | 4 | 1.65 | A5 | Wind |
| AC44 | 1.32G + 0.00QiH + 1.65Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |
| | | | 2 | 0.00 | A3 | Opgelegd |
| | | | 3 | 1.65 | A5 | Wind |
| AC45 | 1.32G + 0.00Qs + 1.65Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 1.3217 | A1 | Blijvend |
| | | | 2 | 0.00 | A4 | Sneeuw |
| | | | 3 | 1.65 | A5 | Wind |
| AC46 | 0.90G | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| AC47 | 0.90G + 1.65QiE | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| AC48 | 0.90G + 1.65QiE + 0.00QiH | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A3 | Opgelegd |
| AC49 | 0.90G + 1.65QiE + 0.00QiH + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A3 | Opgelegd |
| | | | 4 | 0.00 | A5 | Wind |
| AC50 | 0.90G + 1.65QiE + 0.00Qs | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A4 | Sneeuw |
| AC51 | 0.90G + 1.65QiE + 0.00Qs + 0 | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |

## 2.4 ACTIECOMBINATIES

| Actie-Combin. | Actiecombinatie Omschrijving | EN 1990 \| NEN Ontwerpsituatie | No. | Factor | Actie | |
|---|---|---|---|---|---|---|
| | 0.00Qw | | | | | |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A4 | Sneeuw |
| | | | 4 | 0.00 | A5 | Wind |
| AC52 | 0.90G + 1.65QiE + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A5 | Wind |
| AC53 | 0.90G + 1.65QiH | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A3 | Opgelegd |
| AC54 | 0.90G + 1.65QiE + 1.65QiH | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 1.65 | A3 | Opgelegd |
| AC55 | 0.90G + 1.65QiE + 1.65QiH + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 1.65 | A3 | Opgelegd |
| | | | 4 | 0.00 | A5 | Wind |
| AC56 | 0.90G + 1.65QiH + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A3 | Opgelegd |
| | | | 3 | 0.00 | A5 | Wind |
| AC57 | 0.90G + 1.65Qs | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A4 | Sneeuw |
| AC58 | 0.90G + 1.65QiE + 1.65Qs | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 1.65 | A4 | Sneeuw |
| AC59 | 0.90G + 1.65QiE + 1.65Qs + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 1.65 | A4 | Sneeuw |
| | | | 4 | 0.00 | A5 | Wind |
| AC60 | 0.90G + 1.65Qs + 0.00Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A4 | Sneeuw |
| | | | 3 | 0.00 | A5 | Wind |
| AC61 | 0.90G + 1.65Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A5 | Wind |
| AC62 | 0.90G + 1.65QiE + 1.65Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 1.65 | A5 | Wind |
| AC63 | 0.90G + 1.65QiE + 0.00QiH + 1.65Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A3 | Opgelegd |
| | | | 4 | 1.65 | A5 | Wind |
| AC64 | 0.90G + 1.65QiE + 0.00Qs + 1.65Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 1.65 | A2 | Opgelegd |
| | | | 3 | 0.00 | A4 | Sneeuw |
| | | | 4 | 1.65 | A5 | Wind |
| AC65 | 0.90G + 0.00QiH + 1.65Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 0.00 | A3 | Opgelegd |
| | | | 3 | 1.65 | A5 | Wind |
| AC66 | 0.90G + 0.00Qs + 1.65Qw | UGT (STR/GEO) - blijvend / tijdelijk - verg. 6.10a en 6.10b | 1 | 0.90 | A1 | Blijvend |
| | | | 2 | 0.00 | A4 | Sneeuw |
| | | | 3 | 1.65 | A5 | Wind |
| AC67 | 1.00G | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |
| AC68 | 1.00G + 1.00QiE | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 1.00 | A2 | Opgelegd |
| AC69 | 1.00G + 1.00QiE + 0.00QiH | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 1.00 | A2 | Opgelegd |
| | | | 3 | 0.00 | A3 | Opgelegd |
| AC70 | 1.00G + 1.00QiE + 0.00QiH + 0.00Qw | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 1.00 | A2 | Opgelegd |
| | | | 3 | 0.00 | A3 | Opgelegd |
| | | | 4 | 0.00 | A5 | Wind |
| AC71 | 1.00G + 1.00QiE + 0.00Qs | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 1.00 | A2 | Opgelegd |
| | | | 3 | 0.00 | A4 | Sneeuw |
| AC72 | 1.00G + 1.00QiE + 0.00Qs + 0.00Qw | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 1.00 | A2 | Opgelegd |
| | | | 3 | 0.00 | A4 | Sneeuw |
| | | | 4 | 0.00 | A5 | Wind |
| AC73 | 1.00G + 1.00QiE + 0.00Qw | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |

## 2.4 ACTIECOMBINATIES

| Actie-Combin. | Actiecombinatie Omschrijving | EN 1990 \| NEN Ontwerpsituatie | No. | Factor | Actie | |
|---|---|---|---|---|---|---|
| | | | 2 | 1.00 | A2 | Opgelegd |
| | | | 3 | 0.00 | A5 | Wind |
| AC74 | 1.00G + 1.00QiH | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 1.00 | A3 | Opgelegd |
| AC75 | 1.00G + 1.00QiE + 1.00QiH | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 1.00 | A2 | Opgelegd |
| | | | 3 | 1.00 | A3 | Opgelegd |
| AC76 | 1.00G + 1.00QiE + 1.00QiH + 0.00Qw | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 1.00 | A2 | Opgelegd |
| | | | 3 | 1.00 | A3 | Opgelegd |
| | | | 4 | 0.00 | A5 | Wind |
| AC77 | 1.00G + 1.00QiH + 0.00Qw | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 1.00 | A3 | Opgelegd |
| | | | 3 | 0.00 | A5 | Wind |
| AC78 | 1.00G + 1.00Qs | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 1.00 | A4 | Sneeuw |
| AC79 | 1.00G + 1.00QiE + 1.00Qs | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 1.00 | A2 | Opgelegd |
| | | | 3 | 1.00 | A4 | Sneeuw |
| AC80 | 1.00G + 1.00QiE + 1.00Qs + 0.00Qw | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 1.00 | A2 | Opgelegd |
| | | | 3 | 1.00 | A4 | Sneeuw |
| | | | 4 | 0.00 | A5 | Wind |
| AC81 | 1.00G + 1.00Qs + 0.00Qw | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 1.00 | A4 | Sneeuw |
| | | | 3 | 0.00 | A5 | Wind |
| AC82 | 1.00G + 1.00Qw | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 1.00 | A5 | Wind |
| AC83 | 1.00G + 1.00QiE + 1.00Qw | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 1.00 | A2 | Opgelegd |
| | | | 3 | 1.00 | A5 | Wind |
| AC84 | 1.00G + 1.00QiE + 0.00QiH + 1.00Qw | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 1.00 | A2 | Opgelegd |
| | | | 3 | 0.00 | A3 | Opgelegd |
| | | | 4 | 1.00 | A5 | Wind |
| AC85 | 1.00G + 1.00QiE + 0.00Qs + 1.00Qw | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 1.00 | A2 | Opgelegd |
| | | | 3 | 0.00 | A4 | Sneeuw |
| | | | 4 | 1.00 | A5 | Wind |
| AC86 | 1.00G + 0.00QiH + 1.00Qw | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.00 | A3 | Opgelegd |
| | | | 3 | 1.00 | A5 | Wind |
| AC87 | 1.00G + 0.00Qs + 1.00Qw | BGT - Karakteristiek | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.00 | A4 | Sneeuw |
| | | | 3 | 1.00 | A5 | Wind |
| AC88 | 1.00G | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |
| AC89 | 1.00G + 0.90QiE | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.90 | A2 | Opgelegd |
| AC90 | 1.00G + 0.90QiE + 0.00QiH | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.90 | A2 | Opgelegd |
| | | | 3 | 0.00 | A3 | Opgelegd |
| AC91 | 1.00G + 0.90QiE + 0.00QiH + 0.00Qw | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.90 | A2 | Opgelegd |
| | | | 3 | 0.00 | A3 | Opgelegd |
| | | | 4 | 0.00 | A5 | Wind |
| AC92 | 1.00G + 0.90QiE + 0.00Qs | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.90 | A2 | Opgelegd |
| | | | 3 | 0.00 | A4 | Sneeuw |
| AC93 | 1.00G + 0.90QiE + 0.00Qs + 0.00Qw | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.90 | A2 | Opgelegd |
| | | | 3 | 0.00 | A4 | Sneeuw |
| | | | 4 | 0.00 | A5 | Wind |
| AC94 | 1.00G + 0.90QiE + 0.00Qw | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.90 | A2 | Opgelegd |
| | | | 3 | 0.00 | A5 | Wind |
| AC95 | 1.00G + 0.00QiH | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.00 | A3 | Opgelegd |
| AC96 | 1.00G + 0.80QiE + 0.00QiH | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.80 | A2 | Opgelegd |
| | | | 3 | 0.00 | A3 | Opgelegd |
| AC97 | 1.00G + 0.80QiE + | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |

## 2.4 ACTIECOMBINATIES

| Actie-Combin. | Actiecombinatie Omschrijving | EN 1990 \| NEN Ontwerpsituatie | No. | Factor | Actie | |
|---|---|---|---|---|---|---|
| | + 0.00QiH + 0.00Qw | | | | | |
| | | | 2 | 0.80 | A2 | Opgelegd |
| | | | 3 | 0.00 | A3 | Opgelegd |
| | | | 4 | 0.00 | A5 | Wind |
| AC98 | 1.00G + 0.00QiH + 0.00Qw | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.00 | A3 | Opgelegd |
| | | | 3 | 0.00 | A5 | Wind |
| AC99 | 1.00G + 0.20Qs | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.20 | A4 | Sneeuw |
| AC100 | 1.00G + 0.80QiE + 0.20Qs | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.80 | A2 | Opgelegd |
| | | | 3 | 0.20 | A4 | Sneeuw |
| AC101 | 1.00G + 0.80QiE + 0.20Qs + 0.00Qw | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.80 | A2 | Opgelegd |
| | | | 3 | 0.20 | A4 | Sneeuw |
| | | | 4 | 0.00 | A5 | Wind |
| AC102 | 1.00G + 0.20Qs + 0.00Qw | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.20 | A4 | Sneeuw |
| | | | 3 | 0.00 | A5 | Wind |
| AC103 | 1.00G + 0.20Qw | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.20 | A5 | Wind |
| AC104 | 1.00G + 0.80QiE + 0.20Qw | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.80 | A2 | Opgelegd |
| | | | 3 | 0.20 | A5 | Wind |
| AC105 | 1.00G + 0.80QiE + 0.00QiH + 0.20Qw | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.80 | A2 | Opgelegd |
| | | | 3 | 0.00 | A3 | Opgelegd |
| | | | 4 | 0.20 | A5 | Wind |
| AC106 | 1.00G + 0.80QiE + 0.00Qs + 0.20Qw | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.80 | A2 | Opgelegd |
| | | | 3 | 0.00 | A4 | Sneeuw |
| | | | 4 | 0.20 | A5 | Wind |
| AC107 | 1.00G + 0.00QiH + 0.20Qw | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.00 | A3 | Opgelegd |
| | | | 3 | 0.20 | A5 | Wind |
| AC108 | 1.00G + 0.00Qs + 0.20Qw | BGT - Frequent | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.00 | A4 | Sneeuw |
| | | | 3 | 0.20 | A5 | Wind |
| AC109 | 1.00G | BGT - Quasi-blijvend | 1 | 1.00 | A1 | Blijvend |
| AC110 | 1.00G + 0.80QiE | BGT - Quasi-blijvend | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.80 | A2 | Opgelegd |
| AC111 | 1.00G + 0.80QiE + 0.00QiH | BGT - Quasi-blijvend | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.80 | A2 | Opgelegd |
| | | | 3 | 0.00 | A3 | Opgelegd |
| AC112 | 1.00G + 0.80QiE + 0.00QiH + 0.00Qw | BGT - Quasi-blijvend | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.80 | A2 | Opgelegd |
| | | | 3 | 0.00 | A3 | Opgelegd |
| | | | 4 | 0.00 | A5 | Wind |
| AC113 | 1.00G + 0.80QiE + 0.00Qs | BGT - Quasi-blijvend | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.80 | A2 | Opgelegd |
| | | | 3 | 0.00 | A4 | Sneeuw |
| AC114 | 1.00G + 0.80QiE + 0.00Qs + 0.00Qw | BGT - Quasi-blijvend | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.80 | A2 | Opgelegd |
| | | | 3 | 0.00 | A4 | Sneeuw |
| | | | 4 | 0.00 | A5 | Wind |
| AC115 | 1.00G + 0.80QiE + 0.00Qw | BGT - Quasi-blijvend | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.80 | A2 | Opgelegd |
| | | | 3 | 0.00 | A5 | Wind |
| AC116 | 1.00G + 0.00QiH | BGT - Quasi-blijvend | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.00 | A3 | Opgelegd |
| AC117 | 1.00G + 0.00QiH + 0.00Qw | BGT - Quasi-blijvend | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.00 | A3 | Opgelegd |
| | | | 3 | 0.00 | A5 | Wind |
| AC118 | 1.00G + 0.00Qs | BGT - Quasi-blijvend | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.00 | A4 | Sneeuw |
| AC119 | 1.00G + 0.00Qs + 0.00Qw | BGT - Quasi-blijvend | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.00 | A4 | Sneeuw |
| | | | 3 | 0.00 | A5 | Wind |
| AC120 | 1.00G + 0.00Qw | BGT - Quasi-blijvend | 1 | 1.00 | A1 | Blijvend |
| | | | 2 | 0.00 | A5 | Wind |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| BC1 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| BC2 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| BC3 | ULS' | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG150 | 1 | 1.49 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.49 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.49 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.49 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| BC4 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| BC5 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| BC6 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| BC7 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| BC8 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| BC9 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG120 | VB: Dakbelasting |
| BC10 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| BC11 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG150 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| BC12 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG300 | VB: Sneeuw |
| BC13 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG300 | VB: Sneeuw |
| BC14 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG300 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| | | | 6 | 1.65 | BG300 | VB: Sneeuw |
| BC15 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC16 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC17 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC18 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC19 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC20 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC21 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC22 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC23 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG401 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| | | | 6 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC24 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG402 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| | | | 6 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC25 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG403 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| | | | 6 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC26 | ULS' | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG404 | 1 | 1.32 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.32 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.32 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.32 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| | | | 6 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC27 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG120 | VB: Dakbelasting |
| BC28 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG120 | VB: Dakbelasting |
| BC29 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG150 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.65 | BG150 | VB: Heftruck |
| BC30 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG300 | VB: Sneeuw |
| BC31 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG300 | VB: Sneeuw |
| BC32 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG300 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| | | | 6 | 1.65 | BG300 | VB: Sneeuw |
| BC33 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC34 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC35 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC36 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC37 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC38 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC39 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC40 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC41 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG401 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| | | | 6 | 1.65 | BG401 | VB: Wind (+X richting) |
| BC42 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG402 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| | | | 6 | 1.65 | BG402 | VB: Wind (-X richting) |
| BC43 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG403 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| | | | 6 | 1.65 | BG403 | VB: Wind (+Y richting) |
| BC44 | ULS' | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG404 | 1 | 0.90 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 0.90 | BG20 | PB: Dakbedekking |
| | | | 3 | 0.90 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 0.90 | BG40 | PB: Sandwichpaneel |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 5 | 1.65 | BG150 | VB: Heftruck |
| | | | 6 | 1.65 | BG404 | VB: Wind (-Y richting) |
| BC45 | S Ch | BG10 + BG20 + BG30 + BG40 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| BC46 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| BC47 | S Ch | BG10 + BG20 + BG30 + BG40 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG150 | VB: Heftruck |
| BC48 | S Ch | BG10 + BG20 + BG30 + BG40 + BG120 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG120 | VB: Dakbelasting |
| BC49 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG120 | VB: Dakbelasting |
| BC50 | S Ch | BG10 + BG20 + BG30 + BG40 + BG120 + BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG120 | VB: Dakbelasting |
| | | | 6 | 1.00 | BG150 | VB: Heftruck |
| BC51 | S Ch | BG10 + BG20 + BG30 + BG40 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG300 | VB: Sneeuw |
| BC52 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG300 | VB: Sneeuw |
| BC53 | S Ch | BG10 + BG20 + BG30 + BG40 + BG150 + BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG150 | VB: Heftruck |
| | | | 6 | 1.00 | BG300 | VB: Sneeuw |
| BC54 | S Ch | BG10 + BG20 + BG30 + BG40 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC55 | S Ch | BG10 + BG20 + BG30 + BG40 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC56 | S Ch | BG10 + BG20 + BG30 + BG40 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC57 | S Ch | BG10 + BG20 + BG30 + BG40 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC58 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC59 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC60 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | OS | Belastingscombinatie Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 6 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC61 | S Ch | BG10 + BG20 + BG30 + BG40 + BG100 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC62 | S Ch | BG10 + BG20 + BG30 + BG40 + BG150 + BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG150 | VB: Heftruck |
| | | | 6 | 1.00 | BG401 | VB: Wind (+X richting) |
| BC63 | S Ch | BG10 + BG20 + BG30 + BG40 + BG150 + BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG150 | VB: Heftruck |
| | | | 6 | 1.00 | BG402 | VB: Wind (-X richting) |
| BC64 | S Ch | BG10 + BG20 + BG30 + BG40 + BG150 + BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG150 | VB: Heftruck |
| | | | 6 | 1.00 | BG403 | VB: Wind (+Y richting) |
| BC65 | S Ch | BG10 + BG20 + BG30 + BG40 + BG150 + BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 1.00 | BG150 | VB: Heftruck |
| | | | 6 | 1.00 | BG404 | VB: Wind (-Y richting) |
| BC66 | S Fr | BG10 + BG20 + BG30 + BG40 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| BC67 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| BC68 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.9*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.90 | BG150 | VB: Heftruck |
| BC69 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.00 | BG120 | VB: Dakbelasting |
| BC70 | S Fr | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.00 | BG120 | VB: Dakbelasting |
| | | | 6 | 0.80 | BG150 | VB: Heftruck |
| BC71 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.20 | BG300 | VB: Sneeuw |
| BC72 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.20 | BG300 | VB: Sneeuw |
| BC73 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG300 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG150 | VB: Heftruck |
| | | | 6 | 0.20 | BG300 | VB: Sneeuw |
| BC74 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC75 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC76 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |

## 2.5 BELASTINGSCOMBINATIES

| Last Combin. | Belastingscombinatie OS | Omschrijving | No. | Factor | Belastingsgeval | |
|---|---|---|---|---|---|---|
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC77 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC78 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC79 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC80 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC81 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| | | | 6 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC82 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG401 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG150 | VB: Heftruck |
| | | | 6 | 0.20 | BG401 | VB: Wind (+X richting) |
| BC83 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG402 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG150 | VB: Heftruck |
| | | | 6 | 0.20 | BG402 | VB: Wind (-X richting) |
| BC84 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG403 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG150 | VB: Heftruck |
| | | | 6 | 0.20 | BG403 | VB: Wind (+Y richting) |
| BC85 | S Fr | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG404 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG150 | VB: Heftruck |
| | | | 6 | 0.20 | BG404 | VB: Wind (-Y richting) |
| BC86 | S Qp | BG10 + BG20 + BG30 + BG40 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| BC87 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG100 | VB: Opgelegde belasting op vloeren 1 |
| BC88 | S Qp | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 | 1 | 1.00 | BG10 | PB: Eigen Gewicht |
| | | | 2 | 1.00 | BG20 | PB: Dakbedekking |
| | | | 3 | 1.00 | BG30 | PB: KSZ - Metselwerk |
| | | | 4 | 1.00 | BG40 | PB: Sandwichpaneel |
| | | | 5 | 0.80 | BG150 | VB: Heftruck |

## 2.7 RESULTAATCOMBINATIES

| Resulta Combin. | Omschrijving | Belasting |
|---|---|---|
| RC1 | UGT (STR/GEO) - Blijvend / tijdelijk - verg. 6.10a en 6.10b | BC1/b of tot BC44 |
| RC2 | BGT - Karakteristiek | BC45/b of tot BC65 |
| RC3 | BGT - Frequent | BC66/b of tot BC85 |
| RC4 | BGT - Quasi-blijvend | BC86/b of tot BC88 |
| RC10 | DBG1 - Resultaatomhullende - X | BG801/b + BG802/b + BG804/b |
| RC11 | DBG1 - Resultaatomhullende - Y | BG800/b + BG803/b |

## 2.7 RESULTAATCOMBINATIES

| Resulta Combin. | Omschrijving | Belasting |
|---|---|---|
| | Y | |
| RC12 | DBG1 - Resultaatomhullende - 100% X/ 30% Y | RC10/b + 0.3*RC11/b |
| RC13 | DBG1 - Resultaatomhullende - 30% X/ 100% Y | 0.3*RC10/b + RC11/b |
| RC20 | Tabel NB.7 A1.3 | BG10/b + BG20/b + BG30/b + BG40/b + 0.8*BG120 + 0.8*BG100 of 0.8*BG150 of RC12 of RC13 |

**BG20**
PB: Dakbedekking

## 3.15 GEGENEREERDE LASTEN

BG20: PB: Dakbedekking

| No. | Belastingomschrijving | | | | | |
|---|---|---|---|---|---|---|
| 2 | Van Vlaklasten via vlak | | | | | |
| | Vlaklastrichting | Globaal gerelateerd aan geprojecteerde vlak: | | : | ☒ZP | |
| | Lasttoewijzingsbereik | ☒Volledig gesloten vlak | | | | |
| | Lastverdelingstype: | ☒Gecombineerd | | | | |
| | Vlaklast grootte | ☒Constant | | : | -0.850 | kN/m² |
| | Grens van vlaklast vlak | Hoekknopen | | : | 6,10,16,12 | |
| | | Aanwijzing | | : | Elke rij in de lijst geeft een vlak weer | |
| | Verwijder invloed van | Enkele Liggers | | : | 14,15 | |
| | | Staven parallel aan Staaf | | : | 11 | |
| | Gegenereerde totale belastingen in richting | Σ P Vlakken | X | : | 0.00 | kN |
| | | | Y | : | 0.00 | kN |
| | | | Z | : | -23.80 | kN |
| | | ΣP Staven | X | : | 0.00 | kN |
| | | | Y | : | 0.00 | kN |
| | | | Z | : | -23.80 | kN |
| | Totale moment bij de oorsprong | Σ M Vlakken | X | : | -47.60 | kNm |
| | | | Y | : | 83.30 | kNm |
| | | | Z | : | 0.00 | kNm |
| | | ΣM Staven | X | : | -47.60 | kNm |
| | | | Y | : | 83.30 | kNm |
| | | | Z | : | 0.00 | kNm |
| | Cellen geselecteerd voor genereren | Σ aantal cellen | | : | 2 | |
| | | Σ cel vlak | | : | 28000000 | mm² |
| | Converteren van Vlaklasten naar Staaf No. | | | : | 7-9 | |

**BG30**
PB: KSZ - Metselwerk

## 3.3 LIJNBELASTINGEN

BG30: PB: KSZ - Metselwerk

| No. | Referentie tot | Op lijnen No. | Belasting Type | Belasting Verdeling | Belasting Richting | Lastparameters Symbool | Waarde | Eenheid |
|---|---|---|---|---|---|---|---|---|
| 1 | Lijnen | 24-27 | Kracht | Gelijkmatig | ZL | p | -11.25 | kN/m |

**BG40**
PB: Sandwichpaneel

## 3.15 GEGENEREERDE LASTEN

BG40: PB: Sandwichpaneel

| No. | Belastingomschrijving | | | | | |
|---|---|---|---|---|---|---|
| 1 | Van Vlaklasten via vlak | | | | | |
| | Vlaklastrichting | Globaal t.o.v. echt vlak: | | : | ☒ZL | |
| | Lasttoewijzingsbereik | ☒Volledig gesloten vlak | | | | |
| | Lastverdelingstype: | ☒Gecombineerd | | | | |
| | Vlaklast grootte | ☒Constant | | : | -0.300 | kN/m² |
| | Grens van vlaklast vlak | Hoekknopen | | : | 17,18,10,6; 18,20,16,10; 17,19,12,6; 19,20,16,12 | |
| | | Aanwijzing | | : | Elke rij in de lijst geeft een vlak weer | |
| | Verwijder invloed van | Staven parallel aan Staaf | | : | 9,10 | |
| | Gegenereerde totale belastingen in richting | Σ P Vlakken | X | : | 0.00 | kN |
| | | | Y | : | 0.00 | kN |
| | | | Z | : | -10.23 | kN |
| | | ΣP Staven | X | : | 0.00 | kN |
| | | | Y | : | 0.00 | kN |
| | | | Z | : | -10.23 | kN |
| | Totale moment bij de oorsprong | Σ M Vlakken | X | : | -20.46 | kNm |
| | | | Y | : | 35.81 | kNm |
| | | | Z | : | 0.00 | kNm |
| | | ΣM Staven | X | : | -20.46 | kNm |
| | | | Y | : | 35.81 | kNm |
| | | | Z | : | 0.00 | kNm |
| | Cellen geselecteerd voor genereren | Σ aantal cellen | | : | 6 | |
| | | Σ cel vlak | | : | 34100004 | mm² |

## 3.15 GEGENEREERDE LASTEN — BG40: PB: Sandwichpaneel

| No. | Belastingomschrijving | | |
|---|---|---|---|
| | Converteren van Vlaklasten naar Staaf No. | : | 1-6 |

**BG100**
VB: Opgelegde belasting op vloeren 1

## 3.4 VLAKLASTEN — BG100: VB: Opgelegde belasting op vloeren 1

| No. | Op vlakken No. | Belasting Type | Belasting Verdeling | Belasting Richting | Lastparameters Symbool | Waarde | Eenheid |
|---|---|---|---|---|---|---|---|
| 1 | 1 | Kracht | Gelijkmatig | ZL | p | -3.000 | kN/m² |

**BG120**
VB: Dakbelasting

## 3.15 GEGENEREERDE LASTEN — BG120: VB: Dakbelasting

| No. | Belastingomschrijving | | | | | |
|---|---|---|---|---|---|---|
| 1 | Van Vlaklasten via vlak | | | | | |
| | Vlaklastrichting | Globaal gerelateerd aan geprojecteerde vlak: | | : | ☒ZP | |
| | Lasttoewijzingsbereik | ☒Volledig gesloten vlak | | | | |
| | Lastverdelingstype: | ☒Gecombineerd | | | | |
| | Vlaklast grootte | ☒Constant | | : | -1.000 | kN/m² |
| | Grens van vlaklast vlak | Hoekknopen | | : | 6,10,16,12 | |
| | | Aanwijzing | | : | Elke rij in de lijst geeft een vlak weer | |
| | Verwijder invloed van | Staven parallel aan Staaf | | : | 11 | |
| | Gegenereerde totale belastingen in richting | $\Sigma P_{Vlakken}$ | X | : | 0.00 | kN |
| | | | Y | : | 0.00 | kN |
| | | | Z | : | -28.00 | kN |
| | | $\Sigma P_{Staven}$ | X | : | 0.00 | kN |
| | | | Y | : | 0.00 | kN |
| | | | Z | : | -28.00 | kN |
| | Totale moment bij de oorsprong | $\Sigma M_{Vlakken}$ | X | : | -56.00 | kNm |
| | | | Y | : | 98.00 | kNm |
| | | | Z | : | 0.00 | kNm |
| | | $\Sigma M_{Staven}$ | X | : | -56.00 | kNm |
| | | | Y | : | 98.00 | kNm |
| | | | Z | : | 0.00 | kNm |
| | Cellen geselecteerd voor genereren | Σ aantal cellen | | : | 2 | |
| | | Σ cel vlak | | : | 28000000 | mm² |
| | Converteren van Vlaklasten naar Staaf No. | | | : | 7-9 | |

**BG150**
VB: Heftruck

## 3.1 KNOOPBELASTINGEN - PER COMPONENT - COï¿½RDINATENSYSTEEM — BG150: VB: Heftruck

| No. | Op Knoop No. | Coï¿½rdinaten Syteem | Kracht [kN] $P_X$ / $P_U$ | $P_Y$ / $P_V$ | $P_Z$ / $P_W$ | Moment [kNm] $M_X$ / $M_U$ | $M_Y$ / $M_V$ | $M_Z$ / $M_W$ |
|---|---|---|---|---|---|---|---|---|
| 1 | 21-24 | 0 \| Globaal XYZ | 6.00 | 0.00 | -28.00 | 0.00 | 0.00 | 0.00 |

**BG300**
VB: Sneeuw

## 3.15 GEGENEREERDE LASTEN — BG300: VB: Sneeuw

| No. | Belastingomschrijving | | | | | |
|---|---|---|---|---|---|---|
| 1 | Van Vlaklasten via vlak | | | | | |
| | Vlaklastrichting | Globaal gerelateerd aan geprojecteerde vlak: | | : | ☒ZP | |
| | Lasttoewijzingsbereik | ☒Volledig gesloten vlak | | | | |
| | Lastverdelingstype: | ☒Gecombineerd | | | | |
| | Vlaklast grootte | ☒Constant | | : | -1.400 | kN/m² |
| | Grens van vlaklast vlak | Hoekknopen | | : | 6,10,16,12 | |
| | | Aanwijzing | | : | Elke rij in de lijst geeft een vlak weer | |
| | Verwijder invloed van | Staven parallel aan Staaf | | : | 11 | |
| | Gegenereerde totale belastingen in richting | $\Sigma P_{Vlakken}$ | X | : | 0.00 | kN |
| | | | Y | : | 0.00 | kN |
| | | | Z | : | -39.20 | kN |
| | | $\Sigma P_{Staven}$ | X | : | 0.00 | kN |
| | | | Y | : | 0.00 | kN |
| | | | Z | : | -39.20 | kN |
| | Totale moment bij de oorsprong | $\Sigma M_{Vlakken}$ | X | : | -78.40 | kNm |
| | | | Y | : | 137.20 | kNm |
| | | | Z | : | 0.00 | kNm |
| | | $\Sigma M_{Staven}$ | X | : | -78.40 | kNm |
| | | | Y | : | 137.20 | kNm |
| | | | Z | : | 0.00 | kNm |
| | Cellen geselecteerd voor genereren | Σ aantal cellen | | : | 2 | |
| | | Σ cel vlak | | : | 28000000 | mm² |

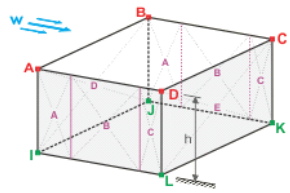
## 3.15 GEGENEREERDE LASTEN — BG300: VB: Sneeuw

| No. | Belastingomschrijving | | | |
|---|---|---|---|---|
| | Converteren van Vlaklasten naar Staaf No. | | : | 7-9 |

**BG401**
VB: Wind (+X richting)

## 3.15 GEGENEREERDE LASTEN — BG401: VB: Wind (+X richting)

| No. | Belastingomschrijving | | | | |
|---|---|---|---|---|---|
| 3 | Van Windbelastingen (Verticale Wanden) | | | | |




| | | | | | |
|---|---|---|---|---|---|
| Snelheidsdruk | Volgens de norm | | : | EN 1991-1-4 | |
| | Nationale Bijlage | | : | Nederland | |
| | Windgebied | | : | III | |
| | Terrein categorie | | : | Categorie II | |
| | Constructie hoogte | h | : | 8500 | mm |
| | Fundamentele windsnelheid | $v_{b,0}$ | : | 24.5 | m/s |
| Basisgeometrie | Knoop | I | : | 5 | |
| | | J | : | 11 | |
| | | K | : | 15 | |
| | | L | : | 9 | |
| Daktype en geometrie | Type | | : | ⦿ Plat-/lessenaarsdak | |
| | Knoop | A | : | 6 | |
| | | B | : | 12 | |
| | | C | : | 16 | |
| | | D | : | 10 | |
| BG genereren | ☒BG w | | : | BG401 | |
| Stel wind in op een zijde | ⦿ A - B | | | | |
| Maak Last Type | ⦿ Staafbelastingen | | | | |
| Lastverdelingstype | ⦿ Constant | | | | |
| Verwijder invloed van | Enkele Liggers | | : | 7,9,10,11,12,13,16,17, 18,19 | |
| | Staven parallel aan Staaf | | : | 22 | |
| Windbelasting wordt gegenereerd op staaf No. | | | : | 1-6 | |
| Wandafmetingen | h | | : | 8500 | mm |
| | b | | : | 4000 | mm |
| | d | | : | 7000 | mm |
| | e | | : | 4000 | mm |
| | A | | : | 89100006 | $mm^2$ |
| | $d_A$ | | : | 800 | mm |
| | $d_B$ | | : | 3200 | mm |
| | $d_C$ | | : | 3000 | mm |

| Gebied | Externe drukcoï¿½fficiï¿½nt $c_{pe,10}$ | Externe Druk $w_e$ [kN/m²] |
|---|---|---|
| A | -1.200 | -0.795 |
| B | -0.800 | -0.530 |
| C | -0.500 | -0.331 |
| D | 0.800 | 0.530 |
| E | -0.511 | -0.338 |

| | | | | | |
|---|---|---|---|---|---|
| Gegenereerde totaalbelastingen | $\Sigma P_{Vlakken}$ | | : | 14.04 | kN |
| | $\Sigma P$ | | : | 14.04 | kN |
| Totale moment bij de oorsprong | $\Sigma M_{Vlakken}$ | | : | 40.00 | kNm |
| | $\Sigma M$ | | : | 40.00 | kNm |
| Cellen geselecteerd voor genereren | Σ aantal cellen | | : | 42 | |
| | Σ cel vlak | | : | 607100044 | $mm^2$ |

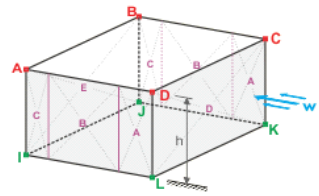
**BG402**
VB: Wind (-X richting)

## 3.15 GEGENEREERDE LASTEN — BG402: VB: Wind (-X richting)

| No. | Belastingomschrijving |
|---|---|
| 3 | Van Windbelastingen (Verticale Wanden) |

## 3.15 GEGENEREERDE LASTEN — BG402: VB: Wind (-X richting)

| No. | Belastingomschrijving |
|---|---|




| | | | | | |
|---|---|---|---|---|---|
| Snelheidsdruk | Volgens de norm | | : | EN 1991-1-4 | |
| | Nationale Bijlage | | : | Nederland | |
| | Windgebied | | : | III | |
| | Terrein categorie | | : | Categorie II | |
| | Constructie hoogte | h | : | 8500 | mm |
| | Fundamentele windsnelheid | $v_{b,0}$ | : | 24.5 | m/s |
| Basisgeometrie | Knoop | I | : | 5 | |
| | | J | : | 11 | |
| | | K | : | 15 | |
| | | L | : | 9 | |
| Daktype en geometrie | Type | | : | ⦿ Plat-/lessenaarsdak | |
| | Knoop | A | : | 6 | |
| | | B | : | 12 | |
| | | C | : | 16 | |
| | | D | : | 10 | |
| BG genereren | ☒BG w | | : | BG402 | |
| Stel wind in op een zijde | ⦿ C - D | | | | |
| Maak Last Type | ⦿ Staafbelastingen | | | | |
| Lastverdelingstype | ⦿ Constant | | | | |
| Verwijder invloed van | Enkele Liggers | | : | 7,9,10,11,12,13,16,17, 18,19 | |
| | Staven parallel aan Staaf | | : | 23 | |
| Windbelasting wordt gegenereerd op staaf No. | | | : | 1-6 | |
| Wandafmetingen | h | | : | 8500 | mm |
| | b | | : | 4000 | mm |
| | d | | : | 7000 | mm |
| | e | | : | 4000 | mm |
| | A | | : | 89100006 | $mm^2$ |
| | $d_A$ | | : | 800 | mm |
| | $d_B$ | | : | 3200 | mm |
| | $d_C$ | | : | 3000 | mm |

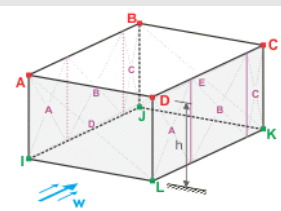
| Gebied | Externe drukcoï¿½fficiï¿½nt $c_{pe,10}$ | Externe Druk $w_e$ [kN/m²] |
|---|---|---|
| A | -1.200 | -0.795 |
| B | -0.800 | -0.530 |
| C | -0.500 | -0.331 |
| D | 0.800 | 0.530 |
| E | -0.511 | -0.338 |

| | | | | | |
|---|---|---|---|---|---|
| Gegenereerde totaalbelastingen | $\Sigma P_{Vlakken}$ | | : | 14.04 | kN |
| | $\Sigma P$ | | : | 14.04 | kN |
| Totale moment bij de oorsprong | $\Sigma M_{Vlakken}$ | | : | 40.00 | kNm |
| | $\Sigma M$ | | : | 40.00 | kNm |
| Cellen geselecteerd voor genereren | Σ aantal cellen | | : | 42 | |
| | Σ cel vlak | | : | 607100044 | $mm^2$ |

**BG403**
VB: Wind (+Y richting)

## 3.15 GEGENEREERDE LASTEN — BG403: VB: Wind (+Y richting)

| No. | Belastingomschrijving |
|---|---|
| 3 | Van Windbelastingen (Verticale Wanden) |




| | | | | | |
|---|---|---|---|---|---|
| Snelheidsdruk | Volgens de norm | | : | EN 1991-1-4 | |
| | Nationale Bijlage | | : | Nederland | |
| | Windgebied | | : | III | |
| | Terrein categorie | | : | Categorie II | |
| | Constructie hoogte | h | : | 8500 | mm |
| | Fundamentele windsnelheid | $v_{b,0}$ | : | 24.5 | m/s |

## 3.15 GEGENEREERDE LASTEN — BG403: VB: Wind (+Y richting)

| No. | Belastingomschrijving | | | | |
|---|---|---|---|---|---|
| | Basisgeometrie | Knoop | I | : | 5 |
| | | | J | : | 11 |
| | | | K | : | 15 |
| | | | L | : | 9 |
| | Daktype en geometrie | Type | | : | ⦿ Plat-/lessenaarsdak |
| | | Knoop | A | : | 6 |
| | | | B | : | 12 |
| | | | C | : | 16 |
| | | | D | : | 10 |
| | BG genereren | ☒BG w | | : | BG403 |
| | Stel wind in op een zijde | ⦿ D - A | | | |
| | Maak Last Type | ⦿ Staafbelastingen | | | |
| | Lastverdelingstype | ⦿ Constant | | | |
| | Verwijder invloed van | Enkele Liggers | | : | 7,9,10,11,12,13,16,17, 18,19 |
| | | Staven parallel aan Staaf | | : | 23 |
| | Windbelasting wordt gegenereerd op staaf No. | | | : | 1-6 |
| | Wandafmetingen | h | | : | 8500 mm |
| | | b | | : | 7000 mm |
| | | d | | : | 4000 mm |
| | | e | | : | 7000 mm |
| | | A | | : | 89100006 $mm^2$ |
| | | $d_A$ | | : | 1400 mm |
| | | $d_B$ | | : | 2600 mm |
| | | $d_C$ | | : | 0 mm |

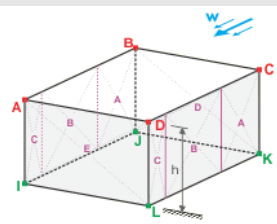
| Gebied | Externe drukcoï¿½fficiï¿½nt $c_{pe,10}$ | Externe Druk $w_e$ [kN/m²] |
|---|---|---|
| A | -1.200 | -0.795 |
| B | -0.800 | -0.530 |
| C | -0.500 | -0.331 |
| D | 0.800 | 0.530 |
| E | -0.556 | -0.369 |

| | | | | | |
|---|---|---|---|---|---|
| | Gegenereerde totaalbelastingen | $\Sigma P_{Vlakken}$ | | : | 24.40 kN |
| | | $\Sigma P$ | | : | 24.40 kN |
| | Totale moment bij de oorsprong | $\Sigma M_{Vlakken}$ | | : | 99.09 kNm |
| | | $\Sigma M$ | | : | 99.09 kNm |
| | Cellen geselecteerd voor genereren | Σ aantal cellen | | : | 20 |
| | | Σ cel vlak | | : | 211600018 $mm^2$ |

**BG404**
VB: Wind (-Y richting)

## 3.15 GEGENEREERDE LASTEN — BG404: VB: Wind (-Y richting)

| No. | Belastingomschrijving | | | | |
|---|---|---|---|---|---|
| 3 | Van Windbelastingen (Verticale Wanden) | | | | |




| | | | | | |
|---|---|---|---|---|---|
| | Snelheidsdruk | Volgens de norm | | : | EN 1991-1-4 |
| | | Nationale Bijlage | | : | Nederland |
| | | Windgebied | | : | III |
| | | Terrein categorie | | : | Categorie II |
| | | Constructie hoogte | h | : | 8500 mm |
| | | Fundamentele windsnelheid | $v_{b,0}$ | : | 24.5 m/s |
| | Basisgeometrie | Knoop | I | : | 5 |
| | | | J | : | 11 |
| | | | K | : | 15 |
| | | | L | : | 9 |
| | Daktype en geometrie | Type | | : | ⦿ Plat-/lessenaarsdak |
| | | Knoop | A | : | 6 |
| | | | B | : | 12 |
| | | | C | : | 16 |
| | | | D | : | 10 |
| | BG genereren | ☒BG w | | : | BG404 |
| | Stel wind in op een zijde | ⦿ B - C | | | |
| | Maak Last Type | ⦿ Staafbelastingen | | | |

## 3.15 GEGENEREERDE LASTEN

BG404: VB: Wind (-Y richting)

| No. | Belastingomschrijving | | | | |
|---|---|---|---|---|---|
| | Lastverdelingstype | ⦿ Constant | | | |
| | Verwijder invloed van | Enkele Liggers | : | 7,9,10,11,12,13,16,17, 18,19 | |
| | | Staven parallel aan Staaf | : | 23 | |
| | Windbelasting wordt gegenereerd op staaf No. | | : | 1-6 | |
| | Wandafmetingen | h | : | 8500 | mm |
| | | b | : | 7000 | mm |
| | | d | : | 4000 | mm |
| | | e | : | 7000 | mm |
| | | A | : | 89100006 | $mm^2$ |
| | | $d_A$ | : | 1400 | mm |
| | | $d_B$ | : | 2600 | mm |
| | | $d_C$ | : | 0 | mm |

| Gebied | Externe drukcoï¿½fficiï¿½nt $c_{pe,10}$ | Externe Druk $w_e$ [kN/m²] |
|---|---|---|
| A | -1.200 | -0.795 |
| B | -0.800 | -0.530 |
| C | -0.500 | -0.331 |
| D | 0.800 | 0.530 |
| E | -0.556 | -0.369 |

| | | | | |
|---|---|---|---|---|
| Gegenereerde totaalbelastingen | $\Sigma P_{Vlakken}$ | : | 24.40 | kN |
| | $\Sigma P$ | : | 24.40 | kN |
| Totale moment bij de oorsprong | $\Sigma M_{Vlakken}$ | : | 99.09 | kNm |
| | $\Sigma M$ | : | 99.09 | kNm |
| Cellen geselecteerd voor genereren | $\Sigma$ aantal cellen | : | 20 | |
| | $\Sigma$ cel vlak | : | 211600018 | $mm^2$ |

## 4.0 RESULTATEN - OPSOMMING

| | Omschrijving | Waarde | Eenh | Opm. |
|---|---|---|---|---|
| Belastingsgeval BG10 - PB: Eigen Gewicht | | | | |
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | -228.33 | kN | |
| | Som van de steunpuntreacties in Z | -228.33 | kN | Afwijking 0.00% |
| | Resultante van reacties om x-as | 0.00 | kNm | Bij zwaartepunt van de Constructie (X:3495.36, Y:2000.00, Z:-33.43 mm) |
| | Resultante van reacties om y-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 0.0 | mm | EE-Knoop nr. 37 (X: 0, Y: 0, Z: 4050 mm) |
| | Max. verplaatsing in y-as | 0.2 | mm | Staaf No. 22, x: 0 mm |
| | Max. verplaatsing in z-as | -1.9 | mm | EE-Knoop nr. 1072 (X: 1750, Y: 0, Z: 4050 mm) |
| | Max. verplaatsing (vector) | 1.9 | mm | EE-Knoop nr. 1072 (X: 1750, Y: 0, Z: 4050 mm) |
| | Max. rotatie om x-as | -0.60 | mrad | EE-Knoop nr. 98 (X: -200, Y: 4000, Z: 0 mm) |
| | Max. rotatie om y-as | -0.41 | mrad | EE-Knoop nr. 40 (X: 7000, Y: 0, Z: 4050 mm) |
| | Max. rotatie om z-as | -0.00 | mrad | EE-Knoop nr. 137 (X: 800, Y: -200, Z: 0 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 3 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 1.002E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 5.378E+04 | | |
| | Stijfheidsmatrix determinant | 4.987E+5897 4 | | |
| | Oneindige Norm | 2.005E+14 | | |
| Belastingsgeval BG20 - PB: Dakbedekking | | | | |
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | -23.80 | kN | |
| | Som van de steunpuntreacties in Z | -23.80 | kN | Afwijking 0.00% |
| | Resultante van reacties om x-as | 0.00 | kNm | Bij zwaartepunt van de Constructie (X:3495.36, Y:2000.00, Z:-33.43 mm) |
| | Resultante van reacties om y-as | 0.11 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | -0.0 | mm | EE-Knoop nr. 95 (X: 200, Y: 4200, Z: 0 mm) |
| | Max. verplaatsing in y-as | -0.2 | mm | EE-Knoop nr. 913 (X: 3500, Y: 0, Z: 2314 mm) |
| | Max. verplaatsing in z-as | -1.1 | mm | EE-Knoop nr. 1035 (X: 3500, Y: 2000, Z: 4050 mm) |
| | Max. verplaatsing (vector) | 1.1 | mm | EE-Knoop nr. 1035 (X: 3500, Y: 2000, Z: 4050 mm) |
| | Max. rotatie om x-as | -0.61 | mrad | EE-Knoop nr. 1026 (X: 3500, Y: 200, Z: 4050 mm) |
| | Max. rotatie om y-as | -0.01 | mrad | EE-Knoop nr. 49 (X: 7200, Y: 2000, Z: 0 mm) |
| | Max. rotatie om z-as | -0.00 | mrad | EE-Knoop nr. 39 (X: 3500, Y: 0, Z: 4050 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 2 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 1.002E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 5.378E+04 | | |
| | Stijfheidsmatrix determinant | 4.987E+5897 4 | | |
| | Oneindige Norm | 2.005E+14 | | |
| Belastingsgeval BG30 - PB: KSZ - Metselwerk | | | | |
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | -157.50 | kN | |
| | Som van de steunpuntreacties in Z | -157.50 | kN | Afwijking 0.00% |
| | Resultante van reacties om x-as | 0.00 | kNm | Bij zwaartepunt van de Constructie (X:3495.36, Y:2000.00, Z:-33.43 mm) |
| | Resultante van reacties om y-as | 0.73 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 0.0 | mm | EE-Knoop nr. 10 (X: 7000, Y: 0, Z: 4050 mm) |
| | Max. verplaatsing in y-as | 0.4 | mm | Staaf No. 22, x: 389 mm |
| | Max. verplaatsing in z-as | -1.5 | mm | EE-Knoop nr. 78 (X: 3600, Y: 4200, Z: 0 mm) |
| | Max. verplaatsing (vector) | 1.5 | mm | EE-Knoop nr. 78 (X: 3600, Y: 4200, Z: 0 mm) |
| | Max. rotatie om x-as | -0.89 | mrad | EE-Knoop nr. 59 (X: 7200, Y: 4000, Z: 0 mm) |
| | Max. rotatie om y-as | -0.12 | mrad | EE-Knoop nr. 49 (X: 7200, Y: 2000, Z: 0 mm) |
| | Max. rotatie om z-as | -0.00 | mrad | EE-Knoop nr. 99 (X: -200, Y: 3800, Z: 0 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 3 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 1.002E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 5.378E+04 | | |
| | Stijfheidsmatrix determinant | 4.987E+5897 4 | | |
| | Oneindige Norm | 2.005E+14 | | |
| Belastingsgeval BG40 - PB: Sandwichpaneel | | | | |
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | 0.00 | kN | |

## 4.0 RESULTATEN - OPSOMMING

| | Omschrijving | Waarde | Eenh | Opm. |
|---|---|---|---|---|
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | -10.23 | kN | |
| | Som van de steunpuntreacties in Z | -10.23 | kN | Afwijking 0.00% |
| | Resultante van reacties om x-as | 0.00 | kNm | Bij zwaartepunt van de Constructie (X:3495.36, Y:2000.00, Z:-33.43 mm) |
| | Resultante van reacties om y-as | 0.05 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | -0.0 | mm | EE-Knoop nr. 10 (X: 7000, Y: 0, Z: 4050 mm) |
| | Max. verplaatsing in y-as | 0.0 | mm | Staaf No. 22, x: 0 mm |
| | Max. verplaatsing in z-as | -0.1 | mm | EE-Knoop nr. 1 (X: -200, Y: -200, Z: 0 mm) |
| | Max. verplaatsing (vector) | 0.1 | mm | EE-Knoop nr. 1 (X: -200, Y: -200, Z: 0 mm) |
| | Max. rotatie om x-as | -0.06 | mrad | EE-Knoop nr. 58 (X: 7200, Y: 3800, Z: 0 mm) |
| | Max. rotatie om y-as | -0.00 | mrad | EE-Knoop nr. 95 (X: 200, Y: 4200, Z: 0 mm) |
| | Max. rotatie om z-as | -0.00 | mrad | EE-Knoop nr. 58 (X: 7200, Y: 3800, Z: 0 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 3 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 1.002E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 5.378E+04 | | |
| | Stijfheidsmatrix determinant | 4.987E+5897 4 | | |
| | Oneindige Norm | 2.005E+14 | | |
| Belastingsgeval BG100 - VB: Opgelegde belasting op vloeren 1 | | | | |
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | -97.68 | kN | |
| | Som van de steunpuntreacties in Z | -97.68 | kN | Afwijking 0.00% |
| | Resultante van reacties om x-as | 0.00 | kNm | Bij zwaartepunt van de Constructie (X:3495.36, Y:2000.00, Z:-33.43 mm) |
| | Resultante van reacties om y-as | 0.45 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 0.0 | mm | |
| | Max. verplaatsing in y-as | 0.0 | mm | |
| | Max. verplaatsing in z-as | -0.4 | mm | EE-Knoop nr. 1 (X: -200, Y: -200, Z: 0 mm) |
| | Max. verplaatsing (vector) | 0.4 | mm | EE-Knoop nr. 1 (X: -200, Y: -200, Z: 0 mm) |
| | Max. rotatie om x-as | 0.00 | mrad | |
| | Max. rotatie om y-as | 0.00 | mrad | |
| | Max. rotatie om z-as | 0.00 | mrad | |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 3 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 1.002E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 5.378E+04 | | |
| | Stijfheidsmatrix determinant | 2.910E+5897 6 | | |
| | Oneindige Norm | 2.005E+14 | | |
| Belastingsgeval BG120 - VB: Dakbelasting | | | | |
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | -28.00 | kN | |
| | Som van de steunpuntreacties in Z | -28.00 | kN | Afwijking 0.00% |
| | Resultante van reacties om x-as | 0.00 | kNm | Bij zwaartepunt van de Constructie (X:3495.36, Y:2000.00, Z:-33.43 mm) |
| | Resultante van reacties om y-as | 0.13 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | -0.0 | mm | EE-Knoop nr. 95 (X: 200, Y: 4200, Z: 0 mm) |
| | Max. verplaatsing in y-as | -0.2 | mm | EE-Knoop nr. 913 (X: 3500, Y: 0, Z: 2314 mm) |
| | Max. verplaatsing in z-as | -1.2 | mm | EE-Knoop nr. 1035 (X: 3500, Y: 2000, Z: 4050 mm) |
| | Max. verplaatsing (vector) | 1.2 | mm | EE-Knoop nr. 1035 (X: 3500, Y: 2000, Z: 4050 mm) |
| | Max. rotatie om x-as | -0.71 | mrad | EE-Knoop nr. 1026 (X: 3500, Y: 200, Z: 4050 mm) |
| | Max. rotatie om y-as | -0.02 | mrad | EE-Knoop nr. 49 (X: 7200, Y: 2000, Z: 0 mm) |
| | Max. rotatie om z-as | -0.00 | mrad | EE-Knoop nr. 39 (X: 3500, Y: 0, Z: 4050 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 3 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 1.002E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 5.378E+04 | | |
| | Stijfheidsmatrix determinant | 4.987E+5897 4 | | |
| | Oneindige Norm | 2.005E+14 | | |
| Belastingsgeval BG150 - VB: Heftruck | | | | |
| | Som van belastingen in X | 24.00 | kN | |
| | Som van de steunpuntreacties in X | 24.00 | kN | Afwijking 0.00% |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | -112.00 | kN | |
| | Som van de steunpuntreacties in Z | -112.00 | kN | Afwijking 0.00% |
| | Resultante van reacties om x-as | 0.00 | kNm | Bij zwaartepunt van de Constructie (X:3495.36, Y:2000.00, Z:-33.43 mm) |

## 4.0 RESULTATEN - OPSOMMING

| | Omschrijving | Waarde | Eenh | Opm. |
|---|---|---|---|---|
| | Resultante van reacties om y-as | 3.19 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 0.9 | mm | EE-Knoop nr. 10 (X: 7000, Y: 0, Z: 4050 mm) |
| | Max. verplaatsing in y-as | -0.1 | mm | Staaf No. 22, x: 3500 mm |
| | Max. verplaatsing in z-as | -0.8 | mm | EE-Knoop nr. 539 (X: 3600, Y: 2000, Z: 0 mm) |
| | Max. verplaatsing (vector) | 1.1 | mm | EE-Knoop nr. 538 (X: 3400, Y: 2000, Z: 0 mm) |
| | Max. rotatie om x-as | -0.33 | mrad | EE-Knoop nr. 283 (X: 2759, Y: 601, Z: 0 mm) |
| | Max. rotatie om y-as | 0.22 | mrad | EE-Knoop nr. 529 (X: 1600, Y: 2000, Z: 0 mm) |
| | Max. rotatie om z-as | -0.01 | mrad | EE-Knoop nr. 127 (X: 1556, Y: 0, Z: 0 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 3 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 1.002E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 5.378E+04 | | |
| | Stijfheidsmatrix determinant | 4.895E+58978 | | |
| | Oneindige Norm | 2.005E+14 | | |

| Belastingsgeval BG300 - VB: Sneeuw | | | | |
|---|---|---|---|---|
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | -39.20 | kN | |
| | Som van de steunpuntreacties in Z | -39.20 | kN | Afwijking 0.00% |
| | Resultante van reacties om x-as | 0.00 | kNm | Bij zwaartepunt van de Constructie (X:3495.36, Y:2000.00, Z:-33.43 mm) |
| | Resultante van reacties om y-as | 0.18 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | -0.0 | mm | EE-Knoop nr. 95 (X: 200, Y: 4200, Z: 0 mm) |
| | Max. verplaatsing in y-as | -0.3 | mm | EE-Knoop nr. 913 (X: 3500, Y: 0, Z: 2314 mm) |
| | Max. verplaatsing in z-as | -1.7 | mm | EE-Knoop nr. 1035 (X: 3500, Y: 2000, Z: 4050 mm) |
| | Max. verplaatsing (vector) | 1.7 | mm | EE-Knoop nr. 1035 (X: 3500, Y: 2000, Z: 4050 mm) |
| | Max. rotatie om x-as | -1.00 | mrad | EE-Knoop nr. 1026 (X: 3500, Y: 200, Z: 4050 mm) |
| | Max. rotatie om y-as | -0.02 | mrad | EE-Knoop nr. 49 (X: 7200, Y: 2000, Z: 0 mm) |
| | Max. rotatie om z-as | -0.00 | mrad | EE-Knoop nr. 39 (X: 3500, Y: 0, Z: 4050 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 3 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 1.002E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 5.378E+04 | | |
| | Stijfheidsmatrix determinant | 4.987E+58974 | | |
| | Oneindige Norm | 2.005E+14 | | |

| Belastingsgeval BG401 - VB: Wind (+X richting) | | | | |
|---|---|---|---|---|
| | Som van belastingen in X | 14.04 | kN | |
| | Som van de steunpuntreacties in X | 14.04 | kN | Afwijking 0.00% |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | 0.00 | kNm | Bij zwaartepunt van de Constructie (X:3495.36, Y:2000.00, Z:-33.43 mm) |
| | Resultante van reacties om y-as | 30.02 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 6.8 | mm | Staaf No. 1, x: 2025 mm |
| | Max. verplaatsing in y-as | -0.5 | mm | EE-Knoop nr. 911 (X: 3500, Y: 0, Z: 1929 mm) |
| | Max. verplaatsing in z-as | -0.2 | mm | EE-Knoop nr. 1035 (X: 3500, Y: 2000, Z: 4050 mm) |
| | Max. verplaatsing (vector) | 6.8 | mm | Staaf No. 4, x: 2025 mm |
| | Max. rotatie om x-as | -0.44 | mrad | EE-Knoop nr. 29 (X: 3500, Y: 4000, Z: 0 mm) |
| | Max. rotatie om y-as | 4.95 | mrad | EE-Knoop nr. 25 (X: 0, Y: 0, Z: 0 mm) |
| | Max. rotatie om z-as | -0.01 | mrad | EE-Knoop nr. 96 (X: -0, Y: 4200, Z: 0 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 3 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 1.002E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 5.378E+04 | | |
| | Stijfheidsmatrix determinant | 3.112E+58977 | | |
| | Oneindige Norm | 2.005E+14 | | |

| Belastingsgeval BG402 - VB: Wind (-X richting) | | | | |
|---|---|---|---|---|
| | Som van belastingen in X | -14.04 | kN | |
| | Som van de steunpuntreacties in X | -14.04 | kN | Afwijking 0.00% |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | 0.00 | kNm | Bij zwaartepunt van de Constructie (X:3495.36, Y:2000.00, Z:-33.43 mm) |
| | Resultante van reacties om y-as | -30.02 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | -6.9 | mm | Staaf No. 3, x: 2025 mm |
| | Max. verplaatsing in y-as | -0.5 | mm | EE-Knoop nr. 911 (X: 3500, Y: 0, Z: 1929 mm) |

## 4.0 RESULTATEN - OPSOMMING

| | Omschrijving | Waarde | Eenh | Opm. |
|---|---|---|---|---|
| | Max. verplaatsing in z-as | -0.2 | mm | EE-Knoop nr. 1016 (X: 0, Y: 2000, Z: 4050 mm) |
| | Max. verplaatsing (vector) | 6.9 | mm | Staaf No. 3, x: 2025 mm |
| | Max. rotatie om x-as | 0.44 | mrad | EE-Knoop nr. 26 (X: 3500, Y: 0, Z: 0 mm) |
| | Max. rotatie om y-as | -4.99 | mrad | EE-Knoop nr. 30 (X: 7000, Y: 4000, Z: 0 mm) |
| | Max. rotatie om z-as | -0.00 | mrad | EE-Knoop nr. 998 (X: 3400, Y: -200, Z: 0 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 3 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 1.002E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 5.378E+04 | | |
| | Stijfheidsmatrix determinant | 3.119E+5897 7 | | |
| | Oneindige Norm | 2.005E+14 | | |

| Belastingsgeval BG403 - VB: Wind (+Y richting) | | | | |
|---|---|---|---|---|
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | 24.40 | kN | |
| | Som van de steunpuntreacties in Y | 24.40 | kN | Afwijking 0.00% |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | -52.90 | kNm | Bij zwaartepunt van de Constructie (X:3495.36, Y:2000.00, Z:-33.43 mm) |
| | Resultante van reacties om y-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.11 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | -7.3 | mm | Staaf No. 1, x: 2025 mm |
| | Max. verplaatsing in y-as | 17.6 | mm | EE-Knoop nr. 14 (X: 3500, Y: 4000, Z: 4050 mm) |
| | Max. verplaatsing in z-as | -0.4 | mm | EE-Knoop nr. 3 (X: 7200, Y: 4200, Z: 0 mm) |
| | Max. verplaatsing (vector) | 17.6 | mm | EE-Knoop nr. 14 (X: 3500, Y: 4000, Z: 4050 mm) |
| | Max. rotatie om x-as | -5.38 | mrad | EE-Knoop nr. 26 (X: 3500, Y: 0, Z: 0 mm) |
| | Max. rotatie om y-as | -5.87 | mrad | Staaf No. 3, x: 4050 mm |
| | Max. rotatie om z-as | 0.03 | mrad | EE-Knoop nr. 37 (X: 0, Y: 0, Z: 4050 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 3 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 1.002E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 5.378E+04 | | |
| | Stijfheidsmatrix determinant | 8.871E+5897 7 | | |
| | Oneindige Norm | 2.005E+14 | | |

| Belastingsgeval BG404 - VB: Wind (-Y richting) | | | | |
|---|---|---|---|---|
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | -24.40 | kN | |
| | Som van de steunpuntreacties in Y | -24.40 | kN | Afwijking 0.00% |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | 52.90 | kNm | Bij zwaartepunt van de Constructie (X:3495.36, Y:2000.00, Z:-33.43 mm) |
| | Resultante van reacties om y-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | -0.11 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | -7.3 | mm | Staaf No. 4, x: 2025 mm |
| | Max. verplaatsing in y-as | -17.6 | mm | EE-Knoop nr. 8 (X: 3500, Y: 0, Z: 4050 mm) |
| | Max. verplaatsing in z-as | -0.4 | mm | EE-Knoop nr. 2 (X: 7200, Y: -200, Z: 0 mm) |
| | Max. verplaatsing (vector) | 17.6 | mm | EE-Knoop nr. 8 (X: 3500, Y: 0, Z: 4050 mm) |
| | Max. rotatie om x-as | 5.38 | mrad | EE-Knoop nr. 29 (X: 3500, Y: 4000, Z: 0 mm) |
| | Max. rotatie om y-as | -5.87 | mrad | Staaf No. 6, x: 4050 mm |
| | Max. rotatie om z-as | -0.03 | mrad | EE-Knoop nr. 41 (X: 0, Y: 4000, Z: 4050 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 3 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 1.002E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 5.378E+04 | | |
| | Stijfheidsmatrix determinant | 8.871E+5897 7 | | |
| | Oneindige Norm | 2.005E+14 | | |

| Belastingsgeval BG800 - DBG1 - Eigenvorm 1, richting - Y | | | | |
|---|---|---|---|---|
| | Berekening Status : De som van de belastingen en de som van de reactiekrachten in richting X zijn niet in evenwicht (afwijking -3.23%). | | | |
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | -21.88 | kN | |
| | Som van de steunpuntreacties in Y | -21.88 | kN | Afwijking 0.00% |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | 62.10 | kNm | Bij zwaartepunt van de Constructie (X:3495.36, Y:2000.00, Z:-33.43 mm) |
| | Resultante van reacties om y-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.05 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 0.0 | mm | EE-Knoop nr. 12 (X: 0, Y: 4000, Z: 4050 mm) |
| | Max. verplaatsing in y-as | -19.5 | mm | EE-Knoop nr. 1123 (X: 5250, Y: 4000, Z: 4050 mm) |
| | Max. verplaatsing in z-as | 0.4 | mm | EE-Knoop nr. 3 (X: 7200, Y: 4200, Z: 0 mm) |
| | Max. verplaatsing (vector) | 19.5 | mm | EE-Knoop nr. 1123 (X: 5250, Y: 4000, Z: 4050 mm) |

## 4.0 RESULTATEN - OPSOMMING

| | Omschrijving | Waarde | Eenh | Opm. |
|---|---|---|---|---|
| | Max. rotatie om x-as | 5.41 | mrad | EE-Knoop nr. 26 (X: 3500, Y: 0, Z: 0 mm) |
| | Max. rotatie om y-as | 0.03 | mrad | EE-Knoop nr. 12 (X: 0, Y: 4000, Z: 4050 mm) |
| | Max. rotatie om z-as | -0.41 | mrad | EE-Knoop nr. 41 (X: 0, Y: 4000, Z: 4050 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 3 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 1.002E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 5.378E+04 | | |
| | Stijfheidsmatrix determinant | 7.753E+58980 | | |
| | Oneindige Norm | 2.005E+14 | | |
| Belastingsgeval BG801 - DBG1 - Eigenvorm 2, richting - X | | | | |
| | Som van belastingen in X | -40.78 | kN | |
| | Som van de steunpuntreacties in X | -40.78 | kN | Afwijking 0.00% |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | 0.00 | kNm | Bij zwaartepunt van de Constructie (X:3495.36, Y:2000.00, Z:-33.43 mm) |
| | Resultante van reacties om y-as | -69.87 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | -33.9 | mm | EE-Knoop nr. 1035 (X: 3500, Y: 2000, Z: 4050 mm) |
| | Max. verplaatsing in y-as | 0.0 | mm | Staaf No. 22, x: 0 mm |
| | Max. verplaatsing in z-as | -0.4 | mm | EE-Knoop nr. 1013 (X: 0, Y: 1400, Z: 4050 mm) |
| | Max. verplaatsing (vector) | 33.9 | mm | EE-Knoop nr. 1035 (X: 3500, Y: 2000, Z: 4050 mm) |
| | Max. rotatie om x-as | -0.11 | mrad | EE-Knoop nr. 101 (X: -200, Y: 3400, Z: 0 mm) |
| | Max. rotatie om y-as | -87.17 | mrad | EE-Knoop nr. 1035 (X: 3500, Y: 2000, Z: 4050 mm) |
| | Max. rotatie om z-as | -16.03 | mrad | EE-Knoop nr. 34 (X: 3500, Y: 4000, Z: 4050 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 6 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 1.002E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 5.378E+04 | | |
| | Stijfheidsmatrix determinant | 3.119E+58977 | | |
| | Oneindige Norm | 2.005E+14 | | |
| Belastingsgeval BG802 - DBG1 - Eigenvorm 4, richting - X | | | | |
| | Som van belastingen in X | -111.86 | kN | |
| | Som van de steunpuntreacties in X | -111.86 | kN | Afwijking 0.00% |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | 0.00 | kNm | Bij zwaartepunt van de Constructie (X:3495.36, Y:2000.00, Z:-33.43 mm) |
| | Resultante van reacties om y-as | -55.95 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | -21.0 | mm | EE-Knoop nr. 1054 (X: 7000, Y: 2000, Z: 4050 mm) |
| | Max. verplaatsing in y-as | 0.0 | mm | Staaf No. 22, x: 0 mm |
| | Max. verplaatsing in z-as | -0.3 | mm | EE-Knoop nr. 6 (X: 0, Y: 0, Z: 4050 mm) |
| | Max. verplaatsing (vector) | 21.0 | mm | EE-Knoop nr. 1054 (X: 7000, Y: 2000, Z: 4050 mm) |
| | Max. rotatie om x-as | -0.08 | mrad | EE-Knoop nr. 101 (X: -200, Y: 3400, Z: 0 mm) |
| | Max. rotatie om y-as | 57.55 | mrad | EE-Knoop nr. 1035 (X: 3500, Y: 2000, Z: 4050 mm) |
| | Max. rotatie om z-as | -10.26 | mrad | EE-Knoop nr. 33 (X: 3500, Y: 0, Z: 4050 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 4 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 1.002E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 5.378E+04 | | |
| | Stijfheidsmatrix determinant | 3.119E+58977 | | |
| | Oneindige Norm | 2.005E+14 | | |
| Belastingsgeval BG803 - DBG1 - Eigenvorm 5, richting - Y | | | | |
| | Som van belastingen in X | 0.00 | kN | |
| | Som van de steunpuntreacties in X | 0.00 | kN | |
| | Som van belastingen in Y | -159.36 | kN | |
| | Som van de steunpuntreacties in Y | -159.36 | kN | Afwijking 0.00% |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | -7.14 | kNm | Bij zwaartepunt van de Constructie (X:3495.36, Y:2000.00, Z:-33.43 mm) |
| | Resultante van reacties om y-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | -1.33 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 0.0 | mm | EE-Knoop nr. 982 (X: 3500, Y: 4000, Z: 3471 mm) |
| | Max. verplaatsing in y-as | -4.9 | mm | Staaf No. 25, x: 3500 mm |
| | Max. verplaatsing in z-as | -0.1 | mm | EE-Knoop nr. 1030 (X: 3500, Y: 1000, Z: 4050 mm) |
| | Max. verplaatsing (vector) | 4.9 | mm | Staaf No. 25, x: 3500 mm |
| | Max. rotatie om x-as | -2.13 | mrad | EE-Knoop nr. 29 (X: 3500, Y: 4000, Z: 0 mm) |
| | Max. rotatie om y-as | 0.01 | mrad | EE-Knoop nr. 6 (X: 0, Y: 0, Z: 4050 mm) |
| | Max. rotatie om z-as | -0.21 | mrad | EE-Knoop nr. 40 (X: 7000, Y: 0, Z: 4050 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |

## 4.0 RESULTATEN - OPSOMMING

| | Omschrijving | Waarde | Eenh | Opm. |
|---|---|---|---|---|
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 3 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 1.002E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 5.378E+04 | | |
| | Stijfheidsmatrix determinant | 7.753E+58980 | | |
| | Oneindige Norm | 2.005E+14 | | |

| Belastingsgeval BG804 - DBG1 - Eigenvorm 7, richting - X | | | | |
|---|---|---|---|---|
| | Som van belastingen in X | -38.27 | kN | |
| | Som van de steunpuntreacties in X | -38.27 | kN | Afwijking 0.00% |
| | Som van belastingen in Y | 0.00 | kN | |
| | Som van de steunpuntreacties in Y | 0.00 | kN | |
| | Som van belastingen in Z | 0.00 | kN | |
| | Som van de steunpuntreacties in Z | 0.00 | kN | |
| | Resultante van reacties om x-as | 0.00 | kNm | Bij zwaartepunt van de Constructie (X:3495.36, Y:2000.00, Z:-33.43 mm) |
| | Resultante van reacties om y-as | 34.99 | kNm | Bij zwaartepunt van de Constructie |
| | Resultante van reacties om z-as | 0.00 | kNm | Bij zwaartepunt van de Constructie |
| | Max. verplaatsing in x-as | 14.1 | mm | EE-Knoop nr. 1016 (X: 0, Y: 2000, Z: 4050 mm) |
| | Max. verplaatsing in y-as | -0.0 | mm | Staaf No. 22, x: 0 mm |
| | Max. verplaatsing in z-as | 0.2 | mm | EE-Knoop nr. 1 (X: -200, Y: -200, Z: 0 mm) |
| | Max. verplaatsing (vector) | 14.1 | mm | EE-Knoop nr. 1016 (X: 0, Y: 2000, Z: 4050 mm) |
| | Max. rotatie om x-as | -0.06 | mrad | EE-Knoop nr. 115 (X: -200, Y: 600, Z: 0 mm) |
| | Max. rotatie om y-as | 40.59 | mrad | EE-Knoop nr. 1016 (X: 0, Y: 2000, Z: 4050 mm) |
| | Max. rotatie om z-as | -7.34 | mrad | EE-Knoop nr. 31 (X: 0, Y: 0, Z: 4050 mm) |
| | Maximum member strain | 0.00000 | - | Staaf No. 0, x: 0 mm |
| | Maximum surface strain | 0.00000 | - | EE knoop No. 0 (X: 0, Y: 0, Z: 0 mm) |
| | Berekeningsmethode | Lineair | | Geometrisch lineaire berekening |
| | Aantal belastingsincrementen | 1 | | |
| | Aantal iteraties | 4 | | |
| | Max. waarde van element van stijfheidsmatrix op diagonaal | 1.002E+14 | | |
| | Min. waarde van element van stijfheidsmatrix op diagonaal | 5.378E+04 | | |
| | Stijfheidsmatrix determinant | 2.520E+58979 | | |
| | Oneindige Norm | 2.005E+14 | | |

| Samenvatting | | | | |
|---|---|---|---|---|
| | Berekening Status: Probleem In BG800 | | | |
| | Max. verplaatsing in x-as | -33.9 | mm | BG801, EE-Knoop nr. 1035 (X: 3500, Y: 2000, Z: 4050 mm) |
| | Max. verplaatsing in y-as | -19.5 | mm | BG800, EE-Knoop nr. 1123 (X: 5250, Y: 4000, Z: 4050 mm) |
| | Max. verplaatsing in z-as | -1.9 | mm | BG10, EE-Knoop nr. 1072 (X: 1750, Y: 0, Z: 4050 mm) |
| | Max. verplaatsing (vector) | 33.9 | mm | BG801, EE-Knoop nr. 1035 (X: 3500, Y: 2000, Z: 4050 mm) |
| | Max. rotatie om x-as | 5.41 | mrad | BG800, EE-Knoop nr. 26 (X: 3500, Y: 0, Z: 0 mm) |
| | Max. rotatie om y-as | -87.17 | mrad | BG801, EE-Knoop nr. 1035 (X: 3500, Y: 2000, Z: 4050 mm) |
| | Max. rotatie om z-as | -16.03 | mrad | BG801, EE-Knoop nr. 34 (X: 3500, Y: 4000, Z: 4050 mm) |
| | Andere instellingen: | | | |
| | Aantal 1D Eindige Elementen | 358 | | |
| | Aantal 2D Eindige Elementen | 834 | | |
| | Aantal 3D Eindige Elementen | 0 | | |
| | Aantal EE-netknopen | 1151 | | |
| | Aantal vergelijkingen | 6906 | | |
| | Max. aantal iteraties | 100 | | |
| | Aantal doorsnedes voor staafresultaten | 10 | | |
| | Verdeling van kabels/fundatie/verlopende staven | 10 | | |
| | Aantal staafverdelingen voor het zoeken naar max. waardes | 10 | | |
| | Onderverdelingen van EE-net voor grafische weergave resultaten | 0 | | |
| | Percentage van iteraties volgens de Picard-methode in combinatie met de Newton-Raphson methode | 5 | % | |
| | Zet Bezweken Staven AAN | ☒ | | |
| | Opties: | | | |
| | Afschuifstijfheid activeren voor Staven (Ay, Az) | ☐ | | |
| | Activeren van staafverdelingen voor grote vervorming of post-kritische berekening | ☒ | | |
| | Activeer ingevoerde stijfheidsmodificaties | ☒ | | |
| | Negeer rotatievrijheidsgraden | ☐ | | |
| | Controle van de kritische staafkrachten | ☐ | | |
| | Niet-symmetrische direct Solver als geï¿½ist door niet-lineair model | ☒ | | |
| | Oplossingsmethode voor de vergelijkingen | Direct | | |
| | Plaat-buigtheorie | Mindlin | | |
| | Solverversie | 64-bit | | |
| | Precisie en Tolerantie: | | | |
| | Wijzig standaardinstelling | ☐ | | |
| | Niet-lineaire effecten - Activeren: | | | |
| | Bezwijkende staven t.g.v. staaftype | ☒ | | |
| | Re-activeren van bezwijkende staven: | | | |
| | Controleer vervorming van bezwijkende staven en re-activeer indien van toepassing. | ☒ | | |
| | Max. aantal van re-activeringen | 5 | | |
| | Aanvullende instellingen: | | | |

## ■ 4.0 RESULTATEN - OPSOMMING

| | | | | |
|---|---|---|---|---|
| | Bezwijkende staven weer gebruiken met gereduceerde stijfheid<br>Reductiefactor voor Stijfheid | 100 | | |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ | $V_z$ | Momenten [kNm] $M_T$ | $M_y$ | $M_z$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 1 | RC1 | 5 | 0 | Max N | 0.67 | -4.24 | 6.14 | 0.00 | 0.00 | 0.00 | BC 43 |
| | | | Links | Min N | -17.43 | 0.00 | -0.86 | 0.00 | -0.00 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -9.30 | 3.48 | -3.68 | 0.00 | -0.00 | -0.00 | BC 23 |
| | | | | Min $V_y$ | 0.67 | -4.24 | 6.14 | 0.00 | 0.00 | 0.00 | BC 35 |
| | | | | Max $V_z$ | 0.67 | -4.24 | 6.14 | 0.00 | 0.00 | 0.00 | BC 35 |
| | | | | Min $V_z$ | -16.37 | -3.49 | -5.88 | 0.00 | -0.00 | 0.00 | BC 26 |
| | | | | Max $M_T$ | -10.55 | 0.00 | -0.35 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -10.55 | 0.00 | -0.35 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -2.30 | -4.24 | 6.04 | 0.00 | 0.00 | 0.00 | BC 25 |
| | | | | Min $M_y$ | -16.37 | -3.49 | -5.88 | 0.00 | -0.00 | 0.00 | BC 26 |
| | | | | Max $M_z$ | -15.97 | -2.29 | -2.08 | 0.00 | -0.00 | 0.00 | BC 24 |
| | | | | Min $M_z$ | -9.30 | 3.48 | -3.68 | 0.00 | -0.00 | -0.00 | BC 23 |
| | | | 0 | Max N | 0.67 | -4.24 | 6.14 | 0.00 | 0.00 | 0.00 | BC 43 |
| | | | Rechts | Min N | -17.43 | 0.00 | -0.86 | 0.00 | -0.00 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -9.30 | 3.48 | -3.68 | 0.00 | -0.00 | -0.00 | BC 23 |
| | | | | Min $V_y$ | 0.67 | -4.24 | 6.14 | 0.00 | 0.00 | 0.00 | BC 35 |
| | | | | Max $V_z$ | 0.67 | -4.24 | 6.14 | 0.00 | 0.00 | 0.00 | BC 35 |
| | | | | Min $V_z$ | -16.37 | -3.49 | -5.88 | 0.00 | -0.00 | 0.00 | BC 26 |
| | | | | Max $M_T$ | -10.55 | 0.00 | -0.35 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -10.55 | 0.00 | -0.35 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.67 | -4.24 | 6.14 | 0.00 | 0.00 | 0.00 | BC 43 |
| | | | | Min $M_y$ | -16.37 | -3.49 | -5.88 | 0.00 | -0.00 | 0.00 | BC 26 |
| | | | | Max $M_z$ | -2.30 | -4.24 | 6.04 | 0.00 | 0.00 | 0.00 | BC 25 |
| | | | | Min $M_z$ | -9.30 | 3.48 | -3.68 | 0.00 | -0.00 | -0.00 | BC 23 |
| | | | 50 | Max N | 0.69 | -4.14 | 6.07 | 0.00 | 0.31 | 0.21 | BC 43 |
| | | | Links | Min N | -17.41 | 0.00 | -0.86 | 0.00 | -0.04 | -0.00 | BC 12 |
| | | | | Max $V_y$ | -9.28 | 3.41 | -3.59 | 0.00 | -0.18 | -0.17 | BC 23 |
| | | | | Min $V_y$ | 0.69 | -4.14 | 6.07 | 0.00 | 0.31 | 0.21 | BC 35 |
| | | | | Max $V_z$ | 0.69 | -4.14 | 6.07 | 0.00 | 0.31 | 0.21 | BC 35 |
| | | | | Min $V_z$ | -16.35 | -3.41 | -5.83 | 0.00 | -0.29 | 0.17 | BC 26 |
| | | | | Max $M_T$ | -10.53 | 0.00 | -0.35 | 0.00 | -0.02 | -0.00 | BC 1 |
| | | | | Min $M_T$ | -10.53 | 0.00 | -0.35 | 0.00 | -0.02 | -0.00 | BC 1 |
| | | | | Max $M_y$ | 0.69 | -4.14 | 6.07 | 0.00 | 0.31 | 0.21 | BC 35 |
| | | | | Min $M_y$ | -16.35 | -3.41 | -5.83 | 0.00 | -0.29 | 0.17 | BC 26 |
| | | | | Max $M_z$ | 0.69 | -4.14 | 6.07 | 0.00 | 0.31 | 0.21 | BC 35 |
| | | | | Min $M_z$ | -9.28 | 3.41 | -3.59 | 0.00 | -0.18 | -0.17 | BC 23 |
| | | | 50 | Max N | 0.69 | -4.14 | 6.07 | 0.00 | 0.31 | 0.21 | BC 43 |
| | | | Rechts | Min N | -17.41 | 0.00 | -0.86 | 0.00 | -0.04 | -0.00 | BC 12 |
| | | | | Max $V_y$ | -9.28 | 3.41 | -3.59 | 0.00 | -0.18 | -0.17 | BC 23 |
| | | | | Min $V_y$ | 0.69 | -4.14 | 6.07 | 0.00 | 0.31 | 0.21 | BC 35 |
| | | | | Max $V_z$ | 0.69 | -4.14 | 6.07 | 0.00 | 0.31 | 0.21 | BC 35 |
| | | | | Min $V_z$ | -16.35 | -3.41 | -5.83 | 0.00 | -0.29 | 0.17 | BC 26 |
| | | | | Max $M_T$ | -10.53 | 0.00 | -0.35 | 0.00 | -0.02 | -0.00 | BC 1 |
| | | | | Min $M_T$ | -10.53 | 0.00 | -0.35 | 0.00 | -0.02 | -0.00 | BC 1 |
| | | | | Max $M_y$ | 0.69 | -4.14 | 6.07 | 0.00 | 0.31 | 0.21 | BC 35 |
| | | | | Min $M_y$ | -16.35 | -3.41 | -5.83 | 0.00 | -0.29 | 0.17 | BC 26 |
| | | | | Max $M_z$ | 0.69 | -4.14 | 6.07 | 0.00 | 0.31 | 0.21 | BC 35 |
| | | | | Min $M_z$ | -9.28 | 3.41 | -3.59 | 0.00 | -0.18 | -0.17 | BC 23 |
| | | | 2500 | Max N | 1.37 | 1.01 | 2.57 | 0.00 | 10.89 | 4.04 | BC 43 |
| | | | Links | Min N | -16.42 | 0.00 | -0.86 | 0.00 | -2.14 | -0.00 | BC 12 |
| | | | | Max $V_y$ | -1.29 | 1.01 | 2.48 | 0.00 | 10.64 | 4.04 | BC 25 |
| | | | | Min $V_y$ | -5.63 | -0.87 | 1.01 | 0.00 | -3.21 | -3.29 | BC 33 |
| | | | | Max $V_z$ | 1.36 | 1.01 | 2.58 | 0.00 | 10.89 | 4.04 | BC 35 |
| | | | | Min $V_z$ | -15.36 | 0.83 | -3.40 | 0.00 | -11.59 | 3.33 | BC 26 |
| | | | | Max $M_T$ | -9.41 | 0.00 | -0.35 | 0.00 | -0.86 | -0.00 | BC 1 |
| | | | | Min $M_T$ | -9.41 | 0.00 | -0.35 | 0.00 | -0.86 | -0.00 | BC 1 |
| | | | | Max $M_y$ | 1.36 | 1.01 | 2.58 | 0.00 | 10.89 | 4.04 | BC 35 |
| | | | | Min $M_y$ | -15.36 | 0.83 | -3.40 | 0.00 | -11.59 | 3.33 | BC 26 |
| | | | | Max $M_z$ | 1.36 | 1.01 | 2.58 | 0.00 | 10.89 | 4.04 | BC 35 |
| | | | | Min $M_z$ | -8.28 | -0.87 | 0.91 | 0.00 | -3.46 | -3.29 | BC 23 |
| | | | 2500 | Max N | 1.37 | 1.01 | 2.57 | 0.00 | 10.89 | 4.04 | BC 43 |
| | | | Rechts | Min N | -16.42 | 0.00 | -0.86 | 0.00 | -2.14 | -0.00 | BC 12 |
| | | | | Max $V_y$ | -1.29 | 1.01 | 2.48 | 0.00 | 10.64 | 4.04 | BC 25 |
| | | | | Min $V_y$ | -5.63 | -0.87 | 1.01 | 0.00 | -3.21 | -3.29 | BC 33 |
| | | | | Max $V_z$ | 1.36 | 1.01 | 2.58 | 0.00 | 10.89 | 4.04 | BC 35 |
| | | | | Min $V_z$ | -15.36 | 0.83 | -3.40 | 0.00 | -11.59 | 3.33 | BC 26 |
| | | | | Max $M_T$ | -9.41 | 0.00 | -0.35 | 0.00 | -0.86 | -0.00 | BC 1 |
| | | | | Min $M_T$ | -9.41 | 0.00 | -0.35 | 0.00 | -0.86 | -0.00 | BC 1 |
| | | | | Max $M_y$ | 1.36 | 1.01 | 2.58 | 0.00 | 10.89 | 4.04 | BC 35 |
| | | | | Min $M_y$ | -15.36 | 0.83 | -3.40 | 0.00 | -11.59 | 3.33 | BC 26 |
| | | | | Max $M_z$ | 1.36 | 1.01 | 2.58 | 0.00 | 10.89 | 4.04 | BC 35 |
| | | | | Min $M_z$ | -8.28 | -0.87 | 0.91 | 0.00 | -3.46 | -3.29 | BC 23 |
| | | | 2550 | Max N | 1.43 | 1.11 | 2.50 | 0.00 | 11.02 | 3.99 | BC 43 |
| | | | Links | Min N | -16.32 | 0.00 | -0.86 | 0.00 | -2.18 | -0.00 | BC 12 |
| | | | | Max $V_y$ | -1.19 | 1.11 | 2.40 | 0.00 | 10.77 | 3.99 | BC 25 |
| | | | | Min $V_y$ | -5.57 | -0.96 | 1.10 | 0.00 | -3.16 | -3.24 | BC 33 |
| | | | | Max $V_z$ | 1.43 | 1.11 | 2.50 | 0.00 | 11.02 | 3.99 | BC 35 |
| | | | | Min $V_z$ | -15.26 | 0.92 | -3.35 | 0.00 | -11.76 | 3.29 | BC 26 |
| | | | | Max $M_T$ | -9.30 | 0.00 | -0.35 | 0.00 | -0.88 | -0.00 | BC 1 |
| | | | | Min $M_T$ | -9.30 | 0.00 | -0.35 | 0.00 | -0.88 | -0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ | $V_z$ | Momenten [kNm] $M_T$ | $M_y$ | $M_z$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 1 | RC1 | | | Max $M_y$ | 1.43 | 1.11 | 2.50 | 0.00 | 11.02 | 3.99 | BC 35 |
| | | | | Min $M_y$ | -15.26 | 0.92 | -3.35 | 0.00 | -11.76 | 3.29 | BC 26 |
| | | | | Max $M_z$ | 1.43 | 1.11 | 2.50 | 0.00 | 11.02 | 3.99 | BC 35 |
| | | | | Min $M_z$ | -8.19 | -0.96 | 1.01 | 0.00 | -3.41 | -3.24 | BC 23 |
| | | | 2550 | Max N | 1.43 | 1.11 | 2.50 | 0.00 | 11.02 | 3.99 | BC 43 |
| | | | Rechts | Min N | -16.32 | 0.00 | -0.86 | 0.00 | -2.18 | -0.00 | BC 12 |
| | | | | Max $V_y$ | -1.19 | 1.11 | 2.40 | 0.00 | 10.77 | 3.99 | BC 25 |
| | | | | Min $V_y$ | -5.57 | -0.96 | 1.10 | 0.00 | -3.16 | -3.24 | BC 33 |
| | | | | Max $V_z$ | 1.43 | 1.11 | 2.50 | 0.00 | 11.02 | 3.99 | BC 35 |
| | | | | Min $V_z$ | -15.26 | 0.92 | -3.35 | 0.00 | -11.76 | 3.29 | BC 26 |
| | | | | Max $M_T$ | -9.30 | 0.00 | -0.35 | 0.00 | -0.88 | -0.00 | BC 1 |
| | | | | Min $M_T$ | -9.30 | 0.00 | -0.35 | 0.00 | -0.88 | -0.00 | BC 1 |
| | | | | Max $M_y$ | 1.43 | 1.11 | 2.50 | 0.00 | 11.02 | 3.99 | BC 35 |
| | | | | Min $M_y$ | -15.26 | 0.92 | -3.35 | 0.00 | -11.76 | 3.29 | BC 26 |
| | | | | Max $M_z$ | 1.43 | 1.11 | 2.50 | 0.00 | 11.02 | 3.99 | BC 35 |
| | | | | Min $M_z$ | -8.19 | -0.96 | 1.01 | 0.00 | -3.41 | -3.24 | BC 23 |
| | | | 4050 | Max N | 3.36 | 4.49 | 0.20 | 0.00 | 13.04 | -0.21 | BC 43 |
| | | | Links | Min N | -13.49 | 0.00 | -0.86 | 0.00 | -3.47 | -0.00 | BC 12 |
| | | | | Max $V_y$ | 1.64 | 4.49 | 0.10 | 0.00 | 12.64 | -0.21 | BC 25 |
| | | | | Min $V_y$ | -3.64 | -3.58 | 3.87 | 0.00 | 0.57 | 0.17 | BC 33 |
| | | | | Max $V_z$ | -3.64 | -3.58 | 3.87 | 0.00 | 0.57 | 0.17 | BC 33 |
| | | | | Min $V_z$ | -12.43 | 3.70 | -1.75 | 0.00 | -15.58 | -0.17 | BC 26 |
| | | | | Max $M_T$ | -6.10 | 0.00 | -0.35 | 0.00 | -1.40 | -0.00 | BC 1 |
| | | | | Min $M_T$ | -6.10 | 0.00 | -0.35 | 0.00 | -1.40 | -0.00 | BC 1 |
| | | | | Max $M_y$ | 3.36 | 4.49 | 0.20 | 0.00 | 13.05 | -0.21 | BC 35 |
| | | | | Min $M_y$ | -12.43 | 3.70 | -1.75 | 0.00 | -15.58 | -0.17 | BC 26 |
| | | | | Max $M_z$ | -3.64 | -3.58 | 3.87 | 0.00 | 0.57 | 0.17 | BC 33 |
| | | | | Min $M_z$ | 1.64 | 4.49 | 0.10 | 0.00 | 12.64 | -0.21 | BC 25 |
| | | 6 | 4050 | Max N | 3.36 | 4.49 | 0.20 | 0.00 | 13.04 | -0.21 | BC 43 |
| | | | Rechts | Min N | -13.49 | 0.00 | -0.86 | 0.00 | -3.47 | -0.00 | BC 12 |
| | | | | Max $V_y$ | 1.64 | 4.49 | 0.10 | 0.00 | 12.64 | -0.21 | BC 25 |
| | | | | Min $V_y$ | -3.64 | -3.59 | 3.87 | 0.00 | 0.57 | 0.17 | BC 33 |
| | | | | Max $V_z$ | -3.64 | -3.59 | 3.87 | 0.00 | 0.57 | 0.17 | BC 33 |
| | | | | Min $V_z$ | -12.43 | 3.70 | -1.75 | 0.00 | -15.58 | -0.17 | BC 26 |
| | | | | Max $M_T$ | -6.10 | 0.00 | -0.35 | 0.00 | -1.40 | -0.00 | BC 1 |
| | | | | Min $M_T$ | -6.10 | 0.00 | -0.35 | 0.00 | -1.40 | -0.00 | BC 1 |
| | | | | Max $M_y$ | 3.36 | 4.49 | 0.20 | 0.00 | 13.05 | -0.21 | BC 35 |
| | | | | Min $M_y$ | -12.43 | 3.70 | -1.75 | 0.00 | -15.58 | -0.17 | BC 26 |
| | | | | Max $M_z$ | -3.64 | -3.59 | 3.87 | 0.00 | 0.57 | 0.17 | BC 33 |
| | | | | Min $M_z$ | 1.64 | 4.49 | 0.10 | 0.00 | 12.64 | -0.21 | BC 25 |
| 2 | RC1 | 7 | 0 | Max N | -2.68 | -0.00 | 8.59 | 0.00 | 0.00 | 0.00 | BC 43 |
| | | | Links | Min N | -29.86 | -0.00 | -1.68 | 0.00 | -0.00 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -16.01 | 0.07 | -5.30 | 0.00 | -0.00 | -0.00 | BC 33 |
| | | | | Min $V_y$ | -13.60 | -0.00 | -5.49 | 0.00 | -0.00 | 0.00 | BC 24 |
| | | | | Max $V_z$ | -2.68 | -0.00 | 8.60 | 0.00 | 0.00 | 0.00 | BC 35 |
| | | | | Min $V_z$ | -20.34 | -0.00 | -8.01 | 0.00 | -0.00 | 0.00 | BC 26 |
| | | | | Max $M_T$ | -15.46 | -0.00 | -0.65 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -15.46 | -0.00 | -0.65 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -7.03 | -0.00 | 8.41 | 0.00 | 0.00 | 0.00 | BC 25 |
| | | | | Min $M_y$ | -13.60 | -0.00 | -5.49 | 0.00 | -0.00 | 0.00 | BC 24 |
| | | | | Max $M_z$ | -15.46 | -0.00 | -0.65 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -20.36 | 0.07 | -5.48 | 0.00 | -0.00 | -0.00 | BC 15 |
| | | | 0 | Max N | -2.68 | -0.00 | 8.59 | 0.00 | 0.00 | 0.00 | BC 43 |
| | | | Rechts | Min N | -29.86 | -0.00 | -1.68 | 0.00 | -0.00 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -16.01 | 0.07 | -5.30 | 0.00 | -0.00 | -0.00 | BC 33 |
| | | | | Min $V_y$ | -13.60 | -0.00 | -5.49 | 0.00 | -0.00 | 0.00 | BC 24 |
| | | | | Max $V_z$ | -2.68 | -0.00 | 8.60 | 0.00 | 0.00 | 0.00 | BC 35 |
| | | | | Min $V_z$ | -20.34 | -0.00 | -8.01 | 0.00 | -0.00 | 0.00 | BC 26 |
| | | | | Max $M_T$ | -15.46 | -0.00 | -0.65 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -15.46 | -0.00 | -0.65 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -2.68 | -0.00 | 8.59 | 0.00 | 0.00 | 0.00 | BC 43 |
| | | | | Min $M_y$ | -20.34 | -0.00 | -8.01 | 0.00 | -0.00 | 0.00 | BC 26 |
| | | | | Max $M_z$ | -13.61 | -0.00 | -5.48 | 0.00 | -0.00 | 0.00 | BC 16 |
| | | | | Min $M_z$ | -20.36 | 0.07 | -5.48 | 0.00 | -0.00 | -0.00 | BC 15 |
| | | | 50 | Max N | -2.66 | -0.00 | 8.45 | 0.00 | 0.43 | 0.00 | BC 43 |
| | | | Links | Min N | -29.84 | -0.00 | -1.68 | 0.00 | -0.08 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -15.99 | 0.07 | -5.17 | 0.00 | -0.26 | -0.00 | BC 33 |
| | | | | Min $V_y$ | -13.58 | -0.00 | -5.35 | 0.00 | -0.27 | 0.00 | BC 24 |
| | | | | Max $V_z$ | -2.66 | -0.00 | 8.45 | 0.00 | 0.43 | 0.00 | BC 35 |
| | | | | Min $V_z$ | -20.32 | -0.00 | -7.91 | 0.00 | -0.40 | 0.00 | BC 26 |
| | | | | Max $M_T$ | -15.44 | -0.00 | -0.65 | 0.00 | -0.03 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -15.44 | -0.00 | -0.65 | 0.00 | -0.03 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -2.66 | -0.00 | 8.45 | 0.00 | 0.43 | 0.00 | BC 35 |
| | | | | Min $M_y$ | -20.32 | -0.00 | -7.91 | 0.00 | -0.40 | 0.00 | BC 26 |
| | | | | Max $M_z$ | -13.58 | -0.00 | -5.35 | 0.00 | -0.27 | 0.00 | BC 24 |
| | | | | Min $M_z$ | -15.99 | 0.07 | -5.17 | 0.00 | -0.26 | -0.00 | BC 33 |
| | | | 50 | Max N | -2.66 | -0.00 | 8.45 | 0.00 | 0.43 | 0.00 | BC 43 |
| | | | Rechts | Min N | -29.84 | -0.00 | -1.68 | 0.00 | -0.08 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -15.99 | 0.07 | -5.17 | 0.00 | -0.26 | -0.00 | BC 33 |
| | | | | Min $V_y$ | -13.58 | -0.00 | -5.35 | 0.00 | -0.27 | 0.00 | BC 24 |
| | | | | Max $V_z$ | -2.66 | -0.00 | 8.45 | 0.00 | 0.43 | 0.00 | BC 35 |
| | | | | Min $V_z$ | -20.32 | -0.00 | -7.91 | 0.00 | -0.40 | 0.00 | BC 26 |
| | | | | Max $M_T$ | -15.44 | -0.00 | -0.65 | 0.00 | -0.03 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -15.44 | -0.00 | -0.65 | 0.00 | -0.03 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -2.66 | -0.00 | 8.45 | 0.00 | 0.43 | 0.00 | BC 35 |
| | | | | Min $M_y$ | -20.32 | -0.00 | -7.91 | 0.00 | -0.40 | 0.00 | BC 26 |
| | | | | Max $M_z$ | -13.58 | -0.00 | -5.35 | 0.00 | -0.27 | 0.00 | BC 24 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ | $V_z$ | Momenten [kNm] $M_T$ | $M_y$ | $M_z$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 2 | RC1 | | | Min $M_z$ | -15.99 | 0.07 | -5.17 | 0.00 | -0.26 | -0.00 | BC 33 |
| | | | 2500 | Max N | -1.99 | -0.00 | 1.47 | 0.00 | 12.58 | 0.00 | BC 43 |
| | | | Links | Min N | -28.85 | -0.00 | -1.68 | 0.00 | -4.19 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -15.32 | 0.07 | 1.39 | 0.00 | -4.90 | -0.17 | BC 33 |
| | | | | Min $V_y$ | -12.59 | -0.00 | 1.20 | 0.00 | -5.36 | 0.00 | BC 24 |
| | | | | Max $V_z$ | -1.99 | -0.00 | 1.47 | 0.00 | 12.58 | 0.00 | BC 35 |
| | | | | Min $V_z$ | -19.32 | -0.00 | -3.05 | 0.00 | -13.83 | 0.00 | BC 26 |
| | | | | Max $M_T$ | -14.32 | -0.00 | -0.65 | 0.00 | -1.62 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -14.32 | -0.00 | -0.65 | 0.00 | -1.62 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -1.99 | -0.00 | 1.47 | 0.00 | 12.58 | 0.00 | BC 35 |
| | | | | Min $M_y$ | -19.32 | -0.00 | -3.05 | 0.00 | -13.83 | 0.00 | BC 26 |
| | | | | Max $M_z$ | -12.59 | -0.00 | 1.20 | 0.00 | -5.36 | 0.00 | BC 24 |
| | | | | Min $M_z$ | -15.32 | 0.07 | 1.39 | 0.00 | -4.90 | -0.17 | BC 33 |
| | | | 2500 | Max N | -1.99 | -0.00 | 1.47 | 0.00 | 12.58 | 0.00 | BC 43 |
| | | | Rechts | Min N | -28.85 | -0.00 | -1.68 | 0.00 | -4.19 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -15.32 | 0.07 | 1.39 | 0.00 | -4.90 | -0.17 | BC 33 |
| | | | | Min $V_y$ | -12.59 | -0.00 | 1.20 | 0.00 | -5.36 | 0.00 | BC 24 |
| | | | | Max $V_z$ | -1.99 | -0.00 | 1.47 | 0.00 | 12.58 | 0.00 | BC 35 |
| | | | | Min $V_z$ | -19.32 | -0.00 | -3.05 | 0.00 | -13.83 | 0.00 | BC 26 |
| | | | | Max $M_T$ | -14.32 | -0.00 | -0.65 | 0.00 | -1.62 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -14.32 | -0.00 | -0.65 | 0.00 | -1.62 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -1.99 | -0.00 | 1.47 | 0.00 | 12.58 | 0.00 | BC 35 |
| | | | | Min $M_y$ | -19.32 | -0.00 | -3.05 | 0.00 | -13.83 | 0.00 | BC 26 |
| | | | | Max $M_z$ | -12.59 | -0.00 | 1.20 | 0.00 | -5.36 | 0.00 | BC 24 |
| | | | | Min $M_z$ | -15.32 | 0.07 | 1.39 | 0.00 | -4.90 | -0.17 | BC 33 |
| | | | 4050 | Max N | -0.09 | -0.00 | -3.28 | 0.00 | 11.17 | 0.00 | BC 43 |
| | | | Links | Min N | -26.07 | -0.00 | -1.68 | 0.00 | -6.79 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -13.42 | 0.07 | 5.54 | 0.00 | 0.47 | -0.28 | BC 33 |
| | | | | Min $V_y$ | -9.81 | -0.00 | 5.36 | 0.00 | -0.28 | 0.00 | BC 24 |
| | | | | Max $V_z$ | -6.66 | -0.00 | 5.54 | 0.00 | 0.47 | 0.00 | BC 34 |
| | | | | Min $V_z$ | -3.24 | -0.00 | -3.46 | 0.00 | 10.44 | 0.00 | BC 25 |
| | | | | Max $M_T$ | -11.19 | -0.00 | -0.65 | 0.00 | -2.63 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -11.19 | -0.00 | -0.65 | 0.00 | -2.63 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.09 | -0.00 | -3.28 | 0.00 | 11.18 | 0.00 | BC 35 |
| | | | | Min $M_y$ | -16.55 | -0.00 | 0.25 | 0.00 | -16.01 | 0.00 | BC 26 |
| | | | | Max $M_z$ | -9.81 | -0.00 | 5.36 | 0.00 | -0.28 | 0.00 | BC 24 |
| | | | | Min $M_z$ | -13.42 | 0.07 | 5.54 | 0.00 | 0.47 | -0.28 | BC 33 |
| | | 8 | 4050 | Max N | -0.09 | -0.00 | -3.28 | 0.00 | 11.17 | 0.00 | BC 43 |
| | | | Rechts | Min N | -26.07 | -0.00 | -1.68 | 0.00 | -6.79 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -13.42 | 0.07 | 5.54 | 0.00 | 0.47 | -0.28 | BC 33 |
| | | | | Min $V_y$ | -9.81 | -0.00 | 5.36 | 0.00 | -0.28 | 0.00 | BC 24 |
| | | | | Max $V_z$ | -6.66 | -0.00 | 5.54 | 0.00 | 0.47 | 0.00 | BC 34 |
| | | | | Min $V_z$ | -3.24 | -0.00 | -3.46 | 0.00 | 10.44 | 0.00 | BC 25 |
| | | | | Max $M_T$ | -11.19 | -0.00 | -0.65 | 0.00 | -2.63 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -11.19 | -0.00 | -0.65 | 0.00 | -2.63 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.09 | -0.00 | -3.28 | 0.00 | 11.18 | 0.00 | BC 35 |
| | | | | Min $M_y$ | -16.55 | -0.00 | 0.25 | 0.00 | -16.01 | 0.00 | BC 26 |
| | | | | Max $M_z$ | -9.81 | -0.00 | 5.36 | 0.00 | -0.28 | 0.00 | BC 24 |
| | | | | Min $M_z$ | -13.42 | 0.07 | 5.54 | 0.00 | 0.47 | -0.28 | BC 33 |
| 3 | RC1 | 9 | 0 | Max N | 0.73 | 4.24 | 6.14 | 0.00 | 0.00 | -0.00 | BC 43 |
| | | | Links | Min N | -17.34 | -0.00 | -0.86 | 0.00 | 0.00 | 0.00 | BC 12 |
| | | | | Max $V_y$ | 0.73 | 4.24 | 6.14 | 0.00 | 0.00 | -0.00 | BC 43 |
| | | | | Min $V_y$ | -6.31 | -3.48 | -3.58 | 0.00 | 0.00 | 0.00 | BC 34 |
| | | | | Max $V_z$ | 0.73 | 4.24 | 6.14 | 0.00 | 0.00 | -0.00 | BC 35 |
| | | | | Min $V_z$ | -16.29 | 3.49 | -5.88 | 0.00 | 0.00 | 0.00 | BC 26 |
| | | | | Max $M_T$ | -10.45 | -0.00 | -0.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -10.45 | -0.00 | -0.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -2.21 | 4.24 | 6.04 | 0.00 | 0.00 | -0.00 | BC 17 |
| | | | | Min $M_y$ | -10.45 | -0.00 | -0.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -16.29 | 3.49 | -5.88 | 0.00 | 0.00 | 0.00 | BC 18 |
| | | | | Min $M_z$ | -2.21 | 4.24 | 6.04 | 0.00 | 0.00 | -0.00 | BC 17 |
| | | | 0 | Max N | 0.73 | 4.24 | 6.14 | 0.00 | 0.00 | -0.00 | BC 43 |
| | | | Rechts | Min N | -17.34 | -0.00 | -0.86 | 0.00 | -0.00 | 0.00 | BC 12 |
| | | | | Max $V_y$ | 0.73 | 4.24 | 6.14 | 0.00 | 0.00 | -0.00 | BC 43 |
| | | | | Min $V_y$ | -6.31 | -3.48 | -3.58 | 0.00 | -0.00 | 0.00 | BC 34 |
| | | | | Max $V_z$ | 0.73 | 4.24 | 6.14 | 0.00 | 0.00 | -0.00 | BC 35 |
| | | | | Min $V_z$ | -16.29 | 3.49 | -5.88 | 0.00 | -0.00 | -0.00 | BC 26 |
| | | | | Max $M_T$ | -10.45 | -0.00 | -0.35 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -10.45 | -0.00 | -0.35 | 0.00 | -0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.73 | 4.24 | 6.14 | 0.00 | 0.00 | -0.00 | BC 35 |
| | | | | Min $M_y$ | -16.29 | 3.49 | -5.88 | 0.00 | -0.00 | -0.00 | BC 26 |
| | | | | Max $M_z$ | -9.25 | -3.48 | -3.68 | 0.00 | -0.00 | 0.00 | BC 16 |
| | | | | Min $M_z$ | -2.21 | 4.24 | 6.04 | 0.00 | 0.00 | -0.00 | BC 17 |
| | | | 50 | Max N | 0.75 | 4.14 | 6.07 | 0.00 | 0.31 | -0.21 | BC 43 |
| | | | Links | Min N | -17.32 | -0.00 | -0.86 | 0.00 | -0.04 | 0.00 | BC 12 |
| | | | | Max $V_y$ | 0.75 | 4.14 | 6.07 | 0.00 | 0.31 | -0.21 | BC 35 |
| | | | | Min $V_y$ | -6.30 | -3.41 | -3.49 | 0.00 | -0.18 | 0.17 | BC 34 |
| | | | | Max $V_z$ | 0.75 | 4.14 | 6.07 | 0.00 | 0.31 | -0.21 | BC 35 |
| | | | | Min $V_z$ | -16.27 | 3.41 | -5.83 | 0.00 | -0.29 | -0.17 | BC 26 |
| | | | | Max $M_T$ | -10.42 | -0.00 | -0.35 | 0.00 | -0.02 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -10.42 | -0.00 | -0.35 | 0.00 | -0.02 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.75 | 4.14 | 6.07 | 0.00 | 0.31 | -0.21 | BC 35 |
| | | | | Min $M_y$ | -16.27 | 3.41 | -5.83 | 0.00 | -0.29 | -0.17 | BC 26 |
| | | | | Max $M_z$ | -6.30 | -3.41 | -3.49 | 0.00 | -0.18 | 0.17 | BC 34 |
| | | | | Min $M_z$ | 0.75 | 4.14 | 6.07 | 0.00 | 0.31 | -0.21 | BC 35 |
| | | | 50 | Max N | 0.75 | 4.14 | 6.07 | 0.00 | 0.31 | -0.21 | BC 43 |
| | | | Rechts | Min N | -17.32 | -0.00 | -0.86 | 0.00 | -0.04 | 0.00 | BC 12 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ | $V_z$ | Momenten [kNm] $M_T$ | $M_y$ | $M_z$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 3 | RC1 | | | Max $V_y$ | 0.75 | 4.14 | 6.07 | 0.00 | 0.31 | -0.21 | BC 35 |
| | | | | Min $V_y$ | -6.30 | -3.41 | -3.49 | 0.00 | -0.18 | 0.17 | BC 34 |
| | | | | Max $V_z$ | 0.75 | 4.14 | 6.07 | 0.00 | 0.31 | -0.21 | BC 35 |
| | | | | Min $V_z$ | -16.27 | 3.41 | -5.83 | 0.00 | -0.29 | -0.17 | BC 26 |
| | | | | Max $M_T$ | -10.42 | -0.00 | -0.35 | 0.00 | -0.02 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -10.42 | -0.00 | -0.35 | 0.00 | -0.02 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.75 | 4.14 | 6.07 | 0.00 | 0.31 | -0.21 | BC 35 |
| | | | | Min $M_y$ | -16.27 | 3.41 | -5.83 | 0.00 | -0.29 | -0.17 | BC 26 |
| | | | | Max $M_z$ | -6.30 | -3.41 | -3.49 | 0.00 | -0.18 | 0.17 | BC 34 |
| | | | | Min $M_z$ | 0.75 | 4.14 | 6.07 | 0.00 | 0.31 | -0.21 | BC 35 |
| | | | 2500 | Max N | 1.42 | -1.01 | 2.58 | 0.00 | 10.89 | -4.04 | BC 43 |
| | | | Links | Min N | -16.33 | -0.00 | -0.86 | 0.00 | -2.14 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -5.62 | 0.87 | 1.01 | 0.00 | -3.22 | 3.28 | BC 42 |
| | | | | Min $V_y$ | -1.20 | -1.01 | 2.48 | 0.00 | 10.65 | -4.04 | BC 17 |
| | | | | Max $V_z$ | 1.42 | -1.01 | 2.58 | 0.00 | 10.90 | -4.04 | BC 35 |
| | | | | Min $V_z$ | -15.28 | -0.83 | -3.40 | 0.00 | -11.60 | -3.33 | BC 26 |
| | | | | Max $M_T$ | -9.30 | -0.00 | -0.35 | 0.00 | -0.86 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -9.30 | -0.00 | -0.35 | 0.00 | -0.86 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 1.42 | -1.01 | 2.58 | 0.00 | 10.90 | -4.04 | BC 35 |
| | | | | Min $M_y$ | -15.28 | -0.83 | -3.40 | 0.00 | -11.60 | -3.33 | BC 26 |
| | | | | Max $M_z$ | -5.62 | 0.87 | 1.01 | 0.00 | -3.21 | 3.28 | BC 34 |
| | | | | Min $M_z$ | 1.42 | -1.01 | 2.58 | 0.00 | 10.89 | -4.04 | BC 43 |
| | | | 2500 | Max N | 1.42 | -1.01 | 2.58 | 0.00 | 10.89 | -4.04 | BC 43 |
| | | | Rechts | Min N | -16.33 | -0.00 | -0.86 | 0.00 | -2.14 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -5.62 | 0.87 | 1.01 | 0.00 | -3.22 | 3.28 | BC 42 |
| | | | | Min $V_y$ | -1.20 | -1.01 | 2.48 | 0.00 | 10.65 | -4.04 | BC 17 |
| | | | | Max $V_z$ | 1.42 | -1.01 | 2.58 | 0.00 | 10.90 | -4.04 | BC 35 |
| | | | | Min $V_z$ | -15.28 | -0.83 | -3.40 | 0.00 | -11.60 | -3.33 | BC 26 |
| | | | | Max $M_T$ | -9.30 | -0.00 | -0.35 | 0.00 | -0.86 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -9.30 | -0.00 | -0.35 | 0.00 | -0.86 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 1.42 | -1.01 | 2.58 | 0.00 | 10.90 | -4.04 | BC 35 |
| | | | | Min $M_y$ | -15.28 | -0.83 | -3.40 | 0.00 | -11.60 | -3.33 | BC 26 |
| | | | | Max $M_z$ | -5.62 | 0.87 | 1.01 | 0.00 | -3.21 | 3.28 | BC 34 |
| | | | | Min $M_z$ | 1.42 | -1.01 | 2.58 | 0.00 | 10.89 | -4.04 | BC 43 |
| | | | 2550 | Max N | 1.49 | -1.11 | 2.50 | 0.00 | 11.02 | -3.99 | BC 43 |
| | | | Links | Min N | -16.23 | -0.00 | -0.86 | 0.00 | -2.18 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -5.55 | 0.96 | 1.10 | 0.00 | -3.16 | 3.24 | BC 42 |
| | | | | Min $V_y$ | -1.11 | -1.11 | 2.40 | 0.00 | 10.78 | -3.99 | BC 17 |
| | | | | Max $V_z$ | 1.49 | -1.11 | 2.50 | 0.00 | 11.03 | -3.99 | BC 35 |
| | | | | Min $V_z$ | -15.19 | -0.91 | -3.35 | 0.00 | -11.77 | -3.29 | BC 26 |
| | | | | Max $M_T$ | -9.20 | -0.00 | -0.35 | 0.00 | -0.88 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -9.20 | -0.00 | -0.35 | 0.00 | -0.88 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 1.49 | -1.11 | 2.50 | 0.00 | 11.03 | -3.99 | BC 35 |
| | | | | Min $M_y$ | -15.19 | -0.91 | -3.35 | 0.00 | -11.77 | -3.29 | BC 26 |
| | | | | Max $M_z$ | -5.55 | 0.96 | 1.10 | 0.00 | -3.16 | 3.24 | BC 34 |
| | | | | Min $M_z$ | 1.49 | -1.11 | 2.50 | 0.00 | 11.02 | -3.99 | BC 43 |
| | | | 2550 | Max N | 1.49 | -1.11 | 2.50 | 0.00 | 11.02 | -3.99 | BC 43 |
| | | | Rechts | Min N | -16.23 | -0.00 | -0.86 | 0.00 | -2.18 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -5.55 | 0.96 | 1.10 | 0.00 | -3.16 | 3.24 | BC 42 |
| | | | | Min $V_y$ | -1.11 | -1.11 | 2.40 | 0.00 | 10.78 | -3.99 | BC 17 |
| | | | | Max $V_z$ | 1.49 | -1.11 | 2.50 | 0.00 | 11.03 | -3.99 | BC 35 |
| | | | | Min $V_z$ | -15.19 | -0.91 | -3.35 | 0.00 | -11.77 | -3.29 | BC 26 |
| | | | | Max $M_T$ | -9.20 | -0.00 | -0.35 | 0.00 | -0.88 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -9.20 | -0.00 | -0.35 | 0.00 | -0.88 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 1.49 | -1.11 | 2.50 | 0.00 | 11.03 | -3.99 | BC 35 |
| | | | | Min $M_y$ | -15.19 | -0.91 | -3.35 | 0.00 | -11.77 | -3.29 | BC 26 |
| | | | | Max $M_z$ | -5.55 | 0.96 | 1.10 | 0.00 | -3.16 | 3.24 | BC 34 |
| | | | | Min $M_z$ | 1.49 | -1.11 | 2.50 | 0.00 | 11.02 | -3.99 | BC 43 |
| | | | 4050 | Max N | 3.42 | -4.49 | 0.20 | 0.00 | 13.05 | 0.21 | BC 43 |
| | | | Links | Min N | -13.40 | -0.00 | -0.86 | 0.00 | -3.47 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -3.62 | 3.59 | 3.87 | 0.00 | 0.57 | -0.17 | BC 34 |
| | | | | Min $V_y$ | 3.42 | -4.49 | 0.20 | 0.00 | 13.06 | 0.21 | BC 35 |
| | | | | Max $V_z$ | -3.62 | 3.59 | 3.87 | 0.00 | 0.57 | -0.17 | BC 34 |
| | | | | Min $V_z$ | -12.35 | -3.70 | -1.75 | 0.00 | -15.59 | 0.17 | BC 26 |
| | | | | Max $M_T$ | -6.00 | -0.00 | -0.35 | 0.00 | -1.40 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -6.00 | -0.00 | -0.35 | 0.00 | -1.40 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 3.42 | -4.49 | 0.20 | 0.00 | 13.06 | 0.21 | BC 35 |
| | | | | Min $M_y$ | -12.35 | -3.70 | -1.75 | 0.00 | -15.59 | 0.17 | BC 26 |
| | | | | Max $M_z$ | 1.73 | -4.49 | 0.11 | 0.00 | 12.66 | 0.21 | BC 17 |
| | | | | Min $M_z$ | -3.62 | 3.59 | 3.87 | 0.00 | 0.56 | -0.17 | BC 42 |
| | | 10 | 4050 | Max N | 3.42 | -4.49 | 0.20 | 0.00 | 13.05 | 0.21 | BC 43 |
| | | | Rechts | Min N | -13.40 | -0.00 | -0.86 | 0.00 | -3.47 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -3.62 | 3.59 | 3.87 | 0.00 | 0.57 | -0.17 | BC 34 |
| | | | | Min $V_y$ | 3.42 | -4.49 | 0.20 | 0.00 | 13.06 | 0.21 | BC 35 |
| | | | | Max $V_z$ | -3.62 | 3.59 | 3.87 | 0.00 | 0.57 | -0.17 | BC 34 |
| | | | | Min $V_z$ | -12.35 | -3.70 | -1.75 | 0.00 | -15.59 | 0.17 | BC 26 |
| | | | | Max $M_T$ | -6.00 | -0.00 | -0.35 | 0.00 | -1.40 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -6.00 | -0.00 | -0.35 | 0.00 | -1.40 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 3.42 | -4.49 | 0.20 | 0.00 | 13.06 | 0.21 | BC 35 |
| | | | | Min $M_y$ | -12.35 | -3.70 | -1.75 | 0.00 | -15.59 | 0.17 | BC 26 |
| | | | | Max $M_z$ | 1.73 | -4.49 | 0.11 | 0.00 | 12.66 | 0.21 | BC 17 |
| | | | | Min $M_z$ | -3.62 | 3.59 | 3.87 | 0.00 | 0.56 | -0.17 | BC 42 |
| 4 | RC1 | 11 | 0 | Max N | 0.67 | -4.24 | -6.14 | 0.00 | -0.00 | 0.00 | BC 44 |
| | | | Links | Min N | -17.43 | 0.00 | 0.86 | 0.00 | 0.00 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -9.30 | 3.48 | 3.68 | 0.00 | 0.00 | -0.00 | BC 23 |
| | | | | Min $V_y$ | 0.67 | -4.24 | -6.14 | 0.00 | -0.00 | 0.00 | BC 36 |
| | | | | Max $V_z$ | -16.37 | -3.49 | 5.88 | 0.00 | 0.00 | 0.00 | BC 25 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ | $V_z$ | Momenten [kNm] $M_T$ | $M_y$ | $M_z$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 4 | RC1 | | | Min $V_z$ | 0.67 | -4.24 | -6.14 | 0.00 | -0.00 | 0.00 | BC 36 |
| | | | | Max $M_T$ | -10.55 | 0.00 | 0.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -10.55 | 0.00 | 0.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -16.37 | -3.49 | 5.88 | 0.00 | 0.00 | 0.00 | BC 25 |
| | | | | Min $M_y$ | -2.30 | -4.24 | -6.04 | 0.00 | -0.00 | 0.00 | BC 26 |
| | | | | Max $M_z$ | -15.97 | -2.29 | 2.08 | 0.00 | 0.00 | 0.00 | BC 24 |
| | | | | Min $M_z$ | -9.30 | 3.48 | 3.68 | 0.00 | 0.00 | -0.00 | BC 23 |
| | | | 0 | Max N | 0.67 | -4.24 | -6.14 | 0.00 | -0.00 | 0.00 | BC 44 |
| | | | Rechts | Min N | -17.43 | 0.00 | 0.86 | 0.00 | 0.00 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -9.30 | 3.48 | 3.68 | 0.00 | 0.00 | -0.00 | BC 23 |
| | | | | Min $V_y$ | 0.67 | -4.24 | -6.14 | 0.00 | -0.00 | 0.00 | BC 36 |
| | | | | Max $V_z$ | -16.37 | -3.49 | 5.88 | 0.00 | 0.00 | 0.00 | BC 25 |
| | | | | Min $V_z$ | 0.67 | -4.24 | -6.14 | 0.00 | -0.00 | 0.00 | BC 36 |
| | | | | Max $M_T$ | -10.55 | 0.00 | 0.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -10.55 | 0.00 | 0.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -16.37 | -3.49 | 5.88 | 0.00 | 0.00 | 0.00 | BC 25 |
| | | | | Min $M_y$ | 0.67 | -4.24 | -6.14 | 0.00 | -0.00 | 0.00 | BC 44 |
| | | | | Max $M_z$ | -2.30 | -4.24 | -6.04 | 0.00 | -0.00 | 0.00 | BC 26 |
| | | | | Min $M_z$ | -9.30 | 3.48 | 3.68 | 0.00 | 0.00 | -0.00 | BC 23 |
| | | | 50 | Max N | 0.69 | -4.14 | -6.07 | 0.00 | -0.31 | 0.21 | BC 44 |
| | | | Links | Min N | -17.41 | 0.00 | 0.86 | 0.00 | 0.04 | -0.00 | BC 12 |
| | | | | Max $V_y$ | -9.28 | 3.41 | 3.59 | 0.00 | 0.18 | -0.17 | BC 23 |
| | | | | Min $V_y$ | 0.69 | -4.14 | -6.07 | 0.00 | -0.31 | 0.21 | BC 36 |
| | | | | Max $V_z$ | -16.35 | -3.41 | 5.83 | 0.00 | 0.29 | 0.17 | BC 25 |
| | | | | Min $V_z$ | 0.69 | -4.14 | -6.07 | 0.00 | -0.31 | 0.21 | BC 36 |
| | | | | Max $M_T$ | -10.53 | 0.00 | 0.35 | 0.00 | 0.02 | -0.00 | BC 1 |
| | | | | Min $M_T$ | -10.53 | 0.00 | 0.35 | 0.00 | 0.02 | -0.00 | BC 1 |
| | | | | Max $M_y$ | -16.35 | -3.41 | 5.83 | 0.00 | 0.29 | 0.17 | BC 25 |
| | | | | Min $M_y$ | 0.69 | -4.14 | -6.07 | 0.00 | -0.31 | 0.21 | BC 36 |
| | | | | Max $M_z$ | 0.69 | -4.14 | -6.07 | 0.00 | -0.31 | 0.21 | BC 36 |
| | | | | Min $M_z$ | -9.28 | 3.41 | 3.59 | 0.00 | 0.18 | -0.17 | BC 23 |
| | | | 50 | Max N | 0.69 | -4.14 | -6.07 | 0.00 | -0.31 | 0.21 | BC 44 |
| | | | Rechts | Min N | -17.41 | 0.00 | 0.86 | 0.00 | 0.04 | -0.00 | BC 12 |
| | | | | Max $V_y$ | -9.28 | 3.41 | 3.59 | 0.00 | 0.18 | -0.17 | BC 23 |
| | | | | Min $V_y$ | 0.69 | -4.14 | -6.07 | 0.00 | -0.31 | 0.21 | BC 36 |
| | | | | Max $V_z$ | -16.35 | -3.41 | 5.83 | 0.00 | 0.29 | 0.17 | BC 25 |
| | | | | Min $V_z$ | 0.69 | -4.14 | -6.07 | 0.00 | -0.31 | 0.21 | BC 36 |
| | | | | Max $M_T$ | -10.53 | 0.00 | 0.35 | 0.00 | 0.02 | -0.00 | BC 1 |
| | | | | Min $M_T$ | -10.53 | 0.00 | 0.35 | 0.00 | 0.02 | -0.00 | BC 1 |
| | | | | Max $M_y$ | -16.35 | -3.41 | 5.83 | 0.00 | 0.29 | 0.17 | BC 25 |
| | | | | Min $M_y$ | 0.69 | -4.14 | -6.07 | 0.00 | -0.31 | 0.21 | BC 36 |
| | | | | Max $M_z$ | 0.69 | -4.14 | -6.07 | 0.00 | -0.31 | 0.21 | BC 36 |
| | | | | Min $M_z$ | -9.28 | 3.41 | 3.59 | 0.00 | 0.18 | -0.17 | BC 23 |
| | | | 2500 | Max N | 1.37 | 1.01 | -2.57 | 0.00 | -10.89 | 4.04 | BC 44 |
| | | | Links | Min N | -16.42 | 0.00 | 0.86 | 0.00 | 2.14 | -0.00 | BC 12 |
| | | | | Max $V_y$ | -1.29 | 1.01 | -2.48 | 0.00 | -10.64 | 4.04 | BC 26 |
| | | | | Min $V_y$ | -5.63 | -0.87 | -1.01 | 0.00 | 3.21 | -3.29 | BC 33 |
| | | | | Max $V_z$ | -15.36 | 0.83 | 3.40 | 0.00 | 11.59 | 3.33 | BC 25 |
| | | | | Min $V_z$ | 1.36 | 1.01 | -2.58 | 0.00 | -10.89 | 4.04 | BC 36 |
| | | | | Max $M_T$ | -9.41 | 0.00 | 0.35 | 0.00 | 0.86 | -0.00 | BC 1 |
| | | | | Min $M_T$ | -9.41 | 0.00 | 0.35 | 0.00 | 0.86 | -0.00 | BC 1 |
| | | | | Max $M_y$ | -15.36 | 0.83 | 3.40 | 0.00 | 11.59 | 3.33 | BC 25 |
| | | | | Min $M_y$ | 1.36 | 1.01 | -2.58 | 0.00 | -10.89 | 4.04 | BC 36 |
| | | | | Max $M_z$ | 1.36 | 1.01 | -2.58 | 0.00 | -10.89 | 4.04 | BC 36 |
| | | | | Min $M_z$ | -8.28 | -0.87 | -0.91 | 0.00 | 3.46 | -3.29 | BC 23 |
| | | | 2500 | Max N | 1.37 | 1.01 | -2.57 | 0.00 | -10.89 | 4.04 | BC 44 |
| | | | Rechts | Min N | -16.42 | 0.00 | 0.86 | 0.00 | 2.14 | -0.00 | BC 12 |
| | | | | Max $V_y$ | -1.29 | 1.01 | -2.48 | 0.00 | -10.64 | 4.04 | BC 26 |
| | | | | Min $V_y$ | -5.63 | -0.87 | -1.01 | 0.00 | 3.21 | -3.29 | BC 33 |
| | | | | Max $V_z$ | -15.36 | 0.83 | 3.40 | 0.00 | 11.59 | 3.33 | BC 25 |
| | | | | Min $V_z$ | 1.36 | 1.01 | -2.58 | 0.00 | -10.89 | 4.04 | BC 36 |
| | | | | Max $M_T$ | -9.41 | 0.00 | 0.35 | 0.00 | 0.86 | -0.00 | BC 1 |
| | | | | Min $M_T$ | -9.41 | 0.00 | 0.35 | 0.00 | 0.86 | -0.00 | BC 1 |
| | | | | Max $M_y$ | -15.36 | 0.83 | 3.40 | 0.00 | 11.59 | 3.33 | BC 25 |
| | | | | Min $M_y$ | 1.36 | 1.01 | -2.58 | 0.00 | -10.89 | 4.04 | BC 36 |
| | | | | Max $M_z$ | 1.36 | 1.01 | -2.58 | 0.00 | -10.89 | 4.04 | BC 36 |
| | | | | Min $M_z$ | -8.28 | -0.87 | -0.91 | 0.00 | 3.46 | -3.29 | BC 23 |
| | | | 2550 | Max N | 1.43 | 1.11 | -2.50 | 0.00 | -11.02 | 3.99 | BC 44 |
| | | | Links | Min N | -16.32 | 0.00 | 0.86 | 0.00 | 2.18 | -0.00 | BC 12 |
| | | | | Max $V_y$ | -1.19 | 1.11 | -2.40 | 0.00 | -10.77 | 3.99 | BC 26 |
| | | | | Min $V_y$ | -5.57 | -0.96 | -1.10 | 0.00 | 3.16 | -3.24 | BC 33 |
| | | | | Max $V_z$ | -15.26 | 0.92 | 3.35 | 0.00 | 11.76 | 3.29 | BC 25 |
| | | | | Min $V_z$ | 1.43 | 1.11 | -2.50 | 0.00 | -11.02 | 3.99 | BC 36 |
| | | | | Max $M_T$ | -9.30 | 0.00 | 0.35 | 0.00 | 0.88 | -0.00 | BC 1 |
| | | | | Min $M_T$ | -9.30 | 0.00 | 0.35 | 0.00 | 0.88 | -0.00 | BC 1 |
| | | | | Max $M_y$ | -15.26 | 0.92 | 3.35 | 0.00 | 11.76 | 3.29 | BC 25 |
| | | | | Min $M_y$ | 1.43 | 1.11 | -2.50 | 0.00 | -11.02 | 3.99 | BC 36 |
| | | | | Max $M_z$ | 1.43 | 1.11 | -2.50 | 0.00 | -11.02 | 3.99 | BC 36 |
| | | | | Min $M_z$ | -8.19 | -0.96 | -1.01 | 0.00 | 3.41 | -3.24 | BC 23 |
| | | | 2550 | Max N | 1.43 | 1.11 | -2.50 | 0.00 | -11.02 | 3.99 | BC 44 |
| | | | Rechts | Min N | -16.32 | 0.00 | 0.86 | 0.00 | 2.18 | -0.00 | BC 12 |
| | | | | Max $V_y$ | -1.19 | 1.11 | -2.40 | 0.00 | -10.77 | 3.99 | BC 26 |
| | | | | Min $V_y$ | -5.57 | -0.96 | -1.10 | 0.00 | 3.16 | -3.24 | BC 33 |
| | | | | Max $V_z$ | -15.26 | 0.92 | 3.35 | 0.00 | 11.76 | 3.29 | BC 25 |
| | | | | Min $V_z$ | 1.43 | 1.11 | -2.50 | 0.00 | -11.02 | 3.99 | BC 36 |
| | | | | Max $M_T$ | -9.30 | 0.00 | 0.35 | 0.00 | 0.88 | -0.00 | BC 1 |
| | | | | Min $M_T$ | -9.30 | 0.00 | 0.35 | 0.00 | 0.88 | -0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ | $V_z$ | Momenten [kNm] $M_T$ | $M_y$ | $M_z$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 4 | RC1 | | | Max $M_y$ | -15.26 | 0.92 | 3.35 | 0.00 | 11.76 | 3.29 | BC 25 |
| | | | | Min $M_y$ | 1.43 | 1.11 | -2.50 | 0.00 | -11.02 | 3.99 | BC 36 |
| | | | | Max $M_z$ | 1.43 | 1.11 | -2.50 | 0.00 | -11.02 | 3.99 | BC 36 |
| | | | | Min $M_z$ | -8.19 | -0.96 | -1.01 | 0.00 | 3.41 | -3.24 | BC 23 |
| | | | 4050 | Max N | 3.36 | 4.49 | -0.20 | 0.00 | -13.04 | -0.21 | BC 44 |
| | | | Links | Min N | -13.49 | 0.00 | 0.86 | 0.00 | 3.47 | -0.00 | BC 12 |
| | | | | Max $V_y$ | 1.64 | 4.49 | -0.10 | 0.00 | -12.64 | -0.21 | BC 26 |
| | | | | Min $V_y$ | -3.64 | -3.58 | -3.87 | 0.00 | -0.57 | 0.17 | BC 33 |
| | | | | Max $V_z$ | -12.43 | 3.70 | 1.75 | 0.00 | 15.58 | -0.17 | BC 25 |
| | | | | Min $V_z$ | -3.64 | -3.58 | -3.87 | 0.00 | -0.57 | 0.17 | BC 33 |
| | | | | Max $M_T$ | -6.10 | 0.00 | 0.35 | 0.00 | 1.40 | -0.00 | BC 1 |
| | | | | Min $M_T$ | -6.10 | 0.00 | 0.35 | 0.00 | 1.40 | -0.00 | BC 1 |
| | | | | Max $M_y$ | -12.43 | 3.70 | 1.75 | 0.00 | 15.58 | -0.17 | BC 25 |
| | | | | Min $M_y$ | 3.36 | 4.49 | -0.20 | 0.00 | -13.05 | -0.21 | BC 36 |
| | | | | Max $M_z$ | -3.64 | -3.58 | -3.87 | 0.00 | -0.57 | 0.17 | BC 33 |
| | | | | Min $M_z$ | 1.64 | 4.49 | -0.10 | 0.00 | -12.64 | -0.21 | BC 26 |
| | | 12 | 4050 | Max N | 3.36 | 4.49 | -0.20 | 0.00 | -13.04 | -0.21 | BC 44 |
| | | | Rechts | Min N | -13.49 | 0.00 | 0.86 | 0.00 | 3.47 | -0.00 | BC 12 |
| | | | | Max $V_y$ | 1.64 | 4.49 | -0.10 | 0.00 | -12.64 | -0.21 | BC 26 |
| | | | | Min $V_y$ | -3.64 | -3.59 | -3.87 | 0.00 | -0.57 | 0.17 | BC 33 |
| | | | | Max $V_z$ | -12.43 | 3.70 | 1.75 | 0.00 | 15.58 | -0.17 | BC 25 |
| | | | | Min $V_z$ | -3.64 | -3.59 | -3.87 | 0.00 | -0.57 | 0.17 | BC 33 |
| | | | | Max $M_T$ | -6.10 | 0.00 | 0.35 | 0.00 | 1.40 | -0.00 | BC 1 |
| | | | | Min $M_T$ | -6.10 | 0.00 | 0.35 | 0.00 | 1.40 | -0.00 | BC 1 |
| | | | | Max $M_y$ | -12.43 | 3.70 | 1.75 | 0.00 | 15.58 | -0.17 | BC 25 |
| | | | | Min $M_y$ | 3.36 | 4.49 | -0.20 | 0.00 | -13.05 | -0.21 | BC 36 |
| | | | | Max $M_z$ | -3.64 | -3.59 | -3.87 | 0.00 | -0.57 | 0.17 | BC 33 |
| | | | | Min $M_z$ | 1.64 | 4.49 | -0.10 | 0.00 | -12.64 | -0.21 | BC 26 |
| 5 | RC1 | 13 | 0 | Max N | -2.68 | -0.00 | -8.59 | 0.00 | -0.00 | 0.00 | BC 44 |
| | | | Links | Min N | -29.86 | -0.00 | 1.68 | 0.00 | 0.00 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -16.01 | 0.07 | 5.30 | 0.00 | 0.00 | -0.00 | BC 33 |
| | | | | Min $V_y$ | -13.60 | -0.00 | 5.49 | 0.00 | 0.00 | 0.00 | BC 24 |
| | | | | Max $V_z$ | -20.34 | -0.00 | 8.01 | 0.00 | 0.00 | 0.00 | BC 25 |
| | | | | Min $V_z$ | -2.68 | -0.00 | -8.60 | 0.00 | -0.00 | 0.00 | BC 36 |
| | | | | Max $M_T$ | -15.46 | -0.00 | 0.65 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -15.46 | -0.00 | 0.65 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -13.60 | -0.00 | 5.49 | 0.00 | 0.00 | 0.00 | BC 24 |
| | | | | Min $M_y$ | -7.03 | -0.00 | -8.41 | 0.00 | -0.00 | 0.00 | BC 26 |
| | | | | Max $M_z$ | -15.46 | -0.00 | 0.65 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -20.36 | 0.07 | 5.48 | 0.00 | 0.00 | -0.00 | BC 15 |
| | | | 0 | Max N | -2.68 | -0.00 | -8.59 | 0.00 | -0.00 | 0.00 | BC 44 |
| | | | Rechts | Min N | -29.86 | -0.00 | 1.68 | 0.00 | 0.00 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -16.01 | 0.07 | 5.30 | 0.00 | 0.00 | -0.00 | BC 33 |
| | | | | Min $V_y$ | -13.60 | -0.00 | 5.49 | 0.00 | 0.00 | 0.00 | BC 24 |
| | | | | Max $V_z$ | -20.34 | -0.00 | 8.01 | 0.00 | 0.00 | 0.00 | BC 25 |
| | | | | Min $V_z$ | -2.68 | -0.00 | -8.60 | 0.00 | -0.00 | 0.00 | BC 36 |
| | | | | Max $M_T$ | -15.46 | -0.00 | 0.65 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -15.46 | -0.00 | 0.65 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -20.34 | -0.00 | 8.01 | 0.00 | 0.00 | 0.00 | BC 25 |
| | | | | Min $M_y$ | -2.68 | -0.00 | -8.59 | 0.00 | -0.00 | 0.00 | BC 44 |
| | | | | Max $M_z$ | -13.61 | -0.00 | 5.48 | 0.00 | 0.00 | 0.00 | BC 16 |
| | | | | Min $M_z$ | -20.36 | 0.07 | 5.48 | 0.00 | 0.00 | -0.00 | BC 15 |
| | | | 50 | Max N | -2.66 | -0.00 | -8.45 | 0.00 | -0.43 | 0.00 | BC 44 |
| | | | Links | Min N | -29.84 | -0.00 | 1.68 | 0.00 | 0.08 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -15.99 | 0.07 | 5.17 | 0.00 | 0.26 | -0.00 | BC 33 |
| | | | | Min $V_y$ | -13.58 | -0.00 | 5.35 | 0.00 | 0.27 | 0.00 | BC 24 |
| | | | | Max $V_z$ | -20.32 | -0.00 | 7.91 | 0.00 | 0.40 | 0.00 | BC 25 |
| | | | | Min $V_z$ | -2.66 | -0.00 | -8.45 | 0.00 | -0.43 | 0.00 | BC 36 |
| | | | | Max $M_T$ | -15.44 | -0.00 | 0.65 | 0.00 | 0.03 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -15.44 | -0.00 | 0.65 | 0.00 | 0.03 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -20.32 | -0.00 | 7.91 | 0.00 | 0.40 | 0.00 | BC 25 |
| | | | | Min $M_y$ | -2.66 | -0.00 | -8.45 | 0.00 | -0.43 | 0.00 | BC 36 |
| | | | | Max $M_z$ | -13.58 | -0.00 | 5.35 | 0.00 | 0.27 | 0.00 | BC 24 |
| | | | | Min $M_z$ | -15.99 | 0.07 | 5.17 | 0.00 | 0.26 | -0.00 | BC 33 |
| | | | 50 | Max N | -2.66 | -0.00 | -8.45 | 0.00 | -0.43 | 0.00 | BC 44 |
| | | | Rechts | Min N | -29.84 | -0.00 | 1.68 | 0.00 | 0.08 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -15.99 | 0.07 | 5.17 | 0.00 | 0.26 | -0.00 | BC 33 |
| | | | | Min $V_y$ | -13.58 | -0.00 | 5.35 | 0.00 | 0.27 | 0.00 | BC 24 |
| | | | | Max $V_z$ | -20.32 | -0.00 | 7.91 | 0.00 | 0.40 | 0.00 | BC 25 |
| | | | | Min $V_z$ | -2.66 | -0.00 | -8.45 | 0.00 | -0.43 | 0.00 | BC 36 |
| | | | | Max $M_T$ | -15.44 | -0.00 | 0.65 | 0.00 | 0.03 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -15.44 | -0.00 | 0.65 | 0.00 | 0.03 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -20.32 | -0.00 | 7.91 | 0.00 | 0.40 | 0.00 | BC 25 |
| | | | | Min $M_y$ | -2.66 | -0.00 | -8.45 | 0.00 | -0.43 | 0.00 | BC 36 |
| | | | | Max $M_z$ | -13.58 | -0.00 | 5.35 | 0.00 | 0.27 | 0.00 | BC 24 |
| | | | | Min $M_z$ | -15.99 | 0.07 | 5.17 | 0.00 | 0.26 | -0.00 | BC 33 |
| | | | 2500 | Max N | -1.99 | -0.00 | -1.47 | 0.00 | -12.58 | 0.00 | BC 44 |
| | | | Links | Min N | -28.85 | -0.00 | 1.68 | 0.00 | 4.19 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -15.32 | 0.07 | -1.39 | 0.00 | 4.90 | -0.17 | BC 33 |
| | | | | Min $V_y$ | -12.59 | -0.00 | -1.20 | 0.00 | 5.36 | 0.00 | BC 24 |
| | | | | Max $V_z$ | -19.32 | -0.00 | 3.05 | 0.00 | 13.83 | 0.00 | BC 25 |
| | | | | Min $V_z$ | -1.99 | -0.00 | -1.47 | 0.00 | -12.58 | 0.00 | BC 36 |
| | | | | Max $M_T$ | -14.32 | -0.00 | 0.65 | 0.00 | 1.62 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -14.32 | -0.00 | 0.65 | 0.00 | 1.62 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -19.32 | -0.00 | 3.05 | 0.00 | 13.83 | 0.00 | BC 25 |
| | | | | Min $M_y$ | -1.99 | -0.00 | -1.47 | 0.00 | -12.58 | 0.00 | BC 36 |
| | | | | Max $M_z$ | -12.59 | -0.00 | -1.20 | 0.00 | 5.36 | 0.00 | BC 24 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ | $V_z$ | Momenten [kNm] $M_T$ | $M_y$ | $M_z$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 5 | RC1 | | | Min $M_z$ | -15.32 | 0.07 | -1.39 | 0.00 | 4.90 | -0.17 | BC 33 |
| | | | 2500 | Max N | -1.99 | -0.00 | -1.47 | 0.00 | -12.58 | 0.00 | BC 44 |
| | | | Rechts | Min N | -28.85 | -0.00 | 1.68 | 0.00 | 4.19 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -15.32 | 0.07 | -1.39 | 0.00 | 4.90 | -0.17 | BC 33 |
| | | | | Min $V_y$ | -12.59 | -0.00 | -1.20 | 0.00 | 5.36 | 0.00 | BC 24 |
| | | | | Max $V_z$ | -19.32 | -0.00 | 3.05 | 0.00 | 13.83 | 0.00 | BC 25 |
| | | | | Min $V_z$ | -1.99 | -0.00 | -1.47 | 0.00 | -12.58 | 0.00 | BC 36 |
| | | | | Max $M_T$ | -14.32 | -0.00 | 0.65 | 0.00 | 1.62 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -14.32 | -0.00 | 0.65 | 0.00 | 1.62 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -19.32 | -0.00 | 3.05 | 0.00 | 13.83 | 0.00 | BC 25 |
| | | | | Min $M_y$ | -1.99 | -0.00 | -1.47 | 0.00 | -12.58 | 0.00 | BC 36 |
| | | | | Max $M_z$ | -12.59 | -0.00 | -1.20 | 0.00 | 5.36 | 0.00 | BC 24 |
| | | | | Min $M_z$ | -15.32 | 0.07 | -1.39 | 0.00 | 4.90 | -0.17 | BC 33 |
| | | | 4050 | Max N | -0.09 | -0.00 | 3.28 | 0.00 | -11.17 | 0.00 | BC 44 |
| | | | Links | Min N | -26.07 | -0.00 | 1.68 | 0.00 | 6.79 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -13.42 | 0.07 | -5.54 | 0.00 | -0.47 | -0.28 | BC 33 |
| | | | | Min $V_y$ | -9.81 | -0.00 | -5.36 | 0.00 | 0.28 | 0.00 | BC 24 |
| | | | | Max $V_z$ | -3.24 | -0.00 | 3.46 | 0.00 | -10.44 | 0.00 | BC 26 |
| | | | | Min $V_z$ | -6.66 | -0.00 | -5.54 | 0.00 | -0.47 | 0.00 | BC 34 |
| | | | | Max $M_T$ | -11.19 | -0.00 | 0.65 | 0.00 | 2.63 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -11.19 | -0.00 | 0.65 | 0.00 | 2.63 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -16.55 | -0.00 | -0.25 | 0.00 | 16.01 | 0.00 | BC 25 |
| | | | | Min $M_y$ | -0.09 | -0.00 | 3.28 | 0.00 | -11.18 | 0.00 | BC 36 |
| | | | | Max $M_z$ | -9.81 | -0.00 | -5.36 | 0.00 | 0.28 | 0.00 | BC 24 |
| | | | | Min $M_z$ | -13.42 | 0.07 | -5.54 | 0.00 | -0.47 | -0.28 | BC 33 |
| | | 14 | 4050 | Max N | -0.09 | -0.00 | 3.28 | 0.00 | -11.17 | 0.00 | BC 44 |
| | | | Rechts | Min N | -26.07 | -0.00 | 1.68 | 0.00 | 6.79 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -13.42 | 0.07 | -5.54 | 0.00 | -0.47 | -0.28 | BC 33 |
| | | | | Min $V_y$ | -9.81 | -0.00 | -5.36 | 0.00 | 0.28 | 0.00 | BC 24 |
| | | | | Max $V_z$ | -3.24 | -0.00 | 3.46 | 0.00 | -10.44 | 0.00 | BC 26 |
| | | | | Min $V_z$ | -6.66 | -0.00 | -5.54 | 0.00 | -0.47 | 0.00 | BC 34 |
| | | | | Max $M_T$ | -11.19 | -0.00 | 0.65 | 0.00 | 2.63 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -11.19 | -0.00 | 0.65 | 0.00 | 2.63 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -16.55 | -0.00 | -0.25 | 0.00 | 16.01 | 0.00 | BC 25 |
| | | | | Min $M_y$ | -0.09 | -0.00 | 3.28 | 0.00 | -11.18 | 0.00 | BC 36 |
| | | | | Max $M_z$ | -9.81 | -0.00 | -5.36 | 0.00 | 0.28 | 0.00 | BC 24 |
| | | | | Min $M_z$ | -13.42 | 0.07 | -5.54 | 0.00 | -0.47 | -0.28 | BC 33 |
| 6 | RC1 | 15 | 0 | Max N | 0.73 | 4.24 | -6.14 | 0.00 | -0.00 | -0.00 | BC 44 |
| | | | Links | Min N | -17.34 | -0.00 | 0.86 | 0.00 | 0.00 | 0.00 | BC 12 |
| | | | | Max $V_y$ | 0.73 | 4.24 | -6.14 | 0.00 | -0.00 | -0.00 | BC 36 |
| | | | | Min $V_y$ | -6.31 | -3.48 | 3.58 | 0.00 | 0.00 | 0.00 | BC 34 |
| | | | | Max $V_z$ | -16.29 | 3.49 | 5.88 | 0.00 | -0.00 | 0.00 | BC 25 |
| | | | | Min $V_z$ | 0.73 | 4.24 | -6.14 | 0.00 | -0.00 | -0.00 | BC 36 |
| | | | | Max $M_T$ | -10.45 | -0.00 | 0.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -10.45 | -0.00 | 0.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -10.45 | -0.00 | 0.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -16.29 | 3.49 | 5.88 | 0.00 | -0.00 | 0.00 | BC 17 |
| | | | | Max $M_z$ | -16.29 | 3.49 | 5.88 | 0.00 | -0.00 | 0.00 | BC 17 |
| | | | | Min $M_z$ | -2.21 | 4.24 | -6.04 | 0.00 | -0.00 | -0.00 | BC 18 |
| | | | 0 | Max N | 0.73 | 4.24 | -6.14 | 0.00 | -0.00 | -0.00 | BC 44 |
| | | | Rechts | Min N | -17.34 | -0.00 | 0.86 | 0.00 | 0.00 | 0.00 | BC 12 |
| | | | | Max $V_y$ | 0.73 | 4.24 | -6.14 | 0.00 | -0.00 | -0.00 | BC 36 |
| | | | | Min $V_y$ | -6.31 | -3.48 | 3.58 | 0.00 | 0.00 | 0.00 | BC 34 |
| | | | | Max $V_z$ | -16.29 | 3.49 | 5.88 | 0.00 | 0.00 | -0.00 | BC 25 |
| | | | | Min $V_z$ | 0.73 | 4.24 | -6.14 | 0.00 | -0.00 | -0.00 | BC 36 |
| | | | | Max $M_T$ | -10.45 | -0.00 | 0.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -10.45 | -0.00 | 0.35 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -16.29 | 3.49 | 5.88 | 0.00 | 0.00 | -0.00 | BC 25 |
| | | | | Min $M_y$ | 0.73 | 4.24 | -6.14 | 0.00 | -0.00 | -0.00 | BC 36 |
| | | | | Max $M_z$ | -9.25 | -3.48 | 3.68 | 0.00 | 0.00 | 0.00 | BC 16 |
| | | | | Min $M_z$ | -2.21 | 4.24 | -6.04 | 0.00 | -0.00 | -0.00 | BC 18 |
| | | | 50 | Max N | 0.75 | 4.14 | -6.07 | 0.00 | -0.31 | -0.21 | BC 44 |
| | | | Links | Min N | -17.32 | -0.00 | 0.86 | 0.00 | 0.04 | 0.00 | BC 12 |
| | | | | Max $V_y$ | 0.75 | 4.14 | -6.07 | 0.00 | -0.31 | -0.21 | BC 44 |
| | | | | Min $V_y$ | -6.30 | -3.41 | 3.49 | 0.00 | 0.18 | 0.17 | BC 34 |
| | | | | Max $V_z$ | -16.27 | 3.41 | 5.83 | 0.00 | 0.29 | -0.17 | BC 25 |
| | | | | Min $V_z$ | 0.75 | 4.14 | -6.07 | 0.00 | -0.31 | -0.21 | BC 36 |
| | | | | Max $M_T$ | -10.42 | -0.00 | 0.35 | 0.00 | 0.02 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -10.42 | -0.00 | 0.35 | 0.00 | 0.02 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -16.27 | 3.41 | 5.83 | 0.00 | 0.29 | -0.17 | BC 25 |
| | | | | Min $M_y$ | 0.75 | 4.14 | -6.07 | 0.00 | -0.31 | -0.21 | BC 36 |
| | | | | Max $M_z$ | -6.30 | -3.41 | 3.49 | 0.00 | 0.18 | 0.17 | BC 34 |
| | | | | Min $M_z$ | 0.75 | 4.14 | -6.07 | 0.00 | -0.31 | -0.21 | BC 36 |
| | | | 50 | Max N | 0.75 | 4.14 | -6.07 | 0.00 | -0.31 | -0.21 | BC 44 |
| | | | Rechts | Min N | -17.32 | -0.00 | 0.86 | 0.00 | 0.04 | 0.00 | BC 12 |
| | | | | Max $V_y$ | 0.75 | 4.14 | -6.07 | 0.00 | -0.31 | -0.21 | BC 44 |
| | | | | Min $V_y$ | -6.30 | -3.41 | 3.49 | 0.00 | 0.18 | 0.17 | BC 34 |
| | | | | Max $V_z$ | -16.27 | 3.41 | 5.83 | 0.00 | 0.29 | -0.17 | BC 25 |
| | | | | Min $V_z$ | 0.75 | 4.14 | -6.07 | 0.00 | -0.31 | -0.21 | BC 36 |
| | | | | Max $M_T$ | -10.42 | -0.00 | 0.35 | 0.00 | 0.02 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -10.42 | -0.00 | 0.35 | 0.00 | 0.02 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -16.27 | 3.41 | 5.83 | 0.00 | 0.29 | -0.17 | BC 25 |
| | | | | Min $M_y$ | 0.75 | 4.14 | -6.07 | 0.00 | -0.31 | -0.21 | BC 36 |
| | | | | Max $M_z$ | -6.30 | -3.41 | 3.49 | 0.00 | 0.18 | 0.17 | BC 34 |
| | | | | Min $M_z$ | 0.75 | 4.14 | -6.07 | 0.00 | -0.31 | -0.21 | BC 44 |
| | | | 2500 | Max N | 1.42 | -1.01 | -2.58 | 0.00 | -10.89 | -4.04 | BC 44 |
| | | | Links | Min N | -16.33 | -0.00 | 0.86 | 0.00 | 2.14 | 0.00 | BC 12 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ | $V_z$ | Momenten [kNm] $M_T$ | $M_y$ | $M_z$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 6 | RC1 | | | Max $V_y$ | -5.62 | 0.87 | -1.01 | 0.00 | 3.22 | 3.28 | BC 42 |
| | | | | Min $V_y$ | -1.20 | -1.01 | -2.48 | 0.00 | -10.65 | -4.04 | BC 18 |
| | | | | Max $V_z$ | -15.28 | -0.83 | 3.40 | 0.00 | 11.60 | -3.33 | BC 25 |
| | | | | Min $V_z$ | 1.42 | -1.01 | -2.58 | 0.00 | -10.90 | -4.04 | BC 36 |
| | | | | Max $M_T$ | -9.30 | -0.00 | 0.35 | 0.00 | 0.86 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -9.30 | -0.00 | 0.35 | 0.00 | 0.86 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -15.28 | -0.83 | 3.40 | 0.00 | 11.60 | -3.33 | BC 25 |
| | | | | Min $M_y$ | 1.42 | -1.01 | -2.58 | 0.00 | -10.90 | -4.04 | BC 36 |
| | | | | Max $M_z$ | -5.62 | 0.87 | -1.01 | 0.00 | 3.21 | 3.28 | BC 34 |
| | | | | Min $M_z$ | 1.42 | -1.01 | -2.58 | 0.00 | -10.89 | -4.04 | BC 44 |
| | | | 2500 | Max N | 1.42 | -1.01 | -2.58 | 0.00 | -10.89 | -4.04 | BC 44 |
| | | | Rechts | Min N | -16.33 | -0.00 | 0.86 | 0.00 | 2.14 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -5.62 | 0.87 | -1.01 | 0.00 | 3.22 | 3.28 | BC 42 |
| | | | | Min $V_y$ | -1.20 | -1.01 | -2.48 | 0.00 | -10.65 | -4.04 | BC 18 |
| | | | | Max $V_z$ | -15.28 | -0.83 | 3.40 | 0.00 | 11.60 | -3.33 | BC 25 |
| | | | | Min $V_z$ | 1.42 | -1.01 | -2.58 | 0.00 | -10.90 | -4.04 | BC 36 |
| | | | | Max $M_T$ | -9.30 | -0.00 | 0.35 | 0.00 | 0.86 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -9.30 | -0.00 | 0.35 | 0.00 | 0.86 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -15.28 | -0.83 | 3.40 | 0.00 | 11.60 | -3.33 | BC 25 |
| | | | | Min $M_y$ | 1.42 | -1.01 | -2.58 | 0.00 | -10.90 | -4.04 | BC 36 |
| | | | | Max $M_z$ | -5.62 | 0.87 | -1.01 | 0.00 | 3.21 | 3.28 | BC 34 |
| | | | | Min $M_z$ | 1.42 | -1.01 | -2.58 | 0.00 | -10.89 | -4.04 | BC 44 |
| | | | 2550 | Max N | 1.49 | -1.11 | -2.50 | 0.00 | -11.02 | -3.99 | BC 44 |
| | | | Links | Min N | -16.23 | -0.00 | 0.86 | 0.00 | 2.18 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -5.55 | 0.96 | -1.10 | 0.00 | 3.16 | 3.24 | BC 42 |
| | | | | Min $V_y$ | -1.11 | -1.11 | -2.40 | 0.00 | -10.78 | -3.99 | BC 18 |
| | | | | Max $V_z$ | -15.19 | -0.91 | 3.35 | 0.00 | 11.77 | -3.29 | BC 25 |
| | | | | Min $V_z$ | 1.49 | -1.11 | -2.50 | 0.00 | -11.03 | -3.99 | BC 36 |
| | | | | Max $M_T$ | -9.20 | -0.00 | 0.35 | 0.00 | 0.88 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -9.20 | -0.00 | 0.35 | 0.00 | 0.88 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -15.19 | -0.91 | 3.35 | 0.00 | 11.77 | -3.29 | BC 25 |
| | | | | Min $M_y$ | 1.49 | -1.11 | -2.50 | 0.00 | -11.03 | -3.99 | BC 36 |
| | | | | Max $M_z$ | -5.55 | 0.96 | -1.10 | 0.00 | 3.16 | 3.24 | BC 34 |
| | | | | Min $M_z$ | 1.49 | -1.11 | -2.50 | 0.00 | -11.02 | -3.99 | BC 44 |
| | | | 2550 | Max N | 1.49 | -1.11 | -2.50 | 0.00 | -11.02 | -3.99 | BC 44 |
| | | | Rechts | Min N | -16.23 | -0.00 | 0.86 | 0.00 | 2.18 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -5.55 | 0.96 | -1.10 | 0.00 | 3.16 | 3.24 | BC 42 |
| | | | | Min $V_y$ | -1.11 | -1.11 | -2.40 | 0.00 | -10.78 | -3.99 | BC 18 |
| | | | | Max $V_z$ | -15.19 | -0.91 | 3.35 | 0.00 | 11.77 | -3.29 | BC 25 |
| | | | | Min $V_z$ | 1.49 | -1.11 | -2.50 | 0.00 | -11.03 | -3.99 | BC 36 |
| | | | | Max $M_T$ | -9.20 | -0.00 | 0.35 | 0.00 | 0.88 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -9.20 | -0.00 | 0.35 | 0.00 | 0.88 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -15.19 | -0.91 | 3.35 | 0.00 | 11.77 | -3.29 | BC 25 |
| | | | | Min $M_y$ | 1.49 | -1.11 | -2.50 | 0.00 | -11.03 | -3.99 | BC 36 |
| | | | | Max $M_z$ | -5.55 | 0.96 | -1.10 | 0.00 | 3.16 | 3.24 | BC 34 |
| | | | | Min $M_z$ | 1.49 | -1.11 | -2.50 | 0.00 | -11.02 | -3.99 | BC 44 |
| | | | 4050 | Max N | 3.42 | -4.49 | -0.20 | 0.00 | -13.05 | 0.21 | BC 44 |
| | | | Links | Min N | -13.40 | -0.00 | 0.86 | 0.00 | 3.47 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -3.62 | 3.59 | -3.87 | 0.00 | -0.57 | -0.17 | BC 34 |
| | | | | Min $V_y$ | 3.42 | -4.49 | -0.20 | 0.00 | -13.06 | 0.21 | BC 36 |
| | | | | Max $V_z$ | -12.35 | -3.70 | 1.75 | 0.00 | 15.59 | 0.17 | BC 25 |
| | | | | Min $V_z$ | -3.62 | 3.59 | -3.87 | 0.00 | -0.57 | -0.17 | BC 34 |
| | | | | Max $M_T$ | -6.00 | -0.00 | 0.35 | 0.00 | 1.40 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -6.00 | -0.00 | 0.35 | 0.00 | 1.40 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -12.35 | -3.70 | 1.75 | 0.00 | 15.59 | 0.17 | BC 25 |
| | | | | Min $M_y$ | 3.42 | -4.49 | -0.20 | 0.00 | -13.06 | 0.21 | BC 36 |
| | | | | Max $M_z$ | 1.73 | -4.49 | -0.11 | 0.00 | -12.66 | 0.21 | BC 18 |
| | | | | Min $M_z$ | -3.62 | 3.59 | -3.87 | 0.00 | -0.56 | -0.17 | BC 42 |
| | | 16 | 4050 | Max N | 3.42 | -4.49 | -0.20 | 0.00 | -13.05 | 0.21 | BC 44 |
| | | | Rechts | Min N | -13.40 | -0.00 | 0.86 | 0.00 | 3.47 | 0.00 | BC 12 |
| | | | | Max $V_y$ | -3.62 | 3.59 | -3.87 | 0.00 | -0.57 | -0.17 | BC 34 |
| | | | | Min $V_y$ | 3.42 | -4.49 | -0.20 | 0.00 | -13.06 | 0.21 | BC 36 |
| | | | | Max $V_z$ | -12.35 | -3.70 | 1.75 | 0.00 | 15.59 | 0.17 | BC 25 |
| | | | | Min $V_z$ | -3.62 | 3.59 | -3.87 | 0.00 | -0.57 | -0.17 | BC 34 |
| | | | | Max $M_T$ | -6.00 | -0.00 | 0.35 | 0.00 | 1.40 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -6.00 | -0.00 | 0.35 | 0.00 | 1.40 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -12.35 | -3.70 | 1.75 | 0.00 | 15.59 | 0.17 | BC 25 |
| | | | | Min $M_y$ | 3.42 | -4.49 | -0.20 | 0.00 | -13.06 | 0.21 | BC 36 |
| | | | | Max $M_z$ | 1.73 | -4.49 | -0.11 | 0.00 | -12.66 | 0.21 | BC 18 |
| | | | | Min $M_z$ | -3.62 | 3.59 | -3.87 | 0.00 | -0.56 | -0.17 | BC 42 |
| 7 | RC1 | 6 | 0 | Max N | 3.88 | 0.00 | 3.23 | 0.00 | 0.11 | 0.00 | BC 33 |
| | | | | Min N | -1.71 | 0.00 | -2.30 | -0.00 | 12.77 | 0.00 | BC 25 |
| | | | | Max $V_y$ | -0.34 | 0.00 | 5.35 | 0.00 | -1.36 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.34 | 0.00 | 5.35 | 0.00 | -1.36 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.83 | 0.00 | 12.82 | 0.00 | -3.37 | 0.00 | BC 12 |
| | | | | Min $V_z$ | -1.62 | 0.00 | -3.81 | -0.00 | 13.16 | 0.00 | BC 43 |
| | | | | Max $M_T$ | -1.62 | 0.00 | 10.27 | 0.00 | -14.99 | 0.00 | BC 36 |
| | | | | Min $M_T$ | -1.62 | 0.00 | -3.81 | -0.00 | 13.16 | 0.00 | BC 35 |
| | | | | Max $M_y$ | -1.62 | 0.00 | -3.81 | -0.00 | 13.16 | 0.00 | BC 35 |
| | | | | Min $M_y$ | -1.71 | 0.00 | 11.77 | 0.00 | -15.38 | 0.00 | BC 26 |
| | | | | Max $M_z$ | -0.34 | 0.00 | 5.35 | 0.00 | -1.36 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.34 | 0.00 | 5.35 | 0.00 | -1.36 | 0.00 | BC 1 |
| | | 12 | 4000 | Max N | 3.88 | 0.00 | -3.23 | 0.00 | 0.11 | 0.00 | BC 33 |
| | | | | Min N | -1.71 | 0.00 | -11.77 | -0.00 | -15.38 | 0.00 | BC 25 |
| | | | | Max $V_y$ | -0.34 | 0.00 | -5.35 | 0.00 | -1.36 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.34 | 0.00 | -5.35 | 0.00 | -1.36 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -1.62 | 0.00 | 3.81 | 0.00 | 13.16 | 0.00 | BC 44 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ | $V_z$ | Momenten [kNm] $M_T$ | $M_y$ | $M_z$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 7 | RC1 | | | Min $V_z$ | -0.83 | 0.00 | -12.82 | 0.00 | -3.37 | 0.00 | BC 12 |
| | | | | Max $M_T$ | -1.62 | 0.00 | 3.81 | 0.00 | 13.16 | 0.00 | BC 36 |
| | | | | Min $M_T$ | -1.62 | 0.00 | -10.27 | -0.00 | -14.99 | 0.00 | BC 35 |
| | | | | Max $M_y$ | -1.62 | 0.00 | 3.81 | 0.00 | 13.16 | 0.00 | BC 36 |
| | | | | Min $M_y$ | -1.71 | 0.00 | -11.77 | -0.00 | -15.38 | 0.00 | BC 25 |
| | | | | Max $M_z$ | -0.34 | 0.00 | -5.35 | 0.00 | -1.36 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.34 | 0.00 | -5.35 | 0.00 | -1.36 | 0.00 | BC 1 |
| 8 | RC1 | 8 | 0 | Max N | 5.58 | 0.00 | 5.91 | 0.00 | -0.19 | 0.00 | BC 34 |
| | | | | Min N | -3.38 | 0.00 | 2.01 | -0.00 | 10.84 | 0.00 | BC 25 |
| | | | | Max $V_y$ | -0.63 | 0.00 | 9.78 | 0.00 | -2.55 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.63 | 0.00 | 9.78 | 0.00 | -2.55 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -1.63 | 0.00 | 24.83 | 0.00 | -6.60 | 0.00 | BC 12 |
| | | | | Min $V_z$ | -3.21 | 0.00 | -0.74 | -0.00 | 11.57 | 0.00 | BC 39 |
| | | | | Max $M_T$ | -3.21 | 0.00 | 12.56 | 0.00 | -15.02 | 0.00 | BC 36 |
| | | | | Min $M_T$ | -3.38 | 0.00 | 2.01 | -0.00 | 10.84 | 0.00 | BC 25 |
| | | | | Max $M_y$ | -3.21 | 0.00 | -0.74 | -0.00 | 11.57 | 0.00 | BC 35 |
| | | | | Min $M_y$ | -3.38 | 0.00 | 15.32 | 0.00 | -15.76 | 0.00 | BC 26 |
| | | | | Max $M_z$ | -0.63 | 0.00 | 9.78 | 0.00 | -2.55 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.63 | 0.00 | 9.78 | 0.00 | -2.55 | 0.00 | BC 1 |
| | | 14 | 4000 | Max N | 5.58 | 0.00 | -5.91 | 0.00 | -0.19 | 0.00 | BC 34 |
| | | | | Min N | -3.38 | 0.00 | -15.32 | -0.00 | -15.76 | 0.00 | BC 25 |
| | | | | Max $V_y$ | -0.63 | 0.00 | -9.78 | 0.00 | -2.55 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.63 | 0.00 | -9.78 | 0.00 | -2.55 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -3.21 | 0.00 | 0.74 | 0.00 | 11.57 | 0.00 | BC 36 |
| | | | | Min $V_z$ | -1.63 | 0.00 | -24.83 | 0.00 | -6.60 | 0.00 | BC 12 |
| | | | | Max $M_T$ | -3.21 | 0.00 | 0.74 | 0.00 | 11.57 | 0.00 | BC 36 |
| | | | | Min $M_T$ | -3.38 | 0.00 | -15.32 | -0.00 | -15.76 | 0.00 | BC 25 |
| | | | | Max $M_y$ | -3.21 | 0.00 | 0.74 | 0.00 | 11.57 | 0.00 | BC 36 |
| | | | | Min $M_y$ | -3.38 | 0.00 | -15.32 | -0.00 | -15.76 | 0.00 | BC 25 |
| | | | | Max $M_z$ | -0.63 | 0.00 | -9.78 | 0.00 | -2.55 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.63 | 0.00 | -9.78 | 0.00 | -2.55 | 0.00 | BC 1 |
| 9 | RC1 | 10 | 0 | Max N | 3.88 | 0.00 | 3.23 | 0.00 | 0.10 | 0.00 | BC 34 |
| | | | | Min N | -1.71 | 0.00 | -2.30 | 0.00 | 12.78 | 0.00 | BC 25 |
| | | | | Max $V_y$ | -0.34 | 0.00 | 5.35 | 0.00 | -1.36 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.34 | 0.00 | 5.35 | 0.00 | -1.36 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.83 | 0.00 | 12.82 | 0.00 | -3.37 | 0.00 | BC 12 |
| | | | | Min $V_z$ | -1.62 | 0.00 | -3.81 | 0.00 | 13.16 | 0.00 | BC 43 |
| | | | | Max $M_T$ | -1.62 | 0.00 | -3.81 | 0.00 | 13.17 | 0.00 | BC 35 |
| | | | | Min $M_T$ | -1.62 | 0.00 | 10.27 | -0.00 | -15.00 | 0.00 | BC 36 |
| | | | | Max $M_y$ | -1.62 | 0.00 | -3.81 | 0.00 | 13.17 | 0.00 | BC 35 |
| | | | | Min $M_y$ | -1.71 | 0.00 | 11.78 | -0.00 | -15.38 | 0.00 | BC 26 |
| | | | | Max $M_z$ | -0.34 | 0.00 | 5.35 | 0.00 | -1.36 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.34 | 0.00 | 5.35 | 0.00 | -1.36 | 0.00 | BC 1 |
| | | 16 | 4000 | Max N | 3.88 | 0.00 | -3.23 | 0.00 | 0.10 | 0.00 | BC 34 |
| | | | | Min N | -1.71 | 0.00 | -11.78 | 0.00 | -15.38 | 0.00 | BC 25 |
| | | | | Max $V_y$ | -0.34 | 0.00 | -5.35 | 0.00 | -1.36 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.34 | 0.00 | -5.35 | 0.00 | -1.36 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -1.62 | 0.00 | 3.81 | -0.00 | 13.16 | 0.00 | BC 44 |
| | | | | Min $V_z$ | -0.83 | 0.00 | -12.82 | 0.00 | -3.37 | 0.00 | BC 12 |
| | | | | Max $M_T$ | -1.62 | 0.00 | -10.27 | 0.00 | -15.00 | 0.00 | BC 35 |
| | | | | Min $M_T$ | -1.62 | 0.00 | 3.81 | -0.00 | 13.17 | 0.00 | BC 36 |
| | | | | Max $M_y$ | -1.62 | 0.00 | 3.81 | -0.00 | 13.17 | 0.00 | BC 36 |
| | | | | Min $M_y$ | -1.71 | 0.00 | -11.78 | 0.00 | -15.38 | 0.00 | BC 25 |
| | | | | Max $M_z$ | -0.34 | 0.00 | -5.35 | 0.00 | -1.36 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.34 | 0.00 | -5.35 | 0.00 | -1.36 | 0.00 | BC 1 |
| 10 | RC1 | 6 | 0 | Max N | 3.75 | 0.00 | 0.38 | -0.00 | 0.00 | 0.00 | BC 26 |
| | | | | Min N | -3.53 | 0.00 | 0.26 | -0.00 | 0.00 | 0.00 | BC 33 |
| | | | | Max $V_y$ | 0.01 | 0.00 | 0.43 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.01 | 0.00 | 0.43 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.01 | 0.00 | 0.43 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -3.53 | 0.00 | 0.26 | -0.00 | 0.00 | 0.00 | BC 33 |
| | | | | Max $M_T$ | 2.92 | 0.00 | 0.26 | 0.00 | 0.00 | 0.00 | BC 43 |
| | | | | Min $M_T$ | 0.03 | 0.00 | 0.38 | -0.00 | 0.00 | 0.00 | BC 12 |
| | | | | Max $M_y$ | -3.48 | 0.00 | 0.38 | -0.00 | 0.00 | 0.00 | BC 16 |
| | | | | Min $M_y$ | 0.01 | 0.00 | 0.26 | -0.00 | 0.00 | 0.00 | BC 4 |
| | | | | Max $M_z$ | 0.01 | 0.00 | 0.43 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.01 | 0.00 | 0.43 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | 8 | 3500 | Max N | 3.75 | 0.00 | -0.38 | -0.00 | 0.00 | 0.00 | BC 26 |
| | | | | Min N | -3.53 | 0.00 | -0.26 | -0.00 | 0.00 | 0.00 | BC 33 |
| | | | | Max $V_y$ | 0.01 | 0.00 | -0.43 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.01 | 0.00 | -0.43 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -3.53 | 0.00 | -0.26 | -0.00 | 0.00 | 0.00 | BC 33 |
| | | | | Min $V_z$ | 0.01 | 0.00 | -0.43 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 2.92 | 0.00 | -0.26 | 0.00 | 0.00 | 0.00 | BC 43 |
| | | | | Min $M_T$ | 0.03 | 0.00 | -0.38 | -0.00 | 0.00 | 0.00 | BC 12 |
| | | | | Max $M_y$ | -3.48 | 0.00 | -0.38 | -0.00 | 0.00 | 0.00 | BC 16 |
| | | | | Min $M_y$ | 0.01 | 0.00 | -0.26 | -0.00 | 0.00 | 0.00 | BC 4 |
| | | | | Max $M_z$ | 0.01 | 0.00 | -0.43 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.01 | 0.00 | -0.43 | -0.00 | 0.00 | 0.00 | BC 1 |
| 11 | RC1 | 8 | 0 | Max N | 3.74 | 0.00 | 0.38 | 0.00 | 0.00 | 0.00 | BC 18 |
| | | | | Min N | -3.57 | 0.00 | 0.26 | 0.00 | 0.00 | 0.00 | BC 42 |
| | | | | Max $V_y$ | 0.01 | 0.00 | 0.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.01 | 0.00 | 0.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.01 | 0.00 | 0.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -3.57 | 0.00 | 0.26 | 0.00 | 0.00 | 0.00 | BC 34 |
| | | | | Max $M_T$ | 0.02 | 0.00 | 0.38 | 0.00 | 0.00 | 0.00 | BC 12 |
| | | | | Min $M_T$ | 2.90 | 0.00 | 0.26 | -0.00 | 0.00 | 0.00 | BC 43 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ | $V_z$ | Momenten [kNm] $M_T$ | $M_y$ | $M_z$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 11 | RC1 | | | Max $M_y$ | 0.02 | 0.00 | 0.38 | 0.00 | 0.00 | 0.00 | BC 12 |
| | | | | Min $M_y$ | 0.01 | 0.00 | 0.26 | 0.00 | 0.00 | 0.00 | BC 4 |
| | | | | Max $M_z$ | 0.01 | 0.00 | 0.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.01 | 0.00 | 0.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 10 | 3500 | Max N | 3.74 | 0.00 | -0.38 | 0.00 | 0.00 | 0.00 | BC 18 |
| | | | | Min N | -3.57 | 0.00 | -0.26 | 0.00 | 0.00 | 0.00 | BC 42 |
| | | | | Max $V_y$ | 0.01 | 0.00 | -0.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.01 | 0.00 | -0.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -3.57 | 0.00 | -0.26 | 0.00 | 0.00 | 0.00 | BC 34 |
| | | | | Min $V_z$ | 0.01 | 0.00 | -0.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.02 | 0.00 | -0.38 | 0.00 | 0.00 | 0.00 | BC 12 |
| | | | | Min $M_T$ | 2.90 | 0.00 | -0.26 | -0.00 | 0.00 | 0.00 | BC 43 |
| | | | | Max $M_y$ | 0.02 | 0.00 | -0.38 | 0.00 | 0.00 | 0.00 | BC 12 |
| | | | | Min $M_y$ | 0.01 | 0.00 | -0.26 | 0.00 | 0.00 | 0.00 | BC 4 |
| | | | | Max $M_z$ | 0.01 | 0.00 | -0.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.01 | 0.00 | -0.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| 12 | RC1 | 12 | 0 | Max N | 3.75 | 0.00 | 0.38 | 0.00 | 0.00 | 0.00 | BC 25 |
| | | | | Min N | -3.53 | 0.00 | 0.26 | 0.00 | 0.00 | 0.00 | BC 33 |
| | | | | Max $V_y$ | 0.01 | 0.00 | 0.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.01 | 0.00 | 0.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.01 | 0.00 | 0.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -3.53 | 0.00 | 0.26 | 0.00 | 0.00 | 0.00 | BC 33 |
| | | | | Max $M_T$ | 0.03 | 0.00 | 0.38 | 0.00 | 0.00 | 0.00 | BC 12 |
| | | | | Min $M_T$ | 2.92 | 0.00 | 0.26 | -0.00 | 0.00 | 0.00 | BC 44 |
| | | | | Max $M_y$ | -3.48 | 0.00 | 0.38 | 0.00 | 0.00 | 0.00 | BC 16 |
| | | | | Min $M_y$ | 0.01 | 0.00 | 0.26 | 0.00 | 0.00 | 0.00 | BC 4 |
| | | | | Max $M_z$ | 0.01 | 0.00 | 0.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.01 | 0.00 | 0.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 14 | 3500 | Max N | 3.75 | 0.00 | -0.38 | 0.00 | 0.00 | 0.00 | BC 25 |
| | | | | Min N | -3.53 | 0.00 | -0.26 | 0.00 | 0.00 | 0.00 | BC 33 |
| | | | | Max $V_y$ | 0.01 | 0.00 | -0.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.01 | 0.00 | -0.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -3.53 | 0.00 | -0.26 | 0.00 | 0.00 | 0.00 | BC 33 |
| | | | | Min $V_z$ | 0.01 | 0.00 | -0.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.03 | 0.00 | -0.38 | 0.00 | 0.00 | 0.00 | BC 12 |
| | | | | Min $M_T$ | 2.92 | 0.00 | -0.26 | -0.00 | 0.00 | 0.00 | BC 44 |
| | | | | Max $M_y$ | -3.48 | 0.00 | -0.38 | 0.00 | 0.00 | 0.00 | BC 16 |
| | | | | Min $M_y$ | 0.01 | 0.00 | -0.26 | 0.00 | 0.00 | 0.00 | BC 4 |
| | | | | Max $M_z$ | 0.01 | 0.00 | -0.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.01 | 0.00 | -0.43 | 0.00 | 0.00 | 0.00 | BC 1 |
| 13 | RC1 | 14 | 0 | Max N | 3.74 | 0.00 | 0.38 | -0.00 | 0.00 | 0.00 | BC 17 |
| | | | | Min N | -3.57 | 0.00 | 0.26 | -0.00 | 0.00 | 0.00 | BC 42 |
| | | | | Max $V_y$ | 0.01 | 0.00 | 0.43 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.01 | 0.00 | 0.43 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.01 | 0.00 | 0.43 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -3.57 | 0.00 | 0.26 | -0.00 | 0.00 | 0.00 | BC 34 |
| | | | | Max $M_T$ | 2.90 | 0.00 | 0.26 | 0.00 | 0.00 | 0.00 | BC 44 |
| | | | | Min $M_T$ | 0.02 | 0.00 | 0.38 | -0.00 | 0.00 | 0.00 | BC 12 |
| | | | | Max $M_y$ | 0.02 | 0.00 | 0.38 | -0.00 | 0.00 | 0.00 | BC 12 |
| | | | | Min $M_y$ | 0.01 | 0.00 | 0.26 | -0.00 | 0.00 | 0.00 | BC 4 |
| | | | | Max $M_z$ | 0.01 | 0.00 | 0.43 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.01 | 0.00 | 0.43 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | 16 | 3500 | Max N | 3.74 | 0.00 | -0.38 | -0.00 | 0.00 | 0.00 | BC 17 |
| | | | | Min N | -3.57 | 0.00 | -0.26 | -0.00 | 0.00 | 0.00 | BC 42 |
| | | | | Max $V_y$ | 0.01 | 0.00 | -0.43 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.01 | 0.00 | -0.43 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -3.57 | 0.00 | -0.26 | -0.00 | 0.00 | 0.00 | BC 34 |
| | | | | Min $V_z$ | 0.01 | 0.00 | -0.43 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 2.90 | 0.00 | -0.26 | 0.00 | 0.00 | 0.00 | BC 44 |
| | | | | Min $M_T$ | 0.02 | 0.00 | -0.38 | -0.00 | 0.00 | 0.00 | BC 12 |
| | | | | Max $M_y$ | 0.02 | 0.00 | -0.38 | -0.00 | 0.00 | 0.00 | BC 12 |
| | | | | Min $M_y$ | 0.01 | 0.00 | -0.26 | -0.00 | 0.00 | 0.00 | BC 4 |
| | | | | Max $M_z$ | 0.01 | 0.00 | -0.43 | -0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.01 | 0.00 | -0.43 | -0.00 | 0.00 | 0.00 | BC 1 |
| 14 | RC1 | 6 | 0 | Max N | 2.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 43 |
| | | | | Min N | -0.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 18 |
| | | | | Max $V_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 14 | 5315 | Max N | 2.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 43 |
| | | | | Min N | -0.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 18 |
| | | | | Max $V_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ | $V_z$ | Momenten [kNm] $M_T$ | $M_y$ | $M_z$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 14 | RC1 | | | Min $M_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 15 | RC1 | 12 | 0 | Max N | 2.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 44 |
| | | | | Min N | -0.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 17 |
| | | | | Max $V_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 8 | 5315 | Max N | 2.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 44 |
| | | | | Min N | -0.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 17 |
| | | | | Max $V_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 16 | RC1 | 5 | 0 | Max N | 8.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 33 |
| | | | | Min N | -0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 24 |
| | | | | Max $V_y$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 8 | 5353 | Max N | 8.88 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 15 |
| | | | | Min N | -0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 42 |
| | | | | Max $V_y$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 17 | RC1 | 7 | 0 | Max N | 8.70 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 34 |
| | | | | Min N | -0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 23 |
| | | | | Max $V_y$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 6 | 5353 | Max N | 8.82 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 16 |
| | | | | Min N | -0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 41 |
| | | | | Max $V_y$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 18 | RC1 | 11 | 0 | Max N | 8.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 33 |
| | | | | Min N | -0.21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 24 |
| | | | | Max $V_y$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 14 | 5353 | Max N | 8.88 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 15 |
| | | | | Min N | -0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 42 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ | $V_z$ | Momenten [kNm] $M_T$ | $M_y$ | $M_z$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 18 | RC1 | | | Max $V_y$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 19 | RC1 | 13 | 0 | Max N | 8.70 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 34 |
| | | | | Min N | -0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 23 |
| | | | | Max $V_y$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 12 | 5353 | Max N | 8.82 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 16 |
| | | | | Min N | -0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 41 |
| | | | | Max $V_y$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 20 | RC1 | 8 | 0 | Max N | 2.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 44 |
| | | | | Min N | -0.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 17 |
| | | | | Max $V_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 16 | 5315 | Max N | 2.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 44 |
| | | | | Min N | -0.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 17 |
| | | | | Max $V_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 21 | RC1 | 14 | 0 | Max N | 2.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 43 |
| | | | | Min N | -0.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 18 |
| | | | | Max $V_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | 10 | 5315 | Max N | 2.42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 43 |
| | | | | Min N | -0.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 18 |
| | | | | Max $V_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $V_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $V_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_T$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_T$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_y$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Max $M_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| | | | | Min $M_z$ | -0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | BC 1 |
| 22 | RC1 | 5 | 0 | Max N | 3.86 | -2.55 | 8.19 | -1.83 | -1.22 | -0.02 | BC 25 |
| | | | | Min N | -3.99 | -1.35 | 5.51 | -0.93 | 2.69 | 0.03 | BC 33 |
| | | | | Max $V_y$ | 3.12 | 1.30 | 5.87 | 0.65 | -1.17 | -0.02 | BC 35 |
| | | | | Min $V_y$ | 2.36 | -5.27 | -3.80 | -3.84 | -0.43 | 0.02 | BC 26 |
| | | | | Max $V_z$ | 3.65 | -2.39 | 8.28 | -1.60 | -1.35 | -0.02 | BC 43 |

## ■ 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ | $V_z$ | Momenten [kNm] $M_T$ | $M_y$ | $M_z$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 22 | RC1 | | | Min $V_z$ | 0.37 | -0.48 | -6.72 | -0.84 | 0.62 | 0.00 | BC 12 |
| | | | | Max $M_T$ | 3.12 | 1.30 | 5.87 | 0.65 | -1.17 | -0.02 | BC 35 |
| | | | | Min $M_T$ | 2.36 | -5.27 | -3.80 | -3.84 | -0.43 | 0.02 | BC 26 |
| | | | | Max $M_y$ | -3.79 | -1.51 | 5.42 | -1.16 | 2.81 | 0.04 | BC 15 |
| | | | | Min $M_y$ | 3.65 | -2.39 | 8.28 | -1.60 | -1.35 | -0.02 | BC 43 |
| | | | | Max $M_z$ | -3.79 | -1.51 | 5.42 | -1.16 | 2.81 | 0.04 | BC 15 |
| | | | | Min $M_z$ | 3.65 | -2.39 | 8.28 | -1.60 | -1.35 | -0.02 | BC 43 |
| | | 7 | 3500 | Max N | 77.82 | 0.80 | 8.45 | 2.15 | 17.28 | -1.73 | BC 23 |
| | | | | Min N | -10.08 | 1.25 | 2.93 | -1.03 | -0.75 | -0.37 | BC 34 |
| | | | | Max $V_y$ | 4.94 | 1.62 | 10.24 | 0.92 | 1.92 | -0.54 | BC 18 |
| | | | | Min $V_y$ | 64.70 | -2.03 | 1.03 | -1.14 | 13.11 | -0.92 | BC 43 |
| | | | | Max $V_z$ | 13.64 | 0.24 | 14.97 | 0.15 | 5.34 | -0.01 | BC 12 |
| | | | | Min $V_z$ | 64.70 | -2.03 | 1.03 | -1.14 | 13.11 | -0.92 | BC 43 |
| | | | | Max $M_T$ | 29.24 | 0.96 | 8.83 | 2.24 | 7.61 | -0.20 | BC 15 |
| | | | | Min $M_T$ | 64.70 | -2.03 | 1.03 | -1.14 | 13.11 | -0.92 | BC 43 |
| | | | | Max $M_y$ | 77.82 | 0.80 | 8.45 | 2.15 | 17.28 | -1.73 | BC 23 |
| | | | | Min $M_y$ | -10.08 | 1.25 | 2.93 | -1.03 | -0.75 | -0.37 | BC 34 |
| | | | | Max $M_z$ | 16.11 | -1.87 | 1.42 | -1.05 | 3.44 | 0.60 | BC 35 |
| | | | | Min $M_z$ | 53.53 | 1.46 | 9.85 | 0.83 | 11.59 | -2.07 | BC 26 |
| 23 | RC1 | 7 | 0 | Max N | 77.73 | -1.16 | -11.34 | 0.87 | 17.33 | -1.74 | BC 23 |
| | | | | Min N | -7.09 | -0.96 | 0.19 | -2.33 | -2.36 | -0.37 | BC 34 |
| | | | | Max $V_y$ | 64.68 | 1.89 | -1.06 | 0.92 | 13.12 | -0.93 | BC 43 |
| | | | | Min $V_y$ | 4.94 | -1.61 | -10.17 | -1.01 | 1.92 | -0.54 | BC 18 |
| | | | | Max $V_z$ | 41.48 | -0.95 | 0.49 | -2.39 | 7.32 | -1.90 | BC 42 |
| | | | | Min $V_z$ | 13.64 | -0.23 | -14.89 | -0.25 | 5.34 | -0.01 | BC 12 |
| | | | | Max $M_T$ | 16.10 | 1.88 | -1.36 | 0.98 | 3.44 | 0.60 | BC 35 |
| | | | | Min $M_T$ | 45.36 | -0.96 | -1.69 | -2.43 | 8.43 | -1.90 | BC 24 |
| | | | | Max $M_y$ | 77.73 | -1.16 | -11.34 | 0.87 | 17.33 | -1.74 | BC 23 |
| | | | | Min $M_y$ | -7.09 | -0.96 | 0.19 | -2.33 | -2.36 | -0.37 | BC 34 |
| | | | | Max $M_z$ | 16.10 | 1.88 | -1.36 | 0.98 | 3.44 | 0.60 | BC 35 |
| | | | | Min $M_z$ | 53.51 | -1.60 | -9.86 | -1.07 | 11.60 | -2.07 | BC 26 |
| | | 9 | 3500 | Max N | 3.79 | 2.55 | -8.43 | 1.83 | -1.19 | -0.02 | BC 25 |
| | | | | Min N | -1.54 | 0.76 | 0.70 | 0.75 | 1.30 | 0.02 | BC 34 |
| | | | | Max $V_y$ | 2.29 | 5.27 | 3.56 | 3.85 | -0.40 | 0.02 | BC 26 |
| | | | | Min $V_y$ | 3.12 | -1.31 | -5.99 | -0.66 | -1.17 | -0.02 | BC 35 |
| | | | | Max $V_z$ | 0.37 | 0.45 | 6.56 | 0.82 | 0.61 | 0.00 | BC 12 |
| | | | | Min $V_z$ | 3.58 | 2.40 | -8.48 | 1.61 | -1.31 | -0.02 | BC 43 |
| | | | | Max $M_T$ | 2.29 | 5.27 | 3.56 | 3.85 | -0.40 | 0.02 | BC 26 |
| | | | | Min $M_T$ | 3.12 | -1.31 | -5.99 | -0.66 | -1.17 | -0.02 | BC 35 |
| | | | | Max $M_y$ | -1.33 | 0.91 | 0.74 | 0.97 | 1.42 | 0.02 | BC 16 |
| | | | | Min $M_y$ | 3.58 | 2.40 | -8.48 | 1.61 | -1.31 | -0.02 | BC 43 |
| | | | | Max $M_z$ | -0.87 | 4.62 | -1.75 | 3.25 | 1.28 | 0.02 | BC 24 |
| | | | | Min $M_z$ | 3.12 | -1.31 | -5.99 | -0.66 | -1.17 | -0.02 | BC 35 |
| 24 | RC1 | 11 | 0 | Max N | 3.86 | 2.55 | 8.19 | 1.83 | -1.22 | 0.02 | BC 26 |
| | | | | Min N | -3.99 | 1.35 | 5.51 | 0.93 | 2.69 | -0.03 | BC 33 |
| | | | | Max $V_y$ | 2.36 | 5.27 | -3.80 | 3.84 | -0.43 | -0.02 | BC 25 |
| | | | | Min $V_y$ | 3.12 | -1.30 | 5.87 | -0.65 | -1.17 | 0.02 | BC 36 |
| | | | | Max $V_z$ | 3.65 | 2.39 | 8.28 | 1.60 | -1.35 | 0.02 | BC 44 |
| | | | | Min $V_z$ | 0.37 | 0.48 | -6.72 | 0.84 | 0.62 | -0.00 | BC 12 |
| | | | | Max $M_T$ | 2.36 | 5.27 | -3.80 | 3.84 | -0.43 | -0.02 | BC 25 |
| | | | | Min $M_T$ | 3.12 | -1.30 | 5.87 | -0.65 | -1.17 | 0.02 | BC 36 |
| | | | | Max $M_y$ | -3.79 | 1.51 | 5.42 | 1.16 | 2.81 | -0.04 | BC 15 |
| | | | | Min $M_y$ | 3.65 | 2.39 | 8.28 | 1.60 | -1.35 | 0.02 | BC 44 |
| | | | | Max $M_z$ | 3.65 | 2.39 | 8.28 | 1.60 | -1.35 | 0.02 | BC 44 |
| | | | | Min $M_z$ | -3.79 | 1.51 | 5.42 | 1.16 | 2.81 | -0.04 | BC 15 |
| | | 13 | 3500 | Max N | 77.82 | -0.80 | 8.45 | -2.15 | 17.28 | 1.73 | BC 23 |
| | | | | Min N | -10.08 | -1.25 | 2.93 | 1.03 | -0.75 | 0.37 | BC 34 |
| | | | | Max $V_y$ | 64.70 | 2.03 | 1.03 | 1.14 | 13.11 | 0.92 | BC 44 |
| | | | | Min $V_y$ | 4.94 | -1.62 | 10.24 | -0.92 | 1.92 | 0.54 | BC 17 |
| | | | | Max $V_z$ | 13.64 | -0.24 | 14.97 | -0.15 | 5.34 | 0.01 | BC 12 |
| | | | | Min $V_z$ | 64.70 | 2.03 | 1.03 | 1.14 | 13.11 | 0.92 | BC 44 |
| | | | | Max $M_T$ | 64.70 | 2.03 | 1.03 | 1.14 | 13.11 | 0.92 | BC 44 |
| | | | | Min $M_T$ | 29.24 | -0.96 | 8.83 | -2.24 | 7.61 | 0.20 | BC 15 |
| | | | | Max $M_y$ | 77.82 | -0.80 | 8.45 | -2.15 | 17.28 | 1.73 | BC 23 |
| | | | | Min $M_y$ | -10.08 | -1.25 | 2.93 | 1.03 | -0.75 | 0.37 | BC 34 |
| | | | | Max $M_z$ | 53.53 | -1.46 | 9.85 | -0.83 | 11.59 | 2.07 | BC 25 |
| | | | | Min $M_z$ | 16.11 | 1.87 | 1.42 | 1.05 | 3.44 | -0.60 | BC 36 |
| 25 | RC1 | 13 | 0 | Max N | 77.73 | 1.16 | -11.34 | -0.87 | 17.33 | 1.74 | BC 23 |
| | | | | Min N | -7.09 | 0.96 | 0.19 | 2.33 | -2.36 | 0.37 | BC 34 |
| | | | | Max $V_y$ | 4.94 | 1.61 | -10.17 | 1.01 | 1.92 | 0.54 | BC 17 |
| | | | | Min $V_y$ | 64.68 | -1.89 | -1.06 | -0.92 | 13.12 | 0.93 | BC 44 |
| | | | | Max $V_z$ | 41.48 | 0.95 | 0.49 | 2.39 | 7.32 | 1.90 | BC 42 |
| | | | | Min $V_z$ | 13.64 | 0.23 | -14.89 | 0.25 | 5.34 | 0.01 | BC 12 |
| | | | | Max $M_T$ | 45.36 | 0.96 | -1.69 | 2.43 | 8.43 | 1.90 | BC 24 |
| | | | | Min $M_T$ | 16.10 | -1.88 | -1.36 | -0.98 | 3.44 | -0.60 | BC 36 |
| | | | | Max $M_y$ | 77.73 | 1.16 | -11.34 | -0.87 | 17.33 | 1.74 | BC 23 |
| | | | | Min $M_y$ | -7.09 | 0.96 | 0.19 | 2.33 | -2.36 | 0.37 | BC 34 |
| | | | | Max $M_z$ | 53.51 | 1.60 | -9.86 | 1.07 | 11.60 | 2.07 | BC 25 |
| | | | | Min $M_z$ | 16.10 | -1.88 | -1.36 | -0.98 | 3.44 | -0.60 | BC 36 |
| | | 15 | 3500 | Max N | 3.79 | -2.55 | -8.43 | -1.83 | -1.19 | 0.02 | BC 26 |
| | | | | Min N | -1.54 | -0.76 | 0.70 | -0.75 | 1.30 | -0.02 | BC 34 |
| | | | | Max $V_y$ | 3.12 | 1.31 | -5.99 | 0.66 | -1.17 | 0.02 | BC 40 |
| | | | | Min $V_y$ | 2.29 | -5.27 | 3.56 | -3.85 | -0.40 | -0.02 | BC 25 |
| | | | | Max $V_z$ | 0.37 | -0.45 | 6.56 | -0.82 | 0.61 | -0.00 | BC 12 |
| | | | | Min $V_z$ | 3.58 | -2.40 | -8.48 | -1.61 | -1.31 | 0.02 | BC 44 |
| | | | | Max $M_T$ | 3.12 | 1.31 | -5.99 | 0.66 | -1.17 | 0.02 | BC 36 |
| | | | | Min $M_T$ | 2.29 | -5.27 | 3.56 | -3.85 | -0.40 | -0.02 | BC 25 |

## 4.6 STAVEN - SNEDEKRACHTEN

Resultaatcombinaties

| Staaf No. | RC | Knoop No. | Snede x [mm] | | Krachten [kN] N | $V_y$ | $V_z$ | Momenten [kNm] $M_T$ | $M_y$ | $M_z$ | Bijbehorend Belastingsgevallen |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 25 | RC1 | | | Max $M_y$ | -1.33 | -0.91 | 0.74 | -0.97 | 1.42 | -0.02 | BC 16 |
| | | | | Min $M_y$ | 3.58 | -2.40 | -8.48 | -1.61 | -1.31 | 0.02 | BC 44 |
| | | | | Max $M_z$ | 3.12 | 1.31 | -5.99 | 0.66 | -1.17 | 0.02 | BC 36 |
| | | | | Min $M_z$ | -0.87 | -4.62 | -1.75 | -3.25 | 1.28 | -0.02 | BC 24 |

**RF-STEEL EC3**
CA1
Ontwerp van stalen staven volgens Eurocode 3

## 1.1 ALGEMENE GEGEVENS

Te ontwerpen staven: 1-21
Te ontwerpen staafverz.:

Nationale bijlagen: NEN

Ontwerp uiterste grenstoestand
Te berekenen belastingscombinaties:

| | |
|---|---|
| BC1 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 |
| BC2 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 |
| BC3 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG150 |
| BC4 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 |
| BC5 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 |
| BC6 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 |
| BC7 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 |
| BC8 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 |
| BC9 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 |
| BC10 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 |
| BC11 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG150 |
| BC12 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG300 |
| BC13 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG300 |
| BC14 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG300 |
| BC15 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG401 |
| BC16 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG402 |
| BC17 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG403 |
| BC18 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG404 |
| BC19 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG401 |
| BC20 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG402 |
| BC21 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG403 |
| BC22 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG404 |
| BC23 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG401 |
| BC24 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG402 |
| BC25 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG403 |
| BC26 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG404 |
| BC27 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 |
| BC28 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 |
| BC29 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG150 |
| BC30 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG300 |
| BC31 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG300 |
| BC32 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG300 |
| BC33 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG401 |
| BC34 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG402 |
| BC35 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG403 |
| BC36 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG404 |
| BC37 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG401 |
| BC38 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG402 |
| BC39 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG403 |
| BC40 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG404 |
| BC41 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG401 |
| BC42 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG402 |
| BC43 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG403 |
| BC44 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG404 |

## 1.1 ALGEMENE GEGEVENS

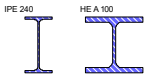
Ontwerp bruikbaarheidsgrenstoestand
Te berekenen belastingscombinaties:

| | |
|---|---|
| BC45 | BG10 + BG20 + BG30 + BG40 |
| BC46 | BG10 + BG20 + BG30 + BG40 + BG100 |
| BC47 | BG10 + BG20 + BG30 + BG40 + BG150 |
| BC48 | BG10 + BG20 + BG30 + BG40 + BG120 |
| BC49 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 |
| BC50 | BG10 + BG20 + BG30 + BG40 + BG120 + BG150 |
| BC51 | BG10 + BG20 + BG30 + BG40 + BG300 |
| BC52 | BG10 + BG20 + BG30 + BG40 + BG100 + BG300 |
| BC53 | BG10 + BG20 + BG30 + BG40 + BG150 + BG300 |
| BC54 | BG10 + BG20 + BG30 + BG40 + BG401 |
| BC55 | BG10 + BG20 + BG30 + BG40 + BG402 |
| BC56 | BG10 + BG20 + BG30 + BG40 + BG403 |
| BC57 | BG10 + BG20 + BG30 + BG40 + BG404 |
| BC58 | BG10 + BG20 + BG30 + BG40 + BG100 + BG401 |
| BC59 | BG10 + BG20 + BG30 + BG40 + BG100 + BG402 |
| BC60 | BG10 + BG20 + BG30 + BG40 + BG100 + BG403 |
| BC61 | BG10 + BG20 + BG30 + BG40 + BG100 + BG404 |
| BC62 | BG10 + BG20 + BG30 + BG40 + BG150 + BG401 |
| BC63 | BG10 + BG20 + BG30 + BG40 + BG150 + BG402 |
| BC64 | BG10 + BG20 + BG30 + BG40 + BG150 + BG403 |
| BC65 | BG10 + BG20 + BG30 + BG40 + BG150 + BG404 |

## 1.2 MATERIALEN

| Matl. No. | Materiaal Omschrijving | E-Modulus E [N/mm²] | Glijdingsmodulu G [N/mm²] | Coï¿½ff. van Poisso ν [-] | Vloeispanning $f_{yk}$ [N/mm²] | Max. Dikte t [mm] |
|---|---|---|---|---|---|---|
| 1 | Staal S 235 \| NEN EN 1993-1-1:2007-11 | 210000.0 | 80769.2 | 0.300 | 235.0 | 40.0 |
| | | | | | 215.0 | 80.0 |
| | | | | | 215.0 | 100.0 |
| | | | | | 195.0 | 150.0 |
| | | | | | 185.0 | 200.0 |
| | | | | | 175.0 | 250.0 |
| | | | | | 165.0 | 400.0 |

## 1.3 DOORSNEDES




| Snede No. | Matl. No. | Doorsnede Omschrijving | Doorsnede Type | Max Ontwerp Unity check | Commentaar |
|---|---|---|---|---|---|
| 1 | 1 | IPE 240 \| Euronorm 19-57 | Gewalst I-profiel | 0.47 | Hoofddraag kolom |
| 2 | 1 | IPE 240 \| Euronorm 19-57 | Gewalst I-profiel | 0.35 | Hoofddraag ligger |
| 3 | 1 | HE A 100 \| Euronorm 53-62 | Gewalst I-profiel | 0.03 | Tussenligger |
| 4 | 1 | L 60x60x6 \| EN 10056-1:1998 | Hoek | 0.01 | Horizontale verbanden |
| 5 | 1 | Rechthoek 6/60 | Platte staaf | 0.10 | Verticale verbanden |


## 1.5 KNIKLENGTES - STAVEN

| Staaf No. | Knik Mogelijk | Knik om y/u-as Mogelijk | $k_{cr,y/u}$ | $L_{cr,y/u}$ [mm] | Knik om z/v-as Mogelijk | $k_{cr,z/v}$ | $L_{cr,z/v}$ [mm] | Kip Mogelijk | $k_z$ | $k_w$ | $L_w$ [mm] | $L_T$ [mm] |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1 | ☒ | ☒ | 1.00 | 4050 | ☒ | 1.00 | 4050 | ☒ | 1.0 | 1.0 | 4050 | 4050 |
| 2 | ☒ | ☒ | 1.00 | 4050 | ☒ | 1.00 | 4050 | ☒ | 1.0 | 1.0 | 4050 | 4050 |
| 3 | ☒ | ☒ | 1.00 | 4050 | ☒ | 1.00 | 4050 | ☒ | 1.0 | 1.0 | 4050 | 4050 |
| 4 | ☒ | ☒ | 1.00 | 4050 | ☒ | 1.00 | 4050 | ☒ | 1.0 | 1.0 | 4050 | 4050 |
| 5 | ☒ | ☒ | 1.00 | 4050 | ☒ | 1.00 | 4050 | ☒ | 1.0 | 1.0 | 4050 | 4050 |
| 6 | ☒ | ☒ | 1.00 | 4050 | ☒ | 1.00 | 4050 | ☒ | 1.0 | 1.0 | 4050 | 4050 |
| 7 | ☒ | ☒ | 1.00 | 4000 | ☒ | 1.00 | 4000 | ☒ | 1.0 | 1.0 | 4000 | 4000 |
| 8 | ☒ | ☒ | 1.00 | 4000 | ☒ | 1.00 | 4000 | ☒ | 1.0 | 1.0 | 4000 | 4000 |
| 9 | ☒ | ☒ | 1.00 | 4000 | ☒ | 1.00 | 4000 | ☒ | 1.0 | 1.0 | 4000 | 4000 |
| 10 | ☒ | ☒ | 1.00 | 3500 | ☒ | 1.00 | 3500 | ☒ | 1.0 | 1.0 | 3500 | 3500 |
| 11 | ☒ | ☒ | 1.00 | 3500 | ☒ | 1.00 | 3500 | ☒ | 1.0 | 1.0 | 3500 | 3500 |
| 12 | ☒ | ☒ | 1.00 | 3500 | ☒ | 1.00 | 3500 | ☒ | 1.0 | 1.0 | 3500 | 3500 |
| 13 | ☒ | ☒ | 1.00 | 3500 | ☒ | 1.00 | 3500 | ☒ | 1.0 | 1.0 | 3500 | 3500 |
| 14 | ☐ | ☐ | 1.00 | 5315 | ☐ | 1.00 | 5315 | ☐ | 1.0 | 1.0 | 5315 | 5315 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 15 | ☐ | ☐ | 1.00 | 5315 | ☐ | 1.00 | 5315 | ☐ | 1.0 | 1.0 | 5315 | 5315 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 16 | ☐ | ☐ | 1.00 | 5353 | ☐ | 1.00 | 5353 | ☐ | 1.0 | 1.0 | 5353 | 5353 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 17 | ☐ | ☐ | 1.00 | 5353 | ☐ | 1.00 | 5353 | ☐ | 1.0 | 1.0 | 5353 | 5353 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 18 | ☐ | ☐ | 1.00 | 5353 | ☐ | 1.00 | 5353 | ☐ | 1.0 | 1.0 | 5353 | 5353 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 19 | ☐ | ☐ | 1.00 | 5353 | ☐ | 1.00 | 5353 | ☐ | 1.0 | 1.0 | 5353 | 5353 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 20 | ☐ | ☐ | 1.00 | 5315 | ☐ | 1.00 | 5315 | ☐ | 1.0 | 1.0 | 5315 | 5315 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 21 | ☐ | ☐ | 1.00 | 5315 | ☐ | 1.00 | 5315 | ☐ | 1.0 | 1.0 | 5315 | 5315 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |

## 1.9 BRUIKBAARHEIDSGEGEVENS

| No. | Verwijzing naar | Staven/VerzamelingNo. | Referentielengte Handmatig | l [mm] | Richt. | Toog $e_0$ [mm] | Staaftype |
|---|---|---|---|---|---|---|---|
| 1 | Staaf | 1 | ☐ | 4050 | y, z | 0.0 | Ligger |
| 2 | Staaf | 2 | ☐ | 4050 | y, z | 0.0 | Ligger |
| 3 | Staaf | 3 | ☐ | 4050 | y, z | 0.0 | Ligger |
| 4 | Staaf | 4 | ☐ | 4050 | y, z | 0.0 | Ligger |
| 5 | Staaf | 5 | ☐ | 4050 | y, z | 0.0 | Ligger |
| 6 | Staaf | 6 | ☐ | 4050 | y, z | 0.0 | Ligger |
| 7 | Staaf | 7 | ☐ | 4000 | y, z | 0.0 | Ligger |
| 8 | Staaf | 8 | ☐ | 4000 | y, z | 0.0 | Ligger |
| 9 | Staaf | 9 | ☐ | 4000 | y, z | 0.0 | Ligger |
| 10 | Staaf | 10 | ☐ | 3500 | y, z | 0.0 | Ligger |
| 11 | Staaf | 11 | ☐ | 3500 | y, z | 0.0 | Ligger |
| 12 | Staaf | 12 | ☐ | 3500 | y, z | 0.0 | Ligger |
| 13 | Staaf | 13 | ☐ | 3500 | y, z | 0.0 | Ligger |
| 14 | Staaf | 14 | ☐ | 5315 | y, z | 0.0 | Ligger |
| 15 | Staaf | 15 | ☐ | 5315 | y, z | 0.0 | Ligger |
| 16 | Staaf | 16 | ☐ | 5353 | y, z | 0.0 | Ligger |
| 17 | Staaf | 17 | ☐ | 5353 | y, z | 0.0 | Ligger |
| 18 | Staaf | 18 | ☐ | 5353 | y, z | 0.0 | Ligger |
| 19 | Staaf | 19 | ☐ | 5353 | y, z | 0.0 | Ligger |
| 20 | Staaf | 20 | ☐ | 5315 | y, z | 0.0 | Ligger |
| 21 | Staaf | 21 | ☐ | 5315 | y, z | 0.0 | Ligger |

## 2.1 BEREKENING PER GEVAL/COMBI

| BG/BC/RC | Belastingsgeval of BC/RC Omschrijving | Staaf No. | Positie x [mm] | Berekening | | vergelijki No. | Omschrijving |
|---|---|---|---|---|---|---|---|
| | Ontwerp uiterste grenstoestand | | | | | | |
| BC26 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG404 | 1 | 50 | 0.47 | ≤ 1 | ST364) | PT |
| | Ontwerp bruikbaarheidsgrenstoestand | | | | | | |
| BC64 | BG10 + BG20 + BG30 + BG40 + BG150 + BG403 | 3 | 2115 | 0.46 | ≤ 1 | SE406) | KR |

## 2.4 BEREKENING PER STAAF

| Staaf No. | Positie x [mm] | BG/BC/RC | Berekening | | vergelijki No. | Omschrijving |
|---|---|---|---|---|---|---|
| 1 | Doorsnede No. 1 - IPE 240 \| Euronorm 19-57 | | | | | |
| | 50 | BC26 | 0.47 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 2 | Doorsnede No. 1 - IPE 240 \| Euronorm 19-57 | | | | | |
| | 50 | BC26 | 0.31 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 3 | Doorsnede No. 1 - IPE 240 \| Euronorm 19-57 | | | | | |
| | 50 | BC26 | 0.47 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 4 | Doorsnede No. 1 - IPE 240 \| Euronorm 19-57 | | | | | |
| | 50 | BC25 | 0.47 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 5 | Doorsnede No. 1 - IPE 240 \| Euronorm 19-57 | | | | | |
| | 50 | BC25 | 0.31 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 6 | Doorsnede No. 1 - IPE 240 \| Euronorm 19-57 | | | | | |
| | 50 | BC25 | 0.47 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 7 | Doorsnede No. 2 - IPE 240 \| Euronorm 19-57 | | | | | |
| | 2000 | BC12 | 0.18 | ≤ 1 | ST331) | Stabiliteitsberekening - Kip volgens 6.3.2.1 en 6.3.2.3 - I-profiel |
| 8 | Doorsnede No. 2 - IPE 240 \| Euronorm 19-57 | | | | | |
| | 2000 | BC12 | 0.35 | ≤ 1 | ST331) | Stabiliteitsberekening - Kip volgens 6.3.2.1 en 6.3.2.3 - I-profiel |
| 9 | Doorsnede No. 2 - IPE 240 \| Euronorm 19-57 | | | | | |
| | 2000 | BC12 | 0.18 | ≤ 1 | ST331) | Stabiliteitsberekening - Kip volgens 6.3.2.1 en 6.3.2.3 - I-profiel |
| 10 | Doorsnede No. 3 - HE A 100 \| Euronorm 53-62 | | | | | |
| | 1750 | BC57 | 0.03 | ≤ 1 | SE401) | Bruikbaarheid - Belastingscombinaties 'Karakteristiek' - z-richting |
| 11 | Doorsnede No. 3 - HE A 100 \| Euronorm 53-62 | | | | | |
| | 1750 | BC61 | 0.03 | ≤ 1 | SE401) | Bruikbaarheid - Belastingscombinaties 'Karakteristiek' - z-richting |
| 12 | Doorsnede No. 3 - HE A 100 \| Euronorm 53-62 | | | | | |
| | 1750 | BC56 | 0.03 | ≤ 1 | SE401) | Bruikbaarheid - Belastingscombinaties 'Karakteristiek' - z-richting |
| 13 | Doorsnede No. 3 - HE A 100 \| Euronorm 53-62 | | | | | |
| | 1750 | BC60 | 0.03 | ≤ 1 | SE401) | Bruikbaarheid - Belastingscombinaties 'Karakteristiek' - z-richting |
| 14 | Doorsnede No. 4 - L 60x60x6 \| EN 10056-1:1998 | | | | | |
| | 0 | BC43 | 0.01 | ≤ 1 | CS101) | Doorsnedecontrole - Trek volgens 6.2.3 |
| 15 | Doorsnede No. 4 - L 60x60x6 \| EN 10056-1:1998 | | | | | |
| | 0 | BC44 | 0.01 | ≤ 1 | CS101) | Doorsnedecontrole - Trek volgens 6.2.3 |
| 16 | Doorsnede No. 5 - Rechthoek 6/60 | | | | | |
| | 5353 | BC15 | 0.10 | ≤ 1 | CS101) | Doorsnedecontrole - Trek volgens 6.2.3 |
| 17 | Doorsnede No. 5 - Rechthoek 6/60 | | | | | |
| | 5353 | BC16 | 0.10 | ≤ 1 | CS101) | Doorsnedecontrole - Trek volgens 6.2.3 |
| 18 | Doorsnede No. 5 - Rechthoek 6/60 | | | | | |

## 2.4 BEREKENING PER STAAF

| Staaf No. | Positie x [mm] | BG/BC/ RC | Berekening | | vergelijki No. | Omschrijving |
|---|---|---|---|---|---|---|
| | 5353 | BC15 | 0.10 | ≤ 1 | CS101) | Doorsnedecontrole - Trek volgens 6.2.3 |
| 19 | Doorsnede No. 5 - Rechthoek 6/60 | | | | | |
| | 5353 | BC16 | 0.10 | ≤ 1 | CS101) | Doorsnedecontrole - Trek volgens 6.2.3 |
| 20 | Doorsnede No. 4 - L 60x60x6 \| EN 10056-1:1998 | | | | | |
| | 0 | BC44 | 0.01 | ≤ 1 | CS101) | Doorsnedecontrole - Trek volgens 6.2.3 |
| 21 | Doorsnede No. 4 - L 60x60x6 \| EN 10056-1:1998 | | | | | |
| | 0 | BC43 | 0.01 | ≤ 1 | CS101) | Doorsnedecontrole - Trek volgens 6.2.3 |

**RF-STEEL EC3**
CA2
Aardbeving

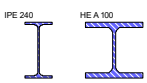
## 1.1 ALGEMENE GEGEVENS

| | | |
|---|---|---|
| Te ontwerpen staven: | 1-21 | |
| Te ontwerpen staafverz.: | | |
| Nationale bijlagen: | NEN | |
| Ontwerp uiterste grenstoestand | | |
| Te berekenen RC's: | RC20 | Tabel NB.7 A1.3 |
| Ontwerp bruikbaarheidsgrenstoestand | | |
| Te berekenen RC's: | RC20 | Tabel NB.7 A1.3 |

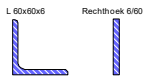
## 1.2 MATERIALEN

| Matl. No. | Materiaal Omschrijving | E-Modulus E [N/mm²] | Glijdingsmodulu G [N/mm²] | Coï¿½ff. van Poisso ν [-] | Vloeispanning $f_{yk}$ [N/mm²] | Max. Dikte t [mm] |
|---|---|---|---|---|---|---|
| 1 | Staal S 235 \| NEN EN 1993-1-1:2007-11 | 210000.0 | 80769.2 | 0.300 | 235.0 | 40.0 |
| | | | | | 215.0 | 80.0 |
| | | | | | 215.0 | 100.0 |
| | | | | | 195.0 | 150.0 |
| | | | | | 185.0 | 200.0 |
| | | | | | 175.0 | 250.0 |
| | | | | | 165.0 | 400.0 |

## 1.3 DOORSNEDES




| Snede No. | Matl. No. | Doorsnede Omschrijving | Doorsnede Type | Max Ontwerp Unity check | Commentaar |
|---|---|---|---|---|---|
| 1 | 1 | IPE 240 \| Euronorm 19-57 | Gewalst I-profiel | 0.32 | Hoofddraag kolom |
| 2 | 1 | IPE 240 \| Euronorm 19-57 | Gewalst I-profiel | 0.96 | Hoofddraag ligger |
| 3 | 1 | HE A 100 \| Euronorm 53-62 | Gewalst I-profiel | 0.08 | Tussenligger |
| 4 | 1 | L 60x60x6 \| EN 10056-1:1998 | Hoek | 0.01 | Horizontale verbanden |
| 5 | 1 | Rechthoek 6/60 | Platte staaf | 0.18 | Verticale verbanden |




## 1.5 KNIKLENGTES - STAVEN

| Staaf No. | Knik Mogelijk | Knik om y/u-as Mogelijk | $k_{cr,y/u}$ | $L_{cr,y/u}$ [mm] | Knik om z/v-as Mogelijk | $k_{cr,z/v}$ | $L_{cr,z/v}$ [mm] | Kip Mogelijk | $k_z$ | $k_w$ | $L_w$ [mm] | $L_T$ [mm] |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1 | ☒ | ☒ | 1.00 | 4050 | ☒ | 1.00 | 4050 | ☒ | 1.0 | 1.0 | 4050 | 4050 |
| 2 | ☒ | ☒ | 1.00 | 4050 | ☒ | 1.00 | 4050 | ☒ | 1.0 | 1.0 | 4050 | 4050 |
| 3 | ☒ | ☒ | 1.00 | 4050 | ☒ | 1.00 | 4050 | ☒ | 1.0 | 1.0 | 4050 | 4050 |
| 4 | ☒ | ☒ | 1.00 | 4050 | ☒ | 1.00 | 4050 | ☒ | 1.0 | 1.0 | 4050 | 4050 |
| 5 | ☒ | ☒ | 1.00 | 4050 | ☒ | 1.00 | 4050 | ☒ | 1.0 | 1.0 | 4050 | 4050 |
| 6 | ☒ | ☒ | 1.00 | 4050 | ☒ | 1.00 | 4050 | ☒ | 1.0 | 1.0 | 4050 | 4050 |
| 7 | ☒ | ☒ | 1.00 | 4000 | ☒ | 1.00 | 4000 | ☒ | 1.0 | 1.0 | 4000 | 4000 |
| 8 | ☒ | ☒ | 1.00 | 4000 | ☒ | 1.00 | 4000 | ☒ | 1.0 | 1.0 | 4000 | 4000 |
| 9 | ☒ | ☒ | 1.00 | 4000 | ☒ | 1.00 | 4000 | ☒ | 1.0 | 1.0 | 4000 | 4000 |
| 10 | ☒ | ☒ | 1.00 | 3500 | ☒ | 1.00 | 3500 | ☒ | 1.0 | 1.0 | 3500 | 3500 |
| 11 | ☒ | ☒ | 1.00 | 3500 | ☒ | 1.00 | 3500 | ☒ | 1.0 | 1.0 | 3500 | 3500 |
| 12 | ☒ | ☒ | 1.00 | 3500 | ☒ | 1.00 | 3500 | ☒ | 1.0 | 1.0 | 3500 | 3500 |
| 13 | ☒ | ☒ | 1.00 | 3500 | ☒ | 1.00 | 3500 | ☒ | 1.0 | 1.0 | 3500 | 3500 |
| 14 | ☐ | ☐ | 1.00 | 5315 | ☐ | 1.00 | 5315 | ☐ | 1.0 | 1.0 | 5315 | 5315 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 15 | ☐ | ☐ | 1.00 | 5315 | ☐ | 1.00 | 5315 | ☐ | 1.0 | 1.0 | 5315 | 5315 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 16 | ☐ | ☐ | 1.00 | 5353 | ☐ | 1.00 | 5353 | ☐ | 1.0 | 1.0 | 5353 | 5353 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 17 | ☐ | ☐ | 1.00 | 5353 | ☐ | 1.00 | 5353 | ☐ | 1.0 | 1.0 | 5353 | 5353 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 18 | ☐ | ☐ | 1.00 | 5353 | ☐ | 1.00 | 5353 | ☐ | 1.0 | 1.0 | 5353 | 5353 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 19 | ☐ | ☐ | 1.00 | 5353 | ☐ | 1.00 | 5353 | ☐ | 1.0 | 1.0 | 5353 | 5353 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 20 | ☐ | ☐ | 1.00 | 5315 | ☐ | 1.00 | 5315 | ☐ | 1.0 | 1.0 | 5315 | 5315 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |
| 21 | ☐ | ☐ | 1.00 | 5315 | ☐ | 1.00 | 5315 | ☐ | 1.0 | 1.0 | 5315 | 5315 |
| | Dit staaftype wordt niet toegestaan in een stabiliteitsberekening. | | | | | | | | | | | |

## 1.9 BRUIKBAARHEIDSGEGEVENS

| No. | Verwijzing naar | Staven/VerzamelingNo. | Referentielengte Handmatig | Referentielengte l [mm] | Richt. | Toog $e_0$ [mm] | Staaftype |
|---|---|---|---|---|---|---|---|
| 1 | Staaf | 1 | ☐ | 4050 | y, z | 0.0 | Ligger |
| 2 | Staaf | 2 | ☐ | 4050 | y, z | 0.0 | Ligger |
| 3 | Staaf | 3 | ☐ | 4050 | y, z | 0.0 | Ligger |
| 4 | Staaf | 4 | ☐ | 4050 | y, z | 0.0 | Ligger |
| 5 | Staaf | 5 | ☐ | 4050 | y, z | 0.0 | Ligger |
| 6 | Staaf | 6 | ☐ | 4050 | y, z | 0.0 | Ligger |
| 7 | Staaf | 7 | ☐ | 4000 | y, z | 0.0 | Ligger |
| 8 | Staaf | 8 | ☐ | 4000 | y, z | 0.0 | Ligger |
| 9 | Staaf | 9 | ☐ | 4000 | y, z | 0.0 | Ligger |
| 10 | Staaf | 10 | ☐ | 3500 | y, z | 0.0 | Ligger |
| 11 | Staaf | 11 | ☐ | 3500 | y, z | 0.0 | Ligger |
| 12 | Staaf | 12 | ☐ | 3500 | y, z | 0.0 | Ligger |
| 13 | Staaf | 13 | ☐ | 3500 | y, z | 0.0 | Ligger |
| 14 | Staaf | 14 | ☐ | 5315 | y, z | 0.0 | Ligger |
| 15 | Staaf | 15 | ☐ | 5315 | y, z | 0.0 | Ligger |
| 16 | Staaf | 16 | ☐ | 5353 | y, z | 0.0 | Ligger |
| 17 | Staaf | 17 | ☐ | 5353 | y, z | 0.0 | Ligger |
| 18 | Staaf | 18 | ☐ | 5353 | y, z | 0.0 | Ligger |
| 19 | Staaf | 19 | ☐ | 5353 | y, z | 0.0 | Ligger |
| 20 | Staaf | 20 | ☐ | 5315 | y, z | 0.0 | Ligger |
| 21 | Staaf | 21 | ☐ | 5315 | y, z | 0.0 | Ligger |

## 2.1 BEREKENING PER GEVAL/COMBI

| BG/BC/RC | Belastingsgeval of BC/RC Omschrijving | Staaf No. | Positie x [mm] | Berekening | | vergelijki No. | Omschrijving |
|---|---|---|---|---|---|---|---|
| | Ontwerp uiterste grenstoestand | | | | | | |
| RC20 | Tabel NB.7 A1.3 | 8 | 2200 | 0.92 | ≤ 1 | CS271) | PT |
| | Ontwerp bruikbaarheidsgrenstoestand | | | | | | |
| RC20 | Tabel NB.7 A1.3 | 8 | 2000 | 0.96 | ≤ 1 | SE406) | KR |

## 2.4 BEREKENING PER STAAF

| Staaf No. | Positie x [mm] | BG/BC/RC | Berekening | | vergelijki No. | Omschrijving |
|---|---|---|---|---|---|---|
| 1 | Doorsnede No. 1 - IPE 240 \| Euronorm 19-57 | | | | | |
| | 192 | RC20 | 0.30 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 2 | Doorsnede No. 1 - IPE 240 \| Euronorm 19-57 | | | | | |
| | 193 | RC20 | 0.32 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 3 | Doorsnede No. 1 - IPE 240 \| Euronorm 19-57 | | | | | |
| | 192 | RC20 | 0.26 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 4 | Doorsnede No. 1 - IPE 240 \| Euronorm 19-57 | | | | | |
| | 192 | RC20 | 0.30 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 5 | Doorsnede No. 1 - IPE 240 \| Euronorm 19-57 | | | | | |
| | 193 | RC20 | 0.32 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 6 | Doorsnede No. 1 - IPE 240 \| Euronorm 19-57 | | | | | |
| | 192 | RC20 | 0.25 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 7 | Doorsnede No. 2 - IPE 240 \| Euronorm 19-57 | | | | | |
| | 2000 | RC20 | 0.65 | ≤ 1 | SE406) | Bruikbaarheid - Belastingscombinaties 'Karakteristiek' - y-richting |
| 8 | Doorsnede No. 2 - IPE 240 \| Euronorm 19-57 | | | | | |
| | 2000 | RC20 | 0.96 | ≤ 1 | SE406) | Bruikbaarheid - Belastingscombinaties 'Karakteristiek' - y-richting |
| 9 | Doorsnede No. 2 - IPE 240 \| Euronorm 19-57 | | | | | |
| | 2000 | RC20 | 0.64 | ≤ 1 | SE406) | Bruikbaarheid - Belastingscombinaties 'Karakteristiek' - y-richting |
| 10 | Doorsnede No. 3 - HE A 100 \| Euronorm 53-62 | | | | | |
| | 194 | RC20 | 0.08 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 11 | Doorsnede No. 3 - HE A 100 \| Euronorm 53-62 | | | | | |
| | 0 | RC20 | 0.03 | ≤ 1 | ST363) | Stabiliteitsberekening - Dubbele buiging volgens 6.3.3, methode 2 |
| 12 | Doorsnede No. 3 - HE A 100 \| Euronorm 53-62 | | | | | |
| | 194 | RC20 | 0.08 | ≤ 1 | ST364) | Stabiliteitsberekening - Buiging en druk volgens 6.3.3, methode 2 |
| 13 | Doorsnede No. 3 - HE A 100 \| Euronorm 53-62 | | | | | |
| | 0 | RC20 | 0.03 | ≤ 1 | ST363) | Stabiliteitsberekening - Dubbele buiging volgens 6.3.3, methode 2 |
| 14 | Doorsnede No. 4 - L 60x60x6 \| EN 10056-1:1998 | | | | | |
| | 0 | RC20 | 0.00 | ≤ 1 | CS102) | Doorsnedecontrole - Druk volgens 6.2.4 |
| 15 | Doorsnede No. 4 - L 60x60x6 \| EN 10056-1:1998 | | | | | |
| | 0 | RC20 | 0.01 | ≤ 1 | CS102) | Doorsnedecontrole - Druk volgens 6.2.4 |
| 16 | Doorsnede No. 5 - Rechthoek 6/60 | | | | | |
| | 0 | RC20 | 0.09 | ≤ 1 | CS102) | Doorsnedecontrole - Druk volgens 6.2.4 |
| 17 | Doorsnede No. 5 - Rechthoek 6/60 | | | | | |
| | 0 | RC20 | 0.17 | ≤ 1 | CS102) | Doorsnedecontrole - Druk volgens 6.2.4 |
| 18 | Doorsnede No. 5 - Rechthoek 6/60 | | | | | |
| | 0 | RC20 | 0.09 | ≤ 1 | CS102) | Doorsnedecontrole - Druk volgens 6.2.4 |

## 2.4 BEREKENING PER STAAF

| Staaf No. | Positie x [mm] | BG/BC/ RC | Berekening | | vergelijki No. | Omschrijving |
|---|---|---|---|---|---|---|
| 19 | Doorsnede No. 5 - Rechthoek 6/60 | | | | | |
| | 0 | RC20 | 0.18 | ≤ 1 | CS102) | Doorsnedecontrole - Druk volgens 6.2.4 |
| 20 | Doorsnede No. 4 - L 60x60x6 \| EN 10056-1:1998 | | | | | |
| | 0 | RC20 | 0.01 | ≤ 1 | CS102) | Doorsnedecontrole - Druk volgens 6.2.4 |
| 21 | Doorsnede No. 4 - L 60x60x6 \| EN 10056-1:1998 | | | | | |
| | 0 | RC20 | 0.00 | ≤ 1 | CS102) | Doorsnedecontrole - Druk volgens 6.2.4 |

**RF-CONCRETE Surfaces**
BG1
Wapeningsberekening

## 1.1 ALGEMENE GEGEVENS

| | | |
|---|---|---|
| Berekening volgens norm: | NEN EN 1992-1-1+C2:2011/NB:2016-11 | |
| UITERSTE GRENSTOESTAND | | |
| Te berekenen BC's: | BC1 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 |
| | | Blijvend en tijdelijk |
| | BC2 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 |
| | | Blijvend en tijdelijk |
| | BC3 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC4 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 |
| | | Blijvend en tijdelijk |
| | BC5 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 |
| | | Blijvend en tijdelijk |
| | BC6 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC7 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 |
| | | Blijvend en tijdelijk |
| | BC8 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC9 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 |
| | | Blijvend en tijdelijk |
| | BC10 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 |
| | | Blijvend en tijdelijk |
| | BC11 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC12 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG300 |
| | | Blijvend en tijdelijk |
| | BC13 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG300 |
| | | Blijvend en tijdelijk |
| | BC14 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG300 |
| | | Blijvend en tijdelijk |
| | BC15 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG401 |
| | | Blijvend en tijdelijk |
| | BC16 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG402 |
| | | Blijvend en tijdelijk |
| | BC17 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG403 |
| | | Blijvend en tijdelijk |
| | BC18 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG404 |
| | | Blijvend en tijdelijk |
| | BC19 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG401 |
| | | Blijvend en tijdelijk |
| | BC20 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG402 |
| | | Blijvend en tijdelijk |
| | BC21 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG403 |
| | | Blijvend en tijdelijk |
| | BC22 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG404 |
| | | Blijvend en tijdelijk |
| | BC23 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG401 |
| | | Blijvend en tijdelijk |
| | BC24 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG402 |
| | | Blijvend en tijdelijk |
| | BC25 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG403 |
| | | Blijvend en tijdelijk |
| | BC26 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG404 |
| | | Blijvend en tijdelijk |
| | BC27 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 |
| | | Blijvend en tijdelijk |
| | BC28 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 |
| | | Blijvend en tijdelijk |
| | BC29 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG150 |
| | | Blijvend en tijdelijk |
| | BC30 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG300 |
| | | Blijvend en tijdelijk |
| | BC31 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG300 |
| | | Blijvend en tijdelijk |
| | BC32 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1 |

## 1.1 ALGEMENE GEGEVENS

| | | |
|---|---|---|
| | | 1.65*BG300 |
| | | Blijvend en tijdelijk |
| | BC33 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG401 |
| | | Blijvend en tijdelijk |
| | BC34 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG402 |
| | | Blijvend en tijdelijk |
| | BC35 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG403 |
| | | Blijvend en tijdelijk |
| | BC36 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG404 |
| | | Blijvend en tijdelijk |
| | BC37 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG401 |
| | | Blijvend en tijdelijk |
| | BC38 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG402 |
| | | Blijvend en tijdelijk |
| | BC39 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG403 |
| | | Blijvend en tijdelijk |
| | BC40 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG404 |
| | | Blijvend en tijdelijk |
| | BC41 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG401 |
| | | Blijvend en tijdelijk |
| | BC42 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG402 |
| | | Blijvend en tijdelijk |
| | BC43 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG403 |
| | | Blijvend en tijdelijk |
| | BC44 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG404 |
| | | Blijvend en tijdelijk |
| BRUIKBAARHEIDSGRENSTOESTAND | | |
| Te berekenen BC's: | BC45 | BG10 + BG20 + BG30 + BG40 |
| | | Karakteristiek met directe belasting, $k_t$ 0.600 |
| | BC46 | BG10 + BG20 + BG30 + BG40 + BG100 |
| | | Karakteristiek met directe belasting, $k_t$ 0.440 |
| | BC47 | BG10 + BG20 + BG30 + BG40 + BG150 |
| | | Karakteristiek met directe belasting, $k_t$ 0.440 |
| | BC48 | BG10 + BG20 + BG30 + BG40 + BG120 |
| | | Karakteristiek met directe belasting, $k_t$ 0.440 |
| | BC49 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 |
| | | Karakteristiek met directe belasting, $k_t$ 0.467 |
| | BC50 | BG10 + BG20 + BG30 + BG40 + BG120 + BG150 |
| | | Karakteristiek met directe belasting, $k_t$ 0.467 |
| | BC51 | BG10 + BG20 + BG30 + BG40 + BG300 |
| | | Karakteristiek met directe belasting, $k_t$ 0.440 |
| | BC52 | BG10 + BG20 + BG30 + BG40 + BG100 + BG300 |
| | | Karakteristiek met directe belasting, $k_t$ 0.467 |
| | BC53 | BG10 + BG20 + BG30 + BG40 + BG150 + BG300 |
| | | Karakteristiek met directe belasting, $k_t$ 0.467 |
| | BC54 | BG10 + BG20 + BG30 + BG40 + BG401 |
| | | Karakteristiek met directe belasting, $k_t$ 0.440 |
| | BC55 | BG10 + BG20 + BG30 + BG40 + BG402 |
| | | Karakteristiek met directe belasting, $k_t$ 0.440 |
| | BC56 | BG10 + BG20 + BG30 + BG40 + BG403 |
| | | Karakteristiek met directe belasting, $k_t$ 0.440 |
| | BC57 | BG10 + BG20 + BG30 + BG40 + BG404 |
| | | Karakteristiek met directe belasting, $k_t$ 0.440 |
| | BC58 | BG10 + BG20 + BG30 + BG40 + BG100 + BG401 |
| | | Karakteristiek met directe belasting, $k_t$ 0.467 |
| | BC59 | BG10 + BG20 + BG30 + BG40 + BG100 + BG402 |
| | | Karakteristiek met directe belasting, $k_t$ 0.467 |
| | BC60 | BG10 + BG20 + BG30 + BG40 + BG100 + BG403 |
| | | Karakteristiek met directe belasting, $k_t$ 0.467 |
| | BC61 | BG10 + BG20 + BG30 + BG40 + BG100 + BG404 |
| | | Karakteristiek met directe belasting, $k_t$ 0.467 |
| | BC62 | BG10 + BG20 + BG30 + BG40 + BG150 + BG401 |
| | | Karakteristiek met directe belasting, $k_t$ 0.467 |
| | BC63 | BG10 + BG20 + BG30 + BG40 + BG150 + BG402 |
| | | Karakteristiek met directe belasting, $k_t$ 0.467 |
| | BC64 | BG10 + BG20 + BG30 + BG40 + BG150 + BG403 |
| | | Karakteristiek met directe belasting, $k_t$ 0.467 |
| | BC65 | BG10 + BG20 + BG30 + BG40 + BG150 + BG404 |
| | | Karakteristiek met directe belasting, $k_t$ 0.467 |
| | BC66 | BG10 + BG20 + BG30 + BG40 |
| | | Frequent, $k_t$ 0.400 |
| | BC67 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 |
| | | Frequent, $k_t$ 0.437 |
| | BC68 | BG10 + BG20 + BG30 + BG40 + 0.9*BG150 |
| | | Frequent, $k_t$ 0.437 |
| | BC69 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 |
| | | Frequent, $k_t$ 0.433 |
| | BC70 | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG150 |
| | | Frequent, $k_t$ 0.433 |
| | BC71 | BG10 + BG20 + BG30 + BG40 + 0.2*BG300 |
| | | Frequent, $k_t$ 0.410 |
| | BC72 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG300 |
| | | Frequent, $k_t$ 0.440 |
| | BC73 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG300 |
| | | Frequent, $k_t$ 0.440 |

## 1.1 ALGEMENE GEGEVENS

| | | |
|---|---|---|
| | BC74 | BG10 + BG20 + BG30 + BG40 + 0.2*BG401 |
| | | Frequent, $k_t$ 0.410 |
| | BC75 | BG10 + BG20 + BG30 + BG40 + 0.2*BG402 |
| | | Frequent, $k_t$ 0.410 |
| | BC76 | BG10 + BG20 + BG30 + BG40 + 0.2*BG403 |
| | | Frequent, $k_t$ 0.410 |
| | BC77 | BG10 + BG20 + BG30 + BG40 + 0.2*BG404 |
| | | Frequent, $k_t$ 0.410 |
| | BC78 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG401 |
| | | Frequent, $k_t$ 0.440 |
| | BC79 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG402 |
| | | Frequent, $k_t$ 0.440 |
| | BC80 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG403 |
| | | Frequent, $k_t$ 0.440 |
| | BC81 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG404 |
| | | Frequent, $k_t$ 0.440 |
| | BC82 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG401 |
| | | Frequent, $k_t$ 0.440 |
| | BC83 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG402 |
| | | Frequent, $k_t$ 0.440 |
| | BC84 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG403 |
| | | Frequent, $k_t$ 0.440 |
| | BC85 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG404 |
| | | Frequent, $k_t$ 0.440 |
| | BC86 | BG10 + BG20 + BG30 + BG40 |
| | | Quasi-blijvend, $k_t$ 0.400 |
| | BC87 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 |
| | | Quasi-blijvend, $k_t$ 0.433 |
| | BC88 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 |
| | | Quasi-blijvend, $k_t$ 0.433 |

| | |
|---|---|
| Definitie van aanwezige bijlegwapening | Automatische ordening volgens de specificaties in tabel 1.4 |
| Controlemethode: | Berekeningsmethode: Door het aannemen van identieke vervormingsverhouding van de langswapening |
| Ontwerp van | |
| Betonspanningsberekening | ☐ |
| Scheurwijdte | ☒ |
| Lay out van de langswapening | |
| Benodigde langswapening is automatisch verhoogd voor ontwerp bruikbaarheidsgrenstoestand: | ☒ |
| DETAILS | |
| Berekeningsmethode voor wapeningsomhullende | Gemengd |
| Pas de snedekrachten toe zonder ribcomponenten | ☐ |
| Ontwerpsituatie instellingen voor bruikbaarheidsgrenstoestandcontrole | |
| Belastingscombinatie: | |
| Karakteristiek met directe belasting | Controles: $k_1$*$f_{ck}$, $k_3$*$f_{yk}$ |
| Karakteristiek met opgelegde vervorming | Controles: $k_1$*$f_{ck}$, $k_4$*$f_{yk}$ |
| Frequent | Controles: $w_k$ |
| Quasi-blijvend | Controles: $k_2$*$f_{ck}$, $w_k$, $u_l$ |

## 1.1.1 NATIONALE BIJLAGE PARAMETERS

| | | | |
|---|---|---|---|
| 2 Basis ontwerp | | | |
| 2.4.2.4 Partiï¿½le veiligheidsfactoren voor materialen | | | |
| Partiï¿½le factor voor beton in de uiterste grenstoestand (blijvend, tijdelijk) | $\gamma_c$ | 1.500 | - |
| Partiï¿½le factor voor staal in de uiterste grenstoestand (blijvend, tijdelijk) | $\gamma_s$ | 1.150 | - |
| Partiï¿½le factor voor beton in de uiterste grenstoestand (buitengewoon) | $\gamma_c$ | 1.200 | - |
| Partiï¿½le factor voor staal in de uiterste grenstoestand (buitengewoon) | $\gamma_s$ | 1.000 | - |
| Partiï¿½le factor voor beton in de bruikbaarheidsgrenstoestand | $\gamma_c$ | 1.000 | - |
| Partiï¿½le factor voor staal in de bruikbaarheidsgrenstoestand | $\gamma_s$ | 1.000 | - |
| 3. Materialen | | | |
| 3.1 Beton | | | |
| Max. waarde van sterkteklasse van beton | $C_{max}$ | C90/105 | |
| Factor voor beschouwing langetermijn acties op druksterkte | $\alpha_{cc}$ | 1.000 | - |
| Factor voor beschouwing langetermijn acties op treksterkte | $\alpha_{ct}$ | 1.000 | - |
| 3.2 Wapeningsstaal | | | |
| Max. waarde van vloeigrens | $f_{yk}$ | 600.00 | N/mm^2 |
| Factor voor berekening van de rekenwaarde voor rekgrens van staal | $k_{ud1}$ | 0.900 | - |
| 4. Duurzaamheid en betondekking | | | |
| 4.4.1 Min. betondekking | | | |
| Constructie-klasse | C.K. | S4 | |
| Aanpassing van de constructie-klasse | | | |
| Min. betondekking | | | |
| Extra veiligheid element voor verhogen van min. betondekking | $\Delta c_{dur,\gamma}$ | 0.000 | m |
| Reductie van de betondekking bij gebruik van roestvast staal | $\Delta c_{dur,st}$ | 0.000 | m |
| Reductiefactor voor de beton met extra bescherming | $\Delta c_{dur,add}$ | 0.000 | m |
| Verhoging van de deklaag onder slijtagebelasting | | | |
| Verhogingswaarde voor slijtageklasse XM1 | $k_1$ | 0.000 | m |
| Verhogingswaarde voor slijtageklasse XM2 | $k_2$ | 0.000 | m |
| Verhogingswaarde voor slijtageklasse XM3 | $k_3$ | 0.000 | m |
| Toelage in berekening voor afwijking | $\Delta c_{dev}$ | 0.005 | m |
| Verhogingswaarde voor betonnering van oneffen vlakken | | | |
| Verhogingswaarde voor grondverbetering | | | |
| Verhogingswaarde voor beton direct op de grond | | | |
| 6. Uiterste grenstoestand (UGT) | | | |
| 6.2.2. Staven zonder ontwerp afschuifwapening | | | |
| Factor $k_0$ voor berekening van de rekenwaarde voor afschuifweerstand | $k_0$ | 0.180 | - |
| Factor $k_1$ voor berekening van de rekenwaarde voor afschuifweerstand | $k_1$ | 0.150 | - |

## 1.1.1 NATIONALE BIJLAGE PARAMETERS

| | | | |
|---|---|---|---|
| Factor $k_2$ voor berekening van de rekenwaarde voor afschuifweerstand | $k_2$ | 0.035 | - |
| 6.2.3 Staven met ontwerp afschuifwapening | | | |
| Min. hoek van drukschoor | $\Theta_{min}$ | 21.801 | ï¿½ |
| Max. hoek van drukschoor | $\Theta_{max}$ | 45.000 | ï¿½ |
| Reductiefactor voor beton gescheurd door afschuiving | | | |
| Reductiefactor $k_1$ voor beton gescheurd door afschuiving | $k_1$ | 0.600 | - |
| Reductiefactor $k_2$ voor beton gescheurd door afschuiving | $k_2$ | 250.000 | - |
| Factor voor beschouwing spanningvoorwaarde in drukregel | $\alpha_{cw}$ | 1.000 | - |
| 7. Bruikbaarheidsgrenstoestand (BGT) | | | |
| 7.2 Spanningsbegrenzing | | | |
| Factor $k_1$ voor beperking van drukspanning in beton | $k_1$ | 0.600 | - |
| Factor $k_2$ voor beperking van drukspanning in beton | $k_2$ | 0.450 | - |
| 7.3 Scheurwijdtecontrole | | | |
| Begrenzing berekende scheurwijdte van gewapend beton en voorgespannen beton met VZA-spankabels | | | |
| Max. grootte van scheurwijdte voor milieuklassen X0, XC1 | $w_{max}$ | 0.400 | mm |
| Max. grootte van scheurwijdte voor milieuklasse XD1-3, XS1-3 | $w_{max}$ | 0.200 | mm |
| Factor $k_3$ voor de berekening van de max. h.o.h.-afstand scheuren | $k_3$ | 3.400 | - |
| Factor $k_4$ voor berekening van de max. h.o.h.-afstand scheuren | $k_4$ | 0.425 | - |
| 8. Detaillering van wapening en voorgespannen spanelementen - Algemeen | | | |
| 8.8 Aanvullende richtlijnen voor grote staafdiameters | | | |
| Staafdiameter | $\varnothing_{groot}$ | 32 | mm |
| 9. Detailleren van staven en bijzondere bepalingen | | | |
| 9.6 Wanden | | | |
| 9.6.2 Verticale wapening | | | |
| Min. gebied van verticale wapening $A_{s,vmin}$ | $k_1$ | 0.000 | - |
| Max. gebied van verticale wapening $A_{s,vmax}$ | $k_2$ | 0.040 | - |
| 9.6.3 Horizontale wapening | | | |
| Min. gebied van horizontale wapening $A_{s,hmin}$ d.m.v. $k_3$ | $k_3$ | 0.000 | - |
| Min. gebied van horizontale wapening $A_{s,hmin}$ d.m.v. $k_4$ | $k_4$ | 0.000 | - |
| 11. Lichtgewicht toeslag betonconstructies | | | |
| 11.3 Materialen | | | |
| Factor voor beschouwing langetermijn acties op druksterkte | $\alpha_{lcc}$ | 0.850 | - |
| Factor voor beschouwing langetermijn acties op treksterkte | $\alpha_{lct}$ | 0.850 | - |
| 11.6 Uiterste grenstoestand berekening (UGT) | | | |
| 11.6.1 Staven zonder ontwerp afschuifwapening | | | |
| Factor $k_0$ voor berekening van de rekenwaarde voor afschuifweerstand | $k_0$ | 0.150 | - |
| Factor $k_1$ voor berekening van de rekenwaarde voor afschuifweerstand | $k_1$ | 0.150 | - |
| Factor $k_2$ voor berekening van de rekenwaarde voor afschuifweerstand | $k_2$ | 0.028 | - |
| 11.6.2 Constructie-element met ontwerp afschuifwapening | | | |
| Reductiefactor $k_1$ voor beton gescheurd door afschuiving | $k_1$ | 0.500 | - |
| Reductiefactor $k_2$ voor beton gescheurd door afschuiving | $k_2$ | 250.000 | - |

## 1.2 MATERIALEN

| Mater. No. | Materiaal omschrijving | | Opm. |
|---|---|---|---|
| | Betonsterkteklasse | Staalomschrijving | |
| 2 | Beton C30/37 | B 500 S (A) | |

## 1.2.1 MATERIAAL PARAMETERS

| Mater. No. | Omschrijving | Naam | Grootte | Eenheid |
|---|---|---|---|---|
| **2** | **Betonsterkteklasse: Beton C30/37** | | | |
| | Karakteristieke cilinderdruksterkte | $f_{ck}$ | 30.00 | N/mm^2 |
| | 5 % Kwantiel van de zuivere treksterkte | $f_{ctk,0.05}$ | 2.00 | N/mm^2 |
| | Karakteristiek voor niet-lineaire berekening | | | |
| | Gem. secans elasticiteitsmodulus | $E_{cm}$ | 33000.00 | N/mm^2 |
| | Gem. cilinderdruksterkte | $f_{cm}$ | 38.00 | N/mm^2 |
| | Gem. zuivere treksterkte | $f_{ctm}$ | 2.90 | N/mm^2 |
| | Uiterste rek bij zuivere druk | $\varepsilon_{c1}$ | -2.200 | ï¿½ |
| | Uiterste rek bij bezwijken | $\varepsilon_{c1u}$ | -3.500 | ï¿½ |
| | Glijdingsmodulus | G | 13750.00 | N/mm^2 |
| | Coï¿½ff. van Poisson | $\nu$ | 0.200 | - |
| | Karakteristieke rekken voor parabolisch-rechthoekig verloop | | | |
| | Uiterste rek bij zuivere druk | $\varepsilon_{c2}$ | -2.000 | ï¿½ |
| | Uiterste rek bij bezwijken | $\varepsilon_{cu2}$ | -3.500 | ï¿½ |
| | Parabool exponent | n | 2.000 | - |
| | Volumiek gewicht | $\gamma$ | 25.00 | kN/m^3 |
| | **Wapeningsstaal: B 500 S (A)** | | | |
| | Elasticiteitsmodulus | $E_s$ | 200000.00 | N/mm^2 |
| | Gem. waarde van de vloeispanning | $f_{ym}$ | 550.00 | N/mm^2 |
| | Karakteristieke vloeispanning | $f_{yk}$ | 500.00 | N/mm^2 |
| | Gem. waarde van de treksterkte | $f_{tm}$ | 551.25 | N/mm^2 |
| | Karakteristieke treksterkte | $f_{tk}$ | 525.00 | N/mm^2 |
| | Rekgrens | $\varepsilon_{uk}$ | 25.000 | ï¿½ |

## 1.3 VLAKKEN

| Vlak No. | Mat. No. | $f_{ct,eff,wk}$ [N/mm²] | $f_{ct,eff,As,min}$ [N/mm²] | $w_{k,+z\ (bov)}$ [mm] / $w_{k,-z\ (ond)}$ [mm] | Gevolgen t.g.v. verhindering: Pas Toe | Gevolgen t.g.v. verhindering: $k_c$ [-] | Opmerkingen |
|---|---|---|---|---|---|---|---|
| 1 | Dikte Type: constant, Dikte: 150 mm | | | | | | |
| | 2 | 2.90 | 2.90 | 0.300<br>0.300 | ☒ | var. | 6) |

Opmerkingen:
6) Berekening van min. wapening voor effecten t.g.v. verhindering

## 1.4 WAPENINGSGROEPNO. 1

| | |
|---|---|
| Toegepast op vlakken: | Alle |
| WAPENINGSVERHOUDING | |
| Min. verdeelwapening | 20.0 % |
| Min. basiswapening | 0.0 % |
| Min. drukwapening | 0.0 % |
| Min. trekwapening | 0.0 % |
| Max. wapeningpercentage | 4.0 % |
| Min. afschuifwapeningpercentage | 0.0 % |
| WAPENINGSGEBIED VOOR BGT-ONTWERP | |
| Gebruik toegepaste basis wapening en benodigde bijlegwapening volgens tabellen 2.1, 2.2, 2.3 | |
| Betondekking volgens norm | ☐ |
| BASISWAPENINGLAYOUT - BOVEN (-z) | |
| Aantal wapeningsrichtingen | 2 |
| Dekking tot hart van de wapening | d-1: 30, d-2: 42 mm |
| Staaldiameter | ds-1: 12, ds-2: 12 mm |
| Wapeningsrichtingen | Phi-1: 0.000°, Phi-2: 90.000° |
| Wapeningsgebied | As-1,-z (bov): 754.000, As-2,-z (bov): 754.000 mm²/m |
| BASISWAPENINGLAYOUT - ONDER (+z) | |
| Aantal wapeningsrichtingen | 2 |
| Dekking tot hart van de wapening | d-1: 30, d-2: 42 mm |
| Staaldiameter | ds-1: 12, ds-2: 12 mm |
| Wapeningsrichtingen | Phi-1: 0.000°, Phi-2: 90.000° |
| Wapeningsgebied | As-1,+z (ond): 754.000, As-2,+z (ond): 754.000 mm²/m |
| LAYOUT BIJLEGWAPENING - BOVEN (-z) | |
| Aantal wapeningsrichtingen | 2 |
| Dekking tot hart van de wapening | d-1: 30, d-2: 40 mm |
| Staaldiameter | ds-1: 10, ds-2: 10 mm |
| Wapeningsrichtingen | Phi-1: 0.000°, Phi-2: 90.000° |
| Wapeningsgebied | Gebruik benodigde bijlegwapeninghoeveelheid volgens tabellen 2.1, 2.2, 2.3 |
| LAYOUT BIJLEGWAPENING - ONDER (+z) | |
| Aantal wapeningsrichtingen | 2 |
| Dekking tot hart van de wapening | d-1: 30, d-2: 40 mm |
| Staaldiameter | ds-1: 10, ds-2: 10 mm |
| Wapeningsrichtingen | Phi-1: 0.000°, Phi-2: 90.000° |
| Wapeningsgebied | Gebruik benodigde bijlegwapeninghoeveelheid volgens tabellen 2.1, 2.2, 2.3 |
| LANGSWAPENING VOOR AFSCHUIFKRACHTCONTROLE | |
| Gebruik benodigde hoeveelheid langswapening | |
| INSTELLINGEN VOOR NEN EN 1992-1-1+C2:2011/NB:2016-11 | |
| Min. langswapening voor platen volgens 9.3.1 | ☒ |
| Richting van min. wapening | |
| Wapeningsrichting met de hoofd trekkracht van de boven (-z) en onder (z+) vlakken, gezamenlijk: | ☒ |
| Min. langswapening voor wanden volgens hoofdstuk 9.6 | ☐ |
| Min. afschuifwapening | ☐ |
| Neutrale lijn hoogte grens | ☒ |
| Variabele betondrukdiagonaal - min | 21.801 ° |
| Variabele hellingshoek van de betonnen schoor - max | 45.000 ° |
| Partïï¿½le veiligheidsfactor $\gamma_s$ | BT 1.15, BU 1.00, BGT 1.00 |
| Partïï¿½le veiligheidsfactor $\gamma_c$ | BT 1.50, BU 1.20, BGT 1.00 |
| Beschouwing van langetermijneffecten Alpha-cc | BT 1.00, BU 1.00, BGT 1.00 |
| Beschouwing van langetermijn effecten Alpha-ct | BGT 1.00 |

## 2.1 BENODIGDE TOTALE WAPENING

| Vlak | Punt | Puntcoï¿½rdinaten [m] | | | | Benodigde Wapening | | | Basis | Bijlegwapening | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| No. | No. | X | Y | Z | Symbool | UGT | BGT | UGT/BGT | Wap. | Benodigd | Toegepast | Eenheid | Opmerkin |
| 1 | G125 | 1.800 | -0.200 | 0.000 | $a_{s,1,-z\ (bov)}$ | 17.795 | 626.445 | 626.445 | 754.000 | 0.000 | 0.000 | mm²/m | |
| 1 | G123 | 0.800 | -0.200 | 0.000 | $a_{s,2,-z\ (bov)}$ | 2.646 | 781.098 | 781.098 | 754.000 | 27.098 | 27.098 | mm²/m | |
| 1 | G109 | 1.300 | 0.300 | 0.000 | $a_{s,1,+z\ (ond)}$ | 33.640 | 661.584 | 661.584 | 754.000 | 0.000 | 0.000 | mm²/m | |
| 1 | G124 | 1.300 | -0.200 | 0.000 | $a_{s,2,+z\ (ond)}$ | 5.836 | 804.953 | 804.953 | 754.000 | 50.953 | 50.953 | mm²/m | |
| 1 | G1 | -0.200 | 3.800 | 0.000 | $a_{sw}$ | 0.000 | - | 0.000 | - | - | - | mm²/m² | |

## 3.1 BRUIKBAARHEID TOTAAL

| Vlak | Punt | Puntcoï¿½rdinaten [m] | | | BG | Controle | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| No. | No. | X | Y | Z | geval | type | Aanw. waarde | Grenswaarde | Eenheid | Unity check | Opmerkinge |
| 1 | G120 | 6.800 | 0.300 | 0.000 | Omhullende F | $a_{s,min}$ | 758.637 | 758.373 | mm²/m | 1.0 | |
| 1 | G61 | -0.200 | 1.800 | 0.000 | Omhullende F | $w_k$ | 0.101 | 0.300 | mm | 0.4 | |

**RF-CONCRETE Members**
BG1
Ontwerp van betonnen staven

## 1.1 ALGEMENE GEGEVENS

| | | |
|---|---|---|
| Ontwerp volgens norm: | NEN EN 1992-1-1+C2:2011/NB:2016-11 | |
| UITERSTE GRENSTOESTAND | | |
| Te ontwerpen belastingscombinaties: | BC1 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 |
| | | Blijvend en tijdelijk |
| | BC2 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG100 |

## 1.1 ALGEMENE GEGEVENS

| | |
|---|---|
| | Blijvend en tijdelijk |
| BC3 | 1.49*BG10 + 1.49*BG20 + 1.49*BG30 + 1.49*BG40 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC4 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 |
| | Blijvend en tijdelijk |
| BC5 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 |
| | Blijvend en tijdelijk |
| BC6 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC7 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 |
| | Blijvend en tijdelijk |
| BC8 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC9 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 |
| | Blijvend en tijdelijk |
| BC10 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG120 |
| | Blijvend en tijdelijk |
| BC11 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG120 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC12 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC13 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC14 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC15 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC16 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC17 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC18 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC19 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC20 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC21 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC22 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG100 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC23 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC24 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC25 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC26 | 1.32*BG10 + 1.32*BG20 + 1.32*BG30 + 1.32*BG40 + 1.65*BG150 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC27 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 |
| | Blijvend en tijdelijk |
| BC28 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG120 |
| | Blijvend en tijdelijk |
| BC29 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG120 + 1.65*BG150 |
| | Blijvend en tijdelijk |
| BC30 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC31 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC32 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG300 |
| | Blijvend en tijdelijk |
| BC33 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC34 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC35 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC36 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG404 |
| | Blijvend en tijdelijk |
| BC37 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG401 |
| | Blijvend en tijdelijk |
| BC38 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG402 |
| | Blijvend en tijdelijk |
| BC39 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG403 |
| | Blijvend en tijdelijk |
| BC40 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG100 + 1.65*BG404 |
| | Blijvend en tijdelijk |

## 1.1 ALGEMENE GEGEVENS

| | | |
|---|---|---|
| | BC41 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG401 |
| | | Blijvend en tijdelijk |
| | BC42 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG402 |
| | | Blijvend en tijdelijk |
| | BC43 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG403 |
| | | Blijvend en tijdelijk |
| | BC44 | 0.9*BG10 + 0.9*BG20 + 0.9*BG30 + 0.9*BG40 + 1.65*BG150 + 1.65*BG404 |
| | | Blijvend en tijdelijk |
| BRUIKBAARHEIDSGRENSTOESTANDEN | | |
| Te ontwerpen belastingscombinaties: | BC45 | BG10 + BG20 + BG30 + BG40 |
| | | Karakteristiek met directe belasting, k-t: 0.600 |
| | BC46 | BG10 + BG20 + BG30 + BG40 + BG100 |
| | | Karakteristiek met directe belasting, k-t: 0.440 |
| | BC47 | BG10 + BG20 + BG30 + BG40 + BG150 |
| | | Karakteristiek met directe belasting, k-t: 0.440 |
| | BC48 | BG10 + BG20 + BG30 + BG40 + BG120 |
| | | Karakteristiek met directe belasting, k-t: 0.440 |
| | BC49 | BG10 + BG20 + BG30 + BG40 + BG100 + BG120 |
| | | Karakteristiek met directe belasting, k-t: 0.467 |
| | BC50 | BG10 + BG20 + BG30 + BG40 + BG120 + BG150 |
| | | Karakteristiek met directe belasting, k-t: 0.467 |
| | BC51 | BG10 + BG20 + BG30 + BG40 + BG300 |
| | | Karakteristiek met directe belasting, k-t: 0.440 |
| | BC52 | BG10 + BG20 + BG30 + BG40 + BG100 + BG300 |
| | | Karakteristiek met directe belasting, k-t: 0.467 |
| | BC53 | BG10 + BG20 + BG30 + BG40 + BG150 + BG300 |
| | | Karakteristiek met directe belasting, k-t: 0.467 |
| | BC54 | BG10 + BG20 + BG30 + BG40 + BG401 |
| | | Karakteristiek met directe belasting, k-t: 0.440 |
| | BC55 | BG10 + BG20 + BG30 + BG40 + BG402 |
| | | Karakteristiek met directe belasting, k-t: 0.440 |
| | BC56 | BG10 + BG20 + BG30 + BG40 + BG403 |
| | | Karakteristiek met directe belasting, k-t: 0.440 |
| | BC57 | BG10 + BG20 + BG30 + BG40 + BG404 |
| | | Karakteristiek met directe belasting, k-t: 0.440 |
| | BC58 | BG10 + BG20 + BG30 + BG40 + BG100 + BG401 |
| | | Karakteristiek met directe belasting, k-t: 0.467 |
| | BC59 | BG10 + BG20 + BG30 + BG40 + BG100 + BG402 |
| | | Karakteristiek met directe belasting, k-t: 0.467 |
| | BC60 | BG10 + BG20 + BG30 + BG40 + BG100 + BG403 |
| | | Karakteristiek met directe belasting, k-t: 0.467 |
| | BC61 | BG10 + BG20 + BG30 + BG40 + BG100 + BG404 |
| | | Karakteristiek met directe belasting, k-t: 0.467 |
| | BC62 | BG10 + BG20 + BG30 + BG40 + BG150 + BG401 |
| | | Karakteristiek met directe belasting, k-t: 0.467 |
| | BC63 | BG10 + BG20 + BG30 + BG40 + BG150 + BG402 |
| | | Karakteristiek met directe belasting, k-t: 0.467 |
| | BC64 | BG10 + BG20 + BG30 + BG40 + BG150 + BG403 |
| | | Karakteristiek met directe belasting, k-t: 0.467 |
| | BC65 | BG10 + BG20 + BG30 + BG40 + BG150 + BG404 |
| | | Karakteristiek met directe belasting, k-t: 0.467 |
| | BC66 | BG10 + BG20 + BG30 + BG40 |
| | | Frequent, k-t: 0.400 |
| | BC67 | BG10 + BG20 + BG30 + BG40 + 0.9*BG100 |
| | | Frequent, k-t: 0.437 |
| | BC68 | BG10 + BG20 + BG30 + BG40 + 0.9*BG150 |
| | | Frequent, k-t: 0.437 |
| | BC69 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0*BG120 |
| | | Frequent, k-t: 0.433 |
| | BC70 | BG10 + BG20 + BG30 + BG40 + 0*BG120 + 0.8*BG150 |
| | | Frequent, k-t: 0.433 |
| | BC71 | BG10 + BG20 + BG30 + BG40 + 0.2*BG300 |
| | | Frequent, k-t: 0.410 |
| | BC72 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG300 |
| | | Frequent, k-t: 0.440 |
| | BC73 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG300 |
| | | Frequent, k-t: 0.440 |
| | BC74 | BG10 + BG20 + BG30 + BG40 + 0.2*BG401 |
| | | Frequent, k-t: 0.410 |
| | BC75 | BG10 + BG20 + BG30 + BG40 + 0.2*BG402 |
| | | Frequent, k-t: 0.410 |
| | BC76 | BG10 + BG20 + BG30 + BG40 + 0.2*BG403 |
| | | Frequent, k-t: 0.410 |
| | BC77 | BG10 + BG20 + BG30 + BG40 + 0.2*BG404 |
| | | Frequent, k-t: 0.410 |
| | BC78 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG401 |
| | | Frequent, k-t: 0.440 |
| | BC79 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG402 |
| | | Frequent, k-t: 0.440 |
| | BC80 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG403 |
| | | Frequent, k-t: 0.440 |
| | BC81 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 + 0.2*BG404 |
| | | Frequent, k-t: 0.440 |
| | BC82 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG401 |
| | | Frequent, k-t: 0.440 |
| | BC83 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG402 |
| | | Frequent, k-t: 0.440 |
| | BC84 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG403 |
| | | Frequent, k-t: 0.440 |
| | BC85 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 + 0.2*BG404 |
| | | Frequent, k-t: 0.440 |
| | BC86 | BG10 + BG20 + BG30 + BG40 |

## 1.1 ALGEMENE GEGEVENS

| | | |
|---|---|---|
| | | Quasi-blijvend, k-t: 0.400 |
| | BC87 | BG10 + BG20 + BG30 + BG40 + 0.8*BG100 |
| | | Quasi-blijvend, k-t: 0.433 |
| | BC88 | BG10 + BG20 + BG30 + BG40 + 0.8*BG150 |
| | | Quasi-blijvend, k-t: 0.433 |
| Ontwerpsituatie instellingen voor bruikbaarheidsgrenstoestandcontrole | | |
| Belastingscombinatie: | | |
| Karakteristiek met directe belasting | Controles: $k_1*f_{ck}$, $k_3*f_{yk}$ | |
| Karakteristiek met opgelegde vervorming | Controles: $k_1*f_{ck}$, $k_4*f_{yk}$ | |
| Frequent | Controles: $w_k$ | |
| Quasi-blijvend | Controles: $k_2*f_{ck}$, $w_k$, $u_l$ | |
| Vervormingen relatief t.o.v.: | Onvervormd systeem | |

## 1.1 INSTELLINGEN - NIET-LINEAIRE BEREKENING

| | |
|---|---|
| Activeer niet-lineaire berekening voor UITERSTE GRENSTOESTAND: | ☐ |
| Activeer niet-lineaire berekening voor BRUIKBAARHEIDSGRENSTOESTAND: | ☐ |
| Zet niet-lineaire berekening aan | ☐ |

## 1.2 MATERIALEN

| Mat. No. | Materiaalomschrijving Betonkwaliteit | Wapeningskwaliteit | Opm. |
|---|---|---|---|
| 2 | Beton C30/37 | B 500 S (A) | |

## 1.2.1 MATERIAAL PARAMETERS

| Mat. No. | Omschrijving | Naam | Grootte | Eenheid |
|---|---|---|---|---|
| **2** | **Betonkwaliteit: Beton C30/37** | | | |
| | Karakteristieke cilinderdruksterkte | $f_{ck}$ | 30.000 | N/mm^2 |
| | Gem. cilinderdruksterkte | $f_{cm}$ | 38.000 | N/mm^2 |
| | Gem. zuivere treksterkte | $f_{ctm}$ | 2.900 | N/mm^2 |
| | 5 % Fractie van de zuivere treksterkte | $f_{ctk,005}$ | 2.000 | N/mm^2 |
| | 95 % Fractie van de zuivere treksterkte | $f_{ctk,0.95}$ | 3.800 | N/mm^2 |
| | Gem. secans elasticiteitsmodulus | $E_{cm}$ | 33000.000 | N/mm^2 |
| | Karakteristieke rekken voor niet-lineaire berekeningen | | | |
| | Uiterste betonstuik bij zuivere druk | $\varepsilon_{c1}$ | -2.200 | ‰ |
| | Uiterste rek bij bezwijken | $\varepsilon_{cu1}$ | -3.500 | ‰ |
| | Karakteristieke rekken voor parabolisch-rechthoekig verloop | | | |
| | Uiterste betonstuik bij zuivere druk | $\varepsilon_{c2}$ | -2.000 | ‰ |
| | Uiterste rek bij bezwijken | $\varepsilon_{cu2}$ | -3.500 | ‰ |
| | Exponent van Parabool | n | 2 | |
| | Vol. gewicht | $\gamma$ | 25.00 | kN/m^3 |
| | **Wapeningskwaliteit: B 500 S (A)** | | | |
| | Elasticiteitsmodulus | $E_s$ | 200000 | N/mm^2 |
| | Karakteristieke waarde van de vloeispanning | $f_{yk}$ | 500 | N/mm^2 |
| | Karakteristieke Waarde van de Trekvastheid | $f_{tk}$ | 525 | N/mm^2 |
| | Rekgrens | $\varepsilon_{uk}$ | 25.000 | ‰ |

Rechthoek 400/650

## 1.3 DOORSNEDES

| Snede No. | Mat. No. | Doorsnede Omschrijving | Opmerkingen | Opm. |
|---|---|---|---|---|
| 6 | 2 | Rechthoek 400/650 | | Randbalk beton |

VLU 800/0/0/150/0...

## 1.4 RIBBEN

| Staaf No. | Doorsnede No. Begin | Eind | Effectieve breedte Vlak No. | b-1 [mm] | Vlak. No | b-2 [mm] | Opmerkingen |
|---|---|---|---|---|---|---|---|
| 22 | 6 | 6 | 1 | 200 | | | |
| 23 | 6 | 6 | 1 | 200 | | | |
| 24 | 6 | 6 | 1 | 200 | | | |
| 25 | 6 | 6 | 1 | 200 | | | |

**RF-CONCRETE Members**
BG1
Ontwerp van betonnen staven

## 1.6 WAPENINGGROEP NO. 1

| | |
|---|---|
| Toegepast op staven: | 22-25 |
| LANGSWAPENING | |
| Beschikbare diameters: | 12.0, 16.0 mm |
| Max. aantal lagen: | 1 |
| Min. h.o.h.-afstand voor 1e laag: | 20.0 mm |
| Type verankering: | Recht |
| Oppervlak: | Geribd |
| Reductie van wapening: | Geen |
| AFSCHUIFWAPENING | |
| Beschikbare diameters: | 10.0 mm |

## 1.6 WAPENINGGROEP NO. 1

| | |
|---|---|
| Aantal beugelbenen: | 2 |
| Hoek: | 90° |
| Type verankering: | Bocht |
| Beugel layout: | |
| | |
| LAY-OUT WAPENING | |
| Betondekking volgens norm | ☐ |
| Betondekking c-boven: | 30.0 mm |
| Betondekking $c_{onder}$: | 30.0 mm |
| Betondekking $c_{flank}$ | 30.0 mm |
| Lay-out wapening: | -z (bov) - +z (ond) (geoptimaliseerde verdeling) |
| Over complete breedte van de doorsnede: | ☒ |
| Wringwapening verdeeld over de omtrek: | ☒ |
| Relevante snedekrachten: | N, V-y, V-z, M-T, M-y, M-z |
| | |
| MIN. WAPENING | |
| Min. wapeningsoppervlak (min. A-s,boven): | 0.00 $mm^2$ |
| Min. wapeningsoppervlak (min. A-s,onder): | 0.00 $mm^2$ |
| Min. langswapening volgens norm: | ☒ |
| Min. afschuifwapening volgens norm: | ☒ |
| Langswapening voor dwarskrachtontwerp: | Gebruik theoretische langswapening |
| | |
| AFSCHUIF VERBINDING | |
| Afschuifverbinding beschikbaar: | ☐ |
| Ontwerp van flensverbindingen bij opgesplitste doorsnedes | ☐ |
| | |
| INSTELLINGEN VOOR EN 1992-1-1:2004/A1:2014 | |
| Max. wapeningspercentage: | 8.00 % |
| Hoogte beperking neutrale lijn | ☒ |
| Partïï¿½le veiligheidsfactor gamma-c | BT 1.50, BU 1.20, BGT 1.00 |
| Partïï¿½le veiligheidsfactor Gamma-s | BT 1.15, BU 1.00, BGT 1.00 |
| Reductiefactor Alpha-cc | BT 1.00, BU 1.00, BGT 1.00 |
| Reductiefactor Alpha-ct | BT 1.00, BU 1.00, BGT 1.00 |
| Min. hellingshoek van de betonschoor | 21.80 ° |
| Max. hellingshoek van de betonschoor | 45.00 ° |
| | |
| BRUIKBAARHEID | |
| Scheurwijdte berekening | |
| Grenswaarde van toelaatbare scheurwijdte $w_{k,max,-z\ (bov)}$: | 0.3 mm |
| Grenswaarde van toelaatbare scheurwijdte $w_{k,max,+z\ (ond)}$: | 0.3 mm |
| Ontwerp zonder directe scheurwijdte berekening: | ☒ |
| Berekening van grensdiameter grens $d_s$: | ☒ |
| Berekening van max. h.o.h.-afstand van de staven grens $s_l$: | ☒ |
| Ontwerp met directe scheurwijdteberekening: | ☒ |
| Gebruik verg. (7.14) voor $s_{r,\ max}$: | ☐ |
| Werkzame betontreksterkte op het tijdstip van scheuren: | 1.000 * $f_{ctm}$ |
| $A_{s,min}$ voor effecten t.g.v. verhindering : | ☒ |
| Spanningsverdeling in het profiel voor scheuren: | Afhankelijk van de gedefinieerde belasting ($k_c$ = 0.0 ... 1.0) |
| $A_{s,min}$ Lay-out: | -z (bov) /+z (ond) |
| Scheurformatie binnen de eerste 28 dagen: | ☐ |
| Spanningsberekening | |
| Begrenzing van de betondrukspanning $\sigma_c$: | ☐ |
| Doorbuigingsberekening | |
| Doorbuiging $u_{l,z}$: | ☐ |
| Bepaling van langswapening | |
| Verhoog de vereiste langswapening automatisch voor ontwerp bruikbaarheidsgrenstoestand : | ☒ |
| Vind de meest economische wapening voor scheurwijdte-ontwerp: | ☒ |
| Beschouw A _s,min volgens 7.3.2 ook voor de directe berekening scheurwijdte volgens 7.3.4: | ☒ |

## 2.3 BENODIGDE WAPENING PER STAAF

| Wapening | Staaf No. | Locatie x [m] | Belasting | Wapening Oppervl. | Eenheid | Foutboodschap of opmerking |
|---|---|---|---|---|---|---|
| Staaf No. 22 - Rib VLU 800/0/0/150/0/400 | | | | | | |
| $A_{s,z}$ | 22 | 0.583 | BC40 | 839.87 | $mm^2$ | 25) 28) |
| $A_{s,+z}$ | 22 | 0.583 | BC40 | 839.87 | $mm^2$ | 25) 29) |
| $A_{s,T}$ | 22 | 1.556 | BC24 | 228.62 | $mm^2$ | |
| $a_{sw,V,bgl}$ | 22 | 0.000 | BC25 | 350.54 | $mm^2/m$ | 58) 69) |
| $a_{sw,T,beugel}$ | 22 | 1.556 | BC24 | 19.59 | $mm^2/m$ | |
| Staaf No. 23 - Rib VLU 800/0/0/150/0/400 | | | | | | |
| $A_{s,z}$ | 23 | 2.917 | BC40 | 683.18 | $mm^2$ | 25) 28) |
| $A_{s,+z}$ | 23 | 2.917 | BC40 | 683.18 | $mm^2$ | 25) 29) |
| $A_{s,T}$ | 23 | 1.944 | BC23 | 191.36 | $mm^2$ | |
| $a_{sw,V,bgl}$ | 23 | 0.000 | BC13 | 350.54 | $mm^2/m$ | 58) 69) |
| $a_{sw,T,beugel}$ | 23 | 1.944 | BC23 | 16.40 | $mm^2/m$ | |
| Staaf No. 24 - Rib VLU 800/0/0/150/0/400 | | | | | | |
| $A_{s,z}$ | 24 | 2.139 | BC39 | 662.20 | $mm^2$ | 25) 28) |
| $A_{s,+z}$ | 24 | 2.139 | BC39 | 662.20 | $mm^2$ | 25) 29) |
| $A_{s,T}$ | 24 | 1.556 | BC24 | 266.70 | $mm^2$ | |
| $a_{sw,V,bgl}$ | 24 | 0.000 | BC26 | 350.54 | $mm^2/m$ | 58) 69) |
| $a_{sw,T,beugel}$ | 24 | 1.556 | BC24 | 22.86 | $mm^2/m$ | |
| Staaf No. 25 - Rib VLU 800/0/0/150/0/400 | | | | | | |
| $A_{s,z}$ | 25 | 1.361 | BC39 | 645.41 | $mm^2$ | 25) 28) |
| $A_{s,+z}$ | 25 | 1.361 | BC39 | 645.41 | $mm^2$ | 25) 29) |
| $A_{s,T}$ | 25 | 1.944 | BC23 | 255.07 | $mm^2$ | |
| $a_{sw,V,bgl}$ | 25 | 0.000 | BC13 | 350.54 | $mm^2/m$ | 58) 69) |
| $a_{sw,T,beugel}$ | 25 | 1.944 | BC23 | 21.86 | $mm^2/m$ | |

## 3.1 TOEGEPASTE LANGSWAPENING

| Onderde No. | Wapening Positie | Aant. Wap. st | $d_s$ [mm] | $A_s$ [cm$^2$] | Lengte [m] | x-positie [m] van | x-positie [m] tot | Gewicht [kg] | Opm. |
|---|---|---|---|---|---|---|---|---|---|
| Staaf No.22 - Rib VLU 800/0/0/150/0/400 | | | | | | | | | |
| 1 | Basis -z (bov) | 3 | 16.0 | 603.19 | 3.820 | -0.160 | 3.660 | 18.09 | |
| 2 | -z (bov) | 4 | 12.0 | 452.39 | 3.740 | -0.120 | 3.620 | 13.28 | |
| 3 | Basis +z (ond) | 3 | 16.0 | 603.19 | 3.820 | -0.160 | 3.660 | 18.09 | |
| 4 | +z (ond) | 4 | 12.0 | 452.39 | 3.740 | -0.120 | 3.620 | 13.28 | |
| 5 | +-y(zijde) | 4 | 12.0 | 452.39 | 3.740 | -0.120 | 3.620 | 13.28 | 158) |
| Staaf No.23 - Rib VLU 800/0/0/150/0/400 | | | | | | | | | |
| 1 | Basis -z (bov) | 3 | 16.0 | 603.19 | 3.820 | -0.160 | 3.660 | 18.09 | |
| 2 | -z (bov) | 2 | 12.0 | 226.19 | 3.740 | -0.120 | 3.620 | 6.64 | |
| 3 | Basis +z (ond) | 3 | 16.0 | 603.19 | 3.820 | -0.160 | 3.660 | 18.09 | |
| 4 | +z (ond) | 2 | 12.0 | 226.19 | 3.740 | -0.120 | 3.620 | 6.64 | |
| 5 | +-y(zijde) | 4 | 12.0 | 452.39 | 3.740 | -0.120 | 3.620 | 13.28 | 158) |
| Staaf No.24 - Rib VLU 800/0/0/150/0/400 | | | | | | | | | |
| 1 | Basis -z (bov) | 3 | 16.0 | 603.19 | 3.820 | -0.160 | 3.660 | 18.09 | |
| 2 | -z (bov) | 2 | 12.0 | 226.19 | 3.740 | -0.120 | 3.620 | 6.64 | |
| 3 | Basis +z (ond) | 3 | 16.0 | 603.19 | 3.820 | -0.160 | 3.660 | 18.09 | |
| 4 | +z (ond) | 2 | 12.0 | 226.19 | 3.740 | -0.120 | 3.620 | 6.64 | |
| 5 | +-y(zijde) | 4 | 12.0 | 452.39 | 3.740 | -0.120 | 3.620 | 13.28 | 158) |
| Staaf No.25 - Rib VLU 800/0/0/150/0/400 | | | | | | | | | |
| 1 | Basis -z (bov) | 3 | 16.0 | 603.19 | 3.820 | -0.160 | 3.660 | 18.09 | |
| 2 | -z (bov) | 2 | 12.0 | 226.19 | 3.740 | -0.120 | 3.620 | 6.64 | |
| 3 | Basis +z (ond) | 3 | 16.0 | 603.19 | 3.820 | -0.160 | 3.660 | 18.09 | |
| 4 | +z (ond) | 2 | 12.0 | 226.19 | 3.740 | -0.120 | 3.620 | 6.64 | |
| 5 | +-y(zijde) | 4 | 12.0 | 452.39 | 3.740 | -0.120 | 3.620 | 13.28 | 158) |

## 3.2 TOEGEPASTE AFSCHUIFWAPENING

| Onderde No. | Aant. Beugel | $d_s$ [mm] | Lengte [m] | x-positie [m] van | x-positie [m] tot | h.o.h.-afst $s_{li}$ [m] | Maatvoering beugel [mm] | Aant. Benen | Gewicht [kg] | Opm. |
|---|---|---|---|---|---|---|---|---|---|---|
| Staaf No. 22 - Rib VLU 800/0/0/150/0/400 | | | | | | | | | | |
| 1 | 18 | 10.0 | 3.400 | 0.000 | 3.400 | 0.200 | 760.0/360.0/139.3 | 2 | 27.95 | 113) |
| 2 | 1 | 10.0 | 0.100 | 3.400 | 3.500 | 0.100 | 760.0/360.0/139.3 | 2 | 1.55 | 113) |
| Staaf No. 23 - Rib VLU 800/0/0/150/0/400 | | | | | | | | | | |
| 3 | 18 | 10.0 | 3.400 | 0.000 | 3.400 | 0.200 | 760.0/360.0/139.3 | 2 | 27.95 | 113) |
| 4 | 1 | 10.0 | 0.100 | 3.400 | 3.500 | 0.100 | 760.0/360.0/139.3 | 2 | 1.55 | 113) |
| Staaf No. 24 - Rib VLU 800/0/0/150/0/400 | | | | | | | | | | |
| 5 | 18 | 10.0 | 3.400 | 0.000 | 3.400 | 0.200 | 760.0/360.0/139.3 | 2 | 27.95 | 113) |
| 6 | 1 | 10.0 | 0.100 | 3.400 | 3.500 | 0.100 | 760.0/360.0/139.3 | 2 | 1.55 | 113) |
| Staaf No. 25 - Rib VLU 800/0/0/150/0/400 | | | | | | | | | | |
| 7 | 18 | 10.0 | 3.400 | 0.000 | 3.400 | 0.200 | 760.0/360.0/139.3 | 2 | 27.95 | 113) |
| 8 | 1 | 10.0 | 0.100 | 3.400 | 3.500 | 0.100 | 760.0/360.0/139.3 | 2 | 1.55 | 113) |

## 4.1 BRUIKBAARHEIDSCONTROLE PER DOORSNEDE

| Prof. No. | Locatie x [m] | Belasting | Ontwerp Type | Aanwezige waar | Grenswaarde | Eenheid | Capaciteit | Opm. |
|---|---|---|---|---|---|---|---|---|
| Doorsnede No.6 - Rechthoek 400/650 | | | | | | | | |
| 22 | 0.583 | BC77 | $A_{s,min}$ | 1281.77 | 839.87 | mm$^2$ | 0.66 | |
| 22 | 0.000 | BC66 | lim $d_s$ | 13.6 | - | mm | 0.00 | |
| 22 | 0.000 | BC66 | max wap afstand | 0.073 | - | m | 0.01 | |
| 22 | 0.000 | BC66 | $w_k$ | 0.000 | 0.300 | mm | 0.00 | 207) |

## OPM.

| No. | Omschrijving |
|---|---|
| 13) | Symmetrische wapening voor dubbele buiging |
| 25) | Min. wapening voor drukwapening volgens 9.5.2(2) |
| 28) | Bovenwapening is verhoogd t.g.v. BGT-eis |
| 29) | Onderwapening is verhoogd t.g.v. BGT-eis |
| 58) | Gebruik maken van de gemiddelde waarde van hefboom z |
| 69) | Min. afschuifwapening volgens 9.2.2.(5) |
| 113) | Min. afschuifwapening voor drukstaven volgens 9.5.3 |
| 158) | Wringwapening verdeeld over de omtrek |
| 207) | Scheurwijdte direct verhinderd (passend) |

## 1.1 GLOBALE GEGEVENS

| | | |
|---|---|---|
| Activiteiten | | ☒ Modale berekening (eigenvectoren)<br>☒ Massa-combinaties<br>☐ Opgelegde trillingen<br>☐ Responsspectra<br>☐ Accelerogrammen<br>☐ Tijddiagrammen<br>☒ Equivalente statische kracht berekening |
| Instelling | Zwaartekrachtversnelling | : 10.00 m/s² |

## 1.2.1 MASSA-GEVAL - ALGEMEEN

| No. | Beschrijving massa-geval | Parameters | |
|---|---|---|---|
| MG1 | PB: BG10+BG20+BG30+BG40 | Type massa-geval<br>Massa's | : Blijvend<br>☒ : Vanuit kracht componenten van Belastingscombinatie BC45 |
| MG7 | VB: BG150 | Type massa-geval<br>Massa's | : Opgelegd - categorie E<br>☒ : Vanuit kracht componenten van Belastingsgeval BG150-VB: Heftruck |

## 1.3.1 MASSA-COMBINATIES - ALGEMEEN

| No. | Beschrijving massa-combinatie | Parameters | | |
|---|---|---|---|---|
| MC1 | Massa Combinatie | Massa-gevallen | : 1.00 | MG1 - PB: BG10+BG20+BG30+BG40 |
| | | | 0.80 | MG7 - VB: BG150 |
| | | Commentaar | : | |

## 1.4.1 NATUURLIJK TRILLINGSGEVAL - ALGEMEEN

| EWG Geval | Eigentrillingsgeval beschrijving | Parameters | |
|---|---|---|---|
| EWG1 | Natuurlijke trillingsgevallen | Aantal van kleinste eigenwaardes<br>Inwerkende massa's<br>Massa's beschouwd in | : 10<br>: MC1 - Massa Combinatie<br>: ☒ X-richting<br>☒ Y-richting |

## 1.4.2. NATUURLIJK TRILLINGSGEVAL - BEREKENING PARAMTERS

| EWG Geval | Eigentrillingsgeval beschrijving | Berekeningsparameters | |
|---|---|---|---|
| EWG1 | Natuurlijke trillingsgevallen | Type massamatrix:<br>Schalen van trillingseigenvormen<br>Oplossingsmethode voor eigenwaardes | : Diagonale matrix (translatie DOFs)<br>: Max $\{u_i\}$ = 1<br>: Lanczos |

## 1.5.1 RESPONSE SPECTRA - ALGEMEEN

| RS Geval | Responsspectra beschrijving | Definitie-type | Commentaar |
|---|---|---|---|
| RS1 | Responsspectra | Volgens norm:<br>EN 1998-1:2010 - Europese Unie<br>Nationale Bijlage:<br>NBN - Belgiï¿½ | |

## 1.5.2 RESPONSSPECTRA - NORMPARAMETERS

| No. | Responsspectrum beschrijving | Massa-geval parameters | | |
|---|---|---|---|---|
| RS1 | Responsspectra | Type spectrum | | |
| | | Type spectrum | | : Ontwerp spectrum voor lineaire berekening |
| | | Type spectrum | | : 2 |
| | | Spectrumrichting | | : Horizontaal spectrum |
| | | Aardbevingsactie | | |
| | | Piekwaarde grondversnelling | PGA | : 0.150 |
| | | Referentie piek-grondversnelling | $a_{gR}$ | : 1.0500 |
| | | Belangcategorie | | : III |
| | | Belangfactor | $\gamma_I$ | : 1.2000 |
| | | Ontwerp grondversnelling | $a_g$ | : 1.2600 |
| | | Parameter voor de omschrijving van het responsspectrum | | |
| | | Bodemtype | | : D |
| | | Bodemfactor | S | : 1.8000 |
| | | Ondergrens van vlak van constante spectrale versnelling (horizontaal) | $T_{B-H}$ | : 0.1000 |
| | | Bovengrens van vlak van constante spectrale versnelling (horizontaal) | $T_{C-H}$ | : 0.3000 |
| | | Waarde definieert het begin van het vlak van constante spectrum verplaatsingen (horizontaal) | $T_{D-H}$ | : 1.2000 |
| | | Factoren | | |

## 1.5.2 RESPONSSPECTRA - NORMPARAMETERS

| No. | Responsspectrum beschrijving | Massa-geval parameters | | | |
|---|---|---|---|---|---|
| | | Gedragsfactor | q | : | 1.5000 |
| | | Grenswaarde voor horizontale ontwerp spectrum | β | : | 0.2000 |

## 1.5.3.1 RESPONSSPECTRA - GRAFIEK

RS1


## 1.8.1 DYNAMISCHE BELASTINGSGEVAL - ALGEMEEN

| DBG Geval | Dynamische belastingsgevallen beschrijving | Parameters | | |
|---|---|---|---|---|
| DBG1 | Dynamische Belastingsgeval | Type methode | : | Equivalente statische kracht berekening (responsspectrum vereist) |
| | | Natuurlijke trilling toewijzen | : | Eigentrillingsgeval: Natuurlijke trillingsgevallen |

## 1.8.5.1 DYNAMISCHE BELASTINGSGEVALLEN - EQUIVALENTE STATISCHE KRACHT BEREKENING

| DBG Geval | Dynamische belastingsgevallen beschrijving | Parameters |
|---|---|---|
| DBG1 | Dynamische Belastingsgeval | Reactiespectrum toewijzen:<br><br>Responsspectrum in richting — Vergrotingsfactor<br>☒ x: RS1 - Responsspectra — 1.000<br>☒ y: RS1 - Responsspectra — 1.000<br><br>Roteer $a_X$ $a_Y$ om Z: — $\alpha$ = 0.00 [°] |
| | | Instellingen:<br><br>☐ Beschouw buitengewone torsie acties: |
| | | Te genereren:<br><br>☒ Belastingsgeval met $E_{X,i}$ / $E_{Z,i}$ vanuit alle modale vormen<br>Nummer van eerst gegenereerd belastingsgeval: 800<br>☒ Resultaatcombinaties(modale combinatie)<br>Aantal van eerst gegenereerde resultaat combinatie: 10<br>☒ Combinatie van richtingscomponenten met<br>☐ SRSS<br>☒ 100 / 30 %<br>☐ 100 / 40 % |
| | | Combinatie regels:<br><br>Combinatieregel modale respons:<br>☒ SRSS<br>☐ CQC<br><br>Opties<br>☒ Gebruik equivalente lineaire combinatie<br><br>☐ Gemerkte resultaten m.b.v. dominante modus |

## 1.8.5.2 DYNAMISCHE BELASTINGSGEVALLEN - EQUIVALENT STATISCHE KRACHT BEREKENING- TE GENEREREN EIGENVORMEN

| DBG Geval | Dynamische belastingsgevallen beschrijving | Vorm No. | Te generer | Nat. frequentie ω [rad/s] | Nat. frequentie f [Hz] | Periode T [s] | Versnelling $S_a$ [m/s²] |
|---|---|---|---|---|---|---|---|
| DBG1 | Dynamische Belastingsgeval | 1 | ☒ | 13.795 | 2.196 | 0.455 | 2.490 |
| | | 2 | ☒ | 20.406 | 3.248 | 0.308 | 3.683 |
| | | 3 | ☐ | 23.521 | 3.743 | 0.267 | 3.780 |
| | | 4 | ☒ | 25.046 | 3.986 | 0.251 | 3.780 |
| | | 5 | ☒ | 27.052 | 4.305 | 0.232 | 3.780 |
| | | 6 | ☐ | 28.897 | 4.599 | 0.217 | 3.780 |
| | | 7 | ☒ | 29.626 | 4.715 | 0.212 | 3.780 |
| | | 8 | ☐ | 43.711 | 6.957 | 0.144 | 3.780 |
| | | 9 | ☐ | 55.429 | 8.822 | 0.113 | 3.780 |
| | | 10 | ☐ | 59.660 | 9.495 | 0.105 | 3.780 |

**EWG1**
Natuurlijke trillingsgevallen

## 5.7 EFFECTIEVE MODALEMASSAFACTOREN

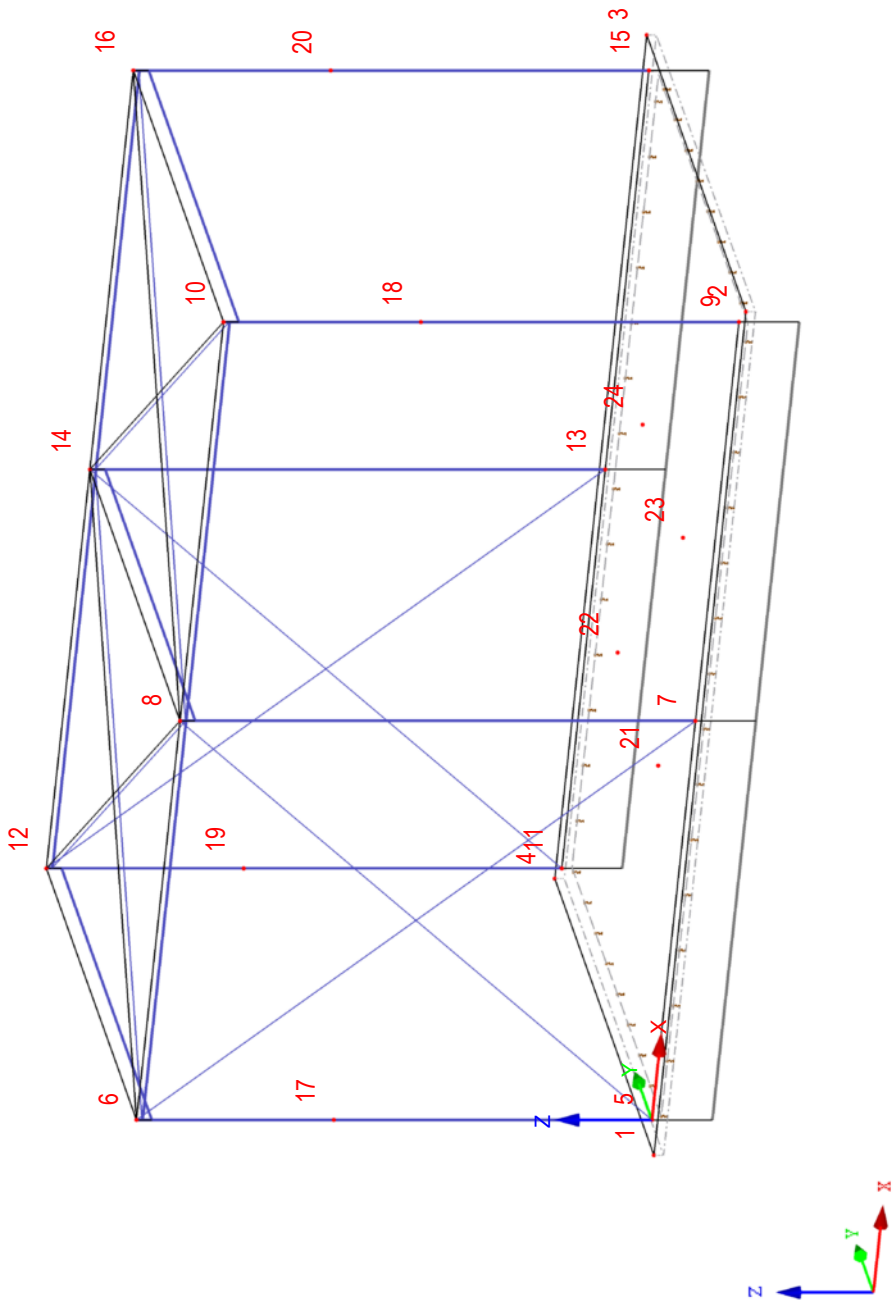
EWG1

| Vorm No. | Modale Ma $M_i$ [kg] | Effectieve modale massa $m_{eX}$ [kg] | $m_{eY}$ [kg] | $m_{eZ}$ [kg] | $m_{\varphi X}$ [kg.m²] | $m_{\varphi Y}$ [kg.m²] | $m_{\varphi Z}$ [kg.m²] | Effectieve modale massafactor $f_{meX}$ [-] | $f_{meY}$ [-] | $f_{meZ}$ [-] |
|---|---|---|---|---|---|---|---|---|---|---|
| 1 | 3958.04 | 0.00 | 8786.92 | 0.00 | 50009.85 | 0.00 | 0.21 | 0.000 | 0.172 | 0.000 |
| 2 | 787.73 | 11070.62 | 0.00 | 0.00 | 0.00 | 17603.38 | 0.00 | 0.217 | 0.000 | 0.000 |
| 3 | 10278.74 | 0.00 | 0.13 | 0.00 | 0.00 | 0.00 | 329780.01 | 0.000 | 0.000 | 0.000 |
| 4 | 2558.54 | 29593.80 | 0.00 | 0.00 | 0.00 | 67.34 | 0.00 | 0.581 | 0.000 | 0.000 |
| 5 | 46669.73 | 0.00 | 42158.92 | 0.00 | 10423.25 | 0.00 | 1.41 | 0.000 | 0.828 | 0.000 |
| 6 | 692.69 | 10.96 | 0.00 | 0.00 | 0.00 | 13.42 | 0.00 | 0.000 | 0.000 | 0.000 |
| 7 | 1012.69 | 10123.38 | 0.00 | 0.00 | 0.00 | 18914.28 | 0.00 | 0.199 | 0.000 | 0.000 |
| 8 | 3125.85 | 0.00 | 0.00 | 0.00 | 0.18 | 0.00 | 9646.38 | 0.000 | 0.000 | 0.000 |
| 9 | 706.91 | 143.00 | 0.00 | 0.00 | 0.00 | 12418.04 | 0.00 | 0.003 | 0.000 | 0.000 |
| 10 | 912.90 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4.37 | 0.000 | 0.000 | 0.000 |
| Som | 70703.83 | 50941.76 | 50945.97 | 0.00 | 60433.27 | 49016.46 | 339432.39 | 1.000 | 1.000 | 0.000 |

## INHOUD

## KNOOPNUMMERING

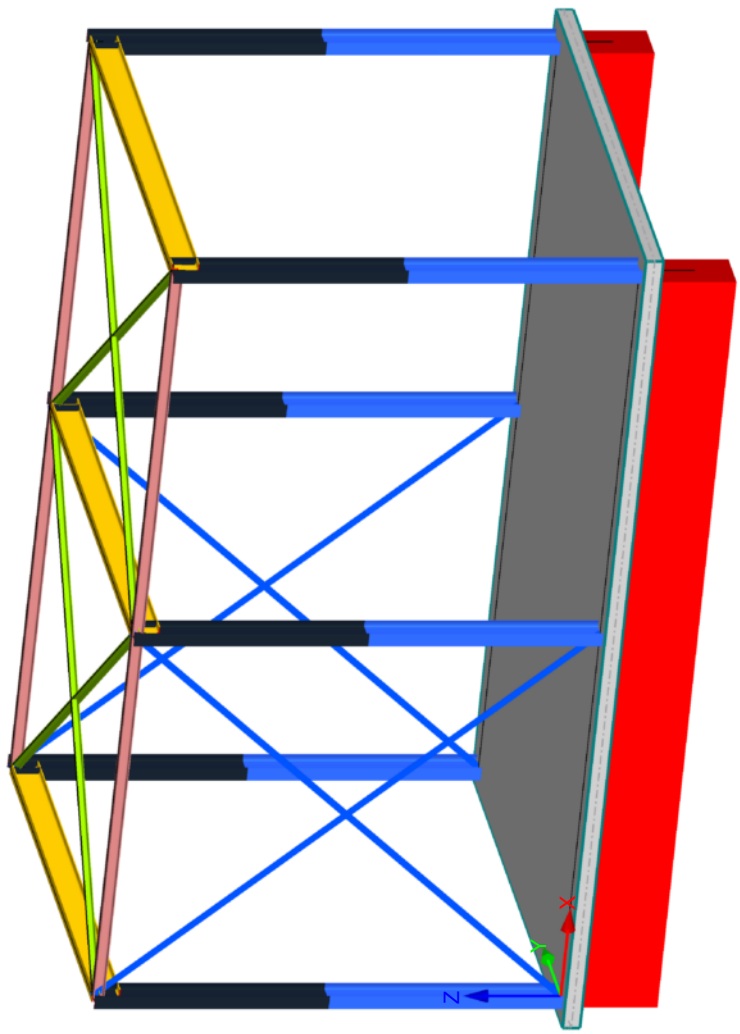
Isometrisch



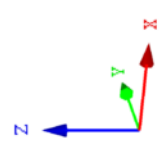

Knoopnummering

## DOORSNEDES

Isometrisch

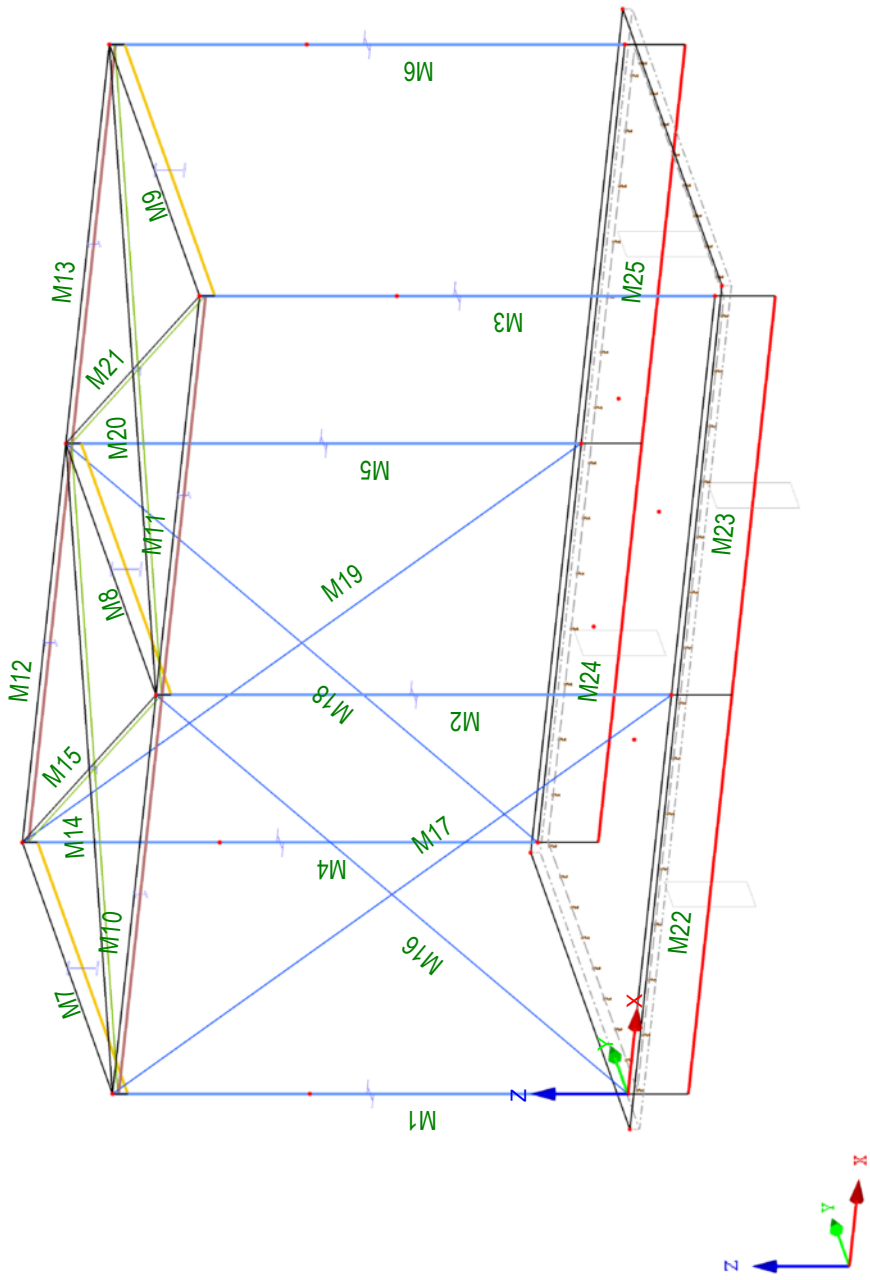



Doorsnedes
1: IPE 240 | Euronorm 1
2: IPE 240 | Euronorm 1
3: HE A 100 | Euronorm
4: L 60x60x6 | EN 1005
5: Rechthoek 6/60; Staa
6: Rechthoek 400/650; E



## STAAFNUMMERING

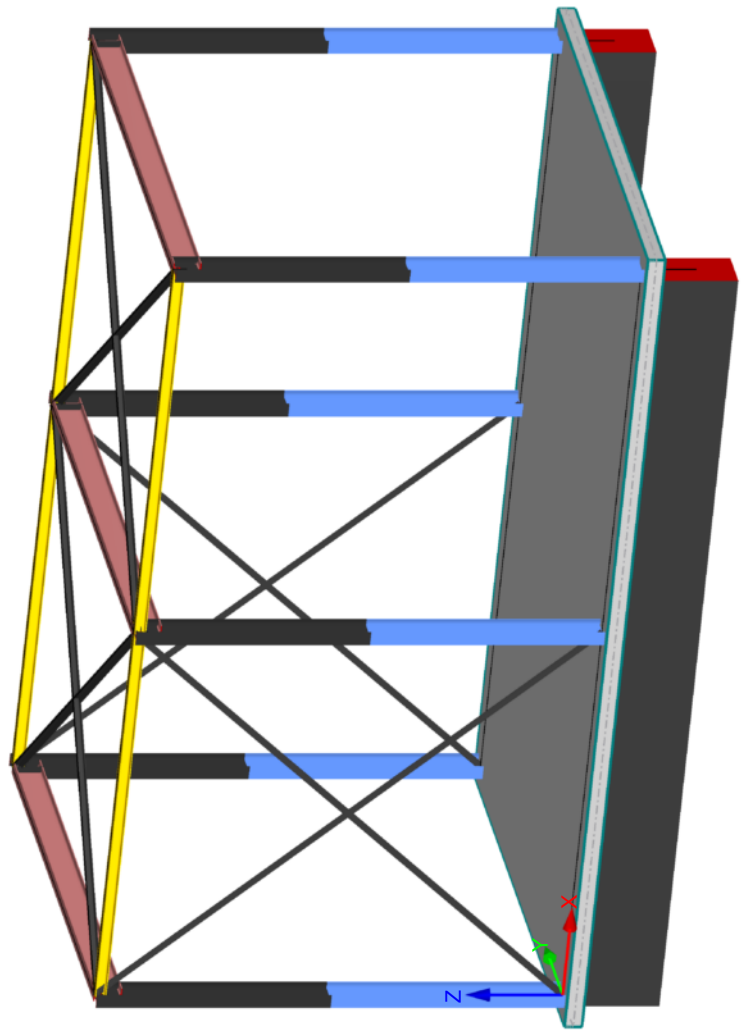
Isometrisch



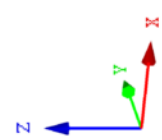

Staafnummering

## STAAFEINDSCHARNIEREN

Isometrisch

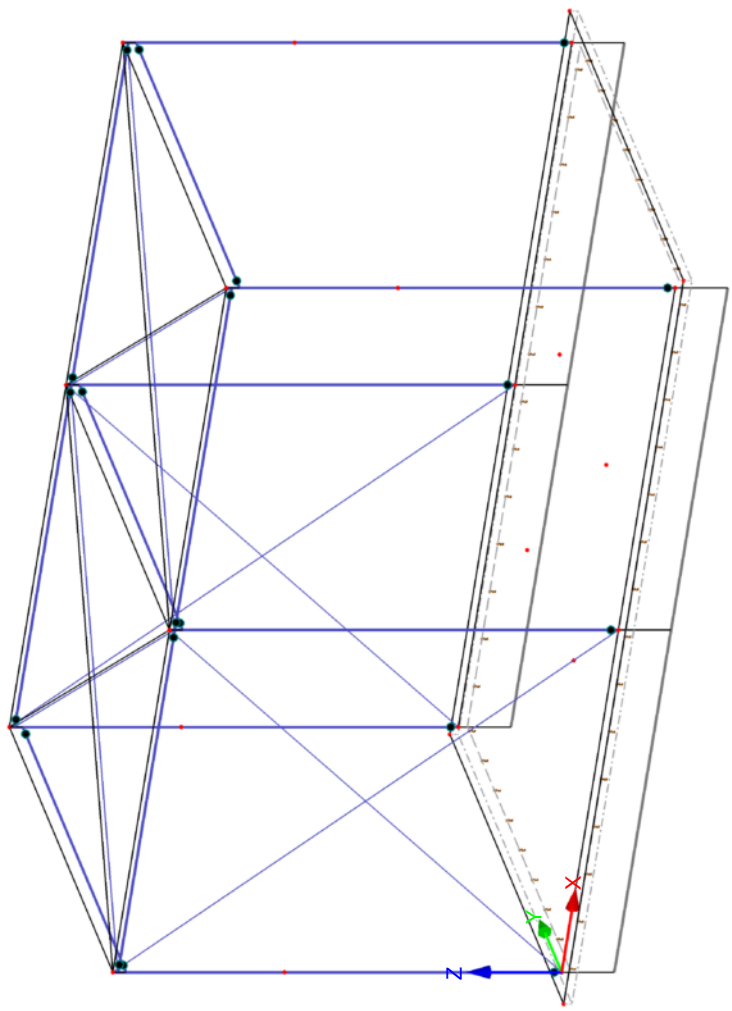



Staafeindscharnieren
1: Lokaal; NNN NYY
2: Lokaal; NNN NYY
3: Lokaal; NNN NEY



## BG10: PB: EIGEN GEWICHT

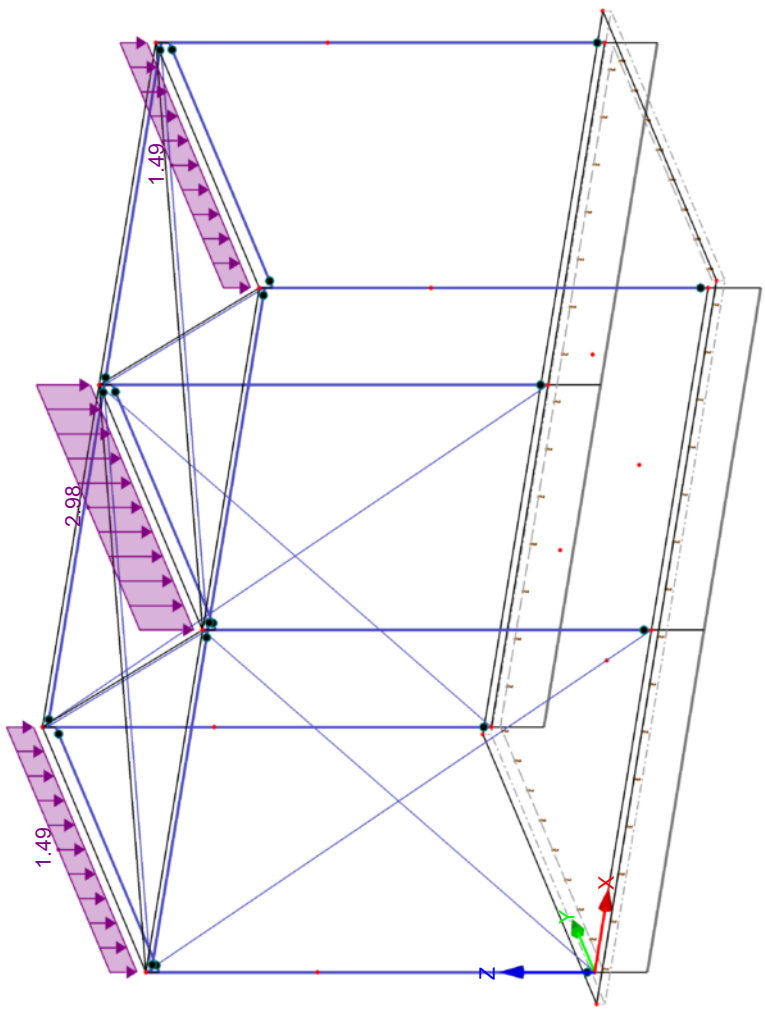
Isometrisch




BG10 : PB: Eigen Gewicht

## BG20: PB: DAKBEDEKKING

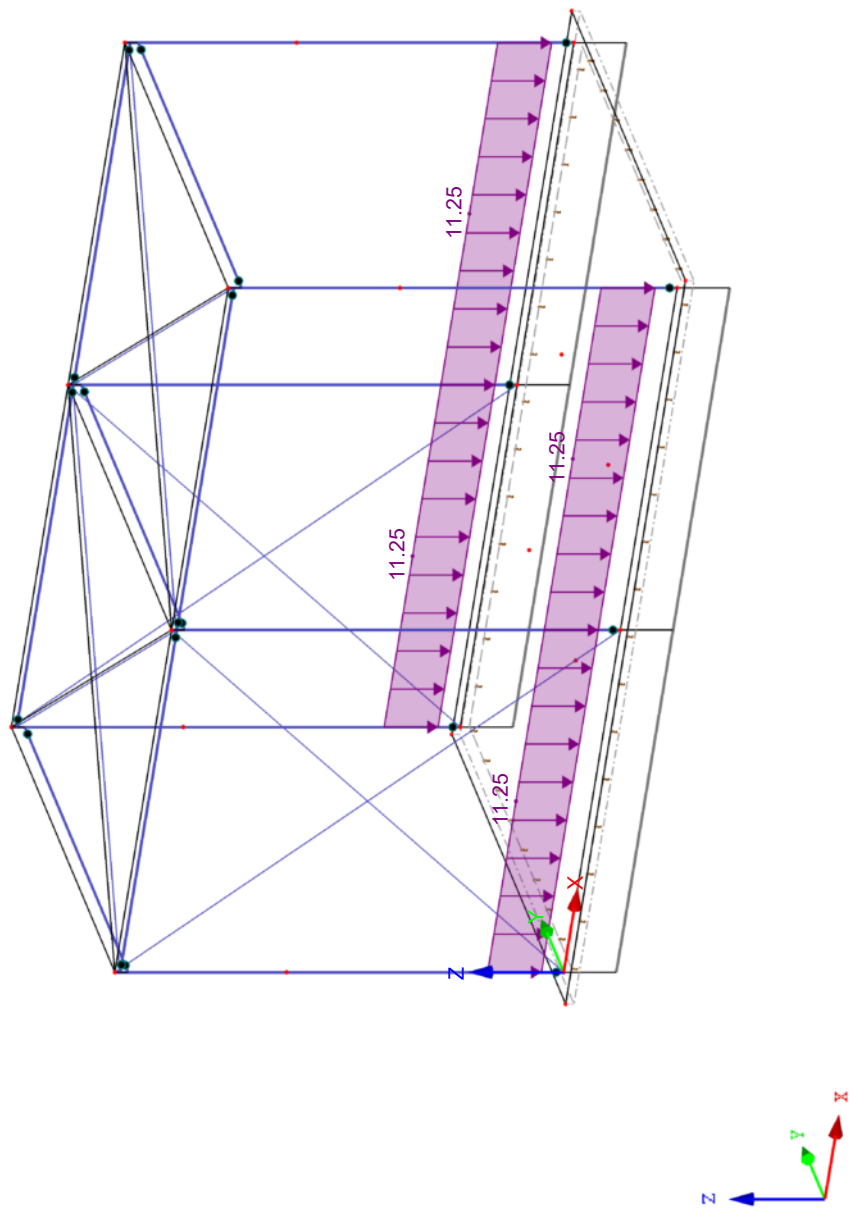
Isometrisch




BG20 : PB: Dakbedekking
Belastingen [kN/m]

## BG30: PB: KSZ - METSELWERK

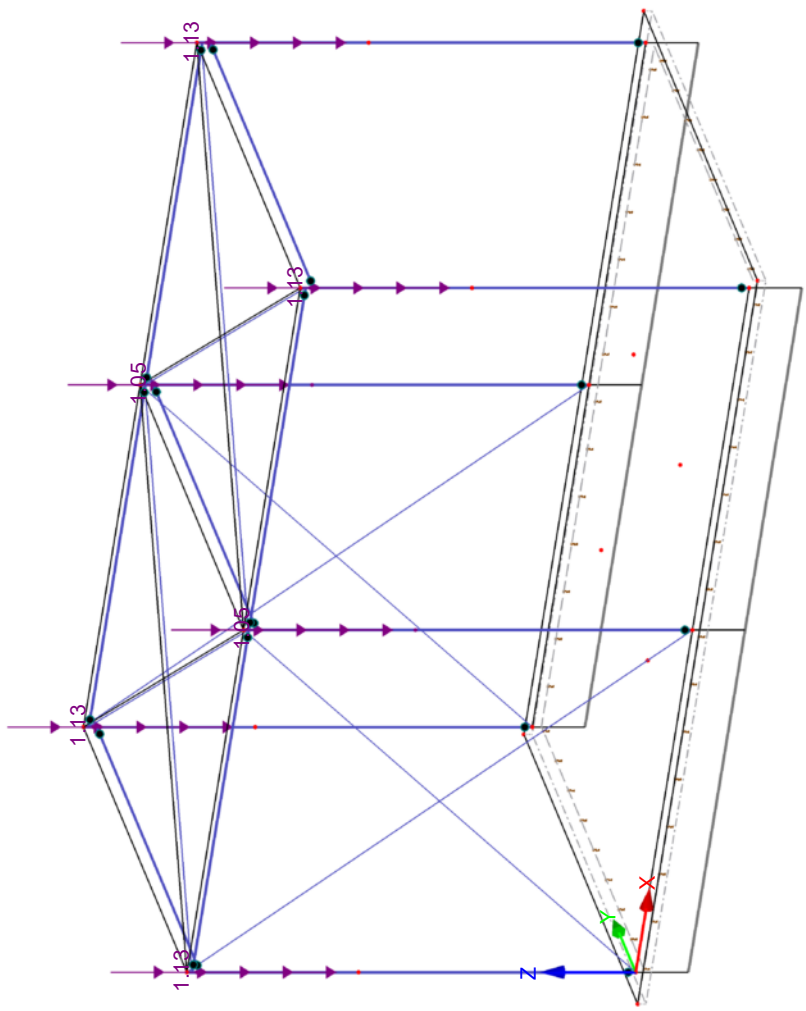
Isometrisch

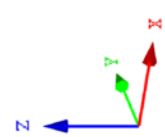



BG30 : PB: KSZ - Metselwerk
Belastingen [kN/m]

## BG40: PB: SANDWICHPANEEL

Isometrisch

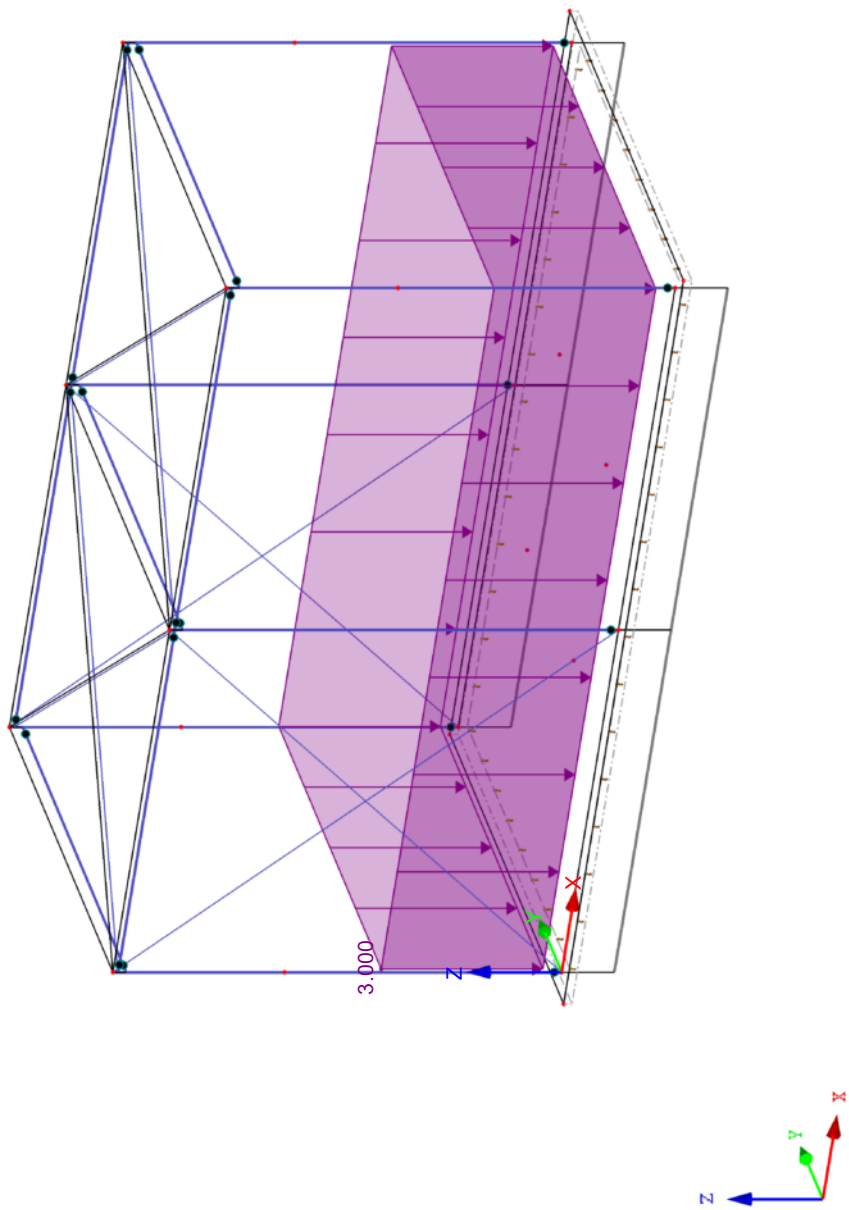



BG40 : PB: Sandwichpaneel
Belastingen [kN/m]

## BG100: VB: OPGELEGDE BELASTING OP VLOEREN 1

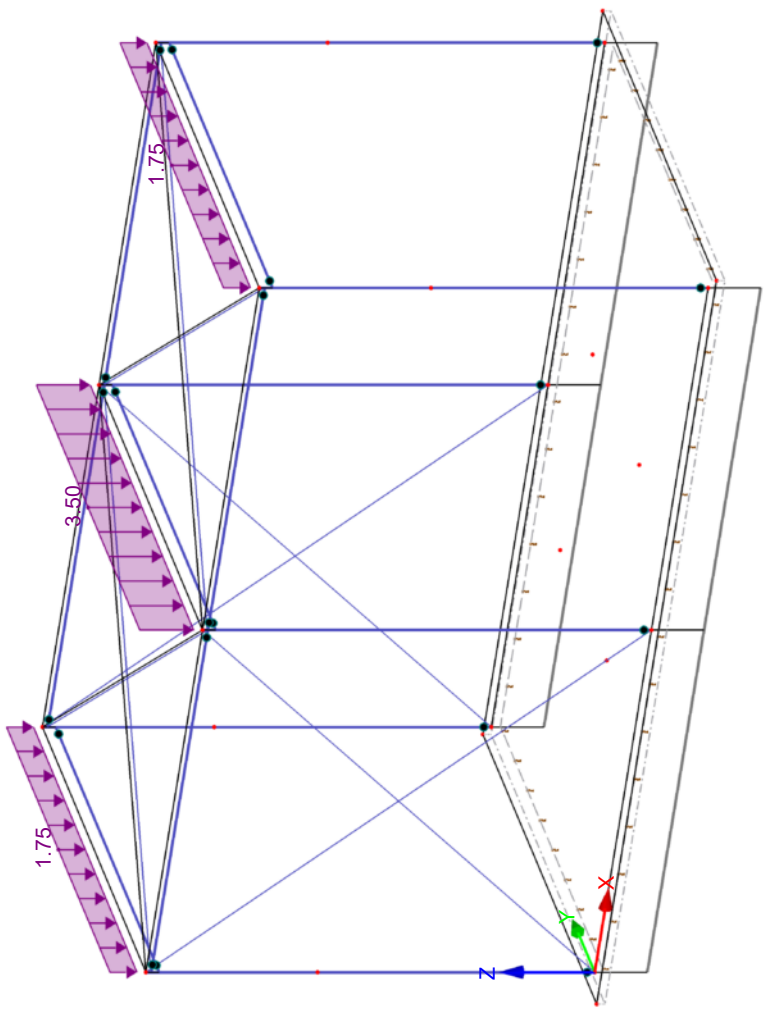
Isometrisch

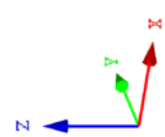



BG100 : VB: Opgelegde belasting op vloeren 1
Belastingen [kN/m^2]

## BG120: VB: DAKBELASTING

Isometrisch

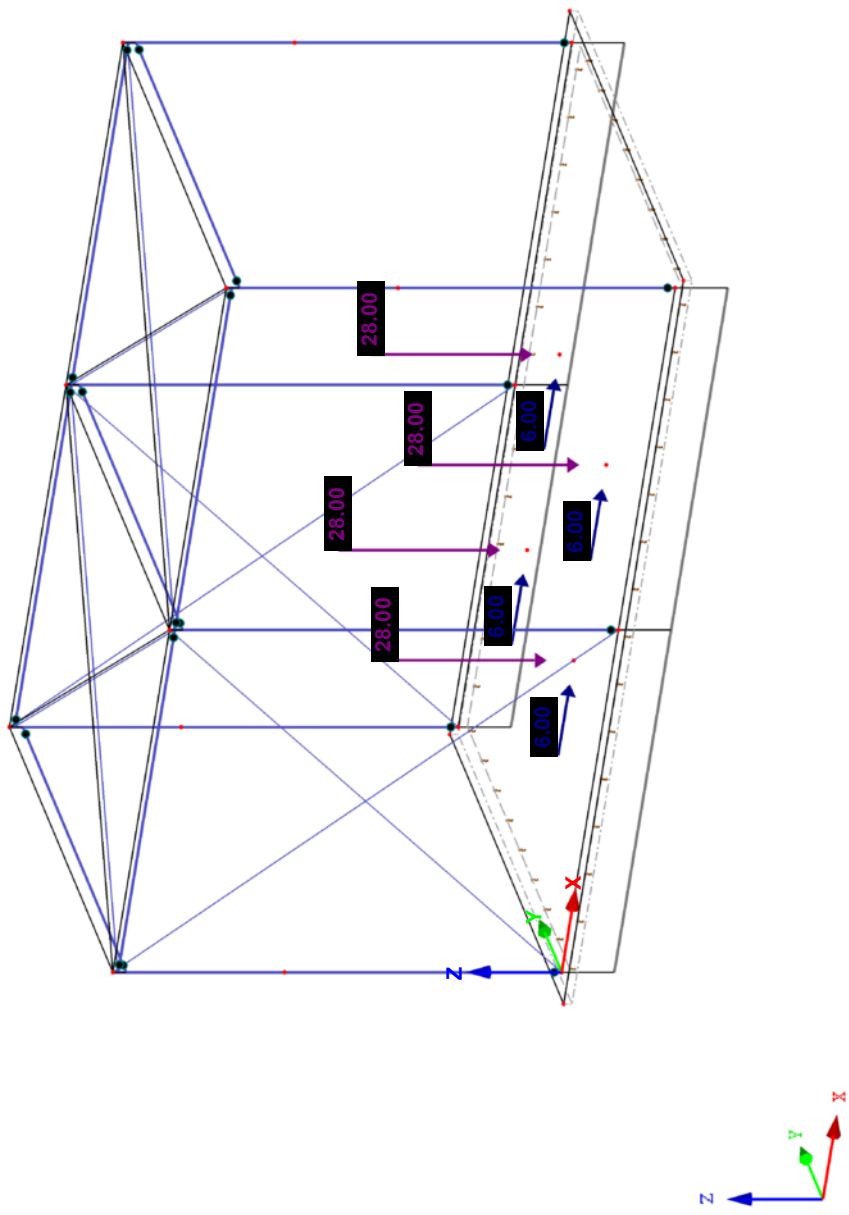



BG120 : VB: Dakbelasting
Belastingen [kN/m]

## BG150: VB: HEFTRUCK

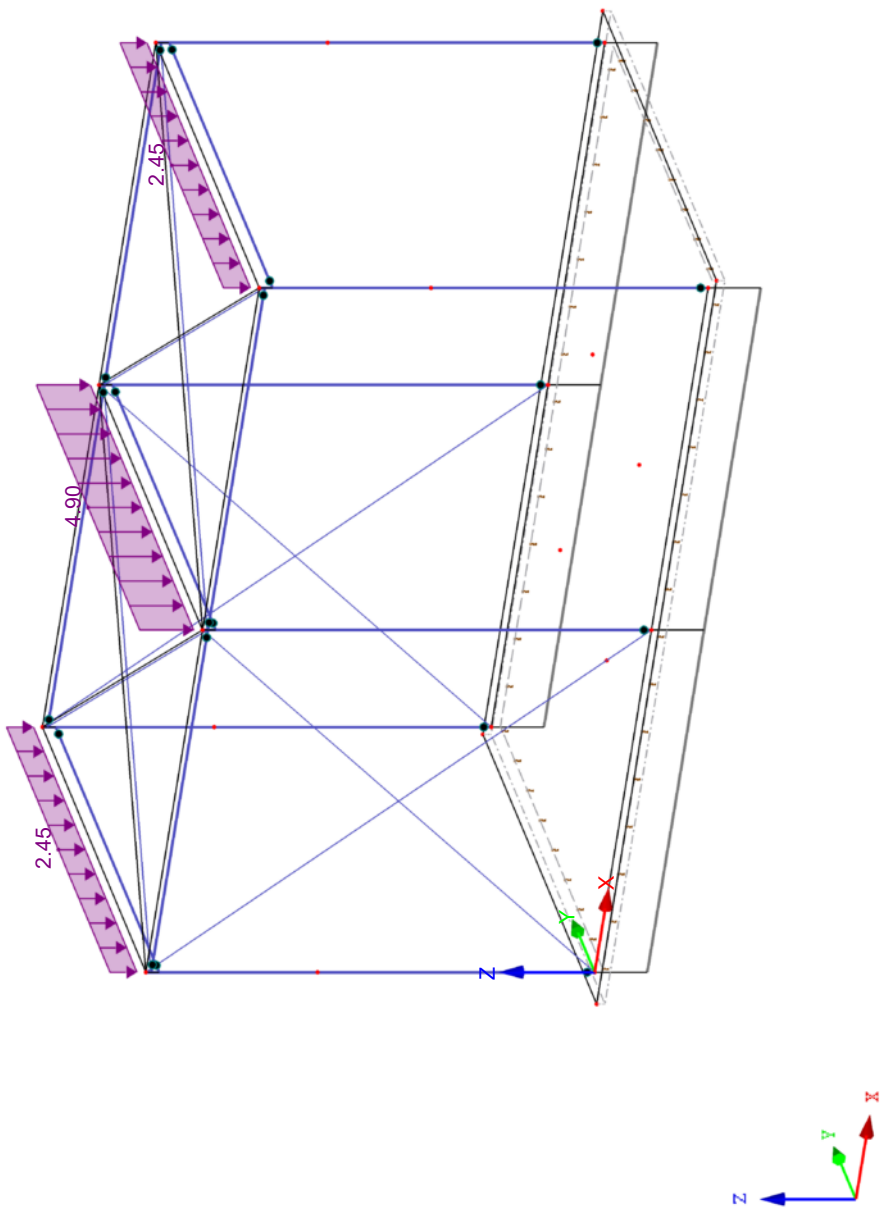
Isometrisch




BG150 : VB: Heftruck
Belastingen [kN]

## BG300: VB: SNEEUW

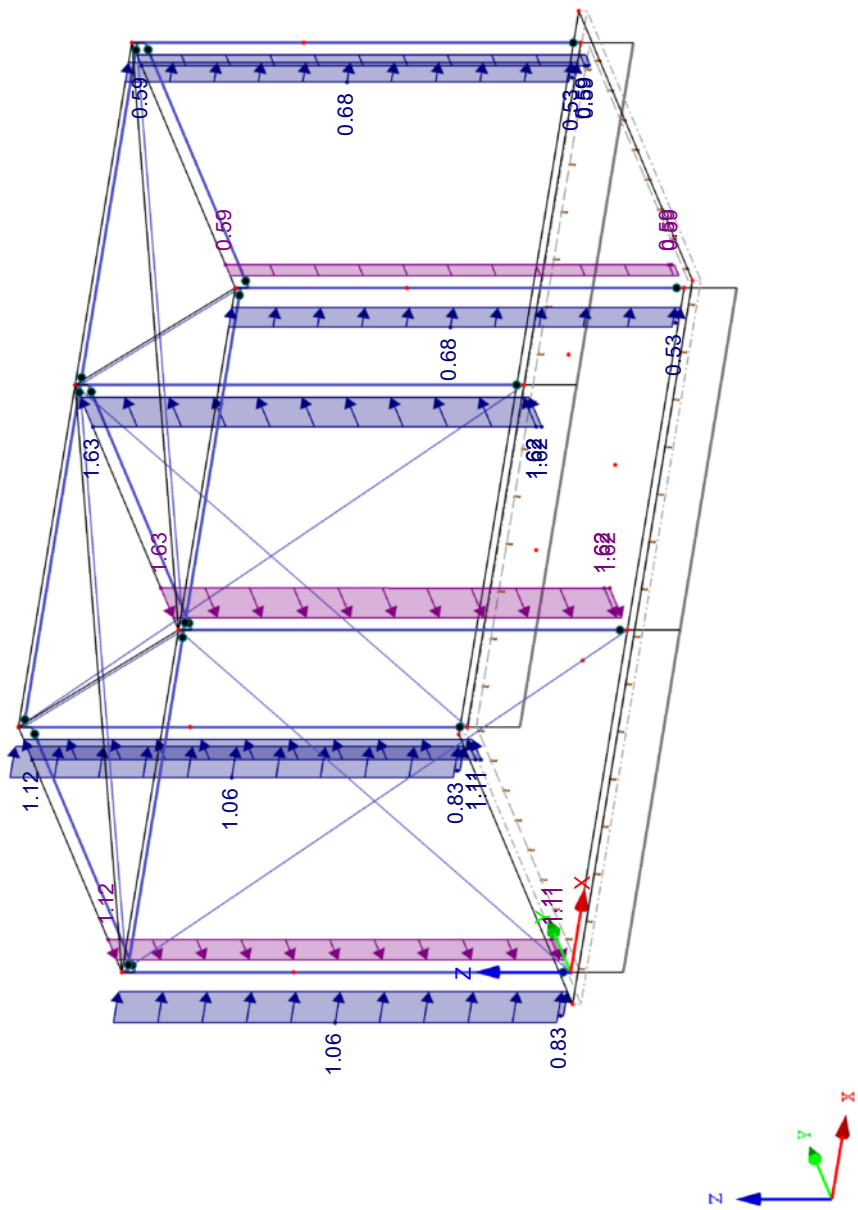
Isometrisch




BG300 : VB: Sneeuw
Belastingen [kN/m]

## BG401: VB: WIND (+X RICHTING)

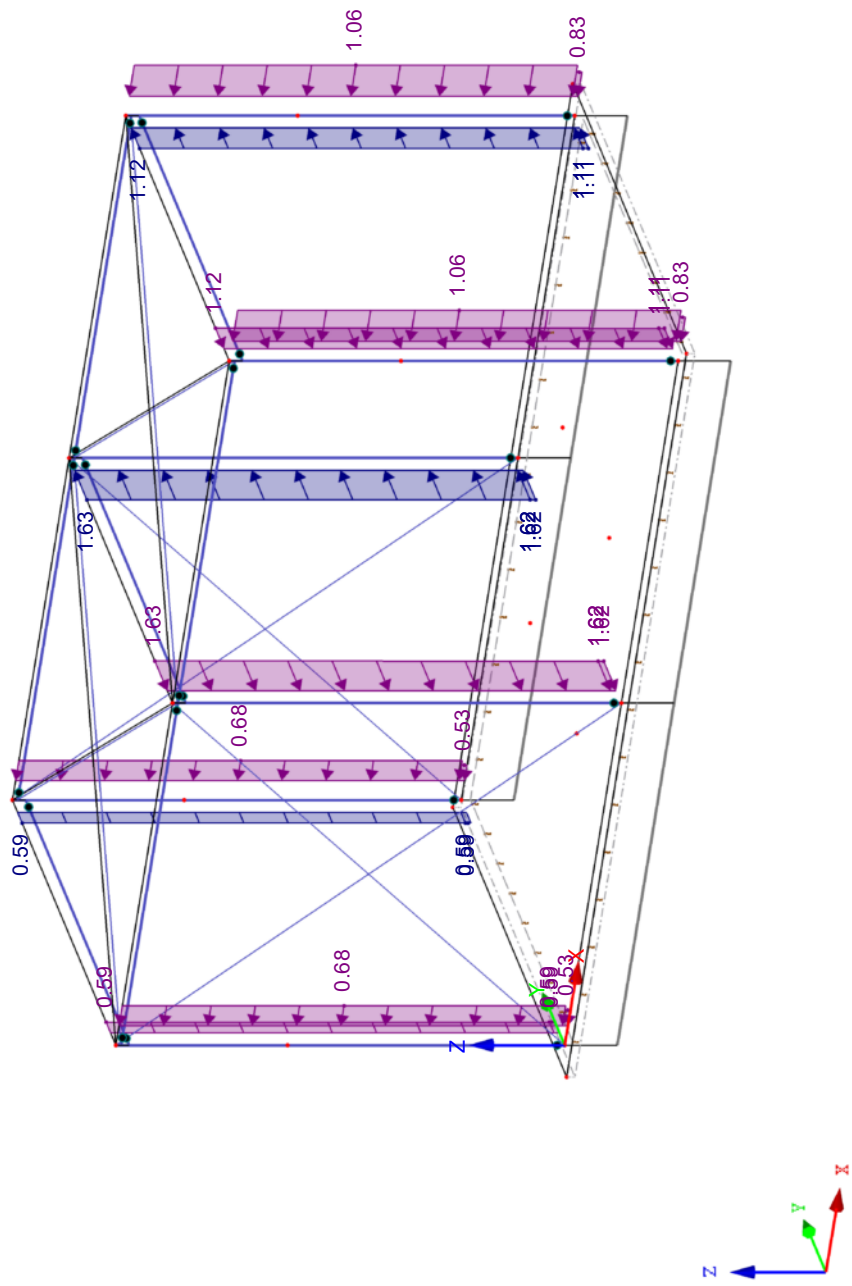
Isometrisch




BG401 : VB: Wind (+X richting)
Belastingen [kN/m]

## BG402: VB: WIND (-X RICHTING)

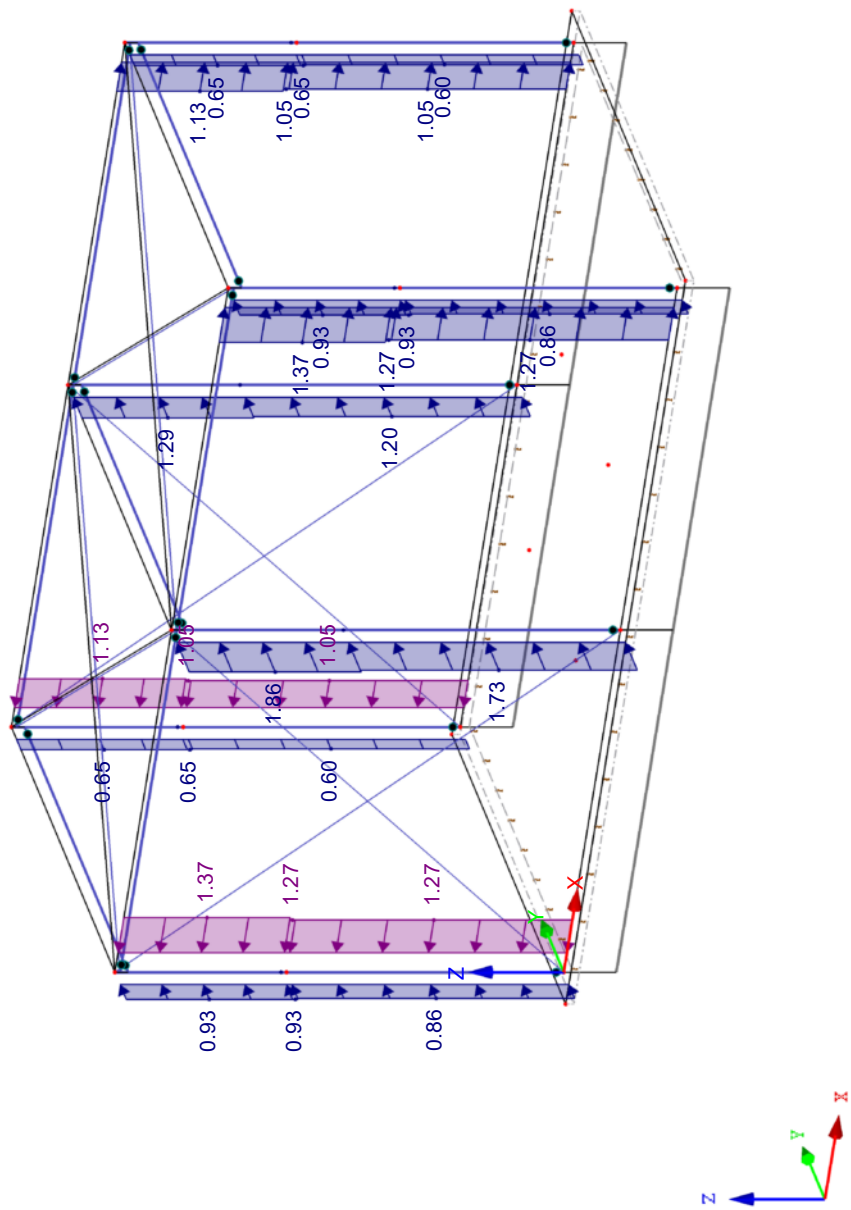
Isometrisch




BG402 : VB: Wind (-X richting)
Belastingen [kN/m]

## BG403: VB: WIND (+Y RICHTING)

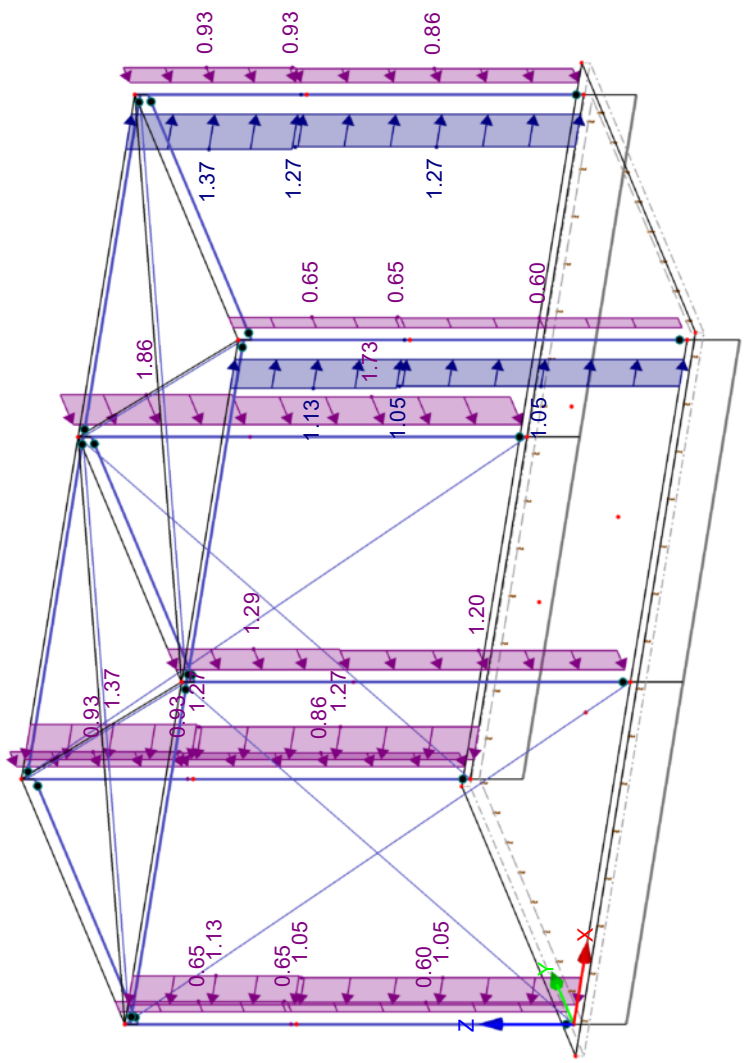
Isometrisch




BG403 : VB: Wind (+Y richting)
Belastingen [kN/m]

## BG404: VB: WIND (-Y RICHTING)

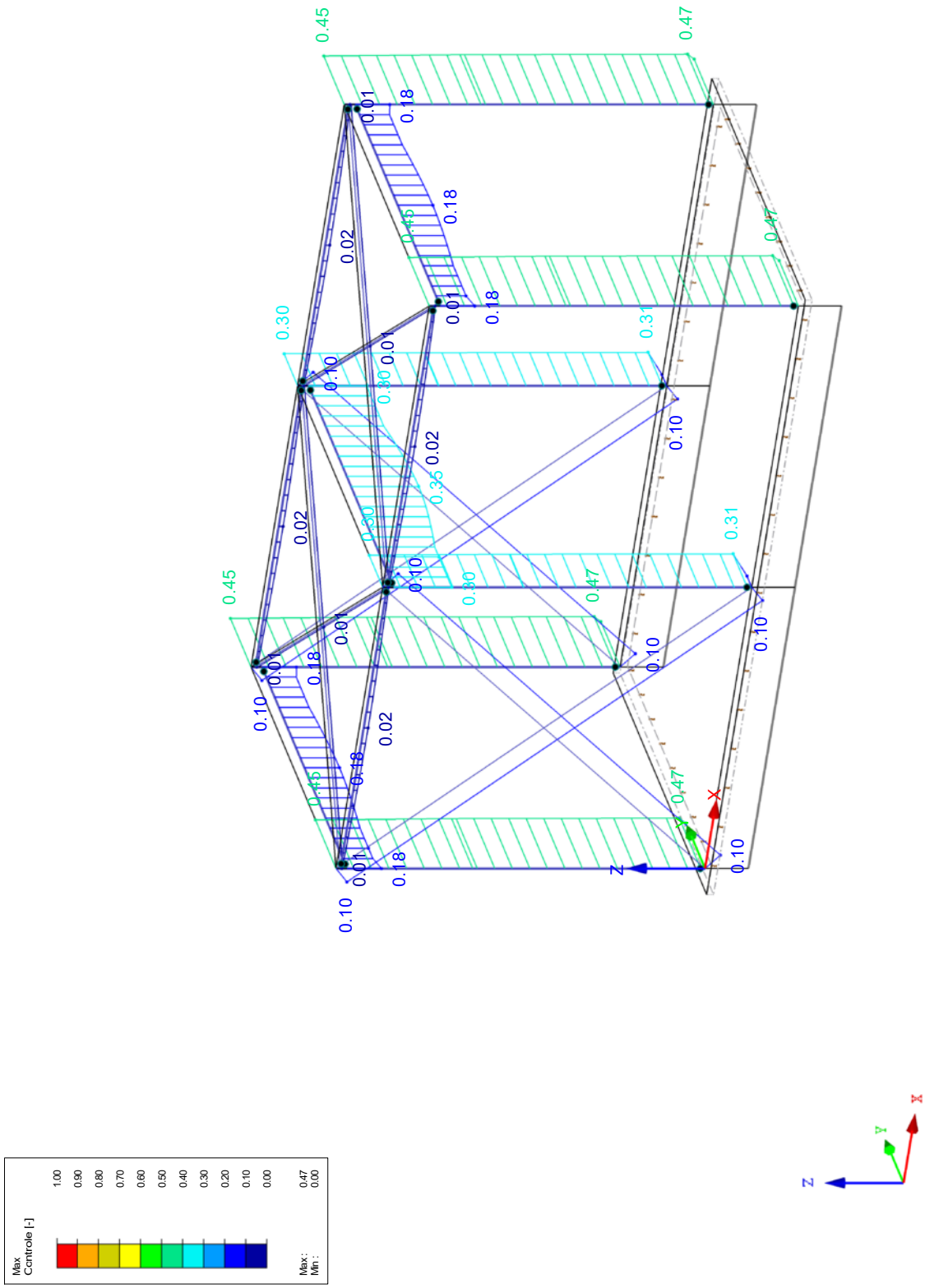
Isometrisch




BG404 : VB: Wind (-Y richting)
Belastingen [kN/m]

## CONTROLE

Isometrisch

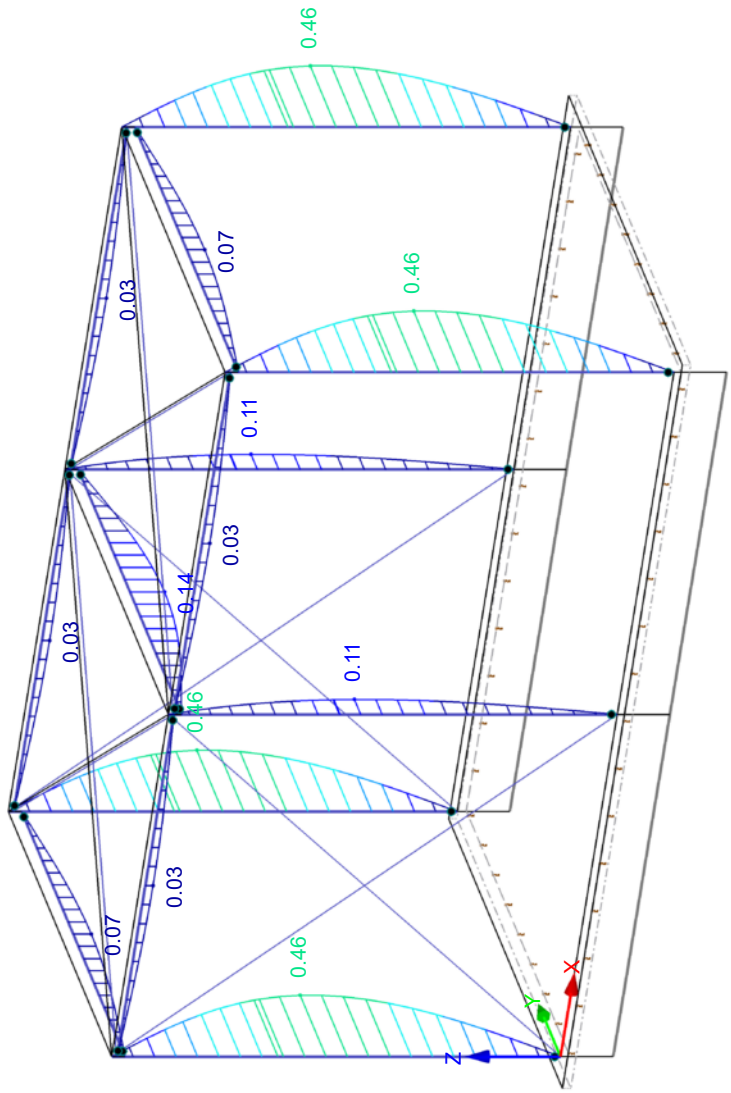



RF-STEEL EC3 BG1
Uiterste grenstoestand: Doorsnedecontrole, Stabiliteitsberekening

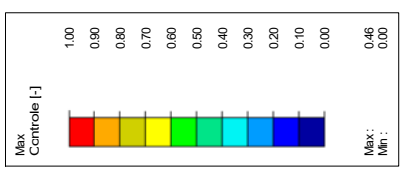
Staven Max Controle: 0.47

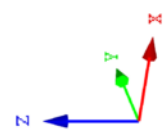
## CONTROLE

Isometrisch




RF-STEEL EC3 BG1
Bruikbaarheidsgrenstoestand: Vervormingen

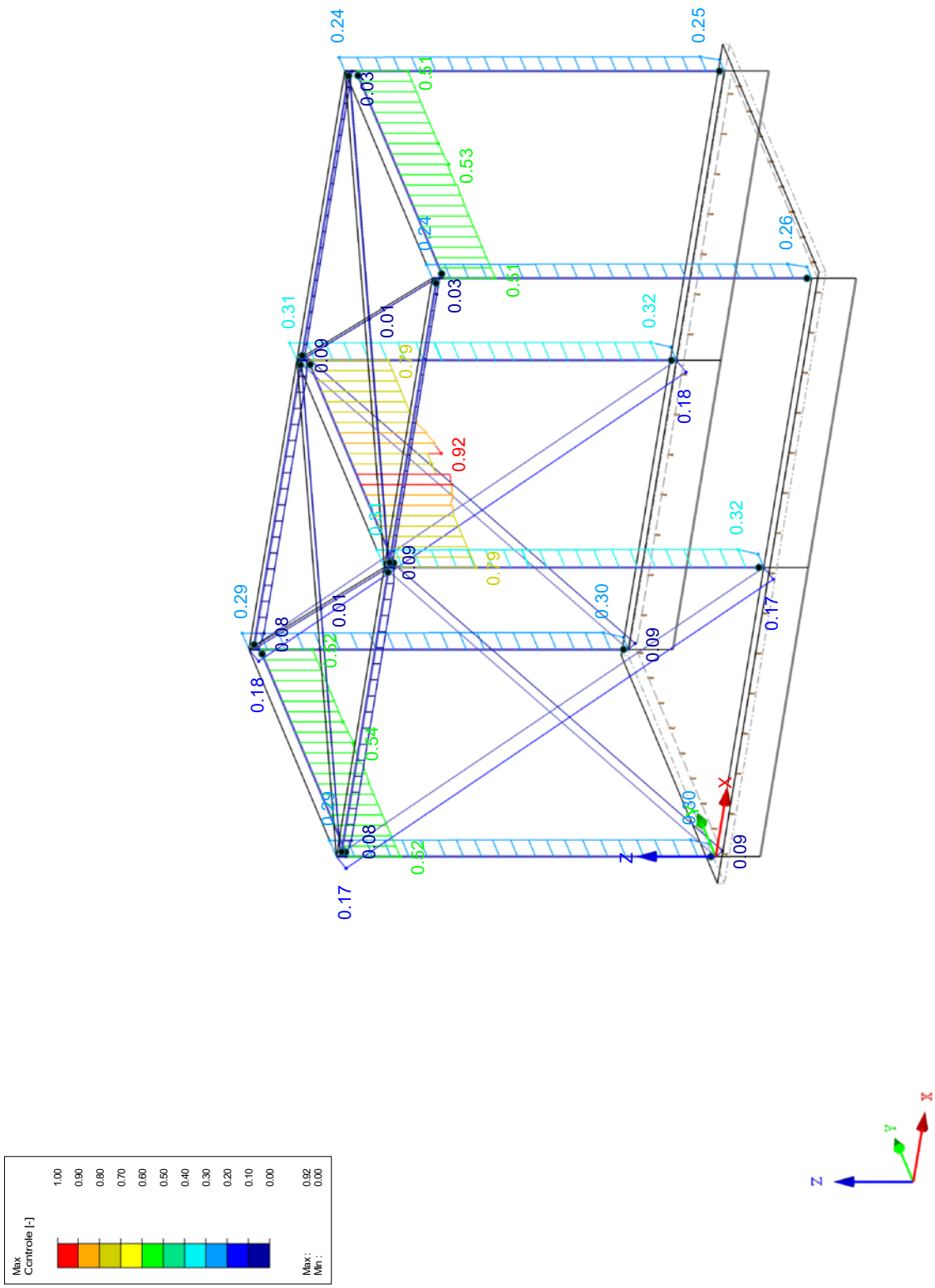



Staven Max Controle: 0.46

## CONTROLE

Isometrisch



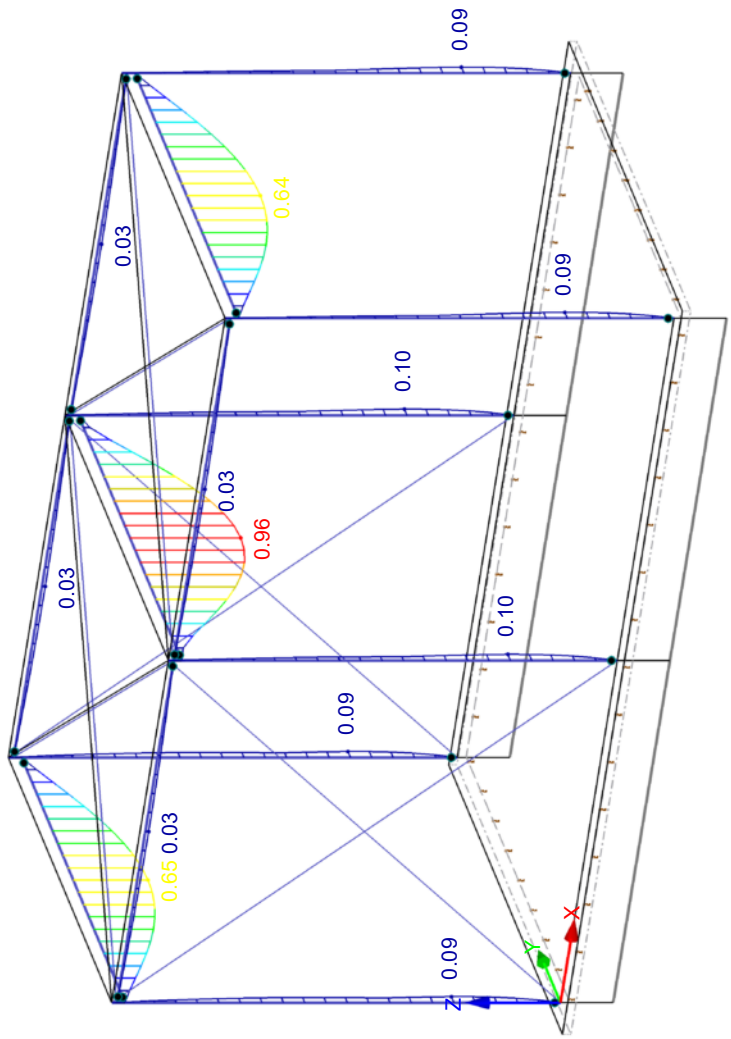

RF-STEEL EC3 BG2
Uiterste grenstoestand: Doorsnedecontrole, Stabiliteitsberekening

Max
Controle [-]
1.00
0.90
0.80
0.70
0.60
0.50
0.40
0.30
0.20
0.10
0.00
Max: 0.92
Min: 0.00

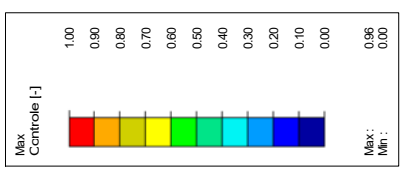
Staven Max Controle: 0.92

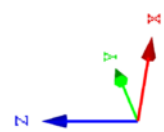
## CONTROLE

Isometrisch




RF-STEEL EC3 BG2
Bruikbaarheidsgrenstoestand: Vervormingen



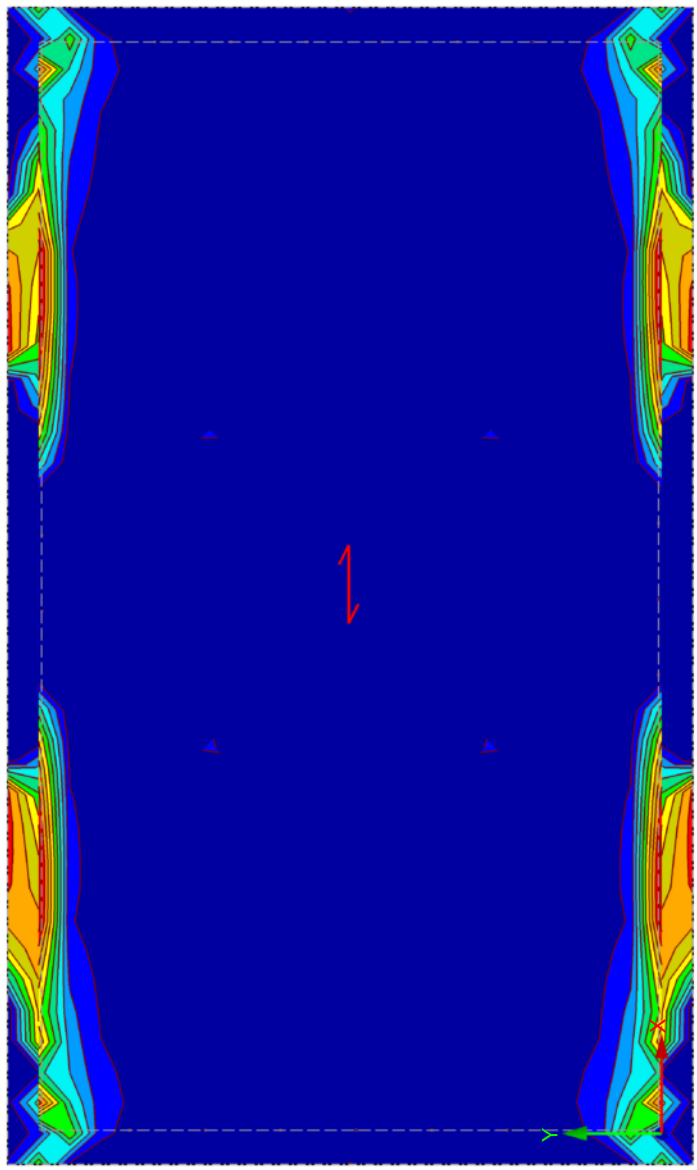




Staven Max Controle: 0.96

## ■ BENODIGDE WAPENING $a_{s,1,-z\ (bov)}$

Tegen Z-richting in

970 mm



RF-CONCRETE Surfaces BG1
Wapeningsberekening
Vlakken Benodigde Wapening a-s,1,-z (bov) [mm²/m]

Benodigde Wapening a-s,1,-z (bov) [mm²/m]

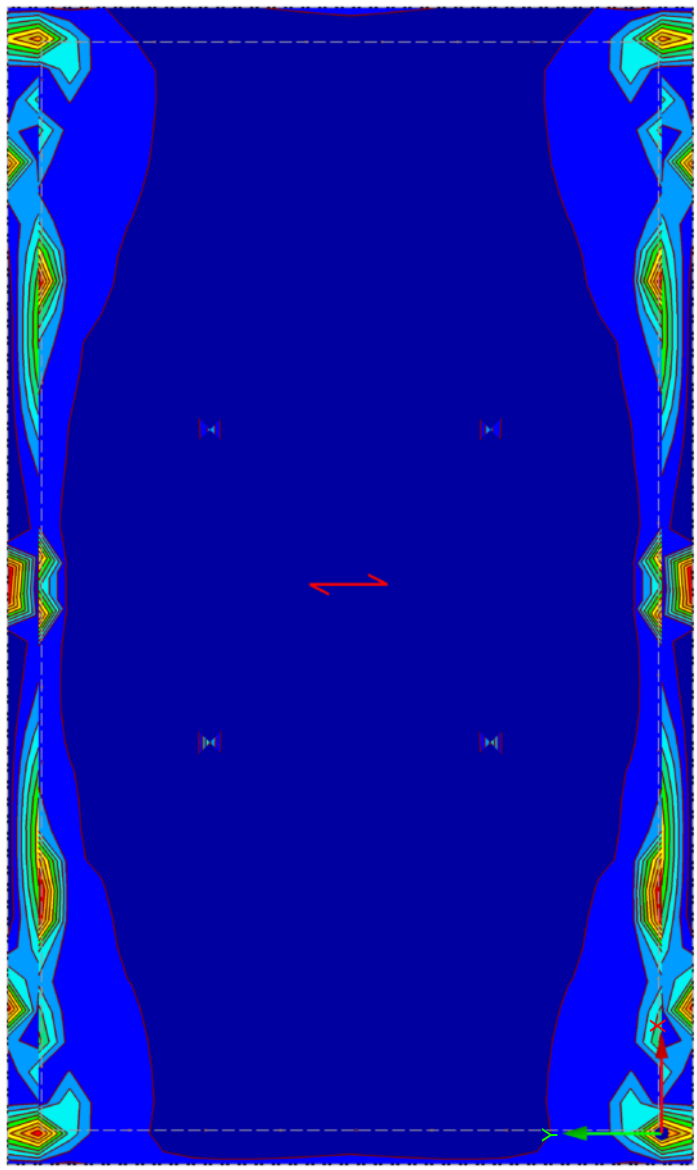
| | |
|---|---|
| | 661.262 |
| | 639.601 |
| | 617.940 |
| | 596.280 |
| | 574.619 |
| | 552.958 |
| | 531.297 |
| | 509.637 |
| | 487.976 |
| | 466.315 |
| | 444.654 |
| | 422.993 |
| Max : | 661.262 |
| Min : | 422.993 |

Max a-s,1,-z (bov): 661.262, Min a-s,1,-z (bov): 422.993 mm²/m

## BENODIGDE WAPENING $a_{s,2,-z\ (bov)}$

Tegen Z-richting in

970 mm



RF-CONCRETE Surfaces BG1
Wapeningsberekening
Vlakken Benodigde Wapening a-s,2,-z (bov) [mm²/m]

Benodigde Wapening a-s,2,-z (bov) [mm²/m]

807.015
783.025
759.036
735.046
711.057
687.067
663.077
639.088
615.098
591.108
567.119
543.129

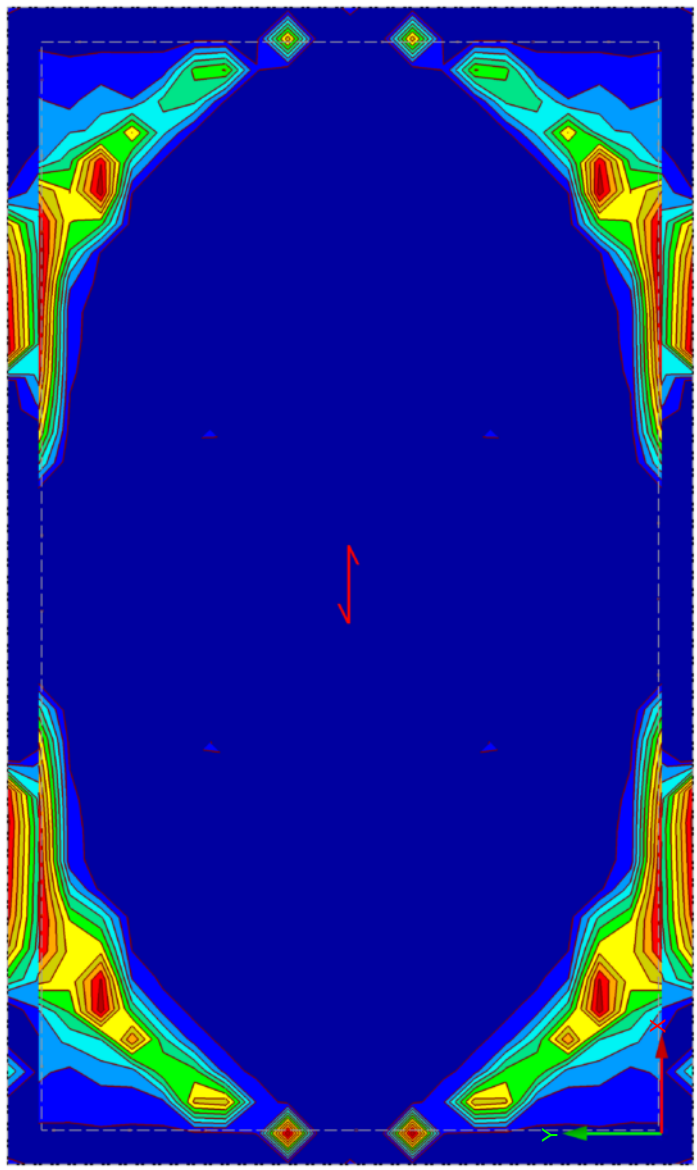
Max : 807.015
Min : 543.129

Max a-s,2,-z (bov): 807.015, Min a-s,2,-z (bov): 543.129 mm²/m

## BENODIGDE WAPENING $a_{s,1,+z\ (ond)}$

Tegen Z-richting in

970 mm



RF-CONCRETE Surfaces BG1
Wapeningsberekening
Vlakken Benodigde Wapening a-s,1,+z (ond) [mm²/m]

Benodigde Wapening a-s,1,+z (ond) [mm²/m]

645.687
625.442
605.197
584.953
564.708
544.463
524.218
503.973
483.728
463.483
443.238
422.993

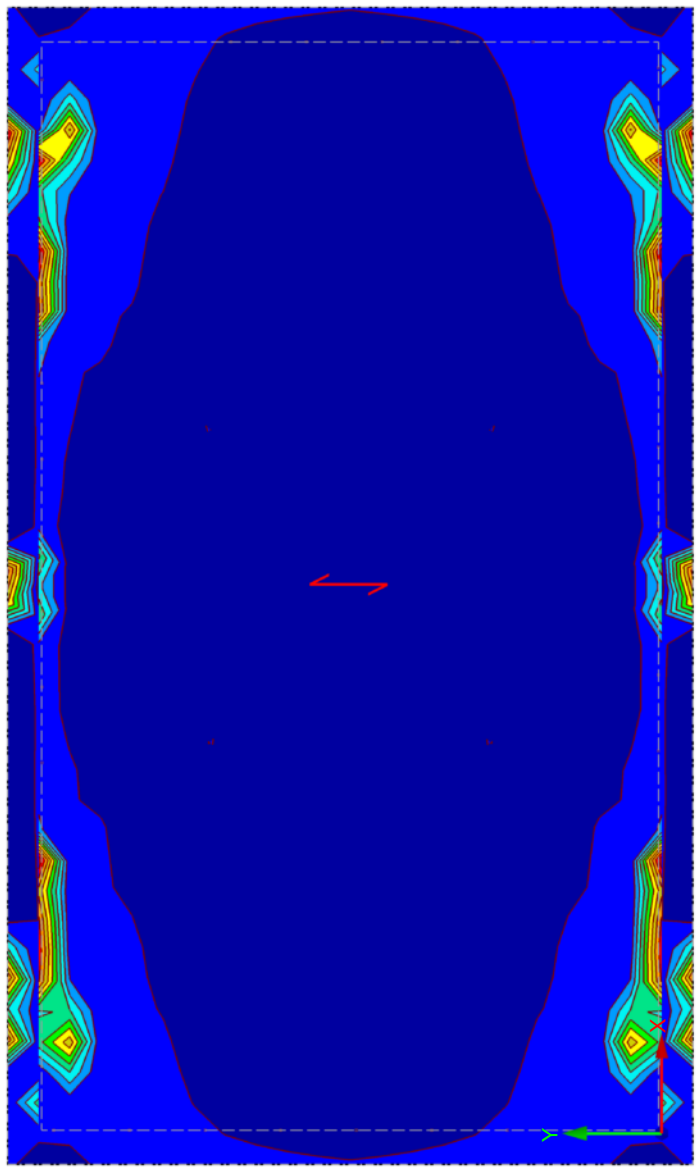
Max : 645.687
Min : 422.993

Max a-s,1,+z (ond): 645.687, Min a-s,1,+z (ond): 422.993 mm²/m

## ■ BENODIGDE WAPENING $a_{s,2,+z\ (ond)}$

Tegen Z-richting in

970 mm



RF-CONCRETE Surfaces BG1
Wapeningsberekening
Vlakken Benodigde Wapening a-s,2,+z (ond) [mm²/m]

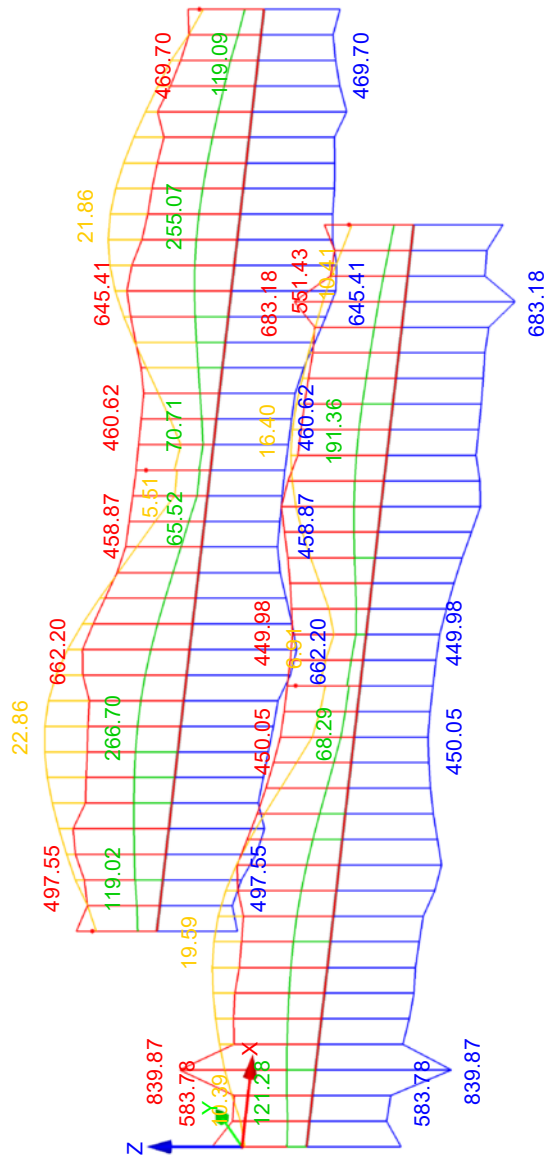
Benodigde Wapening a-s,2,+z (ond) [mm²/m]

| | |
|---|---|
| | 815.889 |
| | 791.093 |
| | 766.296 |
| | 741.500 |
| | 716.703 |
| | 691.907 |
| | 667.111 |
| | 642.314 |
| | 617.518 |
| | 592.722 |
| | 567.925 |
| | 543.129 |
| Max : | 815.889 |
| Min : | 543.129 |

Max a-s,2,+z (ond): 815.889, Min a-s,2,+z (ond): 543.129 mm²/m

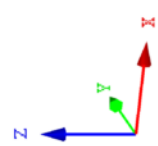
## RESULTATEN

Isometrisch




RF-CONCRETE Members BG1
Ontwerp van betonnen staven

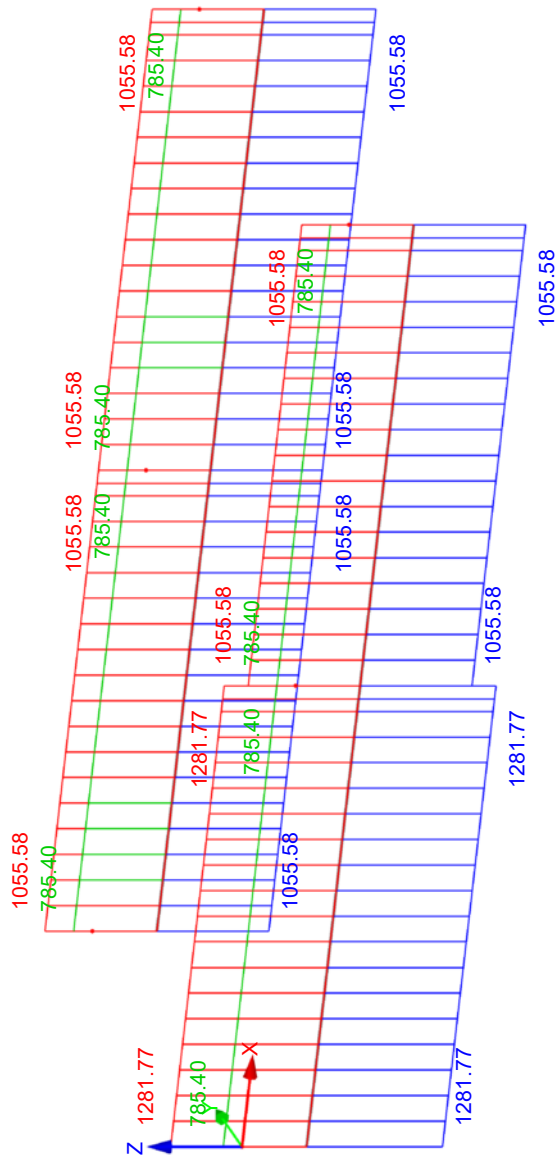
A<sub>s,-z</sub>/s...
A<sub>s,+z</sub>/s...
A-s,T
a-sw,T,beugel




Max $A_{s,-z}$: 839.87 mm²
Max $A_{s,+z}$: 839.87 mm²
Max A-s,T: 266.70 mm²
Max a-sw,T,beugel: 22.86 mm²/m

## RESULTATEN

Isometrisch



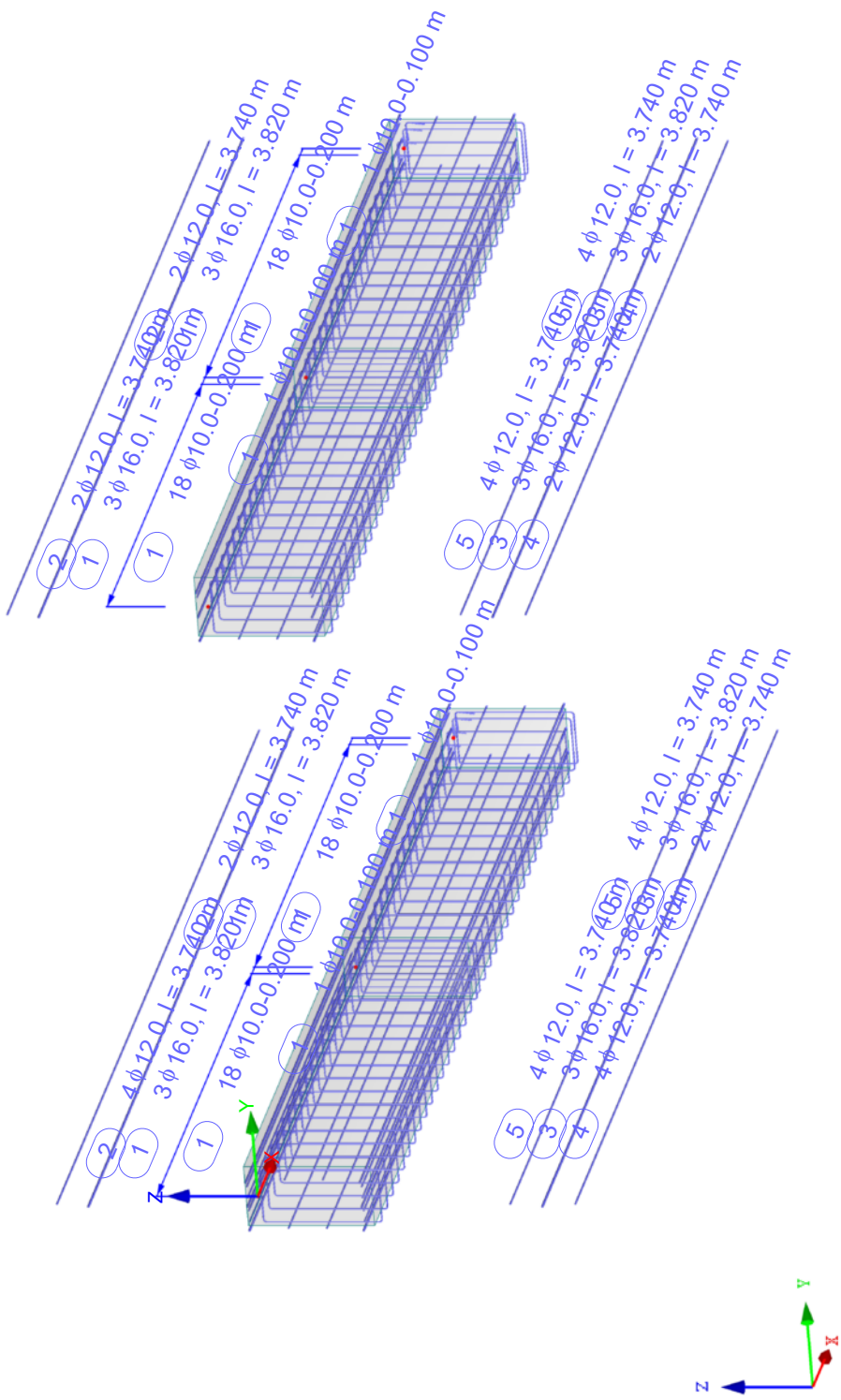

RF-CONCRETE Members BG1
Ontwerp van betonnen staven

A-s,-z (bov),aanw.
A-s,+z (ond),aanw.
a-s,beugel,aan...

Max A-s,-z (bov),aanw.: 1281.77 mm²
Max A-s,+z (ond),aanw.: 1281.77 mm²
Max a-s,beugel,aanw.: 785.40 mm²/m

## MODEL

Isometrisch




RF-CONCRETE Members BG1
Ontwerp van betonnen staven

# Ontwerpadvies fundering

Nieuwbouw bedrijfspand bij Celanese a/d Asselenkuil te Geleen
GC200516.R01.V1.0

15 september 2022


GEONIUS

# Ontwerpadvies fundering

Nieuwbouw bedrijfspand bij Celanese a/d Asselenkuil te Geleen
Documentnummer GC200516.R01.V1.0
15 september 2022

**Opdrachtgever**
VIRO Engineering BV
Velperweg 35
6824BE Arnhem

**Auteurs**
Projectleider Geotechniek ing. M. Vankan
Collegiale toets ir. NPAW Kelleners

+31 88 130 06 00
info@geonius.nl
Postbus 1097
6160 BB Geleen

Geonius.nl

| Functie | Naam | Paraaf |
|---|---|---|
| Projectleider Geotechniek | ing. M. Vankan | |
| Collegiale toets | ir. NPAW Kelleners | |

# Inhoud



## Bijlagen

# 1 Inleiding

Door VIRO Engineering BV werd aan Geonius Geotechniek B.V. opdracht gegeven om een geotechnisch grondonderzoek uit te voeren en een ontwerpadvies voor de fundering op te stellen. Dit onderzoek was nodig voor de nieuwbouw van een bedrijfshal op het terrein van Celanese aan de Asselenkuil in Geleen.

Voorliggend rapport bevat de resultaten van het grondonderzoek en het ontwerpadvies voor de fundering. Het ontwerpadvies is uitgewerkt conform NEN 9997-1 (Geotechnisch ontwerp Deel 1: Algemene regels) en NEN 1997-2 (Geotechnisch ontwerp Deel 2: Grondonderzoek en beproeving). Beide delen vormen de basis van Eurocode 7.

# 2 Projectbeschrijving

## 2.1 Beschrijving

Op het terrein van Celanese aan de Asselenkuil in Geleen is de nieuwbouw van een bedrijfshal gepland, bedoeld voor de opslag van gevaarlijke stoffen. De nieuwbouw heeft afmetingen van ca. 18 x 22 m en wordt met een verbindingsgang verbonden aan het bestaande gebouw.

Voor het ontwerpadvies voor de funderingen van de geplande nieuwbouw zijn door ons de onderstaande mede door de opdrachtgever verstrekte uitgangspunten gehanteerd:

- De nieuwbouw bestaat uit maximaal 1 bouwlaag en wordt niet van een kelder of kruipruimte voorzien;
- Het bouwpeil is op basis van terreinhoogten door ons aangenomen op ca. NAP +74,0 m;
- Door de opdrachtgever is aangegeven dat uitgegaan wordt van een plaatfundering (dikte ca. 0,2 m) met randbalk welke tevens dienst doet als vorstrand tot ca. 0,8 m- peil.
- Het aanlegniveau van de fundering is door ons geschat op ca. NAP +73,8 m voor de plaat en ca. NAP +73,2 m voor de randbalk;
- Door de opdrachtgever is aangegeven dat de rekenwaarde van de maximale grondspanning 156 kN/m$^2$ bedraagt. Dit betreft de grondspanning ter plaatse van de randbalk met een breedte van 0,4 m. Ter plaatse van de vloervelden komt een maximale grondspanning voor van 100 kN/m$^2$ voor als gevolg van kolommen op de vloer. Wij zijn er ten behoeve van dit rapport vanuit gegaan dat deze spanning optreedt op een oppervlakte van 1,0 x 1,0 m;
- Voor de vloerbelasting is uitgegaan van een vlaklast van maximaal 15 kN/m$^2$;
- In dit rapport is uitgegaan van verticaal en centrische belaste funderingen alsmede een horizontaal maaiveld;
- Eventuele beperkingen of randvoorwaarden als gevolg van milieukundige aspecten zijn buiten beschouwing gelaten.

Indien wordt afgeweken van voornoemde uitgangspunten dan dient ons bureau te worden gecontacteerd daar dan het ontwerpadvies mogelijk moet worden aangepast.

Voor het overige verwijzen wij naar de bestektekeningen van de architect.

## 2.2 Geotechnische uitgangspunten

Gezien de belastingen als gevolg van de nieuwbouw en de te verwachten bodemopbouw is het project door ons bureau conform NEN 9997 ingedeeld in de geotechnische categorie 2 (GC2). Dit betekent dat het terrein- en bodemonderzoek moet worden uitgevoerd volgens hoofdstuk 3.2 van NEN 9997 en een onderzoeksrapport dient te worden overlegd conform hoofdstuk 3.4 van NEN 9997.

Het ontwerp van een funderingsconstructie op staal dient getoetst te worden aan de eisen, betreffende constructieve veiligheid en bruikbaarheid conform hoofdstuk 6 van NEN 9997-1.

# 3 Grondonderzoek

## 3.1 Algemeen

Ten behoeve van het grondonderzoek zijn in augustus 2022 in totaal 5 diepsonderingen en 2 handboringen uitgevoerd. De onderzoeksopzet, zowel qua aantal als locaties, is door de opdrachtgever opgegeven. De locatie van sondering SW05 was door de opdrachtgever aangegeven ter plaatse van de verbindingsgang naar het bestaande gebouw. Op deze locatie was de sondering niet uitvoerbaar, waardoor deze enkele meters is verplaatst. Hierna is het uitgevoerde onderzoek verder beschreven.

## 3.2 Diepsonderingen

De sonderingen zijn genummerd GC200516 SW01 t/m SW05. De diepsonderingen zijn gemaakt met een elektrische conus waarbij de conusweerstand continu wordt gemeten, elektrisch geregistreerd en digitaal vastgelegd. De sonderingen zijn uitgevoerd conform NEN-EN-ISO 22476-1.

Bij de sonderingen is tevens de lokale wrijving gemeten. De continue registratie van de ondervonden bodemweerstand verzekert een gedetailleerd beeld van de bodemopbouw. Dit niet alleen voor wat betreft de sterkte van de bodem maar tevens met betrekking tot de aard van de aanwezige ongeroerde grondlagen.

De verhouding tussen de wrijvingsweerstand van de kleefmantel en de weerstand aan de conuspunt, het zogenaamde wrijvingsgetal, heeft voor iedere grondsoort een andere waarde. Voor een gladde elektrische conus gelden bij veel voorkomende ongeroerde gronden onder de grondwaterstand ongeveer de navolgende relaties:

Tabel 3.1: interpretatie van het wrijvingsgetal

| Wrijvingsgetal in % | Grondsoort |
|---|---|
| 0.3 – 1.5 | Zand, grof tot fijn |
| 1.5 – 2.5 | Silt (leem) |
| 2.5 – 5.0 | Klei |
| > 5.0 | Veen |

Tussen de verschillende grondsoorten komen overgangsvormen voor waardoor de aangegeven grenzen niet als hard zijn te beschouwen. In de elektrische conus bevindt zich een hellingmeter. Hierdoor is controle mogelijk op een eventueel afwijken van de verticaal. Bijzondere afwijkingen zijn niet vastgesteld.

## 3.3 Boring

Om de toplagen nader te verkennen zijn op de locatie tevens twee handboringen (genummerd GC200516 HB01 en HB02) tot ca. 3,2 m- maaiveld uitgevoerd. Handboring HB01 is in de puinhoudende toplaag gestrand. Tijdens de boorwerkzaamheden is het bodemmateriaal lithologisch onderzocht. Bij het lithologisch onderzoek worden de grondsoorten geclassificeerd volgens NEN-EN-ISO14688-1. De boorstaten zijn opgenomen in de bijlagen.

## 3.4 Inmeting

De ligging van de onderzoekspunten is op situatietekening GC200516.T01 weergegeven. De resultaten van het grondonderzoek zijn in de bijlagen toegevoegd. De onderzoekspunten zijn met behulp van 06-GPS ingemeten t.o.v. het Rijksdriehoekstelsel en NAP (nauwkeurigheid ca. 0,10 m). Alle gegevens van de inmetingen zijn een momentopname en zijn alleen te gebruiken voor voorliggend onderzoek.

# 4 Grondslag

## 4.1 Terreingesteldheid

Het terrein is half verhard. Ten tijde van het grondonderzoek lag het maaiveld ter plaatse van de sondeerpunten op een niveau van ca. NAP +74,0 m tot NAP +73,7 m. Het terrein kent hiermee een hoogteverschil van ca. 0,3 m.

## 4.2 Bodemopbouw

De bodemopbouw kan op basis van de sonderingen en boring door middel van het volgende lagensysteem worden beschreven:

Toplaag:
Vanaf maaiveld tot ca. NAP +72,5 m à +72,0 m wordt een heterogene toplaag aangetroffen bestaande uit zand, grind en plaatselijk leem. In deze toplaag variëren de gemeten conusweerstanden van ca. 3 tot meer dan 15 MPa.

Tussenlaag:
Onder de toplaag worden tot ca. NAP +63 m matig vaste leemlagen aangetroffen met conusweerstanden van ca. 1,5 tot 4,0 MPa. In de onderste zone is sprake van kleiige leemlagen.

Onderlaag:
Tenslotte worden tot de maximaal verkende diepte van ca. NAP +54 m matig vaste tot zeer vast gepakte lagen aangetroffen. Dit pakket bestaand uit zand, grind doorsneden door kleiige lagen.

## 4.3 Grondwater

Tijdens het grondonderzoek is in de sondeergaten naar de actuele grondwaterstand gepeild. Deze werd niet aangetroffen tot op een diepte van ca. 15 m- maaiveld. Dit komt overeen met ca. NAP +59 m. Het betreft hierbij slechts een eenmalige meting, waardoor deze waarneming slechts als indicatie kan gelden. Daarnaast kan als gevolg van spanningswater, lagenopbouw en lokale omstandigheden een afwijkende waarde worden aangetroffen.

Wij wijzen erop dat de grondwaterstand van seizoen tot seizoen kan verschillen en in nattere jaargetijden mogelijk hoger wordt aangetroffen dan thans het geval is. Exacte grondwaterstanden kunnen alleen middels peilbuismetingen worden verkregen. De grondwaterstand heeft echter geen invloed op de keuze van het funderingssysteem.

# 5 Ontwerpadvies

Gezien de aard van het project en de aangetroffen bodemopbouw kan de door de constructeur voorgenomen funderingswijze van een fundering op staal middels een betonplaat met randbalk toegepast worden.

Wel zal vanwege de los gepakte en/of geroerde toplagen plaatselijk een grondverbetering moeten worden aangebracht om de zettingen en zettingsverschillen te beperken. Onderstaand is de fundering op staal verder uitgewerkt.

Bij de berekening van de funderingsconstructie als een elastisch ondersteunde ligger, kan gebruik gemaakt worden van een rekenwaarde voor de beddingsconstante van ca. 7 MN/m$^3$ voor de randstroken en ca. 10,0 MN/m$^3$ voor de poeren in het vloerveld. Hierbij is uitgegaan van een spreiding van de belastingen in de vloer conform bijlage 4a. Of en in hoeverre de fundering van wapening moet worden voorzien is ter competentie van de constructeur.

In tabel 5.1 zijn de te hanteren niveaus sec ter plaatse van de sonderingen ten opzichte van NAP gegeven. Indien de door ons gehanteerde uitgangspunten sterk mochten afwijken van de werkelijke, dan gelieve ons te contacteren.

Tabel 5.1: te hanteren niveaus voor de fundering

| Sondering nr. | Maaiveldhoogte [m t.o.v. NAP] | Bouwpeilhoogte [m t.o.v. NAP] | Aanlegniveau [m t.o.v. NAP] | Minimaal ontgravingsniveau [m t.o.v. NAP] |
|---|---|---|---|---|
| SW01 | +73,67 | +74,00 | +73,80 / +73,20[1)] | +73,60 / +73,20[2)] |
| SW02 | +74,00 | +74,00 | +73,80 / +73,20[1)] | +73,60 / +73,20[2)] |
| SW03 | +73,98 | +74,00 | +73,80 / +73,20[1)] | +73,60 / +73,10[2)] |
| SW04 | +73,99 | +74,00 | +73,80 / +73,20[1)] | +72,90 / +72,90[2)] |
| SW05 | +73,67 | +74,00 | +73,80 / +73,20[1)] | +73,60 / +73,20[2)] |

.. [1)] aanlegniveau plaat / randbalk

.. [2)] minimaal ontgravingsniveau plaat / randbalk

In ieder geval zal, indien plaatselijk op de in de tabel aangegeven ontgravingsniveaus nog zeer sterk samendrukbare, humushoudende lagen en/of losse geroerde gedeelten worden aangetroffen, dieper moeten worden ontgraven tot het schone en vastere materiaal wordt gevonden. Bij twijfels of afwijkingen gelieve ons kantoor te waarschuwen.

Waar hoger wordt aangelegd dan het minimale ontgravingsvlak zal een grondverbetering moeten worden aangebracht. Richtlijnen betreffende het aanbrengen van grondverbeteringen worden gegeven in de bijlagen. Het toepassen van een verdiepte aanzet middels schrale beton is niet toegestaan.

Bij bovenstaande wijze van funderen zijn de rekenwaarden voor de draagkracht loodrecht op het funderingsoppervlak gegeven in bijlage 4a (voor de randstroken) en 4b (voor de poeren in het vloerveld). Hierbij is gerekend met een gedraineerde, homogene ondergrond en een permanente gronddekking van 0,5 m voor de randstroken en een dekking van 0,2 m (beton) voor de poeren. Verder is uitgegaan van een lage grondwaterstand.

Teneinde een idee te verkrijgen van de orde van grootte van de zettingen, zijn berekeningen uitgevoerd met behulp van geschatte parameters. De optredende maximale zettingen schatten wij omtrent 10 tot 15 mm. De zettingsverschillen bedragen ca. 50%.

De rekenwaarde van de totale funderingsbelasting dient, na omrekening voor de funderingsbreedte, lager te zijn dan de door ons opgegeven rekenwaarden. Hiermede is aan de uiterste grenstoestand 1A (bezwijken van de funderingsgrondslag) voldaan.

Door de constructeur zal het uiteindelijke funderingsontwerp, op basis van de door ons opgegeven parameters, nog getoetst moeten worden aan de uiterste grenstoestand 1B (maximaal toelaatbare vervormingen in de funderingsconstructie).

# 6 Uitvoering

## 6.1 Ontgravingen

Voor een juiste uitvoering van de funderingswerkzaamheden is het noodzakelijk dat de grondwaterstand tenminste 0,5 meter-het ontgravingsvlak staat. Aangezien er geen grondwater op de betreffende niveaus is aangetroffen, verwachten wij dat er normaliter geen bemaling nodig zal zijn. Wel kan tijdens natte perioden wateroverlast in de bouwput ontstaan als gevolg van regenwater dat zeer traag in de ondergrond wordt opgenomen. Dit stagnerend regenwater kan echter worden afgepompt.

Bij het loodrecht uitgraven van de sleuven en/of de bouwput moet rekening worden gehouden met het inkalven van de wanden als gevolg van de weke en plaatselijk geroerde bovengrond.

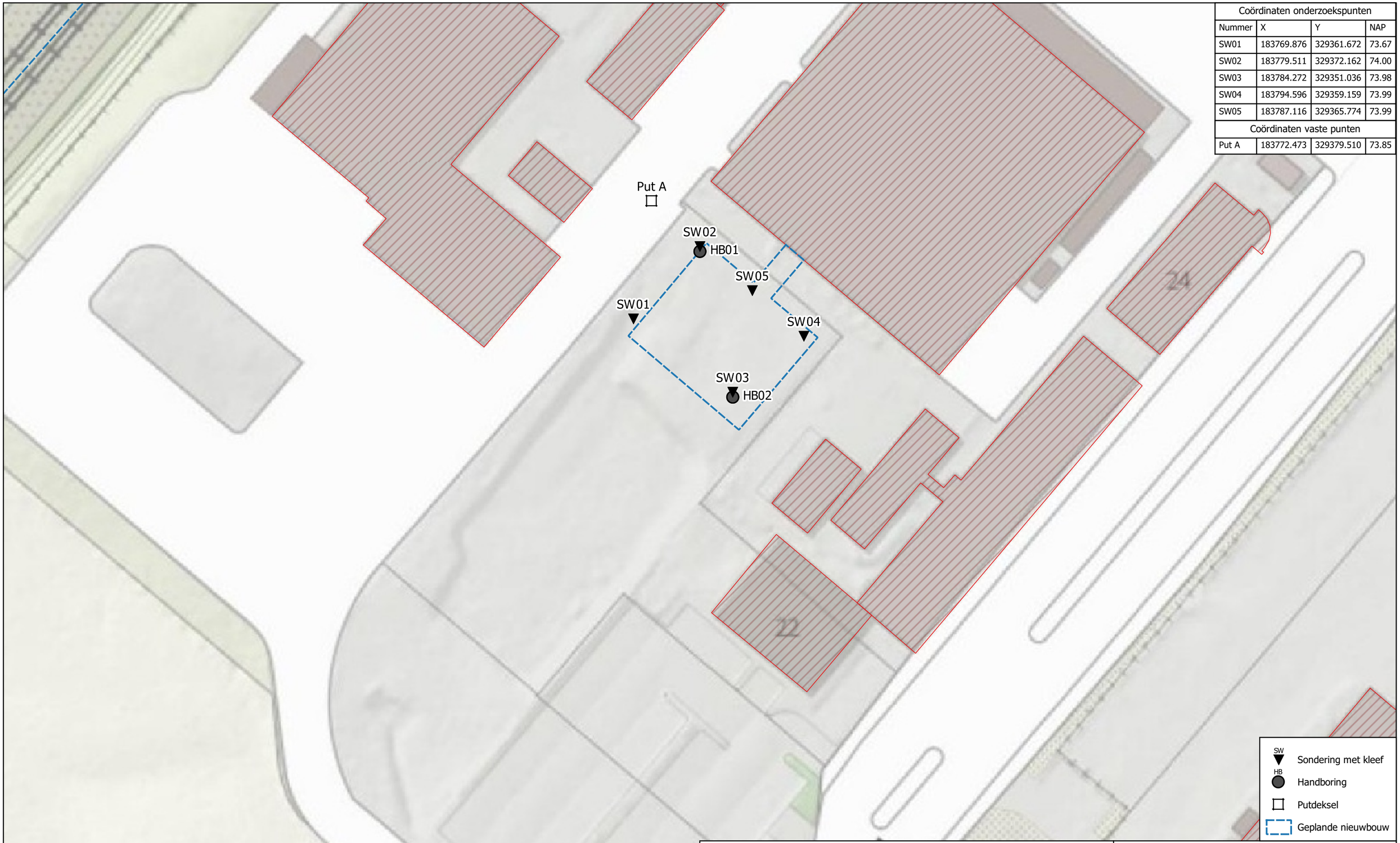
Bij het ontgraven en het aanbrengen van de grondverbetering dient rekening gehouden te worden met de stabiliteit van de fundering van de belendende bebouwing. Het is aanbevelenswaardig om vooraf de aard van de bestaande funderingen (op palen/op staal, aanlegdiepte) vast te stellen middels het graven van enkele (kleine) proefgaten vlak naast deze funderingen. In geen geval mag de gehele fundering worden vrij gegraven. Desgewenst kan ons bureau in dat stadium nader adviseren omtrent de uitvoeringswijze van de nieuwe fundering om stabiliteitsverlies van de bestaande te voorkomen.

Het verdient aanbeveling om het ontgravingsvlak, indien dit althans niet te veel leem- en/of klei bevat, zorgvuldig en in droge toestand af te trillen. Zodoende worden ontgravingsverstoringen teniet gedaan en wordt een zo optimaal mogelijke funderingsgrondslag verkregen.

Bij de ontgravingswerkzaamheden ten behoeve van de funderingen zal het vrijkomend materiaal uit puin, leem, zand, etc. bestaan. Bij eventuele afvoer van de grond van de bouwlocatie zal er rekening moeten worden gehouden dat de benodigde milieukundige verklaringen (b.v. AP04) aanwezig zijn. Indien gewenst kunnen wij dit voor u verzorgen.

# Bijlagen

# Bijlage 1 Situatietekening




| Coördinaten onderzoekspunten | | | |
|---|---|---|---|
| Nummer | X | Y | NAP |
| SW01 | 183769.876 | 329361.672 | 73.67 |
| SW02 | 183779.511 | 329372.162 | 74.00 |
| SW03 | 183784.272 | 329351.036 | 73.98 |
| SW04 | 183794.596 | 329359.159 | 73.99 |
| SW05 | 183787.116 | 329365.774 | 73.99 |
| Coördinaten vaste punten | | | |
| Put A | 183772.473 | 329379.510 | 73.85 |

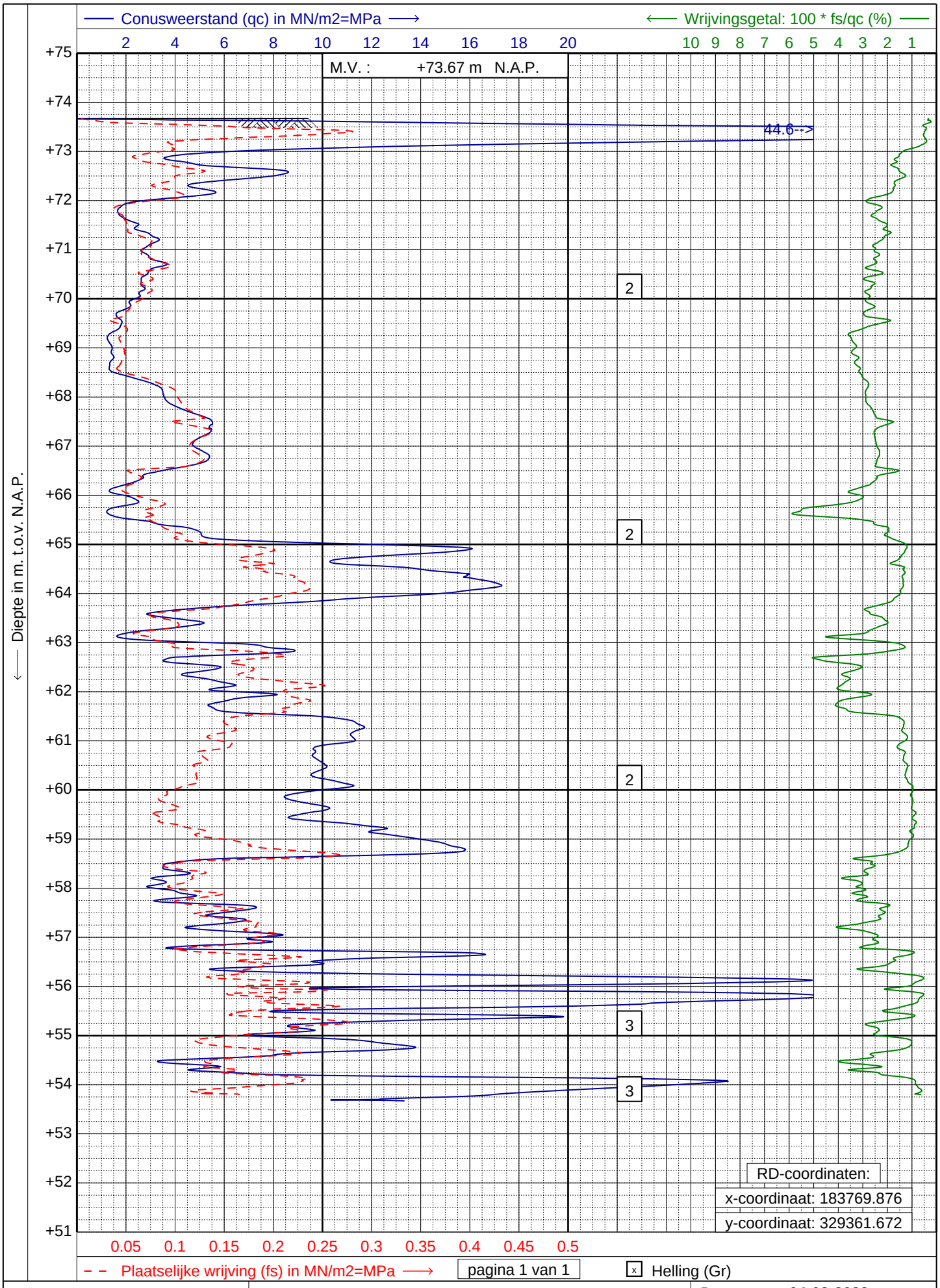
| | | | |
|---|---|---|---|
| Project | Uitbreiding bedrijfspand Celanese | | |
| Locatie | Asselenkuil te Geleen | | |
| Onderdeel | Situatietekening | | |
| Projectnr | GC200516 | Projectleider | M. Vankan |
| Bijlagenr | T01 | Getekend | M. Vankan |
| Datum | 5-8-2022 | Formaat | A3 |

GEONIUS
Geonius Geotechniek
+31 (0) 88 1300 600
De Asselen Kuil 10
6161 RD Geleen
www.geonius.nl

Schaal 1:500

0 5 10 15 20 25 m

# Bijlage 2 Sondeergrafieken

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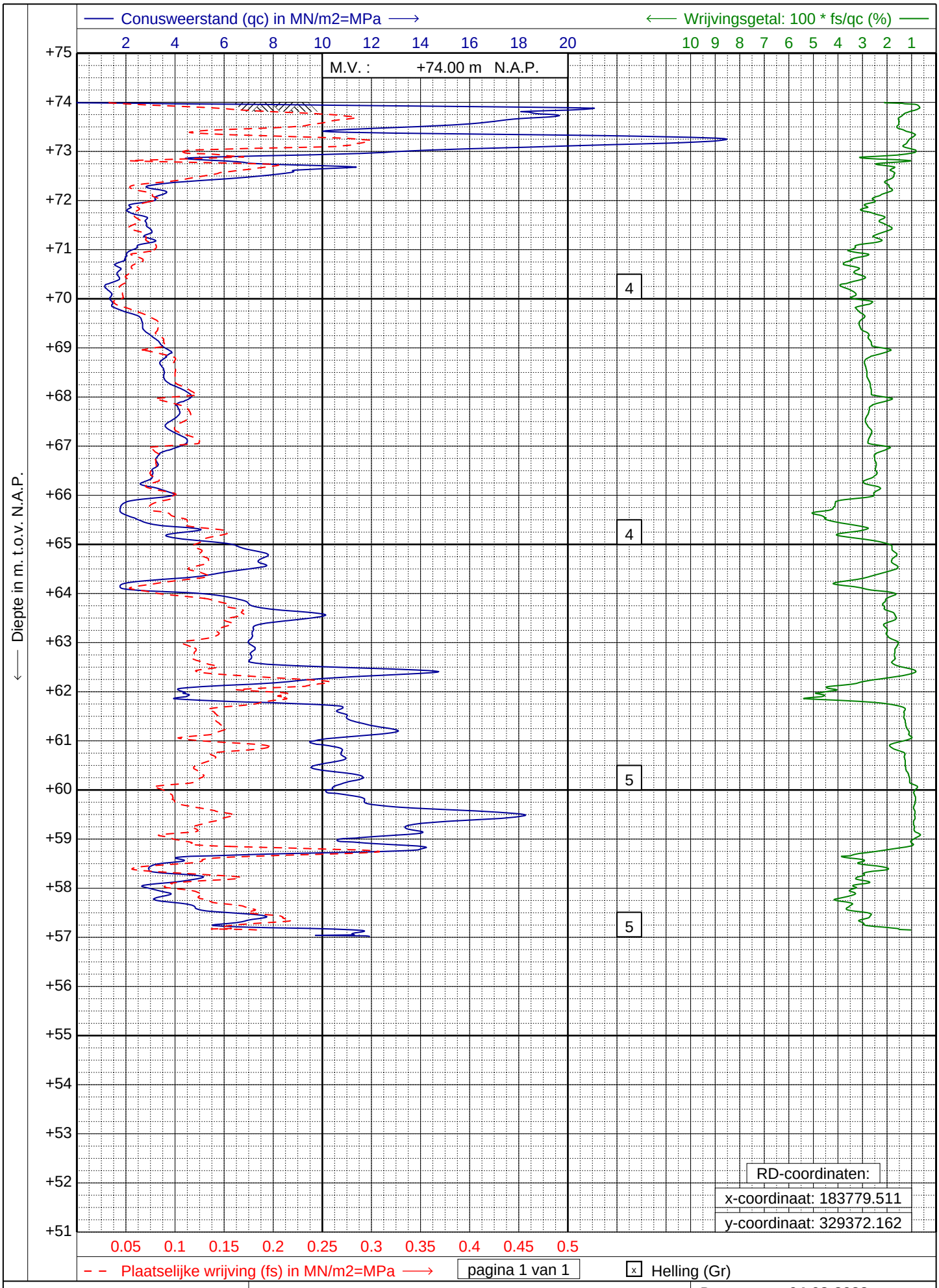
E-mail: info@geonius.nl
Tel.: 088-1300600

Sondering volgens NEN-EN-ISO 22476-1, klasse 2 Type: TE1

Project : **Uitbreiding bedrijfspand Celanese**

Locatie : **Asselenkuil te Geleen**

Datum : **04-08-2022**
Conus : **S15-CFI.1805**
Opdracht : **GC200516**
Sondering : **01**




pagina 1 van 1

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Sondering volgens NEN-EN-ISO 22476-1, klasse 2 Type: TE1

Project : **Uitbreiding bedrijfspand Celanese**

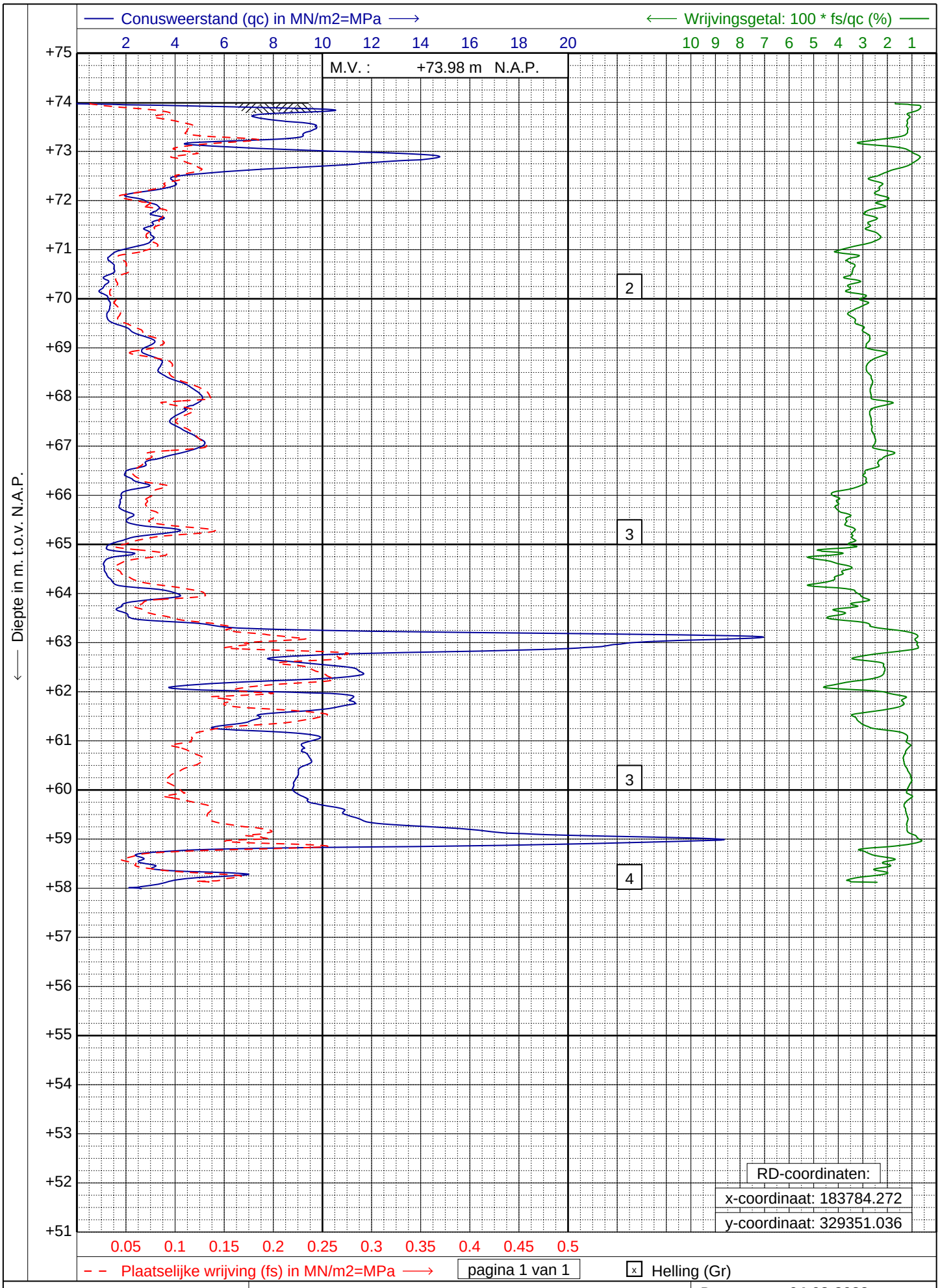
Locatie : **Asselenkuil te Geleen**

Datum : **04-08-2022**

Conus : **S15-CFI.1805**

Opdracht : **GC200516**

Sondering : **02**





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Sondering volgens NEN-EN-ISO 22476-1, klasse 2 Type: TE1

Project : **Uitbreiding bedrijfspand Celanese**

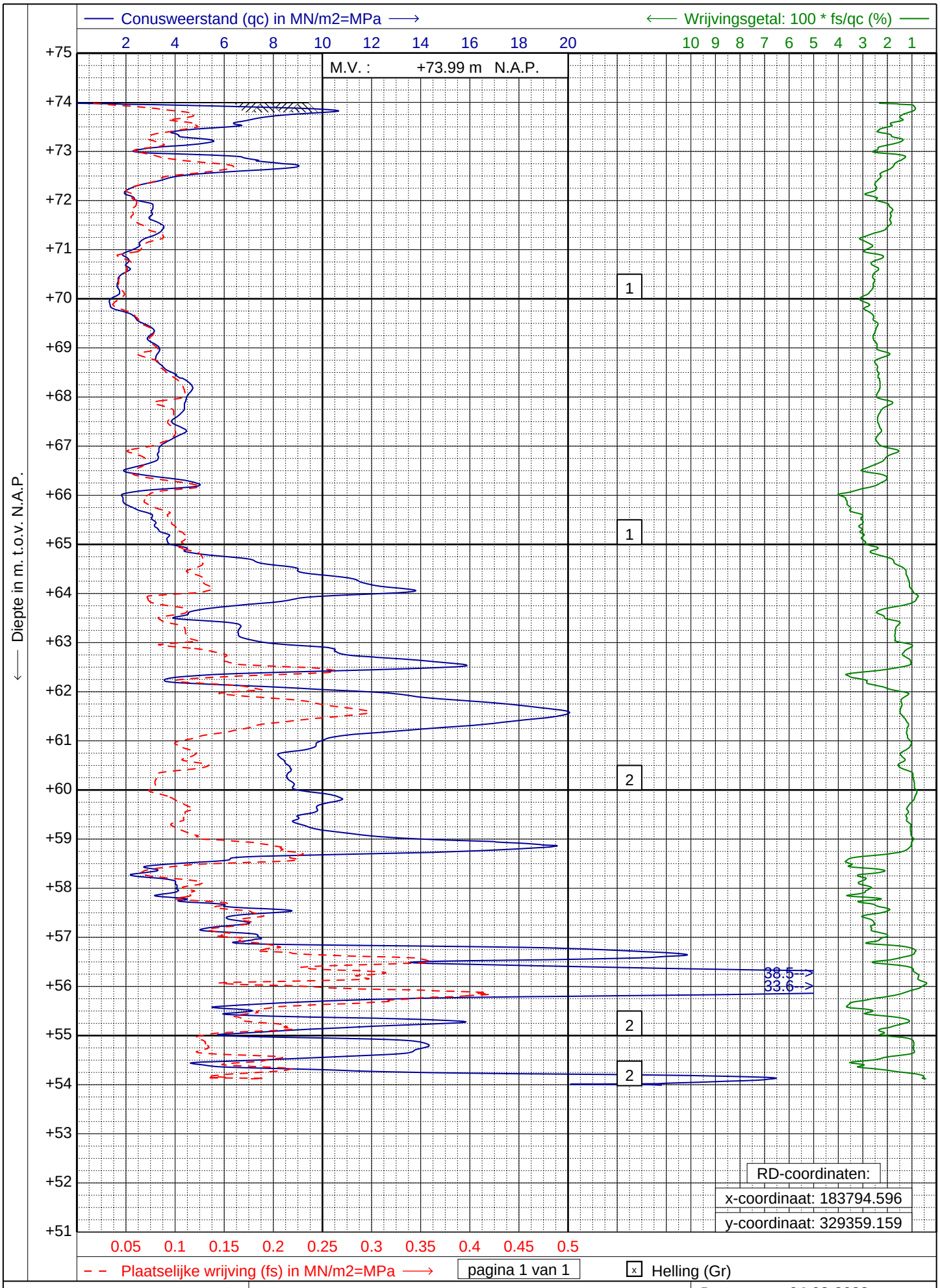
Locatie : **Asselenkuil te Geleen**

Datum : **04-08-2022**

Conus : **S15-CFI.1805**

Opdracht : **GC200516**

Sondering : **03**

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Tel.: 088-1300600

Sondering volgens NEN-EN-ISO 22476-1, klasse 2 Type: TE1

Project : **Uitbreiding bedrijfspand Celanese**

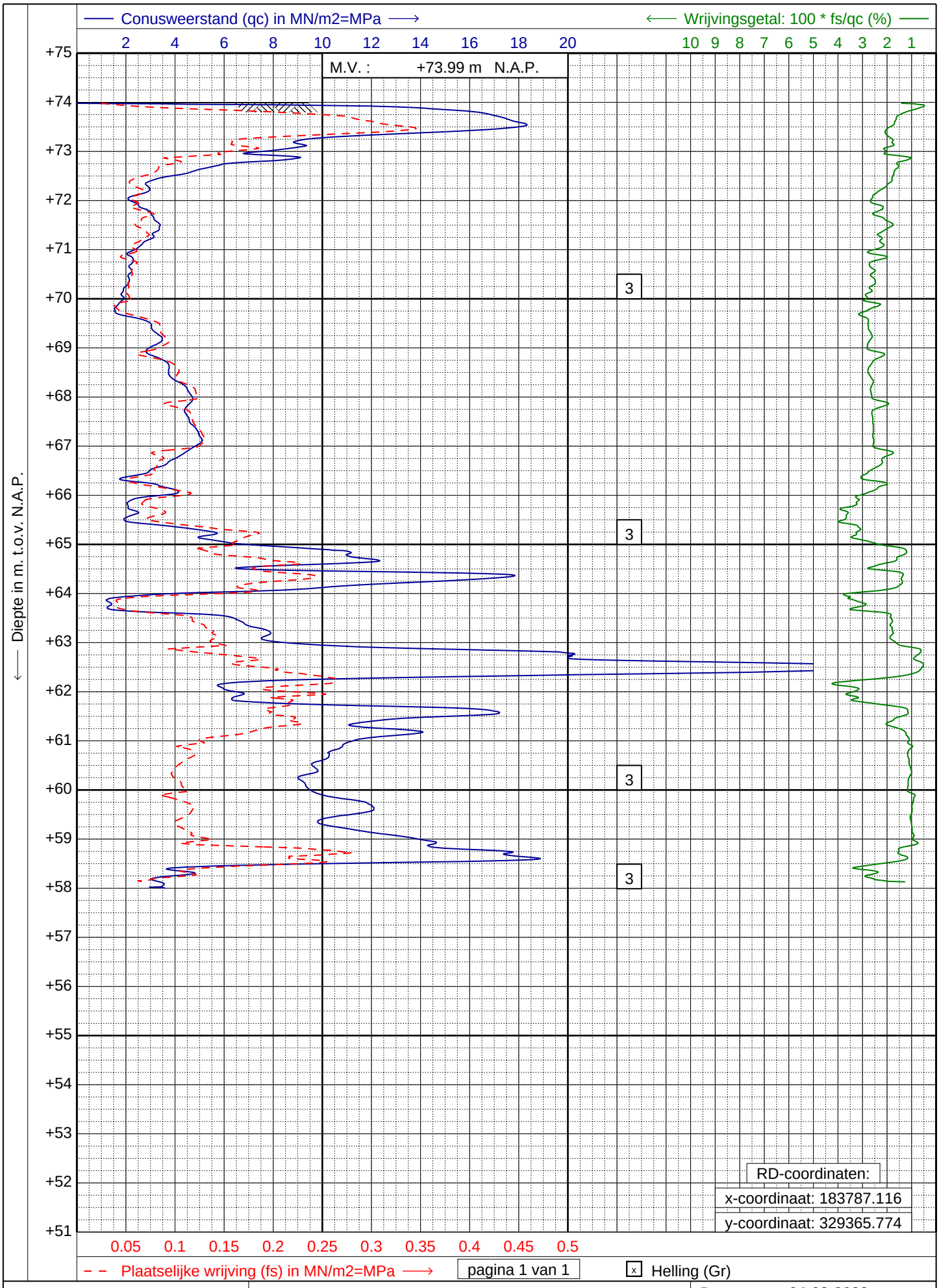
Locatie : **Asselenkuil te Geleen**

Datum : **04-08-2022**

Conus : **S15-CFI.1805**

Opdracht : **GC200516**

Sondering : **04**





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Sondering volgens NEN-EN-ISO 22476-1, klasse 2 Type: TE1

Project : **Uitbreiding bedrijfspand Celanese**

Locatie : **Asselenkuil te Geleen**

Datum : **04-08-2022**

Conus : **S15-CFI.1805**

Opdracht : **GC200516**

Sondering : **05**

# Bijlage 3 Boringen

## Legenda (conform NEN-EN-ISO 14688-1)

### KEIEN (KEITJES)

- KEIEN
- KEIEN, met grind
- KEIEN, met zand
- KEIEN, met silt
- KEIEN, met klei

### GRIND

- GRIND
- GRIND met keien (keitjes)
- GRIND, zwak zandig
- GRIND, sterk zandig
- GRIND, siltig
- GRIND, kleiig

### ZAND

- ZAND
- ZAND, met keien (keitjes)
- ZAND, zwak grindig
- ZAND, sterk grindig
- ZAND, kleiig

### SILT

- SILT, met keien (keitjes)
- SILT, zwak grindig
- SILT, sterk grindig
- SILT, zwak zandig
- SILT, sterk zandig

### KLEI

- KLEI
- KLEI, met keien (keitjes)
- KLEI, zwak grindig
- KLEI, sterk grindig
- KLEI, zwak zandig
- KLEI, sterk zandig

### VEEN (HUMUS, DETRITUS)

- VEEN
- VEEN, zwak zandig
- VEEN, sterk zandig
- VEEN, siltig
- VEEN, kleiig

### geur

- geen geur
- zwakke geur
- matige geur
- sterke geur
- uiterste geur

### olie

- geen olie-water reactie
- zwakke olie-water reactie
- matige olie-water reactie
- sterke olie-water reactie
- uiterste olie-water reactie

### p.i.d.-waarde

- >0
- >1
- >10
- >100
- >1000
- >10000

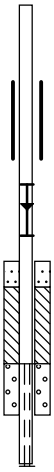
### monsters

- geroerd monster
- ongeroerd monster
- volumering

### overig

- bijzonder bestanddeel
- Gemiddeld hoogste grondwaterstand
- grondwaterstand
- Gemiddeld laagste grondwaterstand

### peilbuis



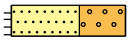
- blinde buis
- casing
- hoogste grondwaterstand
- gemiddelde grondwaterstand
- laagste grondwaterstand
- zand afdichting
- bentoniet/mikoliet/klei afdichting
- grind afdichting
- filter

Projectnummer: GC200516

Projectomschrijving: Uitbreiding bedrijfspand Celanese a/d Asselenkuil te Geleen

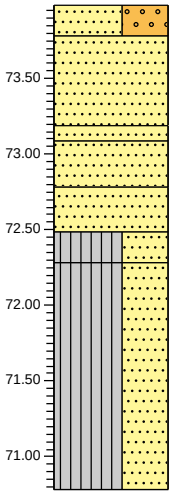
NEN-EN-ISO 14688-1

| | | | |
|---|---|---|---|
| Boring: | HB01 | Boring: | HB02 |
| Maaiveldhoogte: | 73.997 m.t.o.v. N.A.P. | Maaiveldhoogte: | 73.984 m.t.o.v. N.A.P. |
| Datum: | 4-8-2022 | Datum: | 4-8-2022 |
| Opmerking: | T.p.v SW02 | Opmerking: | T.p.v SW03 |



0.00 kiezel

0.20 Zand, middelgrof 420-630, sterk grindig, antropogeen, sterk puinhoudend, matig baksteenhoudend, lichtgrijs, Edelmanboor




0.00 kiezel

0.20 Zand, middelgrof 300-420, sterk grindig, antropogeen, sterk puinhoudend, matig baksteenhoudend, lichtgrijs, Edelmanboor, puinverharding

0.80 Zand, middelgrof 200-300, antropogeen, lichtbruin, Edelmanboor

0.90 Zand, middelgrof 200-300, antropogeen, brokken leem, lichtbruin, Edelmanboor

1.20 Zand, middelgrof 200-300, antropogeen, licht geelbruin, Edelmanboor

1.50 Zand, middelgrof 200-300, antropogeen, lichtgroen, Edelmanboor, week

1.70 Silt, stevig, sterk zandig, antropogeen, standaardgrijs, Edelmanboor

Silt, stevig, sterk zandig, standaardbruin, Edelmanboor

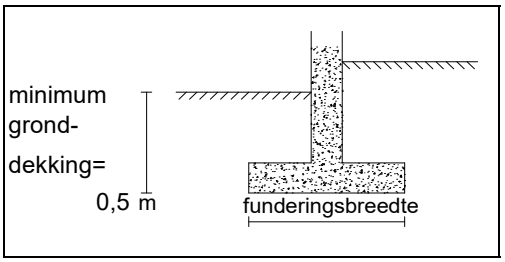
3.20

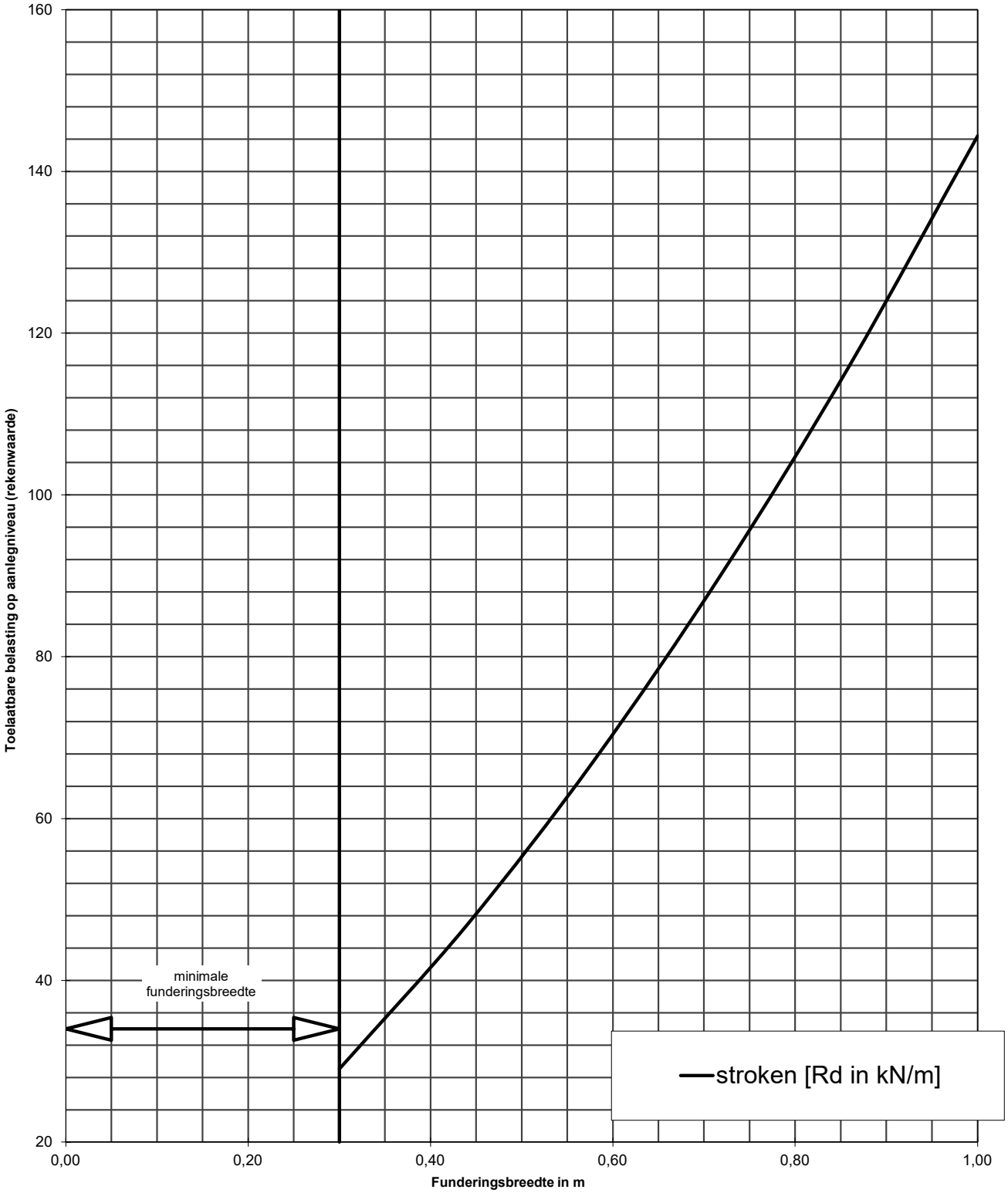
Verticale schaal 1: 50

# Bijlage 4a Funderingsdrukdiagram randbalken

# Rekenwaarde voor de maximaal toelaatbare belasting volgens NEN 9997-1:2016 bij verticaal centrisch belaste funderingen

| | | |
|---|---|---|
| Bijlagenr. | : | GC200516 |
| Project | : | Nieuwbouw bedrijfspand Celenase Geleen |
| Locatie | : | Asselenkuil |
| Grondsoort | : | Leem |
| Volumiek gewicht | : | 17,0 kN/m$^3$ |
| Hoek inw. wrijving | : | 28,0 graden |
| Cohesie | : | 0,0 kN/m$^2$ |





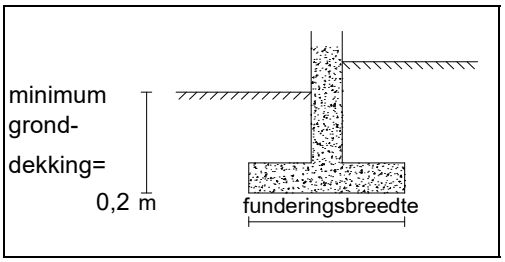
Geonius Geotechniek B.V.
Postbus 1097
6160 BB Geleen

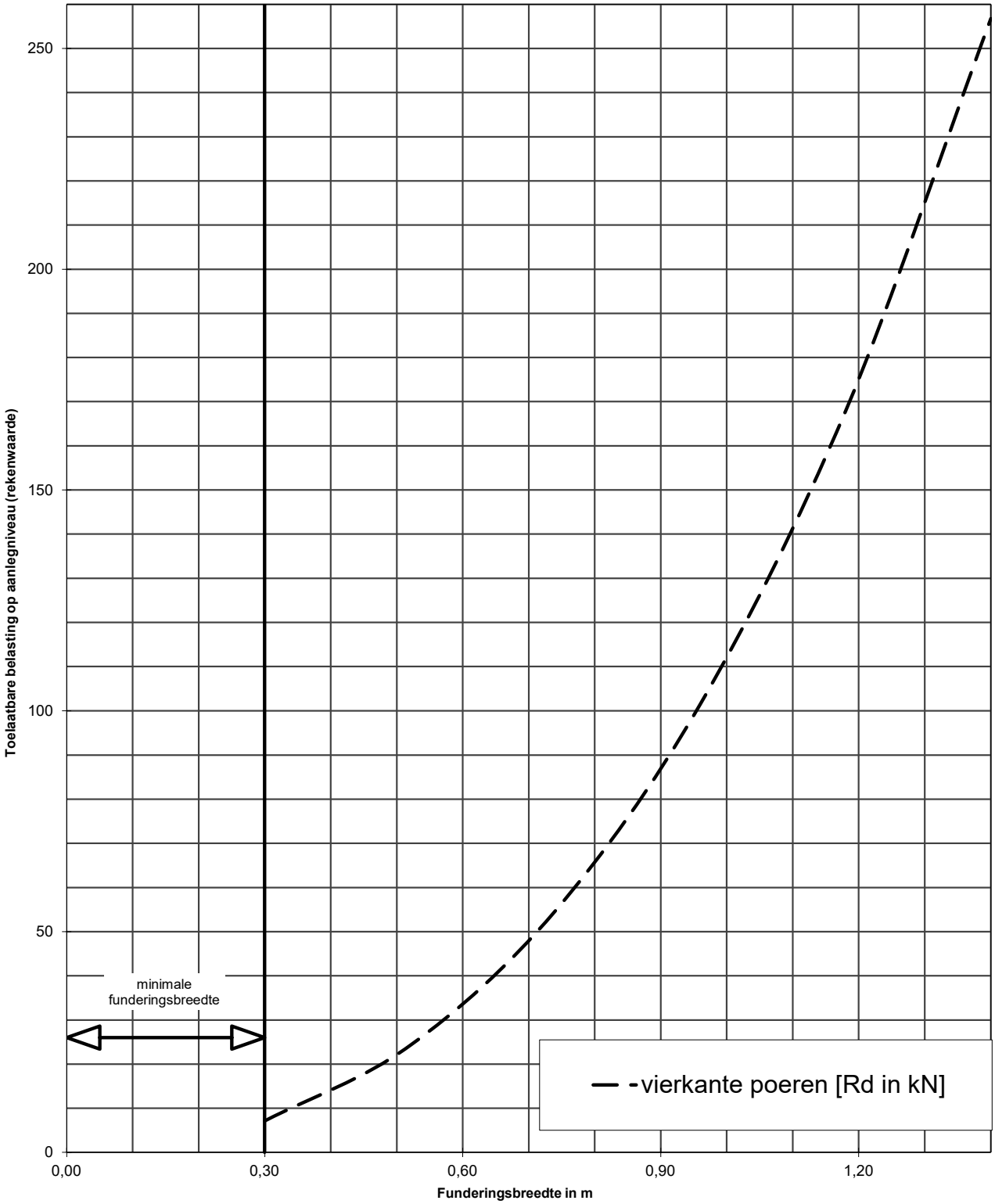
www.geonius.eu
info@geonius.eu
tel.: 088 - 130 06 00
fax.: 088 - 130 06 69

# Bijlage 4b Funderingsdrukdiagram poeren in vloerveld

# Rekenwaarde voor de maximaal toelaatbare belasting volgens NEN 9997-1:2016 bij verticaal centrisch belaste funderingen

| | | |
|---|---|---|
| Bijlagenr. | : | GC200516 |
| Project | : | Nieuwbouw bedrijfspand Celenase Geleen |
| Locatie | : | Asselenkuil |
| Grondsoort | : | Leem |
| Volumiek gewicht | : | 17,0 kN/m$^3$ |
| Hoek inw. wrijving | : | 28,0 graden |
| Cohesie | : | 0,0 kN/m$^2$ |




Geonius Geotechniek B.V.
Postbus 1097
6160 BB Geleen

www.geonius.eu
info@geonius.eu
tel.: 088 - 130 06 00
fax.: 088 - 130 06 69

# Bijlage 5 Richtlijnen uitvoering

# Relevante uitvoeringaspecten

In onderstaande bijlage zijn aspecten opgenomen voor de uitvoering van een grondverbetering/-verdichting en eisen welk gesteld zijn aan het te gebruiken materiaal/materieel en de wijze van controle.

# Te gebruiken materiaal en controle

Onderstaand zijn de eisen omschreven waaraan het materiaal moet voldoen dat voor een grondverbetering wordt gebruikt:

- Het materiaal (van nature aanwezig of aan te voeren) moet bestaan uit schoon, goed gegradeerd en te verdichten zand en/of puingranulaat (korrelverdeling). Verschillende korrelgroottes (fracties) moeten ieder in voldoende mate aanwezig zijn. De korrelvorm is bij voorkeur hoekig;
- De uniformiteitscoëfficiënt [$C_u = D_{60} / D_{10}$ ] dient minimaal 2,0 te bedragen. Hierin is $D_{10}$ de korreldiameter met zeefdoorval van 10 %* en $D_{60}$ de korreldiameter met zeefdoorval van 60 %*;
- De korrelfractie kleiner dan 16 µm mag in het algemeen niet meer bedragen dan 5 %*. Indien minder strenge eisen aan de grondverbetering worden gesteld is een percentage van 10 %* < 63 µm toelaatbaar;
- Het humusgehalte (gehalte organische stof) mag ten hoogste 2 à 3 %* bedragen;
- De curve van de (verzwaarde) proctorproef van het watergehalte versus de maximaal te bereiken (droge) dichtheid dient bij voorkeur een flauw verloop te hebben rond het optimale watergehalte. Hierdoor kan een goede verdichting worden verkregen bij verschillende watergehalten.

* = De genoemde percentages zijn gewichtspercentages

Voordat met de uitvoering wordt begonnen dienen bovenstaande eisen te worden geverifieerd. De controle is erop gericht om aan te tonen dat het gebruikte materiaal qua korrelgrootteverdeling, korrelvorm en verdichtbaarheid voldoet. Dit geldt zowel voor het van nature aanwezige zand als voor eventueel aan te voeren zand. Na een eventuele visuele inspectie waarmee een eerste algehele indruk wordt verkregen, kan het onderzoek geschieden door middel van respectievelijk een zeefanalyse, microscopisch onderzoek en de (verzwaarde) proctorproef.

# Aanbrengen en verdichten grondverbetering

De werkvolgorde van een grondverbetering bestaat normaliter uit een ontgraving, waarna de grondverbetering wordt aangebracht en verdicht. Een grondverbetering kan bestaan uit een uitwisseling van gronden (hoofdzakelijk slappe lagen vervangen door zand/puingranulaat). Of het onder betere condities terugbrengen van natuurlijke gronden, waarbij in de regel sprake is van zeer los gepakt zand. Onderstaande zijn benodigde maatregelen benoemd die bijdragen aan een optimaal resultaat:

- De ontgraving dient met zorgvuldigheid te worden uitgevoerd, waarbij aanwezige obstakels (vegetatieresten, kabels en leidingen, e.d.) en slappe lagen met minimale verstoring worden verwijderd;
- Indien de grondslag uit niet-cohesief materiaal zoals zand of puingranulaat bestaat (met een laag leemgehalte), dient het ontgravingsniveau met een trilplaat te worden afgetrild, voordat de grondverbetering wordt aangebracht. Cohesief materiaal zoals klei/leem/löss kan niet of nauwelijks worden verdicht zonder aanvullende maatregelen en/of toe te passen technieken.
- Voor het verdichten dient de grondwaterstand minimaal ca. 0,5 meter onder het verdichtingsvlak te staan. Indien nodig zal de grondwaterstand verlaagd moeten worden. Bij een hogere grondwaterstand kunnen, afhankelijk van de doorlatendheid van de ondergrond, het te gebruiken materiaal en materieel, drijfzandcondities optreden (liquefaction);
- De aanlegbreedte van de grondverbetering zal zodanig moeten zijn dat een spreiding van de funderingsdrukken mogelijk is onder een hoek van $45^0$ met de horizontaal. Dit vanaf de onderste randen van de fundering tot aan het (geadviseerde) ontgravingsniveau. Daarnaast dient de grondverbetering tenminste over een breedte aanwezig te zijn van 4x de effectieve breedte van de fundering;
- Middels een (verzwaarde) proctorproef kan het optimale watergehalte van het materiaal worden bepaald in relatie tot de hoogst verkregen dichtheid bij een constante hoeveelheid toegevoerde energie. Het watergehalte zal in de regel tijdens het verdichten tussen de ca. 8 en ca. 15 % moeten bedragen. Indien het materiaal óf te nat óf te droog is wordt zelden de vereiste verdichting verkregen.

De grondverbetering dient laagsgewijs te worden opgebouwd. De laagdikte moet in overeenstemming zijn met het toegepaste verdichtingsmaterieel. Het schema in Tabel 1 geeft een globale indicatie bij de toepassing van trilplaten:

Tabel 1: Globale indicatie trilplaat

| Centrifugaalkracht in kN | Gewicht in kg | Laagdikte in meters |
|---|---|---|
| 10 tot 20 | < 100 | 0,2 |
| 25 tot 40 | 150 tot 300 | 0,3 |
| 50 tot 80 | 400 tot 600 | 0,4 |
| > 100 | > 650 | 0,5 tot 0,6 |

Opgemerkt wordt dat de volgens fabrieksspecificatie opgegeven dieptewerking geen maatstaf is voor de toe te passen laagdikte.

Elke laag moet zorgvuldig worden verdicht. Hiervoor zijn minimaal 4 gangen nodig, elkaar kruisend en overlappend. Aangezien de effectiviteit van het trillingsmaterieel zeer snel met de diepte afneemt, moet bij grotere laagdikte rekening worden gehouden met een forse toename van het aantal benodigde gangen. De effectiviteit en daarmee het aantal benodigde gangen is ook afhankelijk van het onderhoud en de slijtage van het materieel.

Wanneer zwaar trillingsmaterieel wordt gebruikt, dient de toplaag nagetrild te worden met een lichte trilplaat, omdat een zware trilplaat of -wals de bovenste laag (ca. 0,15 meter) niet verdicht of losschudt.

# Controle en eisen aan verdichting grondverbetering

Controle op de kwaliteit van de aangebrachte grondverbetering kan geschieden op onderstaande wijze :

- Handsonderingen. Vanwege de beperkte mogelijkheden met betrekking tot de te meten conusweerstand en de te bereiken diepte kan hiermee een zandpakket van maximaal 0,5 à 1,0 m dikte worden gecontroleerd. Het gebruik van een handboring hierbij is noodzakelijk. Deze methode is niet geschikt voor controle van puingranulaat;
- Mechanische (lichte) slagsonderingen. Hierbij kan het volledige grondverbeteringspakket worden gecontroleerd;
- Standaard elektrische sonderingen. Indien de aangebrachte grondverbetering berijdbaar is voor een sondeertruck, kan op deze wijze het volledige pakket worden doorgelicht.
- Plaatdrukproeven. Hiermee wordt een indruk verkregen van de bereikte verdichtingsgraad en het zettingsgedrag van een grondverbeteringspakket en daarmede van de kwaliteit. De werkingsdiepte van de plaatdrukproef bedraagt 1,5 a 2,0 maal de diameter van de plaat. Doorgaans vormt de verhouding tussen, de met de plaatdrukproef bepaalde, Ev2 en Ev1 een maat voor de bereikte verdichtingsgraad. Wanneer de verhouding kleiner is dan 2,0 wordt gesproken over een goed verdicht pakket;
- In-situ-dichtheidsbepalingen. Met behulp van volume-steekringen worden monsters genomen waarvan de dichtheid wordt bepaald. Ook nucleaire dichtheidsmetingen kunnen worden gebruikt.

Bij de controle van de kwaliteit van de aangebrachte grondverbetering worden de volgende kwalitatieve maatstaven gehanteerd:

- Uitgaande van een benodigde (in de berekening gebruikte) effectieve hoek van inwendige wrijving ($\varphi'_k$) van 30 à 35 graden, kan de volgende leidraad worden gevolgd:
    - Bij toepassing van een handsondering met conusoppervlak van 1 $cm^2$, dient de conusweerstand tot een diepte van 40 cm gelijkmatig op te lopen tot 4 $MN/m^2$ of tot een diepte van 30 cm gelijkmatig op te lopen tot 6 $MN/m^2$ en met toenemende diepte niet onder deze waarde terug te vallen. Eén en ander is afhankelijk van de benodigde verdichting en/of aangehouden hoek van inwendige wrijving in de berekeningen;
    - Uitgaande van een lichte slagsonderingen (10 kg) dienen 25 à 30 slagen per 20 cm bereikt te worden tot aan een diepte van 0,6 meter. Hieronder moeten 45 à 50 slagen per 20 cm bereikt worden bij lichte slagsonderingen;
    - Bij gebruik van een standaard elektrische sondering volstaat een gelijkmatige oploop van 1 $MN/m^2$ per 10 cm diepte, waarbij na 1,0 meter de conuswaarde niet onder de 10 $MN/m^2$ terugvalt;
- De dichtheid moet 95 à 98 % bedragen van de maximale dichtheid, zoals bepaald met de proctorproef.

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Geonius is een middelgroot interdisciplinair ingenieursbureau met brede expertise binnen de GWW- en bouwsector. Door onze unieke combinatie van vakkennis op het gebied van wegen, geotechniek, milieu, geodesie, water, ruimtelijke ontwikkeling, landschap, archeologie en ecologie zijn wij goed in staat mee te denken met de klant en projecten zelfstandig uit te voeren. Grenzen tussen de verschillende divisies vervagen, waardoor steeds meer projecten integraal door ons worden uitgevoerd.

Geonius hecht veel waarde aan een informele, positieve bedrijfscultuur, het welzijn van medewerkers en maatschappelijke betrokkenheid.

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- Water
- Ruimtelijke ontwikkeling
- Landschap
- Archeologie
- Ecologie

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